

B.4 Mastrapportage combi-hoekmast HC+0/c

ZUID-WEST 380 KV OOST VERBINDINGEN

Mastrapport combi-hoekmast HC+0/c

TenneT TSO B.V.

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1 INLEIDING

In het basisontwerp van de vakwerkmasten voor de verbinding RLL-TLB380 in het project Zuid-West 380 kV-Oost zijn voor het vaststellen van de haalbaarheid constructieve berekeningen uitgevoerd aan de masten en fundaties. In de Definitief Ontwerpfase, moeten berekeningen verder worden uitgewerkt om te kunnen dienen voor de benodigde vergunningsdocumentatie, voor de aanbesteding en als voorbereiding voor de uitvoeringsfase. Het DO omvat het ontwerp van de mastconstructies, de fundaties en de opstijpunten in de verbinding.

Deze rapportage bevat de resultaten van de toetsing van de combi-hoekmast HC+/c, een masttype geschikt voor twee circuits 380 kV. De toetsing bestaat uit controle van:

- de profielen en boutverbindingen onderdeel van de hoofd draagconstructie
- de knikverkorters
- de liggers voor de isolator kettingen
- de verbinding met de fundatie via blokdeuvels
- aanvullende controle op sterkte-coördinatie
- galloping

Buiten de scope van dit DO-rapport valt de controle van de schetsplaten en overige verbinding details in de constructie. Dit moet in de UO-fase worden uitgewerkt. Ook de voorzieningen voor de high-step rail en bordessen vallen onder uitwerking in UO-fase.

In hoofdstuk 2 zijn de uitgangspunten en randvoorwaarden vanuit de van toepassing zijnde normen en TenneT-specificaties opgenomen. Hoofdstuk 3 beschrijft de gevolgde aanpak van de berekening. In hoofdstuk 4 is de toetsing opgenomen.

2 UITGANGSPUNTEN EN RANDVOORWAARDEN

2.1 Normen

Er is gebruik gemaakt van de normen volgens Tabel 1.

Tabel 1 Gebruikgemaakte normen, voorschriften en richtlijnen

| Norm | Titel |
|--|--|
| NEN-EN 50341-1:2013 | “Overhead electrical lines exceeding AC 1 kV - Part 1: General requirements – Common” |
| NEN-EN 50341-2-15:2019 | “Overhead electrical lines exceeding AC 1 kV Part 2 National Normative Aspects (NNA) for THE NETHERLANDS” |
| NEN-EN 1990+A1+A1/C2:2019/NB:2019nl | “Grondslagen van het ontwerp” |
| NEN-EN 1991-1-4+A1+C2:2011/NB:2019+C1:2020 | “Deel 1-4: Windbelasting op constructies” |
| NEN-EN 1992-1-1+C2:2011/NB:2016+A1:2020 | “Eurocode 2: Ontwerp en berekening van betonconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-1-1+C2+A1:2016 nl | “Eurocode 3: Ontwerp en berekening van staalconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-3-1:2007/NB:2011 nl | “Deel 3-1: Torens, masten en schoorstenen - Torens en masten” |
| NEN-EN 1993-1-8+C2:2011/NB:2011 nl | “Ontwerp en berekening van staalconstructies, deel 1-8: ontwerp en berekening van verbindingen” |

2.2 TenneT-specificaties

In Tabel 2 zijn de documenten opgenomen die relevant zijn voor de berekeningen en toetsingen die binnen dit project in de mastrapportage uitgevoerd zullen worden.

Tabel 2 Relevante documenten t.b.v. mechanische rapportages

| Nummer | Onderwerp |
|-----------------|-------------------------------------|
| PVE.05.000 v3.2 | PvE Lijnen |
| sPVE.05.001 | sPvE Lijnen |
| SPE.05.346 v1.3 | Algemene specificatie stalen masten |

2.3 Eisenverificatie

Voor de eisenverificatie wordt verwezen naar het rapport “Verificatierapport eisen DO Moldau”, DNV GL rapport 21-0451, Meridiannummer 002.678.00 0910757.

2.4 Ontwerppapporten

Voor de achtergrond van het ontwerp wordt verwezen naar het uitgangspuntenrapport “Uitgangspunten definitief ontwerp Moldaumast”, DNV GL rapport 21-0036, Meridiannummer 002.678.00 0876917.

2.5 Materialen

Voor het ontwerp van de mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 3.

Tabel 3 Materialen aangepaste constructie

| | |
|----------------|---|
| Staalsoort | S355J0 (t≤16 mm) S355J2 (16<t≤40 mm) |
| Boutkwaliteit | 8.8 gerolde draad |
| Betonkwaliteit | C30/37 |
| Wapeningsstaal | B500 |



Voor de constructie geldt conform TenneT-specificatie:

- Toe te passen bouten: M16/M20/M24;
- Voor hoekstaal is de minimale afmeting L50x5 mm;
- Minimale plaatdikte 6 mm.

Mocht het noodzakelijk zijn M30 toe te passen, bij grote plaatdiktes is dit als afwijking door TenneT toegestaan.

2.6 Software

De gebruikte software wordt benoemd in Tabel 4.

Tabel 4 Toegepaste software

| Software | | Versie |
|-----------------------|-----------|--------|
| Mastontwerp | PLS-CADD | 16.65 |
| Mastberekeningen | PLS-TOWER | 16.65 |
| Constructieve analyse | AxisVM | X5 R4h |

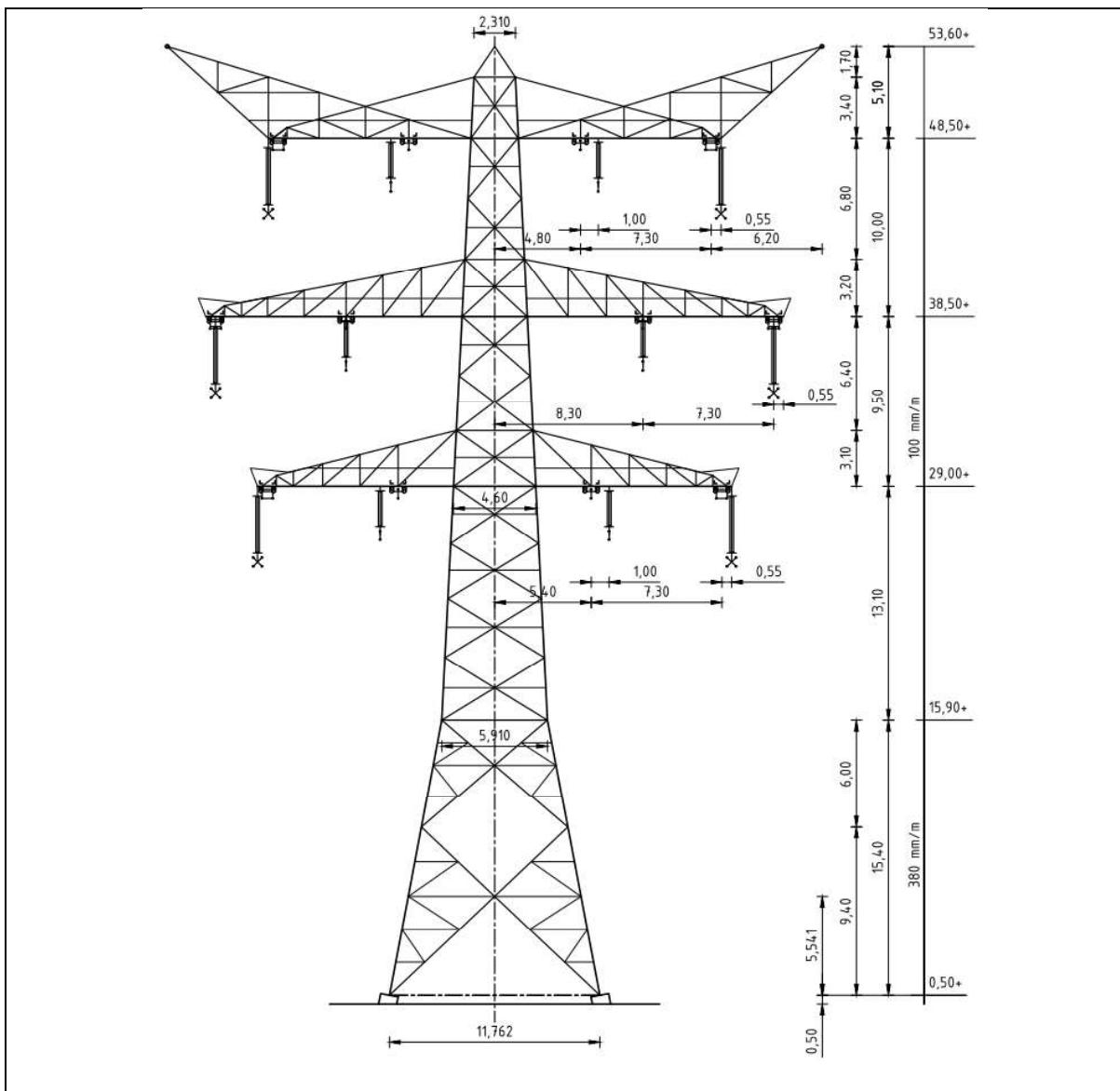
3 MASTONTWERP

3.1 Mastbeeld

In dit hoofdstuk wordt het mastbeeld weergegeven met de belangrijkste maatvoering, voor de tekening van het masttype met volledige maatvoering en aanzichten wordt verwezen naar onderstaande tekeningen:

- Mastbeeldtekening, Meridiannummer 002.678.00 0890099
- Overzichtstekening HC+0/c, Meridiannummer 002.678.00 0927484

Masttype HC+0/c is een combi-hoekmast voor twee circuits 380 kV en twee circuits 150kV. De belastingen grijpen als trekkrachten aan via de afspankettingen. Onder de traverse bevinden zich verticale post-isolatoren die de bretellebogen fixeren.



Figuur 1 Mastbeeld masttype HC+0/c

3.2 Uitgangspunten berekening

De uitgangspunten volgens Tabel 5 zijn van toepassing.

Tabel 5 Uitgangspunten

| | |
|-----------------------------|-----------------------|
| Norm | NEN-EN50341-2-15:2019 |
| Gevolgklasse initieel | CC2 |
| Betrouwbaarheidsniveau | Nieuwbouw |
| Referentieperiode | 50 jaar |
| Windgebied | III |
| Windsnelheid (m/s) | 24,5 |
| Terreincategorie | II |
| Reductiefactor c_{dir} | 1,00 |
| IJsg gebied fasegeleider | B |
| IJsg gebied bliksemgeleider | A |

3.3 Mastenlijst

De mastenlijst is gebaseerd op de “staking table” van het DO-uitgangspuntenrapport en benaamd als “VKA 1.1 Concept 20201112 1037-1044_1086-1094_1099-1105_1192-1204.xlsx”. De mastenlijst is vanwege lopende traceringsvraagstukken aan verandering onderhevig en is derhalve indicatief.

In Tabel 6 zijn alle masten in het tracé van het type HC+0/c opgenomen. De mast met grootste wind span is vetgedrukt aangegeven. Het masttype zal niet met deze wind en weight span worden berekend maar met generieke wind en weight span, zie uitgangspuntenrapport.

Tabel 6 Mastenlijst HC+0/c

| Mast-nummer | Masttype | Lijnhoek (°) | Wind span (m) | Weight span (m) | Hoogteverschil ba+ah (m) | Hoogteverschil back (m) | Hoogteverschil ahead (m) |
|-------------|----------|--------------|---------------|-----------------|--------------------------|-------------------------|--------------------------|
| 1131 | HC+0_c | 134.1 | 265.3 | 260.4 | -0.8 | -0.7 | -0.1 |
| 1133 | HC+0_c | 129.3 | 309.8 | 310.1 | 0.0 | 0.1 | -0.1 |
| 1159 | HC+0_c | 139.3 | 380.5 | 363.7 | -3.7 | -0.3 | -3.4 |
| 1187 | HC+0_c | 129.2 | 384.3 | 369.4 | -3.2 | -2.5 | -0.6 |

3.4 Geleiderbelastingen

De berekening is uitgevoerd met het geleiderbelastingprogramma van DNV GL. De belastingen op de mastconstructie zijn bepaald op basis van de modellering in PLS-TOWER (staafoppervlaktes). Voor de toeslagen op eigen gewicht en windoppervlakte wordt verwezen naar het uitgangspuntenrapport. In Appendix A zijn de resultaten van de geleiderbelastingen samengevat. Masttype HC+0 wordt berekend met minimale en maximale lijnhoek 120° en 140° voor dit type.

3.5 Reacties op de fundering

De oplegreacties op de fundering worden ontleend aan de uitvoer van het geleiderbelastingprogramma. Zie Appendix A.

3.6 Modelling

Op basis van de ontwerptekeningen is de mast in PLS-TOWER ingevoerd. De toetsing wordt per staafgroep uitgevoerd. De hoofdelementen zijn gemodelleerd, niet-dragende profielen als knikverkorters zijn weggelaten, deze worden separaat getoetst. De profielen zijn in PLS-TOWER inclusief de boutverbindingen ingevoerd en getoetst, de controle van de schetsplaten en andere detailverbindingen valt buiten de scope.

De geleiderbelastingen vanuit het geleiderbelastingenprogramma zijn als invoer voor de belastingen gebruikt.

De gewichts- en windbelasting op de mastconstructie wordt door PLS-TOWER automatisch bepaald. Via toeslagfactoren wordt de invloed van niet gemodelleerde elementen als knikverkorters, bordesconstructies en klimvoorzieningen meegenomen. Voor schetsplaten, zinklaag en bouten is een aanvullende toeslag op het gewicht van 20% toeslag gerekend.

Diagonalen in voor- en achtervlak respectievelijk de twee zijvlakken zijn samengenomen in een groep.

3.7 Overige controles

In PLS-TOWER zijn niet alle elementen getoetst. Knikverkortersprofielen en overige profielen voor beloopbaarheid worden separaat getoetst. In Appendix C is dit opgenomen. De verbinding met de fundatie bestaat uit ingestorte profielen voorzien van blokdeuvels. Dit is in Appendix D opgenomen. De liggers van isolatorkettingen vereisen een aanvullende controle op buiging. De toetsing is uitgevoerd met de software AxisVM en is beschreven in Appendix E. Appendix F omvat de toetsing op sterkte-coördinatie. Voor hoekmasten moet een toetsing op vermoeiing worden uitgevoerd voor galloping. Dit is in Appendix G opgenomen.

De mastranden uitgevoerd als XEA-profielen worden separaat op torsieknik gecontroleerd. Dit is in Appendix B opgenomen. De berekende capaciteit die lager is dan de capaciteit voor buigingsknik is in PLS-TOWER via aangepaste buckling-ratio ingevoerd.

3.8 Mastgewicht

Het totale mastgewicht per masttype is met de uitgangspunten van paragraaf 3.6 bepaald op:

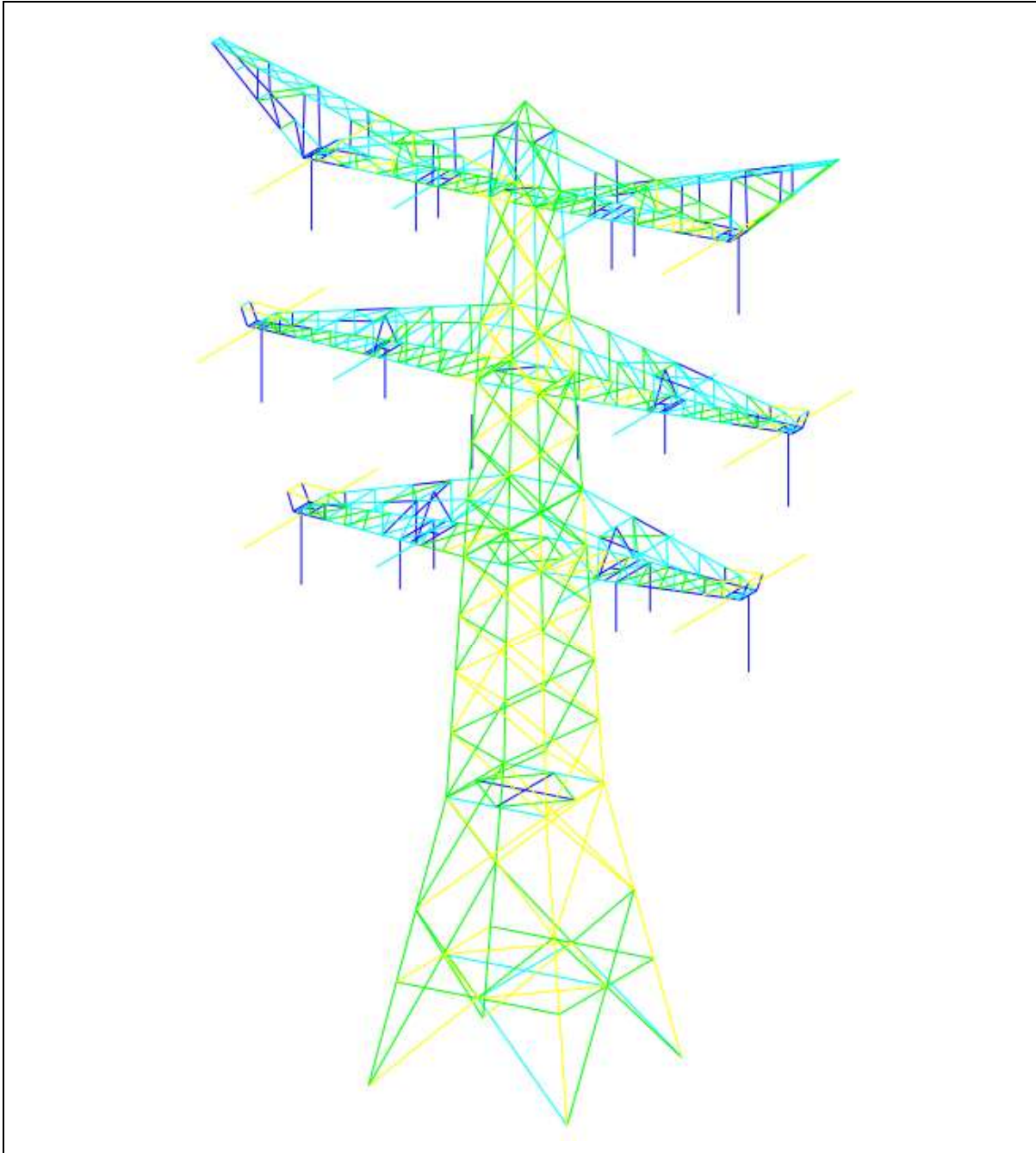
- Masttype HC+0/c 104,1 t

4 TOETSING

4.1 Resultaat PLS-TOWER

Het resultaat van de toetsing met PLS-TOWER is weergegeven in Figuur 2. De belastingen zijn bepaald voor het masttype HC+0/c, inclusief bouwphase en afspannen.

De uitnutting van de constructie loopt op van blauw (0-25%) tot geel (75-100%). Uit de figuur wordt geconcludeerd dat alle profielen en boutverbindingen voldoen.



Figuur 2 Resultaat PLS-TOWER voor masttype HC+0/c

4.2 Toetsing overige onderdelen

In Tabel 7 zijn de resultaten van de uitgevoerde toetsingen weergegeven.

Tabel 7 Samenvatting uitgevoerde controles

| Controle van | Beoordeling | Referentie |
|-----------------------|-------------|------------------------|
| Profielen | Voldoen | Figuur 2 Appendix B |
| Knikverkorters | Voldoen | Appendix C |
| Blokdeuvels randstijl | Voldoen | Appendix D |
| Liggers | Voldoen | Appendix E |
| Sterkte-coördinatie | Voldoet | Appendix F |
| Galloping | Voldoet | Appendix G |

APPENDIX A

Geleiderbelastingen

Geleiderbelastingen opgenomen:

- Masttype HC+0/c – 120gr
- Masttype HC+0/c – 140gr
- Masttype HC+0/c – bouwfase
- Masttype HC+0/c – Afspannen

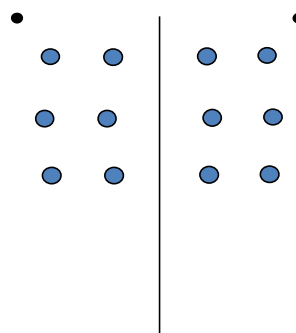
Project: RLL-TLB380
 Tower: HC+0_c - 120gr
 Number: 1187

Auteur: TBR
 Versie: v12.0

Geleiderbelastingen

Algemeen

Benaming HC+0_c - 120gr
 Masttype Hoekmast
 Aantal circuits 4
 Configuratie 4-circuit-dubbel verticaal
 Aantal bliksemgeleiders 2



Uitgangspunten

Norm NEN-EN50341-2-15:2019
 Gevolgklasse initieel CC2
 Betrouwbaarheidsniveau initieel Nieuwbouw
 Referentieperiode initieel 50 jaar
 CC2
 Betrouwbaarheidsniveau na aanpassing n.v.t.
 50 jaar
 Windgebied III
 Windsnelheid (m/s) 24,5 m/s
 Terreincategorie II
 Reductiefactor C_{dir} 1,00
 IJsg gebied fasegeleider B
 IJsg gebied bliksemgeleider A

Geleiders Back

| Omschrijving | Spanning | Geleider Back | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden P_{back} |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 2 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 3 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Circuit 4 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Bliksemdraad 1 | | AACSR 241-AL3-39-A20SA | 1 | A | 2 % | 2 % | 1800 |
| Bliksemdraad 2 | | OPGW AFL-226/38 | 1 | A | 2 % | 2 % | 1800 |

Geleiders Ahead

| Omschrijving | Spanning | Geleider Ahead | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden P_{ahead} |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 2 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 3 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Circuit 4 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Bliksemdraad 1 | | AACSR 241-AL3-39-A20SA | 1 | A | 2 % | 2 % | 1800 |
| Bliksemdraad 2 | | OPGW AFL-226/38 | 1 | A | 2 % | 2 % | 1800 |

Isolatoren (1)

| Omschrijving | Ophanging | Gewicht [kN] | Lengte [m] | Windopp. [m ²] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1 | Afspanketting | 3,00 | 6,50 | 1,10 |
| Circuit 2 | Afspanketting | 3,00 | 6,50 | 1,10 |
| Circuit 3 | Afspanketting | 2,00 | 4,50 | 0,80 |
| Circuit 4 | Afspanketting | 2,00 | 4,50 | 0,80 |
| Bliksemdraad 1 | Afspanketting | 0,10 | 0,20 | 0,10 |
| Bliksemdraad 2 | Afspanketting | 0,10 | 0,20 | 0,10 |

1. Eigenschappen gelden voor geheel van de isolatorset

Ophanghoogte en positie in mast

| Circuits | Aanduiding | Nummer | Ophanghoogte | Aangrijppunt | Positie in mast Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1 | 10 | 380ct1f1 | 48,0 m | 48,0 m | -12,1 m |
| Circuit 1 | 11 | 380ct1f2 | 38,0 m | 38,0 m | -15,6 m |
| Circuit 1 | 12 | 380ct1f3 | 28,5 m | 28,5 m | -12,7 m |
| Circuit 2 | 40 | 380ct2f1 | 48,0 m | 48,0 m | 12,1 m |
| Circuit 2 | 41 | 380ct2f2 | 38,0 m | 38,0 m | 15,6 m |
| Circuit 2 | 42 | 380ct2f3 | 28,5 m | 28,5 m | 12,7 m |
| Circuit 3 | 20 | 150ct3f1 | 48,0 m | 48,0 m | -4,8 m |
| Circuit 3 | 21 | 150ct3f2 | 38,0 m | 38,0 m | -8,3 m |
| Circuit 3 | 22 | 150ct3f3 | 28,5 m | 28,5 m | -5,4 m |
| Circuit 4 | 30 | 150ct4f1 | 48,0 m | 48,0 m | 4,8 m |
| Circuit 4 | 31 | 150ct4f2 | 38,0 m | 38,0 m | 8,3 m |
| Circuit 4 | 32 | 150ct4f3 | 28,5 m | 28,5 m | 5,4 m |
| Bliksemdraad 1 | 1 | bl1 | 53,1 m | 53,1 m | -18,3 m |
| Bliksemdraad 2 | 3 | bl2 | 53,1 m | 53,1 m | 18,3 m |

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Hoogteaanpassing naastgelegen masten (aanpassing wind- en weight span)

| | Back | Ahead | |
|--------------------------------------|--------|--------|---|
| Verhoging voor windbelasting | 18,0 m | 6,0 m | (positief: omhoog) |
| Verlaging voor verticale belasting | -9,0 m | -9,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging: Niet in 0,9EG-combinaties | | | |

Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting

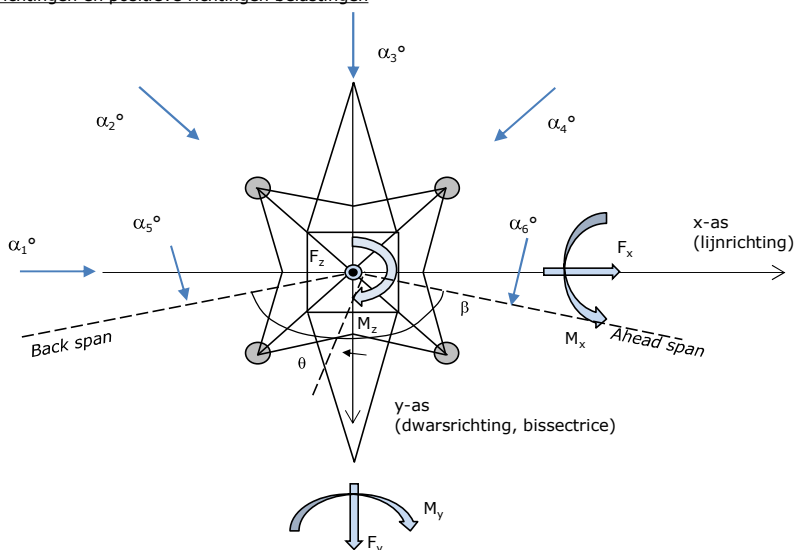
| Circuits | Aanduiding | Nummer | Hoogteverschil | | Richtingsverandering | |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
| | | | Δh back | Δh ahead | Δy back | Δy ahead |
| Circuit 1 | 10 | 380ct1f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 1 | 11 | 380ct1f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 1 | 12 | 380ct1f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 40 | 380ct2f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 41 | 380ct2f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 42 | 380ct2f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 3 | 20 | 150ct3f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 3 | 21 | 150ct3f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 3 | 22 | 150ct3f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 30 | 150ct4f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 31 | 150ct4f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 32 | 150ct4f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Bliksemdraad 1 | 1 | bl1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Bliksemdraad 2 | 3 | bl2 | 0,0 | 0,0 m | 0,0 | 0,0 m |

Lijn- en mastgegevens

| | Back | Ahead |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0 | 400,0 m |
| Lijnhoek β | 120 ° | |
| Rotatie mast t.o.v. bissectrice θ | 0 ° | |
| Vaklengte | 400 | 400 m |
| Hoogte onderkant mast t.o.v. maaiveld | 0,5 m | |
| Beschouwde windrichtingen | α_1 | 0 ° |
| Windrichtingen volgens: | α_2 | 45 ° |
| Geleiderbelastingen | α_3 | 90 ° |
| | α_4 | 135 ° |
| | α_5 | 60 ° |
| | α_6 | 120 ° |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



Beschouwd aantal windrichtingen

| | |
|--------|---|
| 1a | 6 |
| 3 | 6 |
| 4 | 1 |
| 6 | 1 |
| Overig | 1 |

Project: RLL-TLB380
 Tower: HC+0_c - 120gr
 Number: 1187

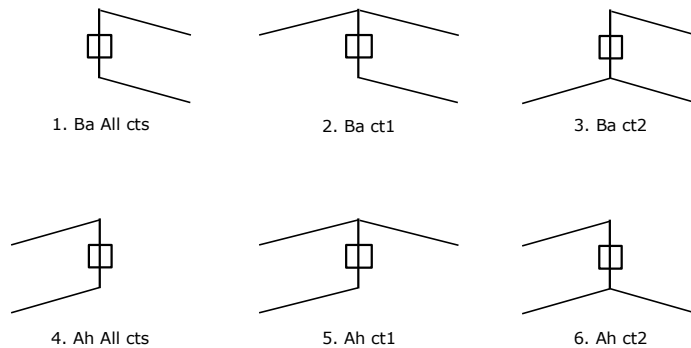
Geleiderafval

| | | SPLS - torsie | | SPLS - Enkelzijdige trek | | 5a - geleiderbreuk | |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
| | | Aanw. | Afw. | Aanw. | Afw. | Aanw. | Afw. |
| Circuit 1 | 380ct1f1 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 1 | 380ct1f2 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 1 | 380ct1f3 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 2 | 380ct2f1 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 2 | 380ct2f2 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 2 | 380ct2f3 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 3 | 150ct3f1 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 3 | 150ct3f2 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 3 | 150ct3f3 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 4 | 150ct4f1 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 4 | 150ct4f2 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 4 | 150ct4f3 | 0 | 1 | 1 | 0 | 1 | 0 |
| Bliksemdraad 1 | b11 | 1 | 0 | 1 | 0 | 1 | 0 |
| Bliksemdraad 2 | b12 | 0 | 1 | 1 | 0 | 1 | 0 |

Belastingssituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

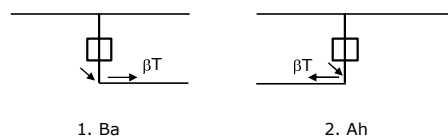
Principe belastingssituaties:



Belastingssituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



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Belastingsituaties 6. Bouw- en onderhoud

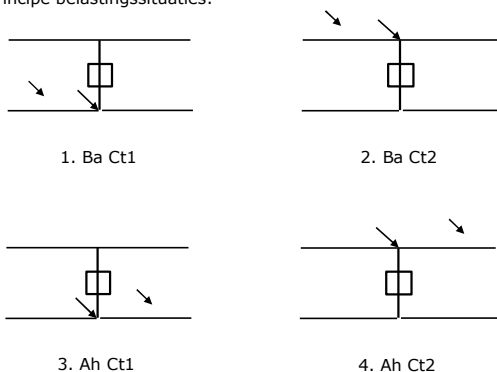
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

| | Fase | Bliksem |
|----------------------|--------|---------|
| Lijnwagen | 4,0 kN | 2,0 kN |
| Puntlast op traverse | 1,0 kN | 1,0 kN |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



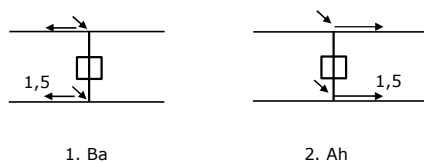
Belastingsituaties 8. Lijndansen als statische belasting

| Geleider | | |
|--------------------------|---------|-------|
| Steunmast fase | 0,866 W | 1,5 W |
| Steunmast bliksem | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingsspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

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Mastconstructie

Eigenschappen

| | |
|-----------------------------|----------------|
| Masttype | Hoekmast |
| Mastbenaming | HC+0_c - 120gr |
| Voetplaat t.o.v. maaiveld | 0,5 m |
| Masthoogte t.o.v. voetplaat | 53,1 m |
| Gewicht mast | 1021,2 kN |

| | | |
|---|-------|---------|
| <i>Breedte en helling mast bij fundatie</i> | x-ri. | y-ri. |
| Pootsprei | 11,76 | 11,76 m |
| Helling van de randstijl | 0,190 | 0,190 - |
| Factor spatkracht | 1,1 | 1,1 - |

Berekening windbelasting

| | |
|---|---------------------------------------|
| Dynamische invloed G_T | 1,00 (<i>Masthoogte < 60 m</i>) |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam | $(1+0,2\sin^2(2\phi))$ |
| Vergroting wind overhoeks traverse | $(1+0,2\sin^2(2\phi))$ |
| Factor wind evenwijdig t.o.v. haaks op traverse | 0,4 |

Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving | h [m] | b ₁ [m] | b ₂ [m] | Δh [m] | Δ _x [m] | A ₀ [m ²] | A ₁ [m ²] | χ = A ₁ /A ₀ [-] | C _t |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk | 15,40 | 11,76 | 5,91 | 15,40 | 0,190 | 136,07 | 31,88 | 0,23 | 2,79 |
| Eerste tussenstuk | 22,20 | 5,91 | 5,23 | 6,80 | 0,050 | 37,88 | 13,58 | 0,36 | 2,34 |
| Tweede tussenstuk | 28,50 | 5,23 | 4,60 | 6,30 | 0,050 | 30,96 | 10,07 | 0,33 | 2,45 |
| Bovenstuk 1 | 38,00 | 4,60 | 3,65 | 9,50 | 0,050 | 39,19 | 12,64 | 0,32 | 2,46 |
| Bovenstuk 2 | 51,40 | 3,65 | 2,31 | 13,40 | 0,050 | 39,93 | 13,53 | 0,34 | 2,40 |
| Topstuk | 53,10 | 2,31 | | 1,70 | | 1,96 | 0,33 | 0,17 | 3,08 |
| Ondertraverse | 28,50 | 10,70 | | 3,10 | | 16,59 | 5,05 | 0,30 | 2,52 |
| Middentraverse | 38,00 | 14,08 | | 3,20 | | 22,52 | 6,95 | 0,31 | 2,50 |
| Boventraverse | 48,00 | 16,98 | | 5,10 | | 43,29 | 8,13 | 0,19 | 2,98 |

Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving | h [m] | b ₁ [m] | b ₂ [m] | Δh [m] | Δ _x [m] | A ₀ [m ²] | A ₁ [m ²] | χ = A ₁ /A ₀ [-] | C _t |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk | 15,40 | 11,76 | 5,91 | 15,40 | 0,190 | 136,07 | 31,88 | 0,23 | 2,79 |
| Eerste tussenstuk | 22,20 | 5,91 | 5,23 | 6,80 | 0,050 | 37,88 | 13,58 | 0,36 | 2,34 |
| Tweede tussenstuk | 28,50 | 5,23 | 4,60 | 6,30 | 0,050 | 30,96 | 10,07 | 0,33 | 2,45 |
| Bovenstuk 1 | 38,00 | 4,60 | 3,65 | 9,50 | 0,050 | 39,19 | 12,64 | 0,32 | 2,46 |
| Bovenstuk 2 | 51,40 | 3,65 | 2,31 | 13,40 | 0,050 | 39,93 | 13,53 | 0,34 | 2,40 |
| Topstuk | 53,10 | 2,31 | | 1,70 | | 1,96 | 0,33 | 0,17 | 3,08 |
| Ondertraverse | 28,50 | 10,70 | | 3,10 | | 16,59 | 5,05 | 0,30 | 2,52 |
| Middentraverse | 38,00 | 14,08 | | 3,20 | | 22,52 | 6,95 | 0,31 | 2,50 |
| Boventraverse | 48,00 | 16,98 | | 5,10 | | 43,29 | 8,13 | 0,19 | 2,98 |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

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Windoppervlak feeders telecominstallaties

| Onderdeel | A (m ² /m) | Factor | Δh | A ₁ |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk | 0,14 | 0,71 | 15,4 | 1,5 |
| Eerste tussenstuk | 0,14 | 0,71 | 6,8 | 0,7 |
| Tweede tussenstuk | 0,14 | 0,71 | 6,3 | 0,6 |
| Bovenstuk 1 | 0,14 | 0,71 | 9,5 | 0,9 |
| Bovenstuk 2 | | | | |

Invoer antennes

| Omschrijving | A (m ²) | h (m) | C _i (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top | | | |
| Antenne o.t. | 4,7 | 34,7 | 1,5 |

Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving | P _w [kN/m ²] | F _{x1} [kN] | F _{x2} [kN] | F _{x3} [kN] | F _{x4} [kN] | h _{ef} [m] | M _{y1} [kNm] | M _{y2} [kNm] | M _{y3} [kNm] | M _{y4} [kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk | 0,70 | 62,3 | 52,8 | 0,0 | -52,8 | 7,7 | 479,4 | 406,8 | 0,0 | -406,8 |
| Eerste tussenstuk | 0,86 | 27,4 | 23,2 | 0,0 | -23,2 | 18,8 | 514,6 | 436,6 | 0,0 | -436,6 |
| Tweede tussenstuk | 0,94 | 23,2 | 19,7 | 0,0 | -19,7 | 25,4 | 588,3 | 499,2 | 0,0 | -499,2 |
| Bovenstuk 1 | 1,02 | 31,7 | 26,9 | 0,0 | -26,9 | 33,3 | 1054,8 | 895,0 | 0,0 | -895,0 |
| Bovenstuk 2 | 1,10 | 35,8 | 30,4 | 0,0 | -30,4 | 44,7 | 1601,8 | 1359,2 | 0,0 | -1359,2 |
| Topstuk | 1,15 | 1,2 | 1,0 | 0,0 | -1,0 | 52,3 | 60,7 | 51,5 | 0,0 | -51,5 |
| Ondertraverse | 0,98 | 25,0 | 14,9 | 0,0 | -14,9 | 29,5 | 739,2 | 439,1 | 0,0 | -439,1 |
| Middentraverse | 1,06 | 37,0 | 22,0 | 0,0 | -22,0 | 39,1 | 1446,1 | 859,0 | 0,0 | -859,0 |
| Boventraverse | 1,13 | 55,0 | 32,7 | 0,0 | -32,7 | 49,7 | 2734,8 | 1624,4 | 0,0 | -1624,4 |
| Totaal | | 298,6 | 223,6 | 0,0 | -223,6 | | 9219,8 | 6570,8 | 0,0 | -6570,8 |

Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving | P _w [kN/m ²] | F _{y1} [kN] | F _{y2} [kN] | F _{y3} [kN] | F _{y4} [kN] | h _{ef} [m] | M _{x1} [kNm] | M _{x2} [kNm] | M _{x3} [kNm] | M _{x4} [kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk | 0,70 | 0,0 | 52,8 | 62,3 | 52,8 | 7,7 | 0,0 | 406,8 | 479,4 | 406,8 |
| Eerste tussenstuk | 0,86 | 0,0 | 23,2 | 27,4 | 23,2 | 18,8 | 0,0 | 436,6 | 514,6 | 436,6 |
| Tweede tussenstuk | 0,94 | 0,0 | 19,7 | 23,2 | 19,7 | 25,4 | 0,0 | 499,2 | 588,3 | 499,2 |
| Bovenstuk 1 | 1,02 | 0,0 | 26,9 | 31,7 | 26,9 | 33,3 | 0,0 | 895,0 | 1054,8 | 895,0 |
| Bovenstuk 2 | 1,10 | 0,0 | 30,4 | 35,8 | 30,4 | 44,7 | 0,0 | 1359,2 | 1601,8 | 1359,2 |
| Topstuk | 1,15 | 0,0 | 1,0 | 1,2 | 1,0 | 52,3 | 0,0 | 51,5 | 60,7 | 51,5 |
| Ondertraverse | 0,98 | 0,0 | 14,9 | 10,0 | 14,9 | 29,5 | 0,0 | 439,1 | 295,7 | 439,1 |
| Middentraverse | 1,06 | 0,0 | 22,0 | 14,8 | 22,0 | 39,1 | 0,0 | 859,0 | 578,5 | 859,0 |
| Boventraverse | 1,13 | 0,0 | 32,7 | 22,0 | 32,7 | 49,7 | 0,0 | 1624,4 | 1093,9 | 1624,4 |
| Totaal | | 0,0 | 223,6 | 228,4 | 223,6 | | 0,0 | 6570,8 | 6267,7 | 6570,8 |

Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F _x [kN] | F _y [kN] | F _z [kN] | M _x [kNm] | M _y [kNm] | M _z [kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting | 0 | 0 | 1021 | 0 | 0 | 0 |
| Windrichting 0° | 306 | 0 | 0 | 0 | 9472 | 0 |
| Windrichting 45° | 229 | 229 | 0 | 6749 | 6749 | 0 |
| Windrichting 90° | 0 | 236 | 0 | 6520 | 0 | 0 |
| Windrichting 135° | -229 | 229 | 0 | 6749 | -6749 | 0 |

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Tussenresultaten geleiderbelastingen

Geleiders back

| Circuit | Geleider | Diameter [mm] | A [mm ²] | G [N/m] | E [N/mm ²] | αT [-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 2 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 3 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 4 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8 | 281,0 | 9,38 | 70165 | 1,97E-05 |
| Bliksemdraad 2 | OPGW AFL-226/38 | 21,7 | 264,0 | 9,13 | 72000 | 1,98E-05 |

Geleiders ahead

| Circuit | Geleider | Diameter [mm] | A [mm ²] | G [N/m] | E [N/mm ²] | αT [-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 2 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 3 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 4 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8 | 281,0 | 9,38 | 70165 | 1,97E-05 |
| Bliksemdraad 2 | OPGW AFL-226/38 | 21,7 | 264,0 | 9,13 | 72000 | 1,98E-05 |

Verticale belasting back

| Circuit | Bundel [-] | Toeslag [%] | $W_{z,G}$ [N/m] | IJsgebied | Formule | $W_{z,ijs}$ [N/m] | $W_{z,ijs,bundel}$ [N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 2 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 3 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Circuit 4 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Bliksemdraad 1 | 1 | 2 | 9,6 | A | 15+0,4d | 23,7 | 23,7 |
| Bliksemdraad 2 | 1 | 2 | 9,3 | A | 15+0,4d | 23,7 | 23,7 |

Verticale belasting ahead

| Circuit | Bundel [-] | Toeslag [%] | $W_{z,G}$ [N/m] | IJsgebied | Formule | $W_{z,ijs}$ [N/m] | $W_{z,ijs,bundel}$ [N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 2 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 3 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Circuit 4 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Bliksemdraad 1 | 1 | 2 | 9,6 | A | 15+0,4d | 23,7 | 23,7 |
| Bliksemdraad 2 | 1 | 2 | 9,3 | A | 15+0,4d | 23,7 | 23,7 |

Isolatoren

| Geleider | $G_{isolator}$ [kN] | Aantal | $F_{v,iso}$ [kN] | Lengte [m] | Windopp. [m ²] | Windhoogte [m] | Stuwdruk [kN/m ²] | Vormfactor [-] | $F_{h,iso}$ [kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 3,00 | 1 | 3 | 6,5 | 1,1 | 48,50 | 1,13 | 1,2 | 1,49 |
| 380ct1f2 | 3,00 | 1 | 3 | 6,5 | 1,1 | 38,50 | 1,06 | 1,2 | 1,40 |
| 380ct1f3 | 3,00 | 1 | 3 | 6,5 | 1,1 | 29,00 | 0,98 | 1,2 | 1,29 |
| 380ct2f1 | 3,00 | 1 | 3 | 6,5 | 1,1 | 48,50 | 1,13 | 1,2 | 1,49 |
| 380ct2f2 | 3,00 | 1 | 3 | 6,5 | 1,1 | 38,50 | 1,06 | 1,2 | 1,40 |
| 380ct2f3 | 3,00 | 1 | 3 | 6,5 | 1,1 | 29,00 | 0,98 | 1,2 | 1,29 |
| 150ct3f1 | 2,00 | 1 | 2 | 4,5 | 0,8 | 48,50 | 1,13 | 1,2 | 1,08 |
| 150ct3f2 | 2,00 | 1 | 2 | 4,5 | 0,8 | 38,50 | 1,06 | 1,2 | 1,02 |
| 150ct3f3 | 2,00 | 1 | 2 | 4,5 | 0,8 | 29,00 | 0,98 | 1,2 | 0,94 |
| 150ct4f1 | 2,00 | 1 | 2 | 4,5 | 0,8 | 48,50 | 1,13 | 1,2 | 1,08 |
| 150ct4f2 | 2,00 | 1 | 2 | 4,5 | 0,8 | 38,50 | 1,06 | 1,2 | 1,02 |
| 150ct4f3 | 2,00 | 1 | 2 | 4,5 | 0,8 | 29,00 | 0,98 | 1,2 | 0,94 |
| bl1 | 0,10 | 1 | 0,1 | 0,2 | 0,1 | 53,60 | 1,16 | 1,2 | 0,14 |
| bl2 | 0,10 | 1 | 0,1 | 0,2 | 0,1 | 53,60 | 1,16 | 1,2 | 0,14 |

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Windbelasting back

| Geleider | hoogte | | G _{c,dwars} | G _{c,trek} | C _c | d _{toeslag} | W _y | W _{y,vak} | D _{jjs,toeslag} | W _{y,ijs} | W _{y,ijs,vak} |
|----------|--------|----------------------|----------------------|---------------------|----------------|----------------------|----------------|--------------------|--------------------------|--------------------|------------------------|
| | wind | Stuwdruk | | | | | | | | | |
| | [m] | [kN/m ²] | [-] | [-] | [-] | [mm] | [N/m] | [N/m] | [mm] | [N/m] | [N/m] |
| 380ct1f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 89,8 | 98,8 | 51,8 | 174,5 | 191,9 |
| 380ct1f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 84,0 | 92,4 | 51,8 | 159,9 | 175,9 |
| 380ct1f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 77,1 | 84,9 | 51,8 | 143,2 | 157,6 |
| 380ct2f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 89,8 | 98,8 | 51,8 | 174,5 | 191,9 |
| 380ct2f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 84,0 | 92,4 | 51,8 | 159,9 | 175,9 |
| 380ct2f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 77,1 | 84,9 | 51,8 | 143,2 | 157,6 |
| 150ct3f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 44,9 | 49,4 | 51,8 | 87,3 | 95,9 |
| 150ct3f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 42,0 | 46,2 | 51,8 | 79,9 | 88,0 |
| 150ct3f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 38,6 | 42,4 | 51,8 | 71,6 | 78,8 |
| 150ct4f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 44,9 | 49,4 | 51,8 | 87,3 | 95,9 |
| 150ct4f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 42,0 | 46,2 | 51,8 | 79,9 | 88,0 |
| 150ct4f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 38,6 | 42,4 | 51,8 | 71,6 | 78,8 |
| bl1 | 55,2 | 1,17 | 0,62 | 0,69 | 1,18 | 22,24 | 19,1 | 21,0 | 63,1 | 55,2 | 60,6 |
| bl2 | 55,2 | 1,17 | 0,62 | 0,69 | 1,18 | 22,13 | 19,0 | 20,9 | 63,0 | 55,1 | 60,5 |

Windbelasting ahead

| Geleider | hoogte | | G _{c,dwars} | G _{c,trek} | C _c | d _{toeslag} | W _y | W _{y,vak} | D _{jjs,toeslag} | W _{y,ijs} | W _{y,ijs,vak} |
|----------|--------|----------------------|----------------------|---------------------|----------------|----------------------|----------------|--------------------|--------------------------|--------------------|------------------------|
| | wind | Stuwdruk | | | | | | | | | |
| | [m] | [kN/m ²] | [-] | [-] | [-] | [mm] | [N/m] | [N/m] | [mm] | [N/m] | [N/m] |
| 380ct1f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 86,5 | 95,1 | 51,8 | 166,0 | 182,6 |
| 380ct1f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 79,9 | 87,9 | 51,8 | 149,7 | 164,8 |
| 380ct1f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 71,7 | 78,9 | 51,8 | 130,4 | 143,6 |
| 380ct2f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 86,5 | 95,1 | 51,8 | 166,0 | 182,6 |
| 380ct2f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 79,9 | 87,9 | 51,8 | 149,7 | 164,8 |
| 380ct2f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 71,7 | 78,9 | 51,8 | 130,4 | 143,6 |
| 150ct3f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 43,2 | 47,6 | 51,8 | 83,0 | 91,3 |
| 150ct3f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 39,9 | 43,9 | 51,8 | 74,9 | 82,4 |
| 150ct3f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 35,8 | 39,5 | 51,8 | 65,2 | 71,8 |
| 150ct4f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 43,2 | 47,6 | 51,8 | 83,0 | 91,3 |
| 150ct4f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 39,9 | 43,9 | 51,8 | 74,9 | 82,4 |
| 150ct4f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 35,8 | 39,5 | 51,8 | 65,2 | 71,8 |
| bl1 | 49,2 | 1,13 | 0,62 | 0,68 | 1,19 | 22,24 | 18,4 | 20,2 | 63,1 | 52,8 | 58,0 |
| bl2 | 49,2 | 1,13 | 0,62 | 0,68 | 1,19 | 22,13 | 18,3 | 20,1 | 63,0 | 52,7 | 57,9 |

NB: belastingen w_v gelden voor bundel

Project: RLL-TLB380
 Masttype: HC+0_c - 120gr
 Mast: 1187

Auteur: TBR
 Versie: v12.0

Geleiderbelastingen

Uitgangspunten

Betrouwbaarheidsniveau Nieuwbouw CC2
 Referentieperiode 50 jaar

| ULS (bezwijksterkte) | | NEN-EN50341-2-15:2019 | | | | | | | |
|--|---------------------------|-----------------------|--------------|---------------------|--|----------|----------|---------------------|--|
| Belastingsgeval | omschrijving | Temp °C | γ_G | | γ_Q | | | γ_a A_k | |
| | | | $G_{k,mast}$ | $G_{k,geleider}$ | Q_{pk} | Q_{wk} | Q_{ik} | | |
| ULS 1a | Wind | 10° | 1,20 | 1,20 | 0,00 | 1,50 | 0,00 | 0,0 | |
| ULS 1a_0,9 | Wind 0,9Gk alleen mast | 10° | 0,90 | 1,20 | 0,00 | 1,50 | 0,00 | 0,0 | |
| ULS 1a_0,9_0,9 | Wind 0,9Gk ook geleider | 10° | 0,90 | 0,90 | 0,00 | 1,50 | 0,00 | 0,0 | |
| ULS 3 | Wind+ijs | -5° | 1,20 | 1,20 | 0,00 | 0,45 | 1,50 | 0,0 | |
| ULS 3_0,9 | Wind+ijs 0,9 | -5° | 0,90 | 1,20 | 0,00 | 0,45 | 1,50 | 0,0 | |
| ULS 4 | Koude+wind | -20° | 1,20 | 1,20 | 0,00 | 0,30 | 0,00 | 0,0 | |
| ULS 4_0,9 | Koude+wind 0,9 | -20° | 0,90 | 1,20 | 0,00 | 0,30 | 0,00 | 0,0 | |
| ULS 5a | Torsiebelastingen | 10° | 1,00 | 1,00 | 1,00 | 0,00 | 0,00 | 1,0 | |
| ULS 5b | Longitudinale belastingen | 10° | 1,00 | 1,00 | 0,00 | 0,00 | 0,00 | 1,0 | |
| ULS 6 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 1,50 | 0,30 | 0,00 | 0,0 | |
| ULS 6_0,9 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 0,00 | 0,30 | 0,00 | 0,0 | |
| ULS 7 | Permanent | 10° | 1,35 | 1,35 | 0,00 | 0,00 | 0,00 | 0,0 | |
| ULS 8 | Special | 10° | 1,00 | 1,00 | 0,00 | 0,00 | 0,00 | 1,0 | |
| SPLS (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) | | | | γ_G G_k | γ_Q Q_{pk} Q_{wk} Q_{ik} | | | A_k | |
| SPLS 1a | Wind | 10° | 1,20 | 1,20 | 0,0 | 0,78 | 0,00 | 0,0 | |
| SPLS 1a_0,9 | Wind 0,9 | 10° | 0,90 | 1,20 | 0,0 | 0,78 | 0,00 | 0,0 | |
| SPLS 1a_0,9_0,9 | Wind 0,9 | 10° | 0,90 | 0,90 | 0,0 | 0,78 | 0,00 | 0,0 | |
| SPLS 3 | Wind+ijs | -5° | 1,20 | 1,20 | 0,0 | 0,36 | 0,34 | 0,0 | |
| SPLS 3_0,9 | Wind+ijs 0,9 | -5° | 0,90 | 1,20 | 0,0 | 0,36 | 0,34 | 0,0 | |
| SPLS 4 | Koude+wind | -20° | 1,20 | 1,20 | 0,0 | 0,24 | 0,00 | 0,0 | |
| SPLS 4_0,9 | Koude+wind 0,9 | -20° | 0,90 | 1,20 | 0,0 | 0,24 | 0,00 | 0,0 | |
| SPLS 6 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 1,2 | 0,24 | 0,0 | 0,0 | |
| SPLS 6_0,9 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 0,0 | 0,24 | 0,0 | 0,0 | |
| SLS (controle van de vervormingen, vermoeiing, EDS) | | | | G_k | Q_{pk} | Q_{wk} | Q_{ik} | A_k | |
| SLS 1a | Wind | 10° | 1,00 | 1,00 | 0,0 | 1,00 | 0,0 | 0,0 | |
| SLS 3 | Wind+ijs | -5° | 1,00 | 1,00 | 0,0 | 0,30 | 1,00 | 0,0 | |
| SLS 4 | Wind | -20° | 1,00 | 1,00 | 0,0 | 0,20 | 0,0 | 0,0 | |
| SLS 6 | Bouw en onderhoud | 5° | 1,00 | 1,00 | 0,0 | 0,20 | 0,0 | 0,0 | |
| SLS 7 | PB (EDS, geen wind) | 10° | 1,00 | 1,00 | 0,0 | 0,00 | 0,0 | 0,0 | |

Aantal windrichtingen 6
 Aantal belastingcombinaties ULS 100
 Aantal belastingcombinaties SPLS 246
 Aantal belastingcombinaties SLS 15
 Aantal knooplasten 12274

Project: RLL-TLB380
 Masttype: HC+0_c - 120gr
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Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

Maximale waarden voor back en ahead span

| Geleider | Fx_ba [kN] | Fx_ah [kN] | Fy_ba [kN] | Fy_ah [kN] | Fz_ba [kN] | Fz_ah [kN] |
|--------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1 | -56,0 | 55,7 | 38,1 | 37,7 | 11,1 | 11,0 |
| 380ct1f1 | -227,0 | 225,3 | 154,2 | 150,7 | 39,8 | 39,7 |
| 380ct1f2 | -224,2 | 222,3 | 148,1 | 144,7 | 39,7 | 39,6 |
| 380ct1f3 | -221,2 | 219,2 | 143,4 | 140,9 | 39,6 | 39,5 |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| 380ct2f1 | -227,0 | 225,3 | 154,2 | 150,7 | 39,8 | 39,7 |
| 380ct2f2 | -224,2 | 222,3 | 148,1 | 144,7 | 39,7 | 39,6 |
| 380ct2f3 | -221,2 | 219,2 | 143,4 | 140,9 | 39,6 | 39,5 |
| 150ct3f1 | -113,4 | 112,6 | 77,6 | 75,8 | 21,3 | 21,3 |
| 150ct3f2 | -112,0 | 111,1 | 74,5 | 72,5 | 21,3 | 21,3 |
| 150ct3f3 | -110,5 | 109,5 | 71,8 | 70,6 | 21,3 | 21,3 |
| 150ct4f1 | -113,4 | 112,6 | 77,6 | 75,8 | 21,3 | 21,3 |
| 150ct4f2 | -112,0 | 111,1 | 74,5 | 72,5 | 21,3 | 21,3 |
| 150ct4f3 | -110,5 | 109,5 | 71,8 | 70,6 | 21,3 | 21,3 |
| bl2 | -55,2 | 54,9 | 37,7 | 37,7 | 11,0 | 10,9 |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |

Min. Weight span (m)

Weight spar Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|-----------------|--------|-------|-------|
| bl1 | 489,9 | 495,8 | 481,0 |
| 380ct1f1 | 484,5 | 495,6 | 481,0 |
| 380ct1f2 | 484,1 | 495,4 | 481,0 |
| 380ct1f3 | 483,5 | 495,2 | 481,0 |
| Post-isolator 1 | | | |
| Post-isolator 2 | | | |
| Post-isolator 3 | | | |
| 380ct2f1 | 484,5 | 495,6 | 481,0 |
| 380ct2f2 | 484,1 | 495,4 | 481,0 |
| 380ct2f3 | 483,5 | 495,2 | 481,0 |
| 150ct3f1 | 484,5 | 495,6 | 481,0 |
| 150ct3f2 | 484,1 | 495,4 | 481,0 |
| 150ct3f3 | 483,5 | 495,2 | 481,0 |
| 150ct4f1 | 484,5 | 495,6 | 481,0 |
| 150ct4f2 | 484,1 | 495,4 | 481,0 |
| 150ct4f3 | 483,5 | 495,2 | 481,0 |
| bl2 | 490,3 | 496,0 | 481,0 |
| Post-isolator 4 | | | |
| Post-isolator 5 | | | |
| Post-isolator 6 | | | |

Max. Weight span (m)

Weight spar Combinatie1

| Geleider | ULS 1a | ULS 3 |
|-----------------|--------|-------|
| bl1 | 548,6 | 461,8 |
| 380ct1f1 | 513,1 | 477,6 |
| 380ct1f2 | 509,4 | 476,9 |
| 380ct1f3 | 505,0 | 476,1 |
| Post-isolator 1 | | |
| Post-isolator 2 | | |
| Post-isolator 3 | | |
| 380ct2f1 | 513,1 | 477,6 |
| 380ct2f2 | 509,4 | 476,9 |
| 380ct2f3 | 505,0 | 476,1 |
| 150ct3f1 | 513,1 | 477,6 |
| 150ct3f2 | 509,4 | 476,9 |
| 150ct3f3 | 505,0 | 476,1 |
| 150ct4f1 | 513,1 | 477,6 |
| 150ct4f2 | 509,4 | 476,9 |
| 150ct4f3 | 505,0 | 476,1 |
| bl2 | 550,6 | 461,4 |
| Post-isolator 4 | | |
| Post-isolator 5 | | |
| Post-isolator 6 | | |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

| | |
|------------------|---------|
| Max. weight span | 548,6 m |
| Min. weight span | 128,9 m |

Wind / Weight span verhouding

| |
|---------|
| 1,371 - |
| 0,322 - |

Project: RLL-TLB380
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Maximale waarden back+ahead span Maximale waarden trekkracht geleider

| Geleider | Fx | Fy | Fz | Ft_ba | Ft_ah |
|--------------|-------|-------|------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] |
| bl1 | 33,6 | 71,1 | 11,1 | -67,6 | 67,1 |
| 380ct1f1 | 178,5 | 280,4 | 39,8 | -271,5 | 269,2 |
| 380ct1f2 | 175,2 | 276,1 | 39,7 | -267,5 | 264,9 |
| 380ct1f3 | 171,7 | 271,3 | 39,6 | -263,3 | 260,2 |
| Post-isolato | 4,2 | 4,2 | 6,8 | 0,0 | |
| Post-isolato | 3,2 | 3,2 | 4,7 | 0,0 | |
| Post-isolato | 4,9 | 4,9 | 6,8 | 0,0 | |
| 380ct2f1 | 178,5 | 280,4 | 39,8 | -271,5 | 269,2 |
| 380ct2f2 | 175,2 | 276,1 | 39,7 | -267,5 | 264,9 |
| 380ct2f3 | 171,7 | 271,3 | 39,6 | -263,3 | 260,2 |
| 150ct3f1 | 94,3 | 140,4 | 21,3 | -135,8 | 134,6 |
| 150ct3f2 | 94,3 | 138,2 | 21,3 | -133,8 | 132,4 |
| 150ct3f3 | 94,2 | 135,8 | 21,3 | -131,6 | 130,1 |
| 150ct4f1 | 94,3 | 140,4 | 21,3 | -135,8 | 134,6 |
| 150ct4f2 | 94,3 | 138,2 | 21,3 | -133,8 | 132,4 |
| 150ct4f3 | 94,2 | 135,8 | 21,3 | -131,6 | 130,1 |
| bl2 | 33,1 | 70,1 | 11,0 | -66,7 | 66,1 |
| Post-isolato | 4,2 | 4,2 | 6,8 | 0,0 | |
| Post-isolato | 3,2 | 3,2 | 4,7 | 0,0 | |
| Post-isolato | 4,9 | 4,9 | 6,8 | 0,0 | |

EDS-belastingen geleiders

| Geleider | Fx | Fy | Fz | Ft_ba | Ft_ah |
|--------------|-------|------|------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] |
| bl1 | 14,9 | 8,6 | 2,4 | -17,2 | 17,2 |
| 380ct1f1 | 113,7 | 65,7 | 20,5 | -131,3 | 131,3 |
| 380ct1f2 | 113,7 | 65,7 | 20,5 | -131,3 | 131,3 |
| 380ct1f3 | 113,7 | 65,7 | 20,5 | -131,3 | 131,3 |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 3,5 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |
| 380ct2f1 | 113,7 | 65,7 | 20,5 | -131,3 | 131,3 |
| 380ct2f2 | 113,7 | 65,7 | 20,5 | -131,3 | 131,3 |
| 380ct2f3 | 113,7 | 65,7 | 20,5 | -131,3 | 131,3 |
| 150ct3f1 | 56,9 | 32,8 | 10,8 | -65,7 | 65,7 |
| 150ct3f2 | 56,9 | 32,8 | 10,8 | -65,7 | 65,7 |
| 150ct3f3 | 56,9 | 32,8 | 10,8 | -65,7 | 65,7 |
| 150ct4f1 | 56,9 | 32,8 | 10,8 | -65,7 | 65,7 |
| 150ct4f2 | 56,9 | 32,8 | 10,8 | -65,7 | 65,7 |
| 150ct4f3 | 56,9 | 32,8 | 10,8 | -65,7 | 65,7 |
| bl2 | 14,5 | 8,4 | 2,3 | -16,8 | 16,8 |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 3,5 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |

Controle uplift SLS-wind

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
| | [kN] | [kN] |
| SLS 4 | | |
| bl1 | 0,0 | 0,0 |
| 380ct1f1 | 0,0 | 0,0 |
| 380ct1f2 | 0,0 | 0,0 |
| 380ct1f3 | 0,0 | 0,0 |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |
| 380ct2f1 | 0,0 | 0,0 |
| 380ct2f2 | 0,0 | 0,0 |
| 380ct2f3 | 0,0 | 0,0 |
| 150ct3f1 | 0,0 | 0,0 |
| 150ct3f2 | 0,0 | 0,0 |
| 150ct3f3 | 0,0 | 0,0 |
| 150ct4f1 | 0,0 | 0,0 |
| 150ct4f2 | 0,0 | 0,0 |
| 150ct4f3 | 0,0 | 0,0 |
| bl2 | 0,0 | 0,0 |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |

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ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders

| Combinatie | Combination | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90 | | -35 | 2342 | 519 | 91364 | -1318 | 0 |
| ULS 1a_0,9_0 | | 81 | 1496 | 331 | 57853 | 3189 | 0 |
| ULS 1a_0,9_0,9_90 | | -41 | 2190 | 211 | 85607 | -1526 | 0 |
| ULS 3_0 | | 41 | 2337 | 789 | 91014 | 1635 | 0 |
| SLS 7 | | 0 | 1216 | 412 | 46916 | 0 | 0 |

ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast

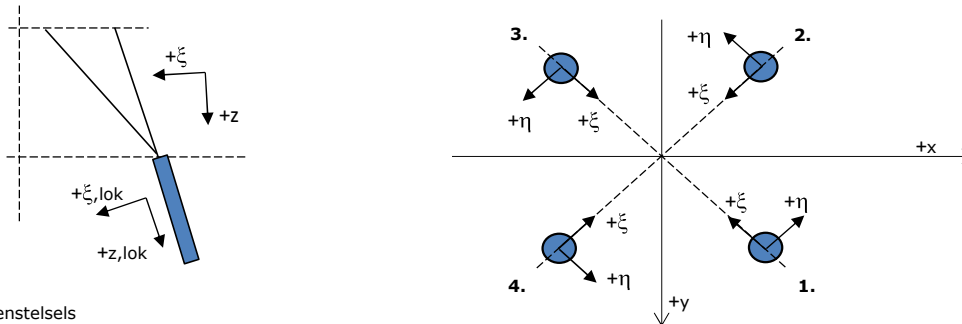
| Combinatie | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90 | -35 | 2696 | 1744 | 101143 | -1318 | 0 |
| ULS 1a_0,9_0,9_90 | -41 | 2544 | 1130 | 95387 | -1526 | 0 |
| SLS 7 | 0 | 1216 | 1434 | 46916 | 0 | 0 |

Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde

| Combinatie | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|----------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 3_0,9_90 | -10 | 2739 | 1448 | 105796 | -368 | 0 |
| SPLS 3_60 Ah All Cts | -1587 | 1117 | 1562 | 42559 | -62279 | 8 |
| SPLS 3_60 Ba Ct1 | 702 | 1473 | 1673 | 57470 | 26401 | -9307 |
| ULS 1a_0,9_60 | -394 | 2584 | 1213 | 96738 | -18023 | 1 |

Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.

Oplegreacties op fundering per randstijl



Assenstelsels

Maximale drukbelasting

| Stijl | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_η [kN] | R_ξ [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|----------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1 | ULS 1a_120 | 1023 | 870 | 5169 | 108 | -1338 | 50 | 5352 |
| 2 | SPLS 1a_0 Ba All Cts | 220 | -408 | 1646 | 133 | -444 | -2 | 1704 |
| 3 | ULS 8 Ba | -161 | -392 | 1472 | -163 | -391 | 4 | 1525 |
| 4 | ULS 1a_60 | -1049 | 897 | 5314 | -107 | -1376 | 52 | 5502 |

Maximale trekbelasting

| Stijl | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_η [kN] | R_ξ [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1 | ULS 8 Ba | -3 | -235 | -718 | 164 | 168 | -25 | -743 |
| 2 | ULS 1a_0,9_60 | -895 | 743 | -4575 | 107 | 1158 | -72 | -4737 |
| 3 | ULS 1a_0,9_120 | 868 | 714 | -4424 | -108 | 1118 | -70 | -4581 |
| 4 | SPLS 1a_0,9_0 Ba All Cts | 80 | -268 | -976 | -133 | 246 | -16 | -1010 |

Maximale torsiebelasting (positief)

| Stijl | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_η [kN] | R_ξ [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|-----------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1 | SPLS 3_90 Ah Ct1 | 605 | 10 | 1647 | 421 | -435 | 7 | 1706 |
| 2 | SPLS 3_0,9_60 Ba Ct2 | -452 | -128 | -935 | 410 | 229 | -22 | -968 |
| 3 | SPLS 3_60 Ba Ct2 | 378 | 713 | -3035 | 237 | 771 | -44 | -3143 |
| 4 | SPLS 3_0,9_120 Ah Ct1 | -551 | 864 | 3860 | 221 | -1001 | 36 | 3997 |

Maximale torsiebelasting (negatief)

| Index | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_η [kN] | R_ξ [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|----------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1 | SPLS 3_0,9_60 Ba Ct1 | 546 | 865 | 3841 | -225 | -998 | 34 | 3978 |
| 2 | SPLS 3_120 Ah Ct2 | -382 | 713 | -3045 | -234 | 774 | -44 | -3153 |
| 3 | SPLS 3_0,9_90 Ah Ct2 | 436 | -140 | -836 | -407 | 209 | -15 | -866 |
| 4 | SPLS 3_60 Ba Ct1 | -620 | 23 | 1739 | -422 | -455 | 12 | 1801 |

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Combinatie Ftrek+Fhor

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|-------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | ULS 8 Ba | -3 | -235 | -718 | 164 | 168 | -25 | -743 |
| 2 | ULS 1a_0,9_60 | -895 | 743 | -4575 | 107 | 1158 | -72 | -4737 |
| 3 | ULS 1a_0,9_120 | 868 | 714 | -4424 | -108 | 1118 | -70 | -4581 |
| 4 | SPLS 3_0,9_0 Ba All Cts | 50 | -270 | -916 | -156 | 226 | -20 | -949 |

Permanente belasting

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SLS 7 | 492 | 379 | 2353 | 80 | -616 | 17 | 2436 |
| 2 | SLS 7 | -342 | 229 | -1636 | 80 | 404 | -36 | -1694 |
| 3 | SLS 7 | 342 | 229 | -1636 | -80 | 404 | -36 | -1694 |
| 4 | SLS 7 | -492 | 379 | 2353 | -80 | -616 | 17 | 2436 |

Omhullenden ongeacht stijl

| Belasting | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------------------|------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk | ULS 1a_60 | -1049 | 897 | 5314 | -107 | -1376 | 52 | 5502 |
| Max. trek | ULS 1a_0,9_60 | -895 | 743 | -4575 | 107 | 1158 | -72 | -4737 |
| Max. pos. torsie | SPLS 3_90 Ah Ct1 | 605 | 10 | 1647 | 421 | -435 | 7 | 1706 |
| Max. neg. torsie | SPLS 3_60 Ba Ct1 | -620 | 23 | 1739 | -422 | -455 | 12 | 1801 |
| Comb. trek+torsie | ULS 1a_0,9_60 | -895 | 743 | -4575 | 107 | 1158 | -72 | -4737 |

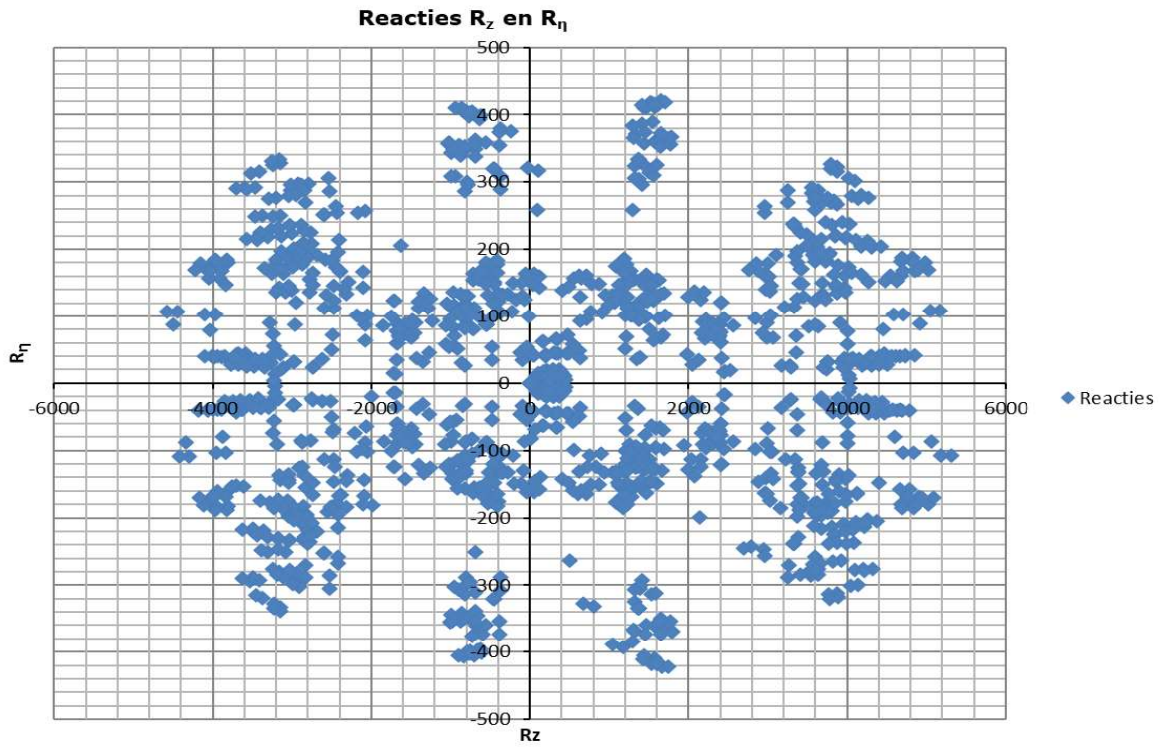
Maximale trekbelasting SLS

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SLS 7 | 492 | 379 | 2353 | 80 | -616 | 17 | 2436 |
| 2 | SLS 1a_60 | -647 | 521 | -3287 | 89 | 826 | -57 | -3403 |
| 3 | SLS 1a_120 | 630 | 502 | -3189 | -90 | 800 | -56 | -3302 |
| 4 | SLS 1a_0 | -419 | 288 | 1945 | -93 | -500 | 22 | 2014 |

Maximale drukbelasting SLS

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SLS 3_120 | 826 | 633 | 3986 | 136 | -1032 | 39 | 4127 |
| 2 | SLS 1a_0 | -269 | 138 | -1227 | 93 | 288 | -41 | -1270 |
| 3 | SLS 7 | 342 | 229 | -1636 | -80 | 404 | -36 | -1694 |
| 4 | SLS 3_60 | -832 | 640 | 4023 | -136 | -1041 | 40 | 4166 |

Project: RLL-TLB380
Masttype: HC+0_c - 120gr
Mast: 1187



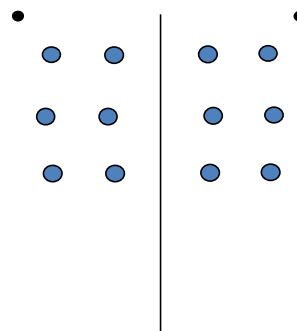
Project: RLL-TLB380
Tower: HC+0_c - 140gr
Number: 1187

Auteur: TBR
Versie: v12.0

Geleiderbelastingen

Algemeen

Benaming HC+0_c - 140gr
Masttype Hoekmast
Aantal circuits 4
Configuratie 4-circuit-dubbel verticaal
Aantal bliksemgeleiders 2



Configuratie geleiders

Uitgangspunten

Norm NEN-EN50341-2-15:2019
Gevolgklasse initieel CC2
Betrouwbaarheidsniveau initieel Nieuwbouw
Referentieperiode initieel 50 jaar
Betrouwbaarheidsniveau na aanpassing n.v.t.
50 jaar
Windgebied III
Windsnelheid (m/s) 24,5 m/s
Terreincategorie II
Reductiefactor C_{dir} 1,00
IJsgebied fasegeleider B
IJsgebied bliksemgeleider A

Geleiders Back

| Omschrijving | Spanning | Geleider Back | Bundel Ba | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden P_{back} |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|--------------------------|
| Circuit 1 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 2 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 3 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Circuit 4 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Bliksemdraad 1 | | AACSR 241-AL3-39-A20SA | 1 | A | 2 % | 2 % | 1800 |
| Bliksemdraad 2 | | OPGW AFL-226/38 | 1 | A | 2 % | 2 % | 1800 |

Geleiders Ahead

| Omschrijving | Spanning | Geleider Ahead | Bundel Ah | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden P_{ahead} |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|---------------------------|
| Circuit 1 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 2 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 3 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Circuit 4 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Bliksemdraad 1 | | AACSR 241-AL3-39-A20SA | 1 | A | 2 % | 2 % | 1800 |
| Bliksemdraad 2 | | OPGW AFL-226/38 | 1 | A | 2 % | 2 % | 1800 |

Isolatoren (1)

| Omschrijving | Ophanging | Gewicht [kN] | Lengte [m] | Windopp. [m ²] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1 | Afspanketting | 3,00 | 6,50 | 1,10 |
| Circuit 2 | Afspanketting | 3,00 | 6,50 | 1,10 |
| Circuit 3 | Afspanketting | 2,00 | 4,50 | 0,80 |
| Circuit 4 | Afspanketting | 2,00 | 4,50 | 0,80 |
| Bliksemdraad 1 | Afspanketting | 0,10 | 0,20 | 0,10 |
| Bliksemdraad 2 | Afspanketting | 0,10 | 0,20 | 0,10 |

1. Eigenschappen gelden voor geheel van de isolatorset

Ophanghoogte en positie in mast

| Circuits | Aanduiding | Nummer | Ophanghoogte | Aangrijppunt | Positie in mast Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1 | 10 | 380ct1f1 | 48,0 m | 48,0 m | -12,1 m |
| Circuit 1 | 11 | 380ct1f2 | 38,0 m | 38,0 m | -15,6 m |
| Circuit 1 | 12 | 380ct1f3 | 28,5 m | 28,5 m | -12,7 m |
| Circuit 2 | 40 | 380ct2f1 | 48,0 m | 48,0 m | 12,1 m |
| Circuit 2 | 41 | 380ct2f2 | 38,0 m | 38,0 m | 15,6 m |
| Circuit 2 | 42 | 380ct2f3 | 28,5 m | 28,5 m | 12,7 m |
| Circuit 3 | 20 | 150ct3f1 | 48,0 m | 48,0 m | -4,8 m |
| Circuit 3 | 21 | 150ct3f2 | 38,0 m | 38,0 m | -8,3 m |
| Circuit 3 | 22 | 150ct3f3 | 28,5 m | 28,5 m | -5,4 m |
| Circuit 4 | 30 | 150ct4f1 | 48,0 m | 48,0 m | 4,8 m |
| Circuit 4 | 31 | 150ct4f2 | 38,0 m | 38,0 m | 8,3 m |
| Circuit 4 | 32 | 150ct4f3 | 28,5 m | 28,5 m | 5,4 m |
| Bliksemdraad 1 | 1 | bl1 | 53,1 m | 53,1 m | -18,3 m |
| Bliksemdraad 2 | 3 | bl2 | 53,1 m | 53,1 m | 18,3 m |

Project: RLL-TLB380
 Tower: HC+0_c - 140gr
 Number: 1187

Hoogteaanpassing naastgelegen masten (aanpassing wind- en weight span)

| | Back | Ahead | |
|------------------------------------|---------------------------|--------|---|
| Verhoging voor windbelasting | 18,0 m | 6,0 m | (positief: omhoog) |
| Verlaging voor verticale belasting | -9,0 m | -9,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging: | Niet in 0,9EG-combinaties | | |

Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting

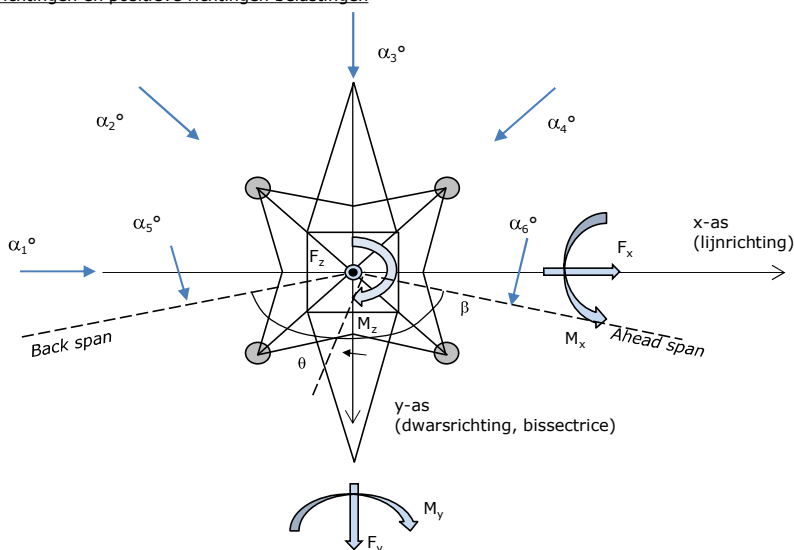
| Circuits | Aanduiding | Nummer | Hoogteverschil | | Richtingsverandering | |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
| | | | Δh back | Δh ahead | Δy back | Δy ahead |
| Circuit 1 | 10 | 380ct1f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 1 | 11 | 380ct1f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 1 | 12 | 380ct1f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 40 | 380ct2f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 41 | 380ct2f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 42 | 380ct2f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 3 | 20 | 150ct3f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 3 | 21 | 150ct3f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 3 | 22 | 150ct3f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 30 | 150ct4f1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 31 | 150ct4f2 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 32 | 150ct4f3 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Bliksemdraad 1 | 1 | bl1 | 0,0 | 0,0 m | 0,0 | 0,0 m |
| Bliksemdraad 2 | 3 | bl2 | 0,0 | 0,0 m | 0,0 | 0,0 m |

Lijn- en mastgegevens

| | Back | Ahead |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0 | 400,0 m |
| Lijnhoek β | 140 ° | |
| Rotatie mast t.o.v. bissectrice θ | 0 ° | |
| Vaklengte | 400 | 400 m |
| Hoogte onderkant mast t.o.v. maaiveld | 0,5 m | |
| Beschouwde windrichtingen | α_1 | 0 ° |
| Windrichtingen volgens: | α_2 | 45 ° |
| Geleiderbelastingen | α_3 | 90 ° |
| | α_4 | 135 ° |
| | α_5 | 70 ° |
| | α_6 | 110 ° |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



Beschouwd aantal windrichtingen

| | |
|--------|---|
| 1a | 6 |
| 3 | 6 |
| 4 | 1 |
| 6 | 1 |
| Overig | 1 |

Project: RLL-TLB380
 Tower: HC+0_c - 140gr
 Number: 1187

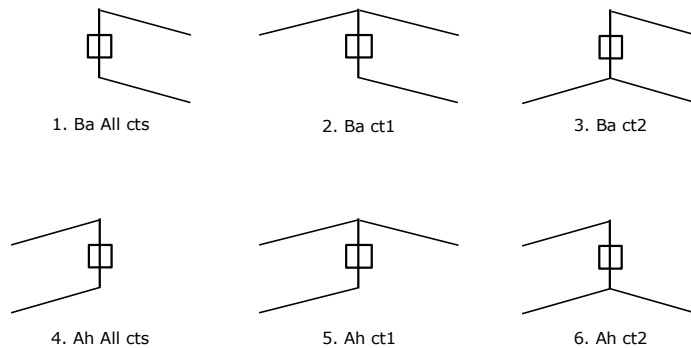
Geleiderafval

| | | SPLS - torsie | | SPLS - Enkelzijdige trek | | 5a - geleiderbreuk | |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
| | | Aanw. | Afw. | Aanw. | Afw. | Aanw. | Afw. |
| Circuit 1 | 380ct1f1 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 1 | 380ct1f2 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 1 | 380ct1f3 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 2 | 380ct2f1 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 2 | 380ct2f2 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 2 | 380ct2f3 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 3 | 150ct3f1 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 3 | 150ct3f2 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 3 | 150ct3f3 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 4 | 150ct4f1 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 4 | 150ct4f2 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 4 | 150ct4f3 | 0 | 1 | 1 | 0 | 1 | 0 |
| Bliksemdraad 1 | b11 | 1 | 0 | 1 | 0 | 1 | 0 |
| Bliksemdraad 2 | b12 | 0 | 1 | 1 | 0 | 1 | 0 |

Belastingssituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

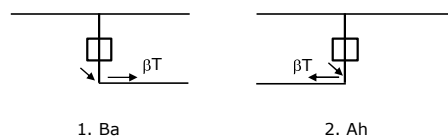
Principe belastingssituaties:



Belastingssituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



Project: RLL-TLB380
 Tower: HC+0_c - 140gr
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Belastingsituaties 6. Bouw- en onderhoud

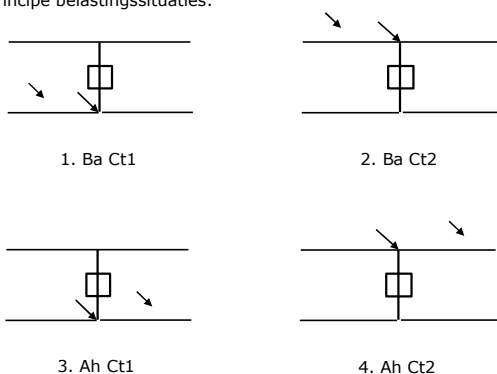
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

| | Fase | Bliksem |
|----------------------|--------|---------|
| Lijnwagen | 4,0 kN | 2,0 kN |
| Puntlast op traverse | 1,0 kN | 1,0 kN |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



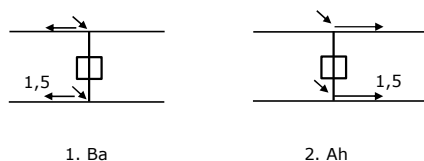
Belastingsituaties 8. Lijndansen als statische belasting

| Geleider | | |
|--------------------------|---------|-------|
| Steunmast fase | 0,866 W | 1,5 W |
| Steunmast bliksem | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingsspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

Project: RLL-TLB380
 Tower: HC+0_c - 140gr
 Number: 1187

Mastconstructie

Eigenschappen

| | |
|-----------------------------|----------------|
| Masttype | Hoekmast |
| Mastbenaming | HC+0_c - 140gr |
| Voetplaat t.o.v. maaiveld | 0,5 m |
| Masthoogte t.o.v. voetplaat | 53,1 m |
| Gewicht mast | 1021,2 kN |

| | | |
|---|-------|---------|
| <i>Breedte en helling mast bij fundatie</i> | x-ri. | y-ri. |
| Pootsprei | 11,76 | 11,76 m |
| Helling van de randstijl | 0,190 | 0,190 - |
| Factor spatkracht | 1,1 | 1,1 - |

Berekening windbelasting

| | |
|---|---------------------------------------|
| Dynamische invloed G_T | 1,00 (<i>Masthoogte < 60 m</i>) |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam | $(1+0,2\sin^2(2\phi))$ |
| Vergroting wind overhoeks traverse | $(1+0,2\sin^2(2\phi))$ |
| Factor wind evenwijdig t.o.v. haaks op traverse | 0,4 |

Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving | h [m] | b ₁ [m] | b ₂ [m] | Δh [m] | Δ _x [m] | A ₀ [m ²] | A ₁ [m ²] | χ = A ₁ /A ₀ [-] | C _t |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk | 15,40 | 11,76 | 5,91 | 15,40 | 0,190 | 136,07 | 31,88 | 0,23 | 2,79 |
| Eerste tussenstuk | 22,20 | 5,91 | 5,23 | 6,80 | 0,050 | 37,88 | 13,58 | 0,36 | 2,34 |
| Tweede tussenstuk | 28,50 | 5,23 | 4,60 | 6,30 | 0,050 | 30,96 | 10,07 | 0,33 | 2,45 |
| Bovenstuk 1 | 38,00 | 4,60 | 3,65 | 9,50 | 0,050 | 39,19 | 12,64 | 0,32 | 2,46 |
| Bovenstuk 2 | 51,40 | 3,65 | 2,31 | 13,40 | 0,050 | 39,93 | 13,53 | 0,34 | 2,40 |
| Topstuk | 53,10 | 2,31 | | 1,70 | | 1,96 | 0,33 | 0,17 | 3,08 |
| Ondertraverse | 28,50 | 10,70 | | 3,10 | | 16,59 | 5,05 | 0,30 | 2,52 |
| Middentraverse | 38,00 | 14,08 | | 3,20 | | 22,52 | 6,95 | 0,31 | 2,50 |
| Boventraverse | 48,00 | 16,98 | | 5,10 | | 43,29 | 8,13 | 0,19 | 2,98 |

Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving | h [m] | b ₁ [m] | b ₂ [m] | Δh [m] | Δ _x [m] | A ₀ [m ²] | A ₁ [m ²] | χ = A ₁ /A ₀ [-] | C _t |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk | 15,40 | 11,76 | 5,91 | 15,40 | 0,190 | 136,07 | 31,88 | 0,23 | 2,79 |
| Eerste tussenstuk | 22,20 | 5,91 | 5,23 | 6,80 | 0,050 | 37,88 | 13,58 | 0,36 | 2,34 |
| Tweede tussenstuk | 28,50 | 5,23 | 4,60 | 6,30 | 0,050 | 30,96 | 10,07 | 0,33 | 2,45 |
| Bovenstuk 1 | 38,00 | 4,60 | 3,65 | 9,50 | 0,050 | 39,19 | 12,64 | 0,32 | 2,46 |
| Bovenstuk 2 | 51,40 | 3,65 | 2,31 | 13,40 | 0,050 | 39,93 | 13,53 | 0,34 | 2,40 |
| Topstuk | 53,10 | 2,31 | | 1,70 | | 1,96 | 0,33 | 0,17 | 3,08 |
| Ondertraverse | 28,50 | 10,70 | | 3,10 | | 16,59 | 5,05 | 0,30 | 2,52 |
| Middentraverse | 38,00 | 14,08 | | 3,20 | | 22,52 | 6,95 | 0,31 | 2,50 |
| Boventraverse | 48,00 | 16,98 | | 5,10 | | 43,29 | 8,13 | 0,19 | 2,98 |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

Project: RLL-TLB380
 Tower: HC+0_c - 140gr
 Number: 1187

Windoppervlak feeders telecominstallaties

| Onderdeel | A (m ² /m) | Factor | Δh | A ₁ |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk | 0,14 | 0,71 | 15,4 | 1,5 |
| Eerste tussenstuk | 0,14 | 0,71 | 6,8 | 0,7 |
| Tweede tussenstuk | 0,14 | 0,71 | 6,3 | 0,6 |
| Bovenstuk 1 | 0,14 | 0,71 | 9,5 | 0,9 |
| Bovenstuk 2 | | | | |

Invoer antennes

| Omschrijving | A (m ²) | h (m) | C _r (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top | | | |
| Antenne o.t. | 4,7 | 34,7 | 1,5 |

Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving | P _w [kN/m ²] | F _{x1} [kN] | F _{x2} [kN] | F _{x3} [kN] | F _{x4} [kN] | h _{ef} [m] | M _{y1} [kNm] | M _{y2} [kNm] | M _{y3} [kNm] | M _{y4} [kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk | 0,70 | 62,3 | 52,8 | 0,0 | -52,8 | 7,7 | 479,4 | 406,8 | 0,0 | -406,8 |
| Eerste tussenstuk | 0,86 | 27,4 | 23,2 | 0,0 | -23,2 | 18,8 | 514,6 | 436,6 | 0,0 | -436,6 |
| Tweede tussenstuk | 0,94 | 23,2 | 19,7 | 0,0 | -19,7 | 25,4 | 588,3 | 499,2 | 0,0 | -499,2 |
| Bovenstuk 1 | 1,02 | 31,7 | 26,9 | 0,0 | -26,9 | 33,3 | 1054,8 | 895,0 | 0,0 | -895,0 |
| Bovenstuk 2 | 1,10 | 35,8 | 30,4 | 0,0 | -30,4 | 44,7 | 1601,8 | 1359,2 | 0,0 | -1359,2 |
| Topstuk | 1,15 | 1,2 | 1,0 | 0,0 | -1,0 | 52,3 | 60,7 | 51,5 | 0,0 | -51,5 |
| Ondertraverse | 0,98 | 25,0 | 14,9 | 0,0 | -14,9 | 29,5 | 739,2 | 439,1 | 0,0 | -439,1 |
| Middentraverse | 1,06 | 37,0 | 22,0 | 0,0 | -22,0 | 39,1 | 1446,1 | 859,0 | 0,0 | -859,0 |
| Boventraverse | 1,13 | 55,0 | 32,7 | 0,0 | -32,7 | 49,7 | 2734,8 | 1624,4 | 0,0 | -1624,4 |
| Totaal | | 298,6 | 223,6 | 0,0 | -223,6 | | 9219,8 | 6570,8 | 0,0 | -6570,8 |

Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving | P _w [kN/m ²] | F _{y1} [kN] | F _{y2} [kN] | F _{y3} [kN] | F _{y4} [kN] | h _{ef} [m] | M _{x1} [kNm] | M _{x2} [kNm] | M _{x3} [kNm] | M _{x4} [kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk | 0,70 | 0,0 | 52,8 | 62,3 | 52,8 | 7,7 | 0,0 | 406,8 | 479,4 | 406,8 |
| Eerste tussenstuk | 0,86 | 0,0 | 23,2 | 27,4 | 23,2 | 18,8 | 0,0 | 436,6 | 514,6 | 436,6 |
| Tweede tussenstuk | 0,94 | 0,0 | 19,7 | 23,2 | 19,7 | 25,4 | 0,0 | 499,2 | 588,3 | 499,2 |
| Bovenstuk 1 | 1,02 | 0,0 | 26,9 | 31,7 | 26,9 | 33,3 | 0,0 | 895,0 | 1054,8 | 895,0 |
| Bovenstuk 2 | 1,10 | 0,0 | 30,4 | 35,8 | 30,4 | 44,7 | 0,0 | 1359,2 | 1601,8 | 1359,2 |
| Topstuk | 1,15 | 0,0 | 1,0 | 1,2 | 1,0 | 52,3 | 0,0 | 51,5 | 60,7 | 51,5 |
| Ondertraverse | 0,98 | 0,0 | 14,9 | 10,0 | 14,9 | 29,5 | 0,0 | 439,1 | 295,7 | 439,1 |
| Middentraverse | 1,06 | 0,0 | 22,0 | 14,8 | 22,0 | 39,1 | 0,0 | 859,0 | 578,5 | 859,0 |
| Boventraverse | 1,13 | 0,0 | 32,7 | 22,0 | 32,7 | 49,7 | 0,0 | 1624,4 | 1093,9 | 1624,4 |
| Totaal | | 0,0 | 223,6 | 228,4 | 223,6 | | 0,0 | 6570,8 | 6267,7 | 6570,8 |

Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F _x [kN] | F _y [kN] | F _z [kN] | M _x [kNm] | M _y [kNm] | M _z [kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting | 0 | 0 | 1021 | 0 | 0 | 0 |
| Windrichting 0° | 306 | 0 | 0 | 0 | 9472 | 0 |
| Windrichting 45° | 229 | 229 | 0 | 6749 | 6749 | 0 |
| Windrichting 90° | 0 | 236 | 0 | 6520 | 0 | 0 |
| Windrichting 135° | -229 | 229 | 0 | 6749 | -6749 | 0 |

Project: RLL-TLB380
 Tower: HC+0_c - 140gr
 Number: 1187

Tussenresultaten geleiderbelastingen

Geleiders back

| Circuit | Geleider | Diameter [mm] | A [mm ²] | G [N/m] | E [N/mm ²] | αT [-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 2 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 3 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 4 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8 | 281,0 | 9,38 | 70165 | 1,97E-05 |
| Bliksemdraad 2 | OPGW AFL-226/38 | 21,7 | 264,0 | 9,13 | 72000 | 1,98E-05 |

Geleiders ahead

| Circuit | Geleider | Diameter [mm] | A [mm ²] | G [N/m] | E [N/mm ²] | αT [-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 2 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 3 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Circuit 4 | AAAC-AL7 620 | 32,4 | 621,0 | 17,71 | 56000 | 2,30E-05 |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8 | 281,0 | 9,38 | 70165 | 1,97E-05 |
| Bliksemdraad 2 | OPGW AFL-226/38 | 21,7 | 264,0 | 9,13 | 72000 | 1,98E-05 |

Verticale belasting back

| Circuit | Bundel [-] | Toeslag [%] | $W_{z,G}$ [N/m] | IJsgebied | Formule | $W_{z,ijs}$ [N/m] | $W_{z,ijs,bundel}$ [N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 2 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 3 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Circuit 4 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Bliksemdraad 1 | 1 | 2 | 9,6 | A | 15+0,4d | 23,7 | 23,7 |
| Bliksemdraad 2 | 1 | 2 | 9,3 | A | 15+0,4d | 23,7 | 23,7 |

Verticale belasting ahead

| Circuit | Bundel [-] | Toeslag [%] | $W_{z,G}$ [N/m] | IJsgebied | Formule | $W_{z,ijs}$ [N/m] | $W_{z,ijs,bundel}$ [N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 2 | 4 | 3 | 73,0 | B | 4+0,2d | 10,5 | 41,9 |
| Circuit 3 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Circuit 4 | 2 | 3 | 36,5 | B | 4+0,2d | 10,5 | 21,0 |
| Bliksemdraad 1 | 1 | 2 | 9,6 | A | 15+0,4d | 23,7 | 23,7 |
| Bliksemdraad 2 | 1 | 2 | 9,3 | A | 15+0,4d | 23,7 | 23,7 |

Isolatoren

| Geleider | $G_{isolator}$ [kN] | Aantal | $F_{v,iso}$ [kN] | Lengte [m] | Windopp. [m ²] | Windhoogte [m] | Stuwdruk [kN/m ²] | Vormfactor [-] | $F_{h,iso}$ [kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 3,00 | 1 | 3 | 6,5 | 1,1 | 48,50 | 1,13 | 1,2 | 1,49 |
| 380ct1f2 | 3,00 | 1 | 3 | 6,5 | 1,1 | 38,50 | 1,06 | 1,2 | 1,40 |
| 380ct1f3 | 3,00 | 1 | 3 | 6,5 | 1,1 | 29,00 | 0,98 | 1,2 | 1,29 |
| 380ct2f1 | 3,00 | 1 | 3 | 6,5 | 1,1 | 48,50 | 1,13 | 1,2 | 1,49 |
| 380ct2f2 | 3,00 | 1 | 3 | 6,5 | 1,1 | 38,50 | 1,06 | 1,2 | 1,40 |
| 380ct2f3 | 3,00 | 1 | 3 | 6,5 | 1,1 | 29,00 | 0,98 | 1,2 | 1,29 |
| 150ct3f1 | 2,00 | 1 | 2 | 4,5 | 0,8 | 48,50 | 1,13 | 1,2 | 1,08 |
| 150ct3f2 | 2,00 | 1 | 2 | 4,5 | 0,8 | 38,50 | 1,06 | 1,2 | 1,02 |
| 150ct3f3 | 2,00 | 1 | 2 | 4,5 | 0,8 | 29,00 | 0,98 | 1,2 | 0,94 |
| 150ct4f1 | 2,00 | 1 | 2 | 4,5 | 0,8 | 48,50 | 1,13 | 1,2 | 1,08 |
| 150ct4f2 | 2,00 | 1 | 2 | 4,5 | 0,8 | 38,50 | 1,06 | 1,2 | 1,02 |
| 150ct4f3 | 2,00 | 1 | 2 | 4,5 | 0,8 | 29,00 | 0,98 | 1,2 | 0,94 |
| bl1 | 0,10 | 1 | 0,1 | 0,2 | 0,1 | 53,60 | 1,16 | 1,2 | 0,14 |
| bl2 | 0,10 | 1 | 0,1 | 0,2 | 0,1 | 53,60 | 1,16 | 1,2 | 0,14 |

Project: RLL-TLB380
 Tower: HC+0_c - 140gr
 Number: 1187

Windbelasting back

| Geleider | hoogte | | G _{c,dwars} | G _{c,trek} | C _c | d _{toeslag} | W _y | W _{y,vak} | D _{jjs,toeslag} | W _{y,ijs} | W _{y,ijs,vak} |
|----------|--------|----------------------|----------------------|---------------------|----------------|----------------------|----------------|--------------------|--------------------------|--------------------|------------------------|
| | wind | Stuwdruk | | | | | | | | | |
| | [m] | [kN/m ²] | [-] | [-] | [-] | [mm] | [N/m] | [N/m] | [mm] | [N/m] | [N/m] |
| 380ct1f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 89,8 | 98,8 | 51,8 | 174,5 | 191,9 |
| 380ct1f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 84,0 | 92,4 | 51,8 | 159,9 | 175,9 |
| 380ct1f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 77,1 | 84,9 | 51,8 | 143,2 | 157,6 |
| 380ct2f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 89,8 | 98,8 | 51,8 | 174,5 | 191,9 |
| 380ct2f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 84,0 | 92,4 | 51,8 | 159,9 | 175,9 |
| 380ct2f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 77,1 | 84,9 | 51,8 | 143,2 | 157,6 |
| 150ct3f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 44,9 | 49,4 | 51,8 | 87,3 | 95,9 |
| 150ct3f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 42,0 | 46,2 | 51,8 | 79,9 | 88,0 |
| 150ct3f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 38,6 | 42,4 | 51,8 | 71,6 | 78,8 |
| 150ct4f1 | 50,1 | 1,14 | 0,62 | 0,68 | 0,96 | 33,37 | 44,9 | 49,4 | 51,8 | 87,3 | 95,9 |
| 150ct4f2 | 40,1 | 1,07 | 0,60 | 0,66 | 0,98 | 33,37 | 42,0 | 46,2 | 51,8 | 79,9 | 88,0 |
| 150ct4f3 | 30,6 | 0,99 | 0,58 | 0,64 | 1,00 | 33,37 | 38,6 | 42,4 | 51,8 | 71,6 | 78,8 |
| bl1 | 55,2 | 1,17 | 0,62 | 0,69 | 1,18 | 22,24 | 19,1 | 21,0 | 63,1 | 55,2 | 60,6 |
| bl2 | 55,2 | 1,17 | 0,62 | 0,69 | 1,18 | 22,13 | 19,0 | 20,9 | 63,0 | 55,1 | 60,5 |

Windbelasting ahead

| Geleider | hoogte | | G _{c,dwars} | G _{c,trek} | C _c | d _{toeslag} | W _y | W _{y,vak} | D _{jjs,toeslag} | W _{y,ijs} | W _{y,ijs,vak} |
|----------|--------|----------------------|----------------------|---------------------|----------------|----------------------|----------------|--------------------|--------------------------|--------------------|------------------------|
| | wind | Stuwdruk | | | | | | | | | |
| | [m] | [kN/m ²] | [-] | [-] | [-] | [mm] | [N/m] | [N/m] | [mm] | [N/m] | [N/m] |
| 380ct1f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 86,5 | 95,1 | 51,8 | 166,0 | 182,6 |
| 380ct1f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 79,9 | 87,9 | 51,8 | 149,7 | 164,8 |
| 380ct1f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 71,7 | 78,9 | 51,8 | 130,4 | 143,6 |
| 380ct2f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 86,5 | 95,1 | 51,8 | 166,0 | 182,6 |
| 380ct2f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 79,9 | 87,9 | 51,8 | 149,7 | 164,8 |
| 380ct2f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 71,7 | 78,9 | 51,8 | 130,4 | 143,6 |
| 150ct3f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 43,2 | 47,6 | 51,8 | 83,0 | 91,3 |
| 150ct3f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 39,9 | 43,9 | 51,8 | 74,9 | 82,4 |
| 150ct3f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 35,8 | 39,5 | 51,8 | 65,2 | 71,8 |
| 150ct4f1 | 44,1 | 1,10 | 0,61 | 0,67 | 0,97 | 33,37 | 43,2 | 47,6 | 51,8 | 83,0 | 91,3 |
| 150ct4f2 | 34,1 | 1,02 | 0,59 | 0,65 | 0,99 | 33,37 | 39,9 | 43,9 | 51,8 | 74,9 | 82,4 |
| 150ct4f3 | 24,6 | 0,93 | 0,56 | 0,62 | 1,02 | 33,37 | 35,8 | 39,5 | 51,8 | 65,2 | 71,8 |
| bl1 | 49,2 | 1,13 | 0,62 | 0,68 | 1,19 | 22,24 | 18,4 | 20,2 | 63,1 | 52,8 | 58,0 |
| bl2 | 49,2 | 1,13 | 0,62 | 0,68 | 1,19 | 22,13 | 18,3 | 20,1 | 63,0 | 52,7 | 57,9 |

NB: belastingen w_v gelden voor bundel

Project: RLL-TLB380
 Masttype: HC+0_c - 140gr
 Mast: 1187

Auteur: TBR
 Versie: v12.0

Geleiderbelastingen

Uitgangspunten

Betrouwbaarheidsniveau Nieuwbouw CC2
 Referentieperiode 50 jaar

| ULS (bezwijksterkte) | | NEN-EN50341-2-15:2019 | | | | | | | |
|--|---------------------------|-----------------------|--------------|---------------------|--|----------|----------|---------------------|--|
| Belastingsgeval | omschrijving | Temp °C | γ_G | | γ_Q | | | γ_a A_k | |
| | | | $G_{k,mast}$ | $G_{k,geleider}$ | Q_{pk} | Q_{wk} | Q_{ik} | | |
| ULS 1a | Wind | 10° | 1,20 | 1,20 | 0,00 | 1,50 | 0,00 | 0,0 | |
| ULS 1a_0,9 | Wind 0,9Gk alleen mast | 10° | 0,90 | 1,20 | 0,00 | 1,50 | 0,00 | 0,0 | |
| ULS 1a_0,9_0,9 | Wind 0,9Gk ook geleider | 10° | 0,90 | 0,90 | 0,00 | 1,50 | 0,00 | 0,0 | |
| ULS 3 | Wind+ijs | -5° | 1,20 | 1,20 | 0,00 | 0,45 | 1,50 | 0,0 | |
| ULS 3_0,9 | Wind+ijs 0,9 | -5° | 0,90 | 1,20 | 0,00 | 0,45 | 1,50 | 0,0 | |
| ULS 4 | Koude+wind | -20° | 1,20 | 1,20 | 0,00 | 0,30 | 0,00 | 0,0 | |
| ULS 4_0,9 | Koude+wind 0,9 | -20° | 0,90 | 1,20 | 0,00 | 0,30 | 0,00 | 0,0 | |
| ULS 5a | Torsiebelastingen | 10° | 1,00 | 1,00 | 1,00 | 0,00 | 0,00 | 1,0 | |
| ULS 5b | Longitudinale belastingen | 10° | 1,00 | 1,00 | 0,00 | 0,00 | 0,00 | 1,0 | |
| ULS 6 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 1,50 | 0,30 | 0,00 | 0,0 | |
| ULS 6_0,9 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 0,00 | 0,30 | 0,00 | 0,0 | |
| ULS 7 | Permanent | 10° | 1,35 | 1,35 | 0,00 | 0,00 | 0,00 | 0,0 | |
| ULS 8 | Special | 10° | 1,00 | 1,00 | 0,00 | 0,00 | 0,00 | 1,0 | |
| SPLS (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) | | | | γ_G G_k | γ_Q Q_{pk} Q_{wk} Q_{ik} | | | A_k | |
| SPLS 1a | Wind | 10° | 1,20 | 1,20 | 0,0 | 0,78 | 0,00 | 0,0 | |
| SPLS 1a_0,9 | Wind 0,9 | 10° | 0,90 | 1,20 | 0,0 | 0,78 | 0,00 | 0,0 | |
| SPLS 1a_0,9_0,9 | Wind 0,9 | 10° | 0,90 | 0,90 | 0,0 | 0,78 | 0,00 | 0,0 | |
| SPLS 3 | Wind+ijs | -5° | 1,20 | 1,20 | 0,0 | 0,36 | 0,34 | 0,0 | |
| SPLS 3_0,9 | Wind+ijs 0,9 | -5° | 0,90 | 1,20 | 0,0 | 0,36 | 0,34 | 0,0 | |
| SPLS 4 | Koude+wind | -20° | 1,20 | 1,20 | 0,0 | 0,24 | 0,00 | 0,0 | |
| SPLS 4_0,9 | Koude+wind 0,9 | -20° | 0,90 | 1,20 | 0,0 | 0,24 | 0,00 | 0,0 | |
| SPLS 6 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 1,2 | 0,24 | 0,0 | 0,0 | |
| SPLS 6_0,9 | Bouw en onderhoud | 5° | 1,20 | 1,20 | 0,0 | 0,24 | 0,0 | 0,0 | |
| SLS (controle van de vervormingen, vermoeiing, EDS) | | | | G_k | Q_{pk} | Q_{wk} | Q_{ik} | A_k | |
| SLS 1a | Wind | 10° | 1,00 | 1,00 | 0,0 | 1,00 | 0,0 | 0,0 | |
| SLS 3 | Wind+ijs | -5° | 1,00 | 1,00 | 0,0 | 0,30 | 1,00 | 0,0 | |
| SLS 4 | Wind | -20° | 1,00 | 1,00 | 0,0 | 0,20 | 0,0 | 0,0 | |
| SLS 6 | Bouw en onderhoud | 5° | 1,00 | 1,00 | 0,0 | 0,20 | 0,0 | 0,0 | |
| SLS 7 | PB (EDS, geen wind) | 10° | 1,00 | 1,00 | 0,0 | 0,00 | 0,0 | 0,0 | |

Aantal windrichtingen 6
 Aantal belastingcombinaties ULS 100
 Aantal belastingcombinaties SPLS 246
 Aantal belastingcombinaties SLS 15
 Aantal knooplasten 12274

Project: RLL-TLB380
 Masttype: HC+0_c - 140gr
 Mast: 1187

Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

Maximale waarden voor back en ahead span

| Geleider | Fx_ba [kN] | Fx_ah [kN] | Fy_ba [kN] | Fy_ah [kN] | Fz_ba [kN] | Fz_ah [kN] |
|--------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1 | -61,8 | 61,4 | 27,8 | 27,5 | 11,1 | 11,0 |
| 380ct1f1 | -249,6 | 247,6 | 115,6 | 112,9 | 39,8 | 39,7 |
| 380ct1f2 | -246,2 | 244,1 | 110,8 | 107,4 | 39,7 | 39,6 |
| 380ct1f3 | -242,7 | 240,3 | 105,1 | 100,7 | 39,6 | 39,5 |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| 380ct2f1 | -249,6 | 247,6 | 115,6 | 112,9 | 39,8 | 39,7 |
| 380ct2f2 | -246,2 | 244,1 | 110,8 | 107,4 | 39,7 | 39,6 |
| 380ct2f3 | -242,7 | 240,3 | 105,1 | 100,7 | 39,6 | 39,5 |
| 150ct3f1 | -124,7 | 123,8 | 58,3 | 56,9 | 21,3 | 21,3 |
| 150ct3f2 | -123,1 | 122,0 | 55,9 | 54,2 | 21,3 | 21,3 |
| 150ct3f3 | -121,3 | 120,1 | 53,0 | 50,8 | 21,3 | 21,3 |
| 150ct4f1 | -124,7 | 123,8 | 58,3 | 56,9 | 21,3 | 21,3 |
| 150ct4f2 | -123,1 | 122,0 | 55,9 | 54,2 | 21,3 | 21,3 |
| 150ct4f3 | -121,3 | 120,1 | 53,0 | 50,8 | 21,3 | 21,3 |
| bl2 | -60,9 | 60,5 | 27,5 | 27,1 | 11,0 | 10,9 |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 0,0 | 0,0 | 0,0 | |

Min. Weight span (m)

Weight spar Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|-----------------|--------|-------|-------|
| bl1 | 483,1 | 497,1 | 481,0 |
| 380ct1f1 | 481,8 | 496,1 | 481,0 |
| 380ct1f2 | 481,7 | 495,8 | 481,0 |
| 380ct1f3 | 481,6 | 495,5 | 481,0 |
| Post-isolator 1 | | | |
| Post-isolator 2 | | | |
| Post-isolator 3 | | | |
| 380ct2f1 | 481,8 | 496,1 | 481,0 |
| 380ct2f2 | 481,7 | 495,8 | 481,0 |
| 380ct2f3 | 481,6 | 495,5 | 481,0 |
| 150ct3f1 | 481,8 | 496,1 | 481,0 |
| 150ct3f2 | 481,7 | 495,8 | 481,0 |
| 150ct3f3 | 481,6 | 495,5 | 481,0 |
| 150ct4f1 | 481,8 | 496,1 | 481,0 |
| 150ct4f2 | 481,7 | 495,8 | 481,0 |
| 150ct4f3 | 481,6 | 495,5 | 481,0 |
| bl2 | 483,2 | 497,3 | 481,0 |
| Post-isolator 4 | | | |
| Post-isolator 5 | | | |
| Post-isolator 6 | | | |

Max. Weight span (m)

Weight spar Combinatie1

| Geleider | ULS 1a | ULS 3 |
|-----------------|--------|-------|
| bl1 | 564,6 | 463,1 |
| 380ct1f1 | 522,6 | 479,3 |
| 380ct1f2 | 518,2 | 478,3 |
| 380ct1f3 | 512,8 | 477,2 |
| Post-isolator 1 | | |
| Post-isolator 2 | | |
| Post-isolator 3 | | |
| 380ct2f1 | 522,6 | 479,3 |
| 380ct2f2 | 518,2 | 478,3 |
| 380ct2f3 | 512,8 | 477,2 |
| 150ct3f1 | 522,6 | 479,3 |
| 150ct3f2 | 518,2 | 478,3 |
| 150ct3f3 | 512,8 | 477,2 |
| 150ct4f1 | 522,6 | 479,3 |
| 150ct4f2 | 518,2 | 478,3 |
| 150ct4f3 | 512,8 | 477,2 |
| bl2 | 567,0 | 462,7 |
| Post-isolator 4 | | |
| Post-isolator 5 | | |
| Post-isolator 6 | | |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

| | |
|------------------|---------|
| Max. weight span | 564,6 m |
| Min. weight span | 110,0 m |

Wind / Weight span verhouding

| |
|---------|
| 1,412 - |
| 0,275 - |

Project: RLL-TLB380
 Masttype: HC+0_c - 140gr
 Mast: 1187

Maximale waarden back+ahead span Maximale waarden trekkracht geleider

| Geleider | Fx | Fy | Fz | Ft_ba | Ft_ah |
|--------------|-------|-------|------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] |
| bl1 | 36,7 | 53,3 | 11,1 | -67,6 | 67,1 |
| 380ct1f1 | 195,1 | 210,8 | 39,8 | -271,5 | 269,2 |
| 380ct1f2 | 191,4 | 203,2 | 39,7 | -267,5 | 264,9 |
| 380ct1f3 | 187,5 | 198,1 | 39,6 | -263,3 | 260,2 |
| Post-isolato | 4,2 | 4,2 | 6,8 | 0,0 | |
| Post-isolato | 3,2 | 3,2 | 4,7 | 0,0 | |
| Post-isolato | 4,9 | 4,9 | 6,8 | 0,0 | |
| 380ct2f1 | 195,1 | 210,8 | 39,8 | -271,5 | 269,2 |
| 380ct2f2 | 191,4 | 203,2 | 39,7 | -267,5 | 264,9 |
| 380ct2f3 | 187,5 | 198,1 | 39,6 | -263,3 | 260,2 |
| 150ct3f1 | 102,8 | 106,2 | 21,3 | -135,8 | 134,6 |
| 150ct3f2 | 102,7 | 101,9 | 21,3 | -133,8 | 132,4 |
| 150ct3f3 | 102,7 | 99,3 | 21,3 | -131,6 | 130,1 |
| 150ct4f1 | 102,8 | 106,2 | 21,3 | -135,8 | 134,6 |
| 150ct4f2 | 102,7 | 101,9 | 21,3 | -133,8 | 132,4 |
| 150ct4f3 | 102,7 | 99,3 | 21,3 | -131,6 | 130,1 |
| bl2 | 36,2 | 52,7 | 11,0 | -66,7 | 66,1 |
| Post-isolato | 4,2 | 4,2 | 6,8 | 0,0 | |
| Post-isolato | 3,2 | 3,2 | 4,7 | 0,0 | |
| Post-isolato | 4,9 | 4,9 | 6,8 | 0,0 | |

EDS-belastingen geleiders

| Geleider | Fx | Fy | Fz | Ft_ba | Ft_ah |
|--------------|-------|------|------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] |
| bl1 | 16,2 | 5,9 | 2,4 | -17,2 | 17,2 |
| 380ct1f1 | 123,4 | 44,9 | 20,5 | -131,3 | 131,3 |
| 380ct1f2 | 123,4 | 44,9 | 20,5 | -131,3 | 131,3 |
| 380ct1f3 | 123,4 | 44,9 | 20,5 | -131,3 | 131,3 |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 3,5 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |
| 380ct2f1 | 123,4 | 44,9 | 20,5 | -131,3 | 131,3 |
| 380ct2f2 | 123,4 | 44,9 | 20,5 | -131,3 | 131,3 |
| 380ct2f3 | 123,4 | 44,9 | 20,5 | -131,3 | 131,3 |
| 150ct3f1 | 61,7 | 22,5 | 10,8 | -65,7 | 65,7 |
| 150ct3f2 | 61,7 | 22,5 | 10,8 | -65,7 | 65,7 |
| 150ct3f3 | 61,7 | 22,5 | 10,8 | -65,7 | 65,7 |
| 150ct4f1 | 61,7 | 22,5 | 10,8 | -65,7 | 65,7 |
| 150ct4f2 | 61,7 | 22,5 | 10,8 | -65,7 | 65,7 |
| 150ct4f3 | 61,7 | 22,5 | 10,8 | -65,7 | 65,7 |
| bl2 | 15,7 | 5,7 | 2,3 | -16,8 | 16,8 |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 3,5 | 0,0 | |
| Post-isolato | 0,0 | 0,0 | 5,0 | 0,0 | |

Controle uplift SLS-wind

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
| | [kN] | [kN] |
| SLS 4 | | |
| bl1 | 0,0 | 0,0 |
| 380ct1f1 | 0,0 | 0,0 |
| 380ct1f2 | 0,0 | 0,0 |
| 380ct1f3 | 0,0 | 0,0 |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |
| 380ct2f1 | 0,0 | 0,0 |
| 380ct2f2 | 0,0 | 0,0 |
| 380ct2f3 | 0,0 | 0,0 |
| 150ct3f1 | 0,0 | 0,0 |
| 150ct3f2 | 0,0 | 0,0 |
| 150ct3f3 | 0,0 | 0,0 |
| 150ct4f1 | 0,0 | 0,0 |
| 150ct4f2 | 0,0 | 0,0 |
| 150ct4f3 | 0,0 | 0,0 |
| bl2 | 0,0 | 0,0 |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |
| Post-isolato | 0,0 | |

Project: RLL-TLB380
 Masttype: HC+0_c - 140gr
 Mast: 1187

ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders

| Combinatie | Combination | F_x | F_y | F_z | M_x | M_y | M_z |
|-------------------|-------------|-------|-------|-------|-------|-------|-------|
| | | [kN] | [kN] | [kN] | [kNm] | [kNm] | [kNm] |
| ULS 1a_90 | | -49 | 1916 | 526 | 74870 | -1824 | 0 |
| ULS 1a_0,9_0 | | 43 | 978 | 335 | 37764 | 1684 | 0 |
| ULS 1a_0,9_0,9_90 | | -55 | 1826 | 200 | 71459 | -2043 | 0 |
| ULS 3_0 | | 18 | 1591 | 789 | 61941 | 722 | 0 |
| SLS 7 | | 0 | 832 | 412 | 32092 | 0 | 0 |

ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast

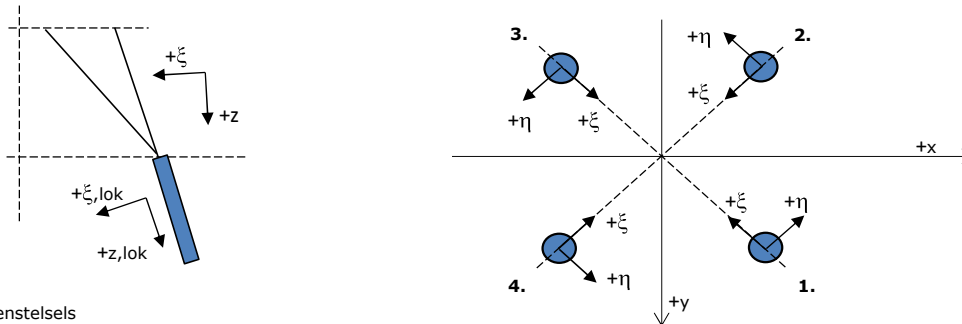
| Combinatie | F_x | F_y | F_z | M_x | M_y | M_z |
|-------------------|-------|-------|-------|-------|-------|-------|
| | [kN] | [kN] | [kN] | [kNm] | [kNm] | [kNm] |
| ULS 1a_90 | -49 | 2270 | 1751 | 84650 | -1824 | 0 |
| ULS 1a_0,9_0,9_90 | -55 | 2180 | 1119 | 81238 | -2043 | 0 |
| SLS 7 | 0 | 832 | 1434 | 32092 | 0 | 0 |

Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde

| Combinatie | F_x | F_y | F_z | M_x | M_y | M_z |
|--------------------------|-------|-------|-------|--------------|---------------|---------------|
| | [kN] | [kN] | [kN] | [kNm] | [kNm] | [kNm] |
| ULS 1a_0,9_90 | -49 | 2270 | 1210 | 84651 | -1824 | 0 |
| SPLS 3_70 Ah All Cts | -1760 | 818 | 1562 | 30867 | -68826 | 9 |
| SPLS 3_70 Ba Ct1 | 789 | 1096 | 1675 | 42893 | 30078 | -10169 |
| SPLS 3_0,9_70 Ah All Cts | -1760 | 818 | 1118 | 30868 | -68826 | 9 |

Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.

Oplegreacties op fundering per randstijl



Assenstelsels

Maximale drukbelasting

| Stijl | Combinatie | R_x | R_y | R_z | R_η | R_ξ | $R_{\xi,lok}$ | $R_{z,lok}$ |
|-------|-----------------------|-------|-------|-------------|----------|---------|---------------|-------------|
| | | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] |
| 1 | SPLS 3_110 Ba All Cts | 786 | 887 | 4571 | -71 | -1183 | 45 | 4733 |
| 2 | SPLS 3_0 Ba All Cts | 312 | -517 | 2218 | 144 | -586 | 10 | 2296 |
| 3 | ULS 8 Ba | -294 | -510 | 2165 | -153 | -568 | 13 | 2242 |
| 4 | SPLS 3_70 Ah All Cts | -796 | 898 | 4629 | 72 | -1198 | 46 | 4793 |

Maximale trekbelasting

| Stijl | Combinatie | R_x | R_y | R_z | R_η | R_ξ | $R_{\xi,lok}$ | $R_{z,lok}$ |
|-------|---------------------------|-------|-------|--------------|----------|---------|---------------|-------------|
| | | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] |
| 1 | ULS 8 Ba | -136 | -353 | -1411 | 154 | 346 | -34 | -1461 |
| 2 | SPLS 3_0,9_90 Ba Ct2 | -656 | 757 | -3959 | -72 | 999 | -64 | -4099 |
| 3 | SPLS 3_0,9_110 Ba All Cts | 643 | 743 | -3886 | 71 | 980 | -64 | -4024 |
| 4 | SPLS 3_0,9_0 Ba All Cts | 169 | -374 | -1534 | -145 | 384 | -28 | -1588 |

Maximale torsiebelasting (positief)

| Stijl | Combinatie | R_x | R_y | R_z | R_η | R_ξ | $R_{\xi,lok}$ | $R_{z,lok}$ |
|-------|-----------------------|-------|-------|-------|------------|---------|---------------|-------------|
| | | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] |
| 1 | SPLS 3_90 Ah Ct1 | 469 | -143 | 843 | 433 | -230 | -4 | 873 |
| 2 | SPLS 3_0,9_90 Ba Ct2 | -308 | -288 | -78 | 422 | 14 | -7 | -81 |
| 3 | SPLS 3_70 Ba Ct2 | 252 | 669 | -2571 | 295 | 651 | -40 | -2663 |
| 4 | SPLS 3_0,9_110 Ah Ct1 | -429 | 824 | 3419 | 279 | -887 | 32 | 3541 |

Maximale torsiebelasting (negatief)

| Index | Combinatie | R_x | R_y | R_z | R_η | R_ξ | $R_{\xi,lok}$ | $R_{z,lok}$ |
|-------|----------------------|-------|-------|-------|-------------|---------|---------------|-------------|
| | | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] |
| 1 | SPLS 3_0,9_70 Ba Ct1 | 420 | 821 | 3378 | -284 | -878 | 30 | 3498 |
| 2 | SPLS 3_110 Ah Ct2 | -260 | 674 | -2605 | -293 | 660 | -40 | -2697 |
| 3 | SPLS 3_0,9_90 Ah Ct2 | 299 | -293 | -32 | -419 | 4 | -4 | -33 |
| 4 | SPLS 3_90 Ba Ct1 | -477 | -137 | 883 | -434 | -240 | -3 | 914 |

Project: RLL-TLB380
 Masttype: HC+0_c - 140gr
 Mast: 1187

Combinatie Ftrek+Fhor

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | ULS 8 Ba | -136 | -353 | -1411 | 154 | 346 | -34 | -1461 |
| 2 | SPLS 3_0,9_70 Ah All Cts | -656 | 757 | -3959 | -72 | 999 | -64 | -4099 |
| 3 | SPLS 3_0,9_110 Ba All Cts | 643 | 743 | -3886 | 71 | 980 | -64 | -4024 |
| 4 | SPLS 3_0,9_0 Ba All Cts | 169 | -374 | -1534 | -145 | 384 | -28 | -1588 |

Permanente belasting

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SLS 7 | 360 | 283 | 1723 | 55 | -455 | 8 | 1784 |
| 2 | SLS 7 | -210 | 133 | -1006 | 55 | 243 | -28 | -1041 |
| 3 | SLS 7 | 210 | 133 | -1006 | -55 | 243 | -28 | -1041 |
| 4 | SLS 7 | -360 | 283 | 1723 | -55 | -455 | 8 | 1784 |

Omhullenden ongeacht stijl

| Belasting | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------------------|--------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk | SPLS 3_70 Ah All Cts | -796 | 898 | 4629 | 72 | -1198 | 46 | 4793 |
| Max. trek | SPLS 3_0,9_70 Ah All Cts | -656 | 757 | -3959 | -72 | 999 | -64 | -4099 |
| Max. pos. torsie | SPLS 3_90 Ah Ct1 | 469 | -143 | 843 | 433 | -230 | -4 | 873 |
| Max. neg. torsie | SPLS 3_90 Ba Ct1 | -477 | -137 | 883 | -434 | -240 | -3 | 914 |
| Comb. trek+torsie | SPLS 3_0,9_70 Ah All Cts | -656 | 757 | -3959 | -72 | 999 | -64 | -4099 |

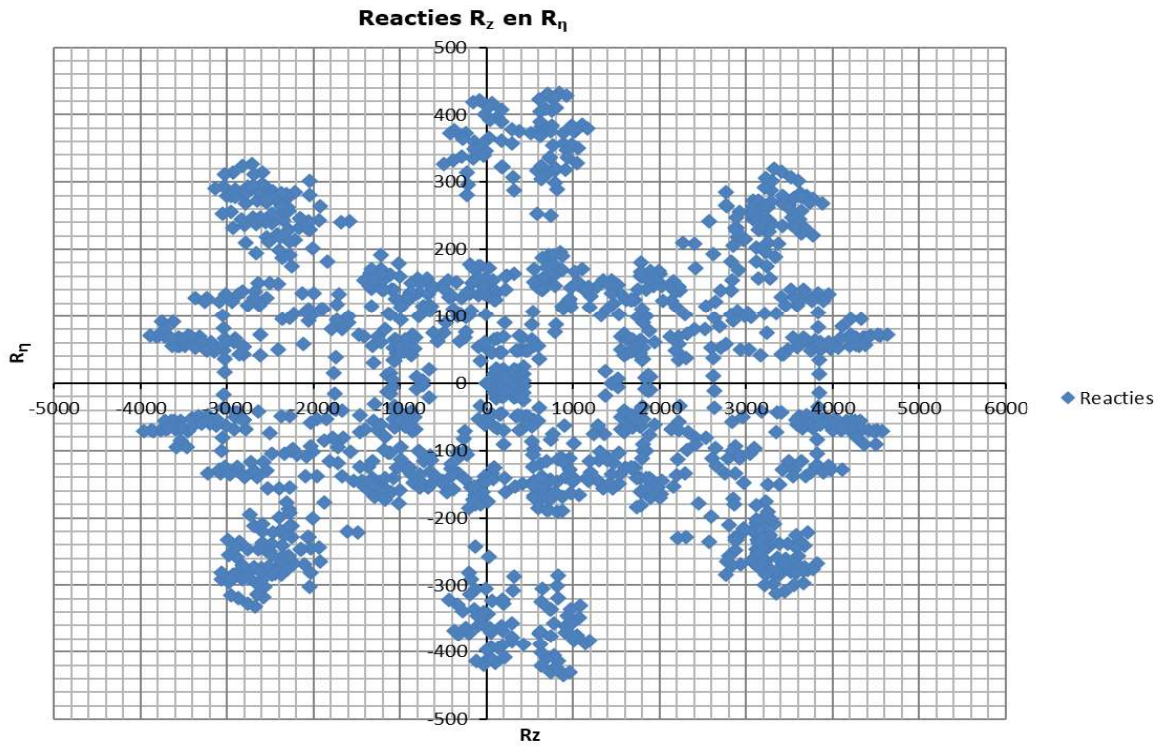
Maximale trekbelasting SLS

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SPLS 3_0,9_70 Ah All Cts | -107 | -349 | -1334 | 171 | 323 | -36 | -1382 |
| 2 | SPLS 3_0,9_70 Ah All Cts | -656 | 757 | -3959 | -72 | 999 | -64 | -4099 |
| 3 | SPLS 3_0,9_110 Ba All Cts | 643 | 743 | -3886 | 71 | 980 | -64 | -4024 |
| 4 | SPLS 3_0,9_110 Ba All Cts | 102 | -341 | -1300 | -169 | 313 | -36 | -1346 |

Maximale drukbelasting SLS

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SPLS 3_110 Ba All Cts | 786 | 887 | 4571 | -71 | -1183 | 45 | 4733 |
| 2 | SPLS 3_110 Ba All Cts | 246 | -483 | 1984 | 168 | -516 | 18 | 2055 |
| 3 | SPLS 3_70 Ah All Cts | -248 | -489 | 2004 | -170 | -521 | 18 | 2075 |
| 4 | SPLS 3_70 Ah All Cts | -796 | 898 | 4629 | 72 | -1198 | 46 | 4793 |

Project: RLL-TLB380
Masttype: HC+0_c - 140gr
Mast: 1187



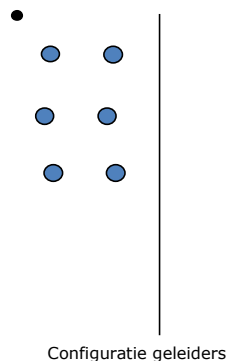
Project: RLL-TLB380
 Tower: HC+0_c - bouwfase
 Number: 1187

Auteur: TBR
 Versie: v12.0

Geleiderbelastingen

Algemeen

Benaming HC+0_c - bouwfase
 Masttype Hoekmast
 Aantal circuits 2
 Configuratie 2-circuit-verticaal
 Aantal bliksemgeleiders 1



Uitgangspunten

Norm NEN-EN50341-2-15:2019
 Gevolgklasse initieel CC2
 Betrouwbaarheidsniveau initieel Nieuwbouw
 Referentieperiode initieel 15 jaar
 Betrouwbaarheidsniveau na aanpassing n.v.t.
 15 jaar
 Windgebied III
 Windsnelheid (m/s) 24.5 m/s
 Terreincategorie II
 Reductiefactor C_{dir} 1.00
 IJsg gebied fasegeleider B
 IJsg gebied bliksemgeleider A

Geleiders Back

| Omschrijving | Spanning | Geleider Back | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden P_{back} |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 2 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Bliksemdraad 1 | | AACSR 241-AL3-39-A20SA | 1 | A | 2 % | 2 % | 1800 |

Geleiders Ahead

| Omschrijving | Spanning | Geleider Ahead | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden P_{ahead} |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1 | 380 kV | AAAC-AL7 620 | 4 | B | 3 % | 3 % | 1800 |
| Circuit 2 | 150 kV | AAAC-AL7 620 | 2 | B | 3 % | 3 % | 1800 |
| Bliksemdraad 1 | | AACSR 241-AL3-39-A20SA | 1 | A | 2 % | 2 % | 1800 |

Isolatoren (1)

| Omschrijving | Ophanging | Gewicht [kN] | Lengte [m] | Windopp. [m ²] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1 | Afspanketting | 3.00 | 6.50 | 1.10 |
| Circuit 2 | Afspanketting | 3.00 | 6.50 | 1.10 |
| Bliksemdraad 1 | Afspanketting | 0.10 | 0.20 | 0.10 |

1. Eigenschappen gelden voor geheel van de isolatorset

Ophanghoogte en positie in mast

| Circuits | Aanduiding | Nummer | Ophanghoogte | Aangrijppunt | Positie in mast Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1 | 10 | 380ct1f1 | 48.0 m | 48.0 m | -12.1 m |
| Circuit 1 | 11 | 380ct1f2 | 38.0 m | 38.0 m | -15.6 m |
| Circuit 1 | 12 | 380ct1f3 | 28.5 m | 28.5 m | -12.7 m |
| Circuit 2 | 40 | 150ct2f1 | 48.0 m | 48.0 m | -4.8 m |
| Circuit 2 | 41 | 150ct2f2 | 38.0 m | 38.0 m | -8.3 m |
| Circuit 2 | 42 | 150ct2f3 | 28.5 m | 28.5 m | -5.4 m |
| Bliksemdraad 1 | 1 | bl1 | 53.1 m | 53.1 m | -18.3 m |

Project: RLL-TLB380
 Tower: HC+0_c - bouwfase
 Number: 1187

Hoogteaanpassing naastgelegen masten (aanpassing wind- en weight span)

| | Back | Ahead | |
|------------------------------------|---------------------------|--------|---|
| Verhoging voor windbelasting | 18.0 m | 6.0 m | (positief: omhoog) |
| Verlaging voor verticale belasting | -9.0 m | -9.0 m | (negatief: omlaag, grotere weight span) |
| Verlaging: | Niet in 0,9EG-combinaties | | |

Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting

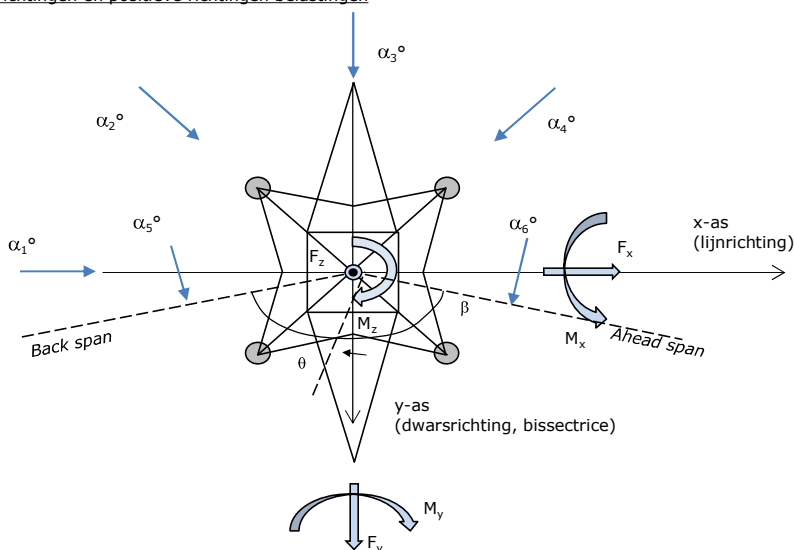
| Circuits | Aanduiding | Nummer | Hoogteverschil | | Richtingsverandering | |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
| | | | Δh back | Δh ahead | Δy back | Δy ahead |
| Circuit 1 | 10 | 380ct1f1 | 0.0 | 0.0 m | 0.0 | 0.0 m |
| Circuit 1 | 11 | 380ct1f2 | 0.0 | 0.0 m | 0.0 | 0.0 m |
| Circuit 1 | 12 | 380ct1f3 | 0.0 | 0.0 m | 0.0 | 0.0 m |
| Circuit 2 | 40 | 150ct2f1 | 0.0 | 0.0 m | 0.0 | 0.0 m |
| Circuit 2 | 41 | 150ct2f2 | 0.0 | 0.0 m | 0.0 | 0.0 m |
| Circuit 2 | 42 | 150ct2f3 | 0.0 | 0.0 m | 0.0 | 0.0 m |
| Bliksemdraad 1 | 1 | bl1 | 0.0 | 0.0 m | 0.0 | 0.0 m |

Lijn- en mastgegevens

| | Back | Ahead |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400.0 | 400.0 m |
| Lijnhoek | β | 140 ° |
| Rotatie mast t.o.v. bissectrice | θ | 0 ° |
| Vaklengte | 400 | 400 m |
| Hoogte onderkant mast t.o.v. maaiveld | 0.5 m | |
| Beschouwde windrichtingen | α_1 | 0 ° |
| Windrichtingen volgens: | α_2 | 45 ° |
| Geleiderbelastingen | α_3 | 90 ° |
| | α_4 | 135 ° |
| | α_5 | 70 ° |
| | α_6 | 110 ° |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



Beschouwd aantal windrichtingen

| | |
|--------|---|
| 1a | 6 |
| 3 | 6 |
| 4 | 1 |
| 6 | 1 |
| Overig | 1 |

Project: RLL-TLB380
 Tower: HC+0_c - bouwfase
 Number: 1187

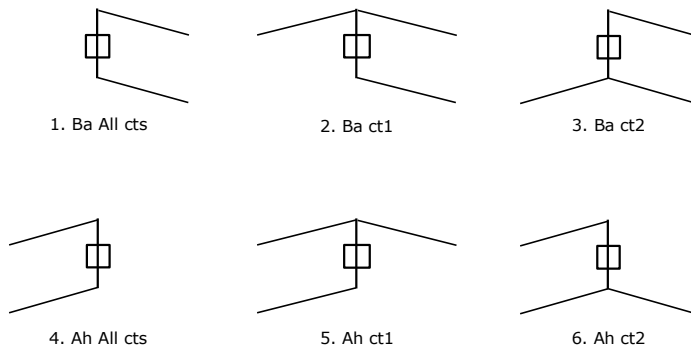
Geleiderafval

| | | SPLS - torsie | | SPLS - Enkelzijdige trek | | 5a - geleiderbreuk | |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
| | | Aanw. | Afw. | Aanw. | Afw. | Aanw. | Afw. |
| Circuit 1 | 380ct1f1 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 1 | 380ct1f2 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 1 | 380ct1f3 | 1 | 0 | 1 | 0 | 1 | 0 |
| Circuit 2 | 150ct2f1 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 2 | 150ct2f2 | 0 | 1 | 1 | 0 | 1 | 0 |
| Circuit 2 | 150ct2f3 | 0 | 1 | 1 | 0 | 1 | 0 |
| Bliksemdraad 1 | bl1 | 1 | 0 | 1 | 0 | 1 | 0 |

Belastingssituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

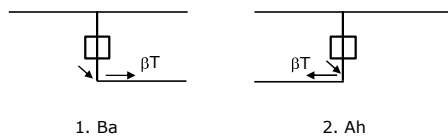
Principe belastingssituaties:



Belastingssituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



Project: RLL-TLB380
 Tower: HC+0_c - bouwfase
 Number: 1187

Belastingsituaties 6. Bouw- en onderhoud

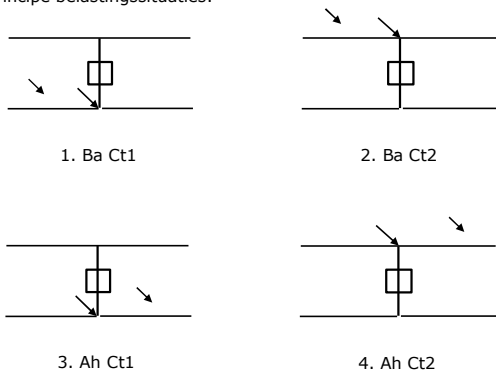
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

| | Fase | Bliksem |
|----------------------|--------|---------|
| Lijnwagen | 4.0 kN | 2.0 kN |
| Puntlast op traverse | 1.0 kN | 1.0 kN |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



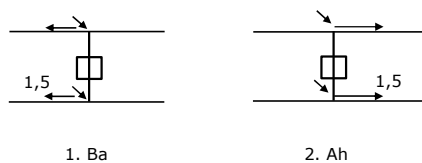
Belastingsituaties 8. Lijndansen als statische belasting

| Geleider | | |
|--------------------------|---------|-------|
| Steunmast fase | 0.866 W | 1.5 W |
| Steunmast bliksem | 1.5 EDS | 1.5 W |
| Hoekmast fase en bliksem | 1.5 EDS | 1.5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten
 Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast
 Door gebruiker via het belastingsspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

Project: RLL-TLB380
 Tower: HC+0_c - bouwfase
 Number: 1187

Mastconstructie

Eigenschappen

| | | |
|---|-------------------|---------|
| Masttype | Hoekmast | |
| Mastbenaming | HC+0_c - bouwfase | |
| Voetplaat t.o.v. maaiveld | 0.5 m | |
| Masthoogte t.o.v. voetplaat | 53.1 m | |
| Gewicht mast | 1021.2 kN | |
| <i>Breedte en helling mast bij fundatie</i> | | |
| | x-ri. | y-ri. |
| Pootsprei | 11.76 | 11.76 m |
| Helling van de randstijl | 0.190 | 0.190 - |
| Factor spatkracht | 1.1 | 1.1 - |

Berekening windbelasting

| | |
|---|---------------------------------------|
| Dynamische invloed G_T | 1.00 (<i>Masthoogte < 60 m</i>) |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam | $(1+0,2\sin^2(2\phi))$ |
| Vergroting wind overhoeks traverse | $(1+0,2\sin^2(2\phi))$ |
| Factor wind evenwijdig t.o.v. haaks op traverse | 0.4 |

Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving | h [m] | b ₁ [m] | b ₂ [m] | Δh [m] | Δ _x [m] | A ₀ [m ²] | A ₁ [m ²] | χ = A ₁ /A ₀ [-] | C _t |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk | 15.40 | 11.76 | 5.91 | 15.40 | 0.190 | 136.07 | 31.88 | 0.23 | 2.79 |
| Eerste tussenstuk | 22.20 | 5.91 | 5.23 | 6.80 | 0.050 | 37.88 | 13.58 | 0.36 | 2.34 |
| Tweede tussenstuk | 28.50 | 5.23 | 4.60 | 6.30 | 0.050 | 30.96 | 10.07 | 0.33 | 2.45 |
| Bovenstuk 1 | 38.00 | 4.60 | 3.65 | 9.50 | 0.050 | 39.19 | 12.64 | 0.32 | 2.46 |
| Bovenstuk 2 | 51.40 | 3.65 | 2.31 | 13.40 | 0.050 | 39.93 | 13.53 | 0.34 | 2.40 |
| Topstuk | 53.10 | 2.31 | | 1.70 | | 1.96 | 0.33 | 0.17 | 3.08 |
| Ondertraverse | 28.50 | 10.70 | | 3.10 | | 16.59 | 5.05 | 0.30 | 2.52 |
| Middentraverse | 38.00 | 14.08 | | 3.20 | | 22.52 | 6.95 | 0.31 | 2.50 |
| Boventraverse | 48.00 | 16.98 | | 5.10 | | 43.29 | 8.13 | 0.19 | 2.98 |

Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving | h [m] | b ₁ [m] | b ₂ [m] | Δh [m] | Δ _x [m] | A ₀ [m ²] | A ₁ [m ²] | χ = A ₁ /A ₀ [-] | C _t |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk | 15.40 | 11.76 | 5.91 | 15.40 | 0.190 | 136.07 | 31.88 | 0.23 | 2.79 |
| Eerste tussenstuk | 22.20 | 5.91 | 5.23 | 6.80 | 0.050 | 37.88 | 13.58 | 0.36 | 2.34 |
| Tweede tussenstuk | 28.50 | 5.23 | 4.60 | 6.30 | 0.050 | 30.96 | 10.07 | 0.33 | 2.45 |
| Bovenstuk 1 | 38.00 | 4.60 | 3.65 | 9.50 | 0.050 | 39.19 | 12.64 | 0.32 | 2.46 |
| Bovenstuk 2 | 51.40 | 3.65 | 2.31 | 13.40 | 0.050 | 39.93 | 13.53 | 0.34 | 2.40 |
| Topstuk | 53.10 | 2.31 | | 1.70 | | 1.96 | 0.33 | 0.17 | 3.08 |
| Ondertraverse | 28.50 | 10.70 | | 3.10 | | 16.59 | 5.05 | 0.30 | 2.52 |
| Middentraverse | 38.00 | 14.08 | | 3.20 | | 22.52 | 6.95 | 0.31 | 2.50 |
| Boventraverse | 48.00 | 16.98 | | 5.10 | | 43.29 | 8.13 | 0.19 | 2.98 |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traveses.

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Windoppervlak feeders telecominstallaties

| Onderdeel | A (m ² /m) | Factor | Δh | A ₁ |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk | 0.14 | 0.71 | 15.4 | 1.5 |
| Eerste tussenstuk | 0.14 | 0.71 | 6.8 | 0.7 |
| Tweede tussenstuk | 0.14 | 0.71 | 6.3 | 0.6 |
| Bovenstuk 1 | 0.14 | 0.71 | 9.5 | 0.9 |
| Bovenstuk 2 | | | | |

Invoer antennes

| Omschrijving | A (m ²) | h (m) | C _i (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top | | | |
| Antenne o.t. | 4.7 | 34.7 | 1.5 |

Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving | P _w [kN/m ²] | F _{x1} [kN] | F _{x2} [kN] | F _{x3} [kN] | F _{x4} [kN] | h _{ef} [m] | M _{y1} [kNm] | M _{y2} [kNm] | M _{y3} [kNm] | M _{y4} [kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk | 0.70 | 62.3 | 52.8 | 0.0 | -52.8 | 7.7 | 479.4 | 406.8 | 0.0 | -406.8 |
| Eerste tussenstuk | 0.86 | 27.4 | 23.2 | 0.0 | -23.2 | 18.8 | 514.6 | 436.6 | 0.0 | -436.6 |
| Tweede tussenstuk | 0.94 | 23.2 | 19.7 | 0.0 | -19.7 | 25.4 | 588.3 | 499.2 | 0.0 | -499.2 |
| Bovenstuk 1 | 1.02 | 31.7 | 26.9 | 0.0 | -26.9 | 33.3 | 1054.8 | 895.0 | 0.0 | -895.0 |
| Bovenstuk 2 | 1.10 | 35.8 | 30.4 | 0.0 | -30.4 | 44.7 | 1601.8 | 1359.2 | 0.0 | -1359.2 |
| Topstuk | 1.15 | 1.2 | 1.0 | 0.0 | -1.0 | 52.3 | 60.7 | 51.5 | 0.0 | -51.5 |
| Ondertraverse | 0.98 | 25.0 | 14.9 | 0.0 | -14.9 | 29.5 | 739.2 | 439.1 | 0.0 | -439.1 |
| Middentraverse | 1.06 | 37.0 | 22.0 | 0.0 | -22.0 | 39.1 | 1446.1 | 859.0 | 0.0 | -859.0 |
| Boventraverse | 1.13 | 55.0 | 32.7 | 0.0 | -32.7 | 49.7 | 2734.8 | 1624.4 | 0.0 | -1624.4 |
| Totaal | | 298.6 | 223.6 | 0.0 | -223.6 | | 9219.8 | 6570.8 | 0.0 | -6570.8 |

Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving | P _w [kN/m ²] | F _{y1} [kN] | F _{y2} [kN] | F _{y3} [kN] | F _{y4} [kN] | h _{ef} [m] | M _{x1} [kNm] | M _{x2} [kNm] | M _{x3} [kNm] | M _{x4} [kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk | 0.70 | 0.0 | 52.8 | 62.3 | 52.8 | 7.7 | 0.0 | 406.8 | 479.4 | 406.8 |
| Eerste tussenstuk | 0.86 | 0.0 | 23.2 | 27.4 | 23.2 | 18.8 | 0.0 | 436.6 | 514.6 | 436.6 |
| Tweede tussenstuk | 0.94 | 0.0 | 19.7 | 23.2 | 19.7 | 25.4 | 0.0 | 499.2 | 588.3 | 499.2 |
| Bovenstuk 1 | 1.02 | 0.0 | 26.9 | 31.7 | 26.9 | 33.3 | 0.0 | 895.0 | 1054.8 | 895.0 |
| Bovenstuk 2 | 1.10 | 0.0 | 30.4 | 35.8 | 30.4 | 44.7 | 0.0 | 1359.2 | 1601.8 | 1359.2 |
| Topstuk | 1.15 | 0.0 | 1.0 | 1.2 | 1.0 | 52.3 | 0.0 | 51.5 | 60.7 | 51.5 |
| Ondertraverse | 0.98 | 0.0 | 14.9 | 10.0 | 14.9 | 29.5 | 0.0 | 439.1 | 295.7 | 439.1 |
| Middentraverse | 1.06 | 0.0 | 22.0 | 14.8 | 22.0 | 39.1 | 0.0 | 859.0 | 578.5 | 859.0 |
| Boventraverse | 1.13 | 0.0 | 32.7 | 22.0 | 32.7 | 49.7 | 0.0 | 1624.4 | 1093.9 | 1624.4 |
| Totaal | | 0.0 | 223.6 | 228.4 | 223.6 | | 0.0 | 6570.8 | 6267.7 | 6570.8 |

Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F _x [kN] | F _y [kN] | F _z [kN] | M _x [kNm] | M _y [kNm] | M _z [kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting | 0 | 0 | 1021 | 0 | 0 | 0 |
| Windrichting 0° | 306 | 0 | 0 | 0 | 9472 | 0 |
| Windrichting 45° | 229 | 229 | 0 | 6749 | 6749 | 0 |
| Windrichting 90° | 0 | 236 | 0 | 6520 | 0 | 0 |
| Windrichting 135° | -229 | 229 | 0 | 6749 | -6749 | 0 |

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Tussenresultaten geleiderbelastingen

Geleiders back

| Circuit | Geleider | Diameter [mm] | A [mm ²] | G [N/m] | E [N/mm ²] | αT [-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1 | AAAC-AL7 620 | 32.4 | 621.0 | 17.71 | 56000 | 2.30E-05 |
| Circuit 2 | AAAC-AL7 620 | 32.4 | 621.0 | 17.71 | 56000 | 2.30E-05 |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21.8 | 281.0 | 9.38 | 70165 | 1.97E-05 |

Geleiders ahead

| Circuit | Geleider | Diameter [mm] | A [mm ²] | G [N/m] | E [N/mm ²] | αT [-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1 | AAAC-AL7 620 | 32.4 | 621.0 | 17.71 | 56000 | 2.30E-05 |
| Circuit 2 | AAAC-AL7 620 | 32.4 | 621.0 | 17.71 | 56000 | 2.30E-05 |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21.8 | 281.0 | 9.38 | 70165 | 1.97E-05 |

Verticale belasting back

| Circuit | Bundel [-] | Toeslag [%] | $W_{z,G}$ [N/m] | IJsgebied | Formule | $W_{z,ijs}$ [N/m] | $W_{z,ijs,bundel}$ [N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1 | 4 | 3 | 73.0 | B | 4+0,2d | 10.5 | 41.9 |
| Circuit 2 | 2 | 3 | 36.5 | B | 4+0,2d | 10.5 | 21.0 |
| Bliksemdraad 1 | 1 | 2 | 9.6 | A | 15+0,4d | 23.7 | 23.7 |

Verticale belasting ahead

| Circuit | Bundel [-] | Toeslag [%] | $W_{z,G}$ [N/m] | IJsgebied | Formule | $W_{z,ijs}$ [N/m] | $W_{z,ijs,bundel}$ [N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1 | 4 | 3 | 73.0 | B | 4+0,2d | 10.5 | 41.9 |
| Circuit 2 | 2 | 3 | 36.5 | B | 4+0,2d | 10.5 | 21.0 |
| Bliksemdraad 1 | 1 | 2 | 9.6 | A | 15+0,4d | 23.7 | 23.7 |

Isolatoren

| Geleider | $G_{isolator}$ [kN] | Aantal | $F_{v,iso}$ [kN] | Lengte [m] | Windopp. [m ²] | Windhoogte [m] | Stuwdruk [kN/m ²] | Vormfactor [-] | $F_{h,iso}$ [kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 3.00 | 1 | 3 | 6.5 | 1.1 | 48.50 | 1.13 | 1.2 | 1.49 |
| 380ct1f2 | 3.00 | 1 | 3 | 6.5 | 1.1 | 38.50 | 1.06 | 1.2 | 1.40 |
| 380ct1f3 | 3.00 | 1 | 3 | 6.5 | 1.1 | 29.00 | 0.98 | 1.2 | 1.29 |
| 150ct2f1 | 3.00 | 1 | 3 | 6.5 | 1.1 | 48.50 | 1.13 | 1.2 | 1.49 |
| 150ct2f2 | 3.00 | 1 | 3 | 6.5 | 1.1 | 38.50 | 1.06 | 1.2 | 1.40 |
| 150ct2f3 | 3.00 | 1 | 3 | 6.5 | 1.1 | 29.00 | 0.98 | 1.2 | 1.29 |
| bl1 | 0.10 | 1 | 0.1 | 0.2 | 0.1 | 53.60 | 1.16 | 1.2 | 0.14 |

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Windbelasting back

| Geleider | hoogte | | G_{c_dwars} | G_{c_trek} | C_c | $d_{toeslag}$ | w_y | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
| | wind | Stuwdruk | | | | | | | | | |
| | [m] | [kN/m ²] | [-] | [-] | [-] | [mm] | [N/m] | [N/m] | [mm] | [N/m] | [N/m] |
| 380ct1f1 | 50.1 | 1.14 | 0.62 | 0.68 | 0.96 | 33.37 | 89.8 | 98.8 | 51.8 | 174.5 | 191.9 |
| 380ct1f2 | 40.1 | 1.07 | 0.60 | 0.66 | 0.98 | 33.37 | 84.0 | 92.4 | 51.8 | 159.9 | 175.9 |
| 380ct1f3 | 30.6 | 0.99 | 0.58 | 0.64 | 1.00 | 33.37 | 77.1 | 84.9 | 51.8 | 143.2 | 157.6 |
| 150ct2f1 | 50.1 | 1.14 | 0.62 | 0.68 | 0.96 | 33.37 | 44.9 | 49.4 | 51.8 | 87.3 | 95.9 |
| 150ct2f2 | 40.1 | 1.07 | 0.60 | 0.66 | 0.98 | 33.37 | 42.0 | 46.2 | 51.8 | 79.9 | 88.0 |
| 150ct2f3 | 30.6 | 0.99 | 0.58 | 0.64 | 1.00 | 33.37 | 38.6 | 42.4 | 51.8 | 71.6 | 78.8 |
| bl1 | 55.2 | 1.17 | 0.62 | 0.69 | 1.18 | 22.24 | 19.1 | 21.0 | 63.1 | 55.2 | 60.6 |

Windbelasting ahead

| Geleider | hoogte | | G_{c_dwars} | G_{c_trek} | C_c | $d_{toeslag}$ | w_y | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
| | wind | Stuwdruk | | | | | | | | | |
| | [m] | [kN/m ²] | [-] | [-] | [-] | [mm] | [N/m] | [N/m] | [mm] | [N/m] | [N/m] |
| 380ct1f1 | 44.1 | 1.10 | 0.61 | 0.67 | 0.97 | 33.37 | 86.5 | 95.1 | 51.8 | 166.0 | 182.6 |
| 380ct1f2 | 34.1 | 1.02 | 0.59 | 0.65 | 0.99 | 33.37 | 79.9 | 87.9 | 51.8 | 149.7 | 164.8 |
| 380ct1f3 | 24.6 | 0.93 | 0.56 | 0.62 | 1.02 | 33.37 | 71.7 | 78.9 | 51.8 | 130.4 | 143.6 |
| 150ct2f1 | 44.1 | 1.10 | 0.61 | 0.67 | 0.97 | 33.37 | 43.2 | 47.6 | 51.8 | 83.0 | 91.3 |
| 150ct2f2 | 34.1 | 1.02 | 0.59 | 0.65 | 0.99 | 33.37 | 39.9 | 43.9 | 51.8 | 74.9 | 82.4 |
| 150ct2f3 | 24.6 | 0.93 | 0.56 | 0.62 | 1.02 | 33.37 | 35.8 | 39.5 | 51.8 | 65.2 | 71.8 |
| bl1 | 49.2 | 1.13 | 0.62 | 0.68 | 1.19 | 22.24 | 18.4 | 20.2 | 63.1 | 52.8 | 58.0 |

NB: belastingen w_v gelden voor bundel

Project: RLL-TLB380
 Masttype: HC+0_c - bouwfase
 Mast: 1187

Auteur: TBR
 Versie: v12.0

Geleiderbelastingen

Uitgangspunten

Betrouwbaarheidsniveau Nieuwbouw CC2
 Referentieperiode 15 jaar

| ULS (bezwijksterkte) | | NEN-EN50341-2-15:2019 | | | | | | | |
|--|---------------------------|-----------------------|--------------|------------------|------------|----------|----------|---------------------|--|
| Belastingsgeval | omschrijving | Temp °C | γ_G | | γ_Q | | | γ_a A_k | |
| | | | $G_{k,mast}$ | $G_{k,geleider}$ | Q_{pk} | Q_{wk} | Q_{ik} | | |
| ULS 1a | Wind | 10° | 1.20 | 1.20 | 0.00 | 1.25 | 0.00 | 0.0 | |
| ULS 1a_0,9 | Wind 0,9Gk alleen mast | 10° | 0.90 | 1.20 | 0.00 | 1.25 | 0.00 | 0.0 | |
| ULS 1a_0,9_0,9 | Wind 0,9Gk ook geleider | 10° | 0.90 | 0.90 | 0.00 | 1.25 | 0.00 | 0.0 | |
| ULS 3 | Wind+ijs | -5° | 1.20 | 1.20 | 0.00 | 0.38 | 1.07 | 0.0 | |
| ULS 3_0,9 | Wind+ijs 0,9 | -5° | 0.90 | 1.20 | 0.00 | 0.38 | 1.07 | 0.0 | |
| ULS 4 | Koude+wind | -20° | 1.20 | 1.20 | 0.00 | 0.25 | 0.00 | 0.0 | |
| ULS 4_0,9 | Koude+wind 0,9 | -20° | 0.90 | 1.20 | 0.00 | 0.25 | 0.00 | 0.0 | |
| ULS 5a | Torsiebelastingen | 10° | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.0 | |
| ULS 5b | Longitudinale belastingen | 10° | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 1.0 | |
| ULS 6 | Bouw en onderhoud | 5° | 1.20 | 1.20 | 1.50 | 0.25 | 0.00 | 0.0 | |
| ULS 6_0,9 | Bouw en onderhoud | 5° | 1.20 | 1.20 | 0.00 | 0.25 | 0.00 | 0.0 | |
| ULS 7 | Permanent | 10° | 1.35 | 1.35 | 0.00 | 0.00 | 0.00 | 0.0 | |
| ULS 8 | Special | 10° | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 1.0 | |
| SPLS (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) | | | γ_G | | γ_Q | | | | |
| | | | G_k | G_k | Q_{pk} | Q_{wk} | Q_{ik} | A_k | |
| SPLS 1a | Wind | 10° | 1.20 | 1.20 | 0.0 | 0.78 | 0.00 | 0.0 | |
| SPLS 1a_0,9 | Wind 0,9 | 10° | 0.90 | 1.20 | 0.0 | 0.78 | 0.00 | 0.0 | |
| SPLS 1a_0,9_0,9 | Wind 0,9 | 10° | 0.90 | 0.90 | 0.0 | 0.78 | 0.00 | 0.0 | |
| SPLS 3 | Wind+ijs | -5° | 1.20 | 1.20 | 0.0 | 0.36 | 0.34 | 0.0 | |
| SPLS 3_0,9 | Wind+ijs 0,9 | -5° | 0.90 | 1.20 | 0.0 | 0.36 | 0.34 | 0.0 | |
| SPLS 4 | Koude+wind | -20° | 1.20 | 1.20 | 0.0 | 0.24 | 0.00 | 0.0 | |
| SPLS 4_0,9 | Koude+wind 0,9 | -20° | 0.90 | 1.20 | 0.0 | 0.24 | 0.00 | 0.0 | |
| SPLS 6 | Bouw en onderhoud | 5° | 1.20 | 1.20 | 1.2 | 0.24 | 0.0 | 0.0 | |
| SPLS 6_0,9 | Bouw en onderhoud | 5° | 1.20 | 1.20 | 0.0 | 0.24 | 0.0 | 0.0 | |
| SLS (controle van de vervormingen, vermoeiing, EDS) | | | G_k | | Q_{pk} | Q_{wk} | Q_{ik} | A_k | |
| SLS 1a | Wind | 10° | 1.00 | 1.00 | 0.0 | 0.87 | 0.0 | 0.0 | |
| SLS 3 | Wind+ijs | -5° | 1.00 | 1.00 | 0.0 | 0.26 | 0.71 | 0.0 | |
| SLS 4 | Wind | -20° | 1.00 | 1.00 | 0.0 | 0.17 | 0.0 | 0.0 | |
| SLS 6 | Bouw en onderhoud | 5° | 1.00 | 1.00 | 0.0 | 0.17 | 0.0 | 0.0 | |
| SLS 7 | PB (EDS, geen wind) | 10° | 1.00 | 1.00 | 0.0 | 0.00 | 0.0 | 0.0 | |

Aantal windrichtingen 6
 Aantal belastingcombinaties ULS 68
 Aantal belastingcombinaties SPLS 222
 Aantal belastingcombinaties SLS 15
 Aantal knooplasten 5185

Project: RLL-TLB380
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Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

Maximale waarden voor back en ahead span

| Geleider | Fx_ba [kN] | Fx_ah [kN] | Fy_ba [kN] | Fy_ah [kN] | Fz_ba [kN] | Fz_ah [kN] |
|--------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1 | -50.6 | 50.1 | 22.9 | 22.5 | 8.2 | 8.2 |
| 380ct1f1 | -225.4 | 223.8 | 103.0 | 100.7 | 35.6 | 35.6 |
| 380ct1f2 | -222.7 | 220.8 | 99.0 | 96.1 | 35.5 | 35.5 |
| 380ct1f3 | -219.7 | 217.7 | 94.3 | 90.6 | 35.4 | 35.4 |
| Post-isolato | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Post-isolato | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Post-isolato | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| 150ct2f1 | -112.6 | 111.8 | 52.4 | 51.2 | 22.5 | 22.5 |
| 150ct2f2 | -111.2 | 110.3 | 50.4 | 48.9 | 22.5 | 22.5 |
| 150ct2f3 | -109.8 | 109.4 | 48.0 | 46.2 | 22.5 | 22.5 |

Min. Weight span (m)

Weight spar Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|-----------------|--------|-------|-------|
| bl1 | 482.6 | 495.9 | 481.0 |
| 380ct1f1 | 481.6 | 495.6 | 481.0 |
| 380ct1f2 | 481.5 | 495.4 | 481.0 |
| 380ct1f3 | 481.4 | 495.2 | 481.0 |
| Post-isolator 1 | | | |
| Post-isolator 2 | | | |
| Post-isolator 3 | | | |
| 150ct2f1 | 481.6 | 495.6 | 481.0 |
| 150ct2f2 | 481.5 | 495.4 | 481.0 |
| 150ct2f3 | 481.4 | 495.2 | 481.0 |

Max. Weight span (m)

Weight spar Combinatie1

| Geleider | ULS 1a | ULS 3 |
|-----------------|--------|-------|
| bl1 | 547.1 | 470.4 |
| 380ct1f1 | 512.2 | 481.3 |
| 380ct1f2 | 508.6 | 480.4 |
| 380ct1f3 | 504.3 | 479.4 |
| Post-isolator 1 | | |
| Post-isolator 2 | | |
| Post-isolator 3 | | |
| 150ct2f1 | 512.2 | 481.3 |
| 150ct2f2 | 508.6 | 480.4 |
| 150ct2f3 | 504.3 | 479.4 |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

| | | Wind / Weight span verhouding |
|------------------|---------|-------------------------------|
| Max. weight span | 547.1 m | 1.368 - |
| Min. weight span | 143.4 m | 0.358 - |

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Maximale waarden back+ahead span Maximale waarden trekkracht geleider

| Geleider | Fx | Fy | Fz | Ft_ba | Ft_ah |
|--------------|-------|-------|------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] |
| bl1 | 36.7 | 43.6 | 8.2 | -55.3 | 54.8 |
| 380ct1f1 | 195.1 | 189.1 | 35.6 | -244.9 | 242.9 |
| 380ct1f2 | 191.4 | 182.1 | 35.5 | -241.5 | 239.3 |
| 380ct1f3 | 187.5 | 177.8 | 35.4 | -237.9 | 235.4 |
| Post-isolato | 3.5 | 3.5 | 6.8 | 0.0 | |
| Post-isolato | 2.7 | 2.7 | 4.7 | 0.0 | |
| Post-isolato | 4.1 | 4.1 | 6.8 | 0.0 | |
| 150ct2f1 | 102.8 | 96.1 | 22.5 | -122.4 | 121.5 |
| 150ct2f2 | 102.7 | 92.4 | 22.5 | -120.8 | 119.7 |
| 150ct2f3 | 102.6 | 89.4 | 22.5 | -119.0 | 117.7 |

EDS-belastingen geleiders

| Geleider | Fx | Fy | Fz | Ft_ba | Ft_ah |
|--------------|-------|------|------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] |
| bl1 | 16.2 | 5.9 | 2.4 | -17.2 | 17.2 |
| 380ct1f1 | 123.4 | 44.9 | 20.5 | -131.3 | 131.3 |
| 380ct1f2 | 123.4 | 44.9 | 20.5 | -131.3 | 131.3 |
| 380ct1f3 | 123.4 | 44.9 | 20.5 | -131.3 | 131.3 |
| Post-isolato | 0.0 | 0.0 | 5.0 | 0.0 | |
| Post-isolato | 0.0 | 0.0 | 3.5 | 0.0 | |
| Post-isolato | 0.0 | 0.0 | 5.0 | 0.0 | |
| 150ct2f1 | 61.7 | 22.5 | 11.8 | -65.7 | 65.7 |
| 150ct2f2 | 61.7 | 22.5 | 11.8 | -65.7 | 65.7 |
| 150ct2f3 | 61.7 | 22.5 | 11.8 | -65.7 | 65.7 |

Controle uplift SLS-wind

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
| | [kN] | [kN] |
| SLS 4 bl1 | 0.0 | 0.0 |
| 380ct1f1 | 0.0 | 0.0 |
| 380ct1f2 | 0.0 | 0.0 |
| 380ct1f3 | 0.0 | 0.0 |
| Post-isolato | 0.0 | |
| Post-isolato | 0.0 | |
| Post-isolato | 0.0 | |
| 150ct2f1 | 0.0 | 0.0 |
| 150ct2f2 | 0.0 | 0.0 |
| 150ct2f3 | 0.0 | 0.0 |

Project: RLL-TLB380
 Masttype: HC+0_c - bouwfase
 Mast: 1187

ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders

| Combinatie | Combination | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90 | | -20 | 864 | 266 | 31193 | -733 | 222 |
| ULS 1a_0.9_0 | | 18 | 487 | 175 | 17205 | 713 | 52 |
| ULS 1a_0.9_0.9_90 | | -23 | 811 | 111 | 30825 | -847 | 257 |
| ULS 3_0 | | 8 | 719 | 359 | 24304 | 303 | -10 |
| SLS 7 | | 0 | 416 | 212 | 14057 | 0 | 0 |

ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast

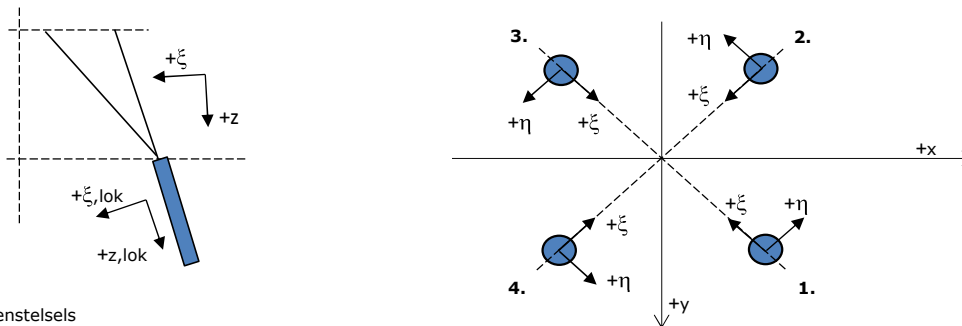
| Combinatie | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90 | -20 | 1159 | 1492 | 39362 | -733 | 222 |
| ULS 1a_0.9_0.9_90 | -23 | 1107 | 1031 | 38995 | -847 | 257 |
| SLS 7 | 0 | 416 | 1233 | 14057 | 0 | 0 |

Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde

| Combinatie | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|--------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0.9_90 | -20 | 1159 | 1077 | 40481 | -733 | 222 |
| SPLS 3_0 Ba All Cts | 909 | 286 | 1398 | 9579 | 34281 | -8920 |
| SPLS 3_70 Ah All Cts | -864 | 454 | 1401 | 15204 | -33964 | 10182 |
| SPLS 3_0.9_70 Ah All Cts | -864 | 454 | 1026 | 15888 | -33964 | 10182 |

Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.

Oplegreacties op fundering per randstijl



Assenstelsels

Maximale drukbelasting

| Stijl | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_{η} [kN] | R_{ξ} [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|-----------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1 | SPLS 3_110 Ba All Cts | 206 | 697 | 2412 | -347 | -638 | 10 | 2497 |
| 2 | SPLS 1a_0 Ba All Cts | 389 | -152 | 1434 | -167 | -383 | 3 | 1485 |
| 3 | ULS 8 Ba | -403 | -77 | 1327 | 230 | -339 | 17 | 1374 |
| 4 | SPLS 3_70 Ah All Cts | -208 | 705 | 2440 | 351 | -645 | 10 | 2527 |

Maximale trekbelasting

| Stijl | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_{η} [kN] | R_{ξ} [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|---------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1 | ULS 8 Ba | 139 | -355 | -695 | 349 | 152 | -34 | -719 |
| 2 | SPLS 3_0.9_70 Ah All Cts | -520 | 145 | -1863 | 265 | 470 | -30 | -1929 |
| 3 | SPLS 3_0.9_110 Ba All Cts | 508 | 141 | -1813 | -259 | 459 | -28 | -1877 |
| 4 | SPLS 1a_0.9_0 Ba All Cts | -55 | -341 | -817 | -280 | 202 | -18 | -846 |

Maximale torsiebelasting (positief)

| Stijl | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_{η} [kN] | R_{ξ} [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1 | SPLS 3_0.9_70 Ah All Cts | 195 | -351 | -512 | 386 | 110 | -27 | -530 |
| 2 | SPLS 3_0.9_70 Ah All Cts | -520 | 145 | -1863 | 265 | 470 | -30 | -1929 |
| 3 | SPLS 3_70 Ah All Cts | -371 | -45 | 1148 | 230 | -294 | 15 | 1188 |
| 4 | SPLS 3_70 Ah All Cts | -208 | 705 | 2440 | 351 | -645 | 10 | 2527 |

Maximale torsiebelasting (negatief)

| Index | Combinatie | R_x [kN] | R_y [kN] | R_z [kN] | R_{η} [kN] | R_{ξ} [kN] | $R_{\xi,lok}$ [kN] | $R_{z,lok}$ [kN] |
|-------|---------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1 | SPLS 3_110 Ba All Cts | 206 | 697 | 2412 | -347 | -638 | 10 | 2497 |
| 2 | ULS 8 Ah | 403 | -77 | 1327 | -230 | -339 | 17 | 1374 |
| 3 | SPLS 3_0.9_110 Ba All Cts | 508 | 141 | -1813 | -259 | 459 | -28 | -1877 |
| 4 | SPLS 3_0.9_110 Ba All Cts | -192 | -344 | -509 | -379 | 108 | -29 | -527 |

Project: RLL-TLB380
 Masttype: HC+0_c - bouwfase
 Mast: 1187

Combinatie Ftrek+Fhor

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | ULS 8 Ba | 139 | -355 | -695 | 349 | 152 | -34 | -719 |
| 2 | SPLS 3_0.9_70 Ah All Cts | -520 | 145 | -1863 | 265 | 470 | -30 | -1929 |
| 3 | SPLS 3_0.9_110 Ba All Cts | 508 | 141 | -1813 | -259 | 459 | -28 | -1877 |
| 4 | SPLS 3_0.9_0 Ba All Cts | -105 | -367 | -773 | -334 | 185 | -22 | -801 |

Permanente belasting

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SLS 7 | 189 | 168 | 906 | 15 | -253 | -10 | 938 |
| 2 | SLS 7 | -60 | 40 | -289 | 15 | 71 | -7 | -299 |
| 3 | SLS 7 | 60 | 40 | -289 | -15 | 71 | -7 | -299 |
| 4 | SLS 7 | -189 | 168 | 906 | -15 | -253 | -10 | 938 |

Omhullenden ongeacht stijl

| Belasting | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------------------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk | SPLS 3_70 Ah All Cts | -208 | 705 | 2440 | 351 | -645 | 10 | 2527 |
| Max. trek | SPLS 3_0.9_70 Ah All Cts | -520 | 145 | -1863 | 265 | 470 | -30 | -1929 |
| Max. pos. torsie | SPLS 3_0.9_70 Ah All Cts | 195 | -351 | -512 | 386 | 110 | -27 | -530 |
| Max. neg. torsie | SPLS 3_0.9_110 Ba All Cts | -192 | -344 | -509 | -379 | 108 | -29 | -527 |
| Comb. trek+torsie | SPLS 3_0.9_70 Ah All Cts | -520 | 145 | -1863 | 265 | 470 | -30 | -1929 |

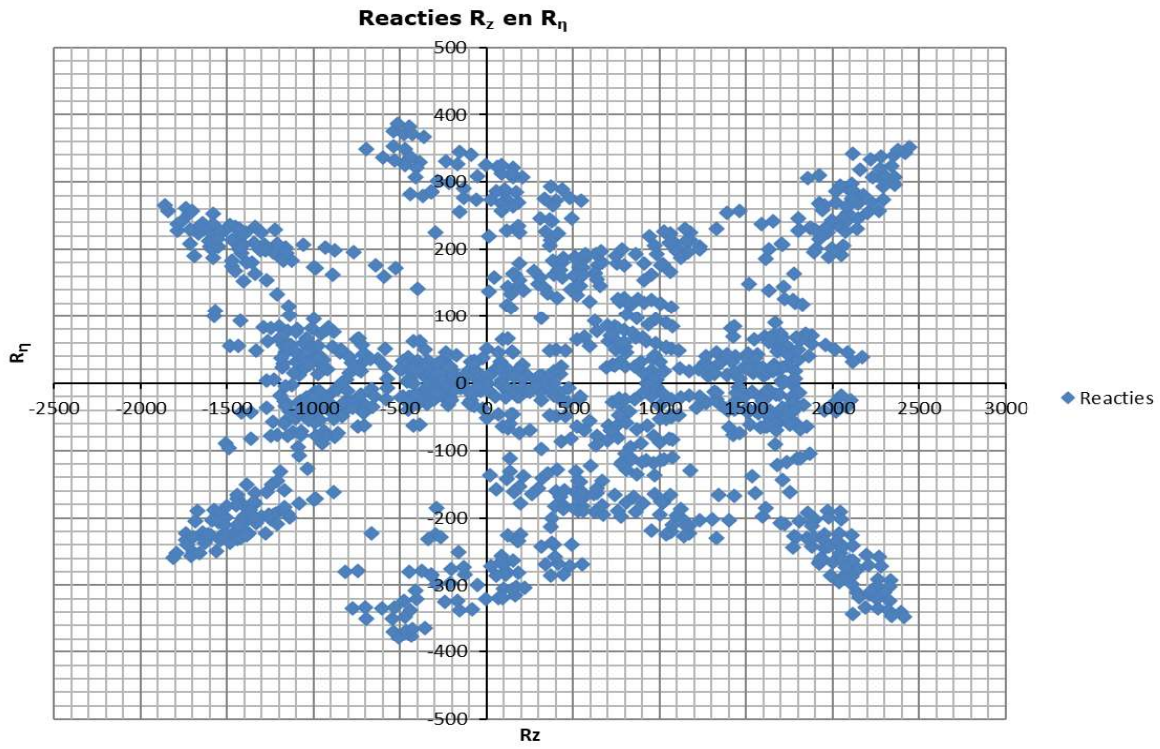
Maximale trekbelasting SLS

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SPLS 3_0.9_110 Ah All Cts | 164 | -335 | -541 | 353 | 121 | -24 | -560 |
| 2 | SPLS 3_0.9_70 Ah All Cts | -520 | 145 | -1863 | 265 | 470 | -30 | -1929 |
| 3 | SPLS 3_0.9_110 Ba All Cts | 508 | 141 | -1813 | -259 | 459 | -28 | -1877 |
| 4 | SPLS 1a_0.9_0 Ba All Cts | -55 | -341 | -817 | -280 | 202 | -18 | -846 |

Maximale drukbelasting SLS

| Stijl | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _η [kN] | R _ξ [kN] | R _{ξ,lok} [kN] | R _{z,lok} [kN] |
|-------|--------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1 | SPLS 3_110 Ba All Cts | 206 | 697 | 2412 | -347 | -638 | 10 | 2497 |
| 2 | SPLS 1a_0.9_0 Ba All Cts | 369 | -135 | 1339 | -165 | -356 | 4 | 1387 |
| 3 | SPLS 3_110 Ah All Cts | -366 | -64 | 1175 | 213 | -304 | 11 | 1216 |
| 4 | SPLS 3_70 Ah All Cts | -208 | 705 | 2440 | 351 | -645 | 10 | 2527 |

Project: RLL-TLB380
Masttype: HC+0_c - bouwfase
Mast: 1187



Belastinggeval - afspannen

Date: 2021-05-31
 Author: TBR
 Version: 1.1

RLL-TLB
 HB+0/c (afspannen)

Invoergegevens

Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting

| Circuits | Aanduiding | Nummer | Hoogteverschil | | Richtingsverandering | |
|----------------|------------|----------|----------------|----------|----------------------|----------|
| | | | Dh_back | Dh_ahead | Dy_back | Dy_ahead |
| Circuit 1 | 10 | 380ct1f1 | 0,0 | -9,0 m | 0,0 | 0,0 m |
| Circuit 1 | 11 | 380ct1f2 | 0,0 | -9,0 m | 0,0 | 0,0 m |
| Circuit 1 | 12 | 380ct1f3 | 0,0 | -9,0 m | 0,0 | 0,0 m |
| Circuit 2 | 40 | 380ct2f1 | -48,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 41 | 380ct2f2 | -38,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 2 | 42 | 380ct2f3 | -28,5 | 0,0 m | 0,0 | 0,0 m |
| Circuit 3 | 20 | 150ct3f1 | 0,0 | -9,0 m | 0,0 | 0,0 m |
| Circuit 3 | 21 | 150ct3f2 | 0,0 | -9,0 m | 0,0 | 0,0 m |
| Circuit 3 | 22 | 150ct3f3 | 0,0 | -9,0 m | 0,0 | 0,0 m |
| Circuit 4 | 30 | 150ct4f1 | -48,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 31 | 150ct4f2 | -38,0 | 0,0 m | 0,0 | 0,0 m |
| Circuit 4 | 32 | 150ct4f3 | -28,5 | 0,0 m | 0,0 | 0,0 m |
| Bliksemdraad 1 | 1 | bl1 | 0,0 | -9,0 m | 0,0 | 0,0 m |
| Bliksemdraad 2 | 3 | bl2 | -53,1 | 0,0 m | 0,0 | 0,0 m |

Lijn- en mastgegevens

| | | Back | Ahead |
|---------------------------------------|----------|-------|---------|
| Ruling span $\sqrt{(SL3/SL)}$ | | 72,8 | 400,0 m |
| Lijnhoek | β | 180 ° | |
| Rotatie mast t.o.v. bissectrice | θ | -30 ° | |
| Vaklengte | | 73 | 400 m |
| Hoogte onderkant mast t.o.v. maaiveld | | 0,5 m | |
| Beschouwde windrichtingen | a1 | 0 ° | |
| Windrichtingen volgens: | a2 | 45 ° | |
| <i>Geleiderbelastingen</i> | a3 | 90 ° | |
| | a4 | 135 ° | |
| | a5 | 120 ° | |
| | a6 | 120 ° | |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

In onderstaande tabel zijn de optredende belastingen weergegeven, voor deze situatie geldt:

- belasting op geleider1, 10 t/m 12 en 20 t/m 22 zijn permanent aanwezig
- van de belasting op de overige geleiders is er telkens één aanwezig per belastingcombinatie

Uitvoer geleiderbelastingen

| Belastingcombi | nummer | Fxtotaal | Fytotaal | Fztotaal | Ftrekahead | Ftrekback |
|------------------|--------|---------------|--------------|--------------|------------|-----------|
| ULS 6b_90 | 1 | 17,9 | 11,2 | 2,9 | 21,1 | 0,0 |
| | 10 | 134,8 | 81,9 | 24,7 | 157,7 | 0,0 |
| | 11 | 134,6 | 81,4 | 24,7 | 157,3 | 0,0 |
| | 12 | 134,4 | 80,8 | 24,6 | 156,8 | 0,0 |
| | 20 | 67,4 | 41,0 | 12,9 | 78,8 | 0,0 |
| | 21 | 67,3 | 40,8 | 12,9 | 78,6 | 0,0 |
| | 22 | 67,1 | 40,5 | 12,9 | 78,4 | 0,0 |
| | 40 | -129,4 | -73,8 | 105,0 | 0,0 | -149,0 |
| | 41 | -129,3 | -73,8 | 84,5 | 0,0 | -148,9 |
| | 42 | -129,3 | -73,8 | 65,1 | 0,0 | -148,8 |
| | 30 | -64,7 | -36,8 | 53,1 | 0,0 | -74,5 |
| | 31 | -64,7 | -36,8 | 42,9 | 0,0 | -74,5 |
| | 32 | -64,7 | -36,8 | 33,1 | 0,0 | -74,4 |
| | 3 | -16,9 | -9,6 | 14,8 | 0,0 | -19,5 |

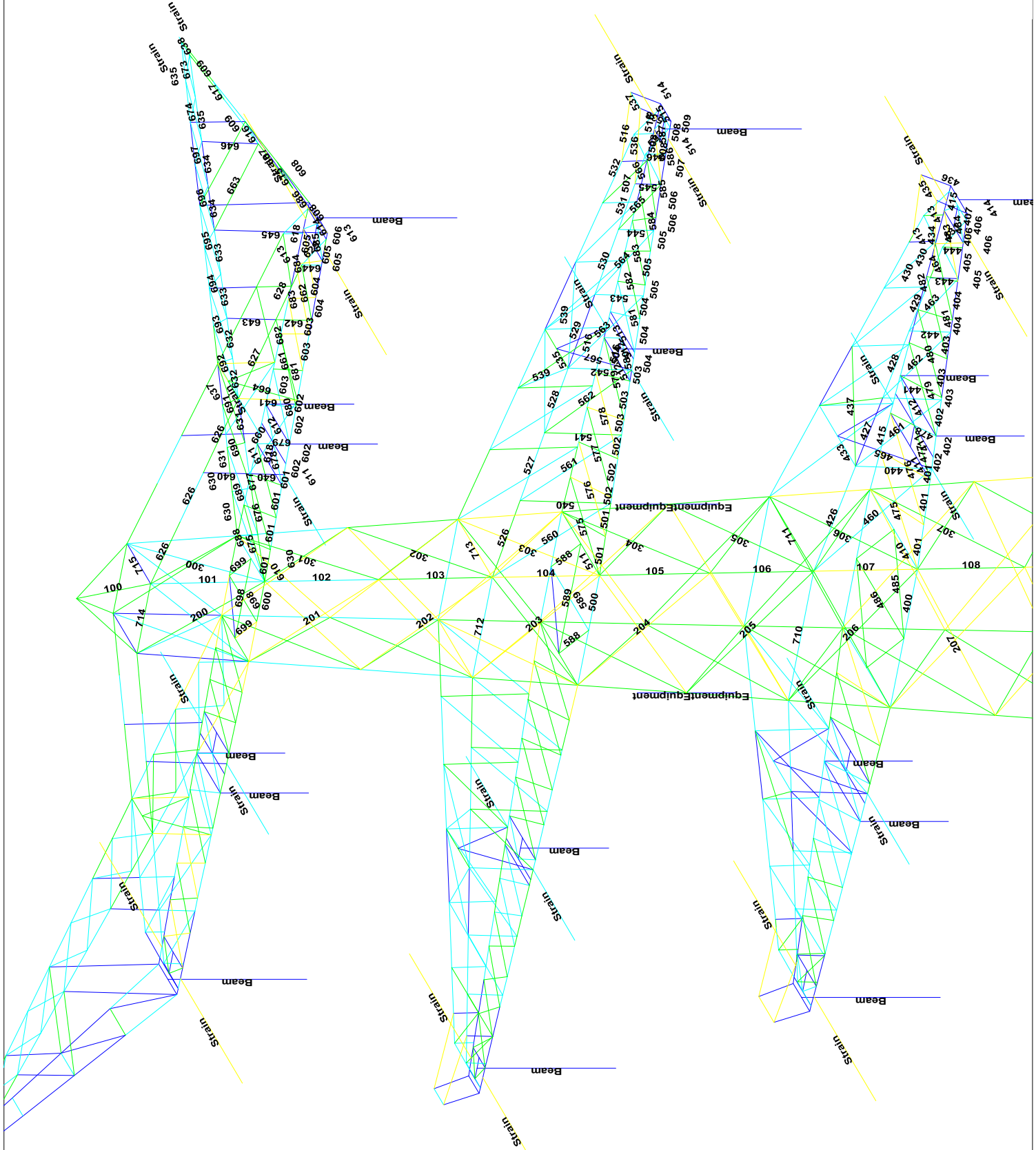


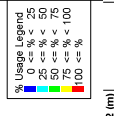
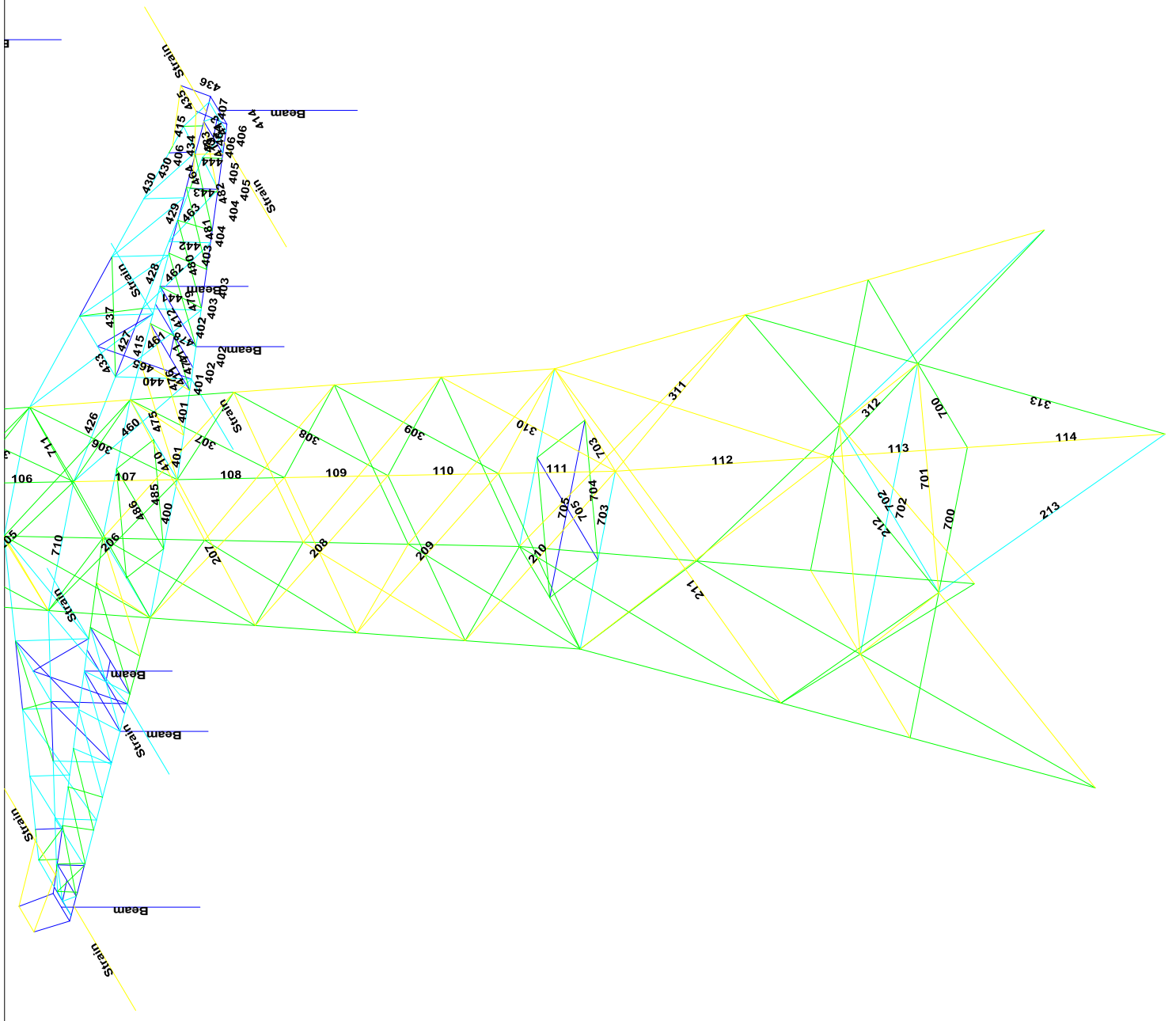
APPENDIX B

Resultaten PLS-TOWER

Deze Appendix bevat de resultaten uit PLS-TOWER voor onderstaande masttype:

- Masttype HC+0/c





Assessment of angle groups

Date 16-7-2021
Author MRE
Version 1.0

RLI-TBG
HC-O/c

Table with 21 columns: Group Label, Description, Type, Profile, Steel Qualities, #shp, c1, c2, p1, RLX, RLZ, RLY, RLL, RLV, RLW, SLenderness, Compression, Lead Case, Buckling, Shear, (Comp)rating, (Comp), U.C., (Comp)edance, (Comp), Tension, Load Case, (Tension), Net Section ear, (Tension)ring, (Tension)ring, U.C., (Tension)ince, (Tension)

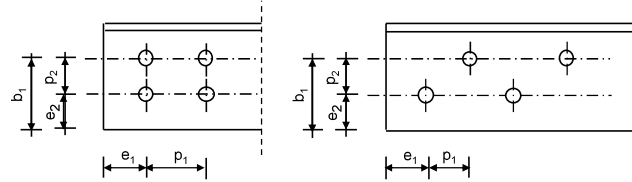
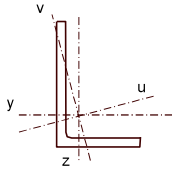
Project: ZW-Oost
Mast: H_C

Angle check

NEN-EN1993-1-1 and EN1993-3-1

Datum: 2021-06-02
Auteur: TBR
Versie: 3.0

| | | |
|--------------------|-----------------------|--|
| Member name | Group 108-109 | Conclusion |
| Section | XEA 200x200x24 | U.C. (compression) 0.88 < 1,0 OK |
| | | U.C. (tension) 0.59 < 1,0 OK |



Steel grade **S355**

Member loads

Compressive force $N_{Ed} =$ **4581 kN**
Tensile force **-4064 kN**

Crossing diagonal loads

Applicable: **No**
Min. tensile force diagonal 2 **1 kN**
Max. comp. force diagonal 1 **1 kN**
Position crossing diagonal y-axis **1.00 m**

Construction loads

Vertical construction load **1.0 kN**
Member angle to horizontal **0 °**
Bending around axis **y-axis**

Geometry

System length y-axis $L_{y,buc} =$ **1.66 m**
System length z-axis $L_{z,buc} =$ **1.66 m**
System length v-axis $L_{v,buc} =$ **1.66 m**
System length x-axis $L_{tk,buc} =$ **1.66 m**
Member type **Leg**
Type bracing **Non staggered**

End conditions

Begin **Continuous**
End **Continuous**
Restraint code TOWER **C4**

Bolted connection

Bolt type **M24**
Bolt class **8.8**
Number of bolts per leg **6** (24 total)
Shearplane through **Thread**
Boltpattern **Zigzag**
Boltpattern (leg-member only) **Staggered**

End distance $e_1 =$ **55 mm** **Ok**
Separation distance // $p_1 =$ **70 mm** **Ok**
Separation distance | $p_2 =$ **100 mm** **Ok**
End distance $e_2 =$ **50 mm** **Ok**
Double strap or single strap **Double**
Tie plate $b_p =$ **230 mm** **OK**
 $t_p =$ **15 mm** **OK**
 $e_2 =$ **40 mm** **OK**

A **18118 mm²**
G **144.9 kg/m**
Partial safety factor $\gamma_{f;Q} =$ **1.50**
Material factors $\gamma_{M0} =$ **1.00**
 $\gamma_{M1} =$ **1.00**
 $\gamma_{M2} =$ **1.25**
Shear strength bolt $F_{v;b;Rd} =$ **135.6 kN**

Slenderness $\lambda_{max} = L / i :$ **22 -**
Allowed: **120 OK**

Bending due to vertical construction load

$M_{y,Ed} = 1/4 F_{Ed} L_{pr} =$ **0.62 kNm**
U.C. = **0.00 < 1,00 OK**

Results stability

| | $\lambda_{eff,rel}$ | λ_{eff} | $\lambda_{eff,mod}$ | χ_{buc} | η | $N_{b,Rd} = \eta \chi A_f \gamma / \gamma_{M1}$ |
|-----------------------|---------------------|-----------------|---------------------|--------------|--------|---|
| $L_{y,buc} =$ 1.66 m | 0.26 | 1,00 I | 0.26 | 0.98 | 1 | 6299 0.73 |
| $L_{z,buc} =$ 1.66 m | 0.26 | 1,00 I | 0.26 | 0.98 | 1 | 6299 0.73 |
| $L_{v,buc} =$ 1.66 m | 0.28 | 0,10+0,80 I | 0.28 | 0.97 | 1 | 6237 0.73 |
| $L_{tk,buc} =$ 1.66 m | 0.55 | | | 0.81 | 1 | 5229 0.88 |

Bolted connection

| Compression | F_{Rd} (kN) | U.C. | Tension | F_{Rd} (kN) | U.C. |
|-------------------------|--------------------|-----------------------|-----------------------|--------------------|-----------------------|
| Cross section angle | $F_{u;Rd} =$ 6432 | 0.71 | Net section angle | $F_{u;Rd} =$ 6987 | 0.58 |
| Cross section tie plate | $F_{u;Rd} =$ 8094 | 0.57 | Net section tie plate | $F_{u;Rd} =$ 6943 | 0.59 |
| Shear strength | $F_{v;Rd} =$ 8675 | 0.53 | Block shear | $F_{u;Rd} =$ 10634 | 0.38 |
| Bearing strength | $F_{b;Rd} =$ 11695 | 0.39 | Shear strength | $F_{v;Rd} =$ 8675 | 0.47 |
| Combined effect | $F_{v;Rd} =$ 8675 | 0.53 elastisch | Bearing strength | $F_{b;Rd} =$ 11825 | 0.34 |
| | | | Combined effect | $F_{v;Rd} =$ 8675 | 0.47 elastisch |

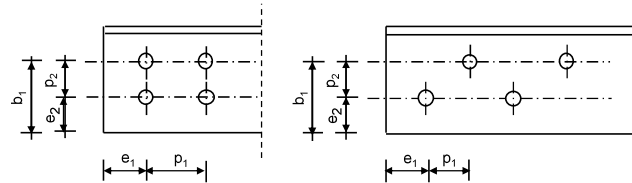
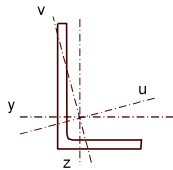
Project: ZW-Oost
Mast: H_C

Angle check

NEN-EN1993-1-1 and EN1993-3-1

Datum: 2021-06-02
Auteur: TBR
Versie: 3.0

| Member name | Group 110-111 | Conclusion |
|-------------|----------------|--|
| Section | XEA 250x250x24 | U.C. (compression) 0.91 < 1,0 OK |
| | | U.C. (tension) 0.74 < 1,0 OK |



Steel grade **S355**

Member loads

Compressive force $N_{Ed} =$ **5685 kN**
Tensile force **-5129 kN**

Crossing diagonal loads

Applicable: **No**
Min. tensile force diagonal 2 **1 kN**
Max. comp. force diagonal 1 **1 kN**
Position crossing diagonal y-axis **1.00 m**

Construction loads

Vertical construction load **1.0 kN**
Member angle to horizontal **0 °**
Bending around axis **y-axis**

Geometry

System length y-axis $L_{y,buc} =$ **1.81 m**
System length z-axis $L_{z,buc} =$ **1.81 m**
System length v-axis $L_{v,buc} =$ **1.81 m**
System length x-axis $L_{tk,buc} =$ **1.81 m**
Member type **Leg**
Type bracing **Non staggered**

End conditions

Begin **Continuous**
End **Continuous**
Restraint code TOWER **C4**

Bolted connection

Bolt type **M24**
Bolt class **8.8**
Number of bolts per leg **6** (24 total)
Shearplane through **Thread**
Bolt pattern **Zigzag**
Bolt pattern (leg-member only) **Staggered**

End distance $e_1 =$ **55 mm** **Ok**
Separation distance // $p_1 =$ **70 mm** **Ok**
Separation distance | $p_2 =$ **100 mm** **Ok**
End distance $e_2 =$ **50 mm** **Ok**
Double strap or single strap **Double**
Tie plate $b_p =$ **230 mm** **OK**
 $t_p =$ **15 mm** **OK**
 $e_2 =$ **40 mm** **OK**

A **23036 mm²**
G **184.3 kg/m**
Partial safety factor $\gamma_{f;Q} =$ **1.50**
Material factors $\gamma_{M0} =$ **1.00**
 $\gamma_{M1} =$ **1.00**
 $\gamma_{M2} =$ **1.25**
Shear strength bolt $F_{v;b;Rd} =$ **135.6 kN**

Slenderness $\lambda_{max} = L / i :$ **19 -**
Allowed: **120 OK**

Bending due to vertical construction load

$M_{y,Ed} = 1/4 F_{Ed} L_{pr} =$ **0.68 kNm**
U.C. = **0.00 < 1,00 OK**

Results stability

| | $\lambda_{eff,rel}$ | λ_{eff} | $\lambda_{eff,mod}$ | χ_{buc} | η | $N_{b,Rd} = \eta \chi A_f \gamma / \gamma_{M1}$ |
|-----------------------|---------------------|-----------------|---------------------|--------------|--------|---|
| $L_{y,buc} =$ 1.81 m | 0.23 | 1,00 I | 0.23 | 0.99 | 1 | 8098 0.70 |
| $L_{z,buc} =$ 1.81 m | 0.23 | 1,00 I | 0.23 | 0.99 | 1 | 8098 0.70 |
| $L_{v,buc} =$ 1.81 m | 0.25 | 0,10+0,80 I | 0.25 | 0.98 | 1 | 8045 0.71 |
| $L_{tk,buc} =$ 1.81 m | 0.64 | | | 0.76 | 1 | 6250 0.91 |

Bolted connection

| Compression | F_{Rd} (kN) | U.C. | Tension | F_{Rd} (kN) | U.C. |
|-------------------------|--------------------|-----------------------|-----------------------|--------------------|-----------------------|
| Cross section angle | $F_{u;Rd} =$ 8178 | 0.70 | Net section angle | $F_{u;Rd} =$ 6987 | 0.73 |
| Cross section tie plate | $F_{u;Rd} =$ 8094 | 0.70 | Net section tie plate | $F_{u;Rd} =$ 6943 | 0.74 |
| Shear strength | $F_{v;Rd} =$ 8675 | 0.66 | Block shear | $F_{u;Rd} =$ 10634 | 0.48 |
| Bearing strength | $F_{b;Rd} =$ 11695 | 0.49 | Shear strength | $F_{v;Rd} =$ 8675 | 0.59 |
| Combined effect | $F_{v;Rd} =$ 8675 | 0.66 elastisch | Bearing strength | $F_{b;Rd} =$ 11825 | 0.43 |
| | | | Combined effect | $F_{v;Rd} =$ 8675 | 0.59 elastisch |

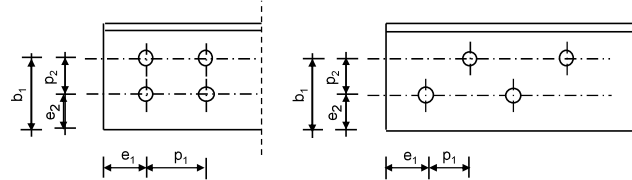
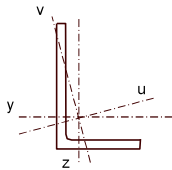
Project: ZW-Oost
Mast: H_C

Angle check

NEN-EN1993-1-1 and EN1993-3-1

Datum: 2021-06-02
Auteur: TBR
Versie: 3.0

| | | |
|--------------------|--------------------------|--|
| Member name | Group 112-113-114 | Conclusion |
| Section | XE A 250x250x24 | U.C. (compression) 0.96 < 1,0 OK |
| | | U.C. (tension) 0.76 < 1,0 OK |



Steel grade **S355**

Member loads

Compressive force $N_{Ed} =$ **5945 kN**
Tensile force **-5299 kN**

Crossing diagonal loads

Applicable: **No**
Min. tensile force diagonal 2 **1 kN**
Max. comp. force diagonal 1 **1 kN**
Position crossing diagonal y-axis **1.00 m**

Construction loads

Vertical construction load **1.0 kN**
Member angle to horizontal **0 °**
Bending around axis **y-axis**

Geometry

System length y-axis $L_{y,buc} =$ **1.96 m**
System length z-axis $L_{z,buc} =$ **1.96 m**
System length v-axis $L_{v,buc} =$ **1.96 m**
System length x-axis $L_{tk,buc} =$ **1.96 m**
Member type **Leg**
Type bracing **Non staggered**

End conditions

Begin **Continuous**
End **Continuous**
Restraint code TOWER **C4**

Bolted connection

Bolt type **M24**
Bolt class **8.8**
Number of bolts per leg **6** (24 total)
Shearplane through **Thread**
Bolt pattern **Zigzag**
Bolt pattern (leg-member only) **Staggered**

End distance $e_1 =$ **55 mm** **Ok**
Separation distance // $p_1 =$ **70 mm** **Ok**
Separation distance | $p_2 =$ **100 mm** **Ok**
End distance $e_2 =$ **50 mm** **Ok**
Double strap or single strap **Double**
Tie plate $b_p =$ **230 mm** **OK**
 $t_p =$ **15 mm** **OK**
 $e_2 =$ **40 mm** **OK**

A **23036 mm²**
G **184.3 kg/m**
Partial safety factor $\gamma_{f;Q} =$ **1.50**
Material factors $\gamma_{M0} =$ **1.00**
 $\gamma_{M1} =$ **1.00**
 $\gamma_{M2} =$ **1.25**
Shear strength bolt $F_{v;Rd} =$ **135.6 kN**

Slenderness $\lambda_{max} = L / i :$ **20 -**
Allowed: **120 OK**

Bending due to vertical construction load

$M_{y,Ed} = 1/4 F_{Ed} L_{pr} =$ **0.74 kNm**
U.C. = **0.00 < 1,00 OK**

Results stability

| | $\lambda_{eff,rel}$ | λ_{eff} | $\lambda_{eff,mod}$ | χ_{buc} | η | $N_{b,Rd} = \eta \chi A_f \gamma / \gamma_{M1}$ |
|-----------------------|---------------------|-----------------|---------------------|--------------|--------|---|
| $L_{y,buc} =$ 1.96 m | 0.25 | 1,00 I | 0.25 | 0.98 | 1 | 8043 0.74 |
| $L_{z,buc} =$ 1.96 m | 0.25 | 1,00 I | 0.25 | 0.98 | 1 | 8043 0.74 |
| $L_{v,buc} =$ 1.96 m | 0.27 | 0,10+0,80 I | 0.27 | 0.98 | 1 | 7985 0.74 |
| $L_{tk,buc} =$ 1.96 m | 0.64 | | | 0.76 | 1 | 6216 0.96 |

Bolted connection

| | F_{Rd} (kN) | U.C. | | F_{Rd} (kN) | U.C. |
|--------------------------------------|---------------|-----------------------|------------------------------------|---------------|-----------------------|
| Compression | | | Tension | | |
| Cross section angle $F_{u;Rd} =$ | 8178 | 0.73 | Net section angle $F_{u;Rd} =$ | 6987 | 0.76 |
| Cross section tie plate $F_{u;Rd} =$ | 8094 | 0.73 | Net section tie plate $F_{u;Rd} =$ | 6943 | 0.76 |
| Shear strength $F_{v;Rd} =$ | 8675 | 0.69 | Block shear $F_{u;Rd} =$ | 10634 | 0.50 |
| Bearing strength $F_{b;Rd} =$ | 11695 | 0.51 | Shear strength $F_{v;Rd} =$ | 8675 | 0.61 |
| Combined effect $F_{v;Rd} =$ | 8675 | 0.69 elastisch | Bearing strength $F_{b;Rd} =$ | 11825 | 0.45 |
| | | | Combined effect $F_{v;Rd} =$ | 8675 | 0.61 elastisch |

APPENDIX C

Knikverkorters

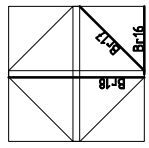
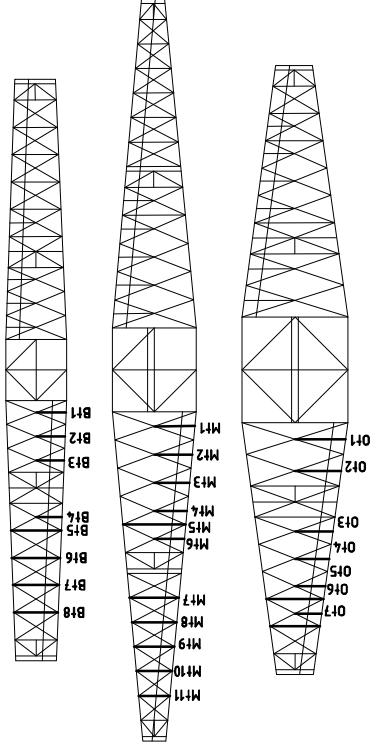
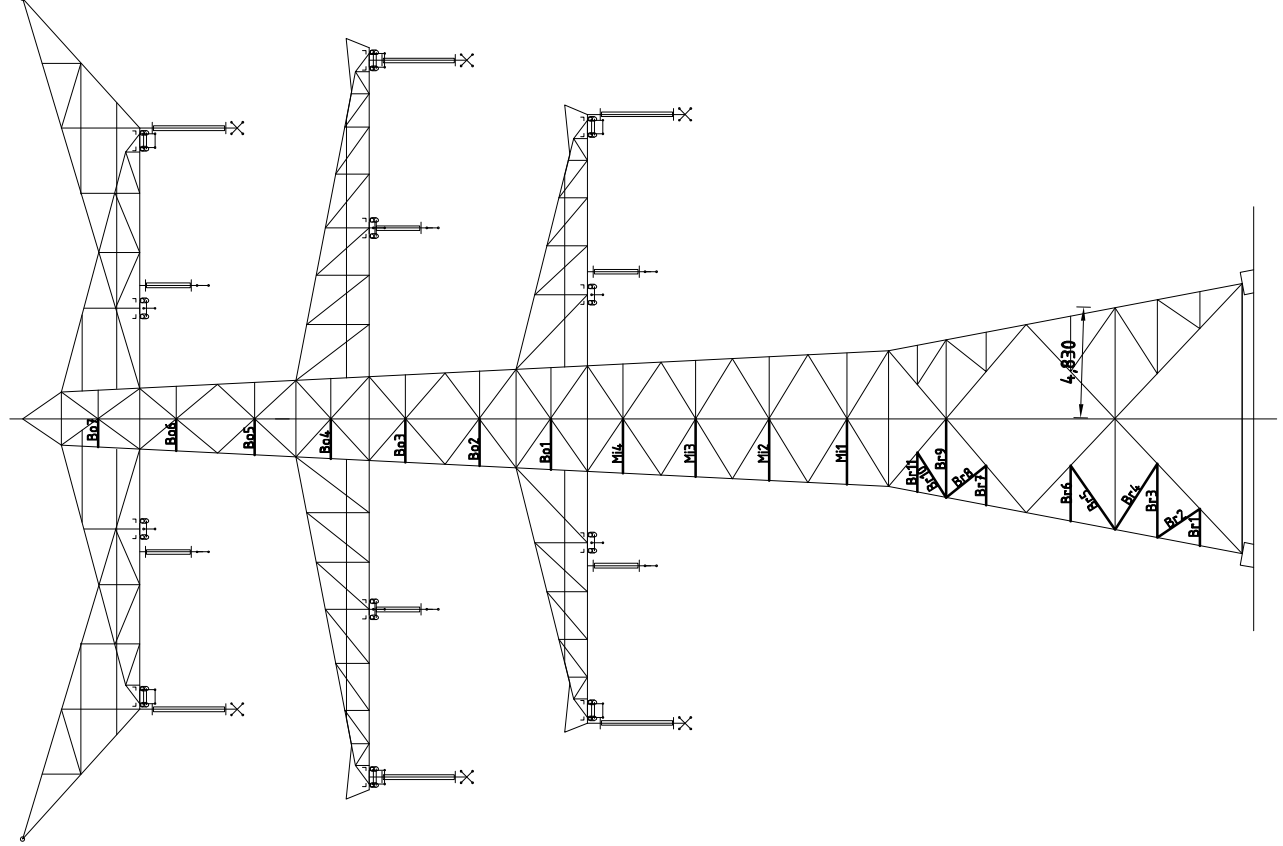
Niet in PLS-TOWER gemodelleerde elementen in de constructie worden aanvullend getoetst. Hieronder vallen de knikverkorters van de randstijl en profielen onderdeel van stabiliteitsverbanden. De staven worden getoetst op:

- voldoende trek- of druksterkte als steungevend profiel voor randstijl, 1% van de knikcapaciteit van de randstijl;
- slankheid;
- klimbelasting

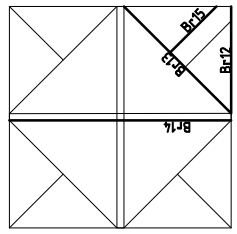
Voor de beloopbaarheid zijn staven in de traverse aanwezig. Deze zijn niet constructief (voorzien van slobgaten) en worden enkel getoetst op de klimbelasting van 1,0 kN. Zie hoofdstuk 4.2.5 en 5.7.2 van het uitgangspuntenrapport.

Profielen uit horizontaalverbanden van het onderstuk zijn in PLS-TOWER aanwezig maar worden in deze Appendix aanvullend getoetst op buiging. Profielafmeting en boutverbinding uit PLS-TOWER is leidend.

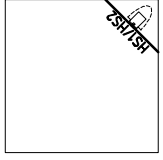
Overzicht knikverkorters – HC+0/c



Tussenschot +15,9m



Tussenschot +6,04m



Standaard frame



Redundant members

RLI-TLB
HC+0/c

Date: 2021-07-09
Author: MRE
Version: 1.9

| Posnr. | Section | Schematization | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Slenderness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Max. usage | Notes |
|--------|--------------------|----------------------------|---------|---------------|--------------|------------|-----------|-------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|------------|----------|
| Br1 | Broekstuk | Enkele staaf | L70x6 | S355J0 | M20 | 8.8 | 1.62 | 0 | 118 | 62.0 | 0.61 | 85.4 | 94.1 | 71.3 | 112.9 | 1.99 | 0.87 | Bearing |
| Br2 | Broekstuk | Enkele staaf | L80x6 | S355J0 | M20 | 8.8 | 2.24 | 55 | 142 | 62.0 | 0.00 | 77.3 | 94.1 | 71.3 | 136.4 | 2.68 | 0.87 | Bearing |
| Br3 | Broekstuk | Enkele staaf | L90x8 | S355J0 | M20 | 8.8 | 3.23 | 0 | 183 | 62.0 | 1.21 | 80.6 | 94.1 | 95.0 | 213.2 | 4.34 | 0.77 | Buckling |
| Br4 | Broekstuk | Enkele staaf | L90x8 | S355J0 | M20 | 8.8 | 3.41 | 33 | 194 | 62.0 | 0.00 | 74.2 | 94.1 | 95.0 | 213.2 | 4.34 | 0.84 | Buckling |
| Br5 | Broekstuk | Enkele staaf | L90x8 | S355J0 | M20 | 8.8 | 3.40 | 33 | 193 | 62.0 | 0.00 | 74.5 | 94.1 | 95.0 | 213.2 | 4.34 | 0.83 | Buckling |
| Br6 | Broekstuk | Enkele staaf | L80x6 | S355J0 | M20 | 8.8 | 2.50 | 0 | 159 | 62.0 | 0.94 | 66.6 | 94.1 | 71.3 | 136.4 | 2.68 | 0.93 | Buckling |
| Br7 | Broekstuk | Enkele staaf | L70x6 | S355J0 | M20 | 8.8 | 1.72 | 0 | 125 | 62.0 | 0.64 | 79.3 | 94.1 | 71.3 | 112.9 | 1.99 | 0.87 | Bearing |
| Br8 | Broekstuk | Enkele staaf | L80x6 | S355J0 | M20 | 8.8 | 2.23 | 51 | 141 | 62.0 | 0.00 | 78.0 | 94.1 | 71.3 | 136.4 | 2.68 | 0.87 | Bearing |
| Br9 | Broekstuk | Enkele staaf | L90x8 | S355J0 | M20 | 8.8 | 3.43 | 0 | 195 | 62.0 | 1.29 | 73.5 | 94.1 | 95.0 | 213.2 | 4.34 | 0.84 | Buckling |
| Br10 | Broekstuk | Enkele staaf | L80x6 | S355J0 | M20 | 8.8 | 2.32 | 33 | 148 | 62.0 | 0.00 | 71.6 | 94.1 | 71.3 | 136.4 | 2.68 | 0.87 | Bearing |
| Br11 | Broekstuk | Enkele staaf | L70x6 | S355J0 | M20 | 8.8 | 1.17 | 0 | 86 | 62.0 | 0.44 | 119.0 | 94.1 | 71.3 | 112.9 | 1.99 | 0.87 | Bearing |
| Br12 | Tussenschot +6,04m | Enkele staaf | L100x8 | S355J0 | M16 | 8.8 | 4.83 | 0 | 245 | 0.0 | 1.81 | 57.4 | 60.3 | 69.7 | 257.2 | 5.49 | 0.34 | Bending |
| Br13 | Tussenschot +6,04m | Kruisende staaf halverwege | L100x8 | S355J0 | M16 | 8.8 | 6.83 | 0 | 222 | 0.0 | 2.56 | 56.8 | 60.3 | 69.7 | 257.2 | 7.19 | 0.25 | Bending |
| Br14 | Tussenschot +6,04m | Enkele staaf | L70x6 | S355J0 | M16 | 8.8 | 3.41 | 0 | 245 | 0.0 | 1.81 | 57.4 | 60.3 | 69.7 | 257.2 | 7.19 | 0.25 | Bending |
| Br15 | Tussenschot +6,04m | Enkele staaf | L130x12 | S355J0 | M16 | 8.8 | 2.94 | 0 | 245 | 0.0 | 1.28 | 29.4 | 60.3 | 52.3 | 122.3 | 1.99 | 0.67 | Bending |
| Br16 | Tussenschot +15,9m | Enkele staaf | L90x8 | S355J0 | M16 | 8.8 | 4.17 | 0 | 74 | 0.0 | 1.10 | 380.6 | 60.3 | 104.5 | 620.9 | 17.91 | 0.06 | Bending |
| Br17 | Tussenschot +15,9m | Enkele staaf | L90x8 | S355J0 | M16 | 8.8 | 5.91 | 0 | 237 | 0.0 | 1.56 | 54.4 | 60.3 | 69.7 | 225.8 | 4.34 | 0.37 | Bending |
| Br18 | Tussenschot +15,9m | Kruisende staaf halverwege | L80x8 | S355J0 | M20 | 8.8 | 2.87 | 0 | 168 | 0.0 | 1.11 | 91.6 | 60.3 | 69.7 | 225.8 | 5.70 | 0.19 | Bending |
| M1 | Middenstuk1 | Enkele staaf | L80x8 | S355J0 | M20 | 8.8 | 2.70 | 0 | 184 | 62.3 | 1.07 | 71.0 | 94.1 | 95.0 | 181.9 | 3.33 | 0.88 | Buckling |
| M2 | Middenstuk1 | Enkele staaf | L80x6 | S355J0 | M20 | 8.8 | 2.53 | 0 | 161 | 52.2 | 0.95 | 65.3 | 94.1 | 95.0 | 181.9 | 3.33 | 0.80 | Buckling |
| M3 | Middenstuk2 | Enkele staaf | L80x6 | S355J0 | M20 | 8.8 | 2.38 | 0 | 151 | 52.2 | 0.89 | 71.4 | 94.1 | 71.3 | 136.4 | 2.68 | 0.80 | Buckling |
| M4 | Middenstuk2 | Enkele staaf | L70x6 | S355J0 | M16 | 8.8 | 2.22 | 0 | 162 | 38.0 | 0.78 | 56.3 | 60.3 | 52.3 | 122.3 | 1.99 | 0.73 | Bearing |
| B01 | Bovenstuk1 | Enkele staaf | L70x6 | S355J0 | M16 | 8.8 | 2.07 | 0 | 151 | 38.0 | 0.71 | 47.5 | 60.3 | 52.3 | 98.8 | 1.4 | 0.80 | Buckling |
| B02 | Bovenstuk1 | Enkele staaf | L60x6 | S355J0 | M16 | 8.8 | 1.90 | 0 | 163 | 38.0 | 0.71 | 47.5 | 60.3 | 52.3 | 98.8 | 1.4 | 0.80 | Buckling |
| B03 | Bovenstuk1 | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.74 | 0 | 179 | 13.6 | 0.65 | 28.8 | 60.3 | 41.3 | 43.1 | 0.8 | 0.83 | Bending |
| B04 | Bovenstuk2 | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.58 | 0 | 162 | 13.6 | 0.59 | 33.3 | 60.3 | 41.3 | 43.1 | 0.8 | 0.75 | Bending |
| B05 | Bovenstuk2 | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.41 | 0 | 144 | 13.6 | 0.53 | 39.0 | 60.3 | 41.3 | 43.1 | 0.8 | 0.67 | Bending |
| B06 | Bovenstuk2 | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.24 | 0 | 127 | 7.4 | 0.46 | 46.0 | 60.3 | 41.3 | 43.1 | 0.8 | 0.59 | Bending |
| B07 | Bovenstuk2 | Enkele staaf | L60x6 | S355J0 | M16 | 8.8 | 2.20 | 0 | 188 | 0.0 | 0.83 | 38.5 | 60.3 | 52.3 | 98.8 | 1.4 | 0.61 | Bending |
| O1 | Ondertaverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.65 | 0 | 207 | 0.0 | 0.75 | 23.2 | 60.3 | 41.3 | 43.1 | 0.8 | 0.96 | Bending |
| O2 | Ondertaverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 2.01 | 0 | 170 | 0.0 | 0.62 | 21.2 | 60.3 | 41.3 | 43.1 | 0.8 | 0.79 | Bending |
| O3 | Ondertaverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.65 | 0 | 153 | 0.0 | 0.56 | 36.0 | 60.3 | 41.3 | 43.1 | 0.8 | 0.71 | Bending |
| O4 | Ondertaverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.49 | 0 | 137 | 0.0 | 0.50 | 41.9 | 60.3 | 41.3 | 43.1 | 0.8 | 0.64 | Bending |
| O5 | Ondertaverse | Enkele staaf | L60x6 | S355J0 | M16 | 8.8 | 1.33 | 0 | 214 | 0.0 | 0.94 | 31.7 | 60.3 | 52.3 | 98.8 | 1.4 | 0.69 | Bending |
| O6 | Ondertaverse | Kruisende staaf halverwege | L50x5 | S355J0 | M16 | 8.8 | 2.50 | 0 | 119 | 0.0 | 0.44 | 49.7 | 60.3 | 41.3 | 43.1 | 0.8 | 0.55 | Bending |
| O7 | Ondertaverse | Kruisende staaf halverwege | L60x6 | S355J0 | M16 | 8.8 | 2.18 | 0 | 187 | 0.0 | 0.82 | 28.2 | 60.3 | 41.3 | 43.1 | 0.8 | 0.60 | Bending |
| O8 | Ondertaverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.77 | 0 | 182 | 0.0 | 0.66 | 39.0 | 60.3 | 41.3 | 43.1 | 0.8 | 0.85 | Bending |
| M1 | Middentraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.65 | 0 | 158 | 0.0 | 0.58 | 34.2 | 60.3 | 41.3 | 43.1 | 0.8 | 0.79 | Bending |
| M2 | Middentraverse | Kruisende staaf halverwege | L50x5 | S355J0 | M16 | 8.8 | 1.54 | 0 | 158 | 0.0 | 0.58 | 34.2 | 60.3 | 41.3 | 43.1 | 0.8 | 0.74 | Bending |
| M3 | Middentraverse | Kruisende staaf halverwege | L50x5 | S355J0 | M16 | 8.8 | 1.43 | 0 | 147 | 0.0 | 0.54 | 38.1 | 60.3 | 41.3 | 43.1 | 0.8 | 0.68 | Bending |
| M4 | Middentraverse | Kruisende staaf halverwege | L60x6 | S355J0 | M16 | 8.8 | 2.74 | 0 | 234 | 0.0 | 1.03 | 27.5 | 60.3 | 52.3 | 98.8 | 1.4 | 0.76 | Bending |
| M5 | Middentraverse | Kruisende staaf halverwege | L50x5 | S355J0 | M16 | 8.8 | 1.31 | 0 | 135 | 0.0 | 0.49 | 42.7 | 60.3 | 41.3 | 43.1 | 0.8 | 0.63 | Bending |
| M6 | Middentraverse | Kruisende staaf halverwege | L60x6 | S355J0 | M16 | 8.8 | 2.15 | 0 | 184 | 0.0 | 0.81 | 39.8 | 60.3 | 52.3 | 98.8 | 1.4 | 0.59 | Bending |
| M7 | Middentraverse | Kruisende staaf halverwege | L50x5 | S355J0 | M16 | 8.8 | 1.96 | 0 | 201 | 0.0 | 0.74 | 24.2 | 60.3 | 41.3 | 43.1 | 0.8 | 0.94 | Bending |
| M8 | Middentraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.76 | 0 | 181 | 0.0 | 0.66 | 28.4 | 60.3 | 41.3 | 43.1 | 0.8 | 0.84 | Bending |
| M9 | Middentraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.90 | 0 | 201 | 0.0 | 0.74 | 24.2 | 60.3 | 41.3 | 43.1 | 0.8 | 0.84 | Bending |
| M10 | Middentraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 1.56 | 0 | 160 | 0.0 | 0.59 | 33.8 | 60.3 | 41.3 | 43.1 | 0.8 | 0.75 | Bending |



Redundant members

RLI-TLB
HC+0/c

Date: 2021-07-09
Author: MRE
Version: 1.9

| Posnr. | Section | Schematization | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Max. usage | Notes |
|--------|----------------|---------------------------|---------|---------------|--------------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|------------|-------|
| M11 | Middentraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 0 | 140 | 0.0 | 0.51 | 40.7 | 60.3 | 41.3 | 43.1 | 0.8 | 0.65 | Bending | |
| B11 | Boventraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 0 | 134 | 0.0 | 0.49 | 43.1 | 60.3 | 41.3 | 43.1 | 0.8 | 0.62 | Bending | |
| B12 | Boventraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 0 | 129 | 0.0 | 0.47 | 44.9 | 60.3 | 41.3 | 43.1 | 0.8 | 0.60 | Bending | |
| B13 | Boventraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 0 | 125 | 0.0 | 0.46 | 46.7 | 60.3 | 41.3 | 43.1 | 0.8 | 0.58 | Bending | |
| B14 | Boventraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 0 | 116 | 0.0 | 0.42 | 51.3 | 60.3 | 41.3 | 43.1 | 0.8 | 0.54 | Bending | |
| B15 | Boventraverse | Enkele staaf | L60x6 | S355J0 | M16 | 8.8 | 0 | 189 | 0.0 | 0.83 | 38.3 | 60.3 | 52.3 | 98.8 | 1.4 | 0.61 | Bending | |
| B16 | Boventraverse | Enkele staaf | L60x6 | S355J0 | M16 | 8.8 | 0 | 181 | 0.0 | 0.79 | 41.0 | 60.3 | 52.3 | 98.8 | 1.4 | 0.59 | Bending | |
| B17 | Boventraverse | Enkele staaf | L50x5 | S355J0 | M16 | 8.8 | 0 | 208 | 0.0 | 0.76 | 23.0 | 60.3 | 41.3 | 43.1 | 0.8 | 0.77 | Bending | |
| B18 | Boventraverse | Kruisende staaf Halverweg | L50x5 | S355J0 | M16 | 8.8 | 0 | 198 | 0.0 | 0.72 | 24.7 | 60.3 | 41.3 | 43.1 | 0.8 | 0.72 | Bending | |
| M11 | High Step | Kruisende staaf Halverweg | L80x6 | S355J0 | M16 | 8.8 | 3.25 | 207 | 0.0 | 2.44 | 43.2 | 60.3 | 52.3 | 145.8 | 2.7 | 0.92 | Bending | |
| M12 | High Step | Kruisende staaf Halverweg | L70x7 | S355J0 | M16 | 8.8 | 2.80 | 205 | 0.0 | 2.10 | 46.0 | 60.3 | 61.0 | 142.7 | 2.2 | 0.97 | Bending | |



APPENDIX D

Blokdeuvels



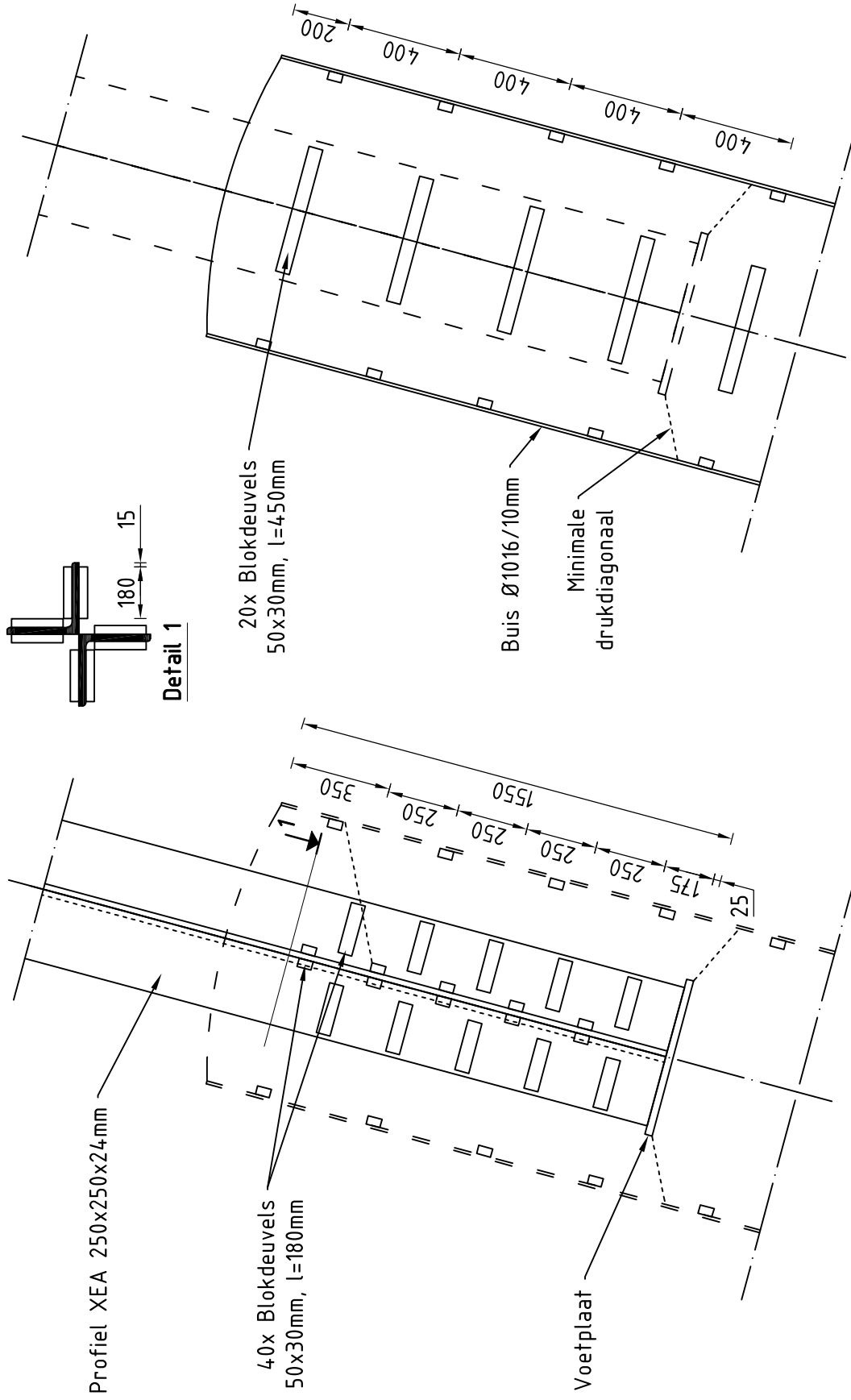
Het uitgangspunt voor de berekening van de ingestorte rand met blokdeuvels zijn de belastingen op de fundatie uit de uitvoer van het geleiderbelastingprogramma van DNV. De belastingen in de richting van de randstijl zijn van toepassing. In de tabellen is dit opgenomen in de laatste kolom $R_{z,lok}$. De controles zijn uitgevoerd met een spreadsheet. Vanwege de helling van de drukdiagonaal wordt per krachtrichting bepaald hoeveel deuvels effectief zijn, hierdoor is het aantal ingevoerde deuvels in de berekening kleiner dan het aantal deuvels op de principetekening.

Er wordt voor gekozen om de blokdeuvels universeel uit te werken op basis van het profiel van de randstijl, dit betreft een XEA250x250x24-profiel en heeft betrekking op de volgende masttypen:

- Masttype HA+0/c, HA+0/ci, HA+3/c, HA+3/ca en HA+6/c;
- Masttype HB+0/c en HB+6/c;
- Masttype HC+0/c;
- Masttype WA+0/c en WA+6/c;
- Masttype WB+0/c;
- Masttype EA-3/co.

De blokdeuvels worden getoetst op de maatgevende belasting van bovenstaande masttypen. De belasting is opgenomen in Appendix A van het betreffende masttype, masttype HC+0/c is maatgevend. De optredende belastingen van masttype HC+0/c zijn 5503kN (druk) en -4739kN (trek), deze worden ruim naar boven afgerond op **5600kN** (druk) en **-4800kN** (trek). Met deze belastingen worden alle masttypen geborgd en hebben eventuele kleine aanpassingen geen invloed op deze uitwerking.

Principe blokdeuvels - combi-hoek-, combi-wissel en combi-eindmasten



Algemene opmerkingen

- Aarding niet aangegeven
- Spiraalwapening niet aangegeven

Project: RLL-TBG
Mast: HA-B-C/c & WA-B/c & EA-co

Shear blocks

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-07-09

Auteur: TBR

Versie: 1.5

| Load | | | Results | | |
|-------------|------------|---------|-------------|------|----------------|
| Compression | $F_{Ed,c}$ | 5600 kN | Compression | U.C. | 0.87 < 1,00 OK |
| Tension | $F_{Ed,t}$ | 4800 kN | Tension | U.C. | 0.78 < 1,00 OK |

Main leg

| | | |
|--------------------|----------|-----------------------|
| Profile | | XEA 250x250x24 |
| Type | | Double (XEA) |
| Steel material | | S355 |
| Cross section | | 22934 mm ² |
| Axial capacity | N_{pl} | 8142 kN |
| Width | b | 500 mm |
| Thickness | t | 24 mm |
| Length in concrete | | 1550 mm |

Capacity shear blocks main leg

| | |
|--|-------------------------|
| $A_{f1} = A_{f1,out} + A_{f1,in} =$ | 10800 mm ² |
| $A_{f2} = A_{f2,out} + A_{f2,in} =$ | 31807.5 mm ² |
| Slope | 1 : 5 |
| $C_A = \sqrt{(A_{f2}/A_{f1})} =$ | 1.72 |
| $f_{jd} = C_A \times f_{cd} =$ | 25.8 N/mm ² |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | 4459 kN |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | 4459 kN |

Shear blocks main leg

| | | |
|--------------------|-----------|--------|
| Sides | | 2 |
| Width | b | 50 mm |
| Thickness | h | 30 mm |
| Length - outside | L_{out} | 180 mm |
| Length - inside | L_{in} | 180 mm |
| Eccentricity | e | 15 mm |
| Welds | a | 5 mm |
| c.t.c. separation | s | 250 mm |
| Number for compr. | n_c | 16 - |
| Number for tension | n_t | 16 - |

Capacity foot plate

| | |
|---|------------------------|
| $k_d =$ | 1.73 - |
| $f_{jd} = C_A \times f_{cd} =$ | 26.0 N/mm ² |
| $c = t\sqrt{(f_{yd} / 3f_{jd})} =$ | 53 mm |
| $m^* = \min(c, m) =$ | 30 mm |
| Type foot plate | Extending |
| Effective for | Compr. and tension |
| $A_{p,c} =$ | 86534 mm ² |
| $F_{Rd,c} = A_{p,druk} \times f_{jd} =$ | 2254 kN |
| $A_{p,t} =$ | 63600 mm ² |
| $F_{Rd,t} = A_{p,t} \times f_{jd} =$ | 1657 kN |

Foot plate

| | | |
|-------------|---|-------|
| Thickness | t | 25 mm |
| Ext. length | m | 30 mm |
| Welds | a | 5 mm |

Capacities

| | |
|---|----------------|
| $F_{rd,c,plate} =$ | 2254 kN |
| $F_{rd,blocks,c} =$ | 4459 kN |
| $F_{rd,c} = F_{rd,blk} + F_{rd,footplate} =$ | 6713 kN |
| U.C. compression | 0.83 < 1,00 OK |
| Welds foot plate (see next page) | 2454 kN |
| $F_{rd,t} = \min. (\text{welds} / \text{foot plate}) =$ | 1657 kN |
| $F_{rd,blocks,t} =$ | 4459 kN |
| $F_{rd,t} = F_{rd,blk} + F_{rd,footplate} =$ | 6116 kN |
| U.C. tension | 0.78 < 1,00 OK |
| U.C. welds | 0.47 < 1,00 OK |

Pile

| | | |
|-------------------|--|-----------------------|
| Name | | Buispaal |
| Diameter | | 1016 mm |
| Thickness | | 10 mm |
| Cross section | | 31604 mm ² |
| Steel material | | S355 |
| Capacity | | 11220 kN |
| Concrete strength | | C30/37 |

Shear blocks pile

| | | |
|----------------------|-----------|--------|
| Width | b | 50 mm |
| Thickness | h | 30 mm |
| Length | L | 450 mm |
| Welds | a | 5 mm |
| c.t.c. separation | s | 400 mm |
| Number for compr. | n_c | 16 - |
| Number for tension | n_t | 16 - |
| Blocks per row | n_{bl} | 4 - |
| Effectivity of total | C_{red} | 100% - |

Capacity shear blocks pile

| | |
|---|------------------------|
| $A_{f1} =$ | 13500 mm ² |
| $A_{f2} =$ | 53076 mm ² |
| $C_A = \sqrt{(A_{f2}/A_{f1})} =$ | 1.98 - |
| $f_{jd} = k_d \times f_{cd} =$ | 29.8 N/mm ² |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} \times C_{red} =$ | 6440 kN |
| U.C. compression | 0.87 < 1,00 OK |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} \times C_{red} =$ | 6440 kN |
| U.C. tension | 0.75 < 1,00 OK |
| U.C. welds | 0.45 < 1,00 OK |

Design value concrete strength

| | | |
|------------------|------------|------------------------|
| Material factor | γ_c | 1.5 |
| Add. mat. factor | γ_m | 1.33 - |
| $f_{cd} =$ | | 15.0 N/mm ² |

"Splitting" of pile

| | | |
|-----------------------|------------|-----------------------|
| Spread of forces | | 45 ° |
| Length force flow | | 1052 mm |
| Splitting force | | 2281 kN/m |
| Yield strength wall | $f_{yd} =$ | 355 N/mm ² |
| Capacity tubular pile | | 7100 kN/m |
| U.C. | | 0.32 < 1,00 OK |

Steel tower stub

| | | |
|------------------|------------|-----------------------|
| Yield strength | $f_{yd} =$ | 355 N/mm ² |
| Tensile strength | $f_{ud} =$ | 490 N/mm ² |

Project: RLL-TBG
 Mast: HA-B-C/c & WA-B/c & EA-co

Welds of shear blocks of main leg

Out-of-plane loading

Plate

t = 50 mm
 Grade S355
 $f_{yd} = 355 \text{ N/mm}^2$
 $f_u = 490 \text{ N/mm}^2$

Member forces

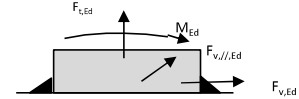
Factor 1.2
 $F_{t,Ed} = 0 \text{ kN}$
 $F_{v,Ed} = F_{rd,c} / n = 334 \text{ kN}$
 $F_{v//,Ed} = 0 \text{ kN}$
 $M_{Ed} = 1/2 b / h \times F_{v,Ed} = 5.02 \text{ kNm}$

Check

$\sigma_{w,Ed} = 203 \text{ N/mm}^2 \leq$
 $\sigma_1 = 102 \text{ N/mm}^2 \leq$

Welds

a = 5 mm
 l = 360 mm
 $\beta_w = 0.9 -$
 $\gamma_{M2} = 1.25 -$



Stress components

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 4al = 0 \text{ N/mm}^2$
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 4al = 66 \text{ N/mm}^2$

 66 N/mm^2
 $b^* = b + 2/3av^2 = 54.7 \text{ mm}$
 $\sigma_1 = \tau_1 = 0.706M_{Ed} / al b^* = 36 \text{ N/mm}^2$
 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$
 $\sigma_{w,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 203 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$ U.C. = **0.47 OK**
 $0.9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$ U.C. = **0.29 OK**

Welds of shear blocks of pile

Out-of-plane loading

Plate

t = 50 mm
 Grade S355
 $f_{yd} = 355 \text{ N/mm}^2$
 $f_u = 490 \text{ N/mm}^2$

Member forces

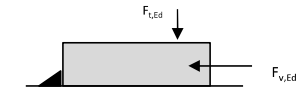
Factor 1.2
 $F_{t,Ed} = 1/2 b / h \times F_{v,Ed} = 145 \text{ kN}$
 $F_{v,Ed} = 483 \text{ kN}$
 $F_{v//,Ed} = 0 \text{ kN}$
 $M_{Ed} = 0.00 \text{ kNm}$

Check

$\sigma_{w,Ed} = 197 \text{ N/mm}^2 \leq$
 $\sigma_1 = 99 \text{ N/mm}^2 \leq$

Welds

a = 5 mm
 l = 450 mm
 $\beta_w = 0.9 -$
 $\gamma_{M2} = 1.25 -$



Stress components

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 2al = 23 \text{ N/mm}^2$
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 2al = 76 \text{ N/mm}^2$

 76 N/mm^2
 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$
 $\sigma_{w,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 197 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$ U.C. = **0.45 OK**
 $0.9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$ U.C. = **0.28 OK**

Welds of foot plate

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$
 Weld size a = 5 mm
 Length l = 2b + 2b - t = 1952 mm
 Capacity $F_{Rd} = a \times l \times f_{w,d} / \sqrt{3} = 2454 \text{ kN}$



APPENDIX E

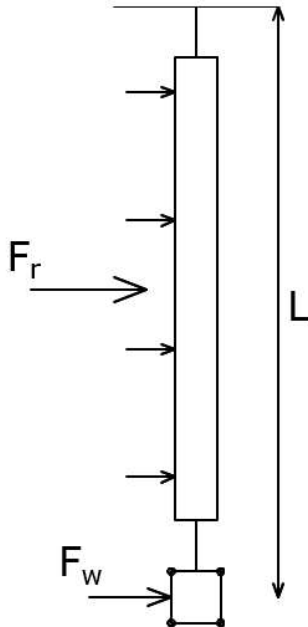
Liggers

1 BEREKENING OPHANGING POSTISOLATOREN

De volgende onderdelen worden berekend:

- De belastingen op de ophanging van de postisolatoren door wind en eigen gewicht;
- De dimensionering van de ophangconstructies.

Onderstaand zijn de optredende belastingen geschematiseerd:



Figuur 1 Belastingeschema

1.1 Uitgangspunten & afmetingen postisolatoren

Voor het berekenen van de liggers voor de ophanging van de postisolatoren in de mastkoppen van de HA-masten wordt één berekening gemaakt met de volgende uitgangspunten:

- Windgebied II;
 - Windhoogte 54,5m (conservatief hoogte masttype HB+6/c aangehouden);
 - Onbebouwd;
- Referentieperiode 50 jaar;
- Belastingfactor 1,5.

De volgende factoren worden gehanteerd:

- Krachtcoëfficiënt 1,2 voor isolatoren
- Constructiefactor geleider 1,0;
- Krachtcoëfficiënt geleider 1,0;
- Constructiefactor geleider 1,0.

Conform het uitgangspuntendocument zijn de afmetingen als volgt:

Tabel 1 Gegevens postisolatoren

| Omschrijving | Ophanging | Gewicht [kN] | Lengte [m] | Windopp. [m] |
|---------------------|---------------|-----------------|---------------|-----------------|
| Fasegeleider 380 kV | Bretelfixatie | 2,0 | 4,5 | 1,0 |
| Fasegeleider 150 kV | Bretelfixatie | 1,5 | 2,7 | 0,7 |

De diameter van de geleiders is 32mm.

1.2 Belastingen

De extreme stuwdruk $q_{p(z)}$ in windgebied II op een hoogte van 54,5m is 1,41 kN/m².

Er komen drie varianten voor:

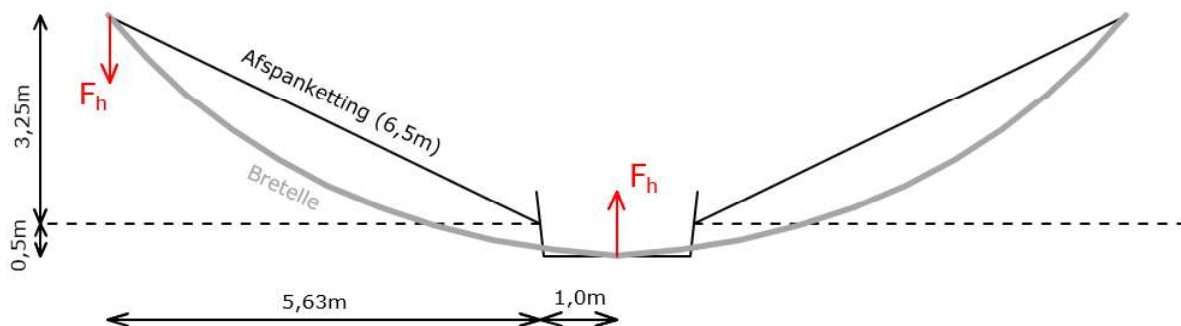
1. 380 kV geleider met één postisolator;
 - Lengte geleider aan postisolator ca. 9 m;
2. 150 kV geleider met één postisolator;
 - Lengte geleider aan postisolator ca. 7 m;
3. 150 kV geleider met twee postisolatoren;
 - Lengte geleider aan postisolator ca. 3,5 m.

In het horizontale vlak bestaat er een afstand tussen het uiteinde van de afspanketting en de postisolator (zie figuur 2). Dit veroorzaakt een extra horizontale kracht vanuit de bretelle op de onderzijde van de postisolator (zie figuur 3). Het gewicht van de bretelle (380kV) is gelijk aan $(4 \times 17,7\text{N/m}) = 70,8\text{N/m}$. De horizontale kracht evenwijdig aan de brettelle is gelijk aan:

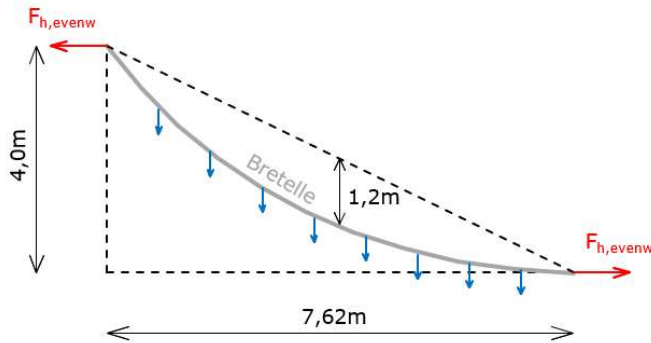
- $F_{h,evenw} = 1/8 \cdot q \cdot L^2 / u = 1/8 \cdot 0,0708\text{kN/m} \cdot (7,62\text{m})^2 / 1,2\text{m} = 0,4 \text{ kN}.$

De horizontale kracht loodrecht op de postisolator is gelijk aan:

- $F_{h,gel} = 2 \cdot 0,4\text{kN} \cdot 3,75\text{m} / 7,62\text{m} = 0,4 \text{ kN}.$



Figuur 2 Bovenaanzicht bretelle



Figuur 3 Zij-aanzicht bretelle

Voor het 180kV-circuit wordt dezelfde berekening gemaakt. De afspanketting heeft een lengte van 4,0m en de tussen afstand is 2 x 2m (i.p.v. 2 x 1m). De postisolator hangt 1,0m naar buiten en de horizontale afstand (ten gevolge van de hoek) is gelijk aan $(\sin(30^\circ) \cdot 4m) = 2m$. De lengte is dan gelijk aan $(\sqrt{(\cos(30^\circ) \cdot 4m + 2m)^2 + (2m + 1m)^2}) = 6,23m$. De krachten zijn dan gelijk aan:

- $F_{h,evenw} = \frac{1}{8} \cdot q \cdot L^2 / u = 1/8 \cdot 0,0354kN/m \cdot (6,23m)^2 / 0,8m = 0,2 \text{ kN};$
- $F_{h,gel} = 2 \cdot 0,4kN \cdot 3,0m / 6,23m = 0,2 \text{ kN}.$

Belasting bij wind loodrecht op de geleider

Voor elke variant zijn in onderstaande tabellen de optredende reactiekrachten (F_h , $F_{v,tot}$ en M_{tot}) op het ophangpunt van de postisolator berekend.

Tabel 2 Optredende belastingen per variant – wind loodrecht

| Var. | $q_p(z)$ [kN/m ²] | G_{post} [kN] | L_{post} [m] | Opp [m ²] | n_{gel} [n] | \emptyset_{gel} [m] | G_{gel} [kN/m] | L_{gel} [m] | $F_{h,gel}$ [kN] |
|------|----------------------------------|--------------------|-------------------|--------------------------|------------------|--------------------------|---------------------|------------------|---------------------|
| 1 | 1,41 | 2 | 4,5 | 1 | 4 | 0,032 | 0,0177 | 9 | 0,4 |
| 2 | 1,41 | 1,5 | 2,7 | 0,7 | 2 | 0,032 | 0,0177 | 7 | 0,2 |
| 3 | 1,41 | 1,5 | 2,7 | 0,7 | 2 | 0,032 | 0,0177 | 3,5 | 0,1 |

| Var. | $C_{f,r}$ [-] | S_r [-] | $F_{r,k}$ [kN] | $M_{r,k}$ [kNm] | $C_{f,w}$ [-] | S_w [-] | $F_{w,k}$ [kN] | $M_{w,k}$ [kNm] |
|------|------------------|--------------|-------------------|--------------------|------------------|--------------|-------------------|--------------------|
| 1 | 1,2 | 1 | 1,69 | 3,81 | 1 | 1 | 1,62 | 7,31 |
| 2 | 1,2 | 1 | 1,18 | 1,60 | 1 | 1 | 0,63 | 1,71 |
| 3 | 1,2 | 1 | 1,18 | 1,60 | 1 | 1 | 0,32 | 0,85 |

| Var. | γ [-] | $F_{v,Ed}$ [kN] | $F_{h,tot,Ed}$ [kN] | $M_{tot,Ed}$ [kNm] |
|------|-----------------|--------------------|------------------------|-----------------------|
| 1 | 1,5 | 4,0 | 5,6 | 19,4 |
| 2 | 1,5 | 2,6 | 3,0 | 5,8 |
| 3 | 1,5 | 2,4 | 2,4 | 4,1 |

Belasting bij wind evenwijdig aan de geleider

Waar relevant wordt er ook getoetst aan wind evenwijdig aan de geleider. In onderstaande tabel zijn de optredende krachten weergegeven.

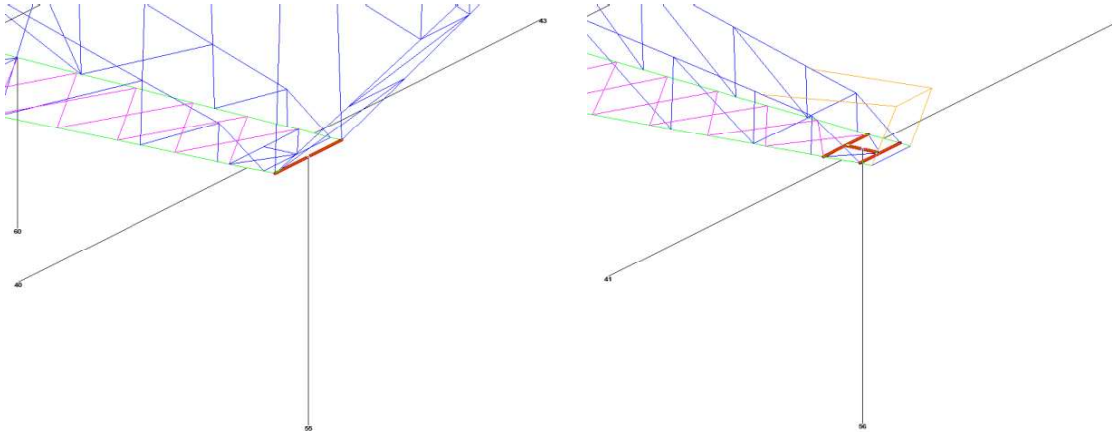
Tabel 3 Optredende belastingen per variant – wind evenwijdig

| Var. | L _{post} [m] | F _{h,gel} [kN] | M _{r,-,k} [kNm] | F _{r,k} [kN] | M _{r,/,k} [kNm] | F _{v,Ed} [kN] | F _{h,-,Ed} [kN] | M _{r,-,Ed} [kNm] | F _{h,/,Ed} [kN] | M _{r,/,Ed} [kNm] |
|------|--------------------------|----------------------------|-----------------------------|--------------------------|-----------------------------|---------------------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
| 1 | 4,5 | 0,4 | 1,8 | 1,69 | 3,81 | 4,0 | 0,6 | 2,7 | 2,5 | 5,7 |
| 2 | 2,7 | 0,2 | 0,54 | 1,18 | 1,60 | 2,6 | 0,3 | 0,8 | 1,8 | 2,4 |
| 3 | 2,7 | 0,1 | 0,27 | 1,18 | 1,60 | 2,4 | 0,2 | 0,4 | 1,8 | 2,4 |

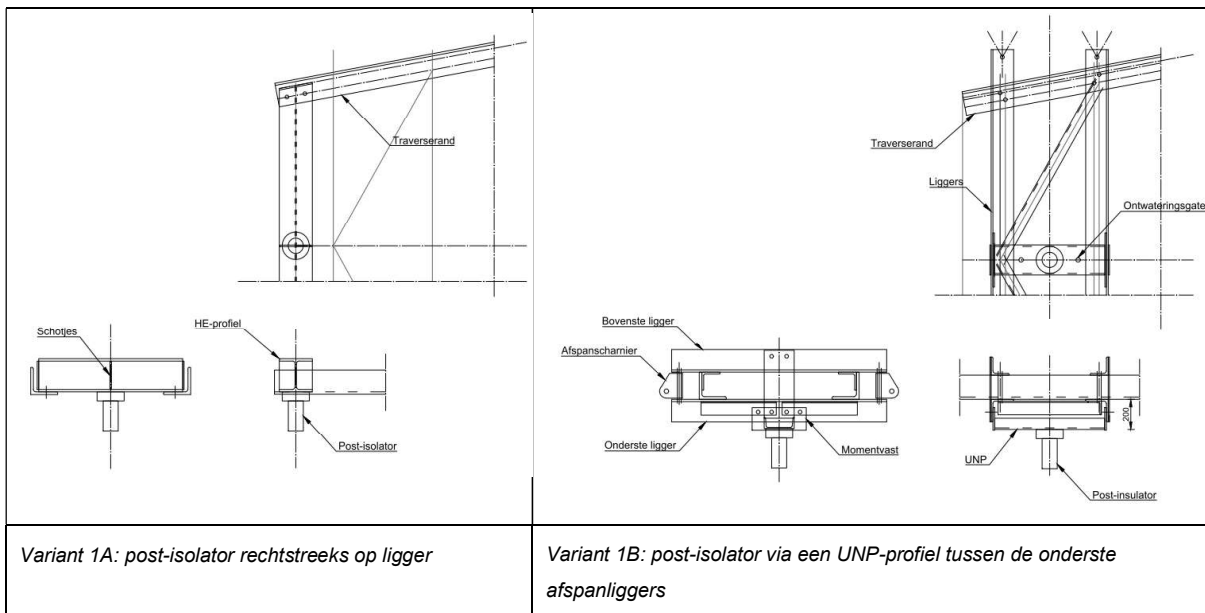
2 VARIANT 1 – 380 KV – 1 POSTISOLATOR

De ophanging van de postisolator bij variant 1 kent twee varianten:

- A. Ophanging aan enkele ligger (onderstaand links);
- B. Ophanging aan frame (onderstaand rechts).



Figuur 4 Principe ophanging variant 1A (links) en 1B (rechts)



Figuur 5 Principedetails voor bevestiging post-insulator variant 1A en 1B

2.1 Variant A

De postisolator wordt opgehangen aan een enkele stalen ligger. Deze ligger wordt daardoor in twee richtingen en op torsie belast. De optredende belastingen zijn:

- Verticaal F_v 4,0 kN;
- Horizontaal $F_{h,tot}$ 5,6 kN;
- Torsiemoment M_{tot} 19,4 kNm.

De maximale lengte van de ligger is 1,82m (boventraverse). Het profiel van de ligger is HEB220 (S355). De ligger wordt getoetst aan de hand van een excel-sheet. Uit berekening blijkt dat de ligger voldoet met een maximale UC van 0,78. Voor berekening, zie na pagina 6.

2.2 Variant B

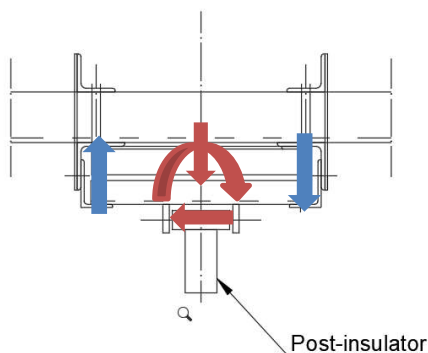
Onderstaand is de situatie schematisch weergegeven. De hoeklijnen hebben een (minimale) doorsnede van 150x150x14mm. De afstand tussen de hoeklijnen is minimaal 600 mm. De bovenste en onderste hoeklijnen worden halverwege de overspanning gekoppeld.

De optredende maximale reactiekracht is gelijk aan $(4,0\text{kN}/2 + 19,4\text{kNm}/0,6\text{m}) = 34,3\text{kN}$. Per ligger is de kracht gelijk aan $(34,3\text{kN} / 2) = 17,2\text{kN}$.

De maximale overspanning is 2,5m (middentraverse → 150kV heeft langste ligger, deze als maatgevend aangehouden). Het totale moment in het hoekstaal wordt dan $(0,25 \cdot (17,2\text{kN} + 5,3\text{kN}/2) \cdot 2,5\text{m}) = 12,4\text{kNm}$.

Het weerstandsmoment is gelijk aan 83500mm^3 . De spanning is gelijk aan $(12,4 \cdot 10^6 \text{ Nmm} / 83500\text{mm}^3) = 158\text{MPa}$. De ligger voldoet met een UC van $(158\text{MPa} / 355\text{MPa}) = 0,45$.

De ligger die hoeklijnen koppelt heeft een doorsnede van UNP220 en wordt om de zwakke as belast. Het optredende moment is gelijk aan $(1/4 \cdot 4,0\text{kN} \cdot 0,6\text{m} + 1/2 \cdot 19,4\text{kNm}) = 10,3\text{kNm}$. De spanning is gelijk aan $(10,3 \cdot 10^6 \text{ Nmm} / 33500\text{mm}^3) = 307\text{MPa}$. De ligger voldoet met een UC van $(307\text{MPa} / 355\text{MPa}) = 0,86$.



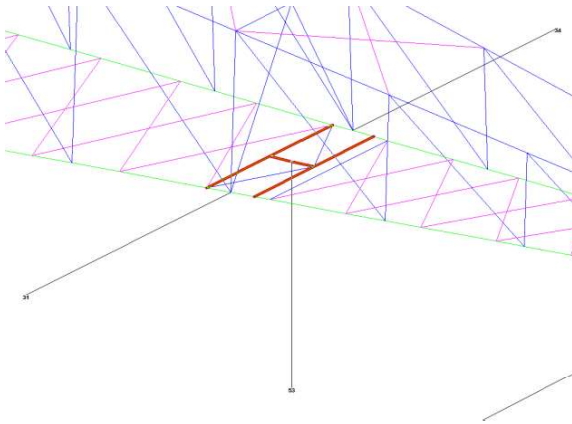
Figuur 6 Schematische weergave opvang variant 1B

3 VARIANT 2 – 150 KV – 1 POSTISOLATOR

Bij deze variant wordt de postisolator opgehangen aan een frame, dit komt overeen met variant 1B. De optredende belastingen zijn:

- Verticaal F_v 2,6 kN;
- Horizontaal $F_{h,tot}$ 3,0 kN;
- Torsiemoment M_{tot} 5,8 kNm.

De belastingen zijn lager en de liggers maximaal even lang als bij variant 1B. Voor variant 2 voldoen profielen 150x150x14mm dus ook, voor uitwerking zie variant 1B.

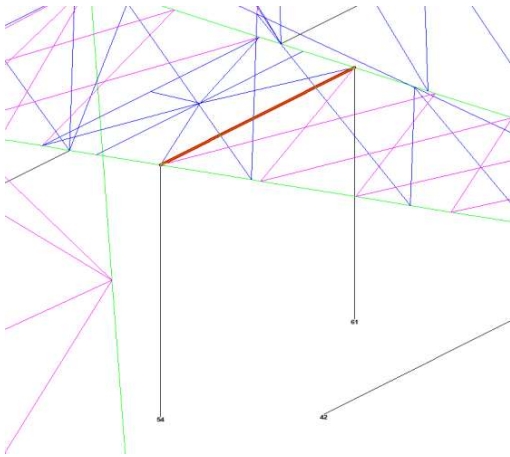


Figuur 7 Principe ophanging variant 2

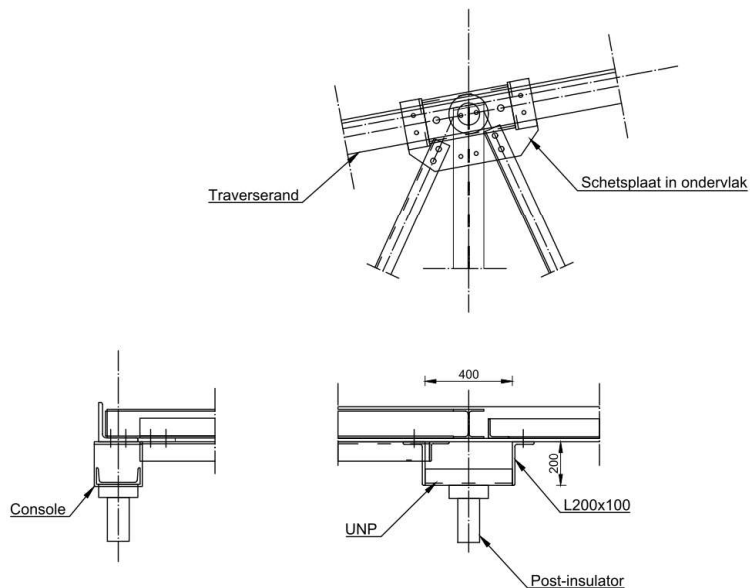
4 VARIANT 3 – 150 KV – 2 POST-ISOLATOR

De postisolator wordt via een verlaagde console ingeklemd in twee richtingen opgehangen aan de onderrand van de traverse. De torsie op de onderrand wordt opgenomen door een ligger uit HE-profiel (diagonalen worden verwaarloosd), in de richting van de onderrand neemt de rand de momenten op. De optredende belastingen zijn:

- Verticaal F_v 2,4 kN;
- Horizontaal $F_{h,tot}$ 2,4 kN;
- Torsiemoment M_{tot} 4,1 kNm.



Figuur 8 Principe ophanging variant 3



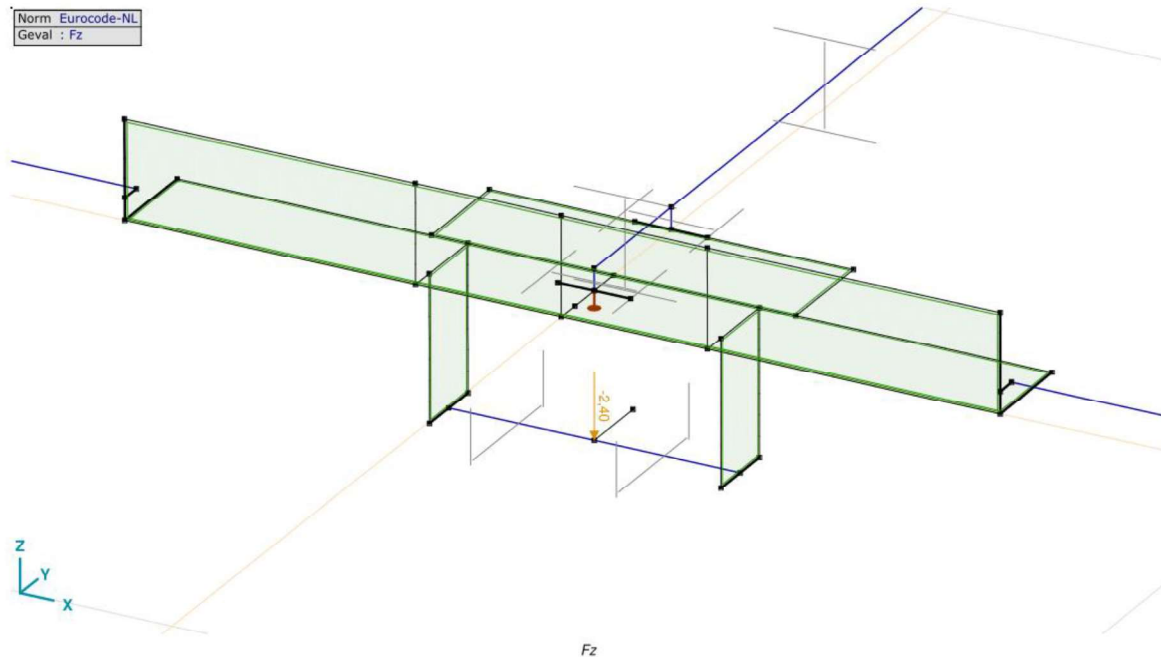
Figuur 9 Principedetail bevestiging post-isolator aan rand

De ligger wordt belast door een kopmoment. Dit moment is volgens Tabel 3 gelijk aan 2,4 kNm. Ligger met praktisch gekozen profiel HE140A volstaat.

Kritisch aspect in de verbinding is de krachtsoverdracht van het buigend moment uit het vlak van de console naar de ligger. De onderrand wordt lokaal (tussen de console en HE-ligger) op torsie belast en de flens van het hoekprofiel

wordt ook op buiging belast. Om de krachtsinleiding mogelijk te maken wordt de onderrand verstijfd met een schetsplaat waarmee de HE-ligger en diagonalen worden verbonden.

De controle is uitgevoerd met het programma AxisVM. Zowel buiging in het vlak als buiging uit het vlak is gecontroleerd. Als minimaal profiel van de onderrand is uitgegaan van L150x150x14. De maximale drukkracht in de rand is in combinatie met de buiging meegenomen.



Figuur 10 Rekenmodel krachtsinleiding post-isolator aan onderrand

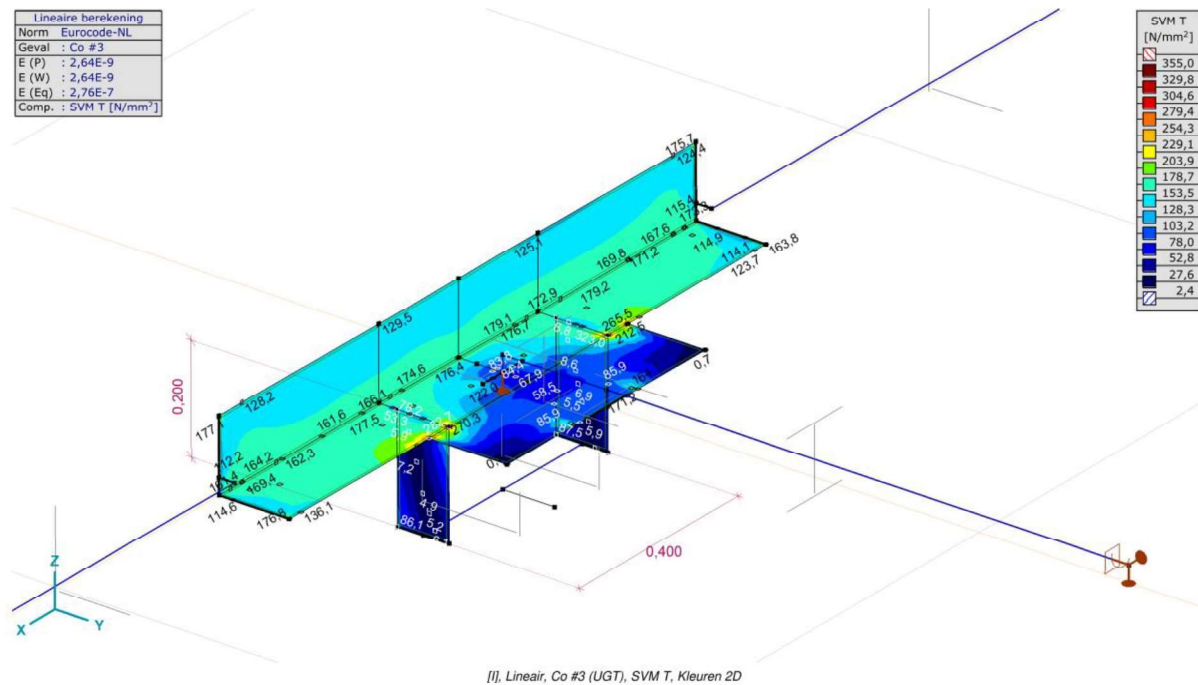
De belastingen zijn ontleend aan Tabel 2 en Tabel 3 voor de 150 kV post-isolator. De belastingen zijn in AxisVM gecombineerd met het verticale gewicht, en met twee richtingen van M_x en M_y , waarbij belastinggevallen zijn verminderd tot een factor 0,71.

Tabel 4 Belastingen op console

| Var. | $F_{z,Ed}$ [kN] | $F_{x,Ed}$ [kN] | $F_{y,Ed}$ [kN] | $M_{x,Ed}$ [kNm] | $M_{y,Ed}$ [kNm] |
|-------|--------------------|--------------------|--------------------|---------------------|---------------------|
| M_x | | | 1,8 | 2,4 | |
| M_y | | 3,0 | | | 5,8 |
| F_z | 2,4 | | | | |
| N | 600 | | | | |

Uit de berekening blijkt dat de combinatie van spanningen door torsie en buiging toelaatbaar is.

| | |
|---------------------|------------------------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | Co #3 |
| E (P) | : 2,64E-9 |
| E (W) | : 2,64E-9 |
| E (Eq) | : 2,76E-7 |
| Comp. | : SVM T [N/mm ²] |



[I], Linear, Co #3 (UGT), SVM T, Kleuren 2D

Figuur 11 Spanningen in de maatgevende belastingcombinatie

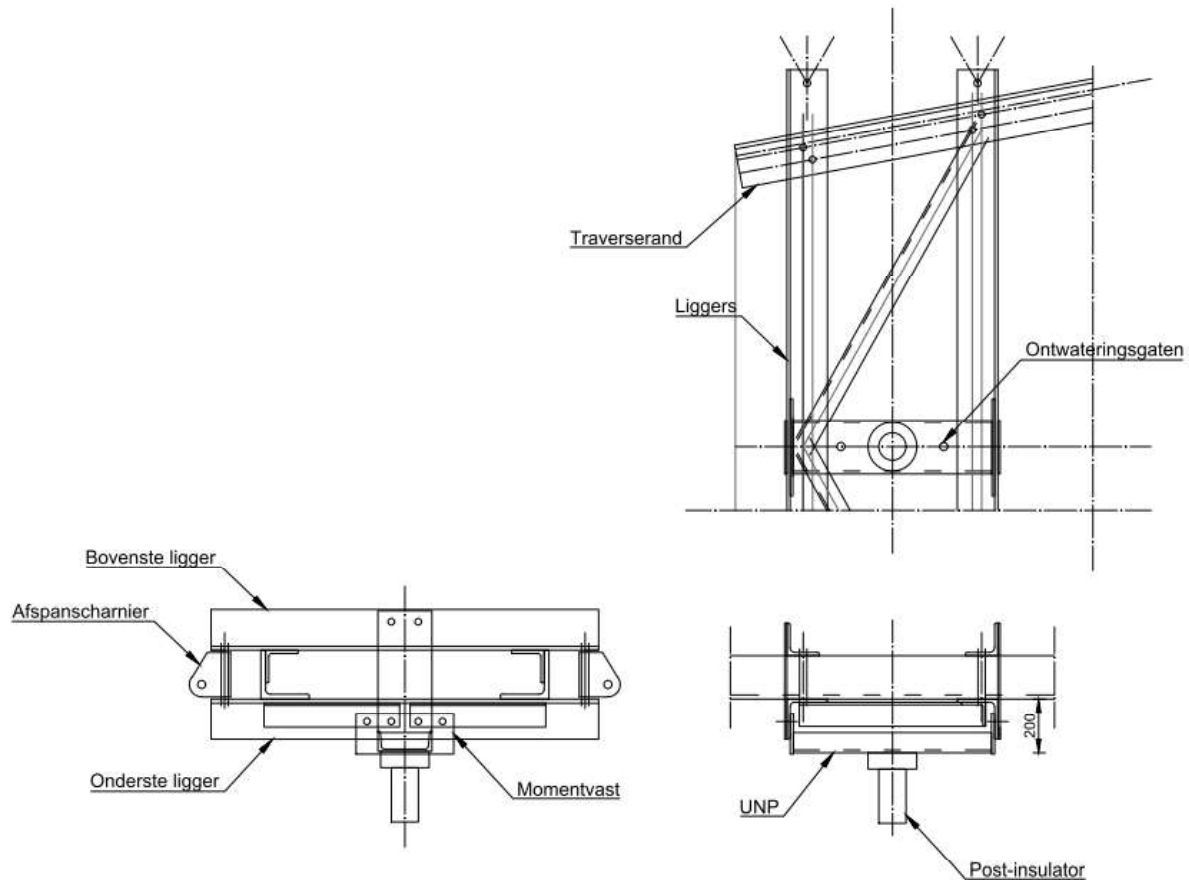
In het model treden elastisch berekend bij hoeken spanningsconcentraties op. Zie Figuur 11. In de uitvoer opgenomen in de bijlage blijkt dat de hoogste spanning 323 N/mm² bedraagt. De toetsing is:

$$U.C. = 323 \text{ N/mm}^2 / 355 \text{ N/mm}^2 = 0,91 \leq 1,00 \text{ OK.}$$

De staalprofielen voldoen.

5 CONTROLE AFSPANLIGGERS

De afspankettingen van de hoekmast worden bevestigd tussen twee paren van hoekprofielen. De liggers worden belast op buiging in het geval van een lijnhoek. Als gevolg van de belasting van het afspanscharnier wordt het hoekprofiel ook op lokale buiging belast.



Figuur 12 Principe van de afspanliggers. De uitkragende ligger wordt in het geval van een lijnhoek op buiging belast door de kracht uit de afspanketting

De profielen worden gecontroleerd op buiging met het programma AxisVM, de profielen worden geschematiseerd met plaalementen.

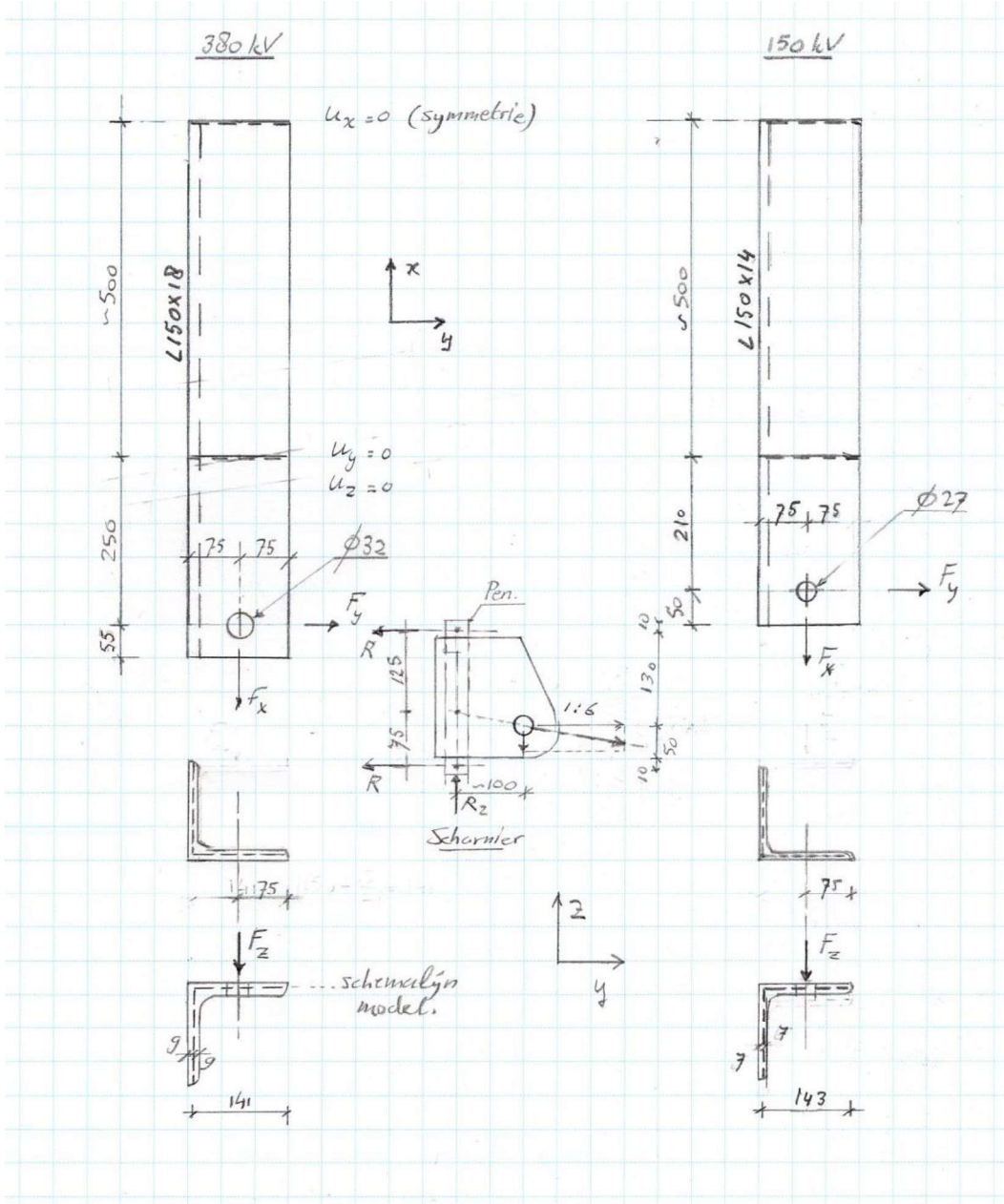
Vanwege uniformiteit over de masttypes in afspanscharnieren wordt de controle uitgevoerd op basis van het masttype met de grootste lijnhoek en de grootste uitkraging. Dit is de HC+0-mast van het solo-type, omdat de ondertraverse de grootste breedteverandering heeft, met bijbehorend grootste uitkraging.

In het DO zal de verbinding verder in detail worden gecontroleerd. Omdat de plaatbuiging bepalend is voor het profiel dat wordt toegepast, wordt nu de controle van de liggers op buiging uitgevoerd.

Twee profielen worden gecontroleerd: het profiel voor de 150 kV-afspankettingen (L150x150x14) en het profiel voor de 380 kV-afspankettingen (L150x150x18).

Voorlopig worden bovenste en onderste ligger gelijk genomen, in UO-fase kan de bovenste ligger nog geoptimaliseerd worden omdat deze niet door de verticale belasting belast wordt.

Schema



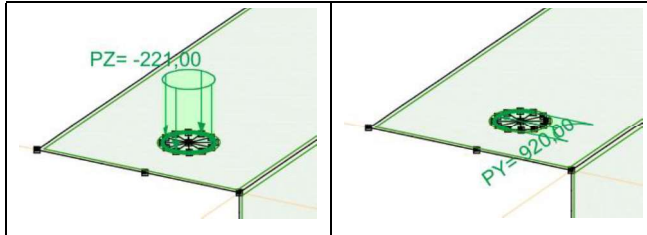
Figuur 13 Schematisering liggers

De helft van de ligger wordt berekend met symmetrie randvoorwaarden. De zwaartelij van de plaatdikte is het uitgangspunt voor de geometrie. De verbinding met de traverserand wordt vereenvoudigd tot een lijnoplegging aan de bovenflens met fixatie van y- en z-richting. De berekening is lineair-elastisch.

Tabel 5 Geleiderbelastingen

| Belastingcombinatie | Spanning | Fxtotaal | Fytotaal | Fztotaal | Ftrekhead |
|---------------------|----------|----------|----------|----------|-----------|
| ULS 3_120 | 380 kV | 220,0 | 142,3 | 44,4 | 261,6 |
| | 150 kV | 109,9 | 71,0 | 22,2 | 130,7 |

De belastingen worden omgezet naar een lijnlast rondom het gat voor de pen. De x- en y-belasting op de helft van de omtrek, de verticale belasting (z-richting) rondom de gehele omtrek.



Figuur 14 Invoer van belastingen als lijnlast rondom boutgat

De belasting van Tabel 5 wordt verdeeld over twee kettingen. Vanwege de geometrie van het afspanscharnier wordt circa 65% van de belasting verdeeld naar de onderste ligger.

Tabel 6 Schematisering belasting

| | d (mm) | Omtrek bij Fx (mm) | Omtrek bij Fy (mm) | Omtrek bij Fz (mm) |
|---------------------|--------|-----------------------|-----------------------|-----------------------|
| 380 kV | 32 | 50,3 | 50,3 | 100,5 |
| 150 kV | 27 | 42,4 | 42,4 | 84,8 |
| Verhouding afdracht | | 0,65 | 0,65 | 1 |

De lijnbelasting wordt berekend met:

$$q = 1/2 \cdot k \cdot F / O$$

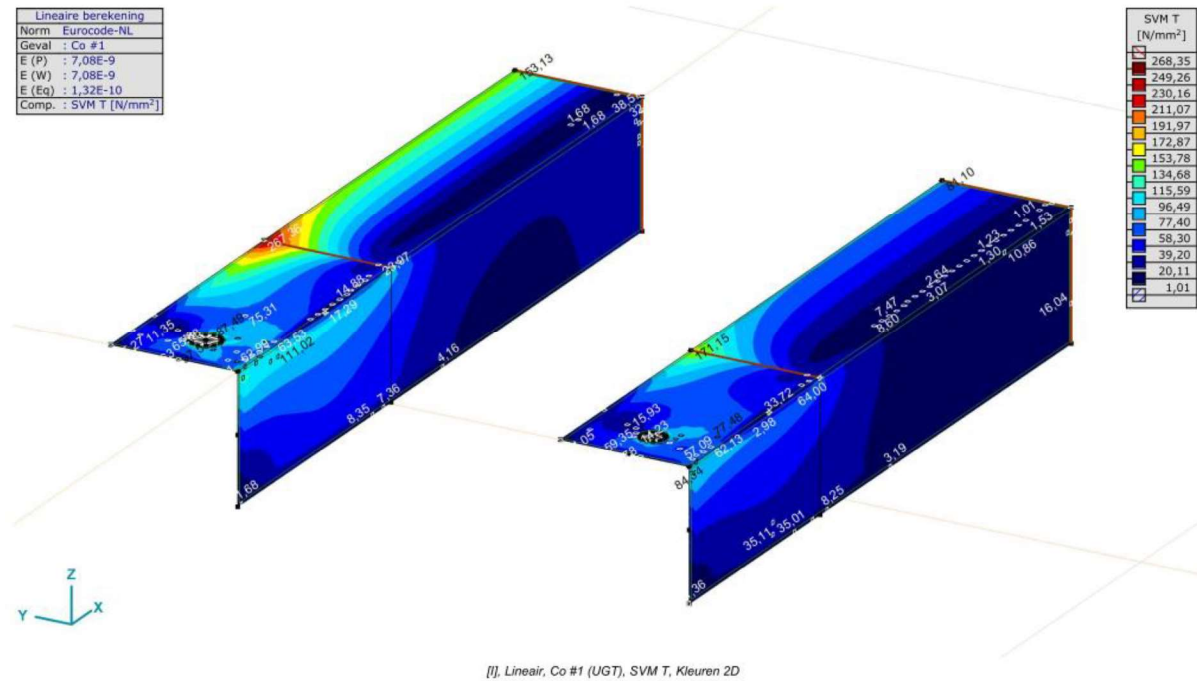
In Tabel 7 zijn de lijnlasten berekend met bovenstaande formule. Deze zijn in AxisVM ingevoerd.

Tabel 7 lijnlast rond gat

| | qx (kN/m) | qy (kN/m) | qz (kN/m) |
|--------|-----------|-----------|-----------|
| 380 kV | 1422 | 920 | 221 |
| 150 kV | 842 | 544 | 131 |

Toetsing

Zie de uitvoer van AxisVM. De combinatie van buiging en lokale buiging op het bovenzvlak van het hoekprofiel ter plaatse van de lijnoplegging is maatgevend.



Figuur 15 Maximale spanning in hoekprofiel voor 380 kV en 150 kV

Toetsing:

L150x18: U.C. : $267 / 355 = 0,75 \leq 1,00$ OK

L150x14: U.C. : $171 / 355 = 0,48 \leq 1,00$ OK

De profielen voldoen.

Project:

Constructeur: DNV GL - Energy




AxisVM X5 R4h - Geregistreerd aan DNV GL - Energy
Post aan onderstrand HA_s,axs

Rapport

Rapport, Inhoudsopgave

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| Fz | | 13 | [I], Linear, Co #5 (UGT), SVM T, Kleuren 2D | | 33 |
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| [I], Linear, Omhullende (Alle UGT), Vy, Lijnen (gevuld) | | 21 | Interne krachten knooppiegging [Linear, Omhullende (Alle UGT)] | | 41 |

Materialen

| Naam | Type | Nationale norm | Materiaalnorm | Model | E_x [N/mm ²] | E_y [N/mm ²] | E_z [N/mm ²] | ν | α_T [1/°C] | ρ [kg/m ³] | Materiaal kleur | Contour kleur | Structuur | P_1 |
|---------|-------|----------------|---------------|---------|----------------------------|----------------------------|----------------------------|-------|-------------------|-----------------------------|---|---|---|-------------------------------------|
| I S 355 | Staal | Eurocode-NL | 10025-2 | Lineair | 210000 | 210000 | 210000 | 0,30 | 1,2E-5 | 7850 |  |  |  | f_y [N/mm ²] = 355,00 |

| Naam | f_{t1} [N/mm ²] | P_2 | P_3 | P_4 | P_5 | P_6 | P_7 | P_8 | P_9 | P_{10} | P_{11} | P_{12} | P_{13} | P_{14} |
|---------|--|-------|-------|-------|-------|-------|-------|-------|-------|----------|----------|----------|----------|----------|
| I S 355 | f_{t1} [N/mm ²] = 510,00 | | | | | | | | | | | | | |
| | f_y^c [N/mm ²] = 335,00 | | | | | | | | | | | | | |
| | f_{t1}^c [N/mm ²] = 470,00 | | | | | | | | | | | | | |

Naam: Materiaalnaam; Type: Type materiaal; Model: Materiaal model; E_x : Elasticiteitsmodulus in lokale x richting; E_y : Elasticiteitsmodulus in lokale y richting; E_z : Elasticiteitsmodulus in lokale z richting; ν : Poisson's verhouding; α_T : Warmteuitzettingscoëfficiënt; ρ : Dichtheid; **Materiaal kleur**: Materiaalkleur;
 Contour kleur: Contourkleur; $P_1, P_2, P_3, P_4, P_5, P_6, P_7, P_8, P_9, P_{10}, P_{11}, P_{12}, P_{13}, P_{14}$: Ontwerpparameter;

Project:

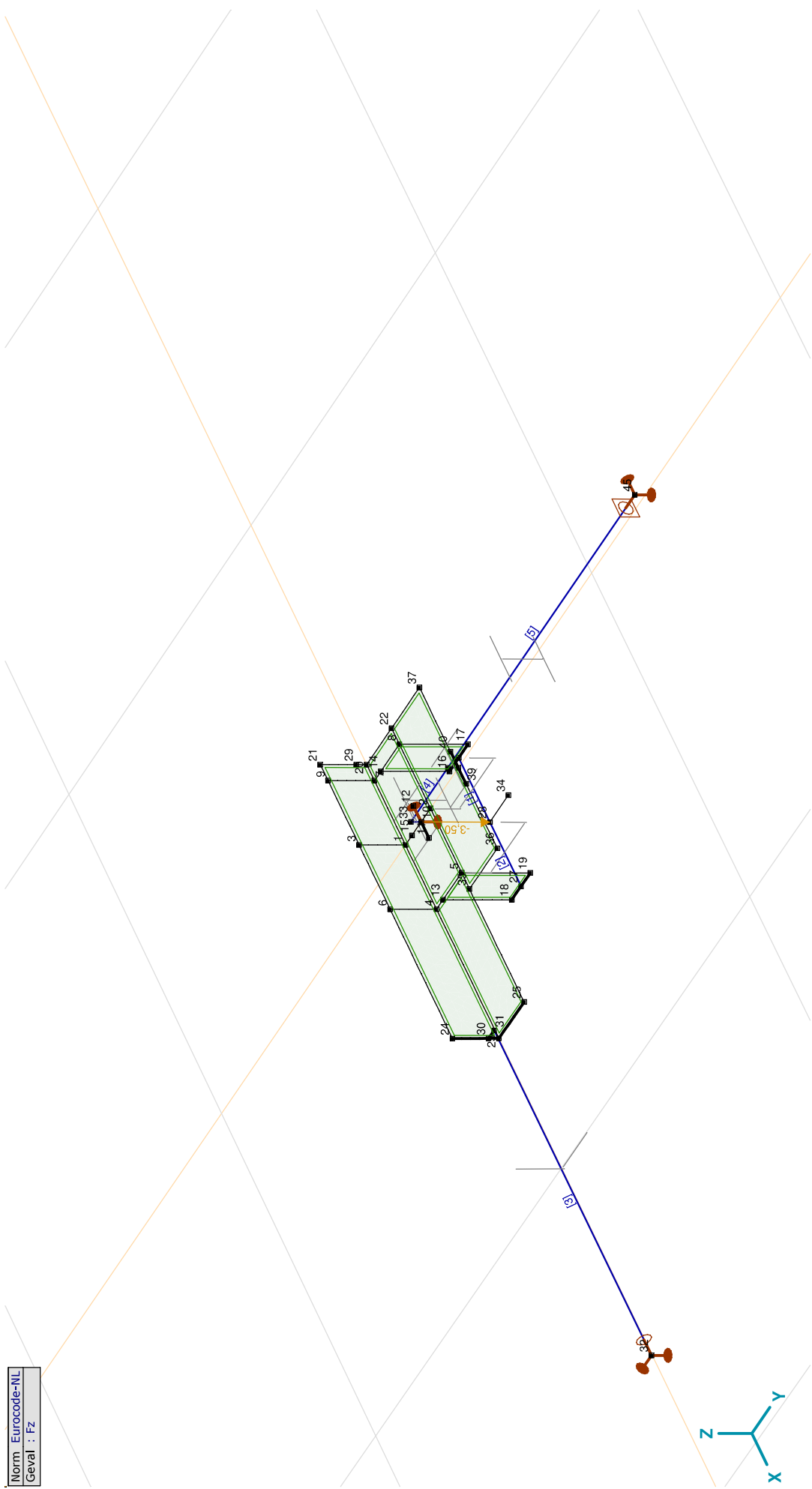
Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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Norm Eurocode-NL
Geval : Fz



Knopen en staven

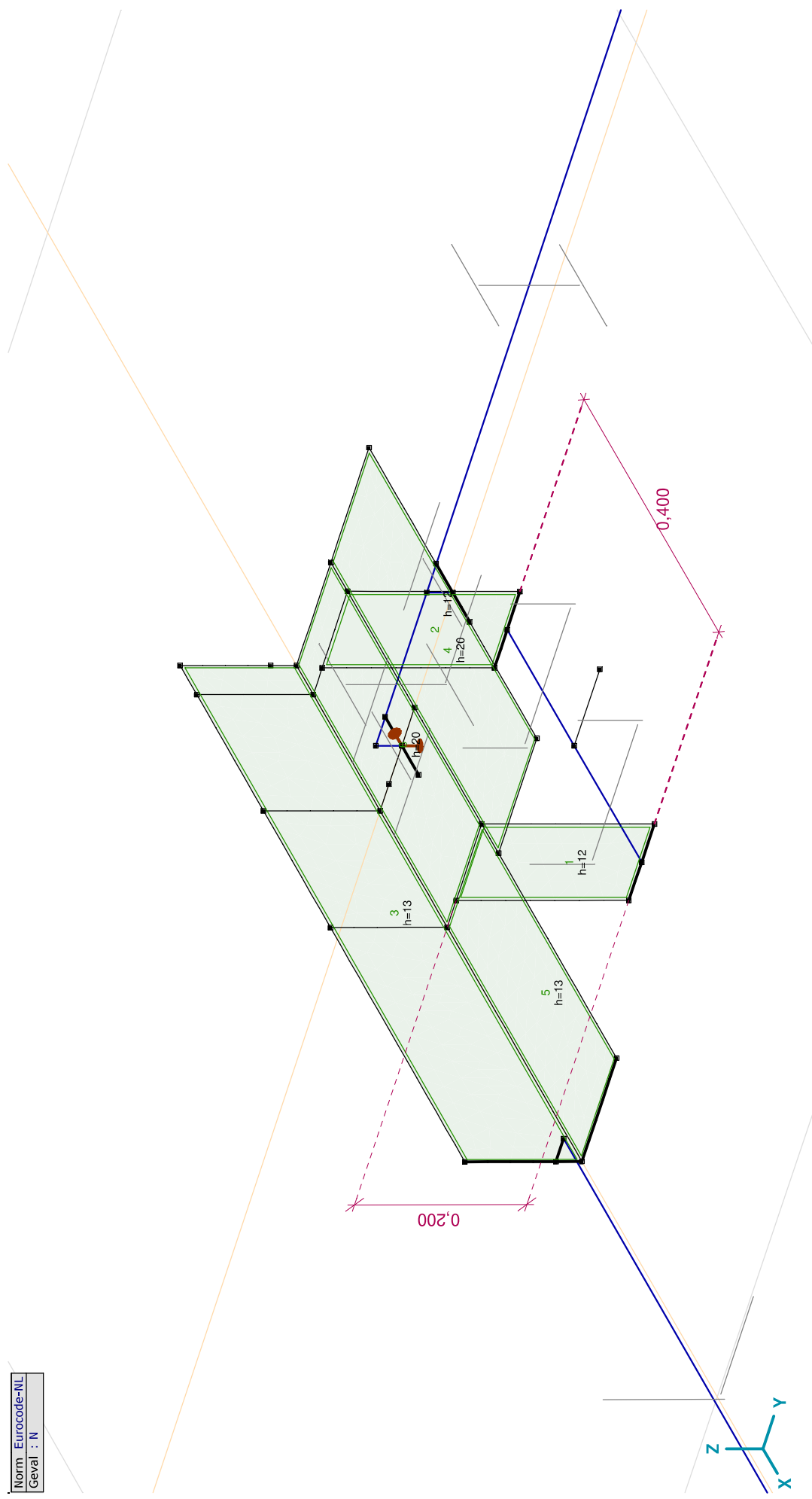
Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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| | |
|-------|-------------|
| Norm | Eurocode-NL |
| Geval | : N |



Dikte

Project:





Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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Profielen

| Naam | Tekening | Productie | Vorm | h [mm] | b [mm] | tw [mm] | tf [mm] | r1 [mm] | r2 [mm] | r3 [mm] | Ax [mm ²] | Ay [mm ²] | Az [mm ²] | Ix [mm ⁴] | Iy [mm ⁴] | Iz [mm ⁴] |
|----------------|---|-----------|------|-----------|-----------|------------|------------|------------|------------|------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| 1 U 200 |  | Gewalst | U | 200,0 | 75,0 | 8,5 | 11,5 | 11,5 | 6,0 | 0 | 3218,52 | 931,26 | 1555,63 | 121078,6 | 1,9E+07 | 1477534,0 |
| 2 L 150X150X14 |  | Gewalst | L | 150,0 | 150,0 | 14,0 | 14,0 | 16,0 | 8,0 | 0 | 4031,60 | 1760,18 | 1776,16 | 278959,0 | 84533331,0 | 8453331,0 |
| 3 HE 140 A |  | Gewalst | I | 133,0 | 140,0 | 5,5 | 8,5 | 12,0 | 0 | 0 | 3142,19 | 2147,66 | 704,86 | 81932,8 | 1E+07 | 3893251,0 |
| 4 L 140X140X13 |  | Gewalst | L | 140,0 | 140,0 | 13,0 | 13,0 | 15,0 | 7,5 | 0 | 3495,25 | 1525,43 | 1539,45 | 208736,7 | 6384907,0 | 6384907,0 |

| Naam | Iyz [mm ⁴] | I1 [mm ⁴] | I2 [mm ⁴] | α [°] | Iω [mm ⁶] | W1,el,t [mm ³] | W1,el,b [mm ³] | W2,el,t [mm ³] | W2,el,b [mm ³] | W1,pl [mm ³] | W2,pl [mm ³] | iy [mm] | iz [mm] | Hy [mm] | Hx [mm] |
|----------------|---------------------------|--------------------------|--------------------------|----------|--------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-----------------------------|-----------------------------|------------|------------|------------|------------|
| 1 U 200 | 0 | 1,9E+07 | 1477534,0 | 0 | 8,9E+09 | 191091,8 | 191091,8 | 26935,4 | 73344,2 | 227755,3 | 51850,6 | 77,1 | 21,4 | 75,0 | 200,0 |
| 2 L 150X150X14 | -4971153,0 | 1,3E+07 | 3482178,0 | 45,00 | 4,2E+08 | 126567,2 | 126567,2 | 65498,4 | 58536,3 | 200109,5 | 102485,0 | 45,8 | 45,8 | 150,0 | 150,0 |
| 3 HE 140 A | 0 | 1E+07 | 3893251,0 | 0 | 1,5E+10 | 155382,8 | 155382,8 | 55617,9 | 55617,9 | 173525,9 | 84852,6 | 57,3 | 35,2 | 140,0 | 133,0 |
| 4 L 140X140X13 | -3754641,0 | 1E+07 | 2630265,0 | 45,00 | 2,7E+08 | 102424,9 | 102424,9 | 53024,7 | 47412,5 | 161917,9 | 82940,4 | 42,7 | 42,7 | 140,0 | 140,0 |

| Naam | yG [mm] | zG [mm] | ys [mm] | zs [mm] | S.p. |
|----------------|------------|------------|------------|------------|------|
| 1 U 200 | 20,1 | 100,0 | -38,7 | 0 | 8 |
| 2 L 150X150X14 | 42,1 | 42,1 | -33,9 | -33,9 | 4 |
| 3 HE 140 A | 70,0 | 66,5 | 0 | 0 | 9 |
| 4 L 140X140X13 | 39,2 | 39,2 | -31,7 | -31,7 | 4 |

Naam: Doorsnede naam; **Productieproces:** Vorm; **Profiel:** h: Doorsnede hoogte; **b:** Doorsnede breedte; **tw:** Lijfdikte; **tf:** Flensdikte; **r1, r2, r3:** Afrondingswaarden; **Ax:** Doorsnede-oppervlak; **Ay, Az:** Afschuivingsoppervlak; **Ix:** Torsieaagheidsmoment; **Iy, Iz:** Buigtraagheidsmoment; **Iyz:** Centrifugaal traagheidsmoment; **I1, I2:** Hoofdbuigtraagheidsmoment; **α:** Hoofdrichtingen; **Iω:** Krommingsconstante; **W1,el,t, W2,el,t, W1,pl, W2,pl:** Traagheidsstraal; **W1,el,b, W2,el,b:** Plasticiteit modulus; **iy, iz:** Traagheidsstraal; **Hy:** Afmeting in lokale Y-richting; **Hx:** Afmeting in lokale Z-richting; **yG:** Y-coördinaat van het zwaartepunt; **zG:** Z-coördinaat van het zwaartepunt; **ys:** Y-coördinaat van het afschuivingsmiddelpunt (torsie); **zs:** Z-coördinaat van het afschuivingsmiddelpunt (torsie); **S.p.:** Spanningspunten;

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s_axs

Domeinen

| Element type | Materiaal | Ref _x | Ref _z | Dikte [mm] | k _{buiging} [I] | k _{torsie} [I] | k _{afschuiving} [I] | Oppervlakte [m ²] | Gat | Mesh |
|--------------|-----------|------------------|------------------|------------|--------------------------|-------------------------|------------------------------|-------------------------------|-----|------|
| 1 # Schaal | S 355 | Auto | Auto | 12 | | | | 0,020 | - | ✓ |
| 2 # Schaal | S 355 | Auto | Auto | 12 | | | | 0,020 | - | ✓ |
| 3 # Schaal | S 355 | Auto | Auto | 13 | | | | 0,115 | - | ✓ |
| 4 # Schaal | S 355 | Auto | Auto | 20 | | | | 0,075 | - | ✓ |
| 5 # Schaal | S 355 | Auto | Auto | 13 | | | | 0,054 | - | ✓ |
| 6 # Schaal | S 355 | Auto | Auto | 20 | | | | 0,061 | - | ✓ |

Element type: Plaatlement type; **Ref_x:** Referentie voor lokale X-richting; **Ref_z:** Referentie voor lokale Z-richting; **k_{buiging}:** Buigsterkte coefficient; **k_{torsie}:** Torsiesterkte coefficient; **k_{afschuiving}:** Dwarskrachtsterkte coefficient; **Oppervlakte:** Domein oppervlak; **Gat:** Aantal gaten in domein; **Mesh:** Gegeneerde mesh;

Knooppopleggingen

| Knoop | X [m] | Y [m] | Z [m] |
|-------|-------|-------|-------|
| 1 | 32 | 1,600 | 0,030 |
| 2 | 45 | 0 | 1,285 |
| 3 | 10 | 0 | 0,085 |

| Knoop | Type | Naam _x | K _x [kN/m] | K _{x,y} [kN/m] | Naam _y | K _y [kN/m] | K _{y,v} [kN/m] | Naam _z | K _z [kN/m] | K _{z,v} [kN/m] | Naam _{xx} | K _{xx} [kNm/rad] | K _{xxv} [kNm/rad] | Naam _{yy} |
|-------|------|-------------------|-----------------------|-------------------------|-------------------|-----------------------|-------------------------|-------------------|-----------------------|-------------------------|--------------------|---------------------------|----------------------------|--------------------|
| 1 | 32 | Glob. | — | — | Vast - translatie | 1E+10 | 1E+10 | Vast - translatie | 1E+10 | 1E+10 | Vast - rotatie | 1E+10 | 1E+10 | — |
| 2 | 45 | Glob. | Vast - translatie | 1E+10 | Vast - translatie | 1E+10 | 1E+10 | Vast - translatie | 1E+10 | 1E+10 | — | — | — | Vast - rotatie |
| 3 | 10 | Glob. | Vast - translatie | 1E+10 | — | — | — | Vast - translatie | 1E+10 | 1E+10 | — | — | — | — |

| Knoop | K _{yy} [kNm/rad] | K _{yyv} [kNm/rad] | Naam _{zz} | K _{zz} [kNm/rad] | K _{z,v} [kNm/rad] |
|-------|---------------------------|----------------------------|--------------------|---------------------------|----------------------------|
| 1 | 32 | — | — | — | — |
| 2 | 45 | 1E+10 | 1E+10 | — | — |
| 3 | 10 | — | — | — | — |

Knoop: Ondersteunde knoop; **Type:** Opleggingstype; **Naam_x:** Naam van de veereigenschappen; **K_x:** Initiele stijfheid; **K_y:** Trillingsstijfheid; **Naam_y:** Naam van de veereigenschappen; **K_y:** Initiele stijfheid; **K_{y,v}:** Trillingsstijfheid; **Naam_z:** Naam van de veereigenschappen; **K_z:** Initiele stijfheid; **K_{z,v}:** Trillingsstijfheid; **Naam_{xx}:** Naam van de veereigenschappen; **K_{xx}:** Initiele stijfheid; **K_{xxv}:** Trillingsstijfheid; **Naam_{yy}:** Naam van de veereigenschappen; **K_{yy}:** Initiele stijfheid; **K_{yyv}:** Trillingsstijfheid; **Naam_{zz}:** Naam van de veereigenschappen; **K_{zz}:** Initiele stijfheid; **K_{zzv}:** Trillingsstijfheid;

Project:

Constructeur: DNV GL - Energy

Model: **Post aan onderrand HA_s.axes**

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Mx: Knoopbelastingen

| | <i>Richting</i> | <i>F_x</i> [kN] | <i>F_y</i> [kN] | <i>F_z</i> [kN] | <i>M_x</i> [kNm] | <i>M_y</i> [kNm] | <i>M_z</i> [kNm] |
|----|-----------------|------------------------------|------------------------------|------------------------------|-------------------------------|-------------------------------|-------------------------------|
| 28 | Global | 0 | 2,50 | 0 | 5,70 | 0 | 0 |

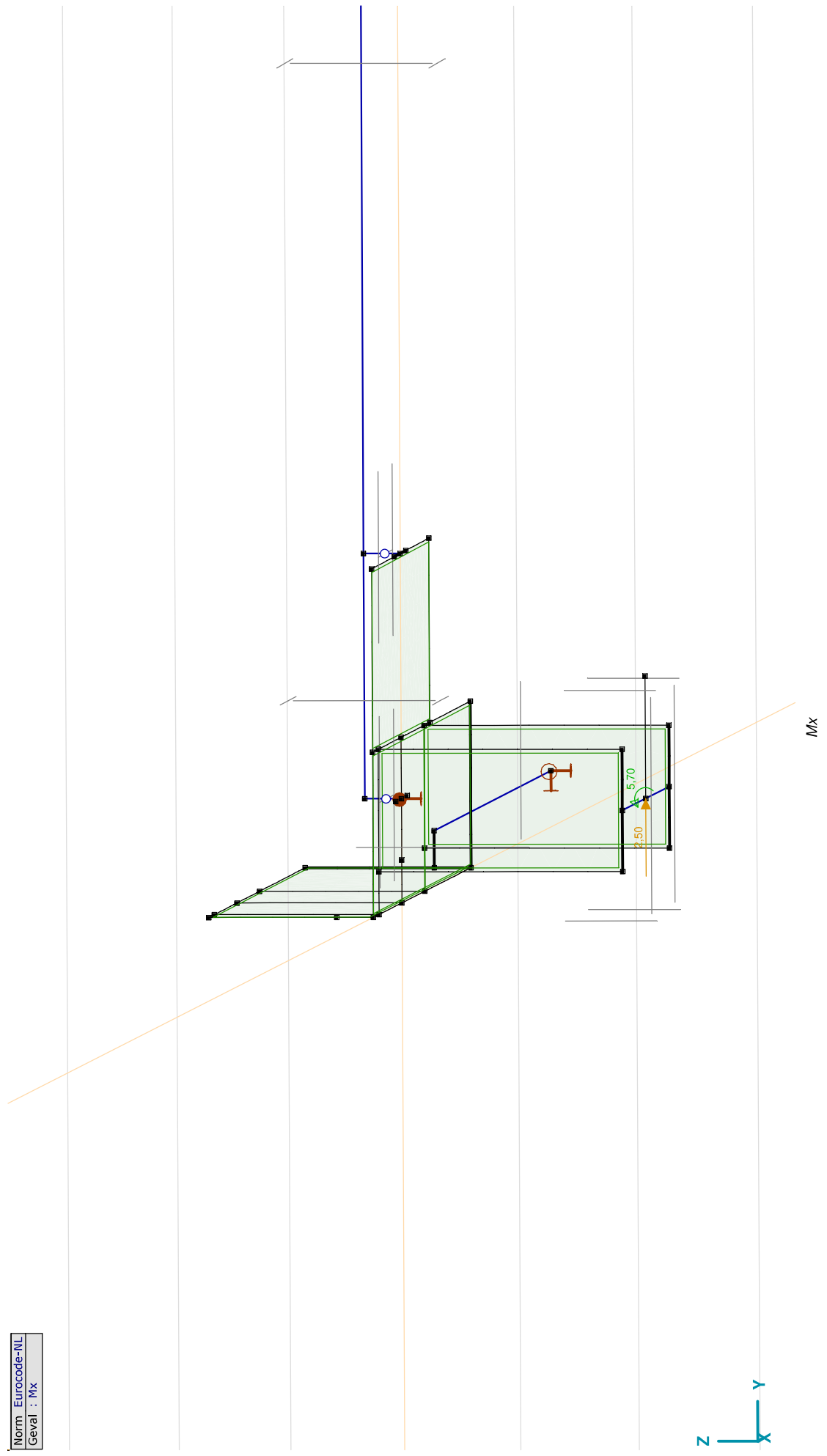
F_x, F_y, F_z: Belastingkracht component; **M_x**, **M_y**, **M_z**: Belastingmoment component;

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axs

| | |
|-------|-------------|
| Norm | Eurocode-NL |
| Geval | Mx |



Project:

Constructeur: DNV GL - Energy

Model: **Post aan onderrand HA_s.axes****My: Knoopbelastingen**

| | <i>Richting</i> | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|----|-----------------|---------------|---------------|---------------|----------------|----------------|----------------|
| 28 | Global | 4,40 | 0 | 0 | 0 | 13,90 | 0 |

Fx, Fy, Fz: Belastingkracht component; **Mx, My, Mz:** Belastingmoment component;

Project:

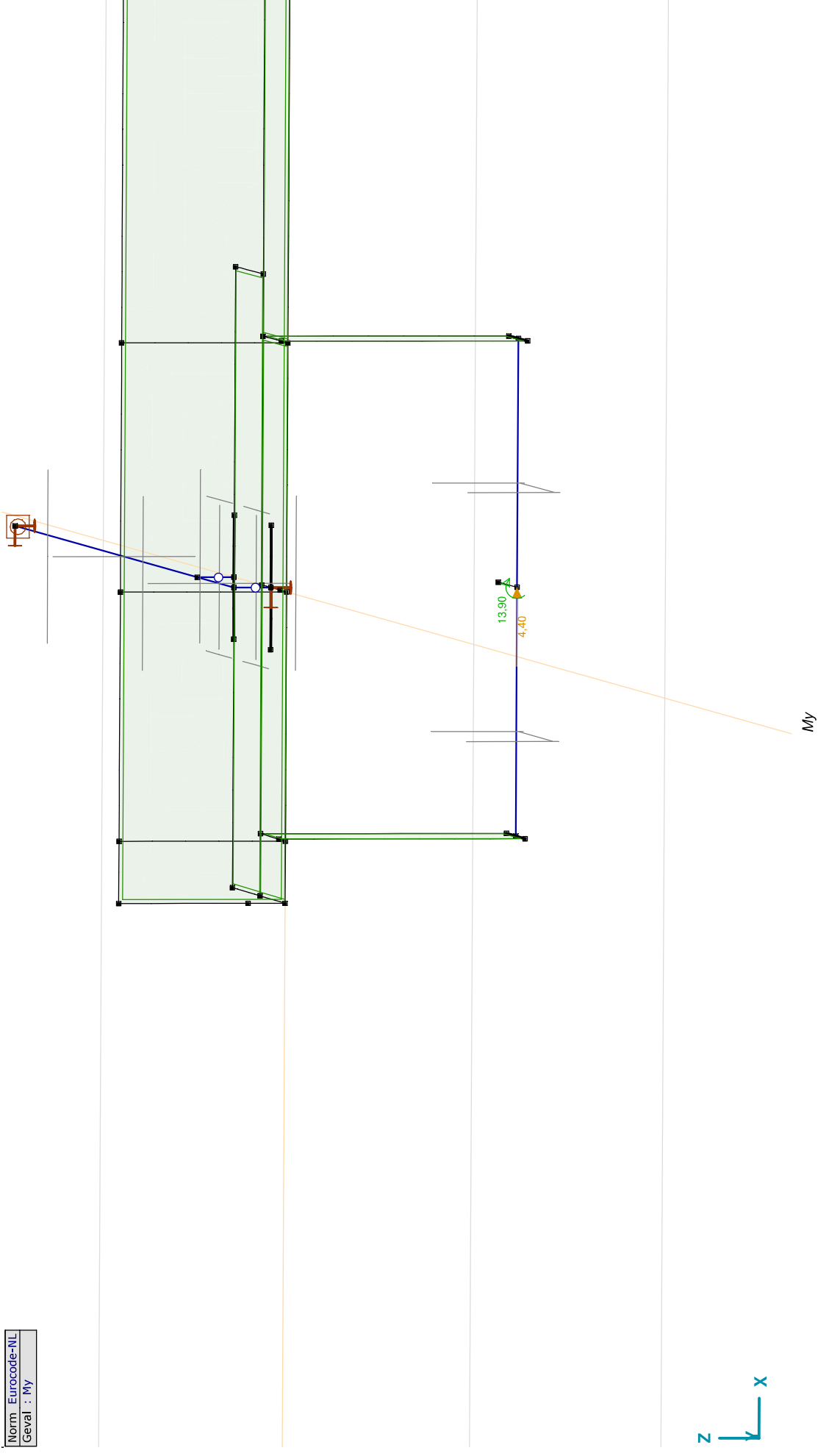
Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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Norm: Eurocode-NL
Geval: My



Project:

Constructeur: DNV GL - Energy

Model: **Post aan onderrand HA_s.axs****Fz: Knoopbelastingen**

| | <i>Richting</i> | <i>F_x</i> [kN] | <i>F_y</i> [kN] | <i>F_z</i> [kN] | <i>M_x</i> [kNm] | <i>M_y</i> [kNm] | <i>M_z</i> [kNm] |
|----|-----------------|------------------------------|------------------------------|------------------------------|-------------------------------|-------------------------------|-------------------------------|
| 28 | Global | 0 | 0 | -3,50 | 0 | 0 | 0 |

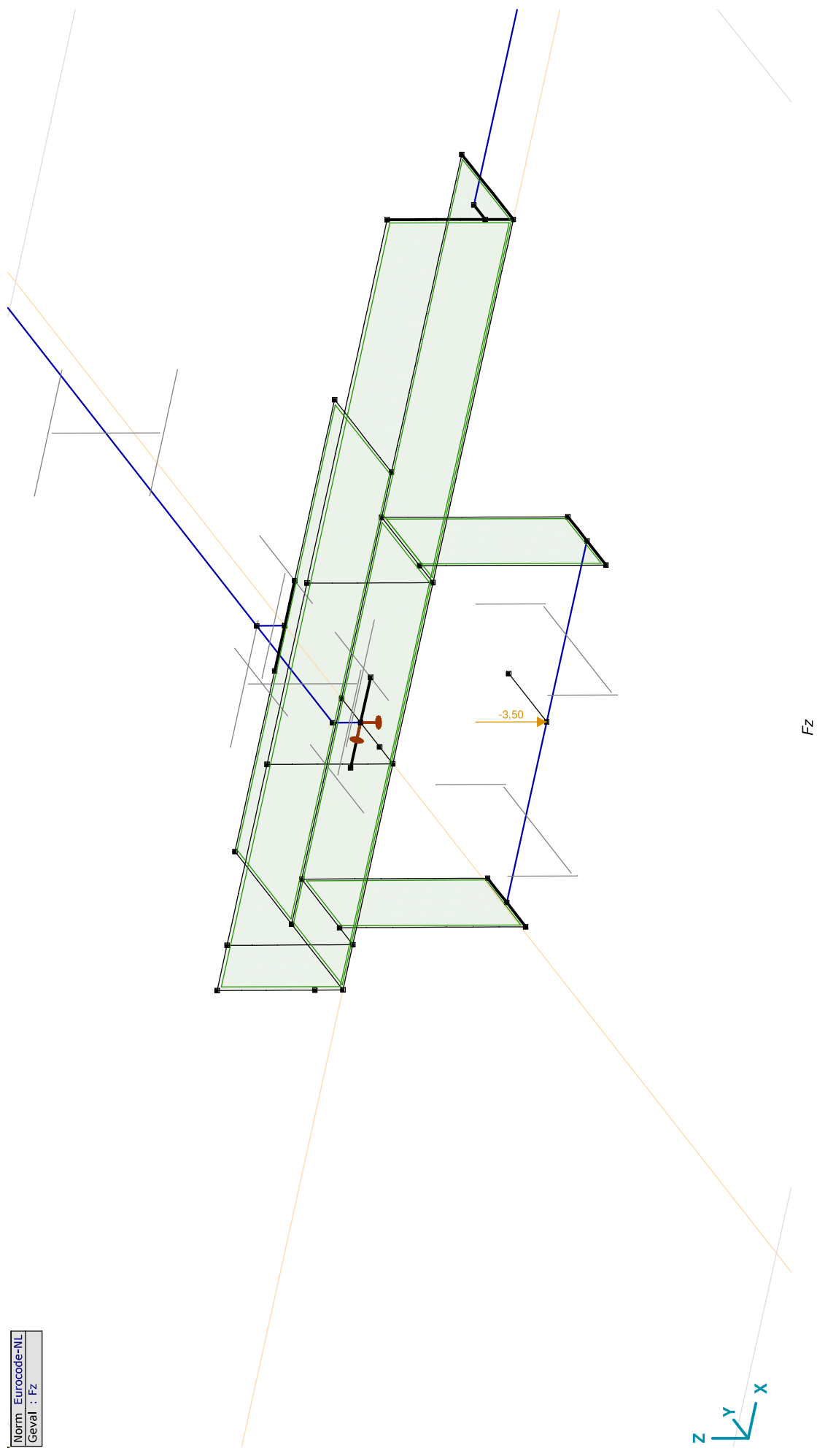
F_x, F_y, F_z: Belastingkracht component; **M_x, M_y, M_z:** Belastingmoment component;

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderwand HA_s.axes

| | |
|-------|-------------|
| Norm | Eurocode-NL |
| Geval | Fz |



Project:

Constructeur: DNV GL - Energy

Model: **Post aan onderrand HA_s.axes**

N: Knoopbelastingen

| | <i>Richting</i> | F_x [kN] | F_y [kN] | F_z [kN] | M_x [kNm] | M_y [kNm] | M_z [kNm] |
|----|-----------------|---------------|---------------|---------------|----------------|----------------|----------------|
| 32 | Globaal | -30,00 | 0 | 0 | 0 | 0 | 0 |

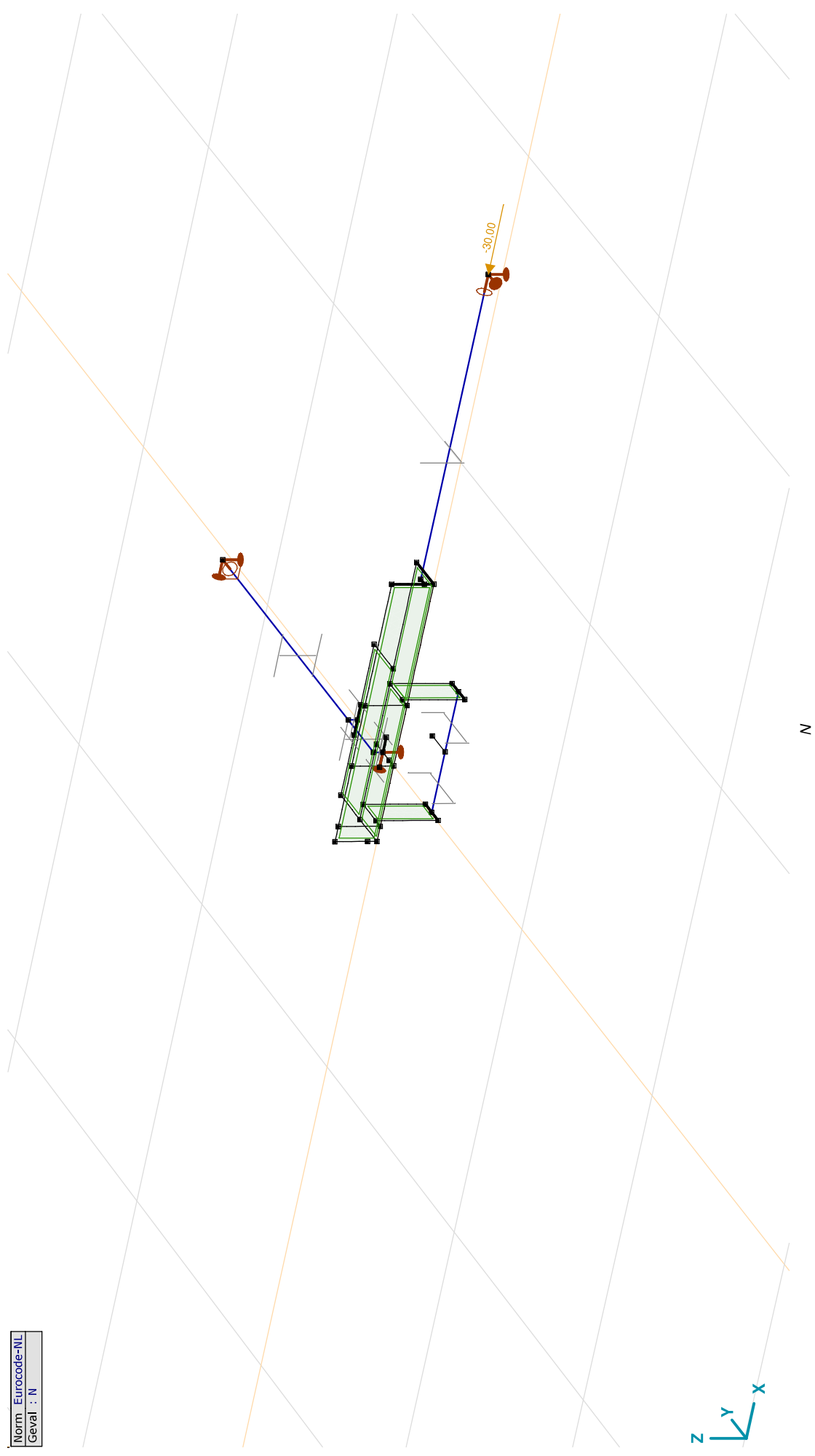
Fx, Fy, Fz: Belastingkracht component; **Mx, My, Mz**: Belastingmoment component;

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axs

| | |
|-------|-------------|
| Norm | Eurocode-NL |
| Geval | : N |



Project:

Constructeur: DNV GL - Energy

Model: **Post aan onderrand HA_s.axes**

Gebruiker gedefinieerde belastingcombinaties uit belastinggevallen

| | <i>Naam</i> | <i>Type</i> | <i>M_x</i> | <i>M_y</i> | <i>F_z</i> | <i>N</i> | <i>Commentaar</i> |
|---|-------------|-------------|----------------------|----------------------|----------------------|----------|-------------------|
| 1 | Co #1 | UGT | 1,00 | 0 | 1,00 | 1,00 | |
| 2 | Co #2 | UGT | 0 | 1,00 | 1,00 | 1,00 | |
| 3 | Co #3 | UGT | -1,00 | 0 | 1,00 | 1,00 | |
| 4 | Co #4 | UGT | 0 | -1,00 | 1,00 | 1,00 | |
| 5 | Co #5 | UGT | 0,71 | 0,71 | 1,00 | 1,00 | |
| 6 | Co #6 | UGT | -0,71 | -0,71 | 1,00 | 1,00 | |

Naam: Naam belastingcombinatie; **T**ype: Type belastingcombinatie; **M_x**, **M_y**, **F_z**, **N**: Factor;

Project:

Constructeur: DNV GL - Energy

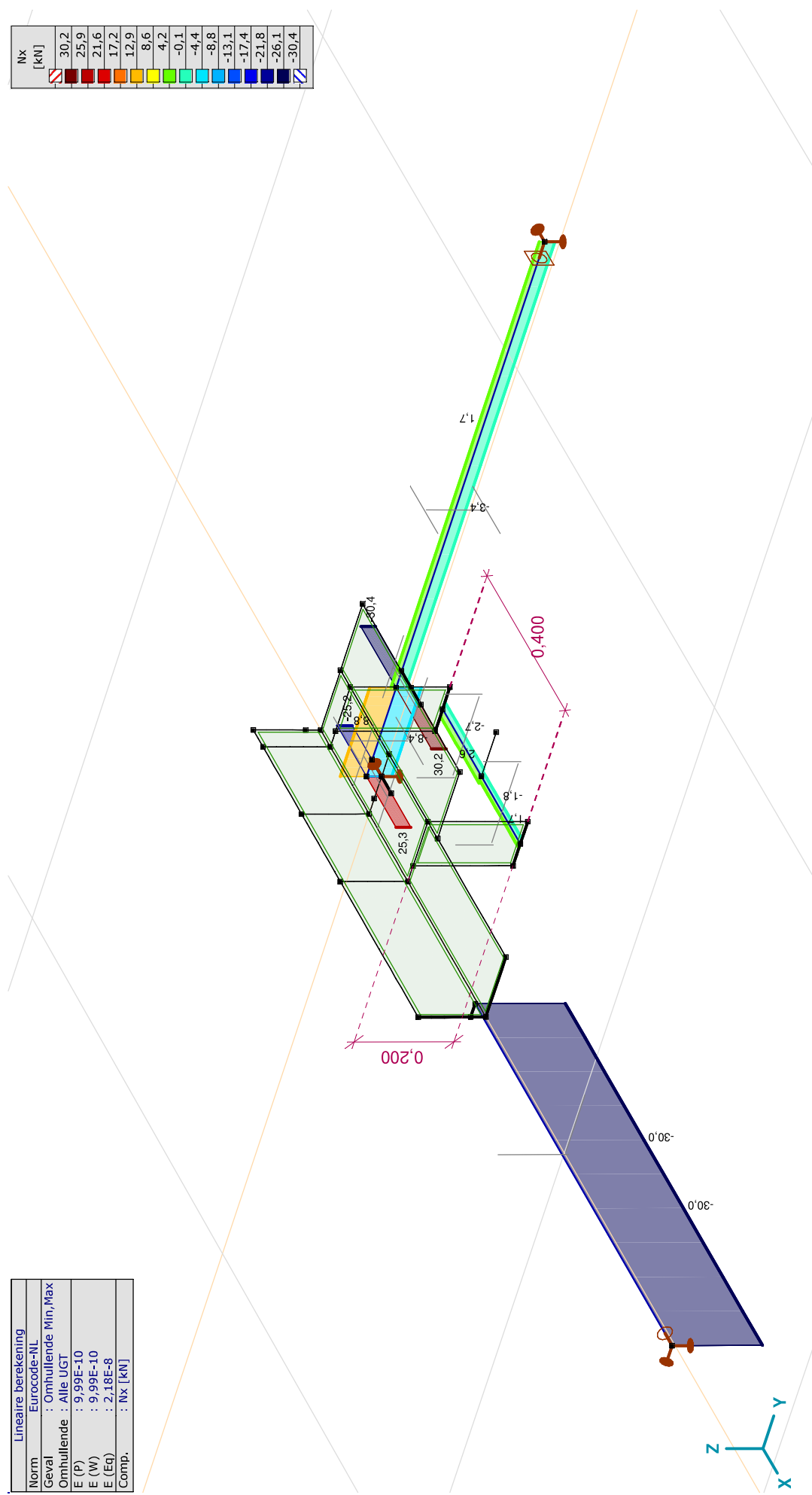
Model: Post aan onderrand HA_s.axes

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| | |
|---------------------|-----------------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : Nx [kN] |

| | Nx [kN] |
|--|---------|
| | 30,2 |
| | 25,9 |
| | 21,6 |
| | 17,2 |
| | 12,9 |
| | 8,6 |
| | 4,2 |
| | -0,1 |
| | -4,4 |
| | -8,8 |
| | -13,1 |
| | -17,4 |
| | -21,8 |
| | -26,1 |
| | -30,4 |



[[], Lineair, Omhullende (Alle UGT), Nx, Lijnen (gevuld)]

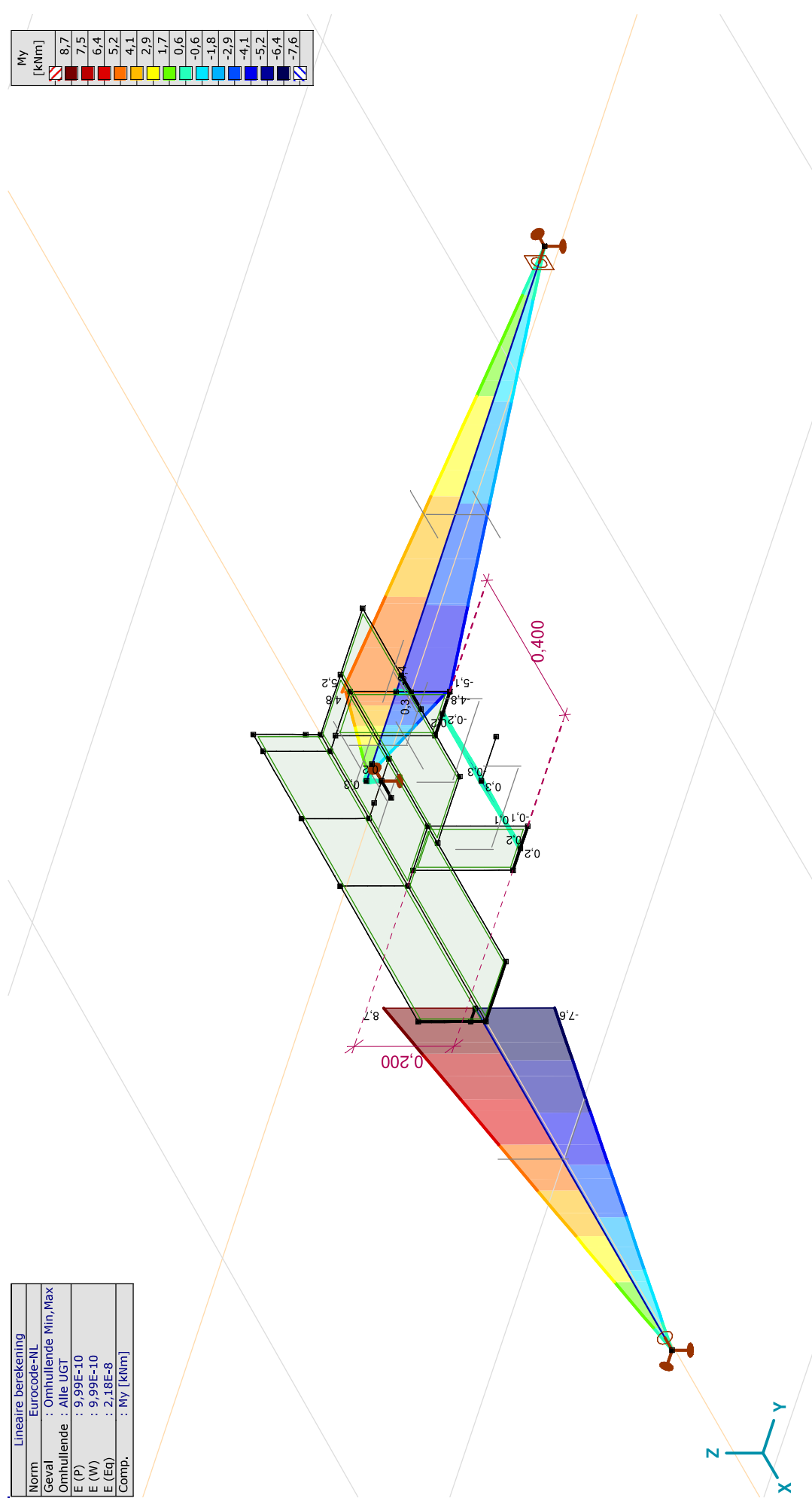
Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

| Lineaire berekening | |
|---------------------|----------------------|
| Norm | : Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : My [kNm] |

| My [kNm] |
|----------|
| 8.7 |
| 7.5 |
| 6.4 |
| 5.2 |
| 4.1 |
| 2.9 |
| 1.7 |
| 0.6 |
| -0.6 |
| -1.8 |
| -2.9 |
| -4.1 |
| -5.2 |
| -6.4 |
| -7.6 |



[I], Lineair, Omhullende (Alle UGT), My, Lijnen (gevuld)

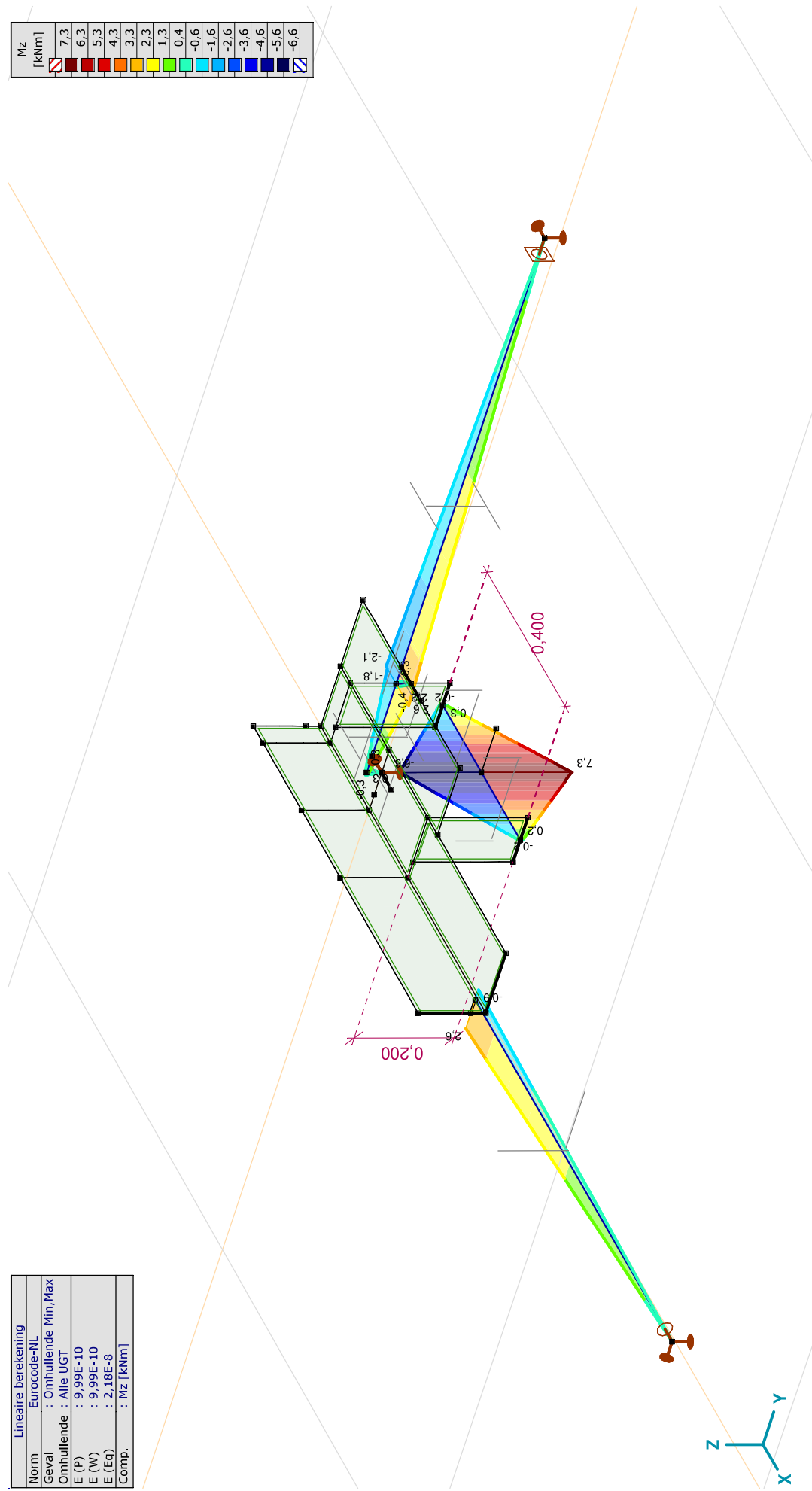
Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

| | |
|---------------------|----------------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : Mz [kNm] |

| | |
|----------|------|
| Mz [kNm] | 7.3 |
| | 6.3 |
| | 5.3 |
| | 4.3 |
| | 3.3 |
| | 2.3 |
| | 1.3 |
| | 0.4 |
| | -0.6 |
| | -1.6 |
| | -2.6 |
| | -3.6 |
| | -4.6 |
| | -5.6 |
| | -6.6 |



[[J], Lineair, Omhullende (Alle UGT), Mz, Lijnen (gevuld)]

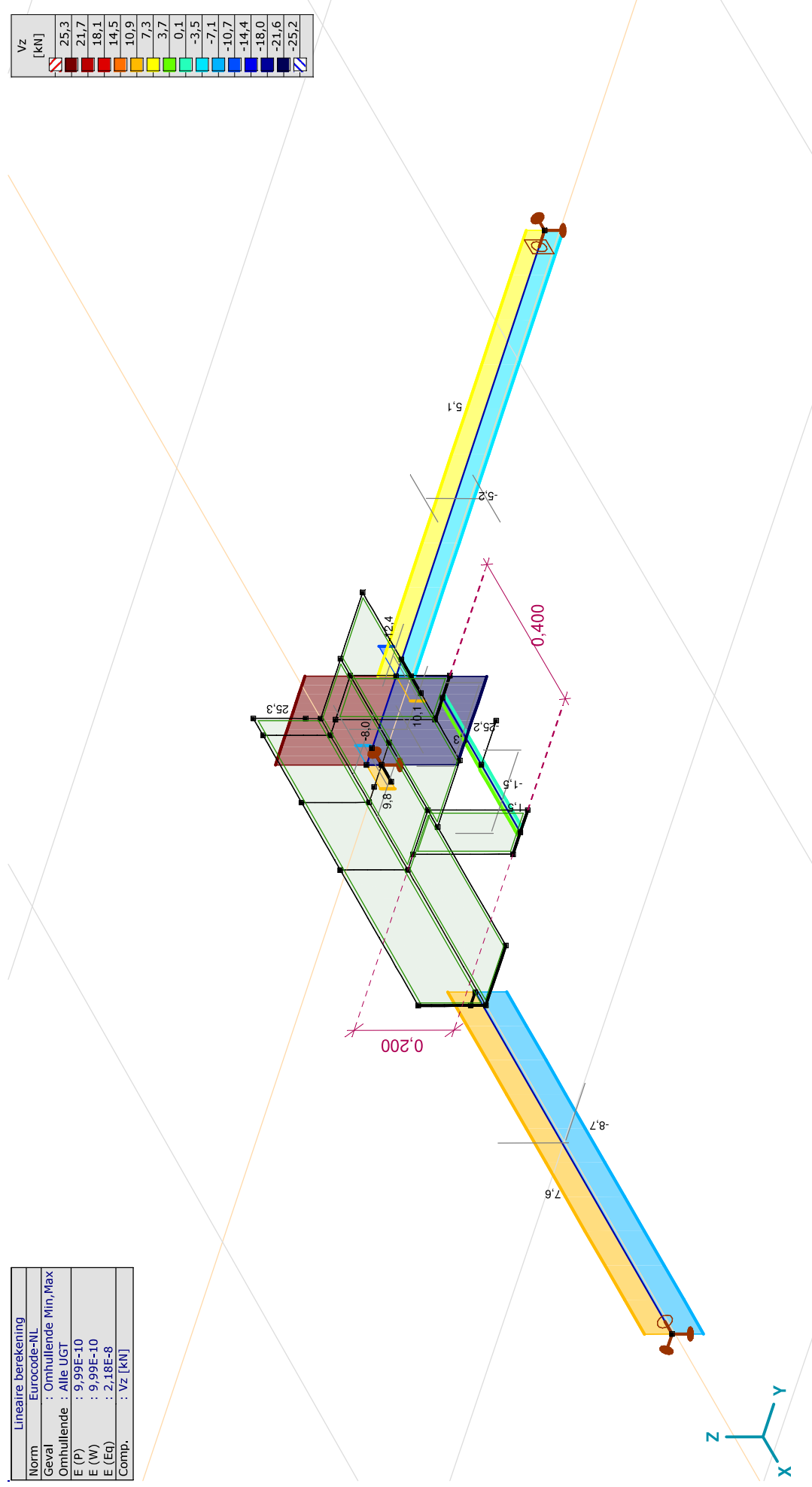
Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

| Lineaire berekening | |
|---------------------|----------------------|
| Norm | Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9,99E-10 |
| E (W) | : 9,99E-10 |
| E (Eq) | : 2,18E-8 |
| Comp. | : Vz [kN] |

| Vz [kN] |
|---------|
| 25,3 |
| 21,7 |
| 18,1 |
| 14,5 |
| 10,9 |
| 7,3 |
| 3,7 |
| 0,1 |
| -3,5 |
| -7,1 |
| -10,7 |
| -14,4 |
| -18,0 |
| -21,6 |
| -25,2 |



[I], Lineair, Omhullende (Alle UGT), Vz, Lijnen (gevuld)

Project:

Constructeur: DNV GL - Energy

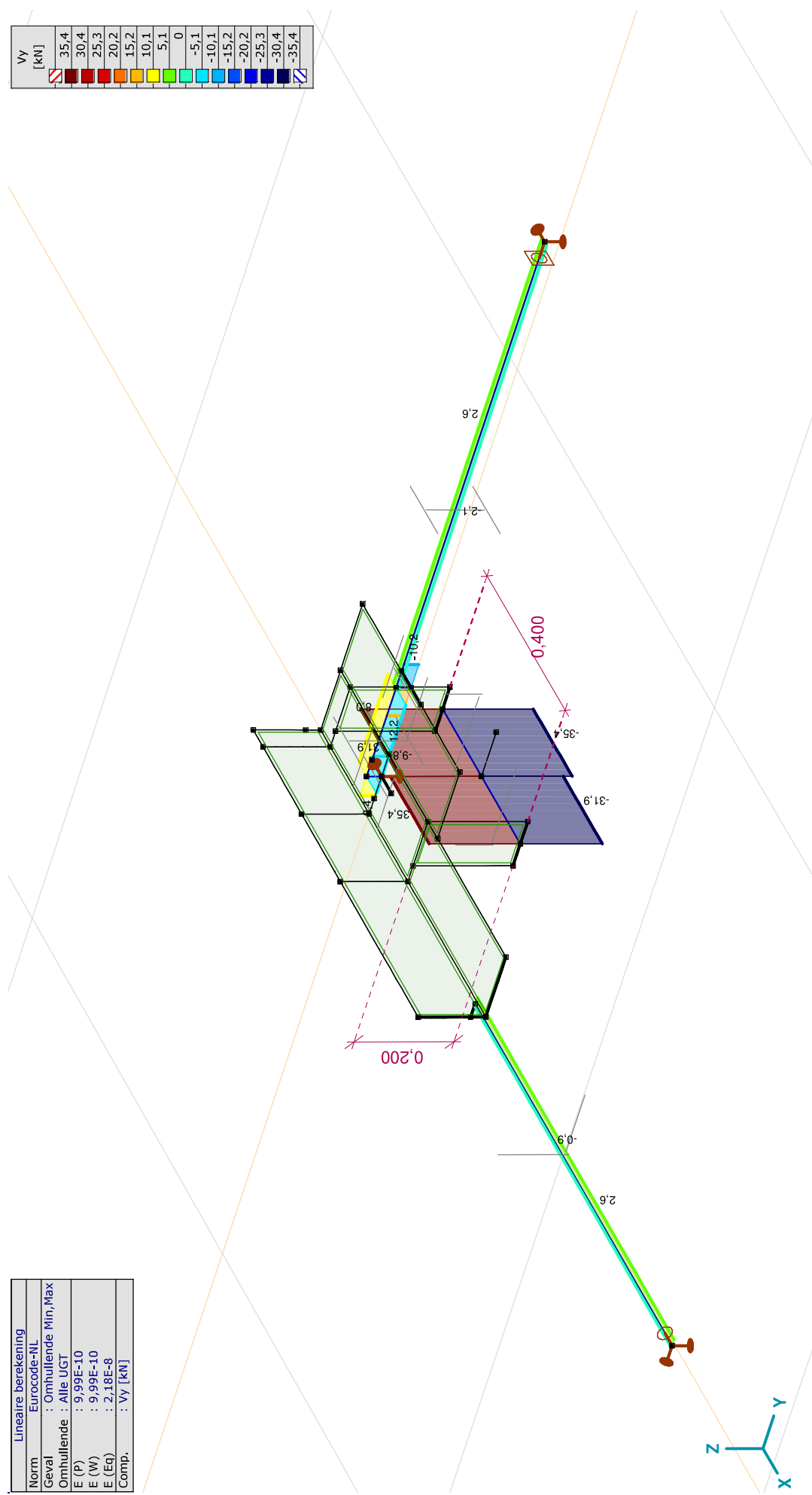
Model: Post aan onderrand HA_s.axes

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| | |
|---------------------|----------------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : Vy [kN] |

| | |
|---------|--|
| Vy [kN] | |
| 35,4 | |
| 30,4 | |
| 25,3 | |
| 20,2 | |
| 15,2 | |
| 10,1 | |
| 5,1 | |
| 0 | |
| -5,1 | |
| -10,1 | |
| -15,2 | |
| -20,2 | |
| -25,3 | |
| -30,4 | |
| -35,4 | |



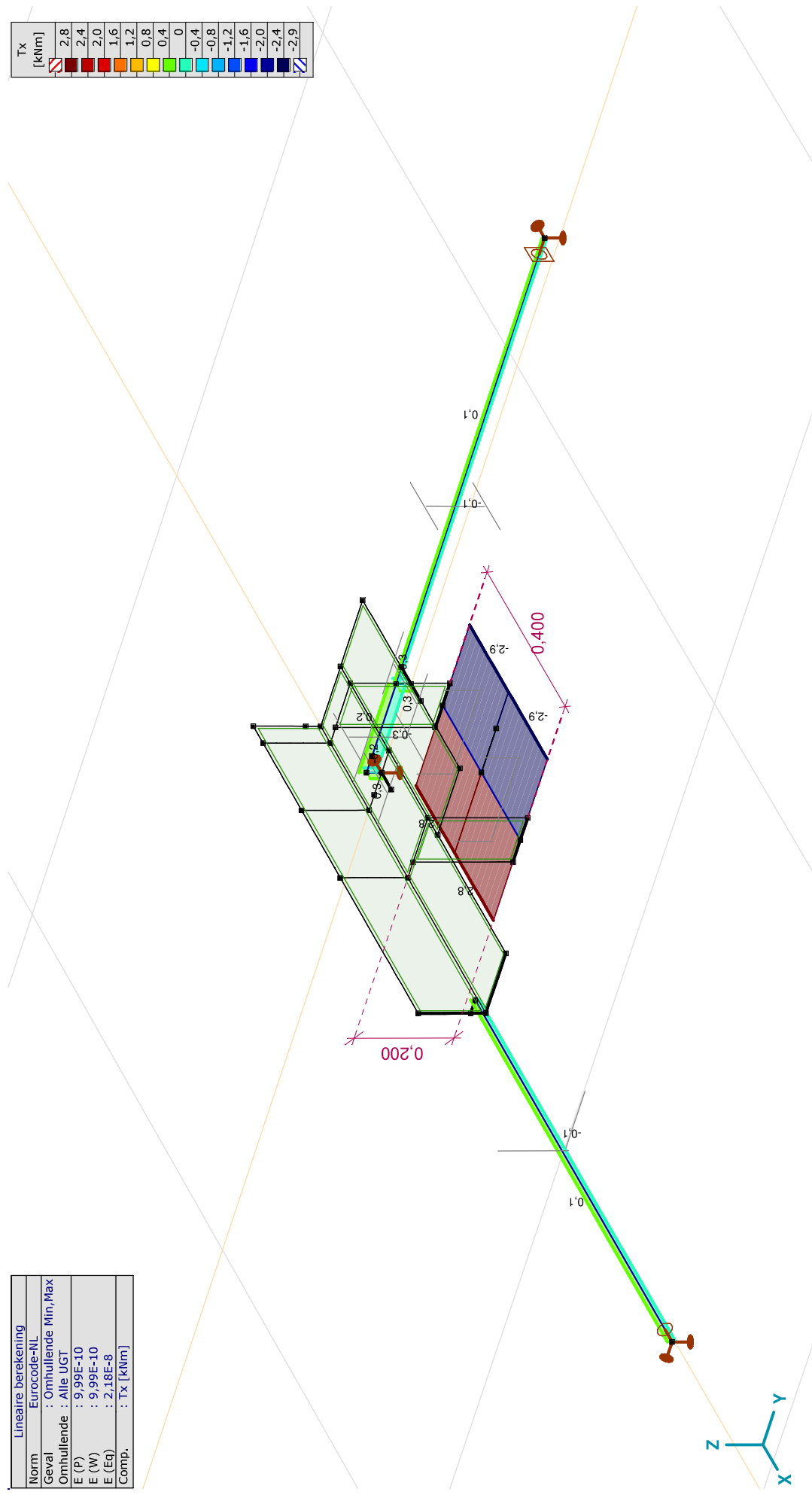
[I], Lineair, Omhullende (Alle UGT), Vy, Lijnen (gevuld)

Project:

Constructeur: DNV GL - Energy
 Model: Post aan onderrand HA_s.axes

| Lineaire berekening | |
|---------------------|----------------------|
| Norm | : Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : Tx [kNm] |

| Tx [kNm] |
|----------|
| 2.8 |
| 2.4 |
| 2.0 |
| 1.6 |
| 1.2 |
| 0.8 |
| 0.4 |
| 0 |
| -0.4 |
| -0.8 |
| -1.2 |
| -1.6 |
| -2.0 |
| -2.4 |
| -2.9 |



[I], Lineair, Omhullende (Alle UGT), Tx, Lijnen (gevuld)

Project:

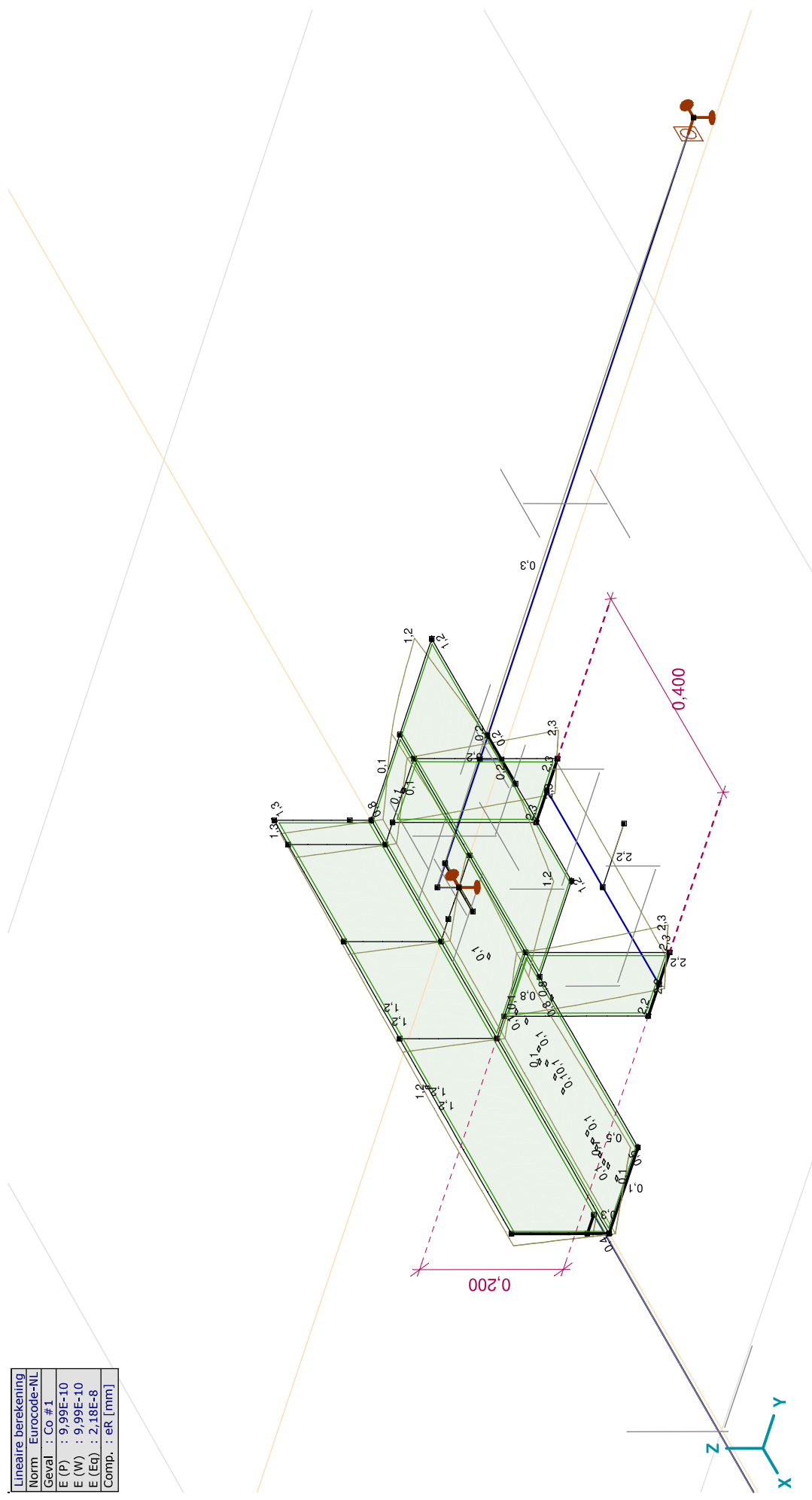
Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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| | |
|---------------------|-------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Co #1 |
| E (P) | : 9,99E-10 |
| E (W) | : 9,99E-10 |
| E (Eq) | : 2,18E-8 |
| Comp. | : eR [mm] |



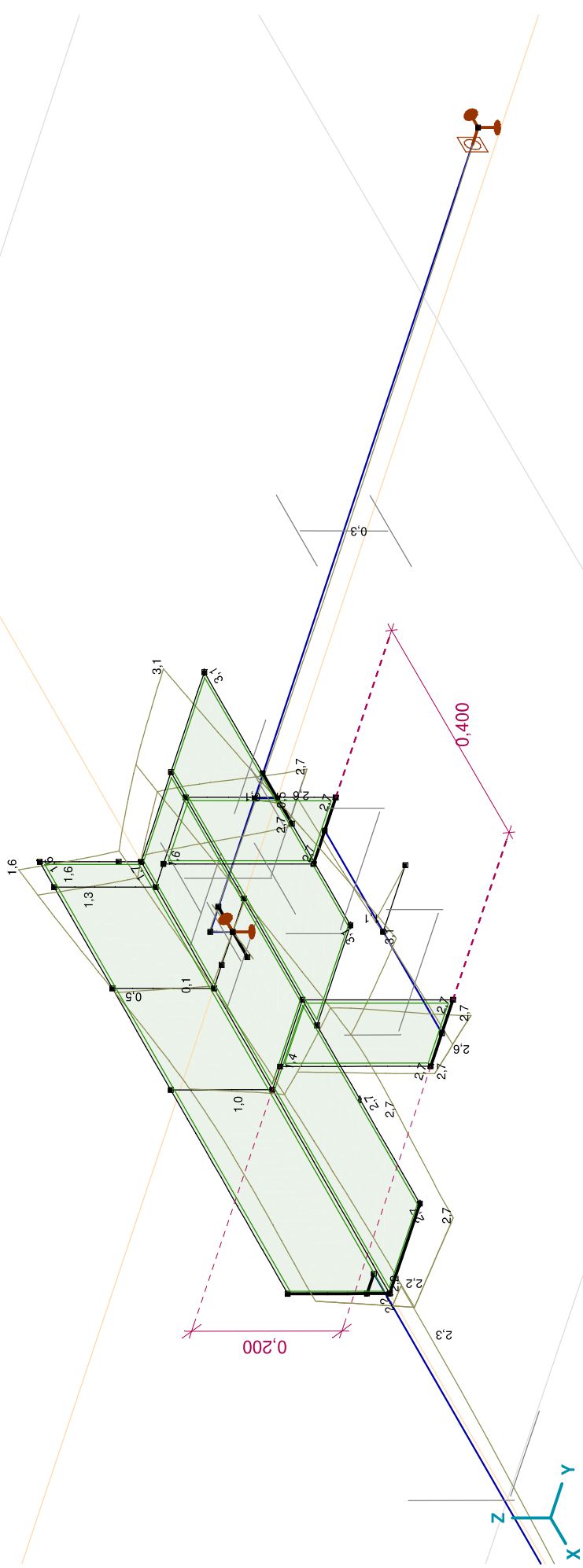
[1], Linear, Co #1 (UGT), eR, Lijnen

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

| |
|---------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #2 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : eR [mm] |



Project:

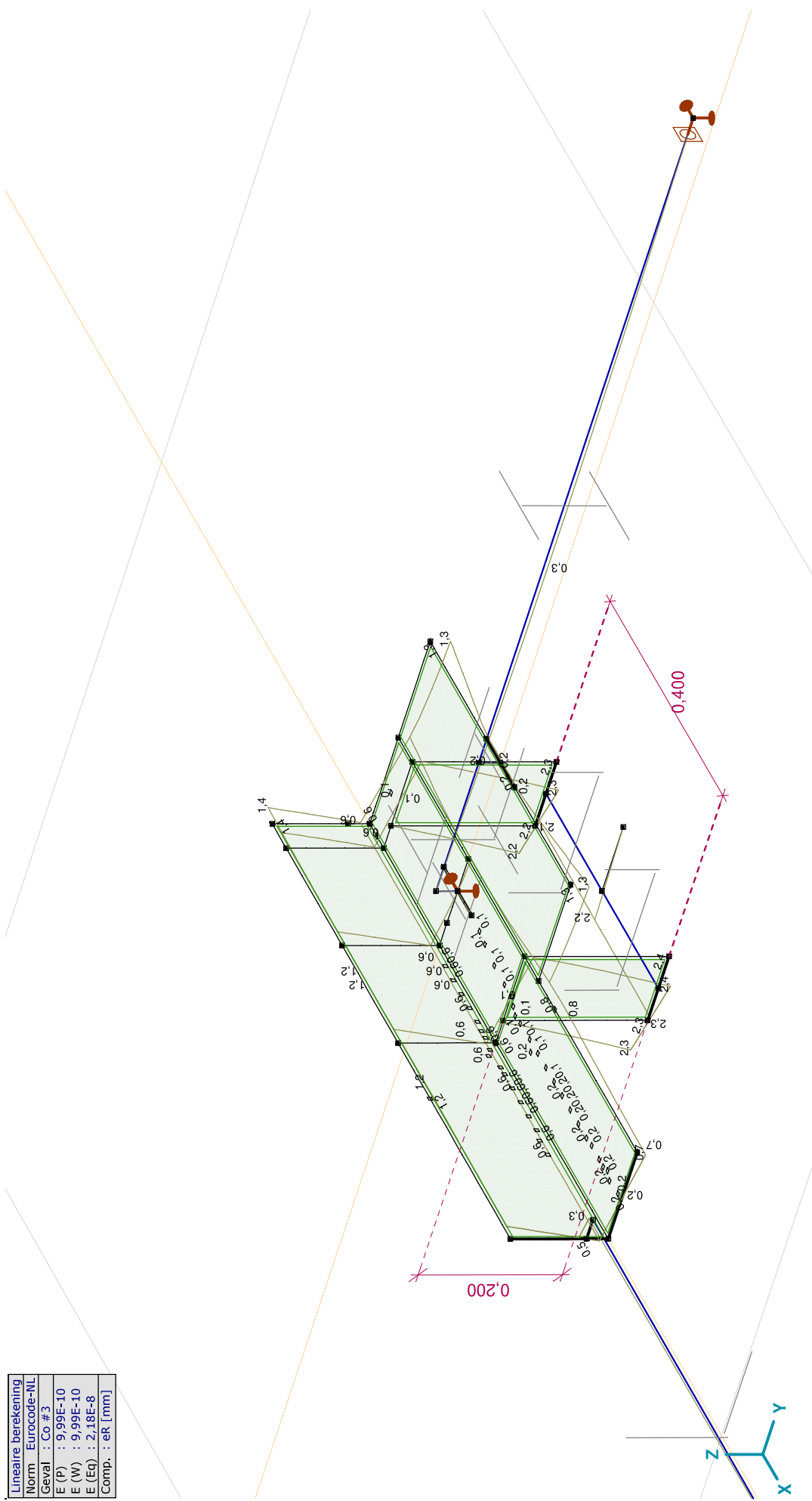
Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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| | |
|---------------------|-------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Co #3 |
| E (P) | : 9,99E-10 |
| E (W) | : 9,99E-10 |
| E (Eq) | : 2,18E-8 |
| Comp. | : eR [mm] |



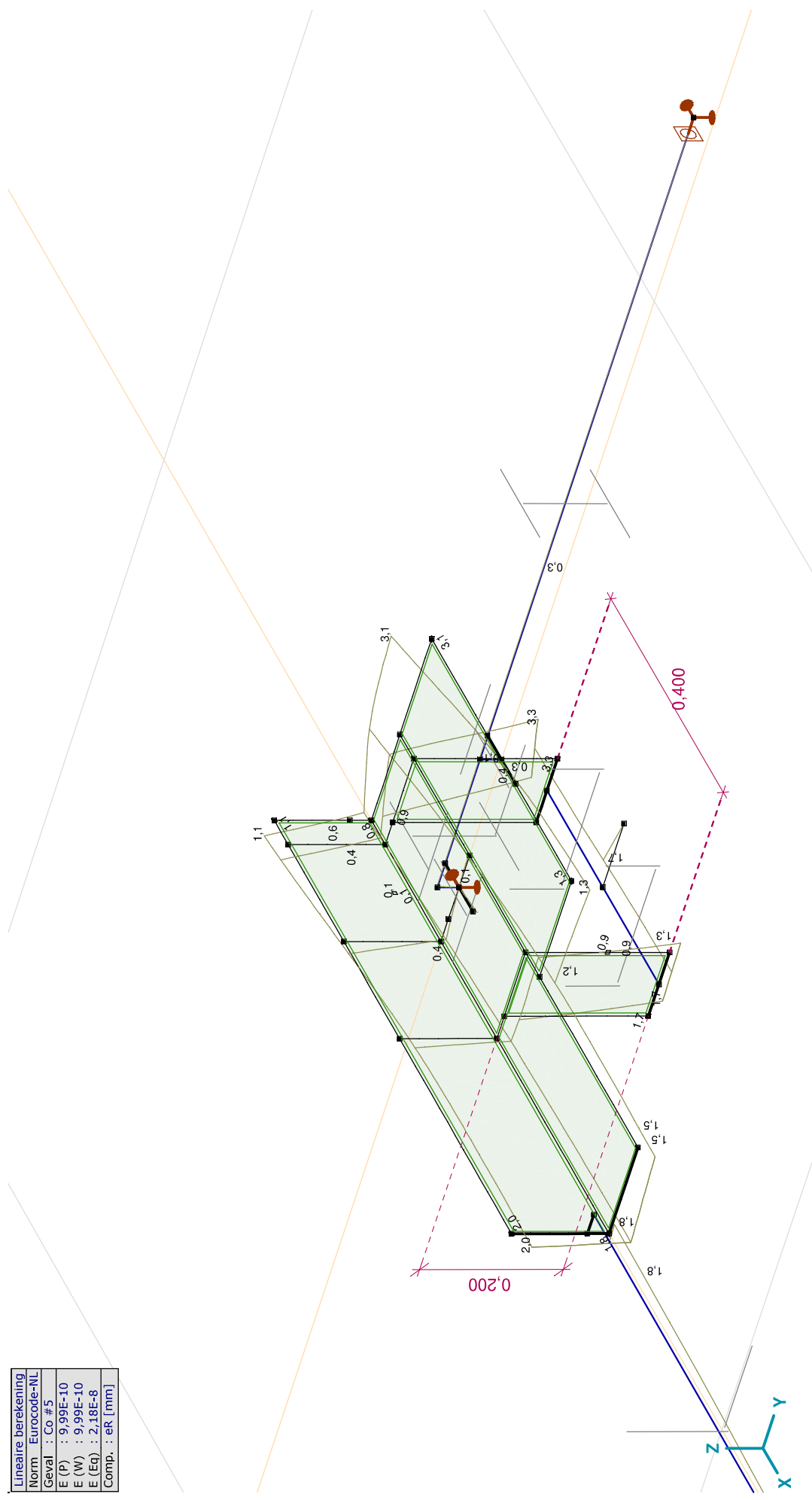
[1], Lineair, Co #3 (UGT), eR, Lijnen

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

| |
|---------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #5 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : eR [mm] |



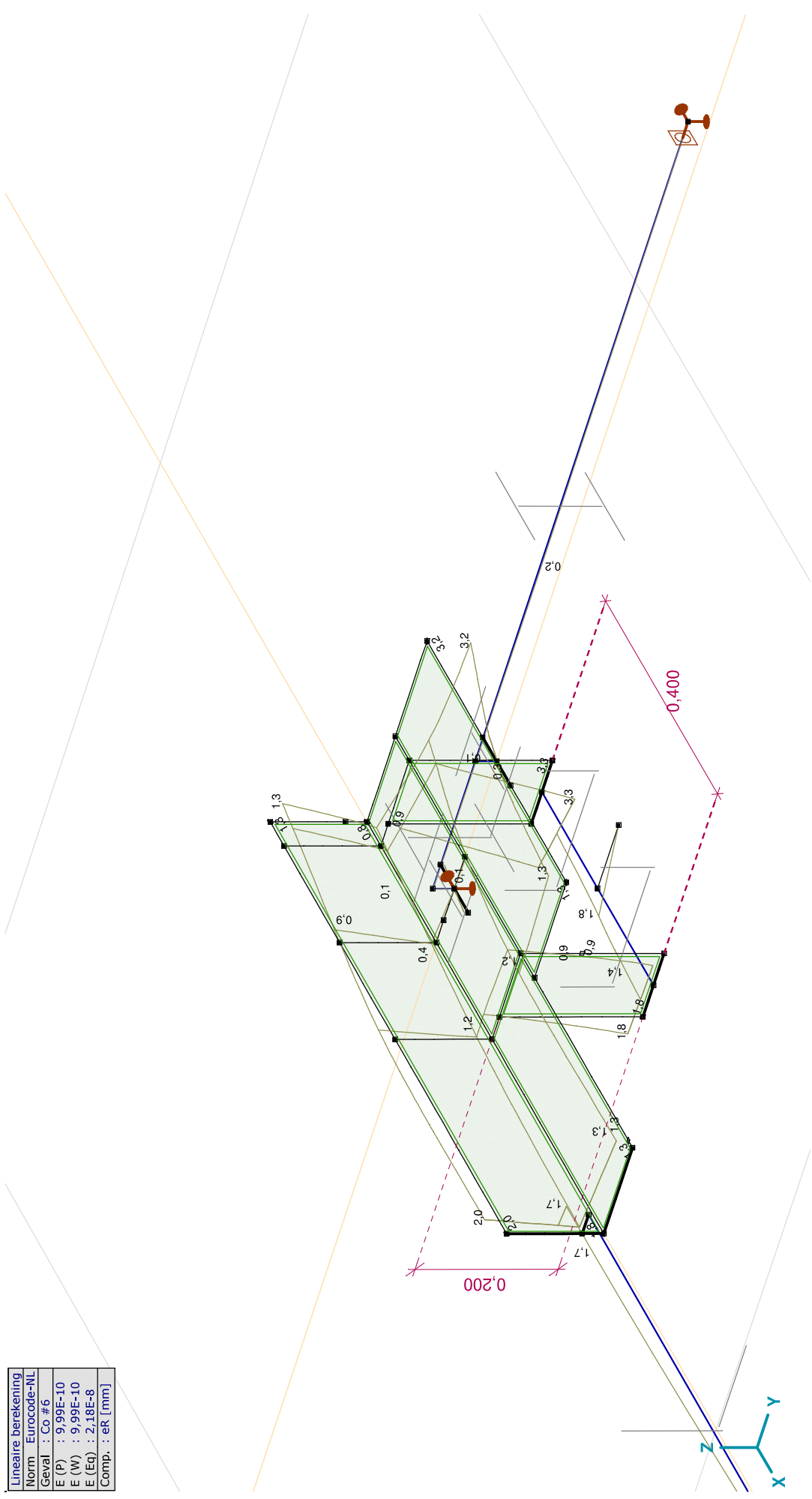
[1], Lineair, Co #5 (UGT), eR, Lijnen

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

| |
|---------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #6 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : eR [mm] |

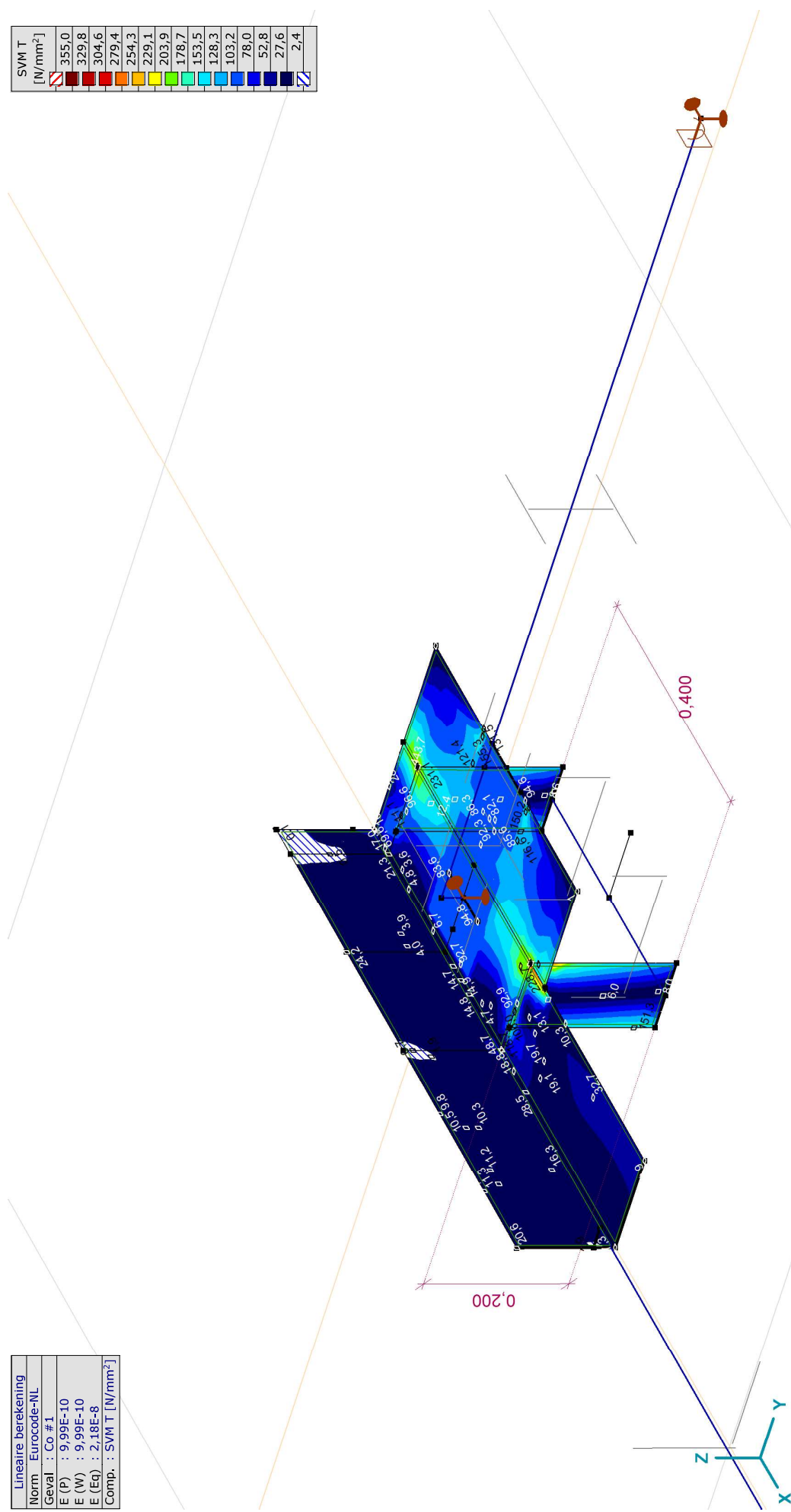


Project:

Constructeur: DNV GL - Energy
 Model: Post aan onderrand HA_s.axs

| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #1 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : SVM T [N/mm ²] |

| SVM T [N/mm ²] |
|----------------------------|
| 355,0 |
| 329,8 |
| 304,6 |
| 279,4 |
| 254,3 |
| 229,1 |
| 203,9 |
| 178,7 |
| 153,5 |
| 128,3 |
| 103,2 |
| 78,0 |
| 52,8 |
| 27,6 |
| 2,4 |



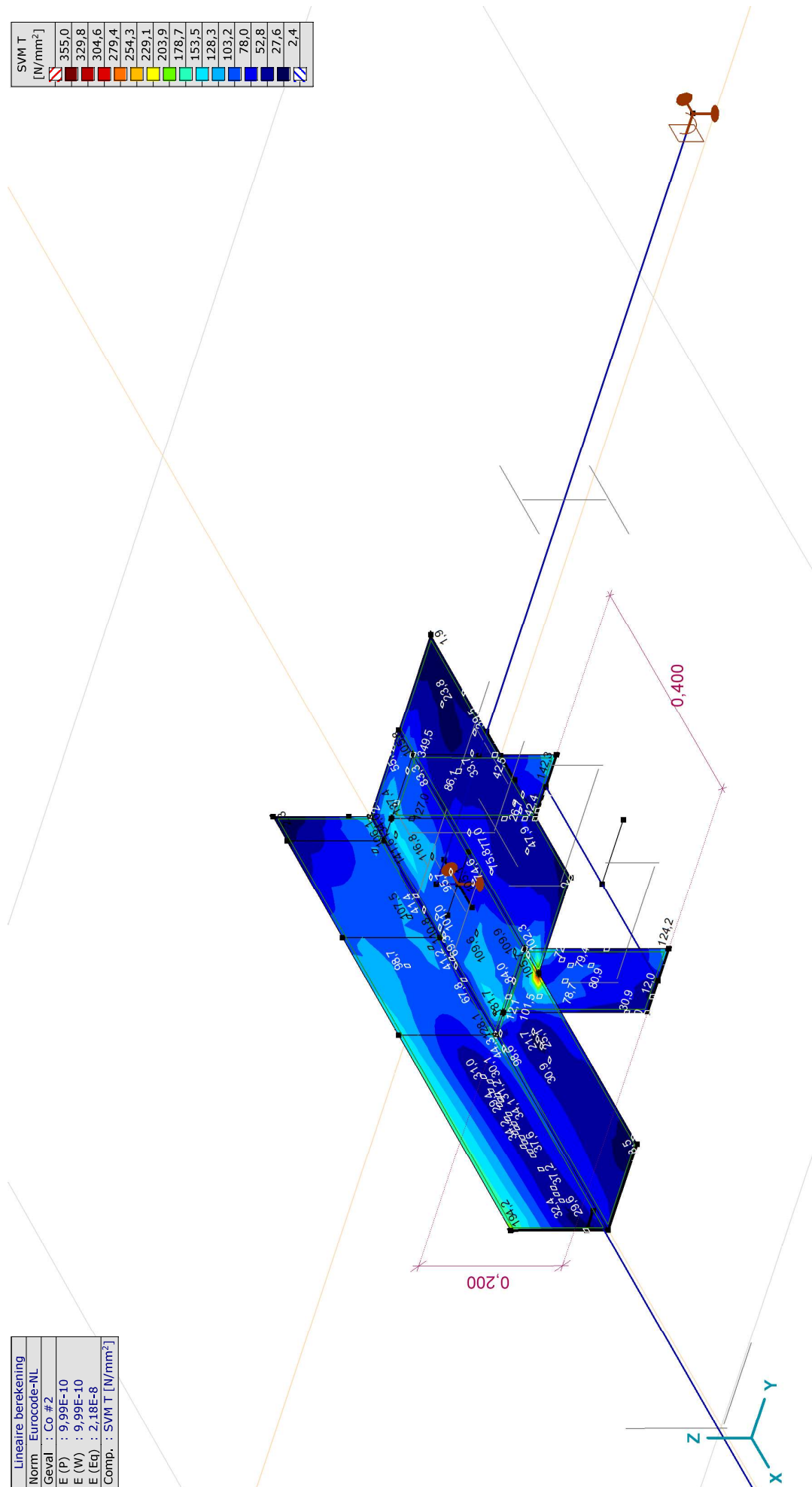
[J], Lineair, Co #1 (UGT), SVM T, Kleuren 2D

Project:

Constructeur: DNV GL - Energy
 Model: Post aan onderrand HA_s.axes

| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #2 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : SVM T [N/mm ²] |

| |
|----------------------------|
| SVM T [N/mm ²] |
| 355,0 |
| 329,8 |
| 304,6 |
| 279,4 |
| 254,3 |
| 229,1 |
| 203,9 |
| 178,7 |
| 153,5 |
| 128,3 |
| 103,2 |
| 78,0 |
| 52,8 |
| 27,6 |
| 2,4 |



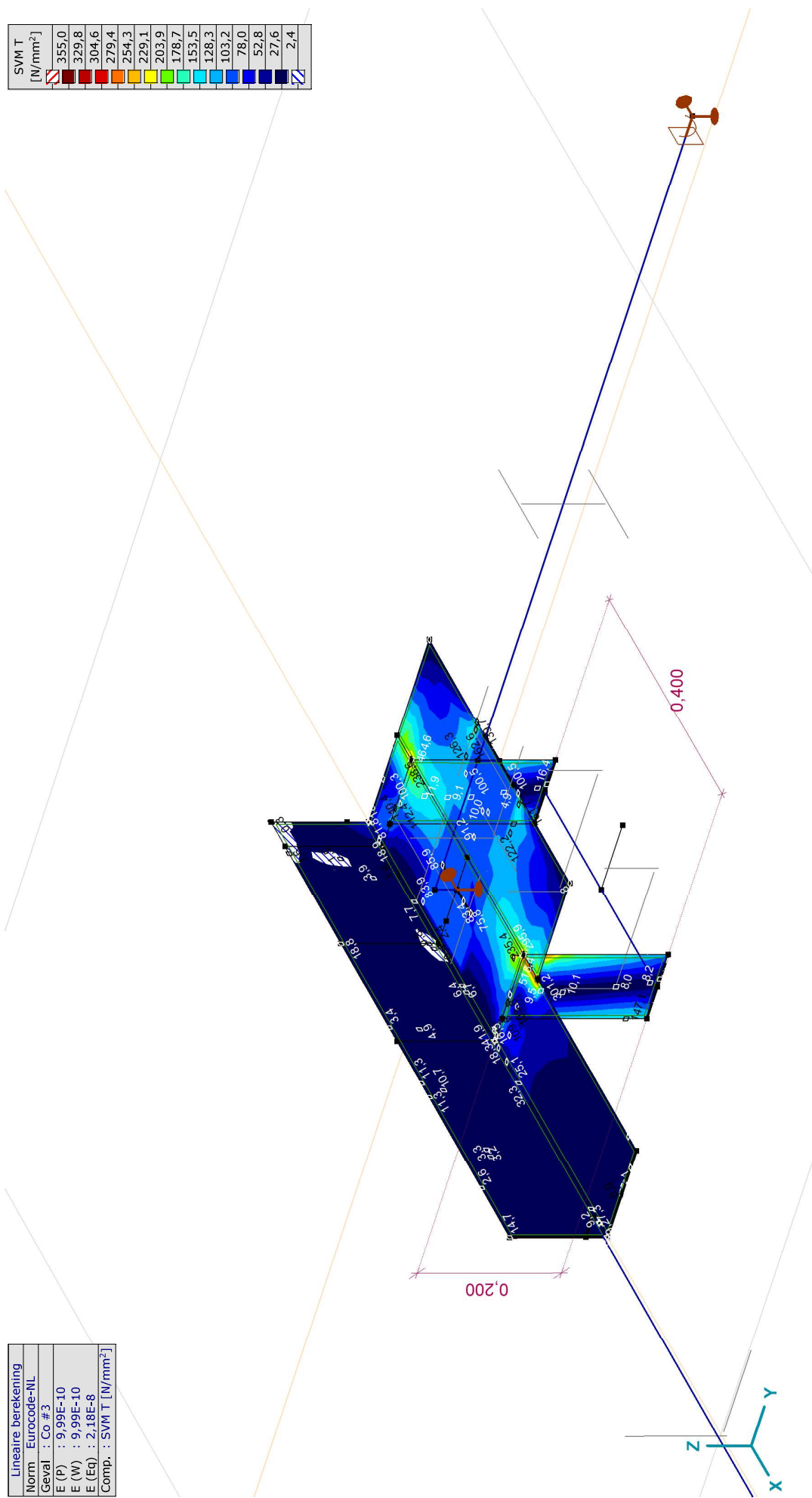
[[J], Lineair, Co #2 (UGT), SVM T, Kleuren 2D

Project:

Constructeur: DNV GL - Energy
 Model: Post aan onderrand HA_s.axes

| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #3 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : SVM T [N/mm ²] |

| SVM T [N/mm ²] |
|----------------------------|
| 355,0 |
| 329,8 |
| 304,6 |
| 279,4 |
| 254,3 |
| 229,1 |
| 203,9 |
| 178,7 |
| 153,5 |
| 128,3 |
| 103,2 |
| 78,0 |
| 52,8 |
| 27,6 |
| 2,4 |



[[J], Lineair, Co #3 (UGT), SVM T, Kleuren 2D

Project:

Constructeur: DNV GL - Energy

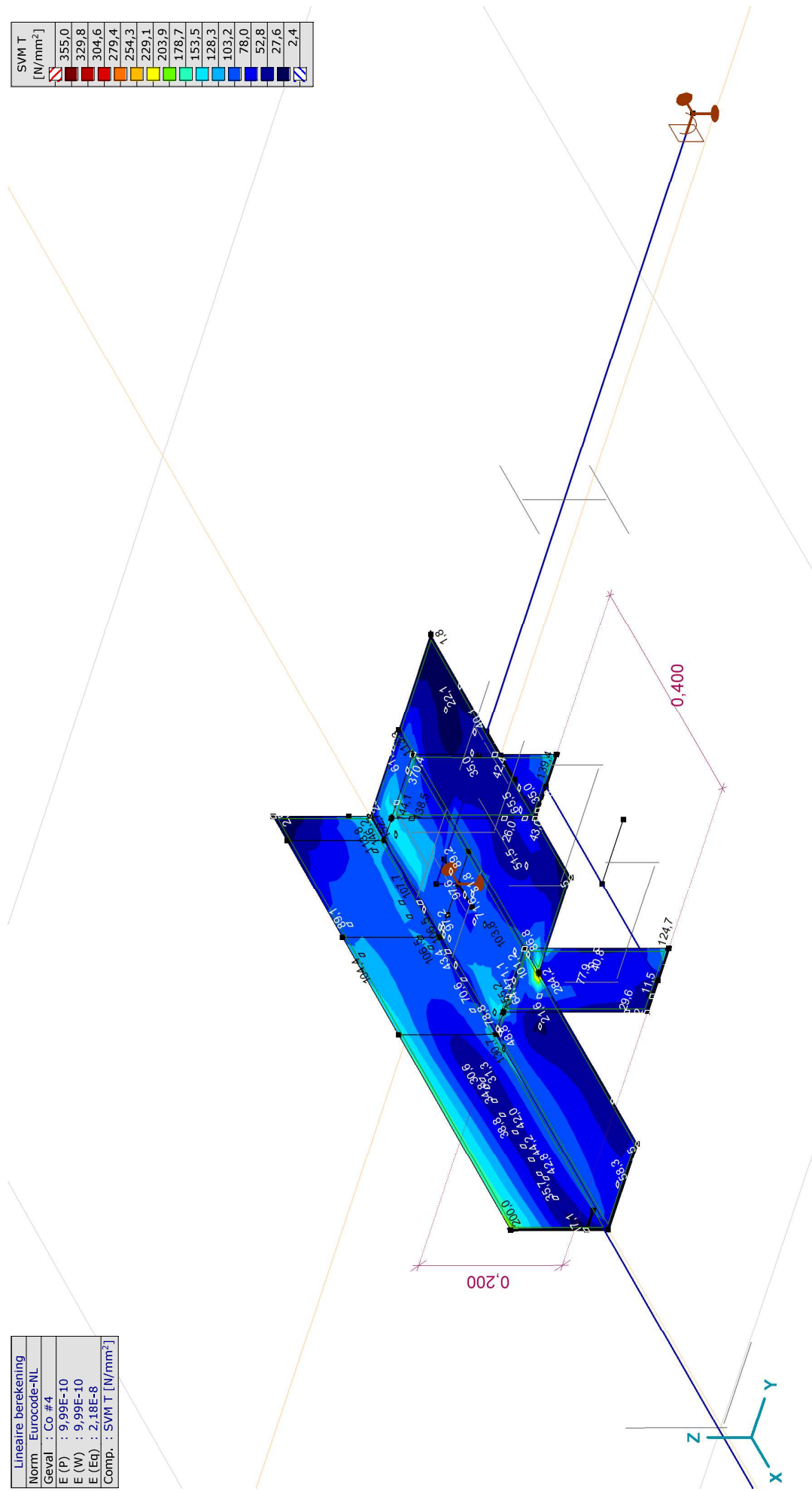
Model: Post aan onderrand HA_s.axs

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| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #4 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq.) : 2,18E-8 |
| Comp. : SVM T [N/mm ²] |

| SVM T [N/mm ²] |
|----------------------------|
| 355,0 |
| 329,8 |
| 304,6 |
| 279,4 |
| 254,3 |
| 229,1 |
| 203,9 |
| 178,7 |
| 153,5 |
| 128,3 |
| 103,2 |
| 78,0 |
| 52,8 |
| 27,6 |
| 2,4 |



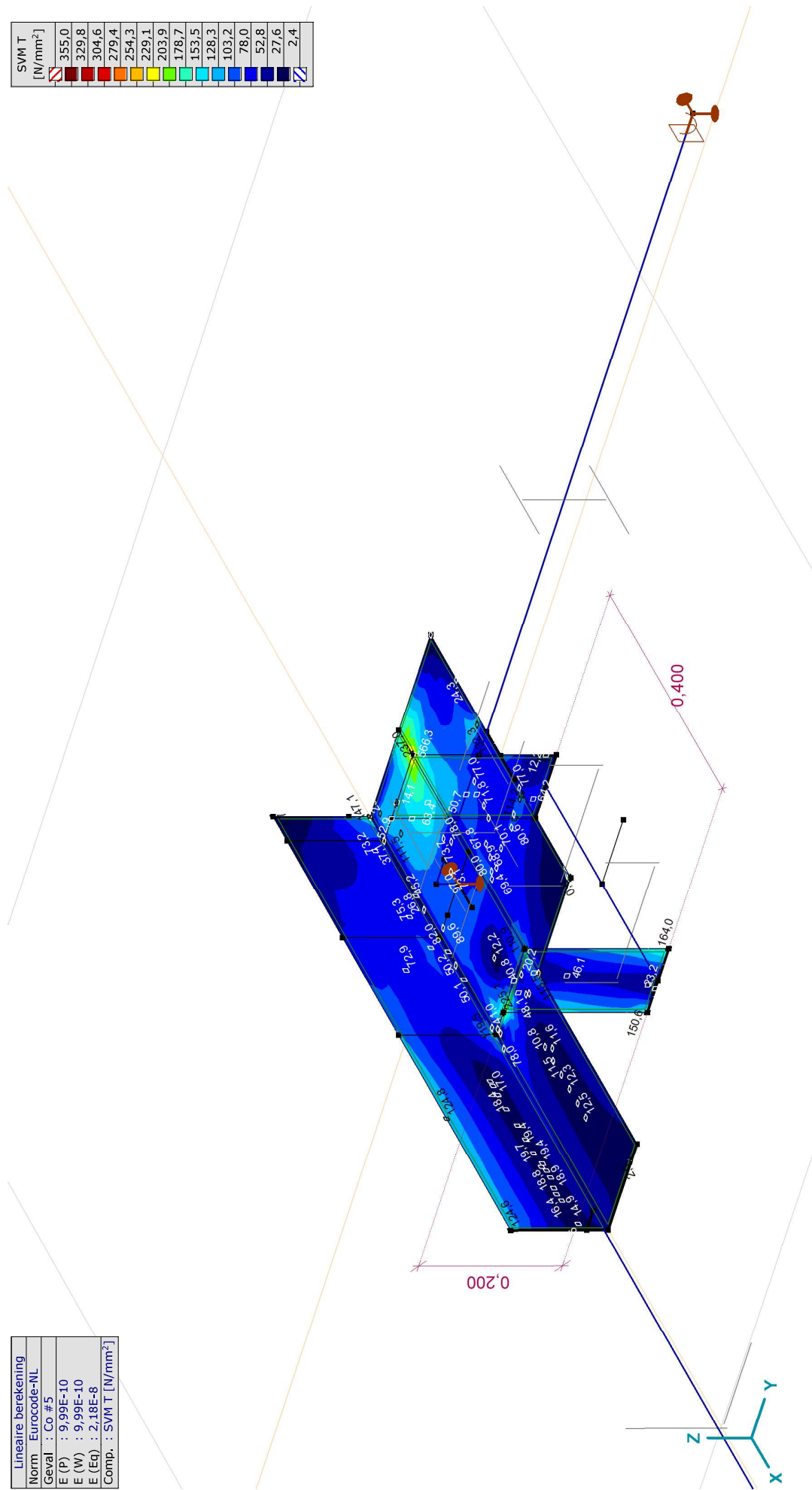
[J], Lineair, Co #4 (UGT), SVM T, Kleuren 2D

Project:

Constructeur: DNV GL - Energy
 Model: Post aan onderrand HA_s.axes

| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #5 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : SVM T [N/mm ²] |

| SVM T [N/mm ²] |
|----------------------------|
| 355,0 |
| 329,8 |
| 304,6 |
| 279,4 |
| 254,3 |
| 229,1 |
| 203,9 |
| 178,7 |
| 153,5 |
| 128,3 |
| 103,2 |
| 78,0 |
| 52,8 |
| 27,6 |
| 2,4 |



[J], Lineair, Co #5 (UGT), SVM T, Kleuren 2D

Project:

Constructeur: DNV GL - Energy

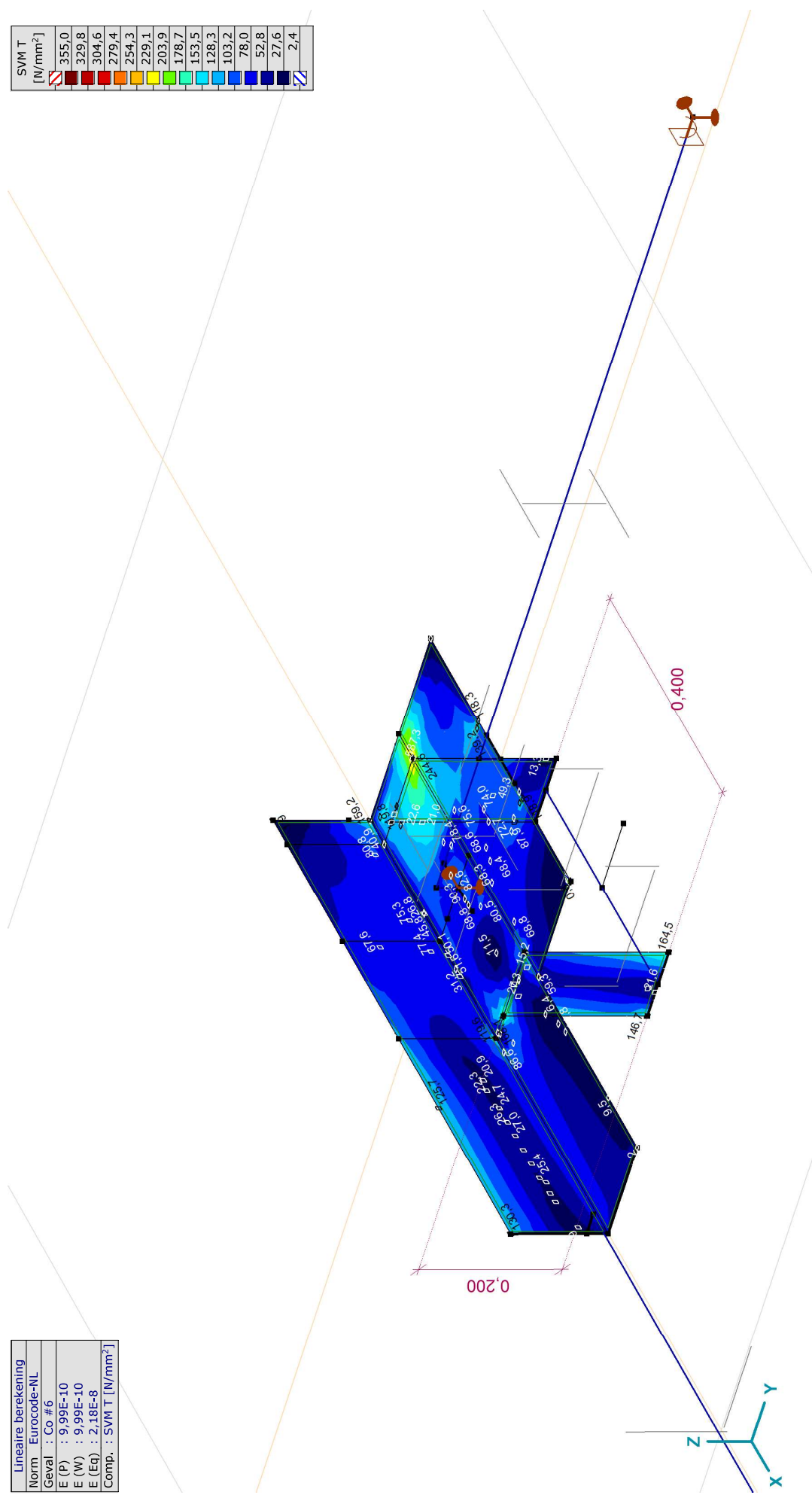
Model: Post aan onderrand HA_s.axes

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| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #6 |
| E (P) : 9,99E-10 |
| E (W) : 9,99E-10 |
| E (Eq) : 2,18E-8 |
| Comp. : SVM T [N/mm ²] |

| SVM T [N/mm ²] |
|----------------------------|
| 355,0 |
| 329,8 |
| 304,6 |
| 279,4 |
| 254,3 |
| 229,1 |
| 203,9 |
| 178,7 |
| 153,5 |
| 128,3 |
| 103,2 |
| 78,0 |
| 52,8 |
| 27,6 |
| 2,4 |



[J], Lineair, Co #6 (UGT), SVM T, Kleuren 2D

Project:

Constructeur: DNV GL - Energy

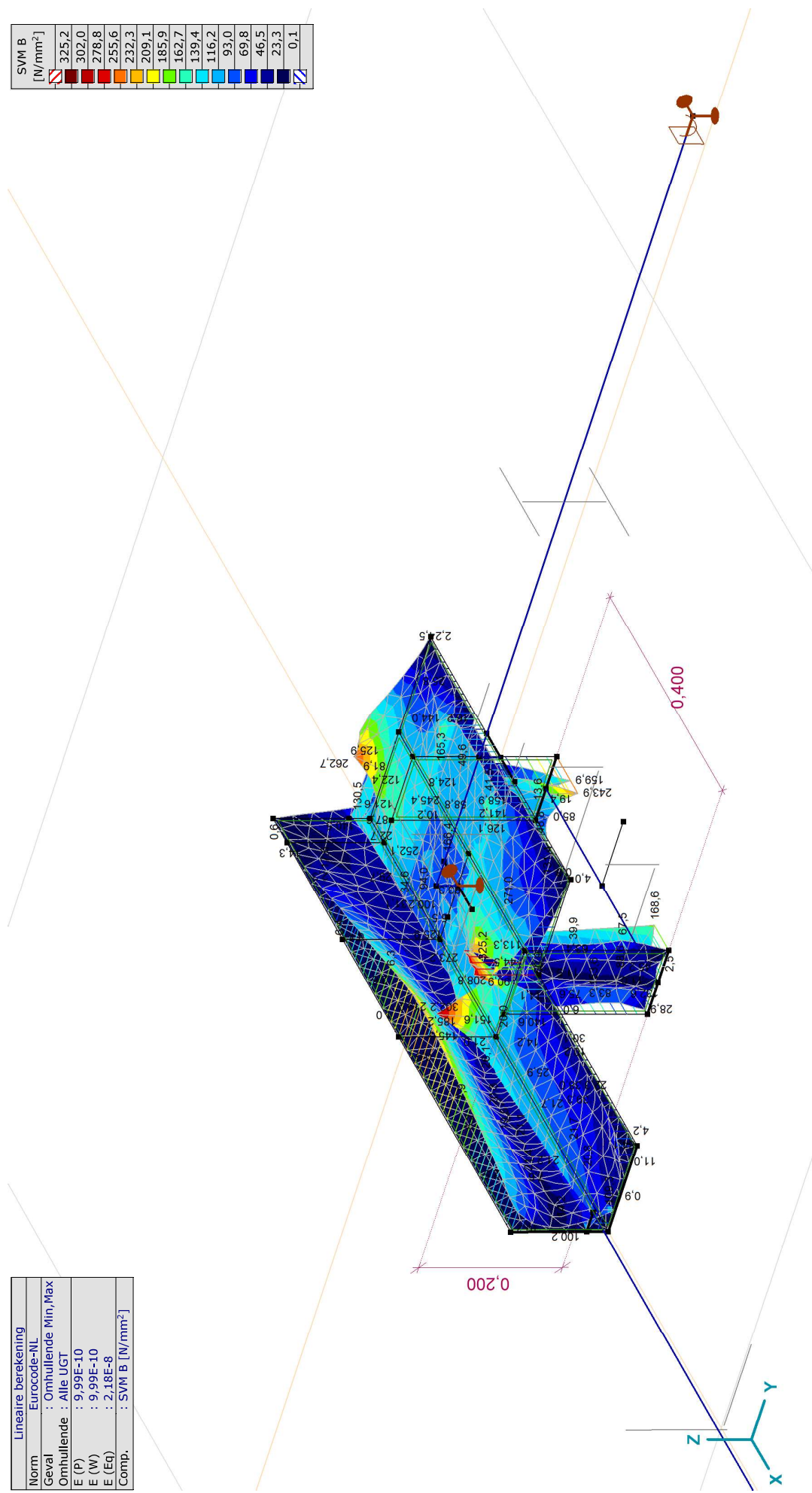
Model: Post aan onderrand HA_s.axes

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| Lineaire berekening | |
|---------------------|------------------------------|
| Norm | : Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : SVM B [N/mm ²] |

| SVM B [N/mm ²] |
|----------------------------|
| 325,2 |
| 302,0 |
| 278,8 |
| 255,6 |
| 232,3 |
| 209,1 |
| 185,9 |
| 162,7 |
| 139,4 |
| 116,2 |
| 93,0 |
| 69,8 |
| 46,5 |
| 23,3 |
| 0,1 |



[I], Lineair, Omhullende (Alle UGT), SVM B, Iso vlakken 3D

Project:

Constructeur: DNV GL - Energy

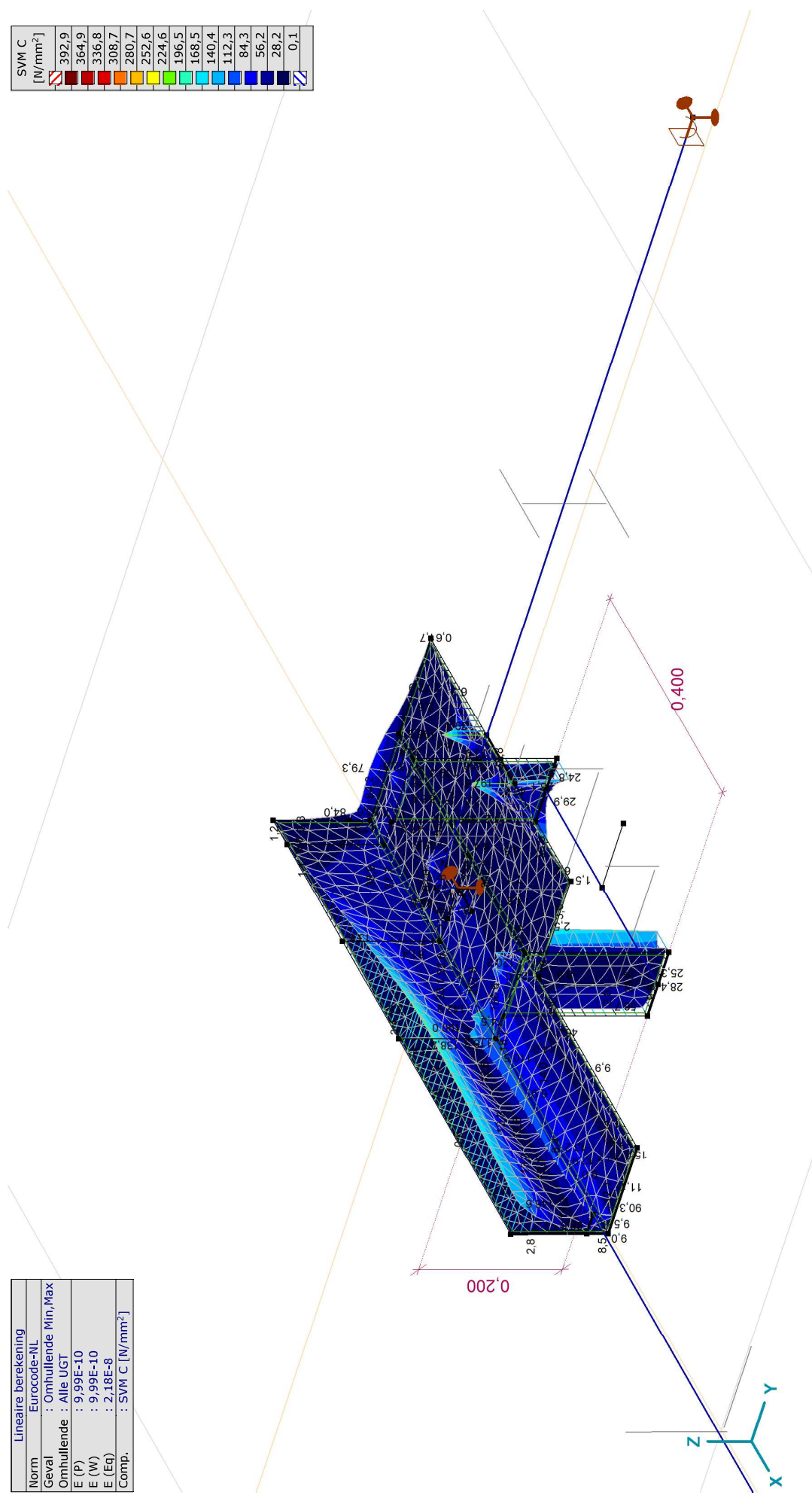
Model: Post aan onderrand HA_s.axes

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| Lineaire berekening | |
|---------------------|------------------------------|
| Norm | : Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : SVM C [N/mm ²] |

| SVM C [N/mm ²] |
|----------------------------|
| 392,9 |
| 364,9 |
| 336,8 |
| 308,7 |
| 280,7 |
| 252,6 |
| 224,6 |
| 196,5 |
| 168,5 |
| 140,4 |
| 112,3 |
| 84,3 |
| 56,2 |
| 28,2 |
| 0,1 |



[I], Lineair, Omhullende (Alle UGT), SVM C, Iso vlakken 3D

Project:

Constructeur: DNV GL - Energy

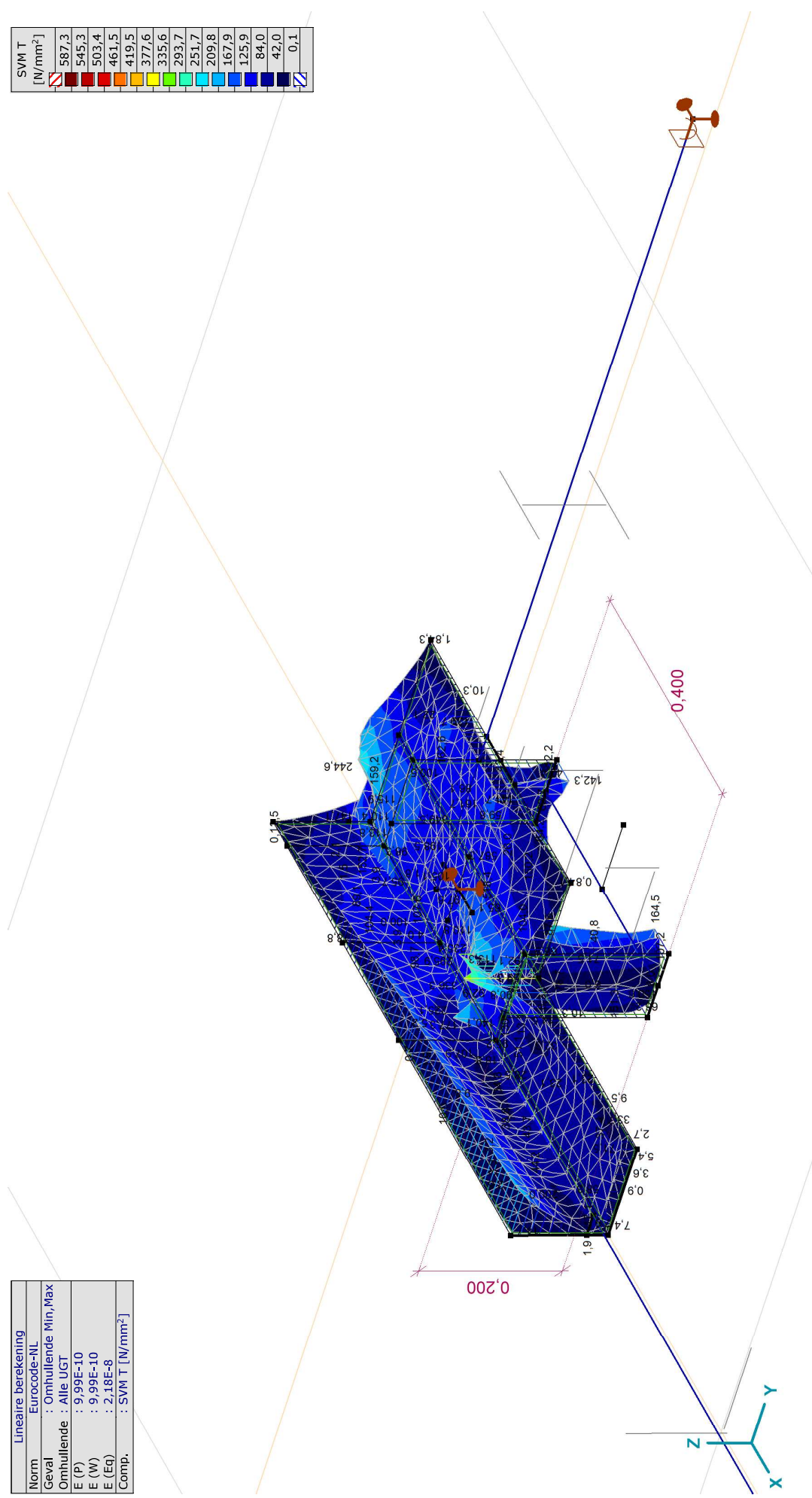
Model: Post aan onderrand HA_s.axes

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| Lineaire berekening | |
|---------------------|------------------------------|
| Norm | : Eurocode-NL |
| Geval | : Omhullende Min,Max |
| Omhullende | : Alle UGT |
| E (P) | : 9.99E-10 |
| E (W) | : 9.99E-10 |
| E (Eq) | : 2.18E-8 |
| Comp. | : SVM T [N/mm ²] |

| SVM T | [N/mm ²] |
|------------------|----------------------|
| [Red] | 587,3 |
| [Dark Red] | 545,3 |
| [Red-Orange] | 503,4 |
| [Orange] | 461,5 |
| [Light Orange] | 419,5 |
| [Yellow] | 377,6 |
| [Light Green] | 335,6 |
| [Green] | 293,7 |
| [Light Blue] | 251,7 |
| [Blue] | 209,8 |
| [Dark Blue] | 167,9 |
| [Very Dark Blue] | 125,9 |
| [Navy] | 84,0 |
| [Black] | 42,0 |
| [White] | 0,1 |



[I], Lineair, Omhullende (Alle UGT), SVM T, Iso vlakken 3D

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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Vlakspanningen [Lineair, Omhullende (Alle UGT)]

| Knoop | C | min. max. | Geval | Oppervlak | Pos. | Sxx [N/mm ²] | Syy [N/mm ²] | Szz [N/mm ²] | Sxy [N/mm ²] | Sxz [N/mm ²] | Syz [N/mm ²] | SVM [N/mm ²] | S1 [N/mm ²] | S2 [N/mm ²] | aS [°] |
|-------|-----|--------------|-------|-----------|------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|----------------------------|----------------------------|-----------|
| Ext. | | | | | | | | | | | | | | | |
| 13 | Sxx | min | Co #6 | Sch 165 | B | -339,3 | -198,1 | 0 | 37,2 | 0 | 0 | 302,2 | -188,9 | -348,5 | 76,10 |
| 13 | | max | Co #5 | Sch 165 | B | 330,1 | 210,5 | 0 | -47,7 | 0 | 0 | 301,0 | 346,8 | 193,8 | -19,30 |
| 8 | Syy | min | Co #5 | Sch 65 | T | -59,0 | -551,7 | 0 | -123,0 | 0 | 0 | 566,3 | -30,0 | -580,8 | -13,27 |
| 8 | | max | Co #6 | Sch 65 | T | 60,8 | 572,1 | 0 | 127,3 | 0 | 0 | 587,3 | 602,1 | 30,8 | 76,76 |
| 1 | Szz | min | Co #1 | Sch 280 | T | -7,8 | -0,7 | 0 | 1,3 | 0 | 0 | 7,8 | -0,5 | -8,0 | 80,09 |
| 1 | | max | Co #1 | Sch 280 | T | -7,8 | -0,7 | 0 | 1,3 | 0 | 0 | 7,8 | -0,5 | -8,0 | 80,09 |
| 5 | Sxy | min | Co #3 | Sch 1 | T | 53,8 | 488,3 | 0 | -133,9 | 0 | 0 | 518,4 | 526,2 | 15,9 | -74,18 |
| 35 | | max | Co #2 | Sch 159 | T | -263,4 | -202,3 | 0 | 136,7 | 0 | 0 | 336,3 | -92,8 | -373,0 | 51,30 |
| 40 | Sxz | min | Co #1 | Sch 554 | C | -0,3 | -4,0 | 0 | 0 | -70,4 | -86,0 | 192,6 | -0,3 | -4,0 | 0,59 |
| 40 | | max | Co #3 | Sch 554 | C | -0,1 | 3,3 | 0 | 0 | 71,7 | 89,6 | 198,8 | 3,3 | -0,1 | -89,37 |
| 39 | Syz | min | Co #1 | Sch 550 | C | -0,3 | -4,0 | 0 | 0 | 68,3 | -86,6 | 191,0 | -0,3 | -4,0 | 0,59 |
| 39 | | max | Co #3 | Sch 550 | C | -0,1 | 3,3 | 0 | 0 | -69,9 | 90,1 | 197,6 | 3,3 | -0,1 | -89,37 |
| 21 | SVM | min | Co #1 | Sch 803 | B | 0 | -0,1 | 0 | 0 | 0 | 0 | 0,1 | 0 | -0,1 | 11,54 |
| 8 | | max | Co #6 | Sch 65 | T | 60,8 | 572,1 | 0 | 127,3 | 0 | 0 | 587,3 | 602,1 | 30,8 | 76,76 |
| 1 | S1 | min | Co #3 | Sch 280 | T | -2,1 | -2,4 | 0 | 0,5 | 0 | 0 | 2,4 | -1,7 | -2,8 | 37,00 |
| 1 | | max | Co #3 | Sch 280 | T | -2,1 | -2,4 | 0 | 0,5 | 0 | 0 | 2,4 | -1,7 | -2,8 | 37,00 |
| 1 | S2 | min | Co #4 | Sch 280 | T | -26,8 | -1,4 | 0 | -25,4 | 0 | 0 | 51,3 | 14,4 | -42,6 | -58,30 |
| 1 | | max | Co #4 | Sch 280 | T | -26,8 | -1,4 | 0 | -25,4 | 0 | 0 | 51,3 | 14,4 | -42,6 | -58,30 |
| 1 | aS | min | Co #4 | Sch 280 | T | -26,8 | -1,4 | 0 | -25,4 | 0 | 0 | 51,3 | 14,4 | -42,6 | -58,30 |
| 1 | | max | Co #4 | Sch 280 | T | -26,8 | -1,4 | 0 | -25,4 | 0 | 0 | 51,3 | 14,4 | -42,6 | -58,30 |

Knoop: Index; **C:** Extreme component; **min.** max.: Extreme type; **Geval:** Belastinggeval van de extreme; **Oppervlak:** Vlak behorend bij knoop; **Pos.:** Punt voor spanningsberekening; **Sxx:** Normaalspanning in lokale x-richting; **Syy:** Normaalspanning in lokale y-richting;

Szz: Normaalspanning in lokale z-richting; **Sxy:** Torsie-/Schuifspanning; **Sxz:** Draal/alschuifspanning; **SVM:** Von Mises spanning; **S1:** Primaire spanning 1; **S2:** Primaire spanning 2; **aS:** Richting primaire spanning;

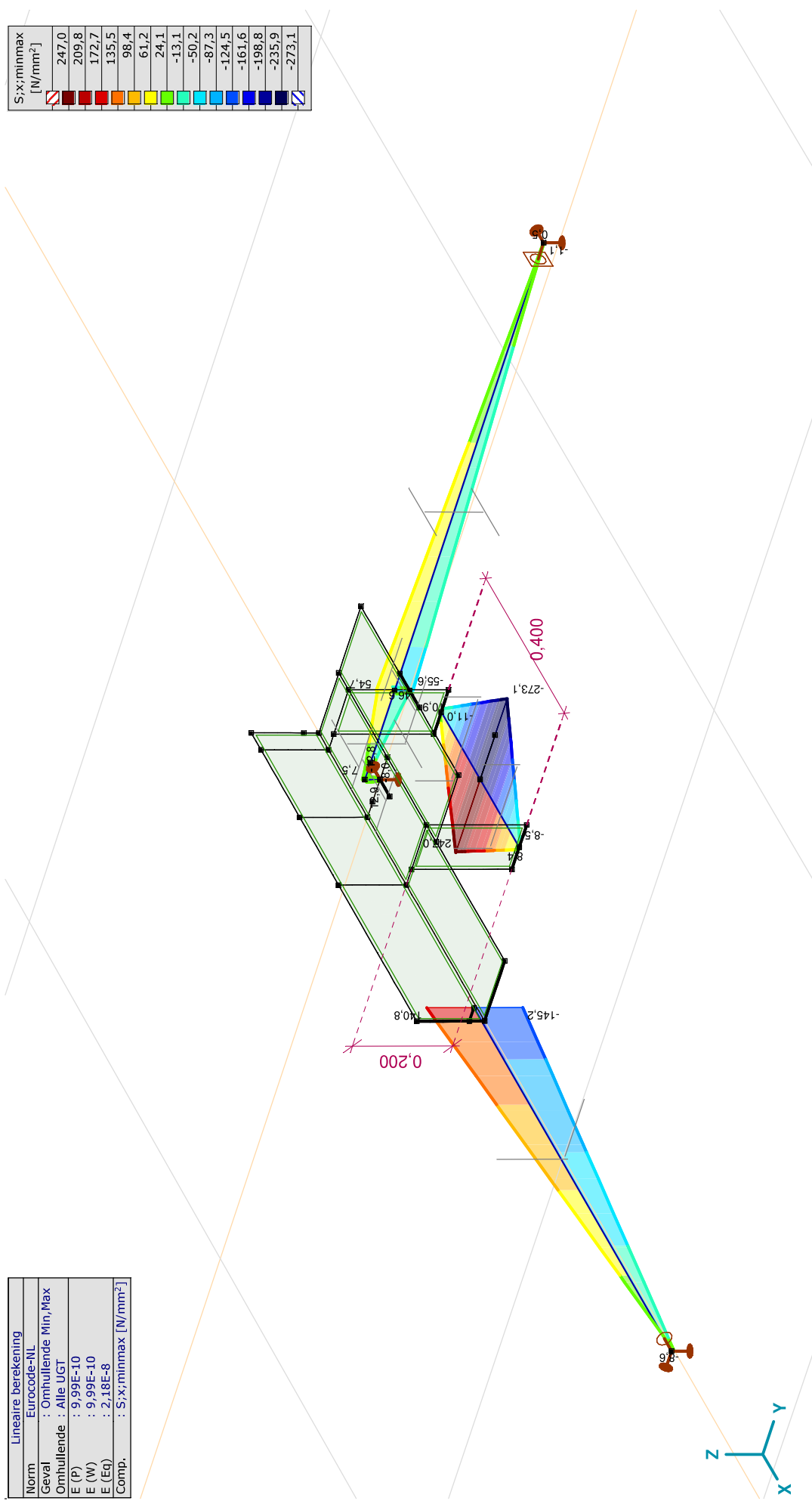
Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

| Lineaire berekening | |
|---------------------|-----------------------------------|
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Alle UGT |
| E (P) | : 9,99E-10 |
| E (W) | : 9,99E-10 |
| E (Eq) | : 2,18E-8 |
| Comp. | : S;x;minmax [N/mm ²] |

| S;x;minmax [N/mm ²] |
|---------------------------------|
| 247,0 |
| 209,8 |
| 172,7 |
| 135,5 |
| 98,4 |
| 61,2 |
| 24,1 |
| -13,1 |
| -50,2 |
| -87,3 |
| -124,5 |
| -161,6 |
| -198,8 |
| -235,9 |
| -273,1 |



[1], Lineair, Omhullende (Alle UGT), S;x;minmax, Lijnen (gevuld)

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

Staatspanningen [Lineair, Omhullende (Alle UGT)]

| Ext. | Prof. | Doorsnede naam | C | min. max. | Geval | Pos. [m] | Knoop | S _x :min [N/mm ²] | S _x :max [N/mm ²] | V _{min} [N/mm ²] | V _{max} [N/mm ²] | S _{min} [N/mm ²] | S _{omax} [N/mm ²] | V _y :gem [N/mm ²] | V _z :gem [N/mm ²] |
|------|-------|----------------|---------------------|-----------|-------|----------|-------|--|--|---------------------------------------|---------------------------------------|---------------------------------------|--|--|--|
| 1 | 1 | U 200 | S _x :min | min | Co #4 | 0,200 | (28) | -273,1 | 99,1 | 0 | 54,7 | 0,8 | 276,5 | -11,0 | -0,3 |
| 7 | 3 | HE 140 A | max | max | Co #3 | 0 | (38) | 9,6 | 9,6 | 4,7 | 11,7 | 12,6 | 22,4 | -3,2 | -0,5 |
| 7 | 3 | HE 140 A | S _x :max | min | Co #1 | 0 | (38) | -9,7 | -9,7 | 2,1 | 9,9 | 10,4 | 19,7 | 3,9 | -0,2 |
| 1 | 1 | U 200 | max | max | Co #2 | 0,200 | (28) | -89,6 | 247,0 | 0 | 52,2 | 0,8 | 250,9 | 9,9 | 0,3 |
| 1 | 1 | U 200 | V _{min} | min | Co #1 | 0 | (26) | -0,5 | 2,0 | 0 | 272,2 | 0,2 | 471,5 | -0,5 | -0,4 |
| 7 | 3 | HE 140 A | max | max | Co #2 | 0 | (38) | 0,5 | 0,5 | 34,9 | 41,0 | 60,5 | 71,1 | 0,4 | -3,9 |
| 3 | 4 | L 140X140X13 | V _{max} | min | Co #5 | 0 | (31) | -103,9 | 64,1 | 0 | 5,0 | 8,6 | 104,0 | -0,1 | 1,5 |
| 1 | 1 | U 200 | max | max | Co #3 | 0 | (26) | -2,2 | 0,5 | 0 | 272,6 | 0,3 | 472,2 | -0,5 | 0,4 |
| 2 | 1 | U 200 | max | max | Co #1 | 0 | (28) | -12,4 | 5,8 | 0 | 272,8 | 0,2 | 472,5 | 0,5 | 0,4 |
| 2 | 1 | U 200 | S _{omin} | min | Co #6 | 0,200 | (27) | -1,7 | 4,3 | 0 | 228,8 | 0,2 | 396,3 | -6,9 | -0,5 |
| 7 | 3 | HE 140 A | max | max | Co #2 | 0,030 | (44) | -2,5 | 3,5 | 34,9 | 41,0 | 60,5 | 71,1 | 0,4 | -3,9 |
| 3 | 4 | L 140X140X13 | S _{omax} | min | Co #5 | 1,000 | (32) | -8,6 | -8,6 | 0 | 5,0 | 8,6 | 12,2 | -0,1 | 1,5 |
| 1 | 1 | U 200 | max | max | Co #3 | 0,200 | (28) | -16,5 | 6,6 | 0 | 272,6 | 0,3 | 472,2 | -0,5 | 0,4 |
| 2 | 1 | U 200 | max | max | Co #1 | 0 | (28) | -12,4 | 5,8 | 0 | 272,8 | 0,2 | 472,5 | 0,5 | 0,4 |
| 1 | 1 | U 200 | V _y :gem | min | Co #4 | 0 | (26) | -11,0 | 3,5 | 0 | 54,7 | 0,8 | 94,8 | -11,0 | -0,3 |
| 2 | 1 | U 200 | max | max | Co #2 | 0 | (28) | -270,5 | 98,6 | 0 | 55,1 | 0,6 | 274,1 | 11,0 | 0,3 |
| 4 | 3 | HE 140 A | V _z :gem | min | Co #3 | 0 | (33) | -5,0 | -0,4 | 4,0 | 40,0 | 6,9 | 69,3 | -0,4 | -8,0 |
| 4 | 3 | HE 140 A | max | max | Co #1 | 0 | (33) | 0,8 | 4,8 | 1,7 | 38,7 | 3,0 | 67,0 | -0,2 | 8,0 |

Prof.: Profiel; C: Extreme component; min. max.: Extreme type; Geval: Belastinggeval van de extreme; Pos.: Lokale X-positie van de doorsnede op de staaf; S_x:min: Doorsnede minimum normaalspanning; S_x:max: Doorsnede maximum normaalspanning;V_{min}: Doorsnede minimum afschuifspanning; V_{max}: Doorsnede maximum afschuifspanning; S_{omin}: Doorsnede minimum Von Mises spanning; S_{omax}: Doorsnede maximum Von Mises spanning; V_y:gem: Afschuifspanning in lokale Y-richting; V_z:gem: Afschuifspanning in lokale Z-richting;

Project:

Constructeur: DNV GL - Energy

Model: Post aan onderrand HA_s.axes

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Interne krachten knooppoplegging [Lineair, Omhullende (Alle UGT)]

| | Knoop | X [m] | Y [m] | Z [m] | Type | C | min. max. | Geval | Rx [kN] | Ry [kN] | Rz [kN] | Rr [kN] | Rcx [kNm] | Rcy [kNm] | Rrz [kNm] | aR |
|------|-------|-------|-------|-------|-------|----|--------------|----------------|------------------------------|---------------------------|----------------------------|--------------|--------------|--------------|--------------|------------------|
| 1 | 32 | 1,600 | 0,030 | 0,030 | Glob. | Ry | min max | Co #4 Co #2 | | -2,6 0,9 | 8,7 -7,6 | 9,1 7,6 | 0 -0,1 | | 0 0,1 | 0,299 -0,119 |
| | | | | | | Rz | min max | Co #2 Co #4 | | 0,9 -2,6 | 7,6 8,7 | 7,6 9,1 | -0,1 0 | | 0 0 | -0,119 0,299 |
| 2 | 45 | 0 | 1,285 | 0,030 | Glob. | Rx | min max | Co #4 Co #2 | -2,1 2,6 | 2,6 -0,9 | 0,4 -0,3 | 3,4 2,8 | | 0,1 -0,1 | 0,1 0,1 | 9,132 -9,372 |
| | | | | | | Ry | min max | Co #3 Co #1 | 0,3 0,1 | -1,7 3,4 | -5,1 5,2 | 5,4 6,2 | 0 0 | 0 0 | 0 0 | -0,346 0,664 |
| | | | | | | Rz | min max | Co #3 Co #1 | 0,3 0,1 | -1,7 3,4 | -5,1 5,2 | 5,4 6,2 | 0 0 | 0 0 | 0 0 | -0,346 0,664 |
| 3 | 10 | 0 | 0,085 | 0 | Glob. | Rx | min max | Co #4 Co #2 | -32,3 -28,2 | | -12,6 4,4 | 34,7 28,5 | | | | -2,571 6,453 |
| | | | | | | Rz | min max | Co #4 Co #2 | -32,3 -28,2 | | -12,6 4,4 | 34,7 28,5 | | | | -2,571 6,453 |
| Ext. | | | | | | | | | | | | | | | | |
| 3 | 10 | 0 | 0,085 | 0 | Glob. | Rx | min max | Co #4 Co #2 | -32,3 2,6 | | -12,6 -0,3 | 34,7 2,8 | | | | -2,571 -9,372 |
| 2 | 45 | 0 | 1,285 | 0,030 | Glob. | Ry | min max | Co #4 Co #1 | -2,6 0,1 | -0,9 3,4 | 8,7 5,2 | 9,1 6,2 | 0 | -0,1 | 0 | 0,299 0,664 |
| 3 | 10 | 0 | 0,085 | 0 | Glob. | Rz | min max | Co #4 Co #4 | -32,3 -2,6 | -2,6 -2,6 | -12,6 8,7 | 34,7 9,1 | 0 | 0 | 0 | -2,571 0,299 |

Knoop: Ondersteunde knoop; **Type:** Opleggingstype; **C:** Extreme component; **min, max.:** Extreem type; **Geval:** Belastinggeval van de extreme; **Rx:** X-component opleggingreactiekracht; **Ry:** Y-component opleggingreactiekracht; **Rz:** Z-component opleggingreactiekracht; **Rr:** Resulterende opleggingreactiekracht; **Rcx:** X-component opleggingreactiemoment; **Rcy:** Y-component opleggingreactiemoment; **Rrz:** Resulterende opleggingreactiemoment; **Rrr:** Resulterende opleggingreactiemoment; **aR:** Verhouding verticale opleggingkracht / horizontale opleggingkracht;

Project:

Constructeur: DNV GL - Energy

AxisVM X5 R4h · Geregistreerd aan DNV GL - Energy
Model 1.axs

Rapport

Rapport, Inhoudsopgave

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Project:

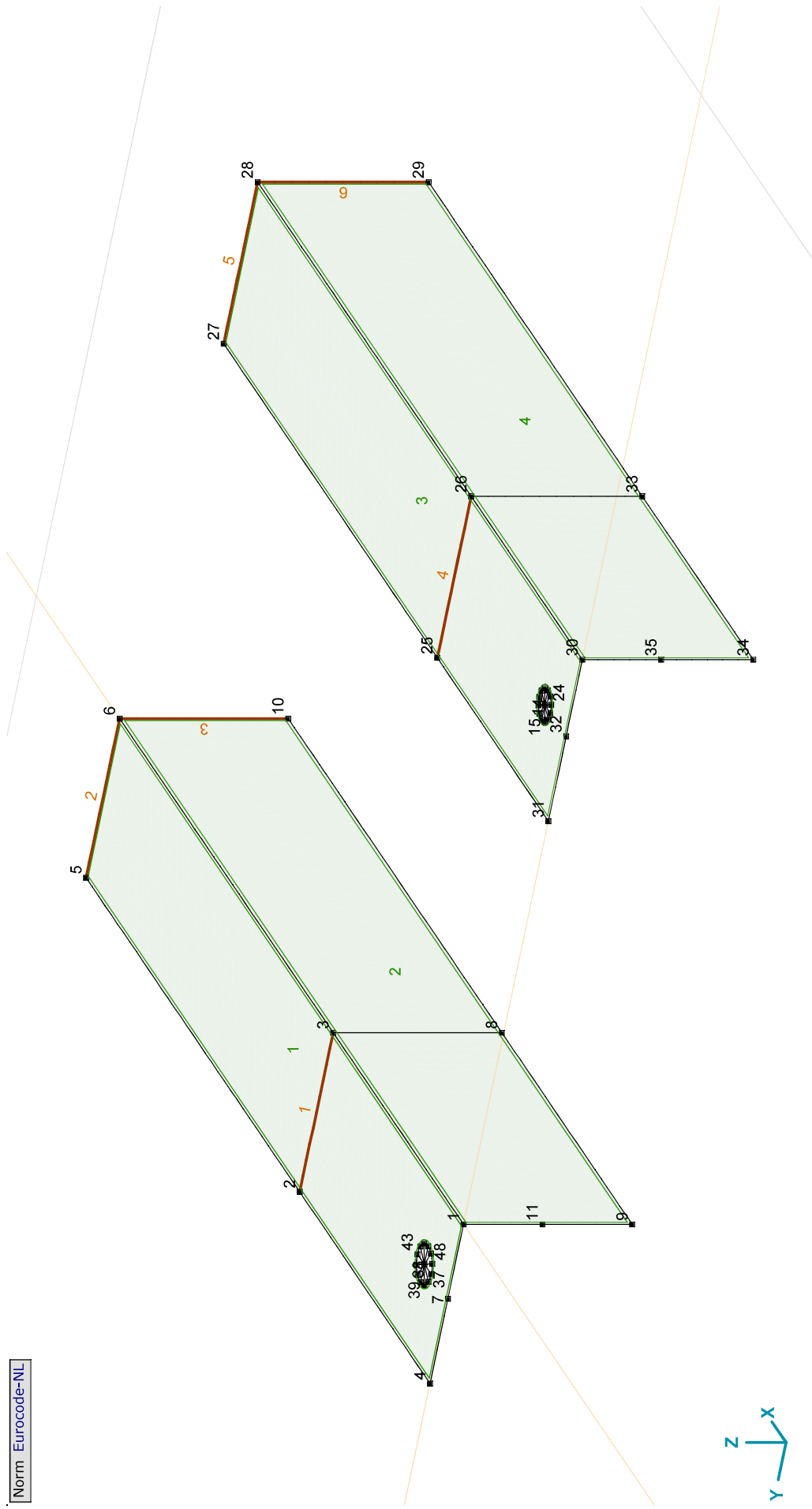
Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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Norm Eurocode-NL



Tekening

Project:

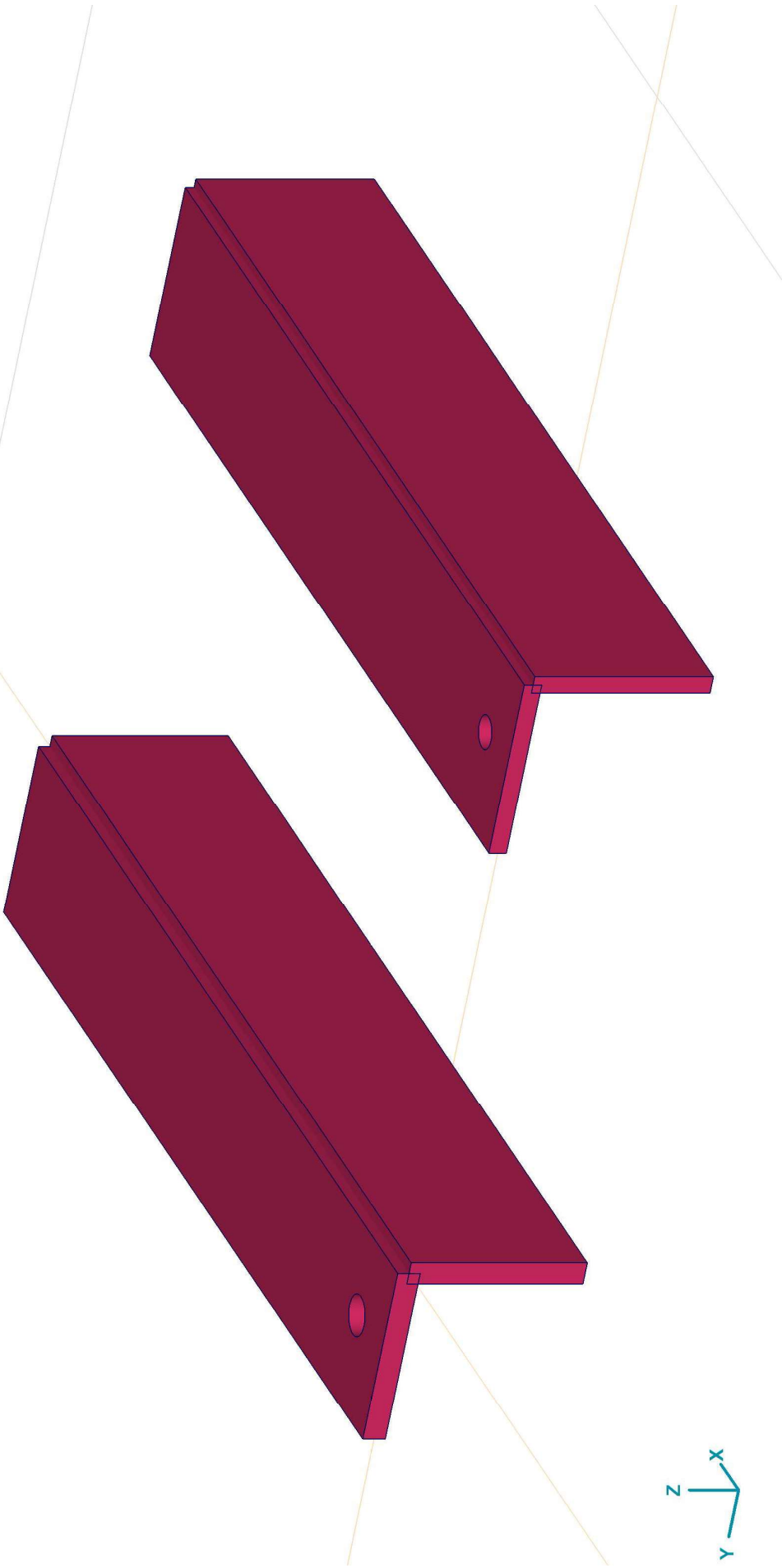
Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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Norm Eurocode-NL



Tekening2

Project:




Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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Materialen

| Naam | Type | Nationale norm | Materiaalnorm | Model | E_x [N/mm ²] | E_y [N/mm ²] | ν | α_T [1/°C] | ρ [kg/m ³] | Materiaal kleur | Contour kleur | Structuur | |
|------|-------|----------------|---------------|---------|----------------------------|----------------------------|--------|-------------------|-----------------------------|-----------------|---|---|---|
| 1 | S 355 | Staal | Eurocode-NL | 10025-2 | Lineair | 210000 | 210000 | 0,30 | 1,2E-5 | 7850 |  |  |  |

| Naam | P_1 | P_2 | P_3 | P_4 | P_5 | P_6 | P_7 | P_8 | P_9 | P_{10} | P_{11} | P_{12} | P_{13} | P_{14} |
|------|-------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------|-------|-------|-------|----------|----------|----------|----------|----------|
| 1 | S 355 | f_y [N/mm ²] = 355,00 | f_u [N/mm ²] = 510,00 | f_y [N/mm ²] = 335,00 | f_u [N/mm ²] = 470,00 | | | | | | | | | |

Naam: Materiaalnaam; Type: Type materiaal; Model: Materiaal model; E_x : Elasticiteitsmodulus in lokale x richting; E_y : Elasticiteitsmodulus in lokale y richting; ν : Poisson's verhouding; α_T : Warmteuitzettingscoëfficiënt; ρ : Dichtheid; **Materiaal kleur**: Materiaalkleur; **Contour Meur**: Contourkleur; $P_1, P_2, P_3, P_4, P_5, P_6, P_7, P_8, P_9, P_{10}, P_{11}, P_{12}, P_{13}, P_{14}$: Ontwerpparameter;

Domeinen

| Element type | Materiaal | Ref _x | Ref _z | Dikte [mm] | k, buiging | k, torsie | k, afschuiving | Oppervlakte [m ²] | Gat | Mesh |
|--------------|----------------|------------------|------------------|------------|------------|-----------|----------------|-------------------------------|-----|------|
| 1 | # Schaal S 355 | Auto | Auto | 18 | | | | 0,113 | 1 | ✓ |
| 2 | # Schaal S 355 | Auto | Auto | 18 | | | | 0,114 | - | ✓ |
| 3 | # Schaal S 355 | Auto | Auto | 14 | | | | 0,108 | 1 | ✓ |
| 4 | # Schaal S 355 | Auto | Auto | 14 | | | | 0,109 | - | ✓ |

Element type: Plaalement type; **Ref_x**: Referentie voor lokale X-richting; **Ref_z**: Referentie voor lokale Z-richting; **k, buiging**: Buigsterkte coefficient; **k, torsie**: Torsiesterkte coefficient; **k, afschuiving**: Dwarskrachtsterkte coefficient; **Oppervlakte**: Domein oppervlakte; **Gat**: Aantal gaten in domein; **Mesh**: Gegenerende mesh;

Project:

Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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Lijnopleggingen

| Lijn | Type | Ref. elem. | Rx [kN/m/m] | Ry [kN/m/m] | Rz [kN/m/m] | Rxx [kNm/rad/m] | Ryy [kNm/rad/m] | Rzz [kNm/rad/m] | NL(x) | NL(y) | NL(z) |
|------|-------------|------------|----------------|----------------|----------------|--------------------|--------------------|--------------------|-------------|-------------|-------------|
| 1 | Rand (2034) | Domein 1 | 0 | 1E+7 | 1E+7 | 0 | 0 | 0 | | Symmetrisch | Symmetrisch |
| 2 | Rand (1959) | Domein 1 | 1E+10 | 0 | 0 | 0 | 0 | 0 | Symmetrisch | | |
| 3 | Rand (104) | Domein 2 | 1E+10 | 0 | 0 | 0 | 0 | 0 | Symmetrisch | | |
| 4 | Rand (3938) | Domein 3 | 0 | 1E+7 | 1E+7 | 0 | 0 | 0 | | Symmetrisch | Symmetrisch |
| 5 | Rand (3866) | Domein 3 | 1E+10 | 0 | 0 | 0 | 0 | 0 | Symmetrisch | | |
| 6 | Rand (5718) | Domein 4 | 1E+10 | 0 | 0 | 0 | 0 | 0 | Symmetrisch | | |

| Lijn | NL(xx) | NL(yy) | NL(zz) | F(x) [kN/m] | F(y) [kN/m] | F(z) [kN/m] | M(x) [kNm/m] | M(y) [kNm/m] | M(z) [kNm/m] |
|------|-------------|--------|--------|----------------|----------------|----------------|-----------------|-----------------|-----------------|
| 1 | Rand (2034) | | | | | | | | |
| 2 | Rand (1959) | | | | | | | | |
| 3 | Rand (104) | | | | | | | | |
| 4 | Rand (3938) | | | | | | | | |
| 5 | Rand (3866) | | | | | | | | |
| 6 | Rand (5718) | | | | | | | | |

Lijn: Ondersteund lijnelement; **Type:** Opleggingstype; **Ref. elem.:** Referentie-element; **Rx, Ry, Rz:** Verplaatsingslijfheid; **Rxx, Ryy, Rzz:** Rotatieslijfheid; **NL(x), NL(y), NL(z), NL(xx), NL(yy), NL(zz):** Niet-lineaire parameters; **F(x):** Weerstand in X-richting; **F(y):** Weerstand in Y-richting; **F(z):** Weerstand in Z-richting; **M(x):** Weerstandsmoment in X-richting; **M(y):** Weerstandsmoment in Y-richting; **M(z):** Weerstandsmoment in Z-richting.

Project:

Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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| |
|-------------------|
| Norm: Eurocode-NL |
| Geval: Fx |



Project:

Constructeur: DNV GL - Energy

Model: **Model 1.axis**

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Fx: Oppervlak lijnlast

| | <i>Richting</i> | p_x [kN/m] | p_y [kN/m] | p_z [kN/m] | p_m [kNm/m] | X [m] | Y [m] | Z [m] | <i>Richting</i> | dL [m] |
|---|-----------------|-----------------|-----------------|-----------------|------------------|------------|------------|------------|------------------------|-------------|
| 1 | Global | -1422,00 | 0 | 0 | 0 | 0,055 | 0,082 | 0 | (0,055; 0,066; 0,000) | 0 |
| | | -1422,00 | 0 | 0 | 0 | 0,055 | 0,050 | 0 | - | 0,050 |
| 4 | Global | -842,00 | 0 | 0 | 0 | 0,050 | -0,419 | 0 | (0,050; -0,432; 0,000) | 0 |
| | | -842,00 | 0 | 0 | 0 | 0,050 | -0,445 | 0 | - | 0,041 |

p_x , p_y , p_z : Belastingkracht component; **p_m :** Belastingmoment component; **X :** Belasting in X-richting; **Y :** Belasting in Y-richting; **Z :** Belasting in Z-richting;

Project:

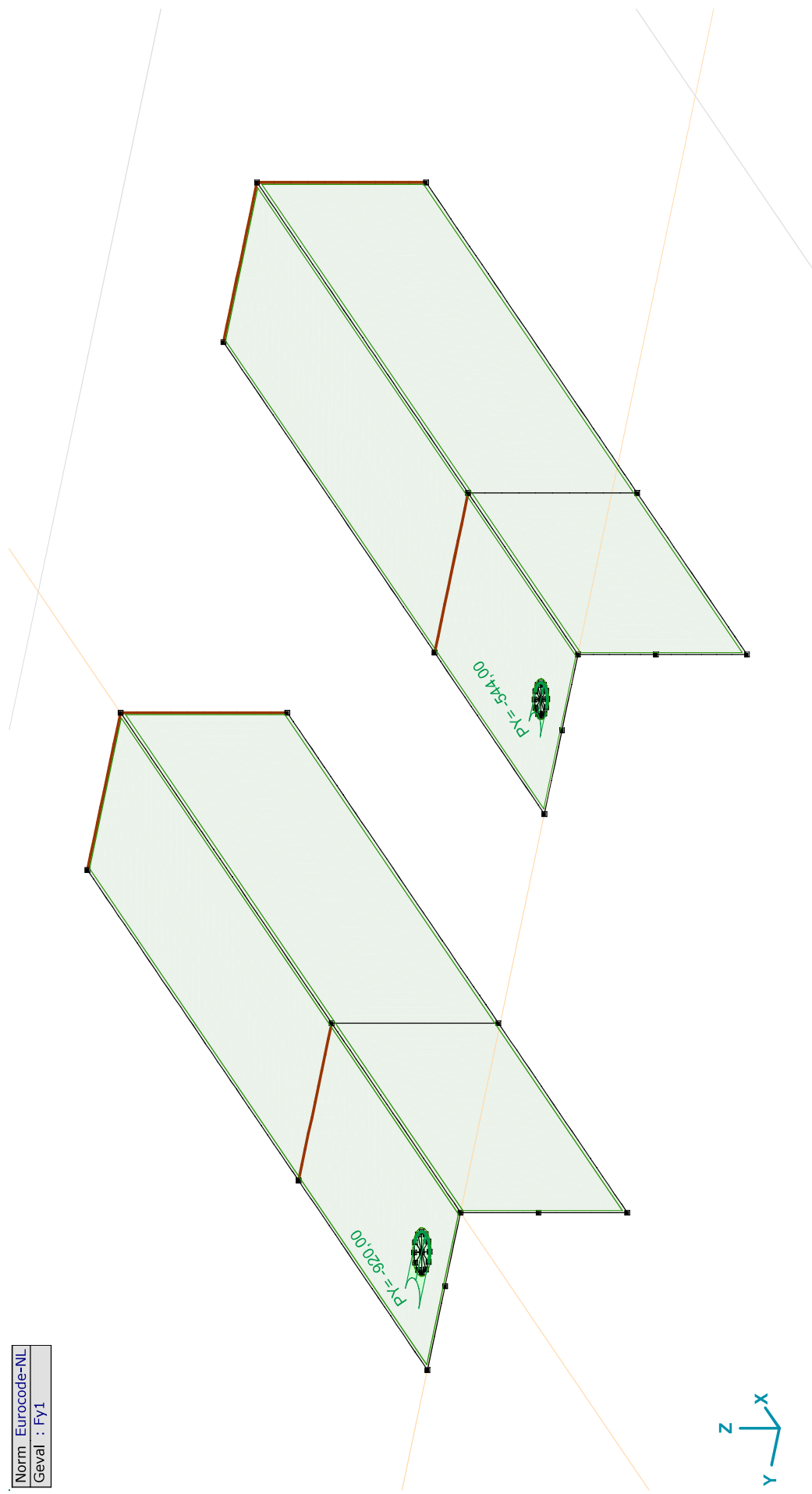
Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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| |
|-------------------|
| Norm: Eurocode-NL |
| Geval: FY1 |



FY1

Project:

Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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Fy1: Oppervlak lijnlast

| | Richting | p_x [kN/m] | p_y [kN/m] | p_z [kN/m] | p_m [kNm/m] | X [m] | Y [m] | Z [m] | Richting | dL [m] |
|---|----------|-----------------|-----------------|-----------------|------------------|----------|----------|----------|------------------------|-------------|
| 5 | Global | 0 | -920,00 | 0 | 0 | 0,071 | 0,066 | 0 | (0,055; 0,066; 0,000) | 0 |
| | | 0 | -920,00 | 0 | 0 | 0,039 | 0,066 | 0 | - | 0,050 |
| 7 | Global | 0 | -544,00 | 0 | 0 | 0,037 | -0,432 | 0 | (0,050; -0,432; 0,000) | 0 |
| | | 0 | -544,00 | 0 | 0 | 0,063 | -0,432 | 0 | - | 0,041 |

p_x , p_y , p_z : Belastingkracht component; **p_m :** Belastingmoment component; **X:** Belasting in X-richting; **Y:** Belasting in Y-richting; **Z:** Belasting in Z-richting;

Project:

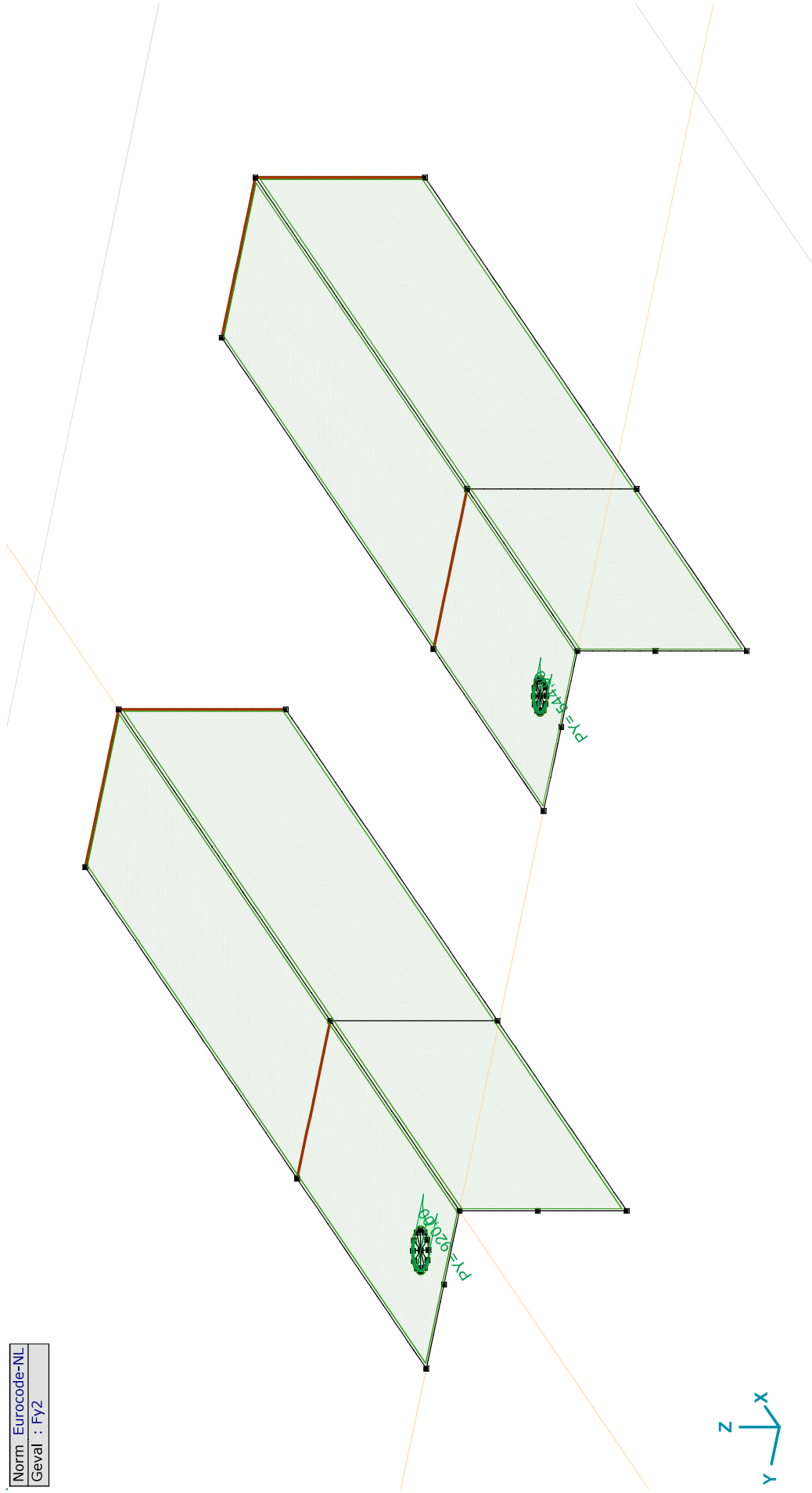
Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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| |
|-------------------|
| Norm: Eurocode-NL |
| Geval: FY2 |



FY2

Project:

Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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Fy2: Oppervlak lijnlast

| | Richting | p_x [kN/m] | p_y [kN/m] | p_z [kN/m] | p_m [kNm/m] | X [m] | Y [m] | Z [m] | Richting | dL [m] |
|---|----------|-----------------|-----------------|-----------------|------------------|------------|------------|------------|------------------------|-------------|
| 6 | Global | 0 | 920,00 | 0 | 0 | 0,071 | 0,066 | 0 | (0,055; 0,066; 0,000) | 0 |
| | | 0 | 920,00 | 0 | 0 | 0,039 | 0,066 | 0 | - | 0,050 |
| 8 | Global | 0 | 544,00 | 0 | 0 | 0,063 | -0,432 | 0 | (0,050; -0,432; 0,000) | 0 |
| | | 0 | 544,00 | 0 | 0 | 0,037 | -0,432 | 0 | - | 0,041 |

p_x , p_y , p_z : Belastingkracht component; **p_m :** Belastingmoment component; **X :** Belasting in X-richting; **Y :** Belasting in Y-richting; **Z :** Belasting in Z-richting;

Project:

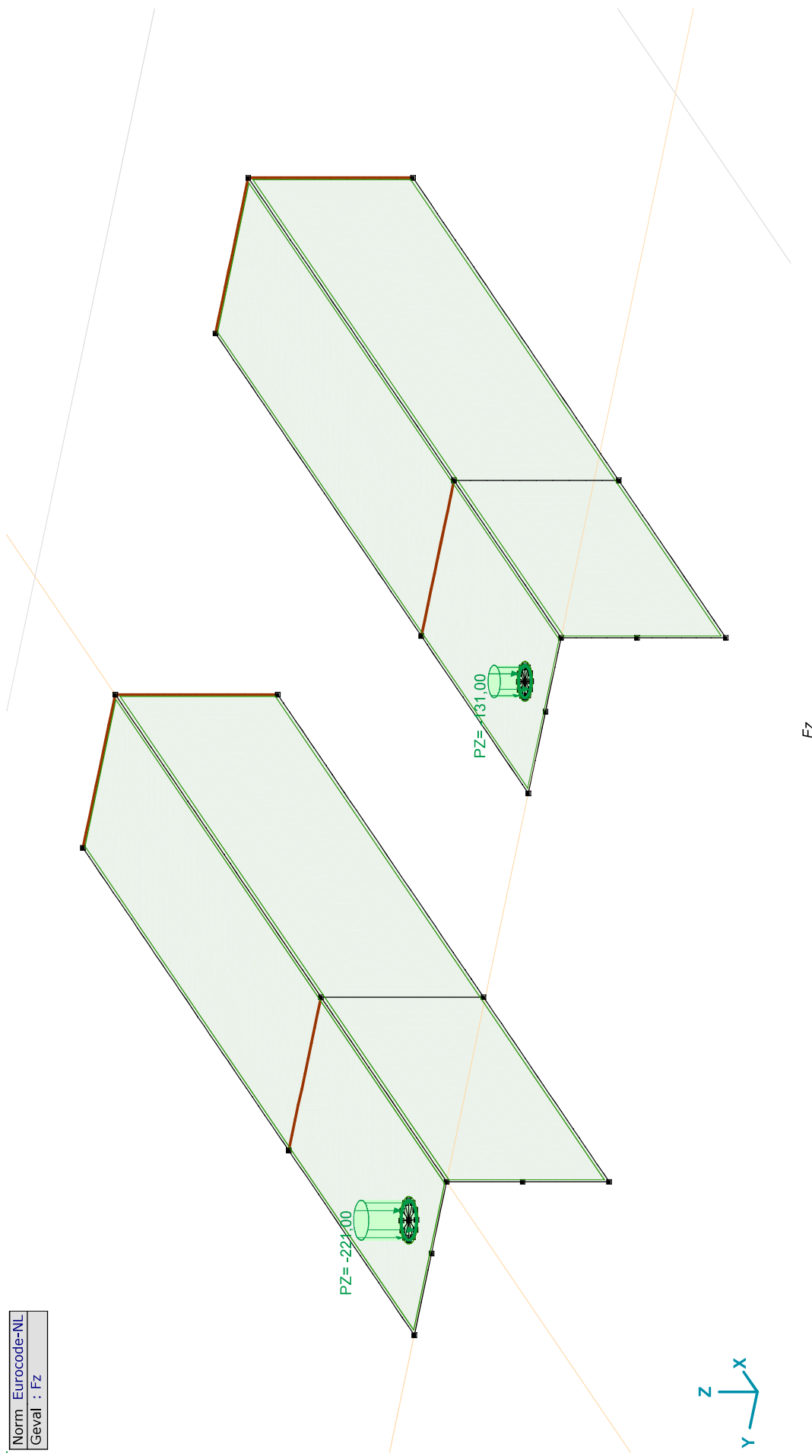
Constructeur: DNV GL - Energy

Model: Model 1.axs

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| |
|-------------------|
| Norm: Eurocode-NL |
| Geval: Fz |



Project:

Constructeur: DNV GL - Energy

Model: **Model 1.axs**

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Fz: Oppervlak lijnlast

| | Richting | p_x [kN/m] | p_y [kN/m] | p_z [kN/m] | p_m [kNm/m] | X [m] | Y [m] | Z [m] | Richting | dL [m] |
|---|----------|-----------------|-----------------|-----------------|------------------|----------|----------|----------|------------------------|-------------|
| 2 | Global | 0 | 0 | -221,00 | 0 | 0,071 | 0,066 | 0 | (0,055; 0,066; 0,000) | 0 |
| | | 0 | 0 | -221,00 | 0 | 0,071 | 0,066 | 0 | - | 0,101 |
| 3 | Global | 0 | 0 | -131,00 | 0 | 0,063 | -0,432 | 0 | (0,050; -0,432; 0,000) | 0 |
| | | 0 | 0 | -131,00 | 0 | 0,063 | -0,432 | 0 | - | 0,082 |

p_x , p_y , p_z : Belastingkracht component; **p_m :** Belastingmoment component; **X:** Belasting in X-richting; **Y:** Belasting in Y-richting; **Z:** Belasting in Z-richting;

Gebruiker gedefinieerde belastingcombinaties uit belastinggevallen

| | Naam | Type | F_x | F_{y1} | F_{y2} | F_z | Commentaar |
|---|-------|------|-------|----------|----------|-------|------------|
| 1 | Co #1 | UGT | 1,00 | 1,00 | 0 | 1,00 | |
| 2 | Co #2 | UGT | 1,00 | 0 | 1,00 | 1,00 | |

Naam: Naam belastingcombinatie; **Type:** Type belastingcombinatie; **F_x , F_{y1} , F_{y2} , F_z :** Factor;

Project:

Constructeur: DNV GL - Energy

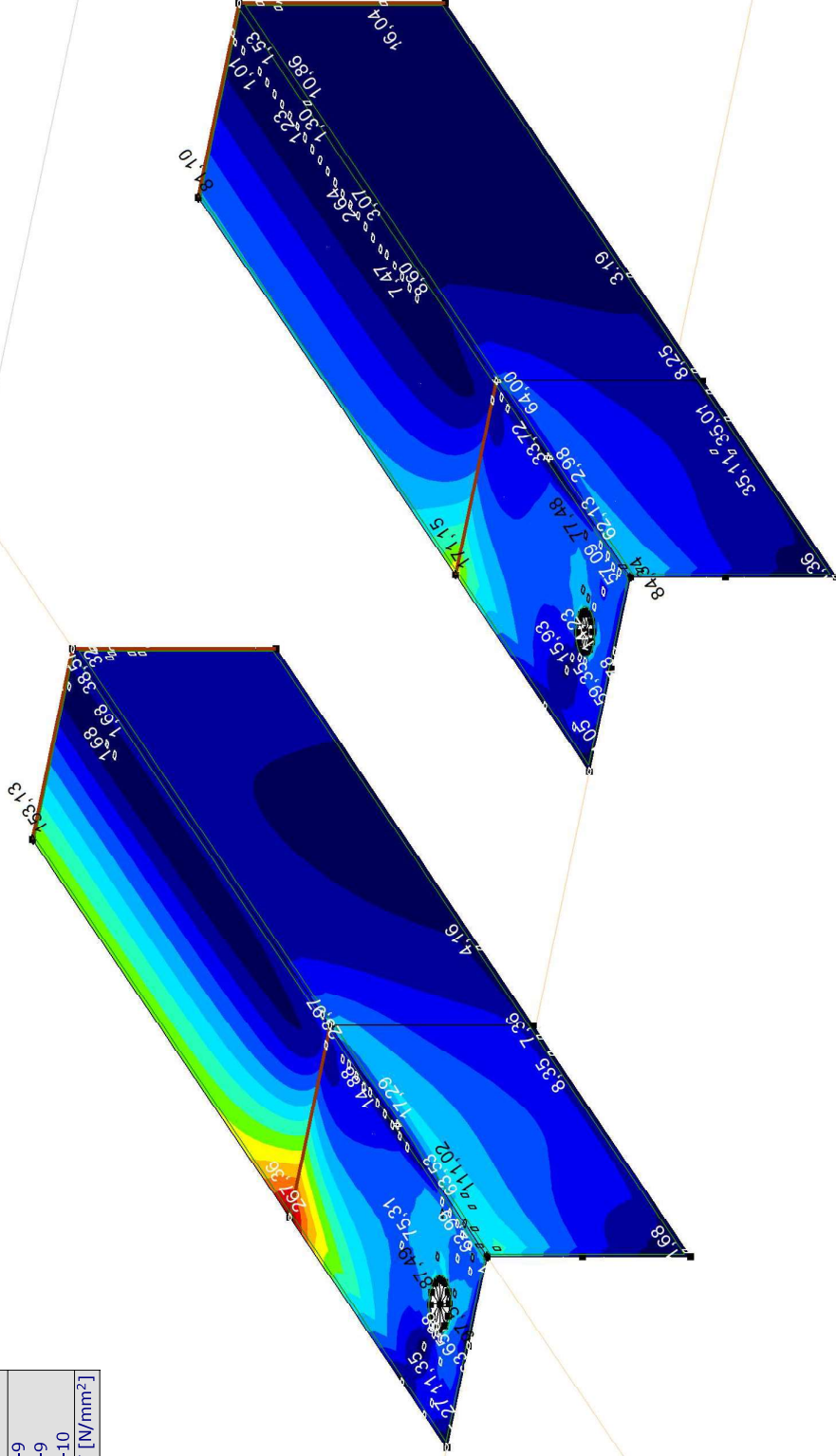
Model: **Model 1.axs**

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Pag. 15

| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #1 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : SVM T [N/mm ²] |

| SVM T [N/mm ²] |
|----------------------------|
| 268,35 |
| 249,26 |
| 230,16 |
| 211,07 |
| 191,97 |
| 172,87 |
| 153,78 |
| 134,68 |
| 115,59 |
| 96,49 |
| 77,40 |
| 58,30 |
| 39,20 |
| 20,11 |
| 1,01 |



[I]. Lineair, Co #1 (UGT), SVM T, Kleuren 2D

Project:

Constructeur: DNV GL - Energy

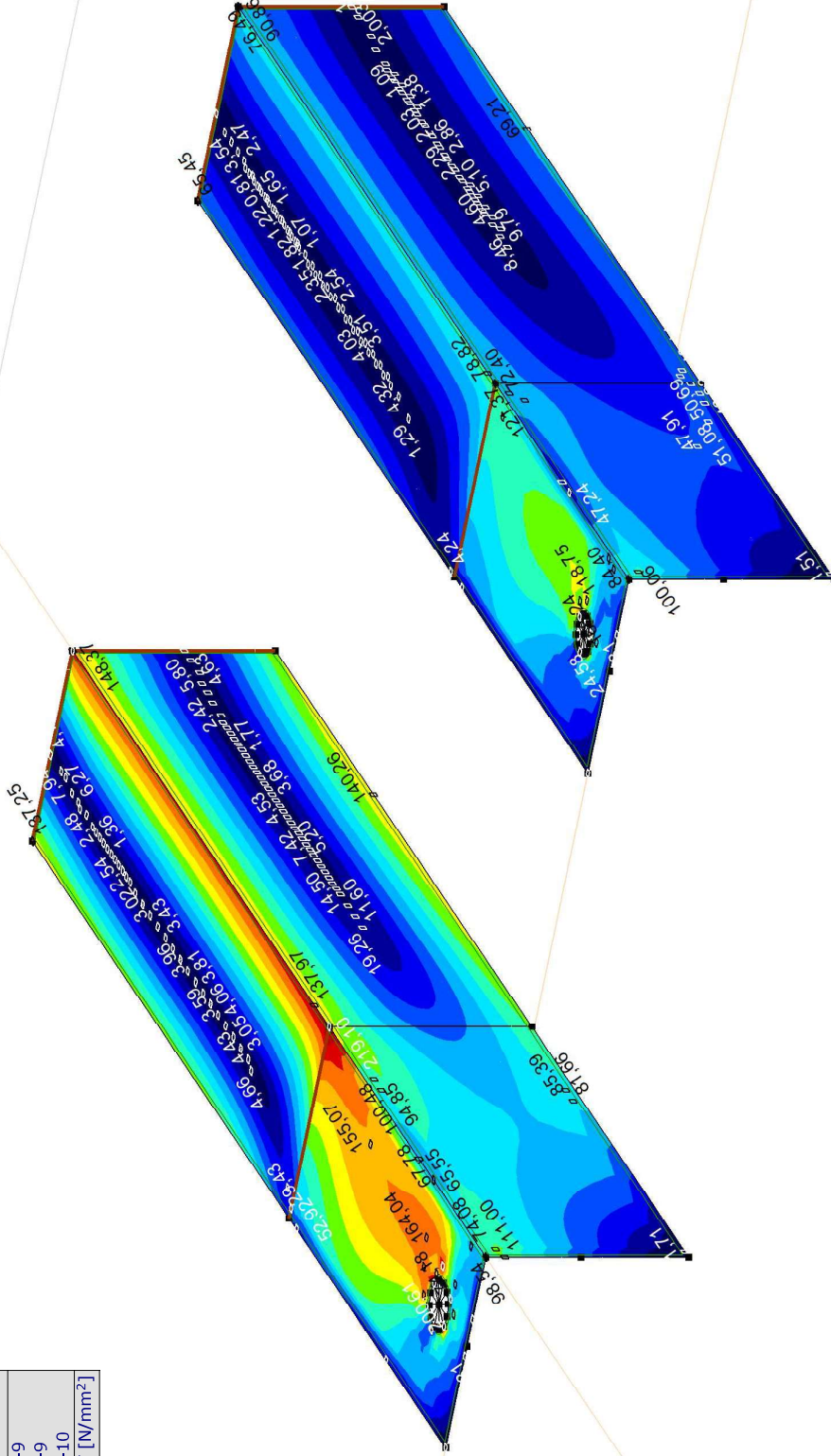
Model: **Model 1.axis**

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| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #2 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : SVM T [N/mm ²] |

| SVM T [N/mm ²] |
|----------------------------|
| 219,10 |
| 203,50 |
| 187,90 |
| 172,30 |
| 156,70 |
| 141,10 |
| 125,50 |
| 109,90 |
| 94,30 |
| 78,70 |
| 63,10 |
| 47,49 |
| 31,89 |
| 16,29 |
| 0,69 |

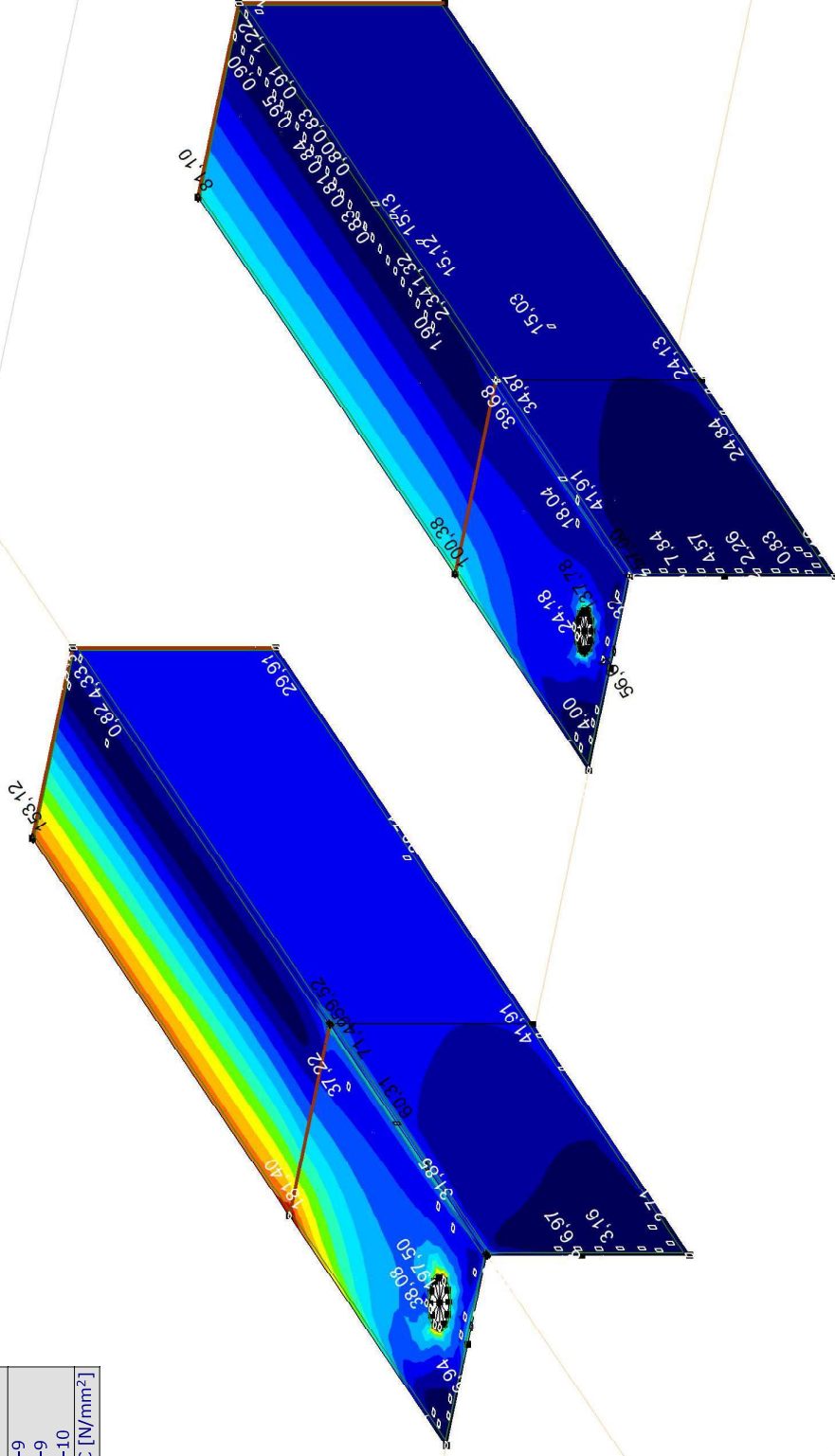


[1]. Lineair, Co #2 (UGT), SVM T, Kleuren 2D

Project:
 Constructeur: DNV GL - Energy
 Model: **Model 1.axs**

| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #1 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : SVM C [N/mm ²] |

| SVM C [N/mm ²] |
|----------------------------|
| 197,50 |
| 183,41 |
| 169,32 |
| 155,23 |
| 141,15 |
| 127,06 |
| 112,97 |
| 98,88 |
| 84,79 |
| 70,71 |
| 56,62 |
| 42,53 |
| 28,44 |
| 14,36 |
| 0,27 |



III. Lineair, Co #1 (UGT), SVM C, Kleuren 2D

Project:

Constructeur: DNV GL - Energy

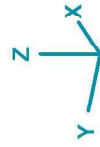
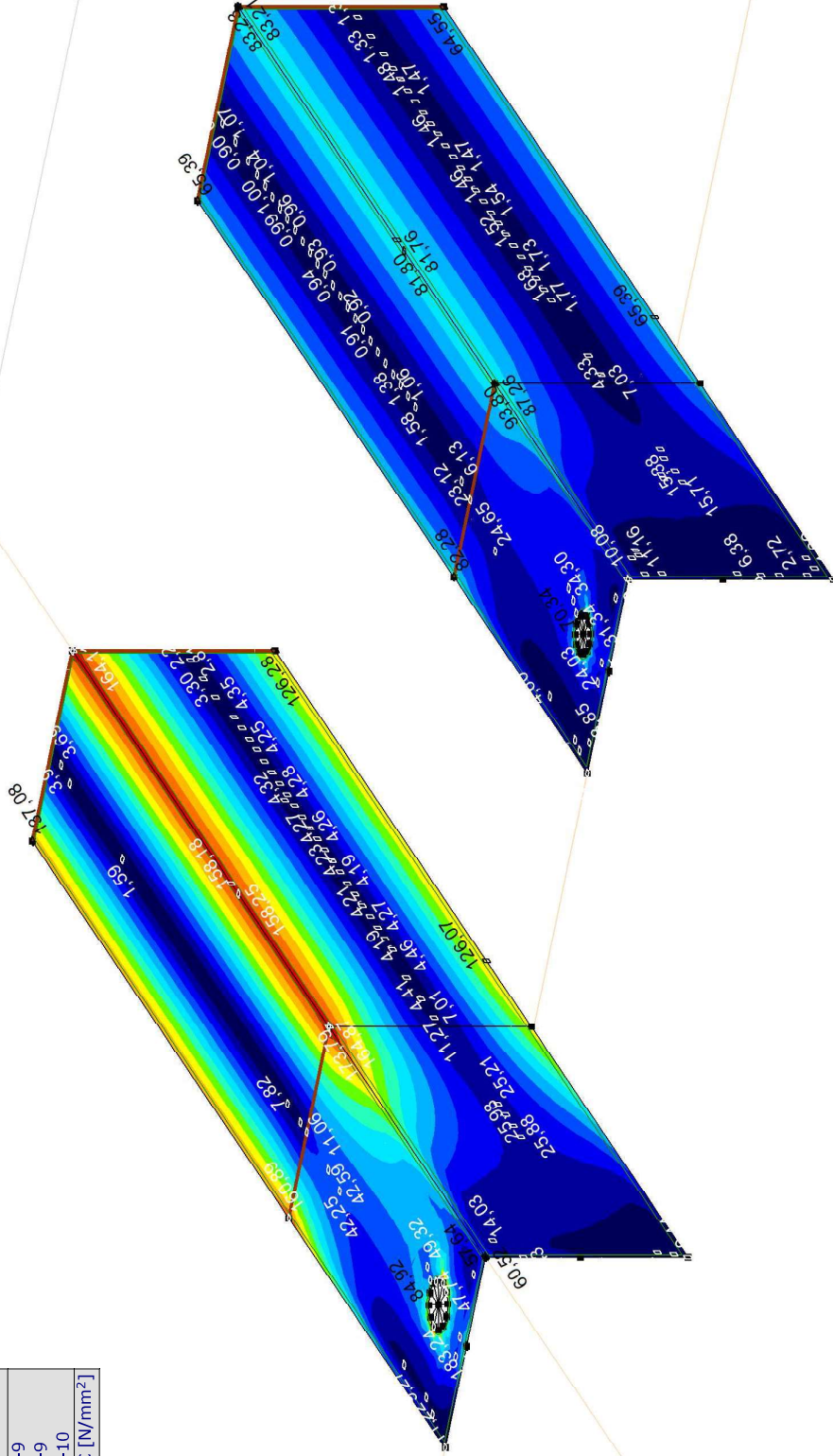
Model: Model 1.axs

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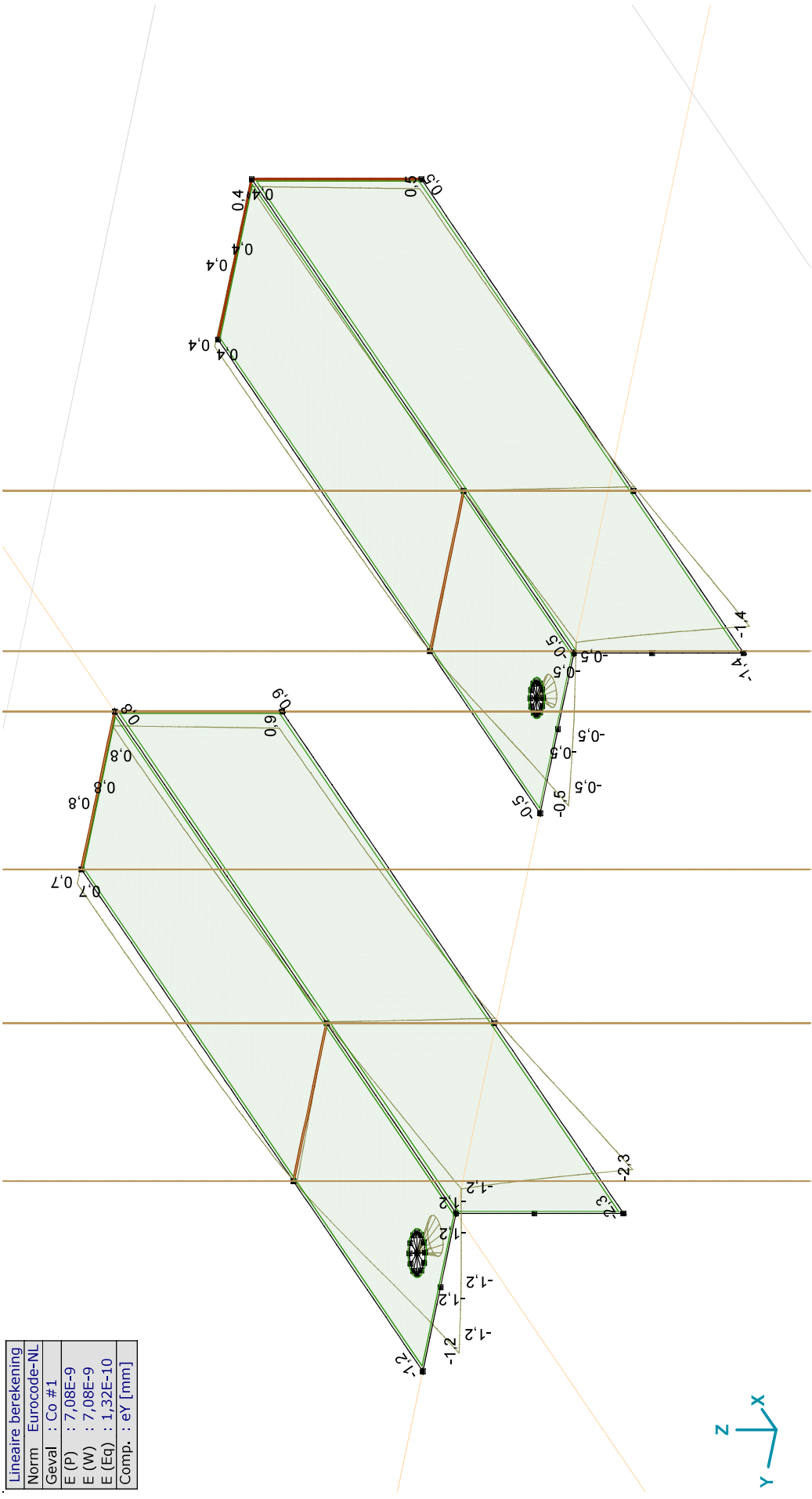
| |
|------------------------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #2 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : SVM C [N/mm ²] |

| SVM C [N/mm ²] |
|----------------------------|
| 192,93 |
| 179,17 |
| 165,42 |
| 151,66 |
| 137,90 |
| 124,14 |
| 110,38 |
| 96,62 |
| 82,86 |
| 69,10 |
| 55,35 |
| 41,59 |
| 27,83 |
| 14,07 |
| 0,31 |



III. Lineair, Co #2 (UGT), SVM C, Kleuren 2D

Project:
Constructeur: DNV GL - Energy
Model: Model 1.axs



[1]. Lineair, Co #1 (UGT), eY, Lijnen

| |
|---------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #1 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : eY [mm] |

Project:

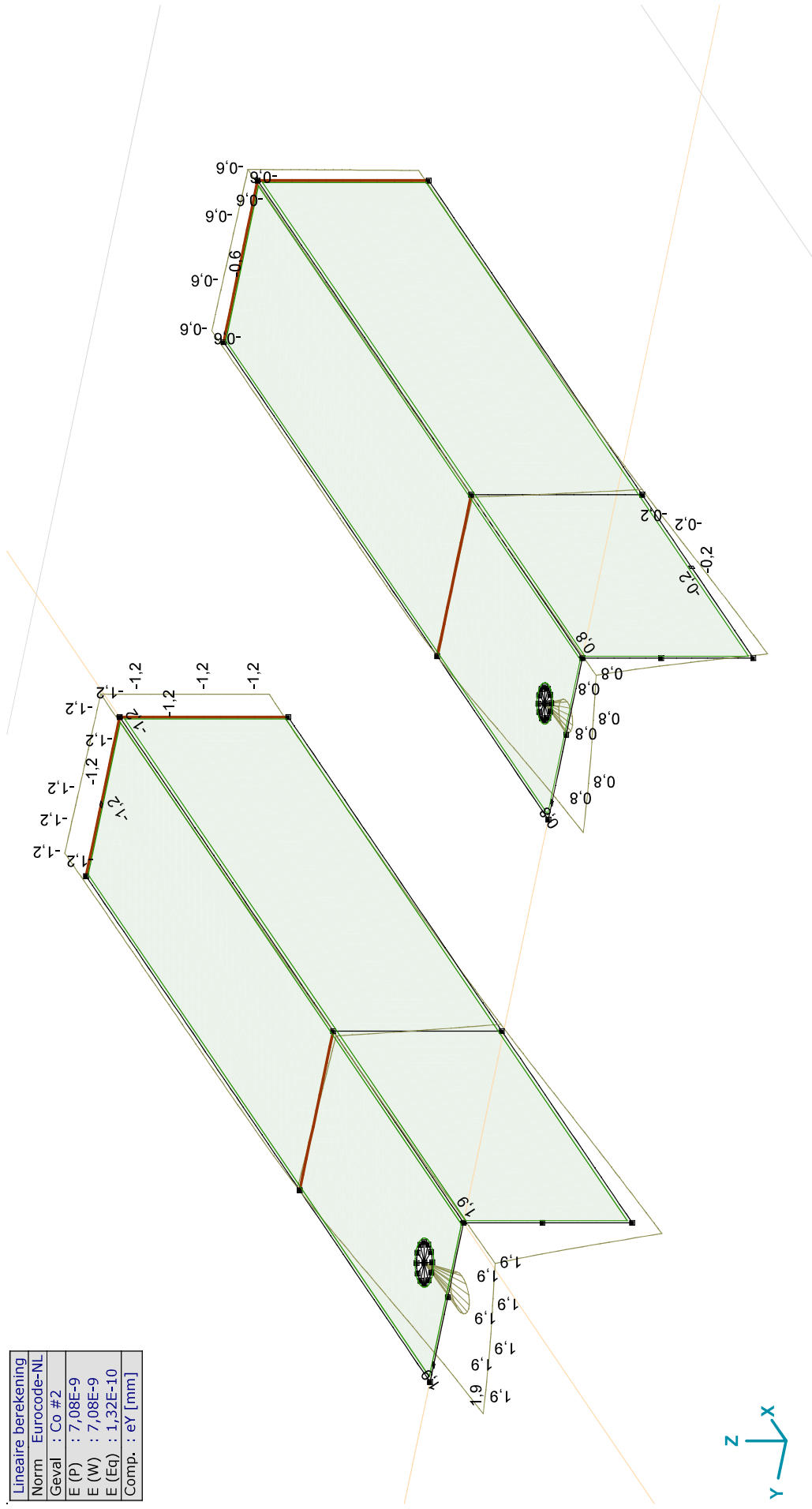
Constructeur: DNV GL - Energy

Model: **Model 1.axis**

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| |
|---------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #2 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : eY [mm] |



[1]. Lineair, Co #2 (UGT), eY, Lijnen

Project:

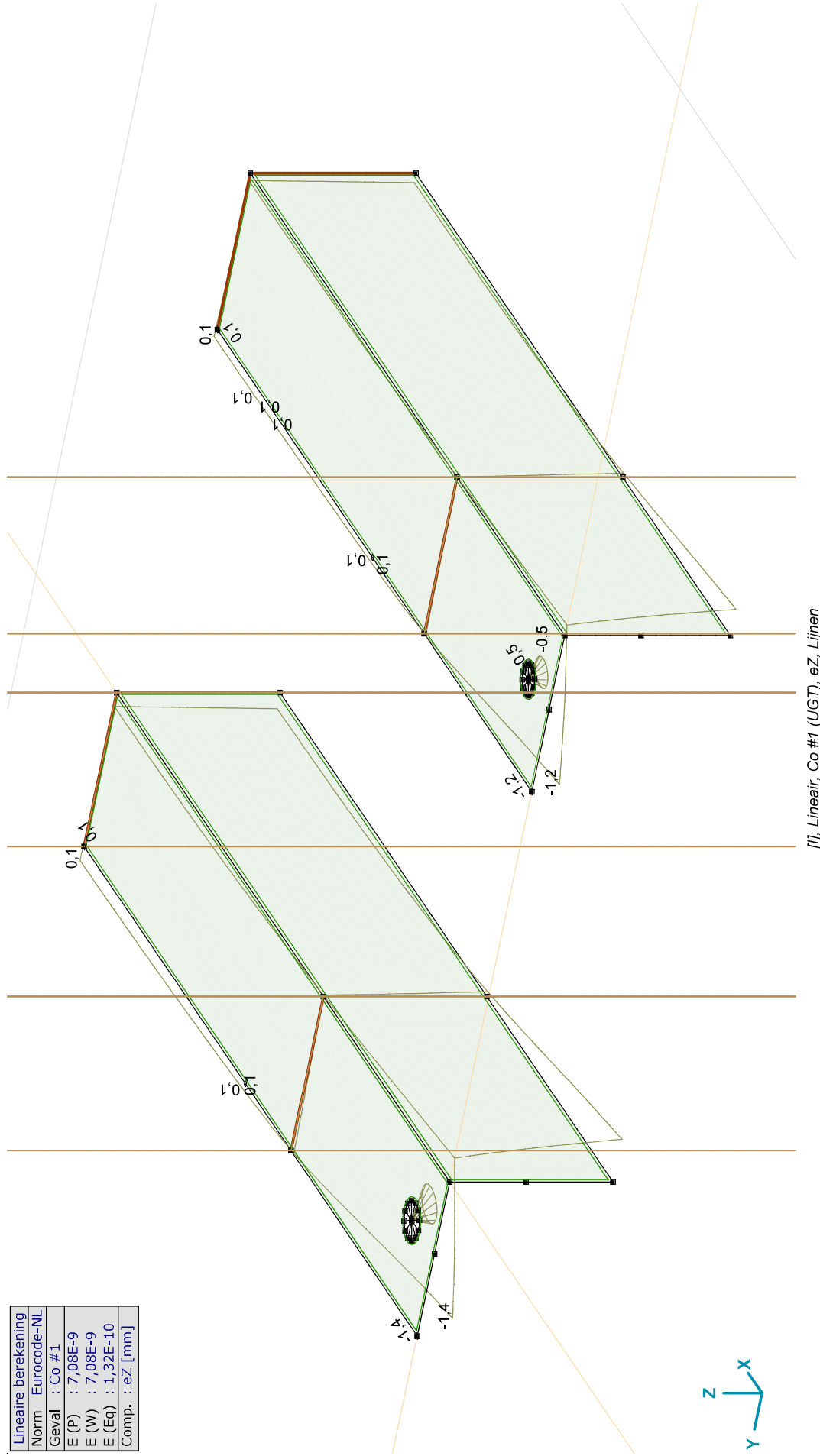
Constructeur: DNV GL - Energy

Model: Model 1.axis

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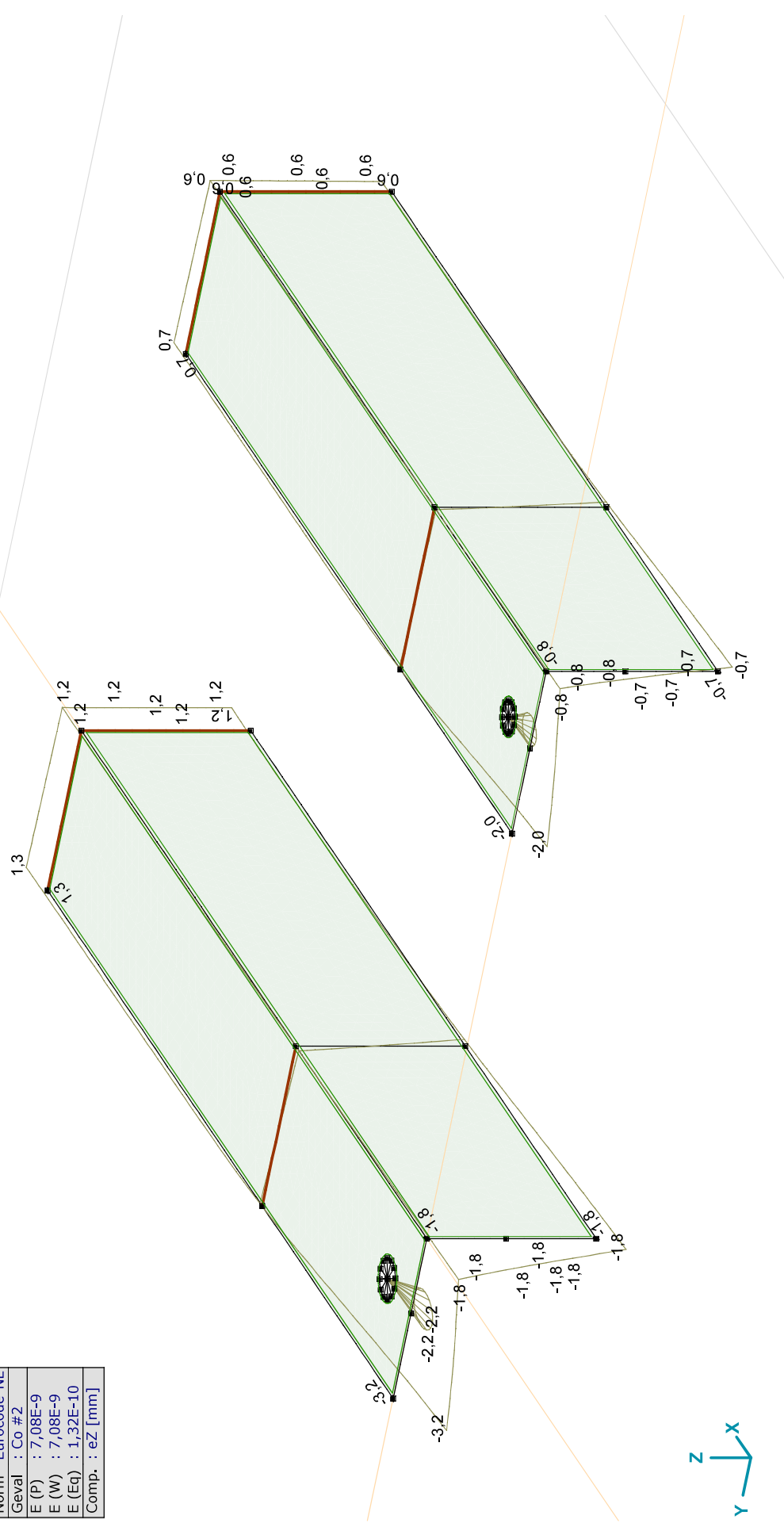
| | |
|---------------------|-------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Co #1 |
| E (P) | : 7,08E-9 |
| E (W) | : 7,08E-9 |
| E (Eq) | : 1,32E-10 |
| Comp. | : eZ [mm] |



[[I]. Lineair, Co #1 (UGT), eZ, Lijnen

Project:
Constructureur: DNV GL - Energy
Model: **Model 1.axis**

| | |
|---------------------|-------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | Co #2 |
| E (P) | : 7,08E-9 |
| E (W) | : 7,08E-9 |
| E (Eq) | : 1,32E-10 |
| Comp. | : eZ [mm] |



[[J]. Lineair, Co #2 (UGT), eZ, Lijnen

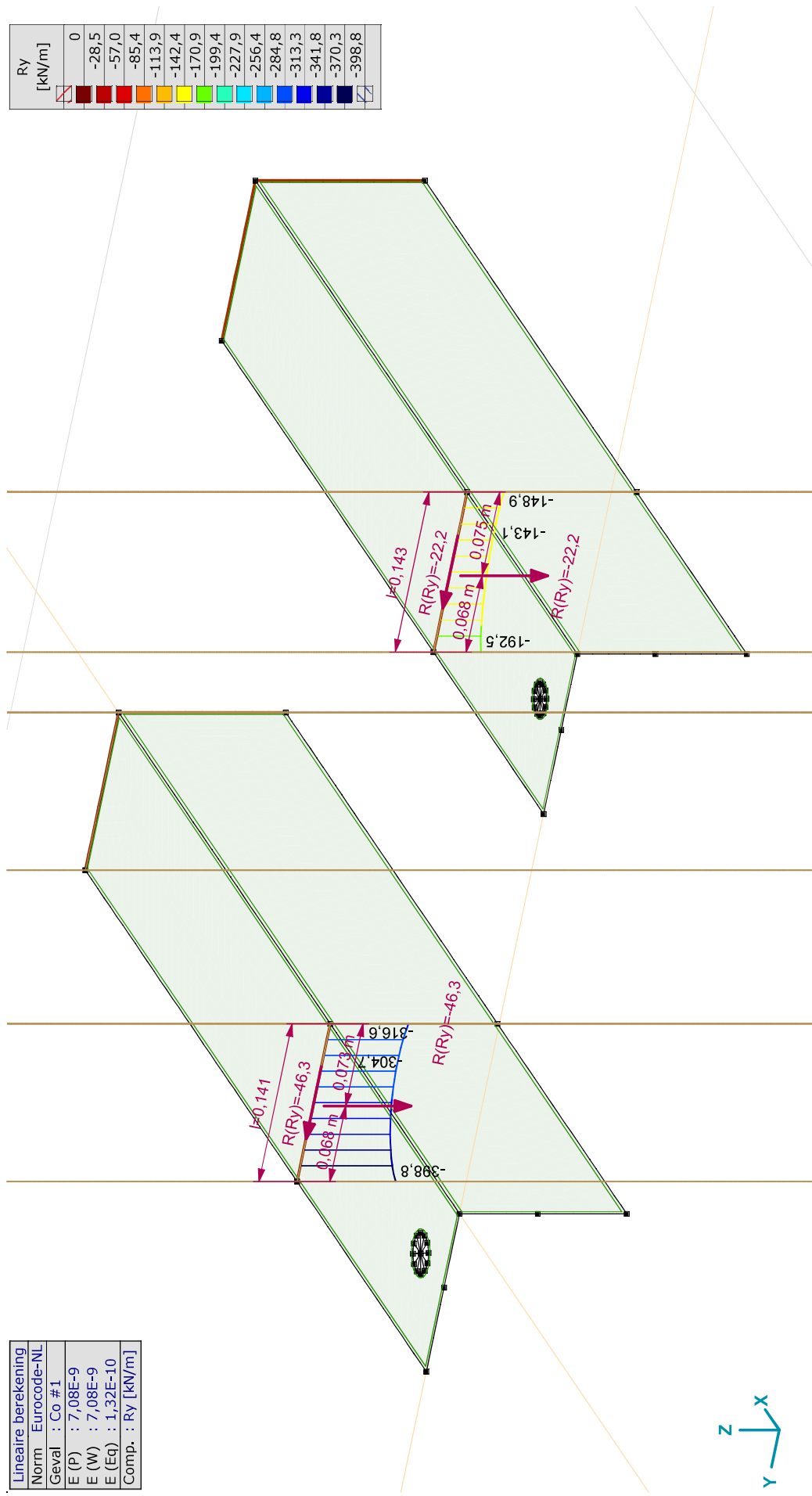
Project:
 Constructeur: DNV GL - Energy
 Model: Model 1.axs

21-2-2021

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| |
|---------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #1 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : Ry [kN/m] |

| | |
|-----------|--------|
| Ry [kN/m] | 0 |
| | -28,5 |
| | -57,0 |
| | -85,4 |
| | -113,9 |
| | -142,4 |
| | -170,9 |
| | -199,4 |
| | -227,9 |
| | -256,4 |
| | -284,8 |
| | -313,3 |
| | -341,8 |
| | -370,3 |
| | -398,8 |



III. Lineair, Co #1 (UGT), Ry (lijnopp.), Doorsnedelij

Project:

Constructeur: DNV GL - Energy

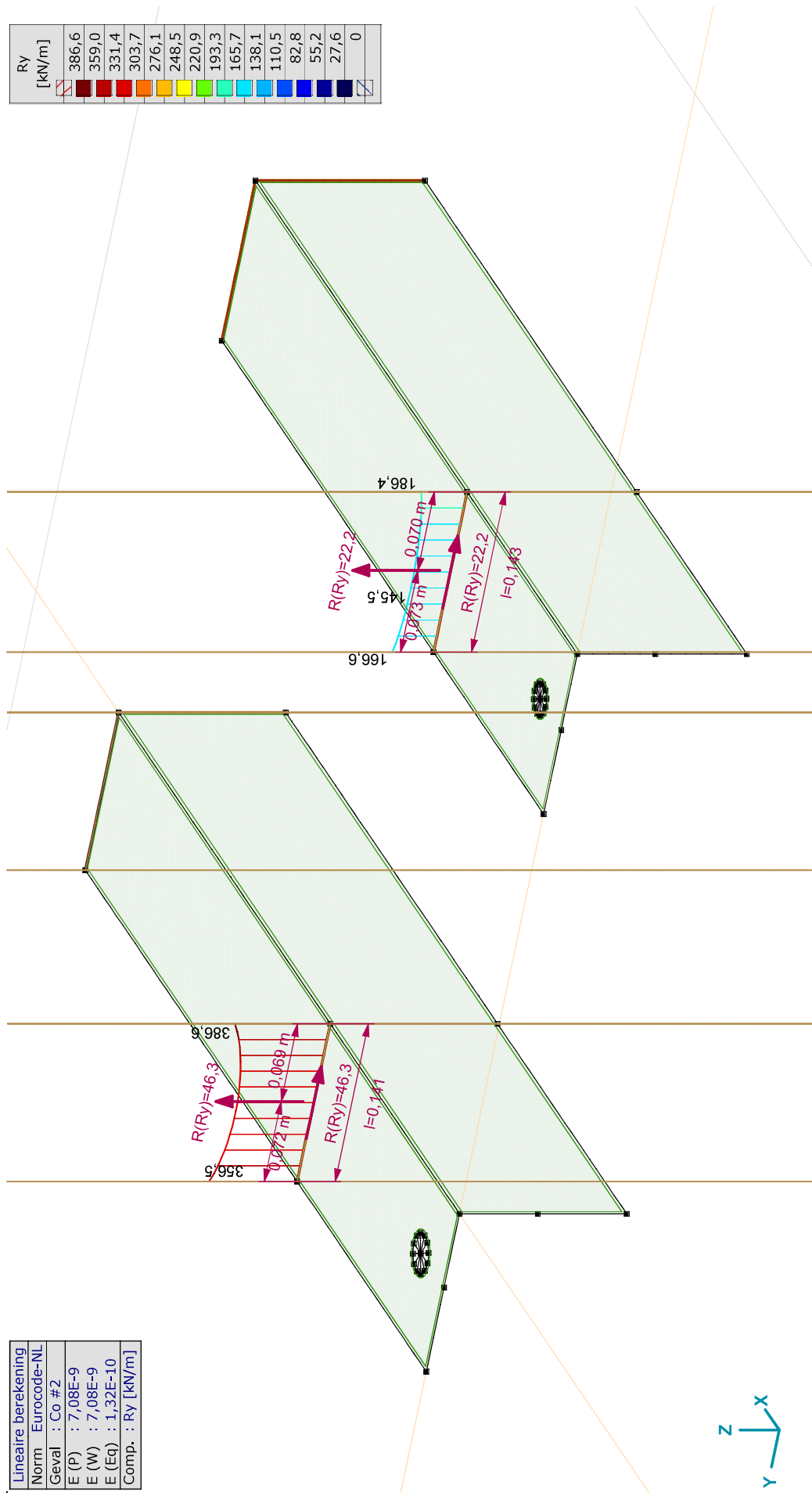
Model: **Model 1.axis**

21-2-2021

Pag. 24

| | |
|---------------------|-------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Co. #2 |
| E (P) | : 7,08E-9 |
| E (W) | : 7,08E-9 |
| E (Eq) | : 1,32E-10 |
| Comp. | : Ry [kN/m] |

| | |
|-----------|--|
| Ry [kN/m] | |
| 386,6 | |
| 359,0 | |
| 331,4 | |
| 303,7 | |
| 276,1 | |
| 248,5 | |
| 220,9 | |
| 193,3 | |
| 165,7 | |
| 138,1 | |
| 110,5 | |
| 82,8 | |
| 55,2 | |
| 27,6 | |
| 0 | |



III. Lineair, Co #2 (UGT), Ry (lijnopp.), Doorsnedelij

Project:

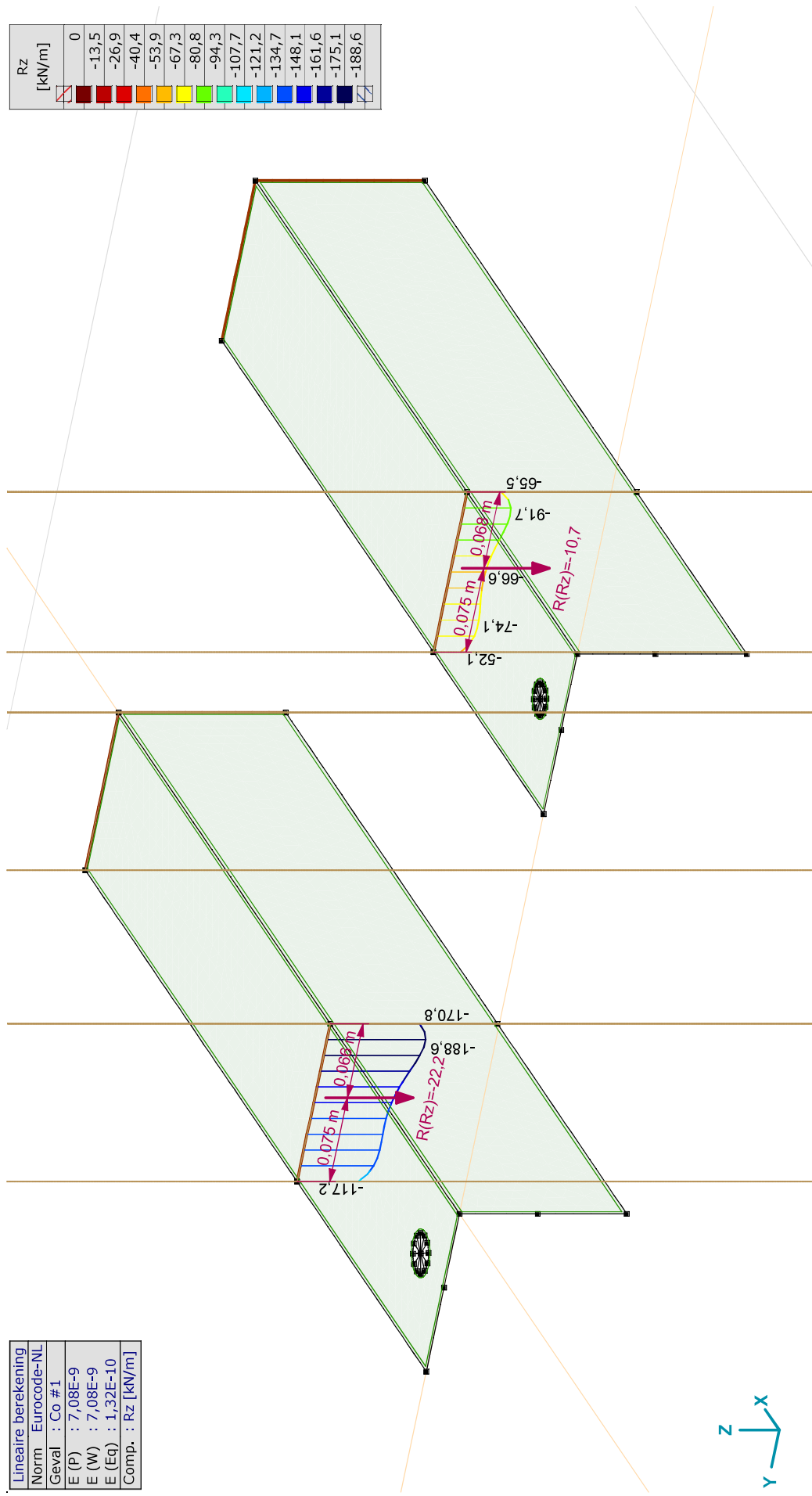
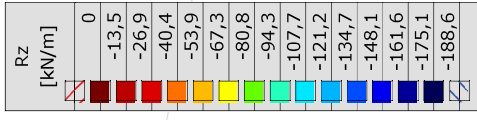
Constructeur: DNV GL - Energy

Model: **Model 1.axis**

21-2-2021

Pag. 25

| |
|---------------------|
| Lineaire berekening |
| Norm Eurocode-NL |
| Geval : Co #1 |
| E (P) : 7,08E-9 |
| E (W) : 7,08E-9 |
| E (Eq) : 1,32E-10 |
| Comp. : Rz [kN/m] |



III. Lineair, Co #1 (UGT), Rz (lijnopp.), DoorsnedeIijn

Project:

Constructeur: DNV GL - Energy

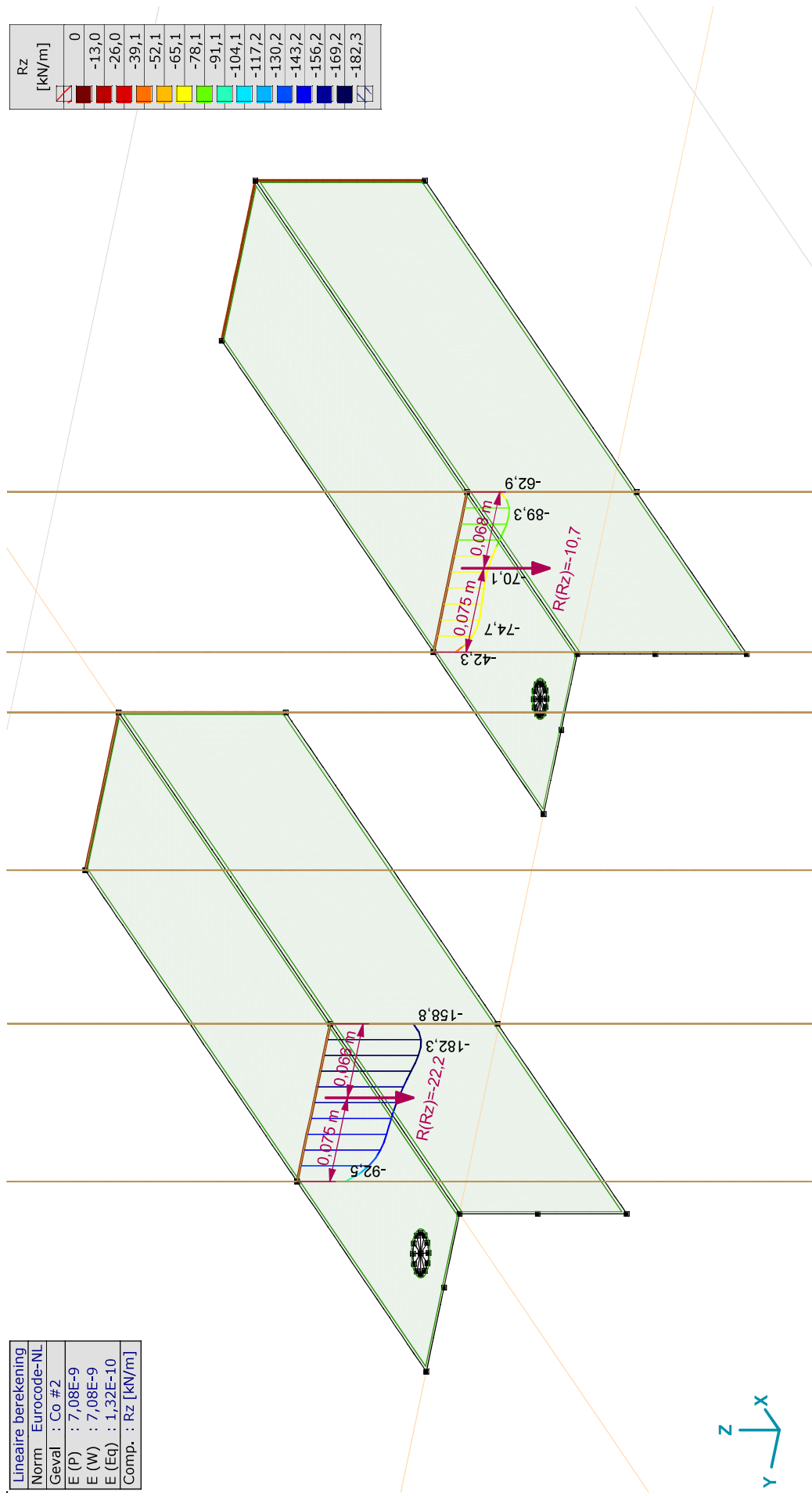
Model: **Model 1.axis**

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| | |
|---------------------|-------------|
| Lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Co #2 |
| E (P) | : 7,08E-9 |
| E (W) | : 7,08E-9 |
| E (Eq) | : 1,32E-10 |
| Comp. | : Rz [kN/m] |

| | |
|-----------|--------|
| Rz [kN/m] | 0 |
| | -13,0 |
| | -26,0 |
| | -39,1 |
| | -52,1 |
| | -65,1 |
| | -78,1 |
| | -91,1 |
| | -104,1 |
| | -117,2 |
| | -130,2 |
| | -143,2 |
| | -156,2 |
| | -169,2 |
| | -182,3 |



III. Lineair, Co #2 (UGT), Rz (lijnopp.), Doorsnedelij

Project: RLL-TBG
 Mast: HA+0_c

Steel beams in torsion
Calculation of unrestrained beams with eccentric load

Datum: 2021-02-22
 Auteur: MRE
 Versie: 1.1

| Load | | Beam 1 | Beam 2 | Beam 3 | Beam 4 | |
|--|---------------------------------------|---------------|---------------|---------------|---------------|-----------------------------------|
| Force on insulator | | 6.88 | | | | kN |
| Angle of insulator (to vertical) | | 54 | | | | ° |
| Horizontal force in direction of Horizontal force | F _h | 5.6 | | | | kN |
| Vertical force | F _v | 4.0 | | | | kN |
| Eccentricity of force (below beam) | e | 3375 | | | | mm |
| Torsional moment | T | 19.4 | | | | kNm |
| Beams | | | | | | |
| Beam length | L | 1820 | | | | mm |
| Yield stress | f _y | 355 | | | | Mpa |
| Elastic modulus | E | 210000 | | | | Mpa |
| Shear modulus | G | 81000 | | | | Mpa |
| Profile | | HEB 220 | | | | |
| | | HEB220 | | | | |
| Height | h | 220 | | | | mm |
| Width | b | 220 | | | | mm |
| Web thickness | t _w | 9.5 | | | | mm |
| Flange thickness | t _f | 16.0 | | | | mm |
| Torsional constant | I _t | 77 | | | | · 10 ⁴ mm ⁴ |
| Warping constant | I _{wa} | 295418 | | | | · 10 ⁶ mm ⁶ |
| Moment of inertia | I _y | 8091 | | | | · 10 ⁴ mm ⁴ |
| | I _z | 2843 | | | | · 10 ⁴ mm ⁴ |
| Flange stiffness | I _f = I _z / 2 = | 1422 | | | | mm ³ |
| Moment of resistance | W _{y,el} | 736 | | | | · 10 ³ mm ³ |
| | W _{z,el} | 258 | | | | · 10 ³ mm ³ |
| Torsional bending constant | d | 997 | | | | mm |
| | L/d | 1.8 | | | | |
| | a | 0.5 | | | | |

Calculation of second derivative of angular deflection φ'':

$$\begin{aligned}
 A &= T / (G \cdot I_t \cdot d) = && 3.12E-07 \\
 B &= \sinh(\alpha \cdot L / d) = && 1.04E+00 \\
 C &= \tanh(L/d) = && 9.49E-01 \\
 D &= \cosh(\alpha \cdot L / d) = && 1.45E+00 \\
 F &= \sinh(0.5 \cdot L / d) = && 1.04E+00 \\
 H &= (B / C - D) \cdot F = && -3.61E-01 \\
 X &= A \cdot H = && -1.13E-07 \\
 \\
 Y &= X \cdot G \cdot I_t \cdot d / T = && -3.61E-01 \\
 \phi'' &= Y \cdot T / (G \cdot I_t \cdot d) = && -1.13E-07 \quad \text{rad/mm}^2
 \end{aligned}$$

Project: RLL-TBG
 Mast: HA+0_c

Steel beams in torsion
Calculation of unrestrained beams with eccentric load

Datum: 2021-02-22
 Auteur: MRE
 Versie: 1.1

Acting moments:

| | | |
|---|------|------------|
| $M_{w,Ed} = E \cdot I_r \cdot (h \cdot t_f) \cdot \phi'' / 2 =$ | 34.3 | <i>kNm</i> |
| $M_{y,Ed} = 1/4 \cdot F \cdot L =$ | 1.8 | <i>kNm</i> |
| $M_{z,Ed} = 1/4 \cdot F \cdot L =$ | 2.5 | <i>kNm</i> |

Capacities of beams:

| | | |
|---------------------------------------|-------|------------|
| $M_{w,Rd} = W_{z,el} \cdot f_y / 2 =$ | 45.9 | <i>kNm</i> |
| $M_{y,Rd} = W_{y,el} \cdot f_y =$ | 261.1 | <i>kNm</i> |
| $M_{z,Rd} = W_{z,el} \cdot f_y =$ | 91.8 | <i>kNm</i> |

Combined check of beam:

UC 0,78

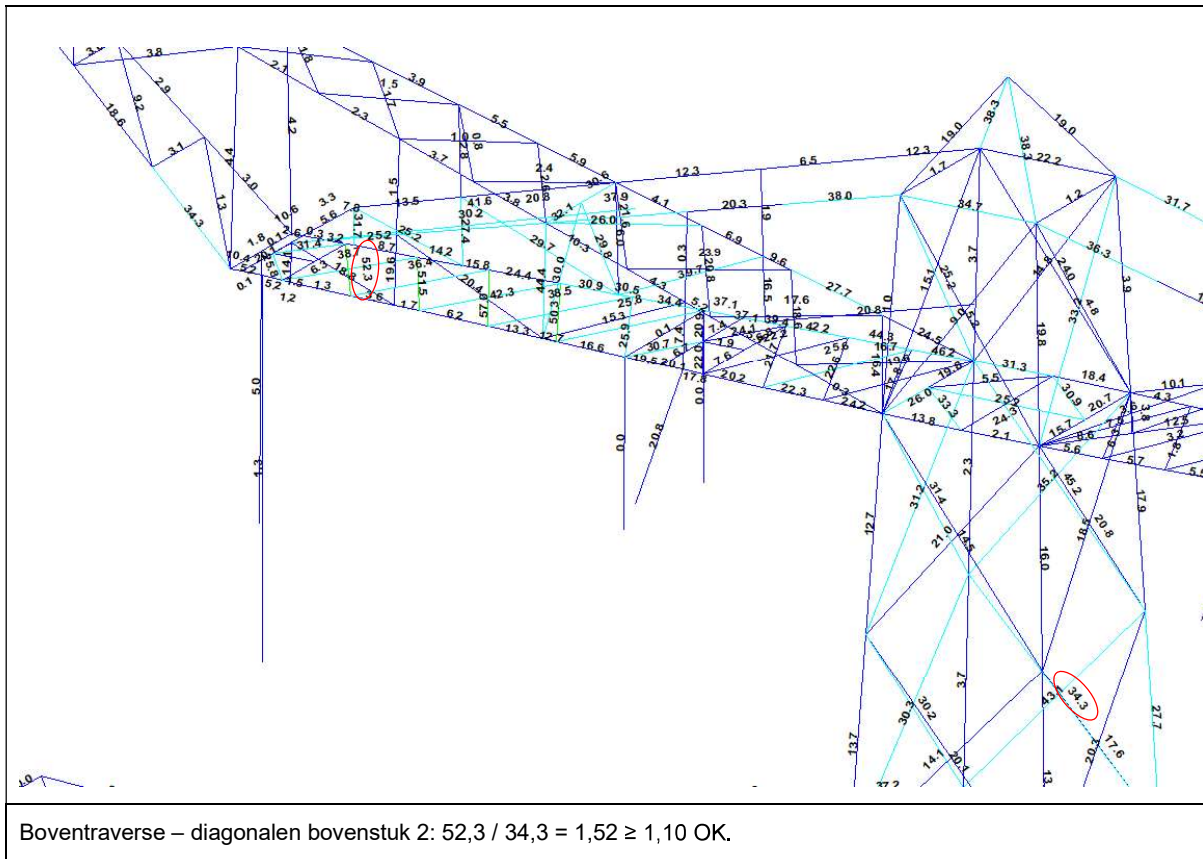
Displacements:

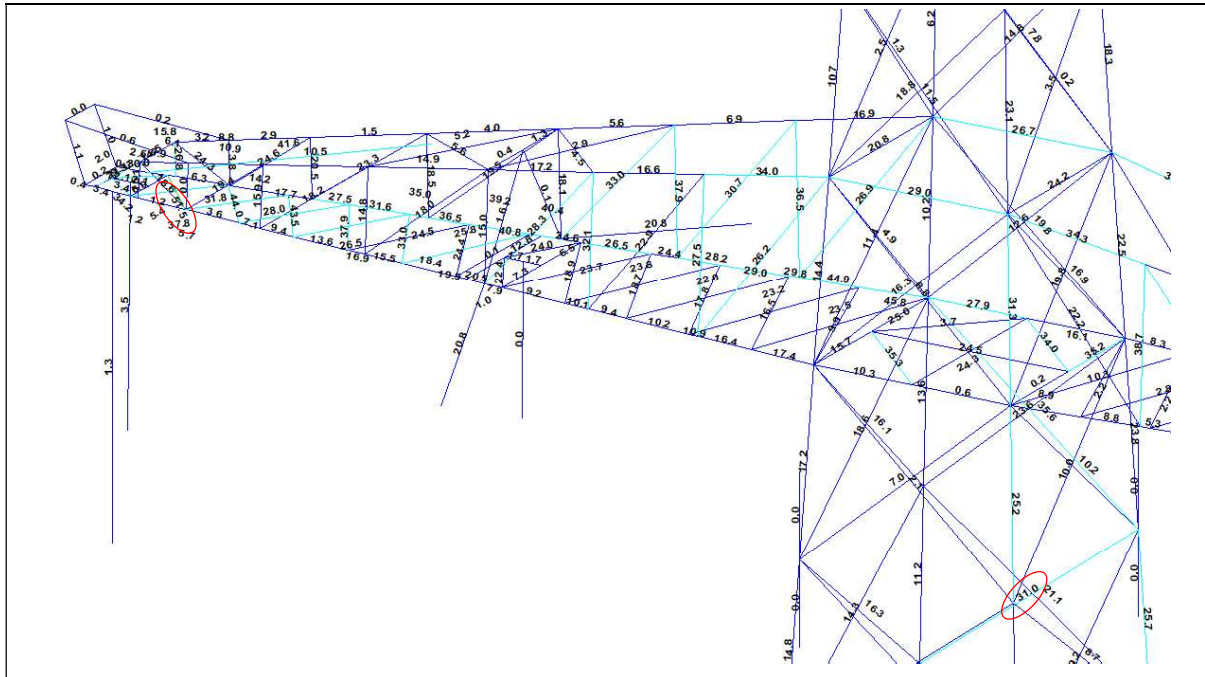
| | | | |
|--------------------------|-------|-------|-----------|
| Factor F_{ed} / F_k | | 1.2 | |
| Displacement y-direction | u_y | 0.02 | <i>mm</i> |
| Relative displacement | rel. | 73062 | - |
| Displacement z-direction | u_z | 0.10 | <i>mm</i> |
| Relative displacement | rel. | 18654 | - |

APPENDIX F

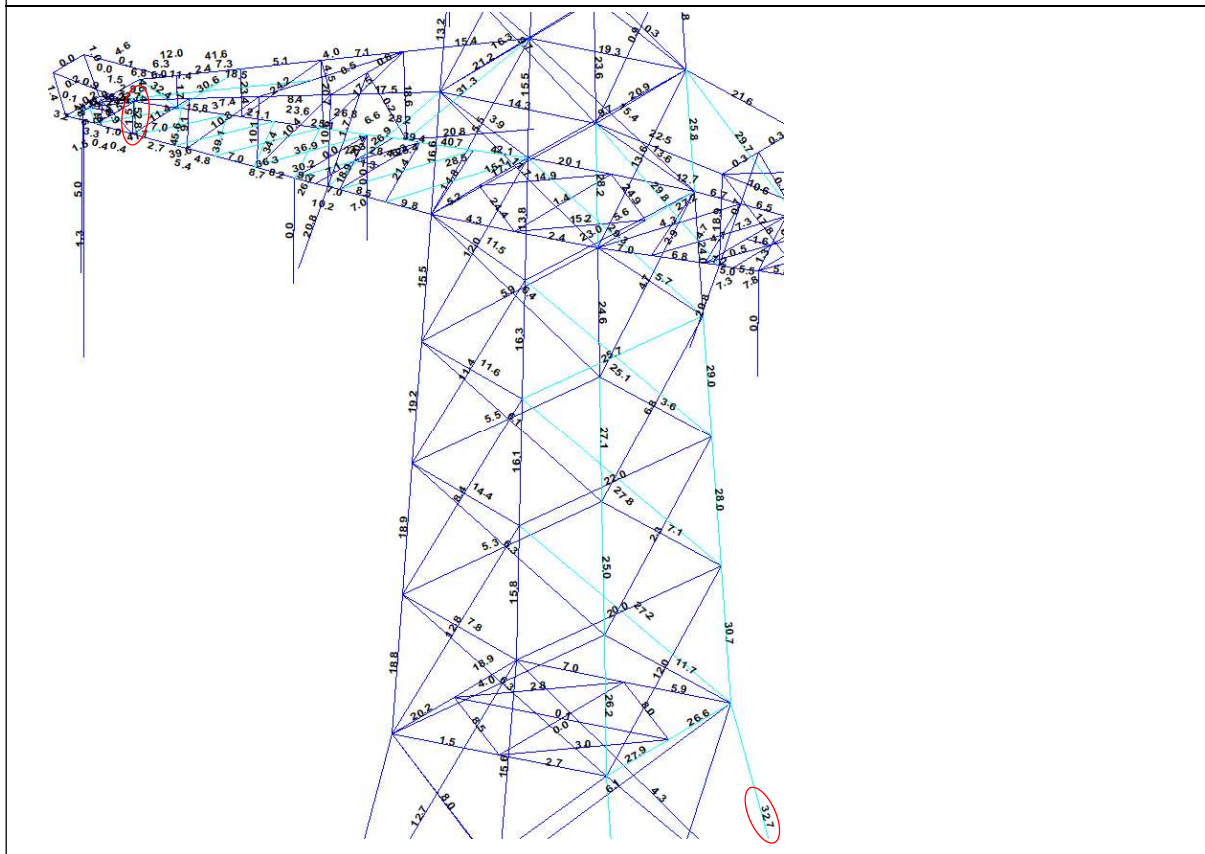
Sterkte-coördinatie

In 5.5.1 van het uitgangspuntenrapport is beschreven dat aan sterkte-coördinatie wordt voldaan als de U.C. van de staven in de traverse 10 procentpunt groter is dan de U.C. van de staven in het mastlichaam. Uitgangspunt is belastingcombinatie 5a, geleiderbreuk. In deze Appendix wordt getoetst of de U.C. van de staven in het mastlichaam voldoende laag is ten opzichte van de U.C. van de staven in de traverse.





Middentraverse – tussenschot: $51,5 / 31,0 = 1,66 \geq 1,10$ OK.



Ondertraverse: $52,8 / 32,7 = 1,61 \geq 1,10$ OK

APPENDIX G

Galloping

Uitgangspunten

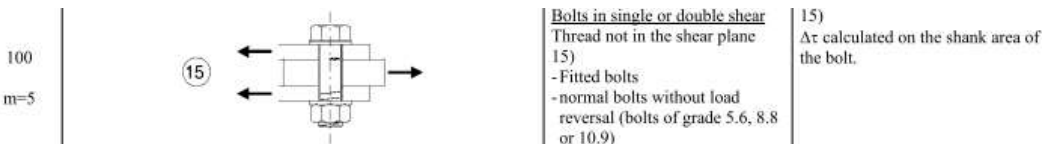
In het uitgangspuntendocument is beschreven dat wordt uitgegaan van een materiaalfactor voor vermoeiing $\gamma_{mf} = 1,15$. Dit komt overeen met de “Safe-life methode” met “Low consequence” van tabel 3.1 van NEN-EN 1993-1-9 of met “Damage tolerant” en “High consequence”.

| Assessment method | Consequence of failure | |
|-------------------|------------------------|------------------|
| | Low consequence | High consequence |
| Damage tolerant | 1,00 | 1,15 |
| Safe life | 1,15 | 1,35 |

Voor staven met gatverzwakking met bouten in ruime gaten geldt volgens fig. 8.1 van NEN-EN 1993-1-9 categorie 50, met $m=3$



Voor niet voorgespannen bouten belast op afschuiving geldt volgens fig. 8.1 van NEN-EN 1993-1-9 categorie 100, met $m=5$.



Het belastingspectrum is in de NNA (NEN-EN 50341-2-15) als volgt gedefinieerd.

Table 4.11/NL.1 Load spectra line galloping for tension supports

| Load spectra line galloping for tension supports | | Number of load cycles in 50 years | |
|--|-------------------|-----------------------------------|--------------|
| Number | Peak-to-peak load | Ice region A | Ice region B |
| 1 | 2·EDS | 7.000 | 3.000 |
| 2 | 1,5·EDS | 36.000 | 17.000 |
| 3 | 1,0·EDS | 125.000 | 65.000 |
| 4 | 0,5·EDS | 482.000 | 265.000 |

Aanpak

De vier belastingen van 0,5 tot 2,0EDS hebben een vaste onderlinge verhouding. Aangezien het aantal wisselingen zich in het $m=3$ gebied van de vermoeiingskromme bevindt vanwege $n < 2 \times 10^6$, kan een relatie worden afgeleid tussen de grootte van de spanningswissel met bijvoorbeeld 1,0EDS en de spanningswisseling die bij 2×10^6 wisselingen op basis van het spectrum nog net toelaatbaar is. Dit staat bekend als de equivalente spanningen methode. Via de factor lambda kan de spanningswisseling worden berekend.

$$\lambda = \left[\frac{\sum \Delta\sigma_i^m \cdot n_i}{2 \cdot 10^6} \right]^{\frac{1}{m}}$$

Toepassen van de formule voor een spanning van 1 N/mm² bij 1,0EDS levert:

| Helling Ijsgebied Wisseling | m=3 | | m=5 | |
|---|-------------------------|-------------------------|-------------------------|-------------------------|
| | A | B | A | B |
| | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ |
| 2,0EDS | 5,60E+04 | 2,40E+04 | 2,24E+05 | 9,60E+04 |
| 1,5EDS | 1,22E+05 | 5,74E+04 | 2,73E+05 | 1,29E+05 |
| 1,0EDS | 1,25E+05 | 6,50E+04 | 1,25E+05 | 6,50E+04 |
| 0,5EDS | 6,03E+04 | 3,31E+04 | 1,51E+04 | 8,28E+03 |
| $\Sigma \sigma_i^m \times n_i$ | 3,63E+05 | 1,80E+05 | 6,37E+05 | 2,98E+05 |
| $\lambda = (\Sigma \sigma_i n_i / 2 \times 10^6)^{1/m}$ | 0,57 | 0,45 | 0,80 | 0,68 |

Voor ijsgebied A is de toelaatbare spanningswisseling bij 1,0 EDS en 125.000 wisselingen dus 1/0,57 (175%) van de toelaatbare spanningswisseling bij een aantal wisselingen van $2,0 \times 10^6$. Er kan ook worden gesteld dat als de spanningswisselingen van 1,0 EDS 363.000 maal voorkomen, dezelfde schade wordt behaald als de vier niveaus afzonderlijk. Deze aanpak is gehanteerd.

- In de berekening van de mast wordt telkens één afspanpunt van de geleiders belast met een trekkracht in lijnrichting van 1,0 EDS.
- Het aantal wisselingen dat deze trekkracht voorkomt wordt vergroot om het hele spectrum te vervangen, dit is afhankelijk van ijsgebied en m-factor.
- Voor iedere staaf in de constructie wordt de schade berekend als gevolg van de trekkracht voor elke geleider.
- De schade wordt gesommeerd over alle geleiders.
- De toetsing is uitgedrukt als de verhouding tussen de optredende spanningswisseling bij $n = 2 \times 10^6$ wisselingen en de toelaatbare spanningswisseling (43 MPa voor het staalprofiel en 87 MPa voor de bout).

Resultaten

In de tabellen zijn de resultaten van mast HC+0/c gegeven. Vanwege de exponentiële invloed van het spanningsniveau heeft de verdeling van de U.C.'s een grote variatie. Het meest zwaar belast zijn de diagonalen in het ondervlak van de traverse in de nabijheid van de afspanpunten en de randen van de traverse. De conclusie is dat de staven en bouten voldoen.



Check galloping- 120gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | | | | | | Controle boutdoorsnede | | | | |
|-------|-----------------|----------------------|---------------|------|----------------------------------|--------------|-------------|------------|------------|--------|--------------|-----------|-----------------|--------------|------------------------|--------|---------|--|--|
| | | | | | ΔF;0 [kN] | Brutto [mm2] | Netto [mm2] | Δσ;0 [Mpa] | DC;0 [Mpa] | Δσ;c;0 | UC opp. [kN] | ΔF;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b | UC bout | | |
| 100 | Main leg | 80x80x8 | 2 | M20 | 15.2 | 1230 | 1054 | 14.4 | 50 | 43 | 0.33 | 23.1 | 314 | 36.8 | 100 | 87 | 0.42 | | |
| 101 | Main leg | 130x130x12 | 4 | M24 | 25.2 | 3000 | 2688 | 9.4 | 50 | 43 | 0.22 | 38.0 | 452 | 21.0 | 100 | 87 | 0.24 | | |
| 102 | Main leg | 180x180x16 | 8 | M24 | 33.1 | 5540 | 5124 | 6.5 | 50 | 43 | 0.15 | 48.4 | 452 | 13.4 | 100 | 87 | 0.15 | | |
| 103 | Main leg | 180x180x16 | 8 | M24 | 63.3 | 5540 | 5124 | 12.4 | 50 | 43 | 0.28 | 89.5 | 452 | 24.8 | 100 | 87 | 0.28 | | |
| 104 | Main leg | 180x180x16 | 10 | M24 | 87.8 | 5540 | 5124 | 17.1 | 50 | 43 | 0.39 | 125.1 | 452 | 27.7 | 100 | 87 | 0.32 | | |
| 105 | Main leg | 250x250x24 | 10 | M24 | 123.2 | 11492 | 10868 | 11.3 | 50 | 43 | 0.26 | 179.9 | 452 | 39.8 | 100 | 87 | 0.46 | | |
| 106 | Main leg | 250x250x24 | 0 | | 149.9 | 11492 | 11492 | 13.0 | 50 | 43 | 0.30 | 217.7 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 107 | Main leg | 250x250x24 | 16 | M24 | 162.5 | 11492 | 10868 | 15.0 | 50 | 43 | 0.34 | 231.0 | 452 | 31.9 | 100 | 87 | 0.37 | | |
| 108 | Main leg | 200x200x24 | 32 | M24 | 191.3 | 9060 | 8436 | 22.7 | 50 | 43 | 0.52 | 267.6 | 452 | 18.5 | 100 | 87 | 0.21 | | |
| 109 | Main leg | 200x200x24 | 20 | M24 | 209.4 | 9060 | 8436 | 24.8 | 50 | 43 | 0.57 | 290.8 | 452 | 32.2 | 100 | 87 | 0.37 | | |
| 110 | Main leg | 250x250x24 | 24 | M24 | 229.1 | 11492 | 10868 | 21.1 | 50 | 43 | 0.48 | 315.4 | 452 | 29.1 | 100 | 87 | 0.33 | | |
| 111 | Main leg | 250x250x24 | 32 | M24 | 241.4 | 11492 | 10868 | 22.2 | 50 | 43 | 0.51 | 328.5 | 452 | 22.7 | 100 | 87 | 0.26 | | |
| 112 | Main leg | 250x250x24 | 32 | M24 | 244.0 | 11492 | 10868 | 22.5 | 50 | 43 | 0.52 | 327.6 | 452 | 22.6 | 100 | 87 | 0.26 | | |
| 113 | Main leg | 250x250x24 | 0 | | 220.2 | 11492 | 11492 | 19.2 | 50 | 43 | 0.44 | 291.5 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 114 | Main leg | 250x250x24 | 24 | M24 | 219.6 | 11492 | 10868 | 20.2 | 50 | 43 | 0.46 | 290.6 | 452 | 26.8 | 100 | 87 | 0.31 | | |
| 200 | Diag front face | 100x100x10 | 2 | M24 | 19.6 | 1920 | 1660 | 11.8 | 50 | 43 | 0.27 | 29.8 | 452 | 33.0 | 100 | 87 | 0.38 | | |
| 201 | Diag front face | 150x150x14 | 6 | M24 | 111.6 | 4014 | 3650 | 30.6 | 50 | 43 | 0.70 | 168.5 | 452 | 62.1 | 100 | 87 | 0.71 | | |
| 202 | Diag front face | 150x150x14 | 5 | M24 | 93.5 | 4014 | 3650 | 25.6 | 50 | 43 | 0.59 | 141.1 | 452 | 62.4 | 100 | 87 | 0.72 | | |
| 203 | Diag front face | 150x150x14 | 5 | M24 | 76.8 | 4014 | 3650 | 21.0 | 50 | 43 | 0.48 | 115.7 | 452 | 51.2 | 100 | 87 | 0.59 | | |
| 204 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 107.1 | 5500 | 5188 | 20.7 | 50 | 43 | 0.47 | 152.4 | 452 | 84.3 | 100 | 87 | 0.97 | | |
| 205 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 93.1 | 5500 | 5188 | 17.9 | 50 | 43 | 0.41 | 132.5 | 452 | 73.3 | 100 | 87 | 0.84 | | |
| 206 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 81.6 | 5500 | 5188 | 15.7 | 50 | 43 | 0.36 | 113.8 | 452 | 62.9 | 100 | 87 | 0.72 | | |
| 207 | Diag front face | 130x130x12#(15,0,33) | 4 | M24 | 82.0 | 6040 | 5728 | 14.3 | 50 | 43 | 0.33 | 108.6 | 452 | 60.1 | 100 | 87 | 0.69 | | |
| 208 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 72.9 | 5500 | 5188 | 14.0 | 50 | 43 | 0.32 | 96.4 | 452 | 53.3 | 100 | 87 | 0.61 | | |
| 209 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 67.0 | 5500 | 5188 | 12.9 | 50 | 43 | 0.30 | 88.1 | 452 | 48.7 | 100 | 87 | 0.56 | | |
| 210 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 65.3 | 5500 | 5188 | 12.6 | 50 | 43 | 0.29 | 85.7 | 452 | 47.4 | 100 | 87 | 0.54 | | |
| 211 | Diag front face | 150x150x12(12,0,33) | 3 | M24 | 54.4 | 6970 | 6658 | 8.2 | 50 | 43 | 0.19 | 72.3 | 452 | 53.3 | 100 | 87 | 0.61 | | |
| 212 | Diag front face | 130x130x12#(15,0,33) | 3 | M24 | 39.7 | 6040 | 5728 | 6.9 | 50 | 43 | 0.16 | 52.6 | 452 | 38.8 | 100 | 87 | 0.45 | | |
| 213 | Diag front face | 150x150x12(12,0,33) | 5 | M24 | 38.7 | 6970 | 6658 | 5.8 | 50 | 43 | 0.13 | 51.2 | 452 | 22.7 | 100 | 87 | 0.26 | | |
| 300 | Diag side face | 80x80x8 | 2 | M24 | 14.8 | 1230 | 1022 | 14.5 | 50 | 43 | 0.33 | 22.6 | 452 | 25.0 | 100 | 87 | 0.29 | | |
| 301 | Diag side face | 150x150x14 | 6 | M24 | 105.7 | 4014 | 3650 | 29.0 | 50 | 43 | 0.67 | 159.7 | 452 | 58.9 | 100 | 87 | 0.68 | | |
| 302 | Diag side face | 150x150x14 | 5 | M24 | 88.9 | 4014 | 3650 | 24.4 | 50 | 43 | 0.56 | 134.3 | 452 | 59.4 | 100 | 87 | 0.68 | | |
| 303 | Diag side face | 150x150x14 | 4 | M24 | 74.5 | 4014 | 3650 | 20.4 | 50 | 43 | 0.47 | 112.5 | 452 | 62.2 | 100 | 87 | 0.72 | | |
| 304 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 93.5 | 5500 | 5188 | 18.0 | 50 | 43 | 0.41 | 129.5 | 452 | 71.6 | 100 | 87 | 0.82 | | |
| 305 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 82.0 | 5500 | 5188 | 15.8 | 50 | 43 | 0.36 | 113.5 | 452 | 62.8 | 100 | 87 | 0.72 | | |



Check galloping- 120gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | Controle boutdoorsnede | | | | | | | |
|-------|------------------------------|----------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|------------------------|--------------|-----------|-----------------|--------------|------------|--------------|---------|
| | | | | | ΔF;o [kN] | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. [kN] | ΔF;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b [Mpa] | UC bout |
| 306 | Diag side face | 120x120x12(12,0.33) | 4 | M24 | 75.7 | 5500 | 5188 | 14.6 | 50 | 43 | 0.34 | 104.3 | 452 | 57.7 | 100 | 87 | 0.66 |
| 307 | Diag side face | 130x130x12#(15,0.33) | 4 | M24 | 82.8 | 6040 | 5728 | 14.5 | 50 | 43 | 0.33 | 109.5 | 452 | 60.6 | 100 | 87 | 0.70 |
| 308 | Diag side face | 120x120x12(12,0.33) | 4 | M24 | 75.7 | 5500 | 5188 | 14.6 | 50 | 43 | 0.34 | 100.2 | 452 | 55.4 | 100 | 87 | 0.64 |
| 309 | Diag side face | 120x120x12(12,0.33) | 4 | M24 | 72.1 | 5500 | 5188 | 13.9 | 50 | 43 | 0.32 | 95.4 | 452 | 52.8 | 100 | 87 | 0.61 |
| 310 | Diag side face | 120x120x12(12,0.33) | 4 | M24 | 68.1 | 5500 | 5188 | 13.1 | 50 | 43 | 0.30 | 90.1 | 452 | 49.8 | 100 | 87 | 0.57 |
| 311 | Diag side face | 150x150x12(12,0.33) | 3 | M24 | 63.3 | 6970 | 6658 | 9.5 | 50 | 43 | 0.22 | 84.4 | 452 | 62.3 | 100 | 87 | 0.72 |
| 312 | Diag side face | 130x130x12#(15,0.33) | 3 | M24 | 47.8 | 6040 | 5728 | 8.3 | 50 | 43 | 0.19 | 63.6 | 452 | 46.9 | 100 | 87 | 0.54 |
| 313 | Diag side face | 150x150x12(12,0.33) | 5 | M24 | 45.6 | 6970 | 6658 | 6.8 | 50 | 43 | 0.16 | 60.7 | 452 | 26.9 | 100 | 87 | 0.31 |
| 400 | Horizontal lower ca. | 180x180x16 | 10 | M24 | 74.6 | 5540 | 5124 | 14.6 | 50 | 43 | 0.33 | 113.6 | 452 | 25.1 | 100 | 87 | 0.29 |
| 401 | Lower chord lower ca. | 150x150x14 | 10 | M24 | 147.2 | 4014 | 3650 | 40.3 | 50 | 43 | 0.93 | 224.0 | 452 | 49.6 | 100 | 87 | 0.57 |
| 402 | Lower chord lower ca. | 150x150x14 | 0 | | 131.4 | 4014 | 4014 | 32.7 | 50 | 43 | 0.75 | 200.6 | 0 | 0.0 | 100 | 87 | 0.00 |
| 403 | Lower chord lower ca. | 150x150x14 | 0 | | 120.4 | 4014 | 4014 | 30.0 | 50 | 43 | 0.69 | 183.8 | 0 | 0.0 | 100 | 87 | 0.00 |
| 404 | Lower chord lower ca. | 150x150x14 | 0 | | 93.9 | 4014 | 4014 | 23.4 | 50 | 43 | 0.54 | 143.4 | 0 | 0.0 | 100 | 87 | 0.00 |
| 405 | Lower chord lower ca. | 150x150x14 | 0 | | 57.3 | 4014 | 4014 | 14.3 | 50 | 43 | 0.33 | 87.5 | 0 | 0.0 | 100 | 87 | 0.00 |
| 406 | Lower chord lower ca. | 150x150x14 | 0 | | 41.9 | 4014 | 4014 | 10.4 | 50 | 43 | 0.24 | 63.9 | 0 | 0.0 | 100 | 87 | 0.00 |
| 410 | Horizontal lower ca. | 130x130x12 | 3 | M24 | 21.5 | 3000 | 2688 | 8.0 | 50 | 43 | 0.18 | 32.5 | 452 | 24.0 | 100 | 87 | 0.28 |
| 411 | Horizontal lower ca. | 150x150x14 (not coup | 2 | M24 | 11.6 | 8028 | 7664 | 1.5 | 50 | 43 | 0.03 | 17.7 | 452 | 19.6 | 100 | 87 | 0.23 |
| 412 | Horizontal lower ca. | HEA140 | 0 | | 0.9 | 3140 | 3140 | 0.3 | 50 | 43 | 0.01 | 1.3 | 0 | 0.0 | 100 | 87 | 0.00 |
| 413 | Horizontal lower ca. | 150x150x18 (not coup | 2 | M24 | 23.4 | 10200 | 9732 | 2.4 | 50 | 43 | 0.06 | 35.8 | 452 | 39.6 | 100 | 87 | 0.46 |
| 414 | Beam lower ca. | HEB220 | 0 | | 1.8 | 9104 | 9104 | 0.2 | 50 | 43 | 0.00 | 2.8 | 0 | 0.0 | 100 | 87 | 0.00 |
| 415 | Horizontal lower ca. | UNP220 | 0 | | 4.6 | 3740 | 3740 | 1.2 | 50 | 43 | 0.03 | 7.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 426 | Upper chord lower ca. | 120x120x12 | 4 | M24 | 14.7 | 2750 | 2438 | 6.0 | 50 | 43 | 0.14 | 22.2 | 452 | 12.3 | 100 | 87 | 0.14 |
| 427 | Upper chord lower ca. | 120x120x12 | 0 | | 14.1 | 2750 | 2750 | 5.1 | 50 | 43 | 0.12 | 21.3 | 0 | 0.0 | 100 | 87 | 0.00 |
| 428 | Upper chord lower ca. | 120x120x12 | 0 | | 14.2 | 2750 | 2750 | 5.2 | 50 | 43 | 0.12 | 21.6 | 0 | 0.0 | 100 | 87 | 0.00 |
| 429 | Upper chord lower ca. | 120x120x12 | 0 | | 15.1 | 2750 | 2750 | 5.5 | 50 | 43 | 0.13 | 22.9 | 0 | 0.0 | 100 | 87 | 0.00 |
| 430 | Upper chord lower ca. | 120x120x12 | 2 | M20 | 15.2 | 2750 | 2486 | 6.1 | 50 | 43 | 0.14 | 23.0 | 314 | 36.6 | 100 | 87 | 0.42 |
| 431 | Upper chord lower ca. | 120x120x12 | 2 | M20 | 18.7 | 2750 | 2486 | 7.5 | 50 | 43 | 0.17 | 28.3 | 314 | 45.1 | 100 | 87 | 0.52 |
| 433 | Stability bracing lower ca. | 70x70x6 | 1 | M16 | 0.3 | 810 | 702 | 0.4 | 50 | 43 | 0.01 | 0.4 | 201 | 1.9 | 100 | 87 | 0.02 |
| 434 | Hand rail | 60x60x6 | 1 | M16 | 0.1 | 690 | 582 | 0.2 | 50 | 43 | 0.00 | 0.2 | 201 | 0.8 | 100 | 87 | 0.01 |
| 435 | Hand rail | 100x50x6 | 2 | M16 | 0.0 | 870 | 762 | 0.0 | 50 | 43 | 0.00 | 0.0 | 201 | 0.0 | 100 | 87 | 0.00 |
| 436 | Hand rail | 60x60x6 | 1 | M16 | 0.0 | 690 | 582 | 0.1 | 50 | 43 | 0.00 | 0.1 | 201 | 0.4 | 100 | 87 | 0.00 |
| 437 | Stability bracing lower ca. | 70x70x6 | 1 | M16 | 1.0 | 810 | 702 | 1.4 | 50 | 43 | 0.03 | 1.5 | 201 | 7.5 | 100 | 87 | 0.09 |
| 440 | Vertical side face lower ca. | 70x70x6 | 1 | M16 | 2.0 | 810 | 702 | 2.9 | 50 | 43 | 0.07 | 3.1 | 201 | 15.2 | 100 | 87 | 0.17 |
| 441 | Vertical side face lower ca. | 70x70x6 | 1 | M16 | 2.6 | 810 | 702 | 3.7 | 50 | 43 | 0.09 | 4.0 | 201 | 19.8 | 100 | 87 | 0.23 |



Check galloping- 120gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | Controle boutdoorsnede | | | | | | | |
|-------|------------------------------|----------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|------------------------|--------------|-----------|-----------------|--------------|------------|--------------|---------|
| | | | | | ΔF;o [kN] | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. [kN] | ΔF;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b [Mpa] | UC bout |
| 442 | Vertical side face lower ca. | 60x60x6 | 1 | M16 | 3.5 | 690 | 582 | 5.9 | 50 | 43 | 0.14 | 5.3 | 201 | 26.2 | 100 | 87 | 0.30 |
| 443 | Vertical side face lower ca. | 60x60x6 | 1 | M16 | 0.5 | 690 | 582 | 0.9 | 50 | 43 | 0.02 | 0.8 | 201 | 3.9 | 100 | 87 | 0.05 |
| 444 | Vertical side face lower ca. | 60x60x6 | 1 | M16 | 10.0 | 690 | 582 | 17.2 | 50 | 43 | 0.40 | 15.3 | 201 | 76.0 | 100 | 87 | 0.87 |
| 460 | Diag side face lower ca. | 90x90x8 | 2 | M16 | 5.5 | 1390 | 1246 | 4.4 | 50 | 43 | 0.10 | 8.1 | 201 | 20.2 | 100 | 87 | 0.23 |
| 461 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 3.3 | 690 | 582 | 5.7 | 50 | 43 | 0.13 | 5.1 | 201 | 12.7 | 100 | 87 | 0.15 |
| 462 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 5.8 | 690 | 582 | 9.9 | 50 | 43 | 0.23 | 8.8 | 201 | 22.0 | 100 | 87 | 0.25 |
| 463 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 8.3 | 690 | 582 | 14.2 | 50 | 43 | 0.33 | 12.6 | 201 | 31.4 | 100 | 87 | 0.36 |
| 464 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 10.6 | 690 | 582 | 18.1 | 50 | 43 | 0.42 | 16.1 | 201 | 40.1 | 100 | 87 | 0.46 |
| 465 | Stability bracing lower ca. | 90x90x9 | 1 | M16 | 0.4 | 1539 | 1377 | 0.3 | 50 | 43 | 0.01 | 0.6 | 201 | 2.8 | 100 | 87 | 0.03 |
| 475 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 11.7 | 940 | 808 | 14.5 | 50 | 43 | 0.33 | 16.3 | 314 | 26.0 | 100 | 87 | 0.30 |
| 476 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 13.8 | 940 | 808 | 17.1 | 50 | 43 | 0.39 | 19.3 | 314 | 30.7 | 100 | 87 | 0.35 |
| 477 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 10.7 | 940 | 808 | 13.3 | 50 | 43 | 0.31 | 16.0 | 314 | 25.5 | 100 | 87 | 0.29 |
| 478 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 11.7 | 940 | 808 | 14.5 | 50 | 43 | 0.33 | 17.9 | 314 | 28.5 | 100 | 87 | 0.33 |
| 479 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 13.0 | 810 | 678 | 19.1 | 50 | 43 | 0.44 | 19.8 | 314 | 31.5 | 100 | 87 | 0.36 |
| 480 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 14.5 | 810 | 678 | 21.4 | 50 | 43 | 0.49 | 22.2 | 314 | 35.3 | 100 | 87 | 0.41 |
| 481 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 16.6 | 810 | 678 | 24.6 | 50 | 43 | 0.56 | 25.4 | 314 | 40.5 | 100 | 87 | 0.47 |
| 482 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 19.7 | 810 | 678 | 29.0 | 50 | 43 | 0.67 | 30.0 | 314 | 47.8 | 100 | 87 | 0.55 |
| 483 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 23.0 | 810 | 678 | 33.9 | 50 | 43 | 0.78 | 35.1 | 314 | 55.9 | 100 | 87 | 0.64 |
| 484 | Diag lower plane lower ca. | 70x70x6 | 2 | M16 | 11.2 | 810 | 702 | 16.0 | 50 | 43 | 0.37 | 17.1 | 157 | 54.6 | 100 | 87 | 0.63 |
| 485 | Plan bracing lower ca. | 120x120x10 | 3 | M24 | 26.8 | 2320 | 2060 | 13.0 | 50 | 43 | 0.30 | 40.3 | 452 | 29.7 | 100 | 87 | 0.34 |
| 486 | Plan bracing lower ca. | 70x70x6 | 1 | M16 | 0.1 | 810 | 702 | 0.1 | 50 | 43 | 0.00 | 0.1 | 201 | 0.4 | 100 | 87 | 0.00 |
| 500 | Horizontal mid ca. | 200x200x18 | 10 | M24 | 123.0 | 6910 | 6442 | 19.1 | 50 | 43 | 0.44 | 186.6 | 452 | 41.3 | 100 | 87 | 0.47 |
| 501 | Lower chord mid ca. | 180x180x18 | 10 | M24 | 212.8 | 6190 | 5722 | 37.2 | 50 | 43 | 0.86 | 322.6 | 452 | 71.4 | 100 | 87 | 0.82 |
| 502 | Lower chord mid ca. | 180x180x18 | 0 | 0 | 206.3 | 6190 | 6190 | 33.3 | 50 | 43 | 0.77 | 313.4 | 0 | 0.0 | 100 | 87 | 0.00 |
| 503 | Lower chord mid ca. | 180x180x18 | 0 | 0 | 190.0 | 6190 | 6190 | 30.7 | 50 | 43 | 0.71 | 289.6 | 0 | 0.0 | 100 | 87 | 0.00 |
| 504 | Lower chord mid ca. | 180x180x18 | 8 | M24 | 168.4 | 6190 | 5722 | 29.4 | 50 | 43 | 0.68 | 257.1 | 452 | 71.1 | 100 | 87 | 0.82 |
| 505 | Lower chord mid ca. | 160x160x15 | 8 | M24 | 146.9 | 4671 | 4281 | 34.3 | 50 | 43 | 0.79 | 224.2 | 452 | 62.0 | 100 | 87 | 0.71 |
| 506 | Lower chord mid ca. | 160x160x15 | 0 | 0 | 109.9 | 4671 | 4671 | 23.5 | 50 | 43 | 0.54 | 167.8 | 0 | 0.0 | 100 | 87 | 0.00 |
| 507 | Lower chord mid ca. | 160x160x15 | 0 | 0 | 76.2 | 4671 | 4671 | 16.3 | 50 | 43 | 0.38 | 116.4 | 0 | 0.0 | 100 | 87 | 0.00 |
| 508 | Lower chord mid ca. | 160x160x15 | 0 | 0 | 46.0 | 4671 | 4671 | 9.9 | 50 | 43 | 0.23 | 70.3 | 0 | 0.0 | 100 | 87 | 0.00 |
| 509 | Lower chord mid ca. | 160x160x15 | 3 | M20 | 0.2 | 4671 | 4341 | 0.1 | 50 | 43 | 0.00 | 0.4 | 314 | 0.6 | 100 | 87 | 0.01 |
| 511 | Horizontal mid ca. | 150x150x12 | 3 | M24 | 37.3 | 3480 | 3168 | 11.8 | 50 | 43 | 0.27 | 56.7 | 452 | 41.8 | 100 | 87 | 0.48 |
| 512 | Beam mid ca. | 150x150x14 (not coup | 2 | M24 | 13.9 | 8028 | 7664 | 1.8 | 50 | 43 | 0.04 | 19.4 | 452 | 21.5 | 100 | 87 | 0.25 |
| 513 | Horizontal mid ca. | HEA140 | 0 | 0 | 0.5 | 3140 | 3140 | 0.1 | 50 | 43 | 0.00 | 0.7 | 0 | 0.0 | 100 | 87 | 0.00 |
| 514 | Beam mid ca. | 150x150x18 (not coup | 2 | M24 | 22.6 | 10200 | 9732 | 2.3 | 50 | 43 | 0.05 | 34.5 | 452 | 38.2 | 100 | 87 | 0.44 |



Check galloping- 120gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | | | | | | Controle boutdoorsnede | | | | |
|-------|----------------------------|------------|---------------|------|----------------------------------|---------------------------|--------------------------|--------------------------|-------------|-----------------------------|--------------|--------------------|------------------------------|-----------------------------|------------------------|-----------------------------|---------|--|--|
| | | | | | $\Delta F; o$ [kN] | Brutto [mm ²] | Netto [mm ²] | $\Delta \sigma; i$ [Mpa] | DC; o [Mpa] | $\Delta \sigma; c; o$ [Mpa] | UC opp. [kN] | $\Delta F; b$ [kN] | Opp. Bout [mm ²] | $\Delta \sigma; i; b$ [Mpa] | DC; b [Mpa] | $\Delta \sigma; c; b$ [Mpa] | UC bout | | |
| 515 | Horizontal mid ca. | HEB220 | 0 | 0 | 2.3 | 9104 | 9104 | 0.2 | 50 | 43 | 0.01 | 3.5 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 516 | Beam mid ca. | UNP220 | 0 | 0 | 7.2 | 3740 | 3740 | 1.9 | 50 | 43 | 0.04 | 11.0 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 526 | Upper chord mid ca. | 120x120x12 | 4 | M24 | 34.7 | 2750 | 2438 | 14.2 | 50 | 43 | 0.33 | 52.6 | 452 | 29.1 | 100 | 87 | 0.33 | | |
| 527 | Upper chord mid ca. | 120x120x12 | 0 | 0 | 35.2 | 2750 | 2750 | 12.8 | 50 | 43 | 0.29 | 53.3 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 528 | Upper chord mid ca. | 120x120x12 | 6 | M24 | 34.3 | 2750 | 2438 | 14.1 | 50 | 43 | 0.32 | 52.1 | 452 | 19.2 | 100 | 87 | 0.22 | | |
| 529 | Upper chord mid ca. | 120x120x12 | 6 | M24 | 31.5 | 2750 | 2438 | 12.9 | 50 | 43 | 0.30 | 48.0 | 452 | 17.7 | 100 | 87 | 0.20 | | |
| 530 | Upper chord mid ca. | 120x120x12 | 0 | 0 | 29.0 | 2750 | 2750 | 10.5 | 50 | 43 | 0.24 | 44.1 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 531 | Upper chord mid ca. | 120x120x12 | 4 | M24 | 26.9 | 2750 | 2438 | 11.0 | 50 | 43 | 0.23 | 40.9 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 532 | Upper chord mid ca. | 120x120x12 | 4 | M24 | 26.9 | 2750 | 2438 | 11.0 | 50 | 43 | 0.25 | 41.0 | 452 | 22.6 | 100 | 87 | 0.26 | | |
| 533 | Upper chord mid ca. | 120x120x12 | 2 | M24 | 28.9 | 2750 | 2438 | 11.9 | 50 | 43 | 0.27 | 44.0 | 452 | 48.7 | 100 | 87 | 0.56 | | |
| 535 | Stability bracing mid ca. | 70x70x6 | 1 | M16 | 0.3 | 810 | 702 | 0.4 | 50 | 43 | 0.01 | 0.4 | 201 | 1.9 | 100 | 87 | 0.02 | | |
| 536 | Hand rail | 60x60x6 | 1 | M16 | 0.1 | 690 | 582 | 0.1 | 50 | 43 | 0.00 | 0.1 | 201 | 0.5 | 100 | 87 | 0.01 | | |
| 537 | Hand rail | 100x50x6 | 2 | M16 | 0.0 | 870 | 762 | 0.0 | 50 | 43 | 0.00 | 0.0 | 201 | 0.0 | 100 | 87 | 0.00 | | |
| 538 | Hand rail | 60x60x6 | 1 | M16 | 0.0 | 690 | 582 | 0.1 | 50 | 43 | 0.00 | 0.0 | 201 | 0.2 | 100 | 87 | 0.00 | | |
| 539 | Stability bracing mid ca. | 70x70x6 | 1 | M16 | 1.3 | 810 | 702 | 1.8 | 50 | 43 | 0.04 | 1.9 | 201 | 9.7 | 100 | 87 | 0.11 | | |
| 540 | Vertical side face mid ca. | 80x80x6 | 1 | M16 | 3.1 | 940 | 832 | 3.7 | 50 | 43 | 0.09 | 4.3 | 201 | 21.6 | 100 | 87 | 0.25 | | |
| 541 | Vertical side face mid ca. | 80x80x6 | 1 | M16 | 3.0 | 940 | 832 | 3.6 | 50 | 43 | 0.08 | 4.3 | 201 | 21.6 | 100 | 87 | 0.25 | | |
| 542 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 1.6 | 690 | 582 | 2.8 | 50 | 43 | 0.06 | 2.5 | 201 | 12.4 | 100 | 87 | 0.14 | | |
| 543 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 2.1 | 690 | 582 | 3.5 | 50 | 43 | 0.08 | 3.2 | 201 | 15.7 | 100 | 87 | 0.18 | | |
| 544 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 2.6 | 690 | 582 | 4.4 | 50 | 43 | 0.10 | 3.9 | 201 | 19.6 | 100 | 87 | 0.23 | | |
| 545 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 0.7 | 690 | 582 | 1.2 | 50 | 43 | 0.03 | 1.1 | 201 | 5.3 | 100 | 87 | 0.06 | | |
| 546 | Vertical side face mid ca. | 60x60x6 | 2 | M16 | 11.4 | 690 | 582 | 19.6 | 50 | 43 | 0.45 | 17.4 | 201 | 43.2 | 100 | 87 | 0.50 | | |
| 560 | Diag side face mid ca. | 80x80x6 | 2 | M16 | 2.9 | 940 | 832 | 3.5 | 50 | 43 | 0.08 | 4.4 | 201 | 10.9 | 100 | 87 | 0.13 | | |
| 561 | Diag side face mid ca. | 70x70x6 | 2 | M16 | 4.7 | 810 | 702 | 6.7 | 50 | 43 | 0.15 | 6.6 | 201 | 16.4 | 100 | 87 | 0.19 | | |
| 562 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 4.7 | 690 | 582 | 8.1 | 50 | 43 | 0.19 | 6.8 | 201 | 17.0 | 100 | 87 | 0.19 | | |
| 563 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 2.9 | 690 | 582 | 5.0 | 50 | 43 | 0.11 | 4.4 | 201 | 11.0 | 100 | 87 | 0.13 | | |
| 564 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 4.9 | 690 | 582 | 8.5 | 50 | 43 | 0.19 | 7.5 | 201 | 18.7 | 100 | 87 | 0.22 | | |
| 565 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 5.6 | 690 | 582 | 9.7 | 50 | 43 | 0.22 | 8.6 | 201 | 21.4 | 100 | 87 | 0.25 | | |
| 566 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 6.6 | 690 | 582 | 11.4 | 50 | 43 | 0.26 | 10.1 | 201 | 25.1 | 100 | 87 | 0.29 | | |
| 567 | Stability bracing mid ca. | 70x70x6 | 1 | M16 | 0.5 | 810 | 702 | 0.6 | 50 | 43 | 0.01 | 0.6 | 201 | 3.2 | 100 | 87 | 0.04 | | |
| 575 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 9.5 | 810 | 678 | 14.0 | 50 | 43 | 0.32 | 13.2 | 314 | 21.0 | 100 | 87 | 0.24 | | |
| 576 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 11.5 | 810 | 678 | 17.0 | 50 | 43 | 0.39 | 16.1 | 314 | 25.6 | 100 | 87 | 0.29 | | |
| 577 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 12.1 | 810 | 678 | 17.9 | 50 | 43 | 0.41 | 16.9 | 314 | 26.9 | 100 | 87 | 0.31 | | |
| 578 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 13.3 | 810 | 678 | 19.7 | 50 | 43 | 0.45 | 18.6 | 314 | 29.7 | 100 | 87 | 0.34 | | |
| 579 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 14.0 | 810 | 678 | 20.7 | 50 | 43 | 0.48 | 19.6 | 314 | 31.2 | 100 | 87 | 0.36 | | |



Check galloping- 120gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLT-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | Controle boutdoorsnede | | | | | | | |
|-------|--------------------------|----------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|------------------------|--------------|-------------|-----------------|--------------|------------|--------------|---------|
| | | | | | ΔF;o [kN] | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. [kN] | ΔF;i;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b [Mpa] | UC bout |
| 580 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 12.0 | 810 | 678 | 17.6 | 50 | 43 | 0.41 | 17.9 | 314 | 28.5 | 100 | 87 | 0.33 |
| 581 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 13.4 | 810 | 678 | 19.8 | 50 | 43 | 0.46 | 20.5 | 314 | 32.6 | 100 | 87 | 0.38 |
| 582 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 14.3 | 810 | 678 | 21.1 | 50 | 43 | 0.49 | 21.8 | 314 | 34.8 | 100 | 87 | 0.40 |
| 583 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 16.4 | 810 | 678 | 24.2 | 50 | 43 | 0.56 | 25.0 | 314 | 39.9 | 100 | 87 | 0.46 |
| 584 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 18.7 | 810 | 678 | 27.5 | 50 | 43 | 0.63 | 28.5 | 314 | 45.4 | 100 | 87 | 0.52 |
| 585 | Diag lower plane mid ca. | 80x80x6 | 2 | M20 | 22.7 | 940 | 808 | 28.0 | 50 | 43 | 0.64 | 34.6 | 314 | 55.1 | 100 | 87 | 0.63 |
| 586 | Diag lower plane mid ca. | 80x80x6 | 2 | M20 | 26.3 | 940 | 808 | 32.6 | 50 | 43 | 0.75 | 40.2 | 314 | 64.0 | 100 | 87 | 0.74 |
| 587 | Diag lower plane mid ca. | 80x60x6 | 2 | M16 | 11.1 | 690 | 582 | 19.1 | 50 | 43 | 0.44 | 17.0 | 201 | 42.2 | 100 | 87 | 0.49 |
| 588 | Plan bracing mid ca. | 140x140x13 | 5 | M24 | 87.8 | 3521 | 3183 | 27.6 | 50 | 43 | 0.63 | 133.6 | 452 | 59.1 | 100 | 87 | 0.68 |
| 589 | Plan bracing mid ca. | 150x150x12 | 4 | M24 | 56.3 | 3480 | 3168 | 17.8 | 50 | 43 | 0.41 | 85.5 | 452 | 47.3 | 100 | 87 | 0.54 |
| 600 | Horizontal top ca. | 200x200x18 | 10 | M24 | 141.7 | 6910 | 6442 | 22.0 | 50 | 43 | 0.51 | 214.3 | 452 | 47.4 | 100 | 87 | 0.55 |
| 601 | Lower chord top ca. | 180x180x18 | 8 | M24 | 186.7 | 6190 | 5722 | 32.6 | 50 | 43 | 0.75 | 284.7 | 452 | 78.7 | 100 | 87 | 0.91 |
| 602 | Lower chord top ca. | 180x180x18 | 8 | M24 | 157.0 | 6190 | 5722 | 27.4 | 50 | 43 | 0.63 | 239.6 | 452 | 66.3 | 100 | 87 | 0.76 |
| 603 | Lower chord top ca. | 150x150x14 | 8 | M24 | 125.7 | 4014 | 3650 | 34.5 | 50 | 43 | 0.79 | 192.0 | 452 | 53.1 | 100 | 87 | 0.61 |
| 604 | Lower chord top ca. | 150x150x14 | 0 | 0 | 69.0 | 4014 | 4014 | 17.2 | 50 | 43 | 0.40 | 105.3 | 0 | 0.0 | 100 | 87 | 0.00 |
| 605 | Lower chord top ca. | 150x150x14 | 0 | 0 | 40.6 | 4014 | 4014 | 10.1 | 50 | 43 | 0.23 | 61.9 | 0 | 0.0 | 100 | 87 | 0.00 |
| 606 | Lower chord top ca. | 150x150x14 | 2 | M20 | 5.9 | 4014 | 3706 | 1.6 | 50 | 43 | 0.04 | 8.2 | 314 | 13.1 | 100 | 87 | 0.15 |
| 608 | Earth peak lower chord | 80x80x8 | 2 | M20 | 7.8 | 1230 | 1054 | 7.4 | 50 | 43 | 0.17 | 10.9 | 314 | 17.4 | 100 | 87 | 0.20 |
| 609 | Earth peak lower chord | 80x80x8 | 2 | M20 | 7.3 | 1230 | 1054 | 7.0 | 50 | 43 | 0.16 | 10.3 | 314 | 16.4 | 100 | 87 | 0.19 |
| 610 | Horizontal top ca. | 130x130x12 | 3 | M24 | 40.8 | 3000 | 2688 | 15.2 | 50 | 43 | 0.35 | 61.4 | 452 | 45.3 | 100 | 87 | 0.52 |
| 611 | Horizontal top ca. | 150x150x14 (not coup | 2 | M24 | 12.0 | 8028 | 7664 | 1.6 | 50 | 43 | 0.04 | 18.3 | 452 | 20.3 | 100 | 87 | 0.23 |
| 612 | Horizontal top ca. | HEA140 | 0 | 0 | 1.0 | 3140 | 3140 | 0.3 | 50 | 43 | 0.01 | 1.5 | 0 | 0.0 | 100 | 87 | 0.00 |
| 613 | Horizontal top ca. | 150x150x18 (not coup | 2 | M24 | 23.9 | 10200 | 9732 | 2.5 | 50 | 43 | 0.06 | 36.6 | 452 | 40.4 | 100 | 87 | 0.46 |
| 614 | Beam top ca. | HEB220 | 0 | 0 | 2.1 | 9104 | 9104 | 0.2 | 50 | 43 | 0.01 | 3.2 | 0 | 0.0 | 100 | 87 | 0.00 |
| 615 | Earth peak horizontal | 60x60x6 | 1 | M16 | 0.8 | 690 | 582 | 1.4 | 50 | 43 | 0.03 | 1.2 | 201 | 6.1 | 100 | 87 | 0.07 |
| 616 | Earth peak horizontal | 60x60x6 | 1 | M16 | 0.8 | 690 | 582 | 1.5 | 50 | 43 | 0.03 | 1.3 | 201 | 6.3 | 100 | 87 | 0.07 |
| 617 | Earth peak horizontal | 60x60x6 | 1 | M16 | 0.0 | 690 | 582 | 0.0 | 50 | 43 | 0.00 | 0.1 | 201 | 0.1 | 100 | 87 | 0.00 |
| 618 | Beam top ca. | UNP220 | 0 | 0 | 4.6 | 3740 | 3740 | 1.2 | 50 | 43 | 0.03 | 7.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 626 | Upper chord top ca. | 120x120x12 | 0 | 0 | 40.7 | 2750 | 2750 | 14.8 | 50 | 43 | 0.34 | 62.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 627 | Upper chord top ca. | 100x100x10 | 3 | M24 | 18.3 | 1920 | 1660 | 11.0 | 50 | 43 | 0.25 | 27.5 | 452 | 20.3 | 100 | 87 | 0.23 |
| 628 | Upper chord top ca. | 100x100x10 | 6 | M24 | 17.3 | 1920 | 1660 | 10.4 | 50 | 43 | 0.24 | 26.2 | 452 | 9.7 | 100 | 87 | 0.11 |
| 629 | Upper chord top ca. | 100x100x10 | 3 | M24 | 16.9 | 1920 | 1660 | 10.2 | 50 | 43 | 0.23 | 25.7 | 452 | 18.9 | 100 | 87 | 0.22 |
| 630 | Earth peak upper chord | 130x130x12 | 0 | 0 | 56.1 | 3000 | 3000 | 18.7 | 50 | 43 | 0.43 | 76.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 631 | Earth peak upper chord | 130x130x12 | 4 | M24 | 48.5 | 3000 | 2688 | 18.1 | 50 | 43 | 0.42 | 68.2 | 452 | 37.7 | 100 | 87 | 0.43 |
| 632 | Earth peak upper chord | 120x120x10 | 4 | M24 | 46.9 | 2320 | 2060 | 22.8 | 50 | 43 | 0.52 | 65.8 | 452 | 36.4 | 100 | 87 | 0.42 |



Check galloping- 120gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | | | | | | Controle boutdoorsnede | | | | |
|-------|-------------------------------|------------|---------------|------|----------------------------------|--------------|-------------|-------------------------|------------|-------------------|--------------|-------------------|------------|-------------------------|------------------------|-------------------|---------|--|--|
| | | | | | ΔF_o [kN] | Brutto [mm2] | Netto [mm2] | $\Delta \sigma_o$ [Mpa] | DC;o [Mpa] | $\Delta \sigma_c$ | UC opp. [kN] | ΔF_i [kN] | Bout [mm2] | $\Delta \sigma_i$ [Mpa] | DC;i [Mpa] | $\Delta \sigma_c$ | UC bout | | |
| 633 | Earth peak upper chord | 120x120x10 | 0 | 0 | 41.6 | 2320 | 2320 | 17.9 | 50 | 43 | 0.41 | 58.3 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 634 | Earth peak upper chord | 120x120x10 | 0 | 0 | 33.0 | 2320 | 2320 | 14.2 | 50 | 43 | 0.33 | 46.3 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 635 | Earth peak upper chord | 120x120x10 | 2 | M20 | 19.6 | 2320 | 2100 | 9.3 | 50 | 43 | 0.21 | 27.4 | 314 | 43.7 | 100 | 87 | 0.50 | | |
| 637 | Stability bracing top ca. | 70x70x7 | 1 | M16 | 8.1 | 940 | 814 | 9.9 | 50 | 43 | 0.23 | 12.2 | 201 | 60.8 | 100 | 87 | 0.70 | | |
| 638 | Earth peak horizontal | HEB160 | 2 | M20 | 4.2 | 5430 | 5254 | 0.8 | 50 | 43 | 0.02 | 5.9 | 314 | 9.4 | 100 | 87 | 0.11 | | |
| 640 | Vertical side face top ca. | 60x60x6 | 2 | M16 | 3.7 | 690 | 582 | 6.4 | 50 | 43 | 0.15 | 5.4 | 201 | 13.5 | 100 | 87 | 0.16 | | |
| 641 | Vertical side face top ca. | 60x60x6 | 2 | M16 | 12.3 | 690 | 582 | 21.2 | 50 | 43 | 0.49 | 18.6 | 201 | 46.2 | 100 | 87 | 0.53 | | |
| 642 | Vertical side face top ca. | 80x80x6 | 1 | M16 | 2.9 | 940 | 832 | 3.5 | 50 | 43 | 0.08 | 4.4 | 201 | 21.8 | 100 | 87 | 0.25 | | |
| 643 | Vertical side face top ca. | 80x80x6 | 1 | M16 | 0.2 | 940 | 832 | 0.3 | 50 | 43 | 0.01 | 0.3 | 201 | 1.7 | 100 | 87 | 0.02 | | |
| 644 | Vertical side face top ca. | 80x80x6 | 1 | M16 | 7.4 | 940 | 832 | 8.9 | 50 | 43 | 0.21 | 11.4 | 201 | 56.5 | 100 | 87 | 0.65 | | |
| 645 | Vertical side face top ca. | 80x80x8 | 1 | M16 | 0.1 | 1230 | 1086 | 0.1 | 50 | 43 | 0.00 | 0.2 | 201 | 0.8 | 100 | 87 | 0.01 | | |
| 646 | Earth peak vertical side face | 60x60x6 | 1 | M16 | 0.3 | 690 | 582 | 0.5 | 50 | 43 | 0.01 | 0.4 | 201 | 1.8 | 100 | 87 | 0.02 | | |
| 660 | Diag side face top ca. | 80x80x6 | 2 | M16 | 5.8 | 940 | 832 | 6.9 | 50 | 43 | 0.16 | 8.0 | 201 | 20.0 | 100 | 87 | 0.23 | | |
| 661 | Diag side face top ca. | 80x80x8 | 2 | M16 | 5.0 | 1230 | 1086 | 4.6 | 50 | 43 | 0.11 | 7.6 | 201 | 19.0 | 100 | 87 | 0.22 | | |
| 662 | Diag side face top ca. | 80x80x8 | 2 | M20 | 8.1 | 1230 | 1054 | 7.7 | 50 | 43 | 0.18 | 12.3 | 314 | 19.6 | 100 | 87 | 0.23 | | |
| 663 | Earth peak diag side face | 80x80x6 | 2 | M16 | 0.3 | 940 | 832 | 0.3 | 50 | 43 | 0.01 | 0.4 | 201 | 1.8 | 100 | 87 | 0.02 | | |
| 664 | Stability bracing top ca. | 80x80x8 | 2 | M16 | 15.4 | 1230 | 1086 | 14.1 | 50 | 43 | 0.33 | 23.2 | 201 | 57.7 | 100 | 87 | 0.66 | | |
| 673 | Earth peak diag upper side | 60x60x6 | 2 | M16 | 7.2 | 690 | 582 | 12.3 | 50 | 43 | 0.28 | 10.1 | 201 | 25.0 | 100 | 87 | 0.29 | | |
| 674 | Earth peak diag upper side | 60x60x6 | 2 | M16 | 5.7 | 690 | 582 | 9.8 | 50 | 43 | 0.23 | 8.0 | 201 | 20.0 | 100 | 87 | 0.23 | | |
| 675 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 11.9 | 810 | 678 | 17.5 | 50 | 43 | 0.40 | 16.5 | 314 | 26.3 | 100 | 87 | 0.30 | | |
| 676 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 14.8 | 810 | 678 | 21.9 | 50 | 43 | 0.50 | 20.8 | 314 | 33.1 | 100 | 87 | 0.38 | | |
| 677 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 14.0 | 810 | 678 | 20.6 | 50 | 43 | 0.47 | 19.5 | 314 | 31.0 | 100 | 87 | 0.36 | | |
| 678 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 12.5 | 810 | 678 | 18.5 | 50 | 43 | 0.43 | 19.0 | 314 | 30.3 | 100 | 87 | 0.35 | | |
| 679 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 12.7 | 810 | 678 | 18.8 | 50 | 43 | 0.43 | 19.4 | 314 | 30.9 | 100 | 87 | 0.36 | | |
| 680 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 13.8 | 810 | 678 | 20.4 | 50 | 43 | 0.47 | 21.1 | 314 | 33.5 | 100 | 87 | 0.39 | | |
| 681 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 21.8 | 810 | 678 | 32.2 | 50 | 43 | 0.74 | 33.3 | 314 | 53.0 | 100 | 87 | 0.61 | | |
| 682 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 24.9 | 810 | 678 | 36.7 | 50 | 43 | 0.84 | 38.0 | 314 | 60.4 | 100 | 87 | 0.69 | | |
| 683 | Diag lower plane top ca. | 80x80x6 | 2 | M20 | 26.4 | 940 | 808 | 32.6 | 50 | 43 | 0.75 | 40.2 | 314 | 64.1 | 100 | 87 | 0.74 | | |
| 684 | Diag lower plane top ca. | 80x80x6 | 2 | M20 | 27.6 | 940 | 808 | 34.2 | 50 | 43 | 0.79 | 42.2 | 314 | 67.2 | 100 | 87 | 0.77 | | |
| 685 | Diag lower plane top ca. | 60x60x6 | 2 | M16 | 10.9 | 690 | 582 | 18.7 | 50 | 43 | 0.43 | 16.6 | 201 | 41.4 | 100 | 87 | 0.48 | | |
| 686 | Earth peak diag lower plane | 70x70x7 | 1 | M16 | 0.4 | 940 | 814 | 0.5 | 50 | 43 | 0.01 | 0.6 | 201 | 3.0 | 100 | 87 | 0.04 | | |
| 687 | Earth peak diag lower plane | 70x70x7 | 1 | M16 | 2.5 | 940 | 814 | 3.1 | 50 | 43 | 0.07 | 3.7 | 201 | 18.5 | 100 | 87 | 0.21 | | |
| 688 | Earth peak diag upper plane | 70x70x6 | 2 | M16 | 7.8 | 810 | 702 | 11.2 | 50 | 43 | 0.26 | 11.7 | 201 | 29.1 | 100 | 87 | 0.33 | | |
| 689 | Earth peak diag upper plane | 70x70x6 | 2 | M16 | 8.6 | 810 | 702 | 12.3 | 50 | 43 | 0.28 | 12.8 | 201 | 32.0 | 100 | 87 | 0.37 | | |
| 690 | Earth peak diag upper plane | 60x60x6 | 2 | M16 | 9.3 | 690 | 582 | 15.9 | 50 | 43 | 0.37 | 13.8 | 201 | 34.3 | 100 | 87 | 0.39 | | |



Check galloping- 120qr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | Controle boutdoorsnede | | | | | | | |
|-------|-------------------------------|-----------------------|---------------|------|----------------------------------|--------------|-------------|------------------------|------------|--------------------------|---------|-------------------|-----------------|--------------------------|------------|--------------------------|---------|
| | | | | | $\Delta F;0$ [kN] | Brutto [mm2] | Netto [mm2] | $\Delta\sigma;0$ [Mpa] | DC;0 [Mpa] | $\Delta\sigma;c;0$ [Mpa] | UC opp. | $\Delta F;b$ [kN] | Opp. Bout [mm2] | $\Delta\sigma;i;b$ [Mpa] | DC;b [Mpa] | $\Delta\sigma;c;b$ [Mpa] | UC bout |
| 691 | Earth peak diag upper plane | 60x60x6 | 2 | M16 | 10.2 | 690 | 582 | 17.5 | 50 | 43 | 0.40 | 15.2 | 201 | 37.8 | 100 | 87 | 0.43 |
| 692 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 2.1 | 690 | 582 | 3.7 | 50 | 43 | 0.08 | 3.0 | 201 | 14.9 | 100 | 87 | 0.17 |
| 693 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 2.3 | 690 | 582 | 3.9 | 50 | 43 | 0.09 | 3.2 | 201 | 16.1 | 100 | 87 | 0.18 |
| 694 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 2.7 | 690 | 582 | 4.6 | 50 | 43 | 0.11 | 3.7 | 201 | 18.6 | 100 | 87 | 0.21 |
| 695 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 3.1 | 690 | 582 | 5.3 | 50 | 43 | 0.12 | 4.3 | 201 | 21.4 | 100 | 87 | 0.25 |
| 696 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 3.6 | 690 | 582 | 6.3 | 50 | 43 | 0.14 | 5.1 | 201 | 25.5 | 100 | 87 | 0.29 |
| 697 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 4.5 | 690 | 582 | 7.6 | 50 | 43 | 0.18 | 6.3 | 201 | 31.1 | 100 | 87 | 0.36 |
| 698 | Plan bracing top ca. | 150x150x12 | 4 | M24 | 59.3 | 3480 | 3168 | 18.7 | 50 | 43 | 0.43 | 89.2 | 452 | 49.3 | 100 | 87 | 0.57 |
| 699 | Plan bracing top ca. | 140x140x13 | 5 | M24 | 97.6 | 3521 | 3183 | 30.7 | 50 | 43 | 0.71 | 146.7 | 452 | 64.9 | 100 | 87 | 0.75 |
| 700 | Hor. Plan bracing hip structu | 100x100x8 | 2 | M20 | 2.4 | 1550 | 1374 | 1.8 | 50 | 43 | 0.04 | 3.2 | 314 | 5.2 | 100 | 87 | 0.06 |
| 701 | Hor. Plan bracing hip structu | 100x100x8 | 2 | M20 | 0.4 | 1550 | 1374 | 0.3 | 50 | 43 | 0.01 | 0.6 | 314 | 0.9 | 100 | 87 | 0.01 |
| 702 | Hor. Plan bracing hip structu | 100x100x8 (not coupl | 2 | M20 | 0.0 | 3100 | 2924 | 0.0 | 50 | 43 | 0.00 | 0.0 | 314 | 0.0 | 100 | 87 | 0.00 |
| 703 | 2nd plan bacing | 130x130x12#(15,0,33 | 3 | M24 | 15.3 | 6040 | 5728 | 2.7 | 50 | 43 | 0.06 | 20.6 | 452 | 15.2 | 100 | 87 | 0.17 |
| 704 | 2nd plan bacing | 90x90x8 | 2 | M20 | 2.6 | 1390 | 1214 | 2.1 | 50 | 43 | 0.05 | 3.8 | 314 | 6.0 | 100 | 87 | 0.07 |
| 705 | 2nd plan bacing | 90x90x8 (not coupled; | 2 | M20 | 0.0 | 2780 | 2604 | 0.0 | 50 | 43 | 0.00 | 0.0 | 314 | 0.0 | 100 | 87 | 0.00 |
| 710 | Horizontal top of lower ca. | 120x120x12 | 4 | M24 | 12.1 | 2750 | 2438 | 5.0 | 50 | 43 | 0.11 | 17.4 | 452 | 9.6 | 100 | 87 | 0.11 |
| 711 | Horizontal top of lower ca. | 130x130x12 | 2 | M24 | 3.4 | 3000 | 2688 | 1.3 | 50 | 43 | 0.03 | 4.9 | 452 | 5.4 | 100 | 87 | 0.06 |
| 712 | Horizontal top of mid ca. | 120x120x12 | 4 | M24 | 11.5 | 2750 | 2438 | 4.7 | 50 | 43 | 0.11 | 15.7 | 452 | 8.7 | 100 | 87 | 0.10 |
| 713 | Horizontal top of mid ca. | 120x120x10 | 2 | M24 | 4.5 | 2320 | 2060 | 2.2 | 50 | 43 | 0.05 | 6.3 | 452 | 7.0 | 100 | 87 | 0.08 |
| 714 | Horizontal top of top ca. | 120x120x12 | 4 | M24 | 19.7 | 2750 | 2438 | 8.1 | 50 | 43 | 0.19 | 30.0 | 452 | 16.6 | 100 | 87 | 0.19 |
| 715 | Horizontal top of top ca. | 100x100x10 | 2 | M24 | 1.0 | 1920 | 1660 | 0.6 | 50 | 43 | 0.01 | 1.4 | 452 | 1.6 | 100 | 87 | 0.02 |



Check galloping- 140gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLT-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | | | | | | Controle boutdoorsnede | | | | |
|-------|-----------------|----------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|--------------|---------|-------------|-----------------|--------------|------------------------|--------------|---------|--|--|
| | | | | | ΔF;o [kN] | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. | ΔF;i;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b [Mpa] | UC bout | | |
| 100 | Main leg | 80x80x8 | 2 | M20 | 16.2 | 1230 | 1054 | 15.4 | 50 | 43 | 0.35 | 24.7 | 314 | 39.3 | 100 | 87 | 0.45 | | |
| 101 | Main leg | 130x130x12 | 4 | M24 | 26.3 | 3000 | 2688 | 9.8 | 50 | 43 | 0.23 | 39.7 | 452 | 22.0 | 100 | 87 | 0.25 | | |
| 102 | Main leg | 180x180x16 | 8 | M24 | 38.1 | 5540 | 5124 | 7.4 | 50 | 43 | 0.17 | 55.5 | 452 | 15.4 | 100 | 87 | 0.18 | | |
| 103 | Main leg | 180x180x16 | 8 | M24 | 59.9 | 5540 | 5124 | 11.7 | 50 | 43 | 0.27 | 84.3 | 452 | 23.3 | 100 | 87 | 0.27 | | |
| 104 | Main leg | 180x180x16 | 10 | M24 | 83.5 | 5540 | 5124 | 16.3 | 50 | 43 | 0.37 | 118.0 | 452 | 26.1 | 100 | 87 | 0.30 | | |
| 105 | Main leg | 250x250x24 | 10 | M24 | 115.7 | 11492 | 10868 | 10.6 | 50 | 43 | 0.24 | 168.8 | 452 | 37.3 | 100 | 87 | 0.43 | | |
| 106 | Main leg | 250x250x24 | 0 | | 140.8 | 11492 | 11492 | 12.2 | 50 | 43 | 0.28 | 204.4 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 107 | Main leg | 250x250x24 | 16 | M24 | 152.6 | 11492 | 10868 | 14.0 | 50 | 43 | 0.32 | 216.5 | 452 | 29.9 | 100 | 87 | 0.34 | | |
| 108 | Main leg | 200x200x24 | 32 | M24 | 179.7 | 9060 | 8436 | 21.3 | 50 | 43 | 0.49 | 250.8 | 452 | 17.3 | 100 | 87 | 0.20 | | |
| 109 | Main leg | 200x200x24 | 20 | M24 | 196.6 | 9060 | 8436 | 23.3 | 50 | 43 | 0.54 | 272.7 | 452 | 30.2 | 100 | 87 | 0.35 | | |
| 110 | Main leg | 250x250x24 | 24 | M24 | 214.9 | 11492 | 10868 | 19.8 | 50 | 43 | 0.45 | 295.7 | 452 | 27.3 | 100 | 87 | 0.31 | | |
| 111 | Main leg | 250x250x24 | 32 | M24 | 226.4 | 11492 | 10868 | 20.8 | 50 | 43 | 0.48 | 307.9 | 452 | 21.3 | 100 | 87 | 0.24 | | |
| 112 | Main leg | 250x250x24 | 32 | M24 | 228.9 | 11492 | 10868 | 21.1 | 50 | 43 | 0.48 | 307.1 | 452 | 21.2 | 100 | 87 | 0.24 | | |
| 113 | Main leg | 250x250x24 | 0 | | 206.6 | 11492 | 11492 | 18.0 | 50 | 43 | 0.41 | 273.3 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 114 | Main leg | 250x250x24 | 24 | M24 | 205.9 | 11492 | 10868 | 18.9 | 50 | 43 | 0.44 | 272.5 | 452 | 25.1 | 100 | 87 | 0.29 | | |
| 200 | Diag front face | 100x100x10 | 2 | M24 | 20.4 | 1920 | 1660 | 12.3 | 50 | 43 | 0.28 | 31.1 | 452 | 34.4 | 100 | 87 | 0.40 | | |
| 201 | Diag front face | 150x150x14 | 6 | M24 | 114.6 | 4014 | 3650 | 31.4 | 50 | 43 | 0.72 | 173.0 | 452 | 63.8 | 100 | 87 | 0.73 | | |
| 202 | Diag front face | 150x150x14 | 5 | M24 | 96.0 | 4014 | 3650 | 26.3 | 50 | 43 | 0.60 | 144.8 | 452 | 64.1 | 100 | 87 | 0.74 | | |
| 203 | Diag front face | 150x150x14 | 5 | M24 | 79.1 | 4014 | 3650 | 21.7 | 50 | 43 | 0.50 | 119.2 | 452 | 52.8 | 100 | 87 | 0.61 | | |
| 204 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 110.5 | 5500 | 5188 | 21.3 | 50 | 43 | 0.49 | 157.4 | 452 | 87.1 | 100 | 87 | 1.00 | | |
| 205 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 96.0 | 5500 | 5188 | 18.5 | 50 | 43 | 0.43 | 136.8 | 452 | 75.7 | 100 | 87 | 0.87 | | |
| 206 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 84.2 | 5500 | 5188 | 16.2 | 50 | 43 | 0.37 | 117.5 | 452 | 65.0 | 100 | 87 | 0.75 | | |
| 207 | Diag front face | 130x130x12#(15,0,33) | 4 | M24 | 83.4 | 6040 | 5728 | 14.6 | 50 | 43 | 0.33 | 110.5 | 452 | 61.1 | 100 | 87 | 0.70 | | |
| 208 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 74.1 | 5500 | 5188 | 14.3 | 50 | 43 | 0.33 | 98.1 | 452 | 54.3 | 100 | 87 | 0.62 | | |
| 209 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 68.5 | 5500 | 5188 | 13.2 | 50 | 43 | 0.30 | 90.1 | 452 | 49.8 | 100 | 87 | 0.57 | | |
| 210 | Diag front face | 120x120x12(12,0,33) | 4 | M24 | 66.9 | 5500 | 5188 | 12.9 | 50 | 43 | 0.30 | 87.9 | 452 | 48.6 | 100 | 87 | 0.56 | | |
| 211 | Diag front face | 150x150x12(12,0,33) | 3 | M24 | 56.0 | 6970 | 6658 | 8.4 | 50 | 43 | 0.19 | 74.1 | 452 | 54.6 | 100 | 87 | 0.63 | | |
| 212 | Diag front face | 130x130x12#(15,0,33) | 3 | M24 | 40.7 | 6040 | 5728 | 7.1 | 50 | 43 | 0.16 | 53.8 | 452 | 39.6 | 100 | 87 | 0.46 | | |
| 213 | Diag front face | 150x150x12(12,0,33) | 5 | M24 | 39.9 | 6970 | 6658 | 6.0 | 50 | 43 | 0.14 | 52.7 | 452 | 23.3 | 100 | 87 | 0.27 | | |
| 300 | Diag side face | 80x80x8 | 2 | M24 | 15.7 | 1230 | 1022 | 15.4 | 50 | 43 | 0.35 | 24.0 | 452 | 26.6 | 100 | 87 | 0.31 | | |
| 301 | Diag side face | 150x150x14 | 6 | M24 | 112.8 | 4014 | 3650 | 30.9 | 50 | 43 | 0.71 | 170.4 | 452 | 62.8 | 100 | 87 | 0.72 | | |
| 302 | Diag side face | 150x150x14 | 5 | M24 | 94.8 | 4014 | 3650 | 26.0 | 50 | 43 | 0.60 | 143.3 | 452 | 63.4 | 100 | 87 | 0.73 | | |
| 303 | Diag side face | 150x150x14 | 4 | M24 | 77.5 | 4014 | 3650 | 21.2 | 50 | 43 | 0.49 | 117.1 | 452 | 64.7 | 100 | 87 | 0.74 | | |
| 304 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 100.6 | 5500 | 5188 | 19.4 | 50 | 43 | 0.45 | 139.5 | 452 | 77.1 | 100 | 87 | 0.89 | | |
| 305 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 88.2 | 5500 | 5188 | 17.0 | 50 | 43 | 0.39 | 122.2 | 452 | 67.6 | 100 | 87 | 0.78 | | |



Check galloping- 140gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | Controle boutdoorsnede | | | | | | | |
|-------|------------------------------|----------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|------------------------|--------------|-----------|-----------------|--------------|------------|--------------|---------|
| | | | | | ΔF;o [kN] | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. [kN] | ΔF;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b [Mpa] | UC bout |
| 306 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 79.8 | 5500 | 5188 | 15.4 | 50 | 43 | 0.35 | 110.3 | 452 | 61.0 | 100 | 87 | 0.70 |
| 307 | Diag side face | 130x130x12#(15,0,33) | 4 | M24 | 89.0 | 6040 | 5728 | 15.5 | 50 | 43 | 0.36 | 117.8 | 452 | 65.2 | 100 | 87 | 0.75 |
| 308 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 81.3 | 5500 | 5188 | 15.7 | 50 | 43 | 0.36 | 107.7 | 452 | 59.5 | 100 | 87 | 0.68 |
| 309 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 77.1 | 5500 | 5188 | 14.9 | 50 | 43 | 0.34 | 102.1 | 452 | 56.5 | 100 | 87 | 0.65 |
| 310 | Diag side face | 120x120x12(12,0,33) | 4 | M24 | 72.4 | 5500 | 5188 | 13.9 | 50 | 43 | 0.32 | 95.8 | 452 | 53.0 | 100 | 87 | 0.61 |
| 311 | Diag side face | 150x150x12(12,0,33) | 3 | M24 | 67.4 | 6970 | 6658 | 10.1 | 50 | 43 | 0.23 | 90.0 | 452 | 66.4 | 100 | 87 | 0.76 |
| 312 | Diag side face | 130x130x12#(15,0,33) | 3 | M24 | 51.2 | 6040 | 5728 | 8.9 | 50 | 43 | 0.21 | 68.3 | 452 | 50.4 | 100 | 87 | 0.58 |
| 313 | Diag side face | 150x150x12(12,0,33) | 5 | M24 | 48.8 | 6970 | 6658 | 7.3 | 50 | 43 | 0.17 | 65.1 | 452 | 28.8 | 100 | 87 | 0.33 |
| 400 | Horizontal lower ca. | 180x180x16 | 10 | M24 | 76.7 | 5540 | 5124 | 15.0 | 50 | 43 | 0.34 | 116.8 | 452 | 25.8 | 100 | 87 | 0.30 |
| 401 | Lower chord lower ca. | 150x150x14 | 10 | M24 | 149.5 | 4014 | 3650 | 40.9 | 50 | 43 | 0.94 | 227.7 | 452 | 50.4 | 100 | 87 | 0.58 |
| 402 | Lower chord lower ca. | 150x150x14 | 0 | | 132.3 | 4014 | 4014 | 33.0 | 50 | 43 | 0.76 | 202.0 | 0 | 0.0 | 100 | 87 | 0.00 |
| 403 | Lower chord lower ca. | 150x150x14 | 0 | | 120.1 | 4014 | 4014 | 29.9 | 50 | 43 | 0.69 | 183.4 | 0 | 0.0 | 100 | 87 | 0.00 |
| 404 | Lower chord lower ca. | 150x150x14 | 0 | | 91.0 | 4014 | 4014 | 22.7 | 50 | 43 | 0.52 | 139.0 | 0 | 0.0 | 100 | 87 | 0.00 |
| 405 | Lower chord lower ca. | 150x150x14 | 0 | | 50.1 | 4014 | 4014 | 12.5 | 50 | 43 | 0.29 | 76.5 | 0 | 0.0 | 100 | 87 | 0.00 |
| 406 | Lower chord lower ca. | 150x150x14 | 0 | | 34.8 | 4014 | 4014 | 8.7 | 50 | 43 | 0.20 | 53.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 407 | Lower chord lower ca. | 150x150x14 | 0 | | 0.4 | 4014 | 4014 | 0.1 | 50 | 43 | 0.00 | 0.6 | 0 | 0.0 | 100 | 87 | 0.00 |
| 410 | Horizontal lower ca. | 130x130x12 | 3 | M24 | 22.2 | 3000 | 2688 | 8.3 | 50 | 43 | 0.19 | 33.6 | 452 | 24.8 | 100 | 87 | 0.28 |
| 411 | Horizontal lower ca. | 150x150x14 (not coup | 2 | M24 | 13.0 | 8028 | 7664 | 1.7 | 50 | 43 | 0.04 | 19.8 | 452 | 21.9 | 100 | 87 | 0.25 |
| 412 | Horizontal lower ca. | HEA140 | 0 | | 0.8 | 3140 | 3140 | 0.3 | 50 | 43 | 0.01 | 1.2 | 0 | 0.0 | 100 | 87 | 0.00 |
| 413 | Horizontal lower ca. | 150x150x18 (not coup | 2 | M24 | 26.3 | 10200 | 9732 | 2.7 | 50 | 43 | 0.06 | 40.1 | 452 | 44.4 | 100 | 87 | 0.51 |
| 414 | Beam lower ca. | HEB220 | 0 | | 2.1 | 9104 | 9104 | 0.2 | 50 | 43 | 0.01 | 3.2 | 0 | 0.0 | 100 | 87 | 0.00 |
| 415 | Horizontal lower ca. | UNP220 | 0 | | 5.1 | 3740 | 3740 | 1.4 | 50 | 43 | 0.03 | 7.8 | 0 | 0.0 | 100 | 87 | 0.00 |
| 426 | Upper chord lower ca. | 120x120x12 | 4 | M24 | 15.3 | 2750 | 2438 | 6.3 | 50 | 43 | 0.14 | 23.1 | 452 | 12.8 | 100 | 87 | 0.15 |
| 427 | Upper chord lower ca. | 120x120x12 | 0 | | 14.6 | 2750 | 2750 | 5.3 | 50 | 43 | 0.12 | 22.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 428 | Upper chord lower ca. | 120x120x12 | 0 | | 14.7 | 2750 | 2750 | 5.4 | 50 | 43 | 0.12 | 22.3 | 0 | 0.0 | 100 | 87 | 0.00 |
| 429 | Upper chord lower ca. | 120x120x12 | 0 | | 15.6 | 2750 | 2750 | 5.7 | 50 | 43 | 0.13 | 23.5 | 0 | 0.0 | 100 | 87 | 0.00 |
| 430 | Upper chord lower ca. | 120x120x12 | 2 | M20 | 15.6 | 2750 | 2486 | 6.3 | 50 | 43 | 0.14 | 23.6 | 314 | 37.6 | 100 | 87 | 0.43 |
| 431 | Upper chord lower ca. | 120x120x12 | 2 | M20 | 19.2 | 2750 | 2486 | 7.7 | 50 | 43 | 0.18 | 29.1 | 314 | 46.4 | 100 | 87 | 0.53 |
| 433 | Stability bracing lower ca. | 70x70x6 | 1 | M16 | 0.3 | 810 | 702 | 0.4 | 50 | 43 | 0.01 | 0.4 | 201 | 2.1 | 100 | 87 | 0.02 |
| 434 | Hand rail | 60x60x6 | 1 | M16 | 0.1 | 690 | 582 | 0.2 | 50 | 43 | 0.00 | 0.2 | 201 | 0.8 | 100 | 87 | 0.01 |
| 435 | Hand rail | 100x50x6 | 2 | M16 | 0.0 | 870 | 762 | 0.0 | 50 | 43 | 0.00 | 0.0 | 201 | 0.0 | 100 | 87 | 0.00 |
| 436 | Hand rail | 60x60x6 | 1 | M16 | 0.1 | 690 | 582 | 0.1 | 50 | 43 | 0.00 | 0.1 | 201 | 0.4 | 100 | 87 | 0.00 |
| 437 | Stability bracing lower ca. | 70x70x6 | 1 | M16 | 1.1 | 810 | 702 | 1.5 | 50 | 43 | 0.04 | 1.6 | 201 | 7.9 | 100 | 87 | 0.09 |
| 440 | Vertical side face lower ca. | 70x70x6 | 1 | M16 | 2.0 | 810 | 702 | 2.9 | 50 | 43 | 0.07 | 3.1 | 201 | 15.2 | 100 | 87 | 0.18 |
| 441 | Vertical side face lower ca. | 70x70x6 | 1 | M16 | 2.6 | 810 | 702 | 3.7 | 50 | 43 | 0.09 | 4.0 | 201 | 19.8 | 100 | 87 | 0.23 |



Check galloping- 140gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | Controle boutdoorsnede | | | | | | | |
|-------|------------------------------|----------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|------------------------|--------------|-------------|-----------------|--------------|------------|--------------|---------|
| | | | | | ΔF;o [kN] | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. [kN] | ΔF;i;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b [Mpa] | UC bout |
| 442 | Vertical side face lower ca. | 60x60x6 | 1 | M16 | 3.5 | 690 | 582 | 5.9 | 50 | 43 | 0.14 | 5.3 | 201 | 26.2 | 100 | 87 | 0.30 |
| 443 | Vertical side face lower ca. | 60x60x6 | 1 | M16 | 0.5 | 690 | 582 | 0.9 | 50 | 43 | 0.02 | 0.8 | 201 | 3.8 | 100 | 87 | 0.04 |
| 444 | Vertical side face lower ca. | 60x60x6 | 1 | M16 | 10.0 | 690 | 582 | 17.2 | 50 | 43 | 0.40 | 15.3 | 201 | 76.0 | 100 | 87 | 0.87 |
| 460 | Diag side face lower ca. | 90x90x8 | 2 | M16 | 5.5 | 1390 | 1246 | 4.4 | 50 | 43 | 0.10 | 8.1 | 201 | 20.2 | 100 | 87 | 0.23 |
| 461 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 3.3 | 690 | 582 | 5.7 | 50 | 43 | 0.13 | 5.1 | 201 | 12.7 | 100 | 87 | 0.15 |
| 462 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 5.8 | 690 | 582 | 9.9 | 50 | 43 | 0.23 | 8.8 | 201 | 21.9 | 100 | 87 | 0.25 |
| 463 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 8.3 | 690 | 582 | 14.2 | 50 | 43 | 0.33 | 12.6 | 201 | 31.4 | 100 | 87 | 0.36 |
| 464 | Diag side face lower ca. | 60x60x6 | 2 | M16 | 10.4 | 690 | 582 | 17.8 | 50 | 43 | 0.41 | 15.8 | 201 | 39.3 | 100 | 87 | 0.45 |
| 465 | Stability bracing lower ca. | 90x90x9 | 1 | M16 | 0.4 | 1539 | 1377 | 0.3 | 50 | 43 | 0.01 | 0.6 | 201 | 3.0 | 100 | 87 | 0.03 |
| 475 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 13.1 | 940 | 808 | 16.3 | 50 | 43 | 0.37 | 18.4 | 314 | 29.3 | 100 | 87 | 0.34 |
| 476 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 15.5 | 940 | 808 | 19.1 | 50 | 43 | 0.44 | 21.5 | 314 | 34.3 | 100 | 87 | 0.39 |
| 477 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 11.8 | 940 | 808 | 14.6 | 50 | 43 | 0.34 | 17.6 | 314 | 28.1 | 100 | 87 | 0.32 |
| 478 | Diag lower plane lower ca. | 80x80x6 | 2 | M20 | 13.0 | 940 | 808 | 16.1 | 50 | 43 | 0.37 | 19.8 | 314 | 31.6 | 100 | 87 | 0.36 |
| 479 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 14.5 | 810 | 678 | 21.4 | 50 | 43 | 0.49 | 22.2 | 314 | 35.3 | 100 | 87 | 0.41 |
| 480 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 16.3 | 810 | 678 | 24.0 | 50 | 43 | 0.55 | 24.9 | 314 | 39.6 | 100 | 87 | 0.46 |
| 481 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 18.7 | 810 | 678 | 27.6 | 50 | 43 | 0.63 | 28.5 | 314 | 45.4 | 100 | 87 | 0.52 |
| 482 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 22.1 | 810 | 678 | 32.6 | 50 | 43 | 0.75 | 33.7 | 314 | 53.7 | 100 | 87 | 0.62 |
| 483 | Diag lower plane lower ca. | 70x70x6 | 2 | M20 | 25.6 | 810 | 678 | 37.8 | 50 | 43 | 0.87 | 39.1 | 314 | 62.3 | 100 | 87 | 0.72 |
| 484 | Diag lower plane lower ca. | 70x70x6 | 2 | M16 | 12.6 | 810 | 702 | 18.0 | 50 | 43 | 0.41 | 19.3 | 157 | 61.4 | 100 | 87 | 0.71 |
| 485 | Plan bracing lower ca. | 120x120x10 | 3 | M24 | 28.4 | 2320 | 2060 | 13.8 | 50 | 43 | 0.32 | 42.8 | 452 | 31.5 | 100 | 87 | 0.36 |
| 486 | Plan bracing lower ca. | 70x70x6 | 1 | M16 | 0.0 | 810 | 702 | 0.1 | 50 | 43 | 0.00 | 0.1 | 201 | 0.3 | 100 | 87 | 0.00 |
| 500 | Horizontal mid ca. | 200x200x18 | 10 | M24 | 128.8 | 6910 | 6442 | 20.0 | 50 | 43 | 0.46 | 195.5 | 452 | 43.2 | 100 | 87 | 0.50 |
| 501 | Lower chord mid ca. | 180x180x18 | 10 | M24 | 220.9 | 6190 | 5722 | 38.6 | 50 | 43 | 0.89 | 335.3 | 452 | 74.2 | 100 | 87 | 0.85 |
| 502 | Lower chord mid ca. | 180x180x18 | 0 | | 213.9 | 6190 | 6190 | 34.6 | 50 | 43 | 0.79 | 325.3 | 0 | 0.0 | 100 | 87 | 0.00 |
| 503 | Lower chord mid ca. | 180x180x18 | 0 | | 196.2 | 6190 | 6190 | 31.7 | 50 | 43 | 0.73 | 299.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 504 | Lower chord mid ca. | 180x180x18 | 8 | M24 | 172.7 | 6190 | 5722 | 30.2 | 50 | 43 | 0.69 | 263.6 | 452 | 72.9 | 100 | 87 | 0.84 |
| 505 | Lower chord mid ca. | 160x160x15 | 8 | M24 | 149.0 | 4671 | 4281 | 34.8 | 50 | 43 | 0.80 | 227.5 | 452 | 62.9 | 100 | 87 | 0.72 |
| 506 | Lower chord mid ca. | 160x160x15 | 0 | | 108.6 | 4671 | 4671 | 23.3 | 50 | 43 | 0.53 | 165.8 | 0 | 0.0 | 100 | 87 | 0.00 |
| 507 | Lower chord mid ca. | 160x160x15 | 0 | | 72.8 | 4671 | 4671 | 15.6 | 50 | 43 | 0.36 | 111.1 | 0 | 0.0 | 100 | 87 | 0.00 |
| 508 | Lower chord mid ca. | 160x160x15 | 0 | | 39.5 | 4671 | 4671 | 8.5 | 50 | 43 | 0.19 | 60.3 | 0 | 0.0 | 100 | 87 | 0.00 |
| 509 | Lower chord mid ca. | 160x160x15 | 3 | M20 | 0.3 | 4671 | 4341 | 0.1 | 50 | 43 | 0.00 | 0.4 | 314 | 0.7 | 100 | 87 | 0.01 |
| 511 | Horizontal mid ca. | 150x150x12 | 3 | M24 | 39.4 | 3480 | 3168 | 12.4 | 50 | 43 | 0.29 | 59.9 | 452 | 44.2 | 100 | 87 | 0.51 |
| 512 | Beam mid ca. | 150x150x14 (not coup | 2 | M24 | 15.5 | 8028 | 7664 | 2.0 | 50 | 43 | 0.05 | 21.5 | 452 | 23.8 | 100 | 87 | 0.27 |
| 513 | Horizontal mid ca. | HEA140 | 0 | | 0.4 | 3140 | 3140 | 0.1 | 50 | 43 | 0.00 | 0.6 | 0 | 0.0 | 100 | 87 | 0.00 |
| 514 | Beam mid ca. | 150x150x18 (not coup | 2 | M24 | 25.1 | 10200 | 9732 | 2.6 | 50 | 43 | 0.06 | 38.4 | 452 | 42.4 | 100 | 87 | 0.49 |



Check galloping- 140gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | | | | | | Controle boutdoorsnede | | | | |
|-------|----------------------------|------------|---------------|------|----------------------------------|--------------|-------------|------------------------|------------|--------------------------|---------------|-------------------|------------|--------------------------|------------------------|--------------------------|---------|--|--|
| | | | | | $\Delta F;0$ [kN] | Brutto [mm2] | Netto [mm2] | $\Delta\sigma;0$ [Mpa] | DC;0 [Mpa] | $\Delta\sigma;c;0$ [Mpa] | UC opp. [Mpa] | $\Delta F;b$ [kN] | Bout [mm2] | $\Delta\sigma;i;b$ [Mpa] | DC;b [Mpa] | $\Delta\sigma;c;b$ [Mpa] | UC bout | | |
| 515 | Horizontaal mid ca. | HEB220 | 0 | 0 | 2.7 | 9104 | 9104 | 0.3 | 50 | 43 | 0.01 | 4.1 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 516 | Beam mid ca. | UNP220 | 0 | 0 | 7.8 | 3740 | 3740 | 2.1 | 50 | 43 | 0.05 | 11.9 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 526 | Upper chord mid ca. | 120x120x12 | 4 | M24 | 36.4 | 2750 | 2438 | 14.9 | 50 | 43 | 0.34 | 55.2 | 452 | 30.5 | 100 | 87 | 0.35 | | |
| 527 | Upper chord mid ca. | 120x120x12 | 0 | 0 | 36.8 | 2750 | 2750 | 13.4 | 50 | 43 | 0.31 | 55.9 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 528 | Upper chord mid ca. | 120x120x12 | 6 | M24 | 35.9 | 2750 | 2438 | 14.7 | 50 | 43 | 0.34 | 54.5 | 452 | 20.1 | 100 | 87 | 0.23 | | |
| 529 | Upper chord mid ca. | 120x120x12 | 6 | M24 | 33.0 | 2750 | 2438 | 13.5 | 50 | 43 | 0.31 | 50.1 | 452 | 18.5 | 100 | 87 | 0.21 | | |
| 530 | Upper chord mid ca. | 120x120x12 | 0 | 0 | 30.3 | 2750 | 2750 | 11.0 | 50 | 43 | 0.25 | 46.0 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 531 | Upper chord mid ca. | 120x120x12 | 0 | 0 | 28.0 | 2750 | 2438 | 11.5 | 50 | 43 | 0.23 | 42.6 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 532 | Upper chord mid ca. | 120x120x12 | 4 | M24 | 28.0 | 2750 | 2438 | 11.5 | 50 | 43 | 0.26 | 42.6 | 452 | 23.6 | 100 | 87 | 0.27 | | |
| 533 | Upper chord mid ca. | 120x120x12 | 2 | M24 | 30.1 | 2750 | 2438 | 12.3 | 50 | 43 | 0.28 | 45.8 | 452 | 50.7 | 100 | 87 | 0.58 | | |
| 535 | Stability bracing mid ca. | 70x70x6 | 1 | M16 | 0.3 | 810 | 702 | 0.4 | 50 | 43 | 0.01 | 0.4 | 201 | 2.0 | 100 | 87 | 0.02 | | |
| 536 | Hand rail | 60x60x6 | 1 | M16 | 0.1 | 690 | 582 | 0.1 | 50 | 43 | 0.00 | 0.1 | 201 | 0.5 | 100 | 87 | 0.01 | | |
| 537 | Hand rail | 100x50x6 | 2 | M16 | 0.0 | 870 | 762 | 0.0 | 50 | 43 | 0.00 | 0.0 | 201 | 0.0 | 100 | 87 | 0.00 | | |
| 538 | Hand rail | 60x60x6 | 1 | M16 | 0.0 | 690 | 582 | 0.1 | 50 | 43 | 0.00 | 0.0 | 201 | 0.2 | 100 | 87 | 0.00 | | |
| 539 | Stability bracing mid ca. | 70x70x6 | 1 | M16 | 1.4 | 810 | 702 | 1.9 | 50 | 43 | 0.04 | 2.1 | 201 | 10.3 | 100 | 87 | 0.12 | | |
| 540 | Vertical side face mid ca. | 80x80x6 | 1 | M16 | 3.1 | 940 | 832 | 3.7 | 50 | 43 | 0.09 | 4.3 | 201 | 21.6 | 100 | 87 | 0.25 | | |
| 541 | Vertical side face mid ca. | 80x80x6 | 1 | M16 | 3.0 | 940 | 832 | 3.6 | 50 | 43 | 0.08 | 4.3 | 201 | 21.5 | 100 | 87 | 0.25 | | |
| 542 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 1.6 | 690 | 582 | 2.7 | 50 | 43 | 0.06 | 2.4 | 201 | 12.1 | 100 | 87 | 0.14 | | |
| 543 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 2.0 | 690 | 582 | 3.5 | 50 | 43 | 0.08 | 3.1 | 201 | 15.3 | 100 | 87 | 0.18 | | |
| 544 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 2.5 | 690 | 582 | 4.3 | 50 | 43 | 0.10 | 3.8 | 201 | 19.0 | 100 | 87 | 0.22 | | |
| 545 | Vertical side face mid ca. | 60x60x6 | 1 | M16 | 0.7 | 690 | 582 | 1.2 | 50 | 43 | 0.03 | 1.1 | 201 | 5.5 | 100 | 87 | 0.06 | | |
| 546 | Vertical side face mid ca. | 60x60x6 | 2 | M16 | 11.5 | 690 | 582 | 19.7 | 50 | 43 | 0.45 | 17.5 | 201 | 43.5 | 100 | 87 | 0.50 | | |
| 560 | Diag side face mid ca. | 80x80x6 | 2 | M16 | 2.9 | 940 | 832 | 3.5 | 50 | 43 | 0.08 | 4.4 | 201 | 10.8 | 100 | 87 | 0.12 | | |
| 561 | Diag side face mid ca. | 70x70x6 | 2 | M16 | 4.7 | 810 | 702 | 6.7 | 50 | 43 | 0.15 | 6.6 | 201 | 16.4 | 100 | 87 | 0.19 | | |
| 562 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 4.7 | 690 | 582 | 8.1 | 50 | 43 | 0.19 | 6.8 | 201 | 16.9 | 100 | 87 | 0.19 | | |
| 563 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 2.8 | 690 | 582 | 4.8 | 50 | 43 | 0.11 | 4.3 | 201 | 10.6 | 100 | 87 | 0.12 | | |
| 564 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 4.8 | 690 | 582 | 8.3 | 50 | 43 | 0.19 | 7.3 | 201 | 18.3 | 100 | 87 | 0.21 | | |
| 565 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 5.5 | 690 | 582 | 9.4 | 50 | 43 | 0.22 | 8.3 | 201 | 20.7 | 100 | 87 | 0.24 | | |
| 566 | Diag side face mid ca. | 60x60x6 | 2 | M16 | 6.2 | 690 | 582 | 10.7 | 50 | 43 | 0.25 | 9.5 | 201 | 23.7 | 100 | 87 | 0.27 | | |
| 567 | Stability bracing mid ca. | 70x70x6 | 1 | M16 | 0.5 | 810 | 702 | 0.7 | 50 | 43 | 0.02 | 0.7 | 201 | 3.4 | 100 | 87 | 0.04 | | |
| 575 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 10.5 | 810 | 678 | 15.5 | 50 | 43 | 0.36 | 14.6 | 314 | 23.3 | 100 | 87 | 0.27 | | |
| 576 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 12.8 | 810 | 678 | 18.8 | 50 | 43 | 0.43 | 17.8 | 314 | 28.4 | 100 | 87 | 0.33 | | |
| 577 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 13.4 | 810 | 678 | 19.8 | 50 | 43 | 0.46 | 18.7 | 314 | 29.8 | 100 | 87 | 0.34 | | |
| 578 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 14.8 | 810 | 678 | 21.8 | 50 | 43 | 0.50 | 20.7 | 314 | 33.0 | 100 | 87 | 0.38 | | |
| 579 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 15.5 | 810 | 678 | 22.9 | 50 | 43 | 0.53 | 21.6 | 314 | 34.5 | 100 | 87 | 0.40 | | |



Check galloping- 140gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | | | | | | Controle boutdoorsnede | | | | |
|-------|--------------------------|----------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|--------------|---------------|-------------|-----------------|--------------|------------------------|--------------|---------|--|--|
| | | | | | ΔF;o [kN] | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. [Mpa] | ΔF;i;b [kN] | Opp. Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa] | Δσ;c;b [Mpa] | UC bout | | |
| 580 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 13.1 | 810 | 678 | 19.4 | 50 | 43 | 0.45 | 19.6 | 314 | 31.2 | 100 | 87 | 0.36 | | |
| 581 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 14.8 | 810 | 678 | 21.9 | 50 | 43 | 0.50 | 22.6 | 314 | 36.0 | 100 | 87 | 0.41 | | |
| 582 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 15.8 | 810 | 678 | 23.3 | 50 | 43 | 0.54 | 24.2 | 314 | 38.5 | 100 | 87 | 0.44 | | |
| 583 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 18.2 | 810 | 678 | 26.8 | 50 | 43 | 0.62 | 27.7 | 314 | 44.1 | 100 | 87 | 0.51 | | |
| 584 | Diag lower plane mid ca. | 70x70x6 | 2 | M20 | 20.7 | 810 | 678 | 30.5 | 50 | 43 | 0.70 | 31.6 | 314 | 50.3 | 100 | 87 | 0.58 | | |
| 585 | Diag lower plane mid ca. | 80x80x6 | 2 | M20 | 25.2 | 940 | 808 | 31.1 | 50 | 43 | 0.72 | 38.4 | 314 | 61.2 | 100 | 87 | 0.70 | | |
| 586 | Diag lower plane mid ca. | 80x80x6 | 2 | M20 | 29.0 | 940 | 808 | 35.8 | 50 | 43 | 0.82 | 44.2 | 314 | 70.4 | 100 | 87 | 0.81 | | |
| 587 | Diag lower plane mid ca. | 80x60x6 | 2 | M16 | 12.3 | 690 | 582 | 21.2 | 50 | 43 | 0.49 | 18.8 | 201 | 46.9 | 100 | 87 | 0.54 | | |
| 588 | Plan bracing mid ca. | 140x140x13 | 5 | M24 | 94.3 | 3521 | 3183 | 29.6 | 50 | 43 | 0.68 | 143.4 | 452 | 63.5 | 100 | 87 | 0.73 | | |
| 589 | Plan bracing mid ca. | 150x150x12 | 4 | M24 | 60.4 | 3480 | 3168 | 19.1 | 50 | 43 | 0.44 | 91.8 | 452 | 50.8 | 100 | 87 | 0.58 | | |
| 600 | Horizontal top ca. | 200x200x18 | 10 | M24 | 147.7 | 6910 | 6442 | 22.9 | 50 | 43 | 0.53 | 223.3 | 452 | 49.4 | 100 | 87 | 0.57 | | |
| 601 | Lower chord top ca. | 180x180x18 | 8 | M24 | 192.5 | 6190 | 5722 | 33.6 | 50 | 43 | 0.77 | 293.6 | 452 | 81.2 | 100 | 87 | 0.93 | | |
| 602 | Lower chord top ca. | 180x180x18 | 8 | M24 | 159.8 | 6190 | 5722 | 27.9 | 50 | 43 | 0.64 | 244.0 | 452 | 67.5 | 100 | 87 | 0.78 | | |
| 603 | Lower chord top ca. | 150x150x14 | 8 | M24 | 125.5 | 4014 | 3650 | 34.4 | 50 | 43 | 0.79 | 191.6 | 452 | 53.0 | 100 | 87 | 0.61 | | |
| 604 | Lower chord top ca. | 150x150x14 | 0 | 0 | 64.4 | 4014 | 4014 | 16.0 | 50 | 43 | 0.37 | 98.2 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 605 | Lower chord top ca. | 150x150x14 | 0 | 0 | 33.4 | 4014 | 4014 | 8.3 | 50 | 43 | 0.19 | 50.8 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 606 | Lower chord top ca. | 150x150x14 | 2 | M20 | 5.8 | 4014 | 3706 | 1.6 | 50 | 43 | 0.04 | 8.5 | 314 | 13.5 | 100 | 87 | 0.16 | | |
| 608 | Earth peak lower chord | 80x80x8 | 2 | M20 | 7.3 | 1230 | 1054 | 6.9 | 50 | 43 | 0.16 | 10.6 | 314 | 16.9 | 100 | 87 | 0.19 | | |
| 609 | Earth peak lower chord | 80x80x8 | 2 | M20 | 6.8 | 1230 | 1054 | 6.4 | 50 | 43 | 0.15 | 9.5 | 314 | 15.2 | 100 | 87 | 0.17 | | |
| 610 | Horizontal top ca. | 130x130x12 | 3 | M24 | 42.9 | 3000 | 2688 | 16.0 | 50 | 43 | 0.37 | 64.3 | 452 | 47.4 | 100 | 87 | 0.55 | | |
| 611 | Horizontal top ca. | 150x150x14 (not coup | 2 | M24 | 13.1 | 8028 | 7664 | 1.7 | 50 | 43 | 0.04 | 20.1 | 452 | 22.2 | 100 | 87 | 0.26 | | |
| 612 | Horizontal top ca. | HEA140 | 0 | 0 | 0.9 | 3140 | 3140 | 0.3 | 50 | 43 | 0.01 | 1.3 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 613 | Horizontal top ca. | 150x150x18 (not coup | 2 | M24 | 26.2 | 10200 | 9732 | 2.7 | 50 | 43 | 0.06 | 40.0 | 452 | 44.3 | 100 | 87 | 0.51 | | |
| 614 | Beam top ca. | HEB220 | 0 | 0 | 2.3 | 9104 | 9104 | 0.3 | 50 | 43 | 0.01 | 3.6 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 615 | Earth peak horizontal | 60x60x6 | 1 | M16 | 0.9 | 690 | 582 | 1.5 | 50 | 43 | 0.03 | 1.3 | 201 | 6.3 | 100 | 87 | 0.07 | | |
| 616 | Earth peak horizontal | 60x60x6 | 1 | M16 | 0.9 | 690 | 582 | 1.5 | 50 | 43 | 0.03 | 1.3 | 201 | 6.4 | 100 | 87 | 0.07 | | |
| 617 | Earth peak horizontal | 60x60x6 | 1 | M16 | 0.9 | 690 | 582 | 0.0 | 50 | 43 | 0.00 | 0.0 | 201 | 0.2 | 100 | 87 | 0.00 | | |
| 618 | Beam top ca. | UNP220 | 0 | 0 | 5.0 | 3740 | 3740 | 1.3 | 50 | 43 | 0.03 | 7.7 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 626 | Upper chord top ca. | 120x120x12 | 0 | 0 | 42.8 | 2750 | 2750 | 15.6 | 50 | 43 | 0.36 | 65.3 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 627 | Upper chord top ca. | 100x100x10 | 3 | M24 | 18.7 | 1920 | 1660 | 11.3 | 50 | 43 | 0.26 | 28.1 | 452 | 20.8 | 100 | 87 | 0.24 | | |
| 628 | Upper chord top ca. | 100x100x10 | 6 | M24 | 17.7 | 1920 | 1660 | 10.7 | 50 | 43 | 0.25 | 26.9 | 452 | 9.9 | 100 | 87 | 0.11 | | |
| 629 | Upper chord top ca. | 100x100x10 | 3 | M24 | 17.2 | 1920 | 1660 | 10.4 | 50 | 43 | 0.24 | 26.2 | 452 | 19.3 | 100 | 87 | 0.22 | | |
| 630 | Earth peak upper chord | 130x130x12 | 0 | 0 | 59.1 | 3000 | 3000 | 19.7 | 50 | 43 | 0.45 | 80.4 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 631 | Earth peak upper chord | 130x130x12 | 4 | M24 | 50.9 | 3000 | 2688 | 18.9 | 50 | 43 | 0.44 | 71.4 | 452 | 39.5 | 100 | 87 | 0.45 | | |
| 632 | Earth peak upper chord | 120x120x10 | 4 | M24 | 48.8 | 2320 | 2060 | 23.7 | 50 | 43 | 0.55 | 68.5 | 452 | 37.9 | 100 | 87 | 0.44 | | |



Check galloping- 140gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLI-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | | | | | | Controle boutdoorsnede | | | | |
|-------|-------------------------------|------------|---------------|------|----------------------------------|--------------|-------------|-------------------------|------------|-------------------------|--------------|-----------------|-------------------------|------------|-------------------------|---------|------|--|--|
| | | | | | ΔF_o [kN] | Brutto [mm2] | Netto [mm2] | $\Delta \sigma_i$ [Mpa] | DC;o [Mpa] | $\Delta \sigma_c$ [Mpa] | UC opp. [kN] | Opp. Bout [mm2] | $\Delta \sigma_i$ [Mpa] | DC;b [Mpa] | $\Delta \sigma_c$ [Mpa] | UC bout | | | |
| 633 | Earth peak upper chord | 120x120x10 | 0 | 0 | 43.0 | 2320 | 2320 | 18.5 | 50 | 43 | 0.43 | 60.3 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 634 | Earth peak upper chord | 120x120x10 | 0 | 0 | 33.6 | 2320 | 2320 | 14.5 | 50 | 43 | 0.33 | 47.1 | 0 | 0.0 | 100 | 87 | 0.00 | | |
| 635 | Earth peak upper chord | 120x120x10 | 2 | M20 | 18.8 | 2320 | 2100 | 8.9 | 50 | 43 | 0.21 | 26.2 | 314 | 41.8 | 100 | 87 | 0.48 | | |
| 637 | Stability bracing top ca. | 70x70x7 | 1 | M16 | 8.7 | 940 | 814 | 10.7 | 50 | 43 | 0.25 | 13.1 | 201 | 65.3 | 100 | 87 | 0.75 | | |
| 638 | Earth peak horizontal | HEB160 | 2 | M20 | 4.5 | 5430 | 5254 | 0.9 | 50 | 43 | 0.15 | 6.4 | 314 | 10.1 | 100 | 87 | 0.15 | | |
| 640 | Vertical side face top ca. | 60x60x6 | 2 | M16 | 3.7 | 690 | 582 | 6.4 | 50 | 43 | 0.52 | 19.9 | 201 | 49.4 | 100 | 87 | 0.57 | | |
| 641 | Vertical side face top ca. | 60x60x6 | 2 | M16 | 13.2 | 690 | 582 | 22.7 | 50 | 43 | 0.08 | 4.3 | 201 | 21.5 | 100 | 87 | 0.25 | | |
| 642 | Vertical side face top ca. | 80x80x6 | 1 | M16 | 2.9 | 940 | 832 | 3.5 | 50 | 43 | 0.01 | 0.3 | 201 | 1.7 | 100 | 87 | 0.02 | | |
| 643 | Vertical side face top ca. | 80x80x6 | 1 | M16 | 0.2 | 940 | 832 | 0.3 | 50 | 43 | 0.01 | 0.3 | 201 | 1.7 | 100 | 87 | 0.02 | | |
| 644 | Vertical side face top ca. | 80x80x6 | 1 | M16 | 7.4 | 940 | 832 | 8.9 | 50 | 43 | 0.20 | 11.3 | 201 | 56.0 | 100 | 87 | 0.64 | | |
| 645 | Vertical side face top ca. | 80x80x8 | 1 | M16 | 0.1 | 1230 | 1086 | 0.1 | 50 | 43 | 0.00 | 0.2 | 201 | 0.8 | 100 | 87 | 0.01 | | |
| 646 | Earth peak vertical side face | 60x60x6 | 1 | M16 | 0.3 | 690 | 582 | 0.5 | 50 | 43 | 0.01 | 0.4 | 201 | 1.8 | 100 | 87 | 0.02 | | |
| 660 | Diag side face top ca. | 80x80x6 | 2 | M16 | 5.8 | 940 | 832 | 7.0 | 50 | 43 | 0.16 | 8.1 | 201 | 20.0 | 100 | 87 | 0.23 | | |
| 661 | Diag side face top ca. | 80x80x8 | 2 | M16 | 5.0 | 1230 | 1086 | 4.6 | 50 | 43 | 0.11 | 7.6 | 201 | 18.8 | 100 | 87 | 0.22 | | |
| 662 | Diag side face top ca. | 80x80x8 | 2 | M20 | 8.0 | 1230 | 1054 | 7.6 | 50 | 43 | 0.17 | 12.0 | 314 | 19.0 | 100 | 87 | 0.22 | | |
| 663 | Earth peak diag side face | 80x80x6 | 2 | M16 | 16.5 | 1230 | 1086 | 15.2 | 50 | 43 | 0.35 | 24.9 | 201 | 62.0 | 100 | 87 | 0.71 | | |
| 673 | Stability bracing top ca. | 80x80x8 | 2 | M16 | 7.6 | 690 | 582 | 13.0 | 50 | 43 | 0.30 | 10.6 | 201 | 26.4 | 100 | 87 | 0.30 | | |
| 675 | Earth peak diag upper side | 60x60x6 | 2 | M16 | 6.1 | 690 | 582 | 10.4 | 50 | 43 | 0.24 | 8.5 | 201 | 21.2 | 100 | 87 | 0.24 | | |
| 676 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 13.1 | 810 | 678 | 19.3 | 50 | 43 | 0.44 | 18.3 | 314 | 29.1 | 100 | 87 | 0.33 | | |
| 677 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 16.4 | 810 | 678 | 24.1 | 50 | 43 | 0.55 | 22.9 | 314 | 36.5 | 100 | 87 | 0.42 | | |
| 678 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 15.4 | 810 | 678 | 22.7 | 50 | 43 | 0.52 | 21.5 | 314 | 34.2 | 100 | 87 | 0.39 | | |
| 679 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 13.9 | 810 | 678 | 20.5 | 50 | 43 | 0.47 | 21.2 | 314 | 33.8 | 100 | 87 | 0.39 | | |
| 680 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 15.3 | 810 | 678 | 22.5 | 50 | 43 | 0.52 | 23.3 | 314 | 37.1 | 100 | 87 | 0.43 | | |
| 681 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 23.9 | 810 | 678 | 35.3 | 50 | 43 | 0.81 | 36.5 | 314 | 58.2 | 100 | 87 | 0.67 | | |
| 682 | Diag lower plane top ca. | 70x70x6 | 2 | M20 | 27.2 | 810 | 678 | 40.1 | 50 | 43 | 0.92 | 41.6 | 314 | 66.2 | 100 | 87 | 0.76 | | |
| 683 | Diag lower plane top ca. | 80x80x6 | 2 | M20 | 28.9 | 940 | 808 | 35.8 | 50 | 43 | 0.82 | 44.1 | 314 | 70.3 | 100 | 87 | 0.81 | | |
| 684 | Diag lower plane top ca. | 80x80x6 | 2 | M20 | 30.1 | 940 | 808 | 37.3 | 50 | 43 | 0.86 | 46.0 | 314 | 73.2 | 100 | 87 | 0.84 | | |
| 685 | Diag lower plane top ca. | 60x60x6 | 2 | M16 | 11.9 | 690 | 582 | 20.5 | 50 | 43 | 0.47 | 18.2 | 201 | 45.3 | 100 | 87 | 0.52 | | |
| 686 | Earth peak diag lower plane | 70x70x7 | 1 | M16 | 0.4 | 940 | 814 | 0.5 | 50 | 43 | 0.01 | 0.6 | 201 | 3.1 | 100 | 87 | 0.04 | | |
| 687 | Earth peak diag lower plane | 70x70x7 | 1 | M16 | 2.6 | 940 | 814 | 3.2 | 50 | 43 | 0.07 | 3.8 | 201 | 19.0 | 100 | 87 | 0.22 | | |
| 688 | Earth peak diag upper plane | 70x70x6 | 2 | M16 | 8.4 | 810 | 702 | 12.0 | 50 | 43 | 0.28 | 12.5 | 201 | 31.1 | 100 | 87 | 0.36 | | |
| 689 | Earth peak diag upper plane | 70x70x6 | 2 | M16 | 9.3 | 810 | 702 | 13.2 | 50 | 43 | 0.30 | 13.8 | 201 | 34.3 | 100 | 87 | 0.39 | | |
| 690 | Earth peak diag upper plane | 60x60x6 | 2 | M16 | 9.9 | 690 | 582 | 17.1 | 50 | 43 | 0.39 | 14.8 | 201 | 36.8 | 100 | 87 | 0.42 | | |



Check galloping- 140gr

Datum: 16-7-2021
 Auteur: TBR
 Versie: 1.0

RLT-TBG
 HC+0/c

| Group | Omschrijving | Profiel | Aantal bouten | Bout | Controle netto oppervlak profiel | | | | | Controle boutdoorsnede | | | | | | | |
|-------|-------------------------------|-----------------------|---------------|------|----------------------------------|--------------|-------------|------------------------|------------|--------------------------|---------|-------------------|-----------------|--------------------------|------------|--------------------------|---------|
| | | | | | $\Delta F;0$ [kN] | Brutto [mm2] | Netto [mm2] | $\Delta\sigma;0$ [Mpa] | DC;0 [Mpa] | $\Delta\sigma;c;0$ [Mpa] | UC opp. | $\Delta F;b$ [kN] | Opp. Bout [mm2] | $\Delta\sigma;i;b$ [Mpa] | DC;b [Mpa] | $\Delta\sigma;c;b$ [Mpa] | UC bout |
| 691 | Earth peak diag upper plane | 60x60x6 | 2 | M16 | 10.9 | 690 | 582 | 18.8 | 50 | 43 | 0.43 | 16.3 | 201 | 40.5 | 100 | 87 | 0.47 |
| 692 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 2.3 | 690 | 582 | 3.9 | 50 | 43 | 0.09 | 3.2 | 201 | 15.7 | 100 | 87 | 0.18 |
| 693 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 2.4 | 690 | 582 | 4.2 | 50 | 43 | 0.10 | 3.4 | 201 | 17.1 | 100 | 87 | 0.20 |
| 694 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 2.8 | 690 | 582 | 4.9 | 50 | 43 | 0.11 | 4.0 | 201 | 19.9 | 100 | 87 | 0.23 |
| 695 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 3.3 | 690 | 582 | 5.6 | 50 | 43 | 0.13 | 4.6 | 201 | 22.9 | 100 | 87 | 0.26 |
| 696 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 3.9 | 690 | 582 | 6.7 | 50 | 43 | 0.15 | 5.5 | 201 | 27.2 | 100 | 87 | 0.31 |
| 697 | Earth peak diag upper plane | 60x60x6 | 1 | M16 | 4.7 | 690 | 582 | 8.2 | 50 | 43 | 0.19 | 6.7 | 201 | 33.2 | 100 | 87 | 0.38 |
| 698 | Plan bracing top ca. | 150x150x12 | 4 | M24 | 63.0 | 3480 | 3168 | 19.9 | 50 | 43 | 0.46 | 94.7 | 452 | 52.4 | 100 | 87 | 0.60 |
| 699 | Plan bracing top ca. | 140x140x13 | 5 | M24 | 103.7 | 3521 | 3183 | 32.6 | 50 | 43 | 0.75 | 155.7 | 452 | 68.9 | 100 | 87 | 0.79 |
| 700 | Hor. Plan bracing hip structu | 100x100x8 | 2 | M20 | 2.4 | 1550 | 1374 | 1.8 | 50 | 43 | 0.04 | 3.2 | 314 | 5.1 | 100 | 87 | 0.06 |
| 701 | Hor. Plan bracing hip structu | 100x100x8 | 2 | M20 | 0.4 | 1550 | 1374 | 0.3 | 50 | 43 | 0.01 | 0.6 | 314 | 1.0 | 100 | 87 | 0.01 |
| 702 | Hor. Plan bracing hip structu | 100x100x8 (not coupl | 2 | M20 | 0.0 | 3100 | 2924 | 0.0 | 50 | 43 | 0.00 | 0.0 | 314 | 0.0 | 100 | 87 | 0.00 |
| 703 | 2nd plan bacing | 130x130x12#(15,0,33 | 3 | M24 | 16.5 | 6040 | 5728 | 2.9 | 50 | 43 | 0.07 | 22.3 | 452 | 16.5 | 100 | 87 | 0.19 |
| 704 | 2nd plan bacing | 90x90x8 | 2 | M20 | 2.7 | 1390 | 1214 | 2.2 | 50 | 43 | 0.05 | 4.0 | 314 | 6.4 | 100 | 87 | 0.07 |
| 705 | 2nd plan bacing | 90x90x8 (not coupled; | 2 | M20 | 0.0 | 2780 | 2604 | 0.0 | 50 | 43 | 0.00 | 0.0 | 314 | 0.0 | 100 | 87 | 0.00 |
| 710 | Horizontal top of lower ca. | 120x120x12 | 4 | M24 | 12.2 | 2750 | 2438 | 5.0 | 50 | 43 | 0.12 | 17.4 | 452 | 9.6 | 100 | 87 | 0.11 |
| 711 | Horizontal top of lower ca. | 130x130x12 | 2 | M24 | 2.2 | 3000 | 2688 | 0.8 | 50 | 43 | 0.02 | 3.1 | 452 | 3.4 | 100 | 87 | 0.04 |
| 712 | Horizontal top of mid ca. | 120x120x12 | 4 | M24 | 12.0 | 2750 | 2438 | 4.9 | 50 | 43 | 0.11 | 16.4 | 452 | 9.0 | 100 | 87 | 0.10 |
| 713 | Horizontal top of mid ca. | 120x120x10 | 2 | M24 | 2.7 | 2320 | 2060 | 1.3 | 50 | 43 | 0.03 | 3.7 | 452 | 4.1 | 100 | 87 | 0.05 |
| 714 | Horizontal top of top ca. | 120x120x12 | 4 | M24 | 20.7 | 2750 | 2438 | 8.5 | 50 | 43 | 0.20 | 31.5 | 452 | 17.4 | 100 | 87 | 0.20 |
| 715 | Horizontal top of top ca. | 100x100x10 | 2 | M24 | 1.0 | 1920 | 1660 | 0.6 | 50 | 43 | 0.01 | 1.5 | 452 | 1.6 | 100 | 87 | 0.02 |



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B.5 Fundatierapport steunmast

ZUID-WEST 380 KV OOST VERBINDINGEN

Definitief ontwerp fundaties steunmasten hoogspanningslijn RLL-TLB

TenneT TSO B.V.

Rapport nr.: 21-1249, Rev. 3

Meridian doc.nr.: 002.678.00 0950630

Datum: 2022-07-07

| | |
|-----------------|------------|
| | |
| DATUM: | 11-07-2022 |
| STATUS TENNET: | DEFINITIEF |
| REVISIE TENNET: | 1.0 |

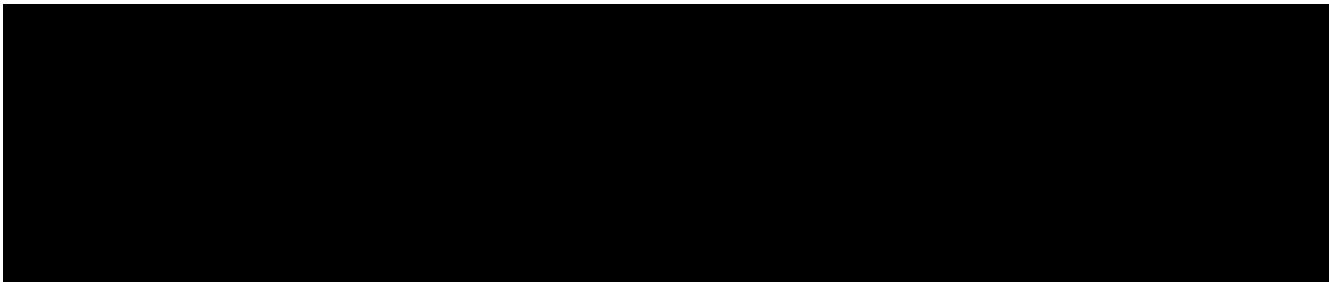




Projectnaam: Zuid-West 380 kV Oost Verbindingen
Rapport titel: Definitief ontwerp fundaties steunmasten
hoogspanningslijn RLL-TLB
Klant: TenneT TSO B.V.,
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Contactpersoon klant: XXXXXXXXXX
Datum uitgave: 2022-07-07
Project nr.: 10124719
Organisatie unit: Overhead Lines (OHL)
Meridian doc.nr.: 002.678.00 0950630
Rapport nr.: 21-1249, Rev. 3

Energy Systems
DNV Netherlands B.V.
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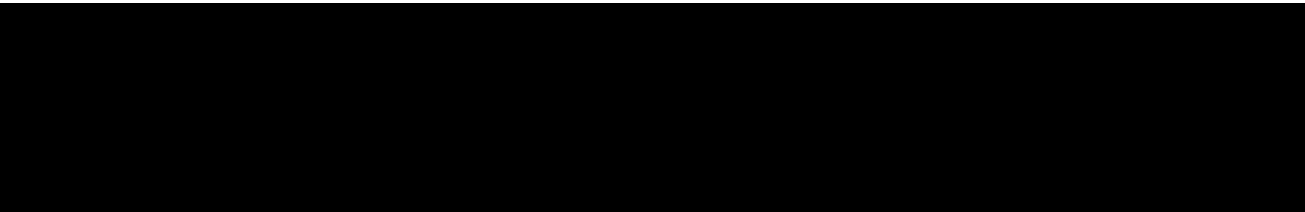


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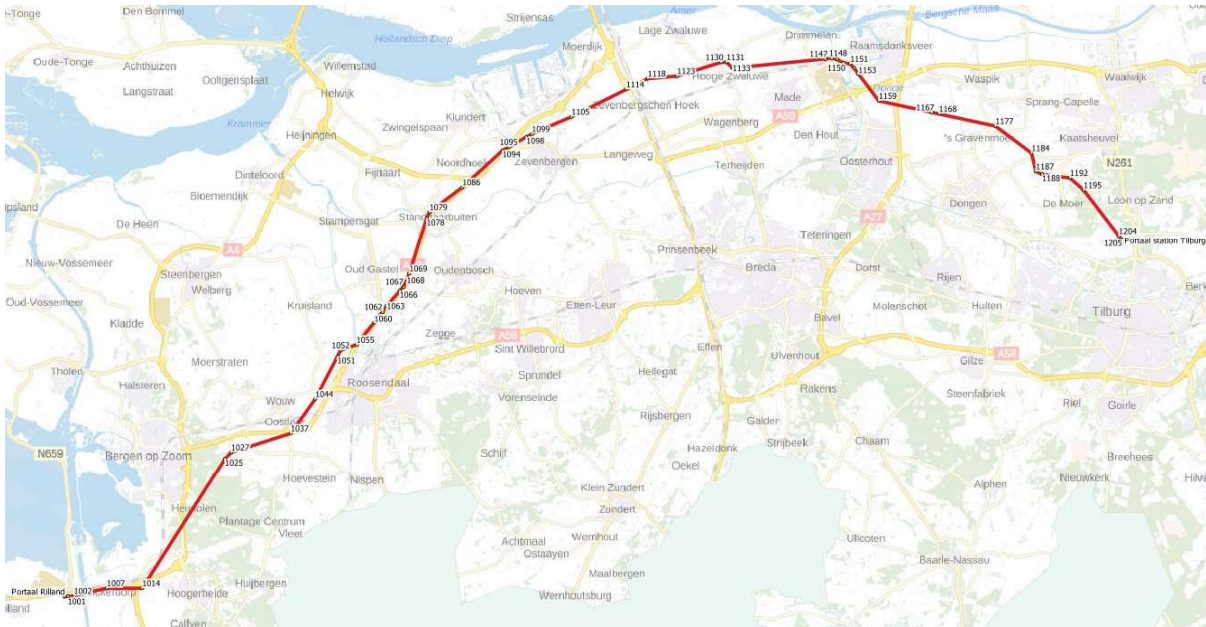


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1 INLEIDING

In het basisonwerp van de verbinding RLL-TLB380 in het project Zuid-West 380 kV-Oost zijn voor het vaststellen van de haalbaarheid constructieve berekeningen uitgevoerd aan de masten en fundaties. In de Definitief Ontwerpfase, moeten berekeningen verder worden uitgewerkt om te kunnen dienen voor de benodigde vergunningsdocumentatie, voor de aanbesteding en als voorbereiding voor de uitvoeringsfase. Het DO omvat het ontwerp van de mastconstructies, de fundaties en de opstijpunten in de verbinding.



Figuur 1 Globale ligging tracé met hoekmastnummers

Het definitieve tracé van de hoogspanningslijn is nog niet vastgesteld. Daardoor zijn sonderingen op de precieze mastlocaties nog niet in uitvoering. Dit heeft tot gevolg dat voor het ontwerp van de fundaties nog geen sonderingen beschikbaar zijn. Om toch een ontwerp op te kunnen stellen is door TenneT een geotechnisch lengteprofiel opgesteld uitgaande van sonderingen in de nabijheid van het tracé. Dit lengteprofiel vormt het uitgangspunt voor de berekeningen.

De uitvoeringsfase van de fundaties zal in de vorm van een UAV GC contractvorm plaatsvinden. Dat houdt in dat in de uitvoeringsfase de sonderingen door de opdrachtnemer worden uitgevoerd. Vervolgens kan de opdrachtnemer het definitieve fundatieontwerp opstellen. De voorliggende rapportage is bedoeld om richting te geven aan het ontwerp op basis van de nu beschikbare gegevens. Het is een indicatie wat verwacht wordt in de uitvoeringsfase.

In het project worden voor mastfundaties enkelpaalsfunderingen en meerpaalsfunderingen toegepast afhankelijk van de bodemgesteldheid, het masttype en de belasting.

Deze rapportage bevat de beschrijving van het constructieve ontwerp van de fundaties voor steunmasten en de toetsing aan de eisen uit de geotechnische normen en TenneT-specificaties. Het aardingsontwerp wordt in een aparte rapportage behandeld.

In hoofdstuk 2 zijn de uitgangspunten en randvoorwaarden vanuit de van toepassing zijnde normen en TenneT-specificaties opgenomen. Hoofdstuk 3 beschrijft het ontwerp van de fundatie. De gevolgde aanpak van de berekening is hoofdstuk 4 opgenomen. Hoofdstuk 5 bevat de resultaten van de uitgevoerde toetsing.

2 UITGANGSPUNTEN EN RANDVOORWAARDEN

2.1 Normen

Er is gebruik gemaakt van de normen volgens Tabel 1.

Tabel 1 Gebruikgemaakte normen, voorschriften en richtlijnen

| Norm | Titel |
|---|--|
| NEN-EN 50341-1:2013 | "Overhead electrical lines exceeding AC 1 kV - Part 1: General requirements – Common" |
| NEN-EN 50341-2-15:2019 | "Overhead electrical lines exceeding AC 1 kV Part 2 National Normative Aspects (NNA) for THE NETHERLANDS" |
| NEN-EN 1990+A1+A1/C2:2011 | "Grondslagen van het ontwerp" |
| NEN-EN 1991-1-4+A1+C2:2011 | "Deel 1-4: Windbelasting op constructies" |
| NEN-EN 1992-1-1+C2:2011/NB:2016+A1:2020 | "Eurocode 2: Ontwerp en berekening van betonconstructies, deel 1-1: algemene regels en regels voor gebouwen" |
| NEN-EN 1993-1-1+C2+A1:2016 nl | "Eurocode 3: Ontwerp en berekening van staalconstructies, deel 1-1: algemene regels en regels voor gebouwen" |
| NEN-EN 1993-1-8+C2:2011/NB:2011 nl | "Ontwerp en berekening van staalconstructies, deel 1-8: ontwerp en berekening van verbindingen" |
| NEN-EN 1997-1+C1+A1:2016/NB:2016 nl | "Geotechnisch – Algemeen" |
| CUR 2001-4 | "Ontwerpregels voor trekpalen" |

2.2 TenneT-specificaties

In Tabel 2 zijn de documenten opgenomen die relevant zijn voor de berekeningen en toetsingen die binnen dit project in de mastrapportage uitgevoerd zullen worden.

Tabel 2 Relevante documenten t.b.v. mechanische rapportages

| Nummer | Onderwerp |
|-----------------|-----------------|
| PVE.05.000 v3.2 | PvE Lijnen |
| sPVE.05.001 | sPvE Lijnen |
| SPE 04.009 | paalfunderingen |

2.3 Ontwerp en eisenverificatie

In Tabel 3 is de lijst opgenomen met documenten die gerelateerd zijn aan deze ontwerpportage van de fundaties van steunmasten. De belastingen in deze rapportage zijn ontleend aan de berekeningen van de mastconstructie zoals beschreven in de volgende rapportages. Daarbij zijn de reacties op de fundatie zoals berekend met PLS-TOWER gebruikt.

Tabel 3 Gerelateerde documenten

| Titel | DNV-nummer | Meridiannummer |
|--|------------|--------------------|
| Uitgangspunten definitief ontwerp Moldaumast | 21-0036 | 002.678.00 0876917 |
| Verificatierapport DO Moldau | 21-1246 | 002.678.00 0950632 |
| Mastrapportage S/s Laag (S+0 - S+9) | 21-0664 | 002.678.00 0920171 |
| Mastrapportage S/s Hoog (S+18/S+24) | 21-1172 | 002.678.00 0946389 |
| Mastrapportage S/c | 21-0728 | 002.678.00 0927722 |

2.4 Materialen

Voor het ontwerp van de mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 4.

Tabel 4 Materialen aangepaste constructie

| | |
|----------------|---|
| Staalsoort | S355J0 (t≤16 mm) S355J2 (16<t≤40 mm) |
| Boutkwaliteit | 8.8 gerolde draad |
| Betonkwaliteit | C30/37 |
| Wapeningsstaal | B500 |

2.5 Software

De gebruikte software wordt benoemd in Tabel 5.

Tabel 5 Toegepaste software

| Software | | Versie |
|-----------------------|----------------------------|--------|
| Mastontwerp | PLS-CADD | 16.65 |
| Mastberekeningen | PLS-TOWER | 16.65 |
| Paalberekening | Technosoft Paalfunderingen | V6 |
| Constructieve analyse | AxisVM | X5 R4h |

2.6 Algemene uitgangspunten

Het ontwerp van de fundaties is gebaseerd op de uitgangspunten volgens Tabel 6.

Tabel 6 Algemene uitgangspunten

| | |
|--|-------------------------------|
| Gevolgklasse | CC2 |
| Geotechnische categorie ¹ | GC2 |
| Ontwerplevensduur fundaties ² | 100 jaar |
| Milieuklasse ³ | XC4/XF3 |
| Uitvoeringsklasse betonconstructies | klasse 3 conform NEN-EN 13670 |

2.7 Sonderingen

Bij het opstellen van deze rapportage zijn nog geen sonderingen beschikbaar aangezien de mastlocaties nog niet definitief zijn vastgesteld. Om te komen tot een ontwerp is door TenneT een geotechnisch lengteprofiel samengesteld. In dit profiel zijn over de lengte van het tracé de hoogtegegevens van het maaiveld weergegeven vanuit de Algemene Hoogtekaart Nederland 3. De vanuit openbare bron (Dino-loket) beschikbare sonderingen in de nabijheid van het tracé zijn weergegeven. Dit betreft elektrische sonderingen in digitaal formaat. Van de mechanische sonderingen die beschikbaar zijn uit de asset-gegevens vanuit de hoogspanningslijnen in de nabijheid van het nieuwe tracé is geen gebruik gemaakt.

De sonderingen bevinden zich doorgaans in de directe nabijheid van het tracé (< 500 m afstand). Voor het verkrijgen van een indicatie is dit voldoende nauwkeurig. Lokaal kunnen echter grote verschillen optreden.

Indien uit nog uit te voeren veld- en bodemonderzoeken naar voren komt dat de sonderingen te veel verschillen (30%) dan is de CUR 114 (toezicht op realisatie van paalfunderingen) van toepassing door opdrachtnemer.

¹ In AM-Req 3260 van TenneT wordt GC3 voorgeschreven, vanwege de bouw van de hoogspanningslijn in een gebied zonder risico voor aardbevingen en het ontbreken van specifieke aanvullende eisen in GC3 aan mastfundaties wordt uitgegaan van GC2.

² Belastingen vanuit de mastconstructie zijn gebaseerd op referentieperiode 50 jaar.

³ Dit is een minimum milieuklasse, bij bijzondere omstandigheden zoals verontreinigde grond kan een zwaardere milieuklasse van toepassing zijn.

2.8 Beschrijving grondopbouw

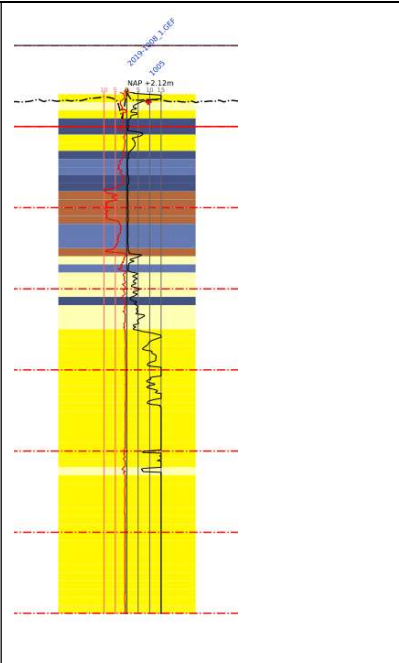
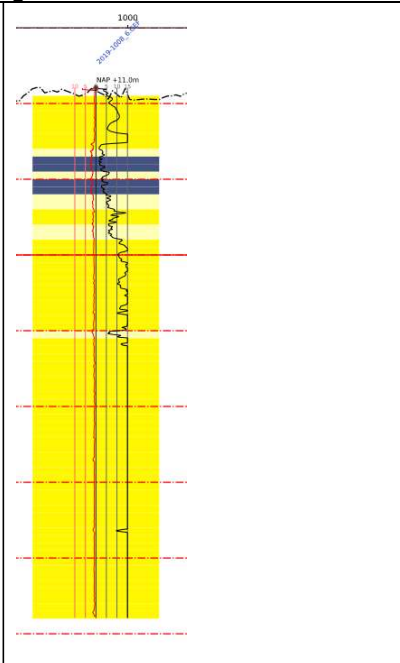
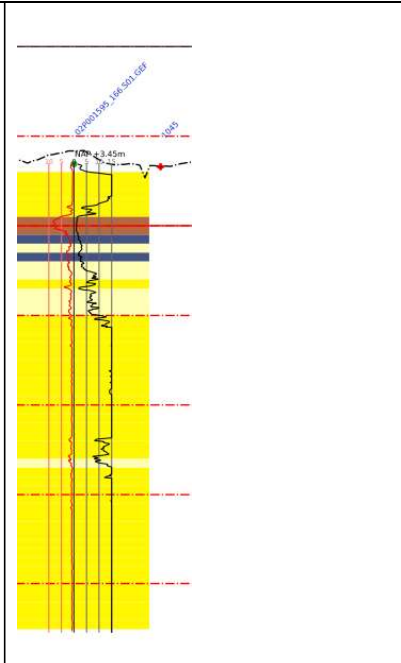
In onderstaande voorbeelden (zie Tabel 3) is de bodemopbouw opgenomen. Voor het beschrijven van de grondopbouw maken we gebruik van de sonderingen die beschikbaar zijn gesteld.

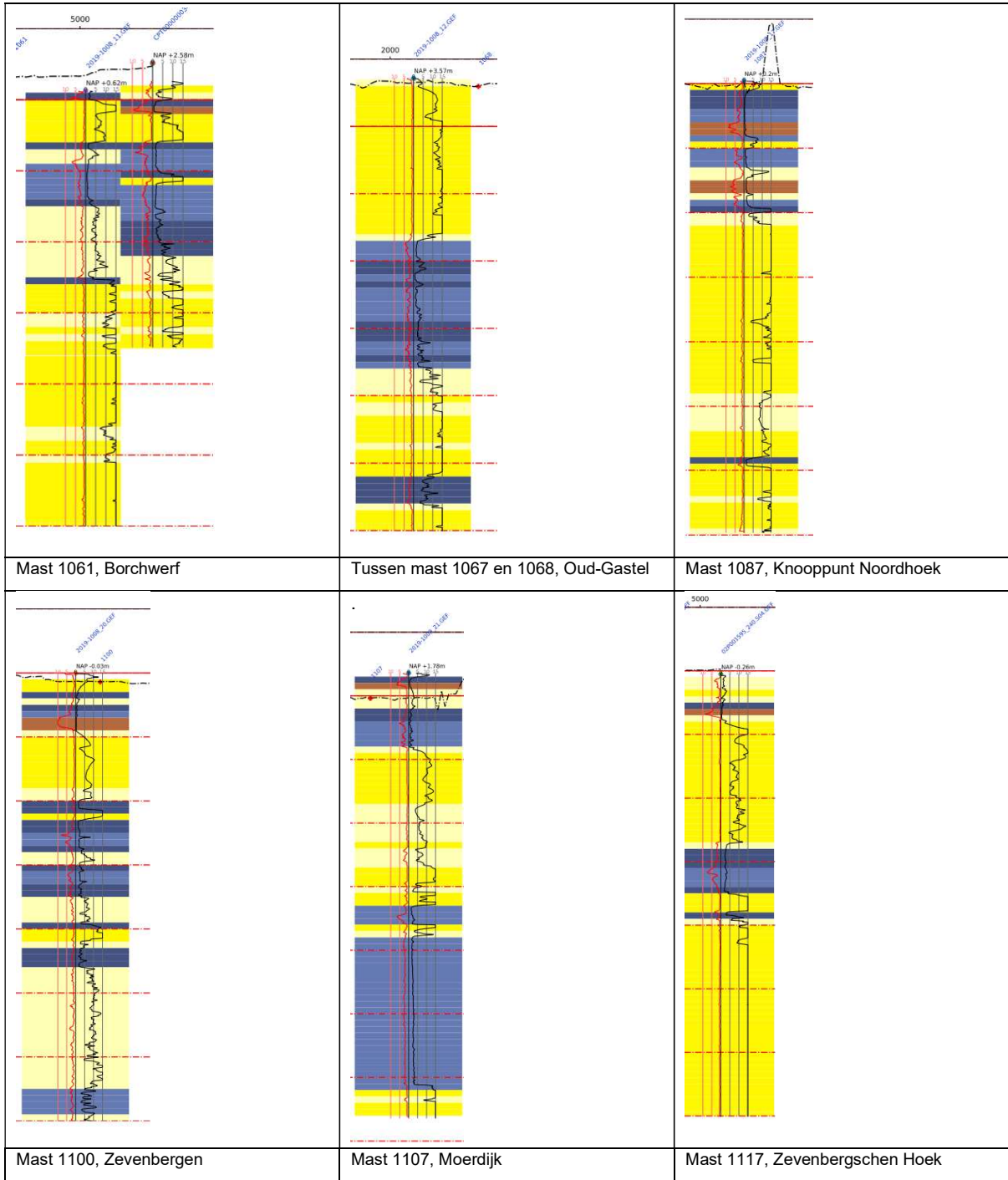
De sonderingen laten over de lengte verschillen zien in ondergrond. Westelijk van Geertruidenberg en dat betekent over circa twee derde van de lengte van het tracé is er een wisselend beeld van zandlagen en cohesieve lagen.

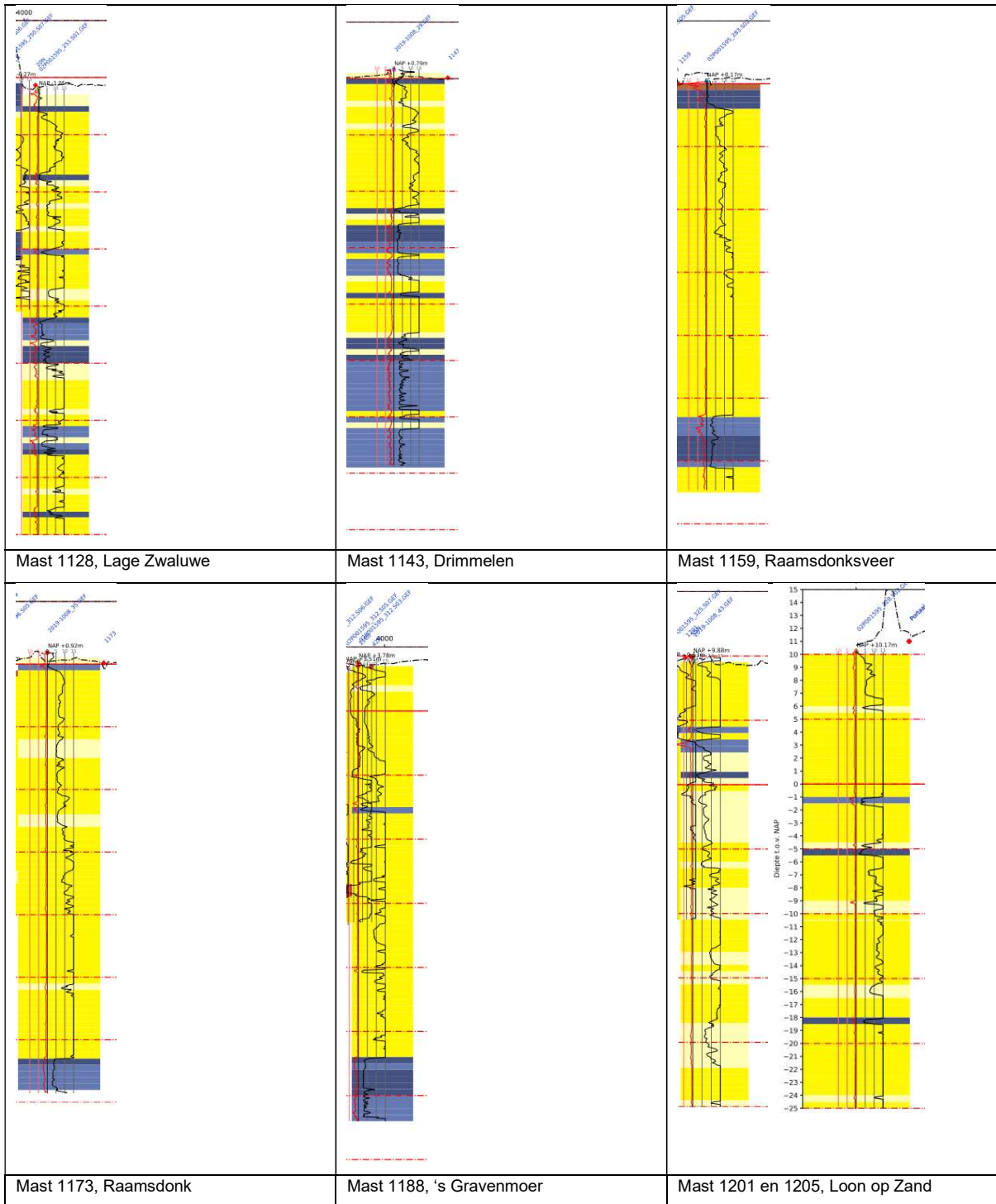
Noemenswaardig is hierbij dat de slappere lagen ook op vrij grote diepte voorkomen met een dikte van meerdere meters. De pakking van de zandlagen is over het algemeen tussen los en matig. Maar er zijn ook locaties met dicht gepakte lagen. Ondiep gelegen slappere lagen komen vooral voor tussen Standdaarbuiten en Moerdijk. Voor afdracht van de horizontale belastingen is dat ongunstig.

Globaal bevindt zich oostelijk van Geertruidenberg over de gehele diepte van de sondering een draagkrachtig zandpakket. Aandachtspunt zijn hier de dieper gelegen kleilagen, die voor de weerstand van de paalpunt op druk nadelige invloed hebben.

Tabel 7 Overzicht voorbeeldsonderingen

| | | |
|--|---|--|
|  |  |  |
| Mast 1005 (omgeving Völckerdorp) | Voor mast 1025, Bergen op Zoom | Mast 1045, knooppunt De Stok |





2.9 Uitgangspunten geotechniek

2.9.1 Paalklassefactoren paaltypes

In tabel 8 zijn de paalklassefactoren van de paaltypes uit deze rapportage op basis van NEN-EN 1997-1 samengevat waarmee de berekeningen worden uitgevoerd.

Tabel 8 Paalklassefactoren enkelpaalsfunderingen steunmasten

| | SI Ø610/850 | SI Ø762/950 |
|---|---------------------|---------------------|
| Paalttype | Schroefinjectiepaal | Schroefinjectiepaal |
| Diameter stalen buis (m) | 0,61 | 0,762 |
| Diameter in berekening (m) ⁴ | 0,73 | 0,86 |
| Factor α_s | 0,009 | 0,009 |
| Factor α_t | 0,009 | 0,009 |
| Factor α_p | 0,63 | 0,63 |
| Factor β | 1,0 | 1,0 |

2.9.2 Kleef cohesieve lagen

In de berekeningen wordt de weerstand van de cohesieve lagen boven de draagkrachtige zandlaag meegenomen. Volgens opmerking (b) van 7.6.3.3 (8) van NEN-EN 1997-1 is de schachtwrijving tot 50% gereduceerd. Negatieve kleef is gerekend over de hoogte van de cohesieve laag en de grondlagen daarboven.

2.9.3 Correlatiefactoren

De correlatiefactoren ksi3 en ksi4 worden toegepast bij de bepaling van de karakteristieke weerstand van een paal. De waarden zijn afhankelijk van de aard van de constructie en het aantal beschikbare sonderingen. De correlatiefactoren zijn ontleend aan NEN-EN 1997-1:2016, bijlage A, tabel 10.

Fundaties met één paal per hoekpunt vallen onder “niet-stijf” met factoren volgens Tabel 8. Het aantal sonderingen dat wordt gebruikt hangt af van het dekkingsbereik van de sonderingen voor een van de vier hoekpunten. Voor het DO, waarin nog geen volledig grondonderzoek beschikbaar is, wordt uitgegaan van een dekkingsbereik per hoekpunt van één sondering: Zowel 1,39 voor ksi3 als ksi4.

Tabel 9 Correlatiefactoren niet-stijf bouwwerk

| Aantal sonderingen | 1 | 2 | 3 | 4 |
|--------------------|------|------|------|------|
| ksi3 | 1,39 | 1,32 | 1,30 | 1,28 |
| ksi4 | 1,39 | 1,32 | 1,30 | 1,03 |

2.9.4 Materiaalfactor $\gamma_{m,var,qc}$

De parameter die de berekende draagkracht reduceert is de partiele factor $\gamma_{m,var,qc}$, volgens NEN-EN 1997-1 artikel 7.6.3.3 (8) opmerking (d). Voor een paal die een wisselende belasting ondergaat tussen trek- en druk treedt een vermindering op van de schuifweerstand. Afhankelijk van de verhouding tussen uiterste trek- en drukkracht in de SLS is de $\gamma_{m,var,qc}$ tussen de 1,0 en 1,5.

$$\gamma_{m,var,qc} = 1 + 0,25 \cdot \frac{F_{t,max,rep} - F_{t,min,rep}}{F_{t,max,rep}} \text{ en } \gamma_{m,var,qc} \leq 1,5$$

Voor steunmasten met variatie waarbij de maximale drukbelasting minimaal gelijk is aan de trekbelasting levert de formule de waarde van 1,50 op. Deze waarde zal worden gebruikt.

⁴ Uitgangspunt voor de palen met groutomhulling is in de berekening de halve dikte van de groutschil

2.9.5 Staaldikte funderingspalen

Voor het dimensioneren van stalen palen dient volgens TenneT-specificatie 04.009 rekening te worden gehouden met afname van staaldikte op basis van NEN 1993-5. Dit komt overeen met de CUR-aanbeveling 166 voor damwanden. Op dit moment is nog geen milieukundig onderzoek beschikbaar waaruit de agressiviteit of zuurtegraad van het grondwater (pH-waarde) kan worden afgeleid. De invloed van het zoutgehalte in het grondwater is gering⁵. Er moet uitgegaan worden van 100 jaar ontwerplevensduur.

Tabel 9.2. Aantasting (mm) van damwanden in bodem en ophogingen met of zonder grondwater (per blootgestelde zijde *).

| Beoogde levensduur (jaar) | 5 ***) | 25 ***) | 50 | 75 | 100 |
|---|--------|---------|------|------|------|
| Ongeroerde, schone bodem | 0,00 | 0,30 | 0,60 | 0,90 | 1,20 |
| Verontreinigde bodem, geroerde grond | 0,15 | 0,75 | 1,50 | 2,25 | 3,00 |
| Zure bodem (veen, moeras) | 0,20 | 1,00 | 1,75 | 2,50 | 3,25 |
| Onverdichte grond (klei, zand) **) | 0,18 | 0,70 | 1,20 | 1,70 | 2,20 |
| Onverdicht, agressief ophoogmateriaal (bodemas, slakken, sintels) | 0,50 | 2,00 | 3,25 | 4,50 | 5,75 |

Figuur 2 Tabel 9.2 uit CUR 166

Voor het DO wordt uitgegaan van zure grond en minimaal 12,5 mm dikte. Met de gereduceerde dikte van 12,5-3,25=9,25 mm is gerekend.

De aanwezigheid van zwerfstromen betekent een risico op snellere corrosie. In de nabijheid van stations is dit risico het grootst. Als mitigerende maatregel kan de buispaal geheel met gewapend beton worden gevuld zodat ook na corrosie van de stalen paal voldoende sterkte aanwezig blijft.

2.9.6 Horizontale bedding

De beddingwaardes worden gebaseerd op ontwerprichtlijn CUR228. Waarden in Tabel 9 zijn hieruit afgeleid en gelden als gemiddelde waarden. De breedte van de grond die wordt gemobiliseerd door een paal ten opzichte van de breedte van de paal wordt uitgedrukt in de schelpfactor. Empirische waarden voor de schelpfactor worden gebruikt volgens Tabel 9.

Tabel 10 Aan te houden waarden voor grondbeddingen en schelpfactoren

| Grond | k_n | schelpfactor | passieve druk |
|-------|----------------------|--------------|---------------|
| | [kN/m ³] | [-] | [-] |
| Klei | 3000 | 1,3 | 2 |
| Veen | 1500 | 1,2 | 2 |
| Zand | 15000 | 2,0 | 3 |

Volgens NEN-EN 50341-2-15:2019 art. 8.2. NL.4 moet het effect van variatie van bedding op de krachtsverdeling worden beschouwd. De berekeningen worden uitgevoerd voor een beddingwaarde die $\sqrt{2}$ lager is en $\sqrt{2}$ hoger is dan de tabelwaarde.

De reactie van de paalbedding is gelimiteerd tot de grenswaarde van de maximale passieve gronddruk die zich kan ontwikkelen afhankelijk van de diepte.

In Appendix E wordt verder ingegaan op de gehanteerde waarden in de berekening.

2.9.7 Verticale bedding

Bij de berekening van de eenpaalsfundering heeft de verticale bedding van de paalpunt geen invloed op de krachtsverdeling. In de berekening is een starre steun gehanteerd.

⁵ Deltares, rapport 1209030, Corrosie van stalen damwandplanken in de grond;

2.10 Vermoeiing

De fundaties worden belast door vakwerkmasten. Deze zijn vanwege de aard van de constructie niet gevoelig voor vortex shedding of andere opslingeringen door wind. De wisselende belasting van wind is een quasi-statische belasting. Dit is op basis van art. 7.3.10 van NEN-EN 50341-1:2013. Toetsing op vermoeiing door galloping, voor zover al relevant voor fundaties, is voor bestaande constructies niet vereist op basis NEN 8701.

2.11 Omgeving

De fundaties hebben een raakvlak met de omgeving. Als eerste vereisen de betonpoeren ruimte buiten de huidige mastvoeten; deze ruimte moet beschikbaar zijn. Daarnaast kunnen er vanuit de omgeving omstandigheden zijn waardoor aanvullende eisen van toepassing zijn aan het ontwerp, bijvoorbeeld de mogelijkheid van hoog water of de nabijheid van een dijklichaam of talud.

Een gedetailleerde studie naar eventuele obstakels direct naast de fundatie valt buiten de scope van deze rapportage. Uit een analyse van TenneT is gebleken dat er bij de steunmasten een locatie is waar mogelijk hoog water kan optreden, zie Tabel 10. Op het moment van schrijven is nog niet definitief bekend of de eisen voor hoogwater voor deze locatie zullen gelden. Het ontwerp van de fundatie voor deze locatie zal in een later stadium worden bepaald.

Tabel 11 Buitendijkse fundatie

| Mastnummer | Gemeente | Masttype | Omgeving | Oplossingsvoorstel |
|------------|----------|----------|-------------|--------------------|
| 1103 | Moerdijk | S+9_c | Buitendijks | Verhoogde fundatie |

2.12 Aarding

Uitwerking van aardingsvoorzieningen vallen buiten de scope van deze rapportage. In de UO-fase dient de aarding in de betonpoeren te worden ontworpen op basis van de van toepassing zijnde TenneT-specificaties.

2.13 Sterkte-coördinatie

TenneT stelt in PVE-lijnen 05.000 eisen aan sterkte-coördinatie tussen mast en fundaties. Dit is gebaseerd op IEC 60826. De daarin opgenomen eisen zijn toegelicht in de CIGRE brochure 178 "Probabilistic design of overhead lines". De ontwerpfilosofie moet zijn dat de fundatie met voldoende zekerheid niet mag falen voordat de mastconstructie faalt.

In de benadering met faalkansen wordt uitgegaan van gemiddelde sterktes en de 5% onderschrijdingskans. Voor fundaties geldt dat er een grote spreiding is in de sterkte als gevolg van het materiaal "grond". Om voldoende betrouwbaarheid te verkrijgen zijn fundaties daarom voor een gegeven vereiste sterkte ruim gedimensioneerd. Daardoor zal de gemiddelde sterkte van een fundatie ruimschoots de gemiddelde sterkte van de mastconstructie overstijgen, die een veel kleinere "extra" sterkte heeft. Bij een calamiteit is de kans op bezwijken van de fundatie voordat de mast bezwijkt dus gering.

Voor dit DO wordt ervan uitgegaan dat om te voldoen aan de eisen ten aanzien van sterkte-coördinatie een normale dimensionering van de fundaties voldoet, dat wil zeggen zonder overdimensionering. Vanwege de onvolledig beschikbare geotechnische gegevens wordt in het DO een maximale unity-check van 0,9 aangehouden.

2.14 Bijzondere ontwerpsituatie door ontgroning

In de rapportage uit het BO, rapport 19-0507 Advies knelpunten VKA 1.0, Meridiannummer 002.678.00 0678995, is bij een aantal mastlocaties sprake van de mogelijkheid van het ontstaan van een krater door het barsten van een ondergrondse hogedrukleiding. De stabiliteit van de fundatie kan hierdoor worden aangetast en de grond kan ontspannen als gevolg van de afgenomen belasting van de bovenste grondlagen op de diepere lagen waaraan draagkracht wordt ontleend.



In de rapportage 21-0507 is beschreven dat behalve in het bijzondere geval van een exploderende gasleiding de invloed van de ontgroning op de capaciteit zodanig klein is dat dit valt binnen de normale ontwerpmarges. De ontgroning valt onder de bijzondere belastingen met partiële factoren gelijk aan één en er is geen gelijktijdigheid van extreme windbelasting en tegelijk ontgroning. De stabiliteit van de paal is gezien de verhouding tussen diameter (ca. 0,6 m) en diepte van de krater (circa 3 m) niet in het geding.

3 FUNDERINGSONTWERP

3.1 Inleiding

Voor de steunmasten in de hoogspanningslijn is de enkelpaalsfundering met schroefinjectiepalen in de basis het uitgangspunt. Bij een tekort in draagvermogen bij de enkelpaalsfundering voor de steunmasten zal voor het DO een tweepaalsfundering worden gekozen. Als alternatief kan ook de geheide MV-paal als enkelpaalsfundering worden toegepast. Aangezien het streven van TenneT is om zoveel mogelijk enkelpaalsfunderingen toe te passen moet de mogelijkheid daarvan in de UO-fase worden onderzocht, waarbij ook het effect van heitrijvingen op de omgeving moet worden meegenomen. In het geval van bijzondere situaties, bijvoorbeeld als de fundatie zich bevindt in een wateroverloopgebied is een speciale, verhoogde fundatie het uitgangspunt.

3.2 Paaltypes

3.2.1 Schroefinjectiepaal

De schroefinjectiepaal als enkelpaalsfundering kan bij alle steunmasttypes worden toegepast, op voorwaarde dat met de bodemgesteldheid voldoende draagvermogen ontwikkeld kan worden. De paal is grondverdringend en wordt schroevend op diepte gebracht. De ruimte tussen schroefpunt en stalen buis wordt tijdens het inbrengen opgevuld met grout. Voor de maximale paallengte van de schroefinjectiepaal wordt op basis van referentieprojecten uitgegaan van 25 meter. De buispaal wordt over het in de poer opgenomen deel voorzien van een betonvulling. Onder het beton komt een zandvulling. Ingeval van bijzondere gevallen of agressieve gronden dient de betonvulling tot de paalpunt door te lopen.

3.2.2 MV-paal

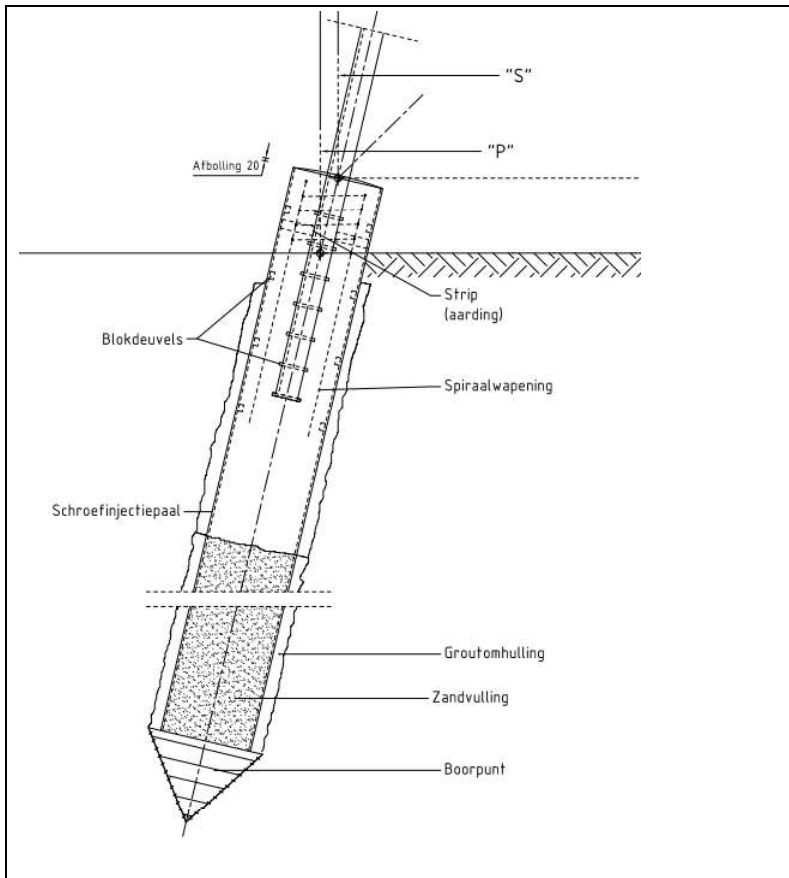
De MV-paal is een geheide stalen buispaal met open punt. Met dit paalttype is een zeer hoog draagvermogen haalbaar. De detaillering van de paalkop is gelijk aan dat van de schroefinjectiepaal. Gebaseerd op de studie in de BO-fase wordt voor de mogelijk toe te passen diameter uitgegaan van 914 mm en van 1016 mm. Beiden gaan uit van een groutschil van 80 mm.

3.3 Enkelpaalsfundering

Eigenschappen van de enkelpaalsfundering:

- de funderingspaal wordt schoor aangebracht en heeft dezelfde helling en richting als de randstijl, de richting is naar buiten vanuit het centrum van de mast gezien, in de overhoekse richting. De schoorstand is in het verticale overhoekse vlak gelijk aan 1:4,71 (212 mm/m);
- de minimale afmeting is 610 mm voor het kunnen instorten van de randstijl rekening houdend met een paalafwijking van 0,1 m.
- de bovenkant van de paal bevindt zich op 0,5 m+ maaiveld. In uitzonderingsgevallen is dit 1,0 m;
- de paal wordt aan bovenzijde voorzien van gelaste blokdeuvels voor de krachtoverdracht met de ingestorte rand van de mastconstructie;
- de paal wordt over de bovenste circa 2,5 m voorzien van een betonvulling. De betonvulling moet met een afbolling worden gestort. Onder de beton komt een zandvulling. Ingeval van bijzondere gevallen of agressieve gronden dient de betonvulling tot paalpunt door te lopen;
- in de betonvulling wordt een spiraalwapening geplaatst;
- de randstijl wordt voor de aarding galvanisch verbonden met de wand van de paal via aangelaste strippen;

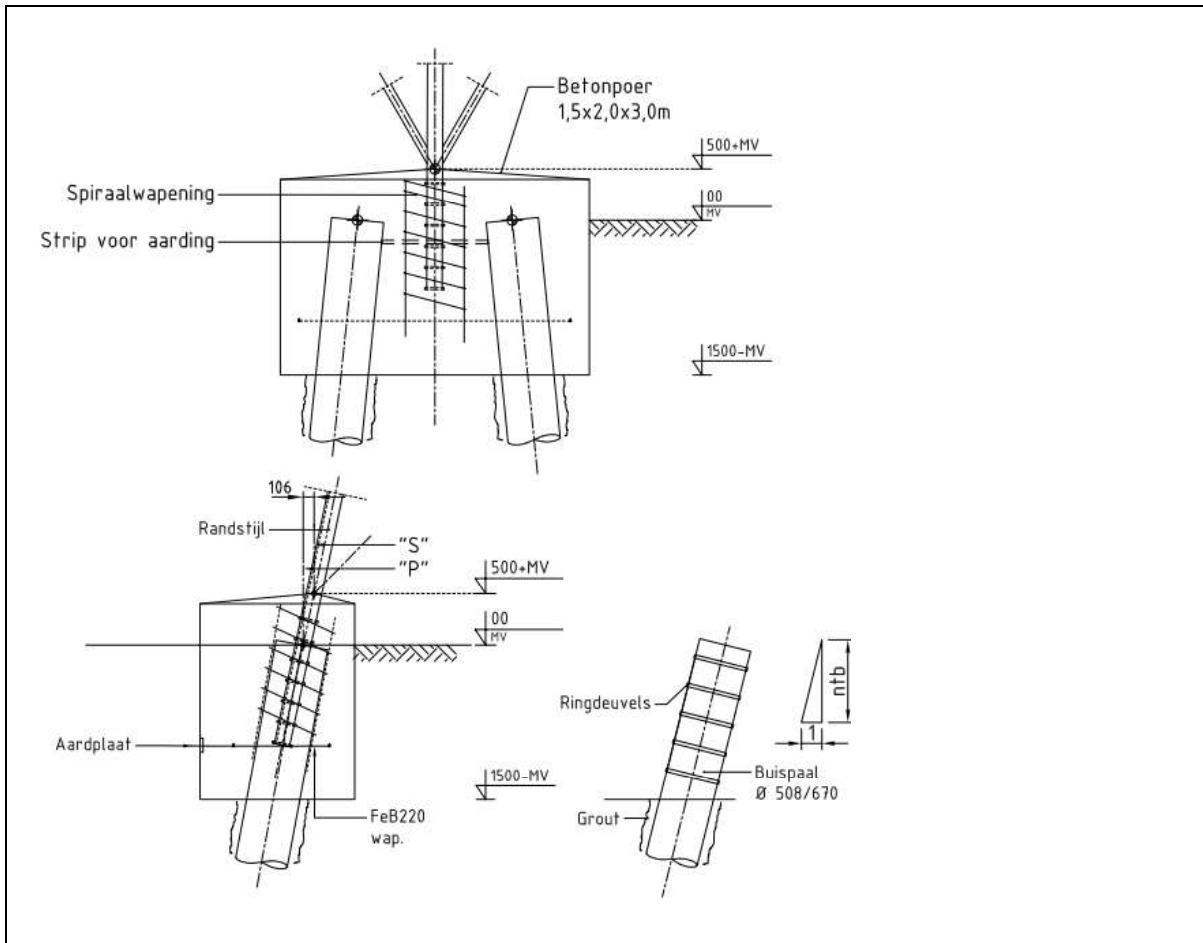
In Figuur 3 is de principetekening opgenomen.



Figuur 3 Principe van de schroefinjectiepaal met ingestorte randstijl

3.4 Tweepaalsfundering

Bij onvoldoende draagvermogen wordt uitgegaan van de tweepaalsfundering. Hierbij worden twee palen opgenomen in een rechthoekige betonnen poer. Als paaltype is voor dit DO de schroefinjectiepaal het uitgangspunt omdat deze het breedst inzetbaar is. Als alternatief kan in het UO ook een vibro-paal of FGI-paal worden toegepast. Voor de beschrijving van deze palen wordt verwezen naar rapportage 21-1250 van de hoekmasten, Meridannummer 002.678.00 0950632.



Figuur 4 Principe van de tweepaalsfundering

3.5 Verhoogde fundering

Mast 1012 en 1013 dienen een verhoogde fundering te bezitten, om voldoende afstand tot een wegbuis te verkrijgen zonder dat een hoger masttype benodigd is, omdat dat bezwaarlijk is vanuit de nabijheid tot de vliegbasis Woensdrecht. De oplossing bestaat uit het toepassen van een enkelpaalsfundering met bovenkant fundatie op 1,0 m boven maaiveld in plaats van 0,5 m boven maaiveld.

Bij mast 1103 zal de fundatie verhoogd worden uitgevoerd vanwege de buitendijkse locatie. Op deze locatie is een tweepaalspoer voorzien, deze zal een betonnen opstorting krijgen zodat de mastconstructie bij hoogwater boven het waterpeil blijft.

4 AANPAK

4.1 Inleiding

Voor alle mastlocaties in het tracé zal uitgaande van de beschikbare sonderingsgegevens het poertype en de paallengte indicatief worden bepaald. De berekening wordt uitgevoerd met de software TS/paalfunderingen. De toetsing vindt plaats ten aanzien van trek- en drukbelasting.

In deze DO-rapportage zal de enkelpaalsfundering worden getoetst met de grootste horizontale belastingen binnen de groep van steunmasttypes waar dit fundatietype wordt toegepast. Het gaat om alle steunmasttypes met uitzondering van S+12/c, S+18/s en S+24/s. Er zal worden uitgegaan van het slechtste bodemprofiel over de lengte van het tracé.

4.2 Belasting

De fundatiebelastingen van de mastconstructies zijn opgenomen in Appendix A. Deze zijn ontleend aan de uitvoer vanuit PLS-TOWER. Dit wijkt af van de uitvoer van de oplegreacties van de mastrapporten. Daarin is gebruik gemaakt van de uitvoer van het programma Geleiderbelastingen. Er is gekozen voor gebruik van de reacties vanuit het 3D-model van PLS-TOWER omdat hierin de werkelijke afdracht van horizontale belastingen gevonden wordt.

Voor de toetsing met TS/paalfunderingen wordt gebruik gemaakt van de belasting in de richting van de randstijl (lokale richting) voor trek- en drukbelasting.

De belastingcombinaties die in het DO worden gehanteerd voor de berekening van de horizontale afdracht bestaat uit de volgende belastingen, alle voor de uiterste grenstoestand. De belastingen gelden voor één van de vier hoekpunten.

- maximale drukbelasting, in deze combinatie belast de randstijl de fundatie met een neerwaartse kracht en een horizontale kracht naar buiten;
- maximale trekbelasting, in deze combinatie belast de randstijl de fundatie met een opwaarts gerichte kracht en een horizontale kracht naar binnen;
- maximale torsiebelasting, hierbij wordt de fundatie haaks op de diagonale richting van het grondvlak belast. De positieve en negatieve horizontale richting wordt onderzocht. De verticale belasting kan van ondergeschikte grootte zijn.
- maximale combinatie van trekbelasting en torsie. Bij een meerpaalspoer leidt de horizontale kracht door torsie tot een vergroting van de trekkracht. In combinatie met een eveneens significante trekkracht vanuit de mast kan dit maatgevend zijn voor een van de palen in de fundatie. Zie hiervoor de toelichting in Appendix C.

4.3 Draagvermogen

Vanuit het geotechnisch lengteprofiel is een representatieve selectie gemaakt waarmee berekeningen zijn uitgevoerd. Bovendien is zoveel mogelijk gebruik gemaakt van sonderingen met een diepte van meer dan 30 meter, omdat paallengtes tot 25 m oplopen. Het lengteprofiel is verdeeld in 15 deeltrajecten. Per deeltrajecten is één sondering gekozen. In tabel zijn de in de berekening gebruikte sonderingen gegeven. De berekeningen zijn voor alle paaltypes bij iedere sondering uitgevoerd.

Tabel 12 Gebruikte sonderingen

| CPT bestand | type | RD_x_sond | RD_y_sond | RD_m_sond | sondeerlengte | gemeente |
|-----------------------|------|-----------|-----------|-----------|---------------|----------------|
| 2019-1008_1.GEF | GEF | 75341,2 | 382565,9 | 2,12 | 34,824 | Reimerswaal |
| 2019-1008_6.GEF | GEF | 81608,3 | 388586,3 | 11 | 34,928 | Bergen op Zoom |
| 02P001595_166.S01.GEF | GEF | 87819,8 | 393422,8 | 3,45 | 26,107 | Roosendaal |
| 2019-1008_11.GEF | GEF | 90949,4 | 398218,9 | 0,62 | 34,898 | Halderberge |
| 2019-1008_12.GEF | GEF | 92691,7 | 399690,8 | 3,57 | 35,066 | Halderberge |

| | | | | | | |
|-----------------------|-----|----------|----------|--------|--------|-----------------|
| 2019-1008_17.GEF | GEF | 96097,9 | 405288,6 | 0,2 | 34,998 | Moerdijk |
| 2019-1008_20.GEF | GEF | 99890,2 | 408354,7 | -0,03 | 35,203 | Moerdijk |
| 2019-1008_21.GEF | GEF | 102678,6 | 409201,9 | 1,78 | 34,974 | Moerdijk |
| 02P001595_251.S01.GEF | GEF | 109537,3 | 411798 | -1,05 | 39,831 | Drimmelen |
| 2019-1008_29.GEF | GEF | 114349,2 | 411937,4 | 0,79 | 35,076 | Drimmelen |
| 02P001595_283.S02.GEF | GEF | 119023,6 | 409980,1 | 0,17 | 32,463 | Geertruidenberg |
| 2019-1008_35.GEF | GEF | 123777,2 | 408715 | 0,92 | 35,167 | Dongen |
| 02P001595_312.S03.GEF | GEF | 127922,2 | 405557,3 | 3,78 | 35,751 | Loon op Zand |
| 2019-1008_43.GEF | GEF | 131482,8 | 403215,2 | 9,88 | 35,044 | Loon op Zand |
| 02P001595_328.S02.GEF | GEF | 132052,7 | 402297,2 | 10,171 | 39,063 | Tilburg |

De sonderingen zijn in digitaal formaat (gef-bestand) ingelezen in het programma Technosoft Paalfunderingen. Aan de hand van de sonderingen en de beschikbare boringen is een grondprofiel geconstrueerd. De gebieden waarin negatieve en positieve schachtwrijving optreedt worden ingesteld per sondering.

Bij de invoer in het programma is rekening gehouden met de situatie dat de berekeningen niet voor één locatie worden uitgevoerd, maar voor een geheel van locaties. Omdat er grote verschillen in maaiveldniveau zijn tussen de sonderingen zijn deze in drie groepen verdeeld; sonderingen waarbij de paalkop zich bevindt op 0.0+, 3.6+ en 10.5+ N.A.P. Met deze onderverdeling wordt bereikt dat de juiste positieve en negatieve kleeft wordt berekend, in het programma wordt geen kleeft toegekend aan het deel van de paal dat uitsteekt boven het (fictieve) maaiveld. Daarnaast is per mast de werkelijke maaiveldhoogte aldaar gebruikt om de limiet van 25 m paallengte zo veel mogelijk niet te overschrijden, hooguit op een paar decimeter na.

Aanvullend op de berekening in Technosoft is een controle op het kluitgewicht uitgevoerd volgens art. 7.6.3.3 (g) van NEN-EN 1997-1, waaruit de minimale lengte voor voldoende te mobiliseren grondmassa volgt.

Geotechnische berekeningen zijn opgenomen in Appendix D. In de uitvoer zijn van toepassing zijnde paalpuntniveau's omkaderd.

4.4 Horizontale krachtafdracht

4.4.1 Krachtsverdeling

Met een staafwerkmodel in het programma AxisVM is de horizontale krachtafdracht berekend. De palen zijn als elastisch ondersteunde liggers zijn ingevoerd. Er wordt geen steun uit de grond tussen maaiveld en 1 m onder maaiveld of tegen de poeren gerekend, alsof de fundaties grenzen aan een waterloop. De horizontale gronddruk is begrensd tot de passieve gronddruk die kan worden ontwikkeld.

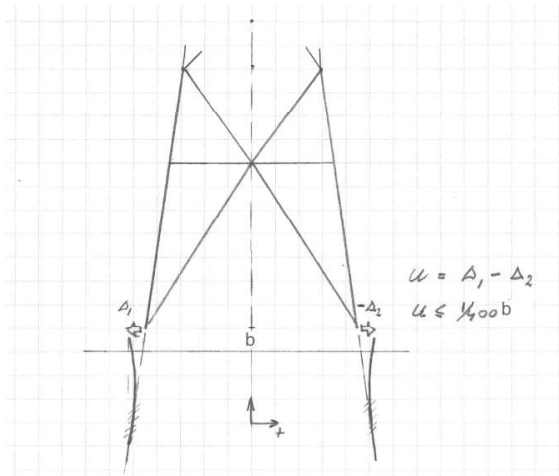
De berekening voor de horizontale krachtafdracht is uitgevoerd uitgaande van het maatgevende bodemprofiel over de lengte van het tracé. Dat wil zeggen voor één van de sonderingen. Als maatgevend is het bodemprofiel van sondering 2019-1008-017 gehanteerd. Hierbij zijn vanaf maaiveld tot circa 10 m diepte kleilagen aanwezig die minder steun verlenen dan zandlagen.

Het kan zijn dat een tweepaalspoer te maken krijgt met herverdeling van belasting (bijv. door verkeerd heien of inmeten). Dit is meegenomen in de controle van de palen op trek- en drukbelasting via de factor "efficiëntie", zie de tabel in Appendix C. Voor een tweepaalspoer is gerekend met 95%. De palen in deze poer kunnen 5% meer belasting opnemen. De éénpaalspoer kan niet herverdelen en de factor is daarom 100%. Er wordt een maximale unity-check van 0,9 aangehouden.

De berekening van de horizontale afdracht verschaft informatie over de combinatie van axiale krachten en buiging in de paalschacht. De aldus gevonden spanningen worden gebruikt in de toetsing van de doorsnede van de buispaal. De éénpaalsfundering is gekozen om te toetsen, deze heeft vanwege de vrijstaande paalkop de grootste horizontale belasting. De berekening is opgenomen in Appendix E.

4.4.2 Horizontale verplaatsing

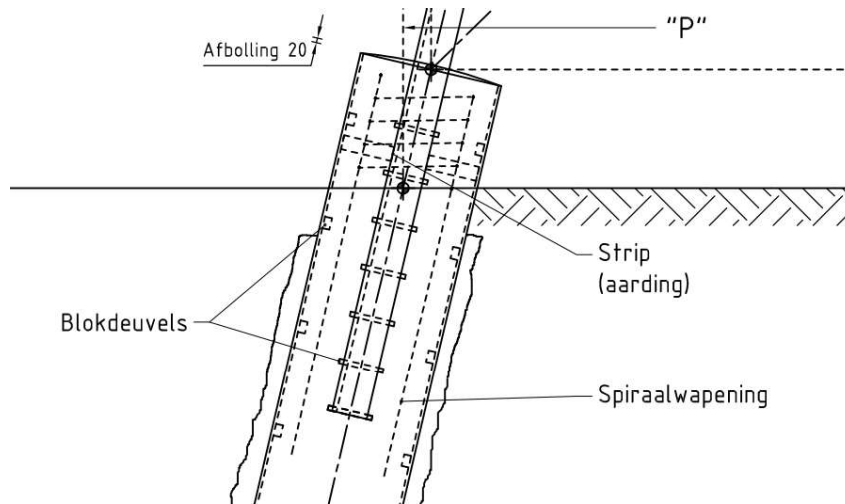
De TenneT-specificatie "Paalfunderingen" stelt eisen aan de maximale onderlinge verplaatsing van de fundatie bij de randstijl. Deze mag niet meer bedragen dan $1/400 b$. Verplaatsingseisen worden gesteld voor de karakteristieke belastingen, zonder belastingfactoren. In Appendix C is verdere invulling gegeven aan deze eis.



Figuur 5 Eis aan de horizontale verplaatsing

4.5 Wapening

Het detailleren van de wapening in de paal(kop) valt buiten de scope van dit rapport. De benodigde wapening is in de UO-fase door opdrachtnemer te bepalen. In Figuur 6 is het principe van de wapening weergegeven.



Figuur 6 Principe van de wapening

Als indicatie kan worden uitgegaan van een splijtwapening uitgevoerd in spiraalwapening. De doorsnede van de splijtwapening wordt bepaald op basis van de drukdiagonalen die vanuit de blokdeuvels ontstaan. De afdracht vindt verdeeld plaats over de ingestorte lengte. De grootste trekbelasting treedt op bij mast S+18_s. en bedraagt $F = 1750$ kN. Uitgaande van een drukdiagonaal van 45° is de trekkracht in de beugels gelijk aan $1750 / 2 = 875$ kN. Bij een ingestorte lengte van 1,5 m en twee effectieve doorsnedes aan weerszijden van het staalprofiel is de verdeelde reactie per doorsnede gelijk aan $875 / (1,5 \times 2) = 292$ kN/m. Uitgaande van een toelaatbare spanning van 435 N/mm^2 in het



wapeningsstaal is de benodigde wapeningsdoorsnede $292 / 0,435 = 671 \text{ mm}^2/\text{m}$. Indicatieve keuze $\text{Ø}10\text{-}100$ (785 mm^2) voldoet.

De verticale wapening wordt gebaseerd op het mogelijk uitbreken van de bovenste betonkegel. Vanwege de voetplaat en de rechtstreekse afdracht van de blokdeuvels wordt uitgegaan van een trekkracht van een kwart van de totale trekkracht. $F = 1/4 \times 1750 \text{ kN} = 440 \text{ kN}$. Een wapeningsdoorsnede van $440 / 0,435 = 1011 \text{ mm}^2$ voldoet. Keuze: 4 haarspelden $\text{Ø}16$: $2 \times 4 \times 201 \text{ mm}^2 = 1608 \text{ mm}^2$.

5 RESULTATEN

5.1 Verticaal draagvermogen

De resultaten van de berekeningen zijn samengevat in Appendix D. Voor alle van toepassing zijnde locaties is de toetsing uitgedrukt in de Unity-Check. De toetsing voor trek en druk is opgenomen. Alle Unity-Checks zijn kleiner dan 0,9, dus voldoen de fundaties aan het gestelde uitgangspunt. De paallengte is groter dan de minimale lengte benodigd voor het kluitgewicht.

In Tabel 12 is per sondering weergegeven in hoeverre de enkelpaalsfundering toepasbaar is. In een aantal gevallen is voor een tweepaalspoer gekozen als alternatief. Voor masttypes S+12/c, S+18/s, S+24/s is een tweepaalsfundering het uitgangspunt in het DO. Dit uitgangspunt staat niet in tabel 12 omdat deze keuze onafhankelijk is van de sonderingen.

Tabel 13 Resultaat per sondering

| CPT bestand | Gemeente | Bijzonderheden |
|-----------------------|-----------------|---|
| 2019-1008_1.GEF | Reimerswaal | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 2019-1008_6.GEF | Bergen op Zoom | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 02P001595_166.S01.GEF | Roosendaal | Trek maatgevend, paaldiameter 762 mm ook toegepast. |
| 2019-1008_11.GEF | Halderberge | Trek maatgevend, paaldiameter 762 mm ook toegepast. |
| 2019-1008_12.GEF | Halderberge | Trek maatgevend, paaldiameter 762 mm ook toegepast. |
| 2019-1008_17.GEF | Moerdijk | Trek maatgevend, alleen paaldiameter 610 mm en tweepaalspoer toegepast. |
| 2019-1008_20.GEF | Moerdijk | Trek maatgevend, alleen tweepaalspoer toegepast. |
| 2019-1008_21.GEF | Moerdijk | Trek en druk maatgevend. alleen paaldiameter 762 mm en tweepaalspoer toegepast. |
| 02P001595_251.S01.GEF | Drimmelen | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 2019-1008_29.GEF | Drimmelen | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 02P001595_283.S02.GEF | Geertruidenberg | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 2019-1008_35.GEF | Dongen | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 02P001595_312.S03.GEF | Loon op Zand | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 2019-1008_43.GEF | Loon op Zand | Trek maatgevend, alleen paaldiameter 610 mm toegepast. |
| 02P001595_328.S02.GEF | Tilburg | Geen steunmasten |

5.2 Horizontale krachtsafdracht

In Appendix E is het resultaat beschreven van de horizontale krachtsafdracht. Uit Tabel 13 blijkt dat de toetsing van de spanning in de buispaal en de horizontale verplaatsing voldoet. Voor masttypes S+12/c, S+18/s, S+24/s is een tweepaalsfundering het uitgangspunt in het DO vanwege de grootte van de horizontale spatkracht. In het UO kan nader bepaald worden of hier een enkelpaalsfundering mogelijk is. Dit uitgangspunt is niet verwerkt in tabel 12.

Tabel 14 Toetsing horizontale krachtsafdracht

| | Berekend | Toelaatbaar | Unity-check |
|---------------------------|----------|-----------------------|-------------|
| Spanningscheck buispaal | 121 | 355 N/mm ² | 0,34 OK |
| Verplaatsing ULS-1a ex/ey | 15,4 | 17,3 mm | 0,89 OK |
| Verplaatsing ULS-5a ex/ey | 20,8 | 25,6 mm | 0,81 OK |

5.3 Hoeveelheden

In Tabel 14 is als samenvatting het aantal palen, de lengte en maximale lengte opgenomen. Dit is gebaseerd op de resultaten per locatie volgens Appendix B.

Tabel 15 Hoeveelheden

| Paaltype | Aantal locaties | Aantal palen | Gem. paallengte (m) | Max. paallengte (m) |
|--------------------------|-----------------|--------------|---------------------|---------------------|
| SI Ø610/850 | 104 | 416 | 21,4 | 25,2 |
| SI Ø762/950 | 10 | 40 | 23,5 | 24,3 |
| SI Ø508/670 ⁶ | 20 | 160 | 19,7 | 23,7 |

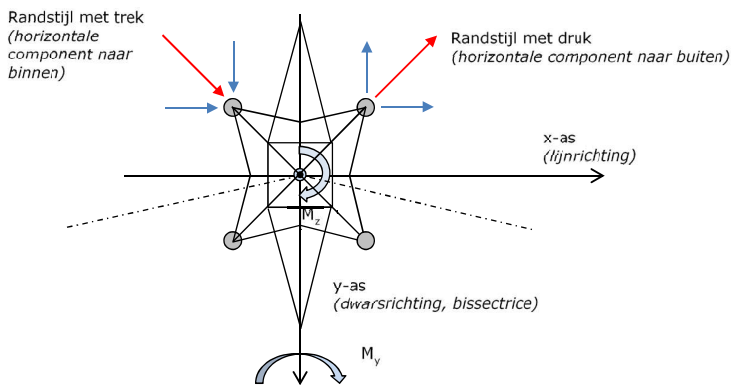
⁶ onderdeel van tweepaalsfundering

APPENDIX A

Fundatiebelastingen

De reacties van de mastconstructie op de fundering worden in deze appendix gepresenteerd. Het gaat om de maatgevende waarden per masttype van de druk-, trek- en horizontale reacties. Vanwege de oriëntatie van de funderingspaal, zijn de waarden beschreven in de X-, Y-, en Z-coördinaat van het globale assenstelsel en in het lokale assenstelsel van de randstijl ("leg direction"). De gegeven waarden zijn een samenvatting over alle berekende belastingcombinaties en zijn gebaseerd op de grootste waarden van elk van de vier fundatiepunten van de mast. De reacties zijn ontleend aan de berekening van PLS-TOWER, dit wijkt af van de mastrapportages waarin uitvoer vanuit het programma "geleiderbelastingen" is opgenomen.

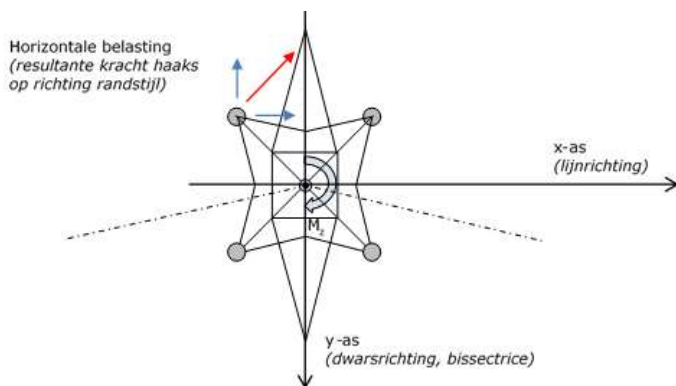
De twee belangrijkste waarden van de funderingsreacties worden gevormd door de trek- en de drukkracht vanuit de randstijl. In geval van een drukkracht zal gezien in het *globale* assenstelsel bij een hellende randstijl een naar buiten gerichte horizontale kracht werken, zie Figuur 6. In geval van een trekkracht in de randstijl is de horizontale component naar binnen gericht.



Figuur 7 Belasting bij maximale trek- of drukbelasting vanuit de mast

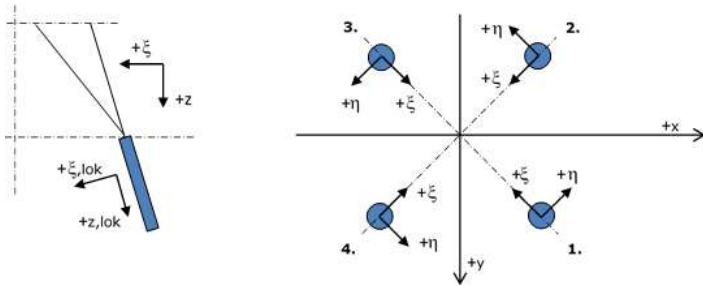
In het geval van torsiebelasting op de mast, bij steunmasten is dat onder de combinatie 5a (geleiderbreuk), bij hoekmasten door de afwezigheid van geleiders aan één zijde van de mast (special limit state), werkt er een significante horizontale kracht op de fundering *haaks* op de richting van de randstijl. Voor de berekening van de horizontale krachtsafdracht van de fundering moet met de belasting door torsie rekening worden gehouden.

In tegenstelling tot de horizontaalkracht bij maximale verticale druk- of trekkracht, is de horizontale belasting door torsie niet gerelateerd aan de trek- of drukkracht in de randstijl. Op de bladzijde "max. trekbelasting en torsie" zijn de combinaties opgezocht waarbij zowel een grote trekkracht optreedt als een horizontale kracht door torsie.



Figuur 8 Belasting bij torsiebelasting vanuit de mast

Belastingen op de fundatie in het lokale coördinatenstelsel zijn uitgedrukt in de radiale en tangentiële richting eta en xi, zie Figuur 8.



Figuur 9 Lokaal assenstelsel



Project: **RLL-TLB**
Uitgangspunt: **Nieuwbouw**
Datum: **14-10-2021**

Betreft: **Trekbelasting**
Richting: **Globale assenstelsel**

| | Mastnummer | Masttype | Verticaal trek [kN] | X-richting [kN] | Y-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase |
|------|------------|----------|---------------------|-----------------|-----------------|------------------------|-----------------------|
| 1011 | S-3_s | | 1108,0 | 167,0 | -162,1 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1064 | S+0_s | | 1214,2 | 180,7 | -174,2 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 0 | S+3_s | | 1322,0 | 194,4 | -186,0 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1059 | S+6_s | | 1103,0 | 169,6 | -161,1 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1057 | S+9_s | | 1125,9 | 172,5 | -164,9 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1003 | S+18_s | | 1703,7 | 295,8 | -275,5 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1149 | S+24_s | | 1463,7 | 253,6 | -239,8 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1119 | S-3_c | | 1215,3 | 183,2 | -160,5 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1111 | S+0_c | | 1307,1 | 206,5 | -163,4 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1104 | S+3_c | | 1433,5 | 222,3 | -175,0 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1101 | S+6_c | | 1449,7 | 220,3 | -206,9 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1073 | S+9_c | | 1464,5 | 218,6 | -207,9 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1077 | S+12_c | | 1539,5 | 267,0 | -247,8 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |



Project: **RLL-TLB**
Uitgangspunt: **Nieuwbouw**
Datum: **14-10-2021**

Betreft: **Drukbelasting**
Richting: **Globale assenstelsel**

| Mastnummer | Masttype | Verticaal druk [kN] | X-richting [kN] | Y-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase |
|------------|----------|---------------------|-----------------|-----------------|------------------------|-----------------------|
| 1011 | S-3_s | -1383,5 | -206,4 | -206,8 | Nieuwbouw CC2 | ULS 1a_45 |
| 1064 | S+0_s | -1499,3 | -221,7 | -220,5 | Nieuwbouw CC2 | ULS 1a_45 |
| 0 | S+3_s | -1614,9 | -236,4 | -233,8 | Nieuwbouw CC2 | ULS 1a_45 |
| 1059 | S+6_s | -1412,5 | -217,1 | -212,7 | Nieuwbouw CC2 | ULS 1a_45 |
| 1057 | S+9_s | -1460,8 | 227,0 | -223,2 | Nieuwbouw CC2 | ULS 1a_135 |
| 1003 | S+18_s | -2109,5 | -369,9 | -353,6 | Nieuwbouw CC2 | ULS 1a_45 |
| 1149 | S+24_s | -1918,4 | -328,5 | -317,2 | Nieuwbouw CC2 | ULS 1a_45 |
| 1119 | S-3_c | -1593,8 | -237,3 | -235,6 | Nieuwbouw CC2 | ULS 1a_45 |
| 1111 | S+0_c | -1704,8 | -257,8 | -251,9 | Nieuwbouw CC2 | ULS 1a_45 |
| 1104 | S+3_c | -1838,2 | -274,1 | -266,7 | Nieuwbouw CC2 | ULS 1a_45 |
| 1101 | S+6_c | -1868,1 | -283,9 | -276,4 | Nieuwbouw CC2 | ULS 1a_45 |
| 1073 | S+9_c | -1913,0 | -288,1 | -282,9 | Nieuwbouw CC2 | ULS 1a_45 |
| 1077 | S+12_c | -2035,5 | -355,8 | -340,4 | Nieuwbouw CC2 | ULS 1a_45 |



Project: **RLL-TLB**
 Uitgangspunt: **Nieuwbouw**
 Datum: **14-10-2021**

Betreft: **Trekbelasting**
 Richting: **Lokale assenstelsel**

| Mastnummer | Masttype | Verticaal trek [kN] | X(-)richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase |
|------------|----------|---------------------|-------------------|-------------------|------------------------|-----------------------|
| 1011 | S-3_s | 1132.2 | 2.3 | 3.4 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1064 | S+0_s | 1239.8 | 6,6 | 4,6 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 0 | S+3_s | 1349.1 | 11.5 | 5.9 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1059 | S+6_s | 1127.5 | 0.2 | 6.0 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1057 | S+9_s | 1150.9 | 0.3 | 5.3 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1003 | S+18_s | 1750.4 | -42.6 | 14.4 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1149 | S+24_s | 1504.2 | -38.4 | 9.8 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1119 | S-3_c | 1239.3 | 14,7 | 16,1 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1111 | S+0_c | 1332.9 | 15,7 | 30,5 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1104 | S+3_c | 1460.6 | 23,2 | 33,4 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1101 | S+6_c | 1480.8 | 5,4 | 9,5 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1073 | S+9_c | 1495.2 | 9,1 | 7,6 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1077 | S+12_c | 1581.5 | -37.4 | 13.6 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |



Project: **RLL-TLB**
 Uitgangspunt: **Nieuwbouw**
 Datum: **14-10-2021**

Betreft: **Drukbelasting**
 Richting: **Lokale assenstelsel**

| Mastnummer | Masttype | Verticaal druk [kN] | X(-)richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase |
|------------|----------|---------------------|-------------------|-------------------|------------------------|-----------------------|
| 1011 | S-3_s | -1414,0 | -1,3 | -0,3 | Nieuwbouw CC2 | ULS 1a_45 |
| 1064 | S+0_s | -1531,6 | -5,4 | 0,9 | Nieuwbouw CC2 | ULS 1a_45 |
| 0 | S+3_s | -1648,7 | -10,1 | 1,8 | Nieuwbouw CC2 | ULS 1a_45 |
| 1059 | S+6_s | -1444,8 | 4,3 | 3,1 | Nieuwbouw CC2 | ULS 1a_45 |
| 1057 | S+9_s | -1495,1 | 8,4 | -2,7 | Nieuwbouw CC2 | ULS 1a_135 |
| 1003 | S+18_s | -2169,7 | 64,1 | 11,5 | Nieuwbouw CC2 | ULS 1a_45 |
| 1149 | S+24_s | -1971,4 | 49,6 | 8,0 | Nieuwbouw CC2 | ULS 1a_45 |
| 1119 | S-3_c | -1628,5 | -3,7 | 1,2 | Nieuwbouw CC2 | ULS 1a_45 |
| 1111 | S+0_c | -1742,5 | -1,2 | 4,1 | Nieuwbouw CC2 | ULS 1a_45 |
| 1104 | S+3_c | -1877,6 | -7,6 | 5,3 | Nieuwbouw CC2 | ULS 1a_45 |
| 1101 | S+6_c | -1909,7 | -0,1 | 5,3 | Nieuwbouw CC2 | ULS 1a_45 |
| 1073 | S+9_c | -1955,1 | -2,0 | 3,7 | Nieuwbouw CC2 | ULS 1a_45 |
| 1077 | S+12_c | -2093,3 | 60,5 | 10,9 | Nieuwbouw CC2 | ULS 1a_45 |



Project: **RLL-TLB**
Uitgangspunt: **Nieuwbouw**
Datum: **14-10-2021**

Betreft **Torsiebelasting positief**
Richting **Lokale assenstelsel**

| Mastnummer | Masttype | Verticaal [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase |
|------------|----------|----------------|------------------|-------------------|------------------------|---------------------------|
| 1011 | S-3_s | -232.9 | -0.1 | 46.7 | Nieuwbouw CC2 | ULS 8 Ba_bouwfase |
| 1064 | S+0_s | -235.8 | -0.9 | 46.9 | Nieuwbouw CC2 | ULS 8 Ba_bouwfase |
| 0 | S+3_s | -246.9 | -2.3 | 46.6 | Nieuwbouw CC2 | ULS 8 Ba_bouwfase |
| 1059 | S+6_s | -246.1 | -0.5 | 44.4 | Nieuwbouw CC2 | ULS 8 Ba_bouwfase |
| 1057 | S+9_s | -327.2 | 4.2 | 38.6 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase |
| 1003 | S+18_s | 1535.0 | -19.2 | 49.0 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1149 | S+24_s | -391.6 | 5.6 | 36.4 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase(24) |
| 1119 | S-3_c | -340.6 | 0.9 | 59.3 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase |
| 1111 | S+0_c | -357.7 | 2.1 | 60.0 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase |
| 1104 | S+3_c | -371.9 | 0.5 | 59.0 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase |
| 1101 | S+6_c | -376.0 | 1.7 | 54.5 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase |
| 1073 | S+9_c | -382.8 | 2.8 | 50.0 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase |
| 1077 | S+12_c | -357.0 | 15.9 | 59.0 | Nieuwbouw CC2 | ULS 5a Ah 11_bouwfase |



Project: **RLL-TLB**
 Uitgangspunt: **Nieuwbouw**
 Datum: **14-10-2021**

Betreft: **Torsiebelasting negatief**
 Richting: **Lokale assenstelsel**

| Mastnummer | Masttype | Verticaal [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase |
|------------|----------|----------------|------------------|-------------------|------------------------|---------------------------|
| 1011 | S-3_s | -232.9 | -0.1 | -46.7 | Nieuwbouw CC2 | ULS 8 Ah_bouwfase |
| 1064 | S+0_s | -235.8 | -0.9 | -46.9 | Nieuwbouw CC2 | ULS 8 Ah_bouwfase |
| 0 | S+3_s | -246.9 | -2.3 | -46.6 | Nieuwbouw CC2 | ULS 8 Ah_bouwfase |
| 1059 | S+6_s | -246.1 | -0.5 | -44.4 | Nieuwbouw CC2 | ULS 8 Ah_bouwfase |
| 1057 | S+9_s | -327.2 | 4.2 | -38.6 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase |
| 1003 | S+18_s | 1535.0 | -19.2 | -49.0 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1149 | S+24_s | -392.0 | 5.4 | -36.1 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase(24) |
| 1119 | S-3_c | -340.6 | 0.9 | -59.3 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase |
| 1111 | S+0_c | -357.7 | 2.1 | -60.0 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase |
| 1104 | S+3_c | -371.9 | 0.5 | -59.0 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase |
| 1101 | S+6_c | -376.0 | 1.7 | -54.5 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase |
| 1073 | S+9_c | -382.8 | 2.8 | -50.0 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase |
| 1077 | S+12_c | -357.0 | 15.9 | -59.0 | Nieuwbouw CC2 | ULS 5a Ba 11_bouwfase |



Project: **RLL-TLB**
Uitgangspunt: **Nieuwbouw**
Datum: **14-10-2021**

Betreft **Max. trekbelasting + torsie**
Richting **Lokale assenstelsel**

| Mastnummer | Masttype | Verticaal [kN] | X(-)richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase |
|------------|----------|----------------|-------------------|-------------------|------------------------|-----------------------|
| 1011 | S-3_s | 1132.2 | 2.3 | 3.4 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1064 | S+0_s | 1239.8 | 6,6 | 4,6 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 0 | S+3_s | 1349.1 | 11.5 | 5.9 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1059 | S+6_s | 1081.2 | 12.3 | 15.1 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1057 | S+9_s | 1150.9 | 0.3 | 5.3 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1003 | S+18_s | 1535.0 | -19.2 | 49.0 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1149 | S+24_s | 1504.2 | -38.4 | 9.8 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_135 |
| 1119 | S-3_c | 1239.3 | 14,7 | 16,1 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1111 | S+0_c | 1332.9 | 15,7 | 30,5 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1104 | S+3_c | 1460.6 | 23,2 | 33,4 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1101 | S+6_c | 1474.0 | 17,8 | 32,2 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1073 | S+9_c | 1468.0 | 20,8 | 22,8 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |
| 1077 | S+12_c | 1498.6 | -19.0 | 47.1 | Nieuwbouw CC2 | ULS 1a_0,9_0,9_90 |

APPENDIX B

Fundatiegegevens

| Paalgegevens | | | | | | | | | | | |
|--------------|----------|--------------|-------------|----------------|-------------------------|------------------------------|-------------------------|-----------------------------------|----------------------------|-------------------------------|--|
| Mastnr. | Masttype | Aantal palen | Paaltype | Paallengte [m] | Paal boven maaiveld [m] | Paalpuntniveau t.o.v. MV [m] | Maaiveld t.o.v. NAP [m] | Bovenkant fundatie t.o.v. NAP [m] | Paal tov. bk. fundatie [m] | Paalpuntniveau t.o.v. NAP [m] | |
| 1003 | S+18_s | 2 | SI Ø508/670 | 22,85 | 0,00 | -22,85 | 1,35 | 1,85 | 0,50 | -21,50 | |
| 1004 | S+18_s | 2 | SI Ø508/670 | 23,01 | 0,00 | -23,01 | 1,51 | 2,01 | 0,50 | -21,50 | |
| 1006 | S+0_s | 1 | SI Ø610/850 | 24,58 | 0,50 | -24,08 | 1,08 | 1,58 | 0,00 | -23,00 | |
| 1008 | S+0_s | 1 | SI Ø610/850 | 24,80 | 0,50 | -24,30 | 1,30 | 1,80 | 0,00 | -23,00 | |
| 1009 | S+0_s | 1 | SI Ø610/850 | 25,16 | 0,50 | -24,66 | 1,66 | 2,16 | 0,00 | -23,00 | |
| 1010 | S+0_s | 1 | SI Ø610/850 | 24,88 | 0,50 | -24,38 | 1,38 | 1,88 | 0,00 | -23,00 | |
| 1011 | S-3_s | 1 | SI Ø610/850 | 23,93 | 0,50 | -23,43 | 1,43 | 1,93 | 0,00 | -22,00 | |
| 1012 | S-3_s | 1 | SI Ø610/850 | 24,71 | 1,00 | -23,71 | 1,71 | 2,71 | 0,00 | -22,00 | |
| 1013 | S-3_s | 1 | SI Ø610/850 | 24,27 | 1,00 | -23,27 | 1,27 | 2,27 | 0,00 | -22,00 | |
| 1026 | S-3_c | 1 | SI Ø610/850 | 16,63 | 0,50 | -16,13 | 7,63 | 8,13 | 0,00 | -8,50 | |
| 1028 | S+0_c | 1 | SI Ø610/850 | 18,70 | 0,50 | -18,20 | 8,70 | 9,20 | 0,00 | -9,50 | |
| 1029 | S+6_c | 1 | SI Ø610/850 | 17,27 | 0,50 | -16,77 | 7,27 | 7,77 | 0,00 | -9,50 | |
| 1030 | S+3_c | 1 | SI Ø610/850 | 19,65 | 0,50 | -19,15 | 8,65 | 9,15 | 0,00 | -10,50 | |
| 1031 | S+0_c | 1 | SI Ø610/850 | 17,30 | 0,50 | -16,80 | 7,30 | 7,80 | 0,00 | -9,50 | |
| 1032 | S+3_c | 1 | SI Ø610/850 | 21,55 | 0,50 | -21,05 | 4,55 | 5,05 | 0,00 | -16,50 | |
| 1034 | S+0_c | 1 | SI Ø610/850 | 22,25 | 0,50 | -21,75 | 6,75 | 7,25 | 0,00 | -15,00 | |
| 1035 | S+0_c | 1 | SI Ø610/850 | 24,04 | 0,50 | -23,54 | 8,54 | 9,04 | 0,00 | -15,00 | |
| 1036 | S+3_c | 1 | SI Ø762/950 | 23,49 | 0,50 | -22,99 | 8,99 | 9,49 | 0,00 | -14,00 | |
| 1038 | S+0_c | 1 | SI Ø610/850 | 22,54 | 0,50 | -22,04 | 7,04 | 7,54 | 0,00 | -15,00 | |
| 1039 | S+3_c | 1 | SI Ø610/850 | 23,33 | 0,50 | -22,83 | 6,33 | 6,83 | 0,00 | -16,50 | |
| 1040 | S+3_c | 1 | SI Ø610/850 | 21,81 | 0,50 | -21,31 | 4,81 | 5,31 | 0,00 | -16,50 | |
| 1041 | S+0_c | 1 | SI Ø610/850 | 19,66 | 0,50 | -19,16 | 4,16 | 4,66 | 0,00 | -15,00 | |
| 1042 | S+0_c | 1 | SI Ø610/850 | 19,77 | 0,50 | -19,27 | 4,27 | 4,77 | 0,00 | -15,00 | |
| 1043 | S+3_c | 1 | SI Ø610/850 | 21,49 | 0,50 | -20,99 | 4,49 | 4,99 | 0,00 | -16,50 | |
| 1045 | S+0_c | 1 | SI Ø610/850 | 18,89 | 0,50 | -18,39 | 3,39 | 3,89 | 0,00 | -15,00 | |
| 1046 | S+0_c | 1 | SI Ø610/850 | 18,01 | 0,50 | -17,51 | 2,51 | 3,01 | 0,00 | -15,00 | |
| 1047 | S+0_c | 1 | SI Ø762/950 | 23,50 | 0,50 | -23,00 | 2,50 | 3,00 | 0,00 | -20,50 | |
| 1048 | S+0_c | 1 | SI Ø610/850 | 24,71 | 0,50 | -24,21 | 1,71 | 2,21 | 0,00 | -22,50 | |
| 1049 | S+0_c | 1 | SI Ø610/850 | 25,04 | 0,50 | -24,54 | 2,04 | 2,54 | 0,00 | -22,50 | |
| 1050 | S+0_c | 1 | SI Ø610/850 | 24,72 | 0,50 | -24,22 | 1,72 | 2,22 | 0,00 | -22,50 | |
| 1054 | S+6_s | 1 | SI Ø762/950 | 24,25 | 0,50 | -23,75 | 4,75 | 5,25 | 0,00 | -19,00 | |
| 1056 | S+6_s | 1 | SI Ø610/850 | 22,59 | 0,50 | -22,09 | 1,59 | 2,09 | 0,00 | -20,50 | |
| 1057 | S+9_s | 1 | SI Ø610/850 | 22,11 | 0,50 | -21,61 | 0,61 | 1,11 | 0,00 | -21,00 | |
| 1059 | S+6_s | 1 | SI Ø610/850 | 22,81 | 0,50 | -22,31 | 1,81 | 2,31 | 0,00 | -20,50 | |
| 1061 | S+0_s | 1 | SI Ø610/850 | 24,39 | 0,50 | -23,89 | 1,89 | 2,39 | 0,00 | -22,00 | |
| 1064 | S+0_s | 1 | SI Ø610/850 | 20,09 | 0,50 | -19,59 | 2,59 | 3,09 | 0,00 | -17,00 | |
| 1065 | S+0_s | 1 | SI Ø610/850 | 21,21 | 0,50 | -20,71 | 3,71 | 4,21 | 0,00 | -17,00 | |
| 1070 | S+3_c | 1 | SI Ø610/850 | 23,93 | 0,50 | -23,43 | 2,93 | 3,43 | 0,00 | -20,50 | |
| 1071 | S+3_c | 1 | SI Ø610/850 | 22,26 | 0,50 | -21,76 | 1,26 | 1,76 | 0,00 | -20,50 | |
| 1072 | S+9_c | 1 | SI Ø610/850 | 21,21 | 0,50 | -20,71 | 0,21 | 0,71 | 0,00 | -20,50 | |
| 1073 | S+9_c | 1 | SI Ø610/850 | 21,60 | 0,50 | -21,10 | 0,60 | 1,10 | 0,00 | -20,50 | |
| 1074 | S+6_c | 1 | SI Ø610/850 | 21,36 | 0,50 | -20,86 | 0,36 | 0,86 | 0,00 | -20,50 | |
| 1075 | S+3_c | 1 | SI Ø762/950 | 22,84 | 0,50 | -22,34 | 5,84 | 6,34 | 0,00 | -16,50 | |
| 1076 | S+12_c | 2 | SI Ø508/670 | 12,08 | 0,00 | -12,08 | 2,08 | 2,58 | 0,50 | -10,00 | |
| 1077 | S+12_c | 2 | SI Ø508/670 | 18,48 | 0,00 | -18,48 | 0,48 | 0,98 | 0,50 | -18,00 | |
| 1080 | S+6_c | 1 | SI Ø610/850 | 24,18 | 0,50 | -23,68 | 0,18 | 0,68 | 0,00 | -23,50 | |
| 1081 | S+0_c | 2 | SI Ø508/670 | 23,66 | 0,00 | -23,66 | 7,16 | 7,66 | 0,50 | -16,50 | |
| 1082 | S+6_c | 1 | SI Ø610/850 | 24,20 | 0,50 | -23,70 | 0,20 | 0,70 | 0,00 | -23,50 | |
| 1083 | S+3_c | 1 | SI Ø610/850 | 24,81 | 0,50 | -24,31 | 0,81 | 1,31 | 0,00 | -23,50 | |
| 1084 | S+0_c | 1 | SI Ø610/850 | 22,56 | 0,50 | -22,06 | 0,06 | 0,56 | 0,00 | -22,00 | |
| 1085 | S+0_c | 1 | SI Ø610/850 | 22,40 | 0,50 | -21,90 | -0,10 | 0,40 | 0,00 | -22,00 | |
| 1087 | S+6_c | 1 | SI Ø610/850 | 23,91 | 0,50 | -23,41 | -0,09 | 0,41 | 0,00 | -23,50 | |
| 1088 | S+9_c | 1 | SI Ø610/850 | 23,78 | 0,50 | -23,28 | -0,22 | 0,28 | 0,00 | -23,50 | |
| 1090 | S+0_c | 1 | SI Ø610/850 | 22,57 | 0,50 | -22,07 | 0,07 | 0,57 | 0,00 | -22,00 | |

| | | | | | | | | | | |
|------|--------|---|-------------|-------|------|--------|-------|-------|------|--------|
| 1091 | S+0_c | 2 | SI Ø508/670 | 20,85 | 0,00 | -20,85 | -0,15 | 0,35 | 0,50 | -21,00 |
| 1092 | S+0_c | 2 | SI Ø508/670 | 20,88 | 0,00 | -20,88 | -0,12 | 0,38 | 0,50 | -21,00 |
| 1093 | S+3_c | 2 | SI Ø508/670 | 22,20 | 0,00 | -22,20 | -0,30 | 0,20 | 0,50 | -22,50 |
| 1096 | S+0_c | 2 | SI Ø508/670 | 21,01 | 0,00 | -21,01 | 0,01 | 0,51 | 0,50 | -21,00 |
| 1097 | S+0_c | 2 | SI Ø508/670 | 21,25 | 0,00 | -21,25 | 0,25 | 0,75 | 0,50 | -21,00 |
| 1100 | S+6_c | 2 | SI Ø508/670 | 21,79 | 0,00 | -21,79 | -0,71 | -0,21 | 0,50 | -22,50 |
| 1101 | S+6_c | 2 | SI Ø508/670 | 22,12 | 0,00 | -22,12 | -0,38 | 0,12 | 0,50 | -22,50 |
| 1102 | S+9_c | 2 | SI Ø508/670 | 22,18 | 0,00 | -22,18 | -0,82 | -0,32 | 0,50 | -23,00 |
| 1103 | S+9_c | 2 | SI Ø508/670 | 18,96 | 0,50 | -18,46 | 0,46 | 0,96 | 0,00 | -18,00 |
| 1104 | S+3_c | 2 | SI Ø508/670 | 16,64 | 0,00 | -16,64 | -0,36 | 0,14 | 0,50 | -17,00 |
| 1106 | S+0_c | 1 | SI Ø762/950 | 23,40 | 0,50 | -22,90 | -0,10 | 0,40 | 0,00 | -23,00 |
| 1107 | S+0_c | 1 | SI Ø762/950 | 23,29 | 0,50 | -22,79 | -0,21 | 0,29 | 0,00 | -23,00 |
| 1108 | S+0_c | 1 | SI Ø762/950 | 23,53 | 0,50 | -23,03 | 0,03 | 0,53 | 0,00 | -23,00 |
| 1109 | S+0_c | 1 | SI Ø762/950 | 23,58 | 0,50 | -23,08 | 0,08 | 0,58 | 0,00 | -23,00 |
| 1110 | S+3_c | 2 | SI Ø508/670 | 17,36 | 0,00 | -17,36 | 0,36 | 0,86 | 0,50 | -17,00 |
| 1112 | S+0_c | 1 | SI Ø762/950 | 23,45 | 0,50 | -22,95 | -0,05 | 0,45 | 0,00 | -23,00 |
| 1113 | S+0_c | 1 | SI Ø762/950 | 23,24 | 0,50 | -22,74 | -0,26 | 0,24 | 0,00 | -23,00 |
| 1115 | S+12_c | 2 | SI Ø508/670 | 18,91 | 0,00 | -18,91 | 0,41 | 0,91 | 0,50 | -18,50 |
| 1116 | S+12_c | 2 | SI Ø508/670 | 18,34 | 0,00 | -18,34 | -0,16 | 0,34 | 0,50 | -18,50 |
| 1117 | S+12_c | 2 | SI Ø508/670 | 16,60 | 0,00 | -16,60 | -0,40 | 0,10 | 0,50 | -17,00 |
| 1119 | S-3_c | 1 | SI Ø610/850 | 20,15 | 0,50 | -19,65 | -0,35 | 0,15 | 0,00 | -20,00 |
| 1120 | S-3_c | 1 | SI Ø610/850 | 20,21 | 0,50 | -19,71 | -0,29 | 0,21 | 0,00 | -20,00 |
| 1121 | S-3_c | 1 | SI Ø610/850 | 20,62 | 0,50 | -20,12 | 0,12 | 0,62 | 0,00 | -20,00 |
| 1122 | S+0_c | 1 | SI Ø610/850 | 21,53 | 0,50 | -21,03 | 0,03 | 0,53 | 0,00 | -21,00 |
| 1124 | S+0_c | 1 | SI Ø610/850 | 20,70 | 0,50 | -20,20 | -0,80 | -0,30 | 0,00 | -21,00 |
| 1125 | S+0_c | 1 | SI Ø610/850 | 20,56 | 0,50 | -20,06 | -0,95 | -0,45 | 0,00 | -21,00 |
| 1126 | S+0_c | 1 | SI Ø610/850 | 20,59 | 0,50 | -20,09 | -0,92 | -0,42 | 0,00 | -21,00 |
| 1127 | S+0_c | 1 | SI Ø610/850 | 20,21 | 0,50 | -19,71 | -1,29 | -0,79 | 0,00 | -21,00 |
| 1129 | S+0_c | 1 | SI Ø610/850 | 20,78 | 0,50 | -20,28 | -0,72 | -0,22 | 0,00 | -21,00 |
| 1132 | S+0_c | 1 | SI Ø610/850 | 20,25 | 0,50 | -19,75 | -1,25 | -0,75 | 0,00 | -21,00 |
| 1134 | S+0_c | 1 | SI Ø610/850 | 19,86 | 0,50 | -19,36 | -1,15 | -0,65 | 0,00 | -20,50 |
| 1135 | S+0_c | 1 | SI Ø610/850 | 20,13 | 0,50 | -19,63 | -0,87 | -0,37 | 0,00 | -20,50 |
| 1136 | S+0_c | 1 | SI Ø610/850 | 20,39 | 0,50 | -19,89 | -0,61 | -0,11 | 0,00 | -20,50 |
| 1138 | S+3_c | 1 | SI Ø610/850 | 22,40 | 0,50 | -21,90 | -0,10 | 0,40 | 0,00 | -22,00 |
| 1139 | S+3_c | 1 | SI Ø610/850 | 22,41 | 0,50 | -21,91 | -0,09 | 0,41 | 0,00 | -22,00 |
| 1140 | S+0_c | 1 | SI Ø610/850 | 20,90 | 0,50 | -20,40 | -0,10 | 0,40 | 0,00 | -20,50 |
| 1141 | S+0_c | 1 | SI Ø610/850 | 21,10 | 0,50 | -20,60 | 0,10 | 0,60 | 0,00 | -20,50 |
| 1142 | S+0_c | 1 | SI Ø610/850 | 21,03 | 0,50 | -20,53 | 0,03 | 0,53 | 0,00 | -20,50 |
| 1143 | S+0_c | 1 | SI Ø610/850 | 21,06 | 0,50 | -20,56 | 0,06 | 0,56 | 0,00 | -20,50 |
| 1144 | S+0_c | 1 | SI Ø610/850 | 21,04 | 0,50 | -20,54 | 0,04 | 0,54 | 0,00 | -20,50 |
| 1145 | S+0_c | 1 | SI Ø610/850 | 20,87 | 0,50 | -20,37 | -0,13 | 0,37 | 0,00 | -20,50 |
| 1146 | S+0_c | 1 | SI Ø610/850 | 20,79 | 0,50 | -20,29 | -0,21 | 0,29 | 0,00 | -20,50 |
| 1149 | S+24_s | 2 | SI Ø508/670 | 15,94 | 0,00 | -15,94 | 0,44 | 0,94 | 0,50 | -15,50 |
| 1155 | S+3_c | 1 | SI Ø610/850 | 20,83 | 0,50 | -20,33 | 0,33 | 0,83 | 0,00 | -20,00 |
| 1156 | S+6_c | 1 | SI Ø610/850 | 22,24 | 0,50 | -21,74 | 0,24 | 0,74 | 0,00 | -21,50 |
| 1157 | S+6_c | 1 | SI Ø610/850 | 23,44 | 0,50 | -22,94 | 1,44 | 1,94 | 0,00 | -21,50 |
| 1160 | S+3_c | 1 | SI Ø610/850 | 22,63 | 0,50 | -22,13 | 0,63 | 1,13 | 0,00 | -21,50 |
| 1161 | S+0_c | 1 | SI Ø610/850 | 20,68 | 0,50 | -20,18 | 0,18 | 0,68 | 0,00 | -20,00 |
| 1162 | S+0_c | 1 | SI Ø610/850 | 20,84 | 0,50 | -20,34 | 0,34 | 0,84 | 0,00 | -20,00 |
| 1164 | S+0_c | 1 | SI Ø610/850 | 21,96 | 0,50 | -21,46 | -0,04 | 0,46 | 0,00 | -21,50 |
| 1165 | S+6_c | 1 | SI Ø610/850 | 23,31 | 0,50 | -22,81 | -0,19 | 0,31 | 0,00 | -23,00 |
| 1166 | S+6_c | 1 | SI Ø610/850 | 23,03 | 0,50 | -22,53 | -0,47 | 0,03 | 0,00 | -23,00 |
| 1169 | S+3_c | 1 | SI Ø610/850 | 23,15 | 0,50 | -22,65 | -0,35 | 0,15 | 0,00 | -23,00 |
| 1170 | S+0_c | 1 | SI Ø610/850 | 21,63 | 0,50 | -21,13 | -0,38 | 0,13 | 0,00 | -21,50 |
| 1171 | S+0_c | 1 | SI Ø610/850 | 21,97 | 0,50 | -21,47 | -0,03 | 0,47 | 0,00 | -21,50 |
| 1172 | S+3_c | 1 | SI Ø610/850 | 22,13 | 0,50 | -21,63 | 0,13 | 0,63 | 0,00 | -21,50 |
| 1173 | S+0_c | 1 | SI Ø610/850 | 22,06 | 0,50 | -21,56 | 0,06 | 0,56 | 0,00 | -21,50 |
| 1174 | S+0_c | 1 | SI Ø610/850 | 22,18 | 0,50 | -21,68 | 0,18 | 0,68 | 0,00 | -21,50 |
| 1175 | S+0_c | 1 | SI Ø610/850 | 22,25 | 0,50 | -21,75 | 0,25 | 0,75 | 0,00 | -21,50 |
| 1176 | S+0_c | 1 | SI Ø610/850 | 22,46 | 0,50 | -21,96 | 0,46 | 0,96 | 0,00 | -21,50 |
| 1178 | S+3_c | 1 | SI Ø610/850 | 18,36 | 0,50 | -17,86 | 0,36 | 0,86 | 0,00 | -17,50 |
| 1179 | S+3_c | 1 | SI Ø610/850 | 18,61 | 0,50 | -18,11 | 0,61 | 1,11 | 0,00 | -17,50 |
| 1180 | S+3_c | 1 | SI Ø610/850 | 18,99 | 0,50 | -18,49 | 0,99 | 1,49 | 0,00 | -17,50 |

| | | | | | | | | | | |
|-------|-------|---|-------------|-------|------|--------|------|-------|------|--------|
| 1181 | S+3_c | 1 | SI Ø610/850 | 19,36 | 0,50 | -18,86 | 1,36 | 1,86 | 0,00 | -17,50 |
| 1182 | S+0_c | 1 | SI Ø610/850 | 17,24 | 0,50 | -16,74 | 1,24 | 1,74 | 0,00 | -15,50 |
| 1183 | S+0_c | 1 | SI Ø610/850 | 17,52 | 0,50 | -17,02 | 1,52 | 2,02 | 0,00 | -15,50 |
| 1185 | S+3_c | 1 | SI Ø610/850 | 20,74 | 0,50 | -20,24 | 2,74 | 3,24 | 0,00 | -17,50 |
| 1186 | S+0_c | 1 | SI Ø610/850 | 20,47 | 0,50 | -19,97 | 2,47 | 2,97 | 0,00 | -17,50 |
| 1189 | S+0_c | 1 | SI Ø610/850 | 20,03 | 0,50 | -19,53 | 4,03 | 4,53 | 0,00 | -15,50 |
| 1190 | S+0_c | 1 | SI Ø610/850 | 20,49 | 0,50 | -19,99 | 4,49 | 4,99 | 0,00 | -15,50 |
| 1191 | S-3_c | 1 | SI Ø610/850 | 16,00 | 0,50 | -15,50 | 5,00 | 5,50 | 0,00 | -10,50 |
| 1193 | S+9_c | 1 | SI Ø610/850 | 18,72 | 0,50 | -18,22 | 5,72 | 6,22 | 0,00 | -12,50 |
| 1195 | S+0_c | 1 | SI Ø610/850 | 17,87 | 0,50 | -17,37 | 6,87 | 7,37 | 0,00 | -10,50 |
| 1197 | S+9_c | 1 | SI Ø610/850 | 21,10 | 0,50 | -20,60 | 8,10 | 8,60 | 0,00 | -12,50 |
| 1197A | S+9_c | 1 | SI Ø610/850 | 21,50 | 0,50 | -21,00 | 8,50 | 9,00 | 0,00 | -12,50 |
| 1198 | S+6_c | 1 | SI Ø610/850 | 20,96 | 0,50 | -20,46 | 8,46 | 8,96 | 0,00 | -12,00 |
| 1200 | S+3_c | 1 | SI Ø610/850 | 21,83 | 0,50 | -21,33 | 9,33 | 9,83 | 0,00 | -12,00 |
| 1201 | S+0_c | 1 | SI Ø610/850 | 20,31 | 0,50 | -19,81 | 9,31 | 9,81 | 0,00 | -10,50 |
| 1202 | S+0_c | 1 | SI Ø610/850 | 20,25 | 0,50 | -19,75 | 9,25 | 9,75 | 0,00 | -10,50 |
| 1203 | S+3_c | 1 | SI Ø610/850 | 22,29 | 0,50 | -21,79 | 9,79 | 10,29 | 0,00 | -12,00 |

Poergegevens

| Mastnr. | Masttype | Poertype | L [m] | b [m]2 | h [m] | Bovenkant poer tov. NAP [m] | Bovenkant poer tov MV [m] (1) | Onderkant poer tov. MV [m] | Volume onder GWS [m] | Volume poer [m3] | EGpoer [kN] |
|---------|----------|----------------|-------|--------|-------|-----------------------------|-------------------------------|----------------------------|----------------------|------------------|-------------|
| 1003 | S+18_s | 2-paalspoer | 3,00 | 1,50 | 2,00 | 1,85 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1004 | S+18_s | 2-paalspoer | 3,00 | 1,50 | 2,00 | 2,01 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1076 | S+12_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 2,58 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1077 | S+12_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,98 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1081 | S+0_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 7,66 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1091 | S+0_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,35 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1092 | S+0_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,38 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1093 | S+3_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,20 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1096 | S+0_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,51 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1097 | S+0_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,75 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1100 | S+6_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | -0,21 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1101 | S+6_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,12 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1102 | S+9_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | -0,32 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1103 | S+9_c | 2-paalspoer HW | 3,00 | 1,80 | 2,50 | 0,96 | 1,00 | -1,50 | 8,10 | 13,50 | 338 |
| 1104 | S+3_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,14 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1110 | S+3_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,86 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1115 | S+12_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,91 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1116 | S+12_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,34 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1117 | S+12_c | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,10 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |
| 1149 | S+24_s | 2-paalspoer | 3,00 | 1,50 | 2,00 | 0,94 | 0,50 | -1,50 | 6,75 | 9,00 | 225 |

APPENDIX C

Resultaten

Controle op trek en drukbelasting

| Toetsing funderingen op trekbelasting | | | | | | | | | | | | |
|---------------------------------------|----------|-----------------------|--------------|-------------|--------------------|---------------------------|----------------------------|---------------------|--------------------------|---------------------------|----------------------------|------|
| Mast | Masttype | Sondering | Poertype | Paaltype | PP niveau [m- NAP] | F _{Ed,mast} [kN] | Aantal palen per randstijl | Effectiviteit palen | F _{poer,d} [kN] | F _{Ed,paal} [kN] | F _{R,d,trek} [kN] | U.C. |
| 1003 | S+18_s | 2019-1008_1.GEF | 2-paalspoer | SI Ø508/670 | -21,5 | -1750 | 2 | 95% | 135 | 850 | 985 | 0,86 |
| 1004 | S+18_s | 2019-1008_1.GEF | 2-paalspoer | SI Ø508/670 | -21,5 | -1750 | 2 | 95% | 135 | 850 | 985 | 0,86 |
| 1006 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | -1240 | 1 | 100% | 0 | 1240 | 1412 | 0,88 |
| 1008 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | -1240 | 1 | 100% | 0 | 1240 | 1412 | 0,88 |
| 1009 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | -1240 | 1 | 100% | 0 | 1240 | 1412 | 0,88 |
| 1010 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | -1240 | 1 | 100% | 0 | 1240 | 1412 | 0,88 |
| 1011 | S-3_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -22,0 | -1132 | 1 | 100% | 0 | 1132 | 1297 | 0,87 |
| 1012 | S-3_s | 2019-1008_1.GEF | 1-paals hoog | SI Ø610/850 | -22,0 | -1132 | 1 | 100% | 0 | 1132 | 1297 | 0,87 |
| 1013 | S-3_s | 2019-1008_1.GEF | 1-paals hoog | SI Ø610/850 | -22,0 | -1132 | 1 | 100% | 0 | 1132 | 1297 | 0,87 |
| 1026 | S-3_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -8,5 | -1239 | 1 | 100% | 0 | 1239 | 1408 | 0,88 |
| 1028 | S+0_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -9,5 | -1333 | 1 | 100% | 0 | 1333 | 1523 | 0,88 |
| 1029 | S+6_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -9,5 | -1481 | 1 | 100% | 0 | 1481 | 1523 | 0,97 |
| 1030 | S+3_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -10,5 | -1461 | 1 | 100% | 0 | 1461 | 1638 | 0,89 |
| 1031 | S+0_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -9,5 | -1333 | 1 | 100% | 0 | 1333 | 1523 | 0,88 |
| 1032 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0,89 |
| 1034 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0,90 |
| 1035 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0,90 |
| 1036 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø762/950 | -14,0 | -1461 | 1 | 100% | 0 | 1461 | 1620 | 0,90 |
| 1038 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0,90 |
| 1039 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0,89 |
| 1040 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0,89 |
| 1041 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0,90 |
| 1042 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0,90 |
| 1043 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0,89 |
| 1045 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0,90 |
| 1046 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0,90 |
| 1047 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø762/950 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1497 | 0,89 |
| 1048 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,5 | -1333 | 1 | 100% | 0 | 1333 | 1479 | 0,90 |
| 1049 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,5 | -1333 | 1 | 100% | 0 | 1333 | 1479 | 0,90 |
| 1050 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,5 | -1333 | 1 | 100% | 0 | 1333 | 1479 | 0,90 |
| 1054 | S+6_s | 2019-1008_11.GEF | 1-paals | SI Ø762/950 | -19,0 | -1128 | 1 | 100% | 0 | 1128 | 1292 | 0,87 |
| 1056 | S+6_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -20,5 | -1128 | 1 | 100% | 0 | 1128 | 1252 | 0,90 |
| 1057 | S+9_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -21,0 | -1151 | 1 | 100% | 0 | 1151 | 1309 | 0,88 |
| 1059 | S+6_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -20,5 | -1128 | 1 | 100% | 0 | 1128 | 1252 | 0,90 |
| 1061 | S+0_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,0 | -1240 | 1 | 100% | 0 | 1240 | 1421 | 0,87 |
| 1064 | S+0_s | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -17,0 | -1240 | 1 | 100% | 0 | 1240 | 1378 | 0,90 |
| 1065 | S+0_s | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -17,0 | -1240 | 1 | 100% | 0 | 1240 | 1378 | 0,90 |
| 1070 | S+3_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | -1461 | 1 | 100% | 0 | 1461 | 1681 | 0,87 |
| 1071 | S+3_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | -1461 | 1 | 100% | 0 | 1461 | 1681 | 0,87 |
| 1072 | S+9_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | -1495 | 1 | 100% | 0 | 1495 | 1681 | 0,89 |
| 1073 | S+9_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | -1495 | 1 | 100% | 0 | 1495 | 1681 | 0,89 |
| 1074 | S+6_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | -1481 | 1 | 100% | 0 | 1481 | 1681 | 0,88 |
| 1075 | S+3_c | 2019-1008_12.GEF | 1-paals | SI Ø762/950 | -16,5 | -1461 | 1 | 100% | 0 | 1461 | 1618 | 0,90 |
| 1076 | S+12_c | 2019-1008_12.GEF | 2-paalspoer | SI Ø508/670 | -10,0 | -1582 | 2 | 95% | 135 | 761 | 910 | 0,84 |
| 1077 | S+12_c | 2019-1008_17.GEF | 2-paalspoer | SI Ø508/670 | -18,0 | -1582 | 2 | 95% | 135 | 761 | 874 | 0,87 |
| 1080 | S+6_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | -1481 | 1 | 100% | 0 | 1481 | 1661 | 0,89 |
| 1081 | S+0_c | 2019-1008_17.GEF | 2-paalspoer | SI Ø508/670 | -16,5 | -1333 | 2 | 95% | 135 | 630 | 727 | 0,87 |
| 1082 | S+6_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | -1481 | 1 | 100% | 0 | 1481 | 1661 | 0,89 |
| 1083 | S+3_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | -1461 | 1 | 100% | 0 | 1461 | 1661 | 0,88 |
| 1084 | S+0_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -22,0 | -1333 | 1 | 100% | 0 | 1333 | 1488 | 0,90 |
| 1085 | S+0_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -22,0 | -1333 | 1 | 100% | 0 | 1333 | 1488 | 0,90 |
| 1087 | S+6_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | -1481 | 1 | 100% | 0 | 1481 | 1661 | 0,89 |
| 1088 | S+9_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | -1495 | 1 | 100% | 0 | 1495 | 1661 | 0,90 |
| 1090 | S+0_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -22,0 | -1333 | 1 | 100% | 0 | 1333 | 1488 | 0,90 |
| 1091 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | -1333 | 2 | 95% | 135 | 630 | 745 | 0,85 |
| 1092 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | -1333 | 2 | 95% | 135 | 630 | 745 | 0,85 |
| 1093 | S+3_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -22,5 | -1461 | 2 | 95% | 135 | 698 | 799 | 0,87 |
| 1096 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | -1333 | 2 | 95% | 135 | 630 | 745 | 0,85 |
| 1097 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | -1333 | 2 | 95% | 135 | 630 | 745 | 0,85 |
| 1100 | S+6_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -22,5 | -1481 | 2 | 95% | 135 | 708 | 799 | 0,89 |

| | | | | | | | | | | | | |
|------|--------|-----------------------|----------------|-------------|-------|-------|---|------|-----|------|------|------|
| 1101 | S+6_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -22,5 | -1481 | 2 | 95% | 135 | 708 | 799 | 0.89 |
| 1102 | S+9_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -23,0 | -1495 | 2 | 95% | 135 | 716 | 813 | 0.88 |
| 1103 | S+9_c | 2019-1008_21.GEF | 2-paalspoer HW | SI Ø508/670 | -18,0 | -1495 | 2 | 95% | 223 | 670 | 814 | 0.82 |
| 1104 | S+3_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -17,0 | -1461 | 2 | 95% | 135 | 698 | 787 | 0.89 |
| 1106 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0.90 |
| 1107 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0.90 |
| 1108 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0.90 |
| 1109 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0.90 |
| 1110 | S+3_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -17,0 | -1461 | 2 | 95% | 135 | 698 | 787 | 0.89 |
| 1112 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0.90 |
| 1113 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | -1333 | 1 | 100% | 0 | 1333 | 1473 | 0.90 |
| 1115 | S+12_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -18,5 | -1582 | 2 | 95% | 135 | 761 | 863 | 0.88 |
| 1116 | S+12_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -18,5 | -1582 | 2 | 95% | 135 | 761 | 863 | 0.88 |
| 1117 | S+12_c | 02P001595_251.S01.GEF | 2-paalspoer | SI Ø508/670 | -17,0 | -1582 | 2 | 95% | 135 | 761 | 890 | 0.86 |
| 1119 | S-3_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -20,0 | -1239 | 1 | 100% | 0 | 1239 | 1400 | 0.89 |
| 1120 | S-3_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -20,0 | -1239 | 1 | 100% | 0 | 1239 | 1400 | 0.89 |
| 1121 | S-3_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -20,0 | -1239 | 1 | 100% | 0 | 1239 | 1400 | 0.89 |
| 1122 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | -1333 | 1 | 100% | 0 | 1333 | 1528 | 0.87 |
| 1124 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | -1333 | 1 | 100% | 0 | 1333 | 1528 | 0.87 |
| 1125 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | -1333 | 1 | 100% | 0 | 1333 | 1528 | 0.87 |
| 1126 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | -1333 | 1 | 100% | 0 | 1333 | 1528 | 0.87 |
| 1127 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | -1333 | 1 | 100% | 0 | 1333 | 1528 | 0.87 |
| 1129 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | -1333 | 1 | 100% | 0 | 1333 | 1528 | 0.87 |
| 1132 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | -1333 | 1 | 100% | 0 | 1333 | 1528 | 0.87 |
| 1134 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1135 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1136 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1138 | S+3_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -22,0 | -1461 | 1 | 100% | 0 | 1461 | 1655 | 0.88 |
| 1139 | S+3_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -22,0 | -1461 | 1 | 100% | 0 | 1461 | 1655 | 0.88 |
| 1140 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1141 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1142 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1143 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1144 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1145 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1146 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | -1333 | 1 | 100% | 0 | 1333 | 1483 | 0.90 |
| 1149 | S+24_s | 02P001595_283.S02.GEF | 2-paalspoer | SI Ø508/670 | -15,5 | -1504 | 2 | 95% | 135 | 721 | 808 | 0.89 |
| 1155 | S+3_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -20,0 | -1461 | 1 | 100% | 0 | 1461 | 1514 | 0.96 |
| 1156 | S+6_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -21,5 | -1481 | 1 | 100% | 0 | 1481 | 1684 | 0.88 |
| 1157 | S+6_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -21,5 | -1481 | 1 | 100% | 0 | 1481 | 1684 | 0.88 |
| 1160 | S+3_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -21,5 | -1461 | 1 | 100% | 0 | 1461 | 1684 | 0.87 |
| 1161 | S+0_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -20,0 | -1333 | 1 | 100% | 0 | 1333 | 1514 | 0.88 |
| 1162 | S+0_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -20,0 | -1333 | 1 | 100% | 0 | 1333 | 1514 | 0.88 |
| 1164 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1333 | 1 | 100% | 0 | 1333 | 1484 | 0.90 |
| 1165 | S+6_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -23,0 | -1481 | 1 | 100% | 0 | 1481 | 1655 | 0.89 |
| 1166 | S+6_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -23,0 | -1481 | 1 | 100% | 0 | 1481 | 1655 | 0.89 |
| 1169 | S+3_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -23,0 | -1461 | 1 | 100% | 0 | 1461 | 1655 | 0.88 |
| 1170 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1333 | 1 | 100% | 0 | 1333 | 1484 | 0.90 |
| 1171 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1333 | 1 | 100% | 0 | 1333 | 1484 | 0.90 |
| 1172 | S+3_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1461 | 1 | 100% | 0 | 1461 | 1484 | 0.98 |
| 1173 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1333 | 1 | 100% | 0 | 1333 | 1484 | 0.90 |
| 1174 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1333 | 1 | 100% | 0 | 1333 | 1484 | 0.90 |
| 1175 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1333 | 1 | 100% | 0 | 1333 | 1484 | 0.90 |
| 1176 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | -1333 | 1 | 100% | 0 | 1333 | 1484 | 0.90 |
| 1178 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0.89 |
| 1179 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0.89 |
| 1180 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0.89 |
| 1181 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0.89 |
| 1182 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | -1333 | 1 | 100% | 0 | 1333 | 1477 | 0.90 |
| 1183 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | -1333 | 1 | 100% | 0 | 1333 | 1477 | 0.90 |
| 1185 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | -1461 | 1 | 100% | 0 | 1461 | 1646 | 0.89 |
| 1186 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | -1333 | 1 | 100% | 0 | 1333 | 1646 | 0.81 |
| 1189 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | -1333 | 1 | 100% | 0 | 1333 | 1477 | 0.90 |
| 1190 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | -1333 | 1 | 100% | 0 | 1333 | 1477 | 0.90 |
| 1191 | S-3_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | -1239 | 1 | 100% | 0 | 1239 | 1479 | 0.84 |
| 1193 | S+9_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,5 | -1495 | 1 | 100% | 0 | 1495 | 1709 | 0.87 |
| 1195 | S+0_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | -1333 | 1 | 100% | 0 | 1333 | 1479 | 0.90 |



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|-------|-------|------------------|---------|-------------|-------|-------|---|------|---|------|------|------|
| 1197 | S+9_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,5 | -1495 | 1 | 100% | 0 | 1495 | 1709 | 0,87 |
| 1197A | S+9_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,5 | -1495 | 1 | 100% | 0 | 1495 | 1709 | 0,87 |
| 1198 | S+6_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,0 | -1481 | 1 | 100% | 0 | 1481 | 1652 | 0,90 |
| 1200 | S+3_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,0 | -1461 | 1 | 100% | 0 | 1461 | 1652 | 0,88 |
| 1201 | S+0_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | -1333 | 1 | 100% | 0 | 1333 | 1479 | 0,90 |
| 1202 | S+0_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | -1333 | 1 | 100% | 0 | 1333 | 1479 | 0,90 |
| 1203 | S+3_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,0 | -1461 | 1 | 100% | 0 | 1461 | 1652 | 0,88 |

Toetsing funderingen op drukbelasting

| Mast | Masttype | Sondering | Poorttype | Paalttype | PP niveau [m- NAP] | F _{Ed,mast} [kN] | Aantal palen per randstijl | Effectiviteit palen | F _{Poer,d} [kN] | F _{Ed,paal} [kN] | F _{R,d,druk} [kN] | U.C. |
|------|----------|-----------------------|----------------|-------------|-----------------------------|------------------------------|-------------------------------------|------------------------|-----------------------------|------------------------------|-------------------------------|------|
| 1003 | S+18_s | 2019-1008_1.GEF | 2-paalspoer | SI Ø508/670 | -21,5 | 2170 | 2 | 95% | 270 | 1284 | 3011 | 0,43 |
| 1004 | S+18_s | 2019-1008_1.GEF | 2-paalspoer | SI Ø508/670 | -21,5 | 2170 | 2 | 95% | 270 | 1284 | 3011 | 0,43 |
| 1006 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | 1532 | 1 | 100% | 0 | 1532 | 5740 | 0,27 |
| 1008 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | 1532 | 1 | 100% | 0 | 1532 | 5740 | 0,27 |
| 1009 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | 1532 | 1 | 100% | 0 | 1532 | 5740 | 0,27 |
| 1010 | S+0_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -23,0 | 1532 | 1 | 100% | 0 | 1532 | 5740 | 0,27 |
| 1011 | S-3_s | 2019-1008_1.GEF | 1-paals | SI Ø610/850 | -22,0 | 1414 | 1 | 100% | 0 | 1414 | 5554 | 0,25 |
| 1012 | S-3_s | 2019-1008_1.GEF | 1-paals hoog | SI Ø610/850 | -22,0 | 1414 | 1 | 100% | 0 | 1414 | 5554 | 0,25 |
| 1013 | S-3_s | 2019-1008_1.GEF | 1-paals hoog | SI Ø610/850 | -22,0 | 1414 | 1 | 100% | 0 | 1414 | 5554 | 0,25 |
| 1026 | S-3_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -8,5 | 1628 | 1 | 100% | 0 | 1628 | 4805 | 0,34 |
| 1028 | S+0_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -9,5 | 1743 | 1 | 100% | 0 | 1743 | 5053 | 0,34 |
| 1029 | S+6_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -9,5 | 1910 | 1 | 100% | 0 | 1910 | 5053 | 0,38 |
| 1030 | S+3_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -10,5 | 1878 | 1 | 100% | 0 | 1878 | 5850 | 0,32 |
| 1031 | S+0_c | 2019-1008_6.GEF | 1-paals | SI Ø610/850 | -9,5 | 1743 | 1 | 100% | 0 | 1743 | 5053 | 0,34 |
| 1032 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | 1878 | 1 | 100% | 0 | 1878 | 4639 | 0,40 |
| 1034 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | 1743 | 1 | 100% | 0 | 1743 | 3983 | 0,44 |
| 1035 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | 1743 | 1 | 100% | 0 | 1743 | 3983 | 0,44 |
| 1036 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø762/950 | -14,0 | 1878 | 1 | 100% | 0 | 1878 | 4767 | 0,39 |
| 1038 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | 1743 | 1 | 100% | 0 | 1743 | 3983 | 0,44 |
| 1039 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | 1878 | 1 | 100% | 0 | 1878 | 4639 | 0,40 |
| 1040 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | 1878 | 1 | 100% | 0 | 1878 | 4639 | 0,40 |
| 1041 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | 1743 | 1 | 100% | 0 | 1743 | 3983 | 0,44 |
| 1042 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | 1743 | 1 | 100% | 0 | 1743 | 3983 | 0,44 |
| 1043 | S+3_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -16,5 | 1878 | 1 | 100% | 0 | 1878 | 4639 | 0,40 |
| 1045 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | 1743 | 1 | 100% | 0 | 1743 | 3983 | 0,44 |
| 1046 | S+0_c | 02P001595_166.S01.GEF | 1-paals | SI Ø610/850 | -15,0 | 1743 | 1 | 100% | 0 | 1743 | 3983 | 0,44 |
| 1047 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø762/950 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 4178 | 0,42 |
| 1048 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,5 | 1743 | 1 | 100% | 0 | 1743 | 3239 | 0,54 |
| 1049 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,5 | 1743 | 1 | 100% | 0 | 1743 | 3239 | 0,54 |
| 1050 | S+0_c | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,5 | 1743 | 1 | 100% | 0 | 1743 | 3239 | 0,54 |
| 1054 | S+6_s | 2019-1008_11.GEF | 1-paals | SI Ø762/950 | -19,0 | 1445 | 1 | 100% | 0 | 1445 | 4595 | 0,31 |
| 1056 | S+6_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -20,5 | 1445 | 1 | 100% | 0 | 1445 | 3283 | 0,44 |
| 1057 | S+9_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -21,0 | 1495 | 1 | 100% | 0 | 1495 | 3352 | 0,45 |
| 1059 | S+6_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -20,5 | 1445 | 1 | 100% | 0 | 1445 | 3283 | 0,44 |
| 1061 | S+0_s | 2019-1008_11.GEF | 1-paals | SI Ø610/850 | -22,0 | 1532 | 1 | 100% | 0 | 1532 | 3242 | 0,47 |
| 1064 | S+0_s | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -17,0 | 1532 | 1 | 100% | 0 | 1532 | 2556 | 0,60 |
| 1065 | S+0_s | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -17,0 | 1532 | 1 | 100% | 0 | 1532 | 2556 | 0,60 |
| 1070 | S+3_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | 1878 | 1 | 100% | 0 | 1878 | 3851 | 0,49 |
| 1071 | S+3_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | 1878 | 1 | 100% | 0 | 1878 | 3851 | 0,49 |
| 1072 | S+9_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | 1955 | 1 | 100% | 0 | 1955 | 3851 | 0,51 |
| 1073 | S+9_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | 1955 | 1 | 100% | 0 | 1955 | 3851 | 0,51 |
| 1074 | S+6_c | 2019-1008_12.GEF | 1-paals | SI Ø610/850 | -20,5 | 1910 | 1 | 100% | 0 | 1910 | 3851 | 0,50 |
| 1075 | S+3_c | 2019-1008_12.GEF | 1-paals | SI Ø762/950 | -16,5 | 1878 | 1 | 100% | 0 | 1878 | 3002 | 0,63 |
| 1076 | S+12_c | 2019-1008_12.GEF | 2-paalspoer | SI Ø508/670 | -10,0 | 2093 | 2 | 95% | 270 | 1244 | 1596 | 0,78 |
| 1077 | S+12_c | 2019-1008_17.GEF | 2-paalspoer | SI Ø508/670 | -18,0 | 2093 | 2 | 95% | 270 | 1244 | 1465 | 0,85 |
| 1080 | S+6_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | 1910 | 1 | 100% | 0 | 1910 | 3274 | 0,58 |
| 1081 | S+0_c | 2019-1008_17.GEF | 2-paalspoer | SI Ø508/670 | -16,5 | 1743 | 2 | 95% | 270 | 1059 | 1406 | 0,75 |
| 1082 | S+6_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | 1910 | 1 | 100% | 0 | 1910 | 3274 | 0,58 |
| 1083 | S+3_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | 1878 | 1 | 100% | 0 | 1878 | 3274 | 0,57 |
| 1084 | S+0_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -22,0 | 1743 | 1 | 100% | 0 | 1743 | 3186 | 0,55 |
| 1085 | S+0_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -22,0 | 1743 | 1 | 100% | 0 | 1743 | 3186 | 0,55 |
| 1087 | S+6_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | 1910 | 1 | 100% | 0 | 1910 | 3274 | 0,58 |
| 1088 | S+9_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -23,5 | 1955 | 1 | 100% | 0 | 1955 | 3274 | 0,60 |
| 1090 | S+0_c | 2019-1008_17.GEF | 1-paals | SI Ø610/850 | -22,0 | 1743 | 1 | 100% | 0 | 1743 | 3186 | 0,55 |
| 1091 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | 1743 | 2 | 95% | 270 | 1059 | 1297 | 0,82 |
| 1092 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | 1743 | 2 | 95% | 270 | 1059 | 1297 | 0,82 |
| 1093 | S+3_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -22,5 | 1878 | 2 | 95% | 270 | 1130 | 1367 | 0,83 |
| 1096 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | 1743 | 2 | 95% | 270 | 1059 | 1297 | 0,82 |
| 1097 | S+0_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -21,0 | 1743 | 2 | 95% | 270 | 1059 | 1297 | 0,82 |
| 1100 | S+6_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -22,5 | 1910 | 2 | 95% | 270 | 1147 | 1367 | 0,84 |
| 1101 | S+6_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -22,5 | 1910 | 2 | 95% | 270 | 1147 | 1367 | 0,84 |
| 1102 | S+9_c | 2019-1008_20.GEF | 2-paalspoer | SI Ø508/670 | -23,0 | 1955 | 2 | 95% | 270 | 1171 | 1627 | 0,72 |
| 1103 | S+9_c | 2019-1008_21.GEF | 2-paalspoer HW | SI Ø508/670 | -18,0 | 1955 | 2 | 95% | 405 | 1242 | 1357 | 0,92 |

| | | | | | | | | | | | | |
|-------|--------|-----------------------|-------------|-------------|-------|------|---|------|-----|------|------|------|
| 1104 | S+3_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -17,0 | 1878 | 2 | 95% | 270 | 1130 | 1235 | 0,92 |
| 1106 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | 1743 | 1 | 100% | 0 | 1743 | 2422 | 0,72 |
| 1107 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | 1743 | 1 | 100% | 0 | 1743 | 2422 | 0,72 |
| 1108 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | 1743 | 1 | 100% | 0 | 1743 | 2422 | 0,72 |
| 1109 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | 1743 | 1 | 100% | 0 | 1743 | 2422 | 0,72 |
| 1110 | S+3_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -17,0 | 1878 | 2 | 95% | 270 | 1130 | 1235 | 0,92 |
| 1112 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | 1743 | 1 | 100% | 0 | 1743 | 2422 | 0,72 |
| 1113 | S+0_c | 2019-1008_21.GEF | 1-paals | SI Ø762/950 | -23,0 | 1743 | 1 | 100% | 0 | 1743 | 2422 | 0,72 |
| 1115 | S+12_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -18,5 | 2093 | 2 | 95% | 270 | 1244 | 1382 | 0,90 |
| 1116 | S+12_c | 2019-1008_21.GEF | 2-paalspoer | SI Ø508/670 | -18,5 | 2093 | 2 | 95% | 270 | 1244 | 1382 | 0,90 |
| 1117 | S+12_c | 02P001595_251.S01.GEF | 2-paalspoer | SI Ø508/670 | -17,0 | 2093 | 2 | 95% | 270 | 1244 | 2032 | 0,61 |
| 1119 | S-3_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -20,0 | 1628 | 1 | 100% | 0 | 1628 | 2503 | 0,65 |
| 1120 | S-3_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -20,0 | 1628 | 1 | 100% | 0 | 1628 | 2503 | 0,65 |
| 1121 | S-3_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -20,0 | 1628 | 1 | 100% | 0 | 1628 | 2503 | 0,65 |
| 1122 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | 1743 | 1 | 100% | 0 | 1743 | 2572 | 0,68 |
| 1124 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | 1743 | 1 | 100% | 0 | 1743 | 2572 | 0,68 |
| 1125 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | 1743 | 1 | 100% | 0 | 1743 | 2572 | 0,68 |
| 1126 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | 1743 | 1 | 100% | 0 | 1743 | 2572 | 0,68 |
| 1127 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | 1743 | 1 | 100% | 0 | 1743 | 2572 | 0,68 |
| 1129 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | 1743 | 1 | 100% | 0 | 1743 | 2572 | 0,68 |
| 1132 | S+0_c | 02P001595_251.S01.GEF | 1-paals | SI Ø610/850 | -21,0 | 1743 | 1 | 100% | 0 | 1743 | 2572 | 0,68 |
| 1134 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1135 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1136 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1138 | S+3_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -22,0 | 1878 | 1 | 100% | 0 | 1878 | 3429 | 0,55 |
| 1139 | S+3_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -22,0 | 1878 | 1 | 100% | 0 | 1878 | 3429 | 0,55 |
| 1140 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1141 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1142 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1143 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1144 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1145 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1146 | S+0_c | 2019-1008_29.GEF | 1-paals | SI Ø610/850 | -20,5 | 1743 | 1 | 100% | 0 | 1743 | 3650 | 0,48 |
| 1149 | S+24_s | 02P001595_283.S02.GEF | 2-paalspoer | SI Ø508/670 | -15,5 | 1971 | 2 | 95% | 270 | 1180 | 2354 | 0,50 |
| 1155 | S+3_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -20,0 | 1878 | 1 | 100% | 0 | 1878 | 4552 | 0,41 |
| 1156 | S+6_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -21,5 | 1910 | 1 | 100% | 0 | 1910 | 5289 | 0,36 |
| 1157 | S+6_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -21,5 | 1910 | 1 | 100% | 0 | 1910 | 5289 | 0,36 |
| 1160 | S+3_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -21,5 | 1878 | 1 | 100% | 0 | 1878 | 5289 | 0,35 |
| 1161 | S+0_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -20,0 | 1743 | 1 | 100% | 0 | 1743 | 4552 | 0,38 |
| 1162 | S+0_c | 02P001595_283.S02.GEF | 1-paals | SI Ø610/850 | -20,0 | 1743 | 1 | 100% | 0 | 1743 | 4552 | 0,38 |
| 1164 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1743 | 1 | 100% | 0 | 1743 | 4481 | 0,39 |
| 1165 | S+6_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -23,0 | 1910 | 1 | 100% | 0 | 1910 | 4409 | 0,43 |
| 1166 | S+6_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -23,0 | 1910 | 1 | 100% | 0 | 1910 | 4409 | 0,43 |
| 1169 | S+3_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -23,0 | 1878 | 1 | 100% | 0 | 1878 | 4409 | 0,43 |
| 1170 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1743 | 1 | 100% | 0 | 1743 | 4481 | 0,39 |
| 1171 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1743 | 1 | 100% | 0 | 1743 | 4481 | 0,39 |
| 1172 | S+3_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1878 | 1 | 100% | 0 | 1878 | 4481 | 0,42 |
| 1173 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1743 | 1 | 100% | 0 | 1743 | 4481 | 0,39 |
| 1174 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1743 | 1 | 100% | 0 | 1743 | 4481 | 0,39 |
| 1175 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1743 | 1 | 100% | 0 | 1743 | 4481 | 0,39 |
| 1176 | S+0_c | 2019-1008_35.GEF | 1-paals | SI Ø610/850 | -21,5 | 1743 | 1 | 100% | 0 | 1743 | 4481 | 0,39 |
| 1178 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | 1878 | 1 | 100% | 0 | 1878 | 3489 | 0,54 |
| 1179 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | 1878 | 1 | 100% | 0 | 1878 | 3489 | 0,54 |
| 1180 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | 1878 | 1 | 100% | 0 | 1878 | 3489 | 0,54 |
| 1181 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | 1878 | 1 | 100% | 0 | 1878 | 3489 | 0,54 |
| 1182 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | 1743 | 1 | 100% | 0 | 1743 | 3888 | 0,45 |
| 1183 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | 1743 | 1 | 100% | 0 | 1743 | 3888 | 0,45 |
| 1185 | S+3_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | 1878 | 1 | 100% | 0 | 1878 | 3489 | 0,54 |
| 1186 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -17,5 | 1743 | 1 | 100% | 0 | 1743 | 3489 | 0,50 |
| 1189 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | 1743 | 1 | 100% | 0 | 1743 | 3888 | 0,45 |
| 1190 | S+0_c | 02P001595_312.S03.GEF | 1-paals | SI Ø610/850 | -15,5 | 1743 | 1 | 100% | 0 | 1743 | 3888 | 0,45 |
| 1191 | S-3_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | 1628 | 1 | 100% | 0 | 1628 | 3923 | 0,42 |
| 1193 | S+9_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,5 | 1955 | 1 | 100% | 0 | 1955 | 4210 | 0,46 |
| 1195 | S+0_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | 1743 | 1 | 100% | 0 | 1743 | 3923 | 0,44 |
| 1197 | S+9_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,5 | 1955 | 1 | 100% | 0 | 1955 | 4210 | 0,46 |
| 1197A | S+9_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,5 | 1955 | 1 | 1 | 0 | 1955 | 4210 | 0,46 |
| 1198 | S+6_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,0 | 1910 | 1 | 100% | 0 | 1910 | 4198 | 0,45 |



| | | | | | | | | | | | | |
|------|-------|------------------|---------|-------------|-------|------|---|------|---|------|------|------|
| 1200 | S+3_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,0 | 1878 | 1 | 100% | 0 | 1878 | 4198 | 0,45 |
| 1201 | S+0_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | 1743 | 1 | 100% | 0 | 1743 | 3923 | 0,44 |
| 1202 | S+0_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -10,5 | 1743 | 1 | 100% | 0 | 1743 | 3923 | 0,44 |
| 1203 | S+3_c | 2019-1008_43.GEF | 1-paals | SI Ø610/850 | -12,0 | 1878 | 1 | 100% | 0 | 1878 | 4198 | 0,45 |

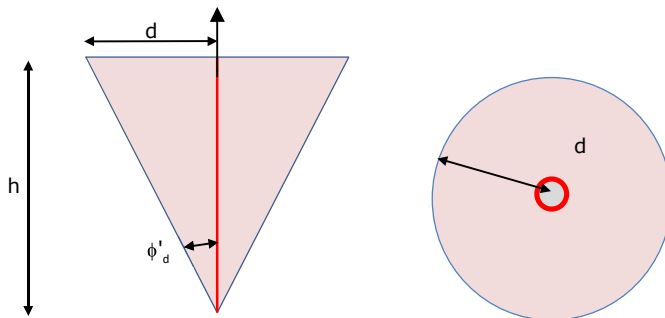
Controle kluitgewicht

De minimaal benodigde lengte van de paal op basis van het kluitgewicht is onderzocht. Het kluitgewicht is het gewicht van de kluit grond die zich door wrijving verzet tegen het uittrekken van de paal met die kluit uit de grond. Zolang dit gewicht groter is dan de trekkracht zal de paal met de kluit grond niet uit de grond getrokken worden.

Kluitgewicht kan een issue zijn voor korte palen die op trek worden belast, waarvan de kleef de trekkracht wel kan weerstaan. Als voorbeeld betreft het zandgronden zonder veel slappe lagen.

De minimale paallengtes op basis van de sonderingen zijn 16 m respectievelijk 12,1 m voor de enkelpaalsfundering en de tweepaalsfundering. De bijbehorende belastingen zijn 1333 kN voor de enkelpaalsfundering en 1540 kN voor de tweepaalsfundering. Voor de tweepaalsfundering is de bijbehorende belasting $2 \times 770 = 1540$ kN.

In deze berekening wordt bepaald wat de minimaal benodigde paallengte is voor voldoende kluitgewicht voor de enkelpaalsfundering belast door 1333 kN en de tweepaalsfundering belast door 1540 kN. Indien de lengte onvoldoende is, dan zal de paal met kluit uit de grond getrokken worden. Zie hieronder.



Figuur. Zijaanzicht (links) en bovenaanzicht (rechts) van de kluit grond

Algemene gegevens

| | | | |
|-----------------------------|-----------------|------|-------------------|
| Volumiek gewicht grond | | 18 | kN/m ³ |
| Volumiek gewicht water | | 10 | kN/m ³ |
| Veiligheidsfactor | $\gamma_g =$ | 0,9 | - |
| Hoek van inwendige wrijving | $\phi' =$ | 27,5 | ° |
| Veiligheidsfactor | $\gamma_\psi =$ | 1,25 | - |

Berekening kluitgewicht voor 1 paal

| | | | |
|------------------------|---|--------|----------------|
| Diepte minimaal | $h =$ | 10,578 | m |
| Radius kegel op mv. | $d = L \times (\tan \alpha / \gamma) =$ | 4,41 | m |
| Grondoppervlak kegel | $A = \pi d^2 =$ | 61,0 | m ² |
| Inhoud kegel | $I_{kluit} = 1/3Gh =$ | 215,0 | m ³ |
| Gewicht grond | $F_{gr} =$ | 3869 | kN |
| Opwaartse kracht water | $F_w =$ | 2150 | kN |
| Rekenwaarde | $F_{r,d} = 0,9F_{gr} - F_w =$ | 1333 | kN |

Uit de berekening van het kluitgewicht bij de enkelpaalsfundering blijkt dat de lengte van de paal niet onder de 10,6 m mag komen bij de belasting van 1333 kN.

Berekening kluitgewicht voor 2 palen

| | | | |
|-----------------|-------|------|---|
| Diepte minimaal | $h =$ | 11,1 | m |
|-----------------|-------|------|---|

| | | |
|------------------------|---|----------------------|
| Radius kegel op mv. | $d = L \times (\tan \alpha / \gamma) =$ | 4,62 m |
| Grondoppervlak kegel | $A = \pi d^2 =$ | 67,1 m ² |
| Inhoud kegel | $I_{kluit} = 1/3Gh =$ | 248,4 m ³ |
| Gewicht grond | $F_{gr} =$ | 4471 kN |
| Opwaartse kracht water | $F_w =$ | 2484 kN |
| Rekenwaarde | $F_{r,d} = 0,9F_{gr} - F_w =$ | 1540 kN |

Uit de berekening van het kluitgewicht bij de tweepaalsfundering blijkt dat de lengte van de paal niet onder de 11,1 m mag komen bij de belasting van 1540 kN. Hier is conservatief de tweepaalspoer als een enkelpaalspoer beschouwd, het tussenoppervlak van de wig is verwaarloosd.

De minimale paallengtes op basis van de sonderingen zijn 16 m respectievelijk 12,1 m voor de enkelpaalsfundering en de tweepaalsfundering. Er is voldoende kluitgewicht. In het UO mag bij eventuele optimalisatie de lengte van de paal niet kleiner worden dan de hierboven berekende minimale paallengtes (10,6 en 11,1 m), tenzij de belasting kleiner is dan de aangehouden waarden van 1333 kN respectievelijk 1540 kN.

De maximale belasting voor de éénpaalsfundering is nooit groter dan 1495 kN (met paallengte 18,7 m op basis van sonderingen en een daarbij gemobiliseerd gewicht 7363 kN > 1495 kN). Deze lengte (bij die specifieke belasting) mag niet kleiner worden dan 11 m want dan wordt de trekbelasting 1495 kN meer dan het kluitgewicht.

De maximale belasting voor de tweepaalsfundering is nooit groter dan 2 palen x 859 = 1718 kN (met paallengte 22,8 m op basis van sondering en een daarbij gemobiliseerd gewicht 13346 kN > 1718). Deze lengte (bij die specifieke belasting) mag niet kleiner worden dan 11,5 m want dan wordt de trekbelasting 1718 kN meer dan het kluitgewicht.

Palen die een lage belasting hebben en dus een korte paaldiepte L1 hebben op basis van analyse sondering (en een nog lagere minimum paallengte L2 op basis van analyse kluitgewicht) hoeven we niet te verlengen tot minimale paaldiepte L4 (met L4 > L1) op basis van analyse kluitgewicht bij palen die een hoge belasting hebben (en een nog hogere paallengte L3 op basis van analyse sondering). In het uitvoeringsontwerp (UO) moet kluitgewicht worden gecontroleerd indien op basis van sonderingen wordt besloten de paallengte uit het definitief ontwerp (DO) te verlagen. Hierbij moet ook worden gelet op de minimale paallengte van 7 m of 13,5 m de middellijn volgens 7.6.3.3. van NEN-EN 1997-1.



APPENDIX D

Uitvoer TS paalfunderingen

ALGEMENE GEGEVENS

Project : ZW0380 Funderingen
 Onderdeel : RLL-TBG380
 Datum : 27-03-2021
 Bestand : P:\EANL_Projects\10124719 - TenneT Engineering
 ZW380 kV Oost\2 Content\007 DO
 vakwerkmasten\TS Paalfunderingen\ZW0380
 steunmast DO.pvw
 Berekeningstype : Verticaal belaste paal
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Toegepaste normen volgens Eurocode met Nederlandse NB

| | | | |
|-------------|--------------------|------------|---------|
| Geotechniek | EN 1997-1:2004 | AC:2009 | |
| | NEN-EN 1997-1:2005 | C1+A1:2013 | NB:2016 |
| | NEN 9997-1:2016 | C2:2017 | |

BODEMPROFIELGEGEVENS: 19-1008_1

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)
 Hoogte maaiveld [m] : 2.12 Grondwaterstand [m] : 1.12

| Laag | Van [m] | Tot [m] | Omschrijving | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1 | 2.12 | 0.47 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 2 | 0.47 | -0.23 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 3 | -0.23 | -1.33 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 4 | -1.33 | -7.83 | Klei - Organisch - Matig | 1.0 | 50.0 | | |
| 5 | -7.83 | -12.63 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 6 | -12.63 | -17.12 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 7 | -17.12 | -19.80 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 8 | -19.80 | -21.20 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 9 | -21.20 | -32.70 | Zand - Schoon - Vast | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 19-1008_6

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)
 Hoogte maaiveld [m] : 11.00 Grondwaterstand [m] : 10.00

| Laag | Van [m] | Tot [m] | Omschrijving | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1 | 11.00 | 8.25 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 2 | 8.25 | 7.45 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 3 | 7.45 | 3.15 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 4 | 3.15 | 1.15 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 5 | 1.15 | -3.95 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 6 | -3.95 | -4.25 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 7 | -4.25 | -5.35 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 8 | -5.35 | -13.16 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 9 | -13.16 | -16.89 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 10 | -16.89 | -18.28 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 11 | -18.28 | -23.93 | Zand - Schoon - Vast | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 166.S01

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)
 Hoogte maaiveld [m] : 3.45 Grondwaterstand [m] : 2.45

| Laag | Van [m] | Tot [m] | Omschrijving | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1 | 3.45 | 1.40 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 2 | 1.40 | 0.60 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 3 | 0.60 | -1.60 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 4 | -1.60 | -3.40 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 5 | -3.40 | -3.60 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 6 | -3.60 | -4.90 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 7 | -4.90 | -11.10 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 8 | -11.10 | -11.70 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 9 | -11.70 | -13.21 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 10 | -13.21 | -21.31 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 11 | -21.31 | -22.66 | Zand - Schoon - Vast | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 19-1008_11

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)
 Hoogte maaiveld [m] : 0.62 Grondwaterstand [m] : -0.38

| Laag | Van [m] | Tot [m] | Omschrijving | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1 | 0.62 | -0.83 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 2 | -0.83 | -2.83 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 3 | -2.83 | -4.13 | Klei - Schoon - Vast | 1.0 | 50.0 | | |
| 4 | -4.13 | -7.43 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 5 | -7.43 | -11.82 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 6 | -11.82 | -12.64 | Klei - Schoon - Matig | 1.0 | 50.0 | | |
| 7 | -12.64 | -17.92 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 8 | -17.92 | -22.71 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 9 | -22.71 | -25.46 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 10 | -25.46 | -29.39 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 11 | -29.39 | -32.78 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 12 | -32.78 | -33.83 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 13 | -33.83 | -34.28 | Zand - Schoon - Los | 1.0 | 100.0 | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

BODEMPROFIELGEGEVENS: 19-1008 12

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | OCR | Aandeel pos. kleeft [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|-----------------------------|-----|-------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | |
| 1 | 3.57 | 1.12 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 2 | 1.12 | 0.72 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 3 | 0.72 | -3.28 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 4 | -3.28 | -3.68 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 5 | -3.68 | -6.38 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 6 | -6.38 | -7.58 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 7 | -7.58 | -8.48 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 8 | -8.48 | -19.19 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 9 | -19.19 | -25.26 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 10 | -25.26 | -27.97 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 11 | -27.97 | -30.88 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 12 | -30.88 | -31.50 | Zand - Schoon - Los | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 19-1008 17

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | OCR | Aandeel pos. kleeft [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|------------------------------|-----|-------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | |
| 1 | 0.20 | -0.85 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 2 | -0.85 | -2.95 | Klei - Schoon - Matig | 1.0 | 50.0 | | |
| 3 | -2.95 | -4.05 | Klei - Schoon - Vast | 1.0 | 50.0 | | |
| 4 | -4.05 | -4.95 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 5 | -4.95 | -5.15 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 6 | -5.15 | -6.65 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 7 | -6.65 | -7.25 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 8 | -7.25 | -9.65 | Klei - Schoon - Matig | 1.0 | 50.0 | | |
| 9 | -9.65 | -10.05 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 10 | -10.05 | -10.25 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 11 | -10.25 | -11.55 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 12 | -11.55 | -12.85 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 13 | -12.85 | -14.75 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 14 | -14.75 | -17.25 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 15 | -17.25 | -18.55 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 16 | -18.55 | -20.64 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 17 | -20.64 | -21.14 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 18 | -21.14 | -21.54 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 19 | -21.54 | -24.23 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 20 | -24.23 | -28.91 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 21 | -28.91 | -29.73 | Klei - Organisch - Matig | 1.0 | 50.0 | | |
| 22 | -29.73 | -30.67 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 23 | -30.67 | -34.80 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 19-1008 20

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | OCR | Aandeel pos. kleeft [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|------------------------------|-----|-------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | |
| 1 | -0.03 | -1.28 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 2 | -1.28 | -3.18 | Klei - Zwak zandig - Slap | 1.0 | 50.0 | | |
| 3 | -3.18 | -4.88 | Klei - Schoon - Matig | 1.0 | 50.0 | | |
| 4 | -4.88 | -9.78 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 5 | -9.78 | -10.68 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 6 | -10.68 | -11.38 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 7 | -11.38 | -13.58 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 8 | -13.58 | -14.38 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 9 | -14.38 | -17.38 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 10 | -17.38 | -19.68 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 11 | -19.68 | -20.48 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 12 | -20.48 | -23.07 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 13 | -23.07 | -30.25 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 14 | -30.25 | -31.84 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 15 | -31.84 | -32.83 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 16 | -32.83 | -34.29 | Klei - Schoon - Vast | 1.0 | 50.0 | | |
| 17 | -34.29 | -35.23 | Klei - Schoon - Vast | 1.0 | 50.0 | | |

BODEMPROFIELGEGEVENS: 19-1008 21

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | OCR | Aandeel pos. kleeft [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|------------------------------|-----|-------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | |
| 1 | 1.78 | -1.17 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 2 | -1.17 | -4.17 | Klei - Schoon - Matig | 1.0 | 50.0 | | |
| 3 | -4.17 | -8.26 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 4 | -8.26 | -12.28 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 5 | -12.28 | -12.98 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 6 | -12.98 | -14.68 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 7 | -14.68 | -16.58 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 8 | -16.58 | -17.88 | Klei - Schoon - Matig | 1.0 | 50.0 | | |
| 9 | -17.88 | -18.88 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 10 | -18.88 | -30.48 | Klei - Schoon - Matig | 1.0 | 50.0 | | |
| 11 | -30.48 | -33.19 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

BODEMPROFIELGEGEVENS: 251.S01

Alle niveaus/hogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | Grondwaterstand [m] | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|-------------------------------|---------------------|-----|------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | | |
| 1 | -1.05 | -3.60 | Klei - Schoon - Matig | -2.05 | 1.0 | 50.0 | | |
| 2 | -3.60 | -7.80 | Zand - Zwak siltig - Kleilig | | 1.0 | 100.0 | | |
| 3 | -7.80 | -9.10 | Klei - Organisch - Matig | | 1.0 | 50.0 | | |
| 4 | -9.10 | -14.80 | Zand - Sterk siltig - Kleilig | | 1.0 | 100.0 | | |
| 5 | -14.80 | -15.40 | Klei - Schoon - Matig | | 1.0 | 50.0 | | |
| 6 | -15.40 | -18.31 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 7 | -18.31 | -19.21 | Leem - Zwak zandig - Vast | | 1.0 | 50.0 | | |
| 8 | -19.21 | -20.23 | Zand - Sterk siltig - Kleilig | | 1.0 | 100.0 | | |
| 9 | -20.23 | -26.29 | Klei - Zwak zandig - Vast | | 1.0 | 50.0 | | |
| 10 | -26.29 | -28.61 | Zand - Schoon - Vast | | 1.0 | 100.0 | | |
| 11 | -28.61 | -30.30 | Zand - Schoon - Los | | 1.0 | 100.0 | | |
| 12 | -30.30 | -33.03 | Klei - Zwak zandig - Matig | | 1.0 | 50.0 | | |
| 13 | -33.03 | -37.54 | Zand - Sterk siltig - Kleilig | | 1.0 | 100.0 | | |
| 14 | -37.54 | -38.23 | Klei - Schoon - Vast | | 1.0 | 50.0 | | |
| 15 | -38.23 | -40.24 | Zand - Sterk siltig - Kleilig | | 1.0 | 100.0 | | |
| 16 | -40.24 | -40.88 | Zand - Schoon - Los | | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 19-1008_29

Alle niveaus/hogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | Grondwaterstand [m] | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|-------------------------------|---------------------|-----|------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | | |
| 1 | 0.79 | -2.26 | Zand - Sterk siltig - Kleilig | -0.21 | 1.0 | 100.0 | | |
| 2 | -2.26 | -11.15 | Zand - Zwak siltig - Kleilig | | 1.0 | 100.0 | | |
| 3 | -11.15 | -12.15 | Klei - Organisch - Matig | | 1.0 | 50.0 | | |
| 4 | -12.15 | -12.85 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 5 | -12.85 | -15.55 | Klei - Zwak zandig - Matig | | 1.0 | 50.0 | | |
| 6 | -15.55 | -15.75 | Zand - Schoon - Vast | | 1.0 | 100.0 | | |
| 7 | -15.75 | -17.65 | Klei - Zwak zandig - Matig | | 1.0 | 50.0 | | |
| 8 | -17.65 | -18.98 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 9 | -18.98 | -19.38 | Leem - Zwak zandig - Vast | | 1.0 | 50.0 | | |
| 10 | -19.38 | -22.38 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 11 | -22.38 | -23.98 | Klei - Zwak zandig - Matig | | 1.0 | 50.0 | | |
| 12 | -23.98 | -24.18 | Zand - Sterk siltig - Kleilig | | 1.0 | 100.0 | | |
| 13 | -24.18 | -29.47 | Klei - Zwak zandig - Matig | | 1.0 | 50.0 | | |
| 14 | -29.47 | -30.99 | Zand - Sterk siltig - Kleilig | | 1.0 | 100.0 | | |
| 15 | -30.99 | -34.29 | Leem - Zwak zandig - Vast | | 1.0 | 50.0 | | |

BODEMPROFIELGEGEVENS: 283.S02

Alle niveaus/hogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | Grondwaterstand [m] | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|---------------------------|---------------------|-----|------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | | |
| 1 | 0.17 | -1.58 | Klei - Zwak zandig - Slap | -0.83 | 1.0 | 0.0 | | |
| 2 | -1.58 | -15.18 | Zand - Schoon - Los | | 1.0 | 100.0 | | |
| 3 | -15.18 | -26.29 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 4 | -26.29 | -28.61 | Klei - Schoon - Vast | | 1.0 | 50.0 | | |
| 5 | -28.61 | -30.60 | Klei - Schoon - Matig | | 1.0 | 50.0 | | |
| 6 | -30.60 | -32.29 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 19-1008_35

Alle niveaus/hogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | Grondwaterstand [m] | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|----------------------------|---------------------|-----|------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | | |
| 1 | 0.92 | -0.23 | Klei - Zwak zandig - Matig | -0.08 | 1.0 | 50.0 | | |
| 2 | -0.23 | -19.34 | Zand - Schoon - Los | | 1.0 | 100.0 | | |
| 3 | -19.34 | -25.33 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 4 | -25.33 | -25.93 | Leem - Zwak zandig - Vast | | 1.0 | 50.0 | | |
| 5 | -25.93 | -28.72 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 6 | -28.72 | -30.64 | Zand - Schoon - Vast | | 1.0 | 100.0 | | |
| 7 | -30.64 | -34.25 | Klei - Schoon - Matig | | 1.0 | 50.0 | | |

BODEMPROFIELGEGEVENS: 312.S03

Alle niveaus/hogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Hoogte maaiveld [m] | | Omschrijving | Grondwaterstand [m] | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------------------|---------|------------------------------|---------------------|-----|------------------------|------------|---------------|
| | Van [m] | Tot [m] | | | | | | |
| 1 | 3.78 | -3.57 | Zand - Schoon - Los | 2.78 | 1.0 | 100.0 | | |
| 2 | -3.57 | -4.86 | Zand - Schoon - Matig | | 1.0 | 100.0 | | |
| 3 | -4.86 | -6.86 | Zand - Schoon - Los | | 1.0 | 100.0 | | |
| 4 | -6.86 | -7.85 | Klei - Zwak zandig - Vast | | 1.0 | 50.0 | | |
| 5 | -7.85 | -20.13 | Zand - Zwak siltig - Kleilig | | 1.0 | 100.0 | | |
| 6 | -20.13 | -20.47 | Klei - Organisch - Slap | | 1.0 | 50.0 | | |
| 7 | -20.47 | -27.08 | Zand - Zwak siltig - Kleilig | | 1.0 | 100.0 | | |
| 8 | -27.08 | -31.92 | Klei - Zwak zandig - Matig | | 1.0 | 50.0 | | |
| 9 | -31.92 | -31.97 | Zand - Schoon - Vast | | 1.0 | 100.0 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

BODEMPROFIELGEGEVENS: 19-1008_43

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Van [m] | Tot [m] | Omschrijving | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1 | 9.88 | 4.60 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 2 | 4.60 | 4.00 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 3 | 4.00 | 3.40 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 4 | 3.40 | 3.00 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 5 | 3.00 | -6.39 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 6 | -6.39 | -10.29 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 7 | -10.29 | -12.28 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 8 | -12.28 | -14.98 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 9 | -14.98 | -16.30 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 10 | -16.30 | -18.73 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 11 | -18.73 | -21.25 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 12 | -21.25 | -25.16 | Zand - Schoon - Matig | 1.0 | 100.0 | | |

BODEMPROFIELGEGEVENS: 328.S02

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Van [m] | Tot [m] | Omschrijving | OCR | Aandeel pos. kleef [%] | α_s | d_{50} [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1 | 10.17 | 5.82 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 2 | 5.82 | -0.06 | Zand - Schoon - Vast | 1.0 | 100.0 | | |
| 3 | -0.06 | -1.16 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 4 | -1.16 | -1.56 | Klei - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 5 | -1.56 | -4.56 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 6 | -4.56 | -5.39 | Klei - Zwak zandig - Matig | 1.0 | 50.0 | | |
| 7 | -5.39 | -15.50 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |
| 8 | -15.50 | -16.08 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 9 | -16.08 | -17.81 | Zand - Schoon - Matig | 1.0 | 100.0 | | |
| 10 | -17.81 | -18.39 | Leem - Zwak zandig - Vast | 1.0 | 50.0 | | |
| 11 | -18.39 | -27.62 | Zand - Zwak siltig - Kleiig | 1.0 | 100.0 | | |
| 12 | -27.62 | -28.07 | Zand - Schoon - Los | 1.0 | 100.0 | | |
| 13 | -28.07 | -28.89 | Zand - Sterk siltig - Kleiig | 1.0 | 100.0 | | |

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_1

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

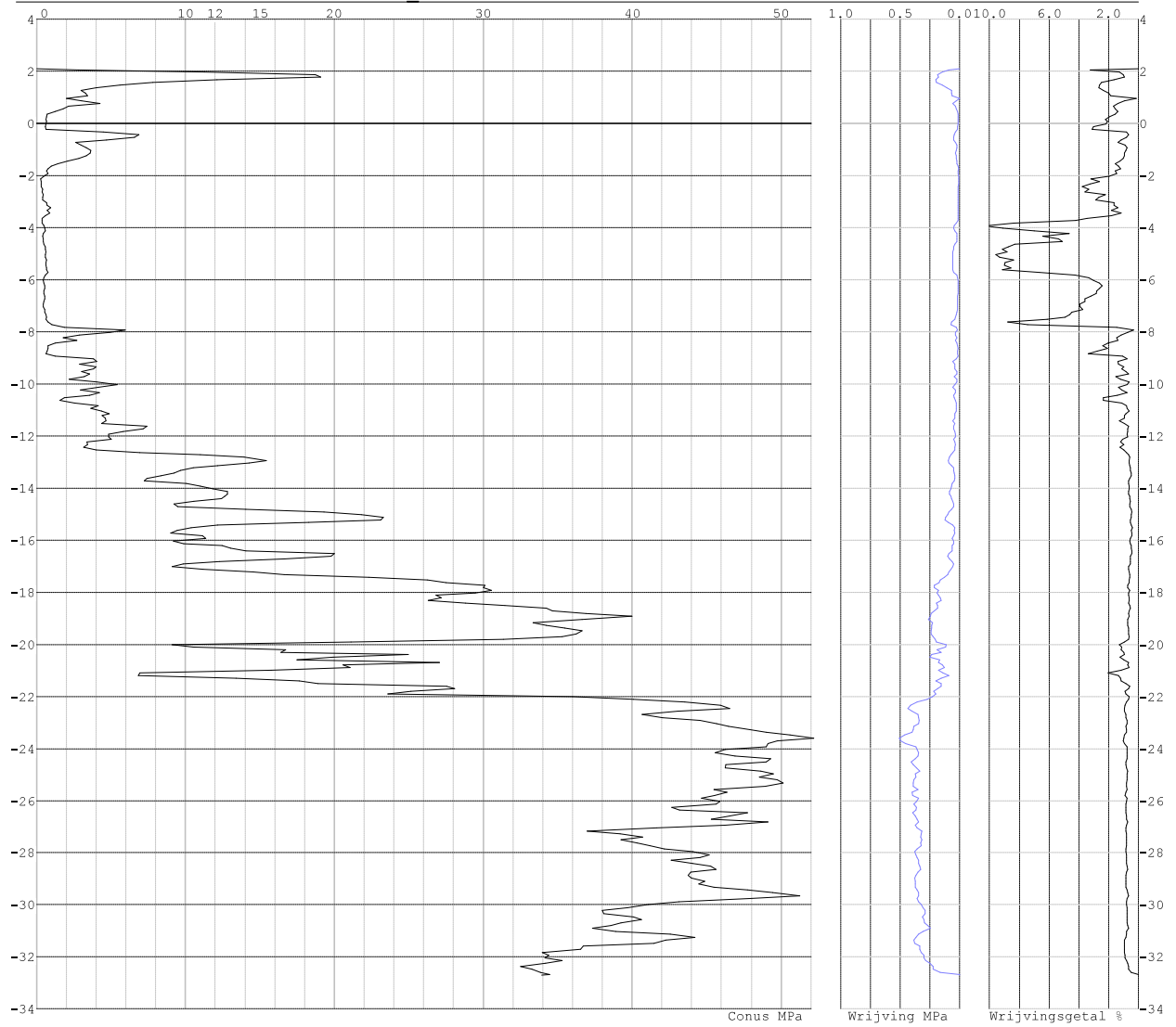
Hoogte maaiveld [m] : 2.12 Bodemprofiel: 19-1008_1

Traject negatieve kleef : 2.12 tot -4.90 [m]

Traject positieve kleef : -7.30 tot -32.70 [m]

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS GRAFIEK: 19-1008 1

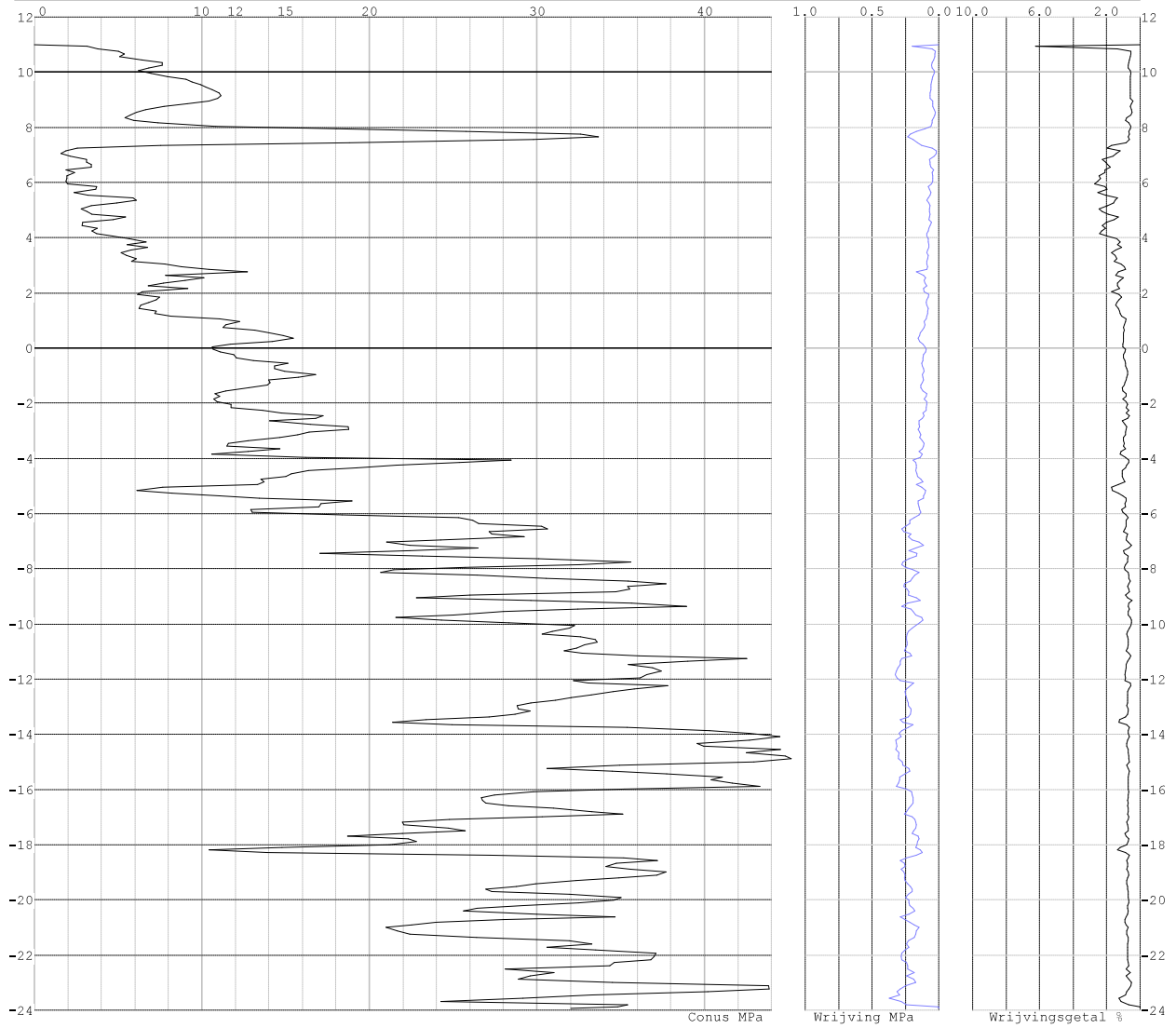


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_6

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 11.00 Bodemprofiel: 19-1008_6
Traject negatieve kleeft : 11.00 tot 6.90 [m]
Traject positieve kleeft : 4.20 tot -23.93 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_6

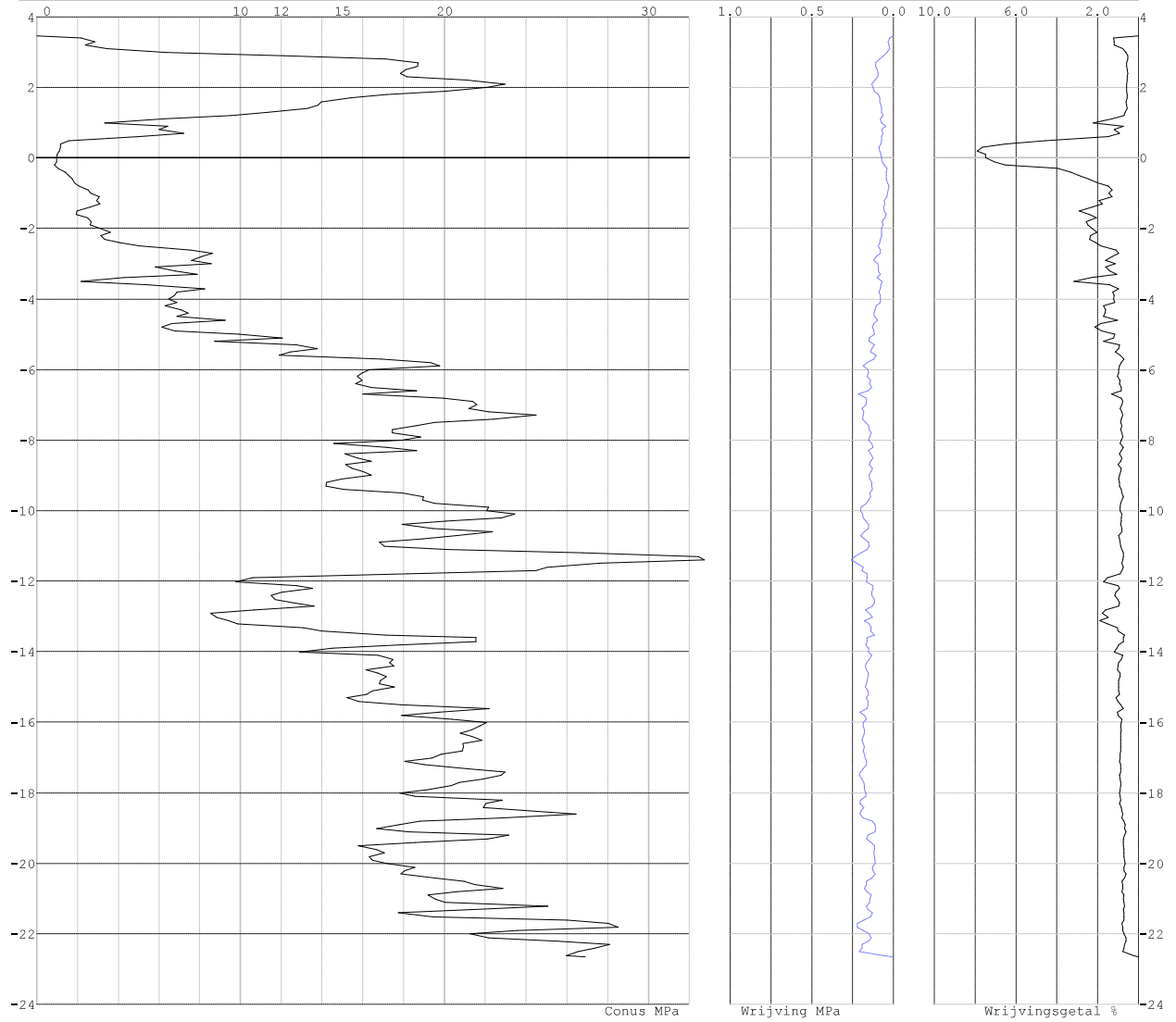


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 166.S01

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 3.45 Bodemprofiel: 166.S01
Traject negatieve kleeft : 3.45 tot -0.30 [m]
Traject positieve kleeft : -1.30 tot -22.66 [m]

SONDERINGSGEGEVENS GRAFIEK: 166.S01

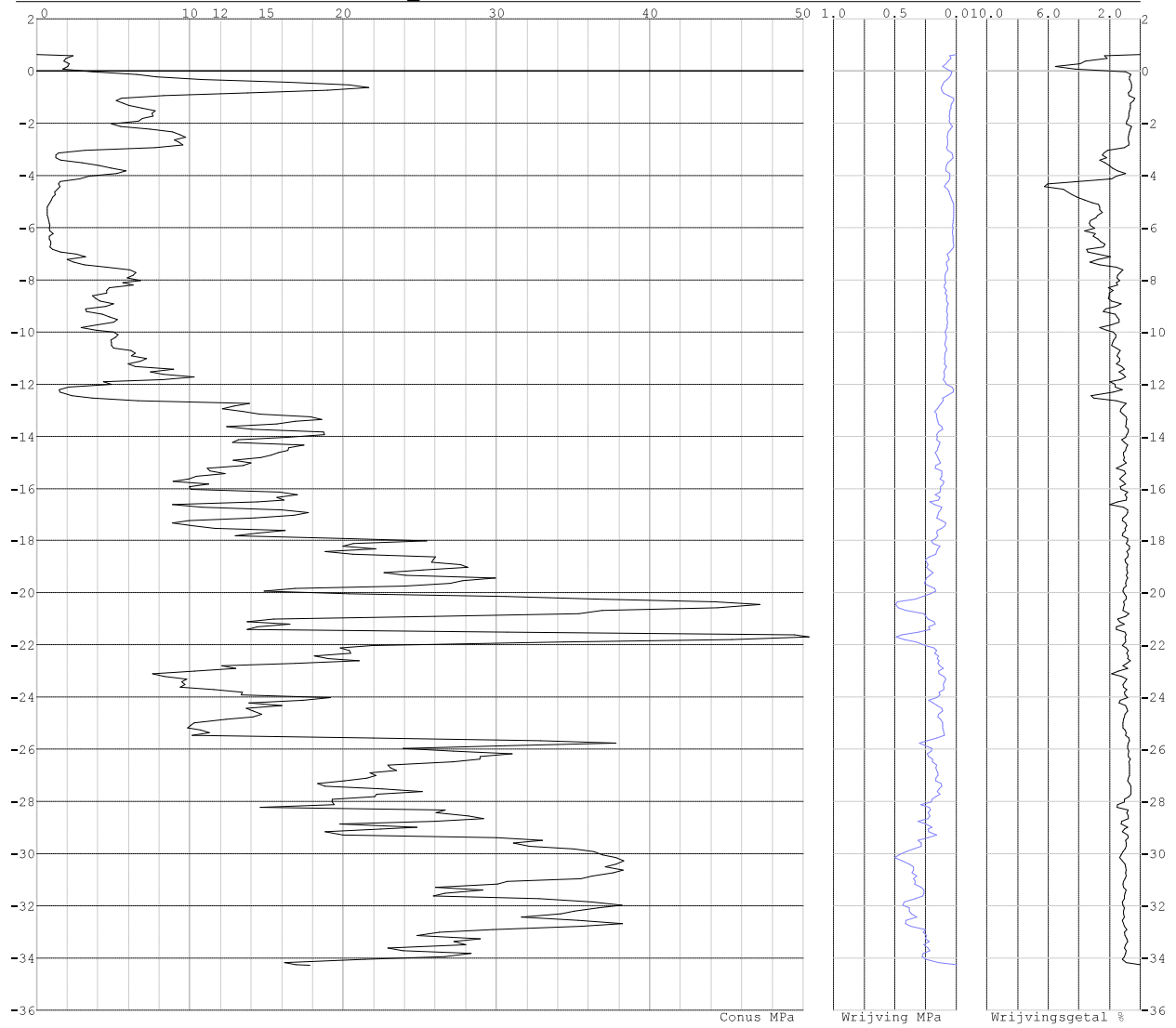


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_11

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 0.62 Bodemprofiel: 19-1008_11
Traject negatieve kleef : 0.62 tot -5.20 [m]
Traject positieve kleef : -6.80 tot -34.28 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_11

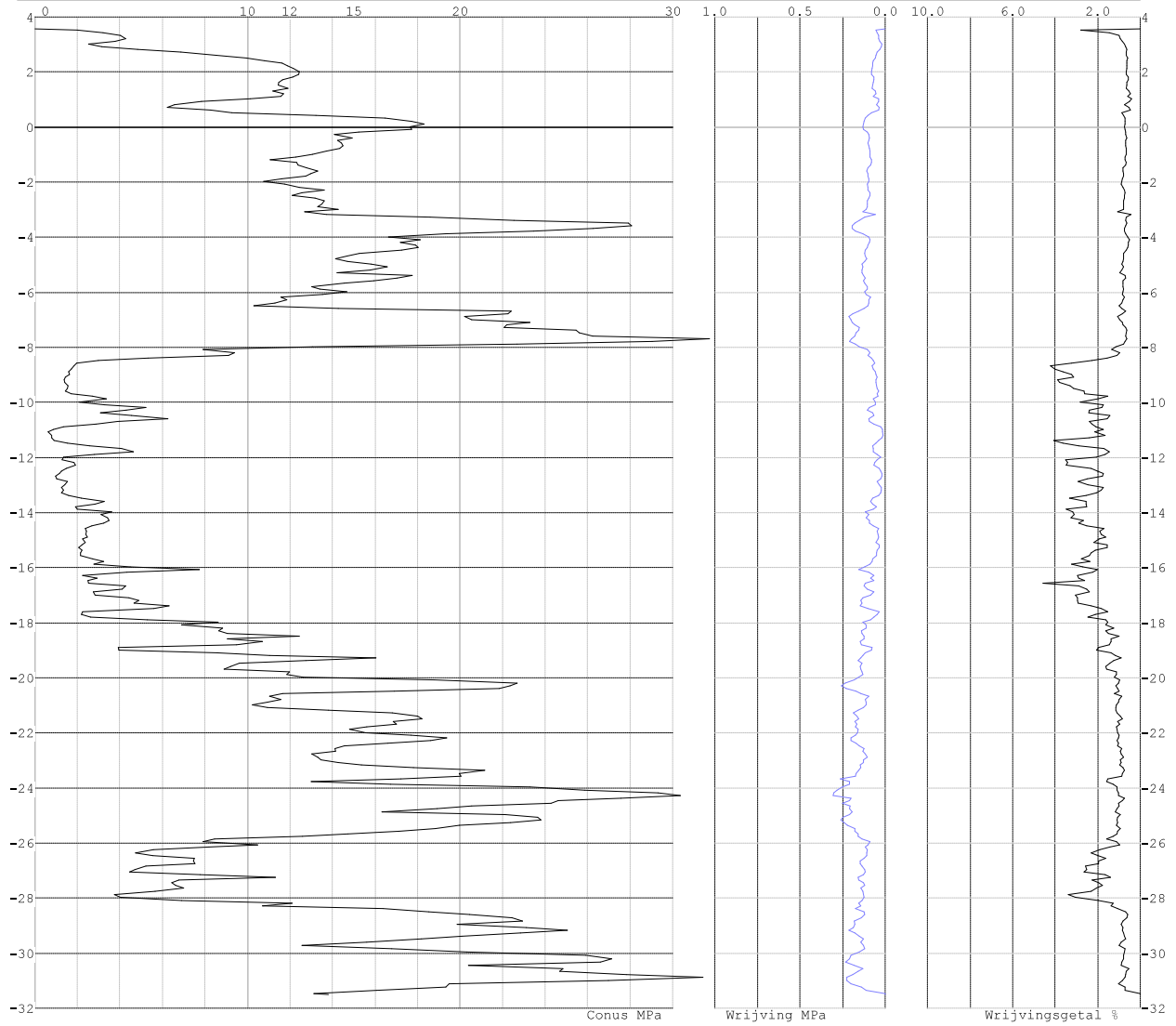


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_12

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 3.57 Bodemprofiel: 19-1008_12
Traject negatieve kleeft : 3.57 tot 3.00 [m]
Traject positieve kleeft : 2.80 tot -31.50 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_12

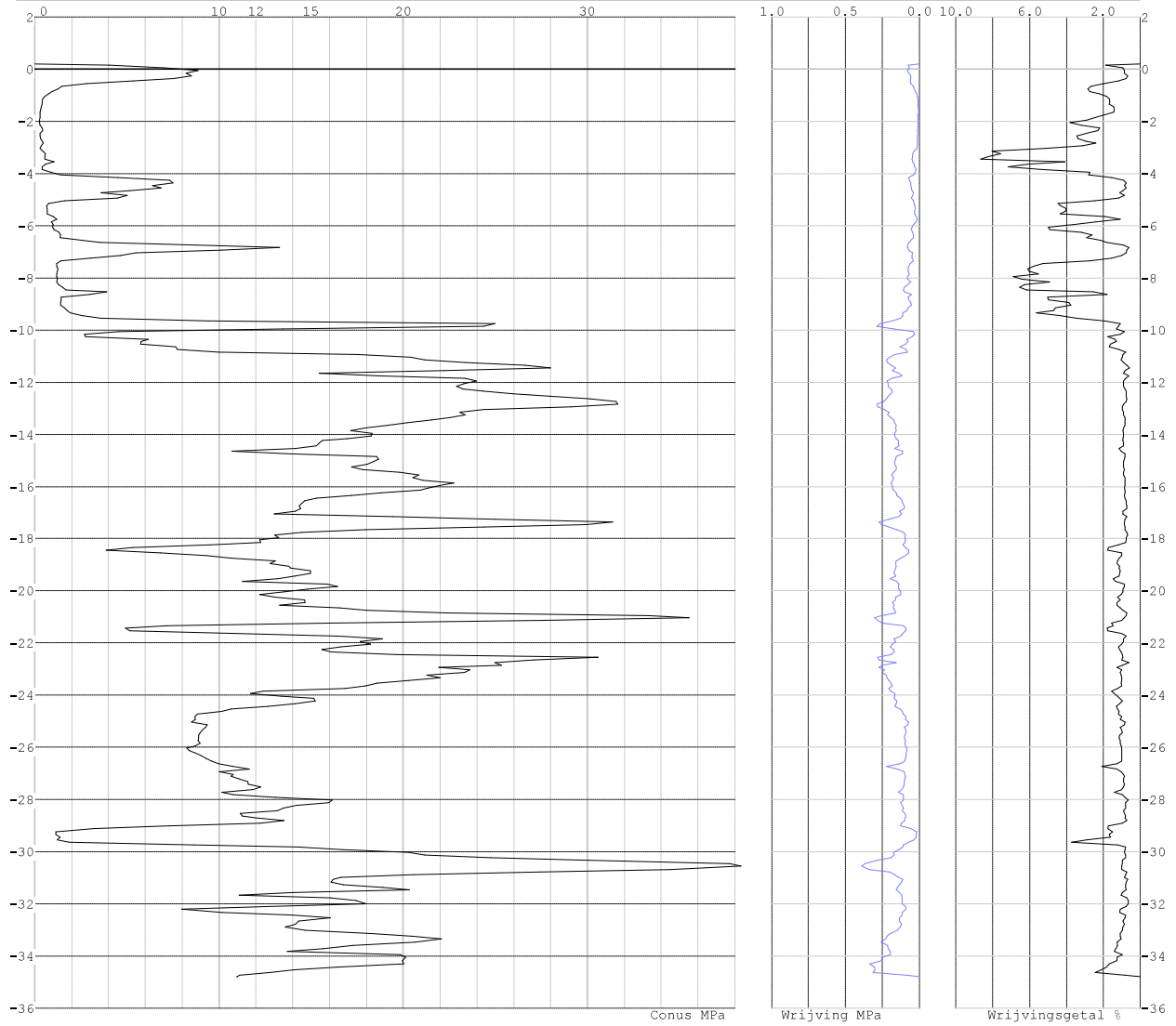


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_17

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 0.20 Bodemprofiel: 19-1008_17
Traject negatieve kleeft : 0.20 tot -7.50 [m]
Traject positieve kleeft : -10.30 tot -34.80 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_17

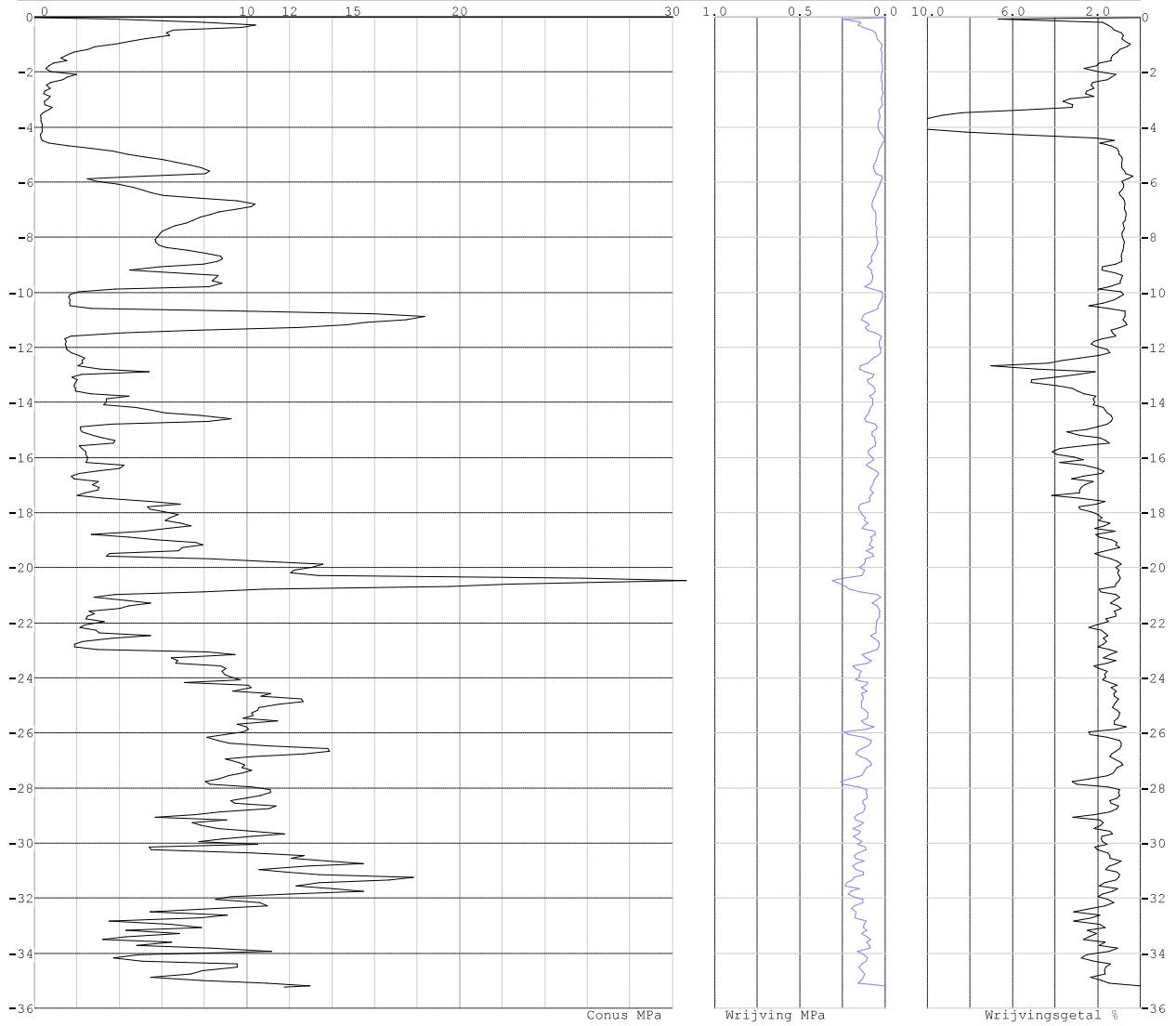


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_20

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : -0.03 Bodemprofiel: 19-1008_20
Traject negatieve kleeft : -0.03 tot -3.20 [m]
Traject positieve kleeft : -4.50 tot -35.23 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_20

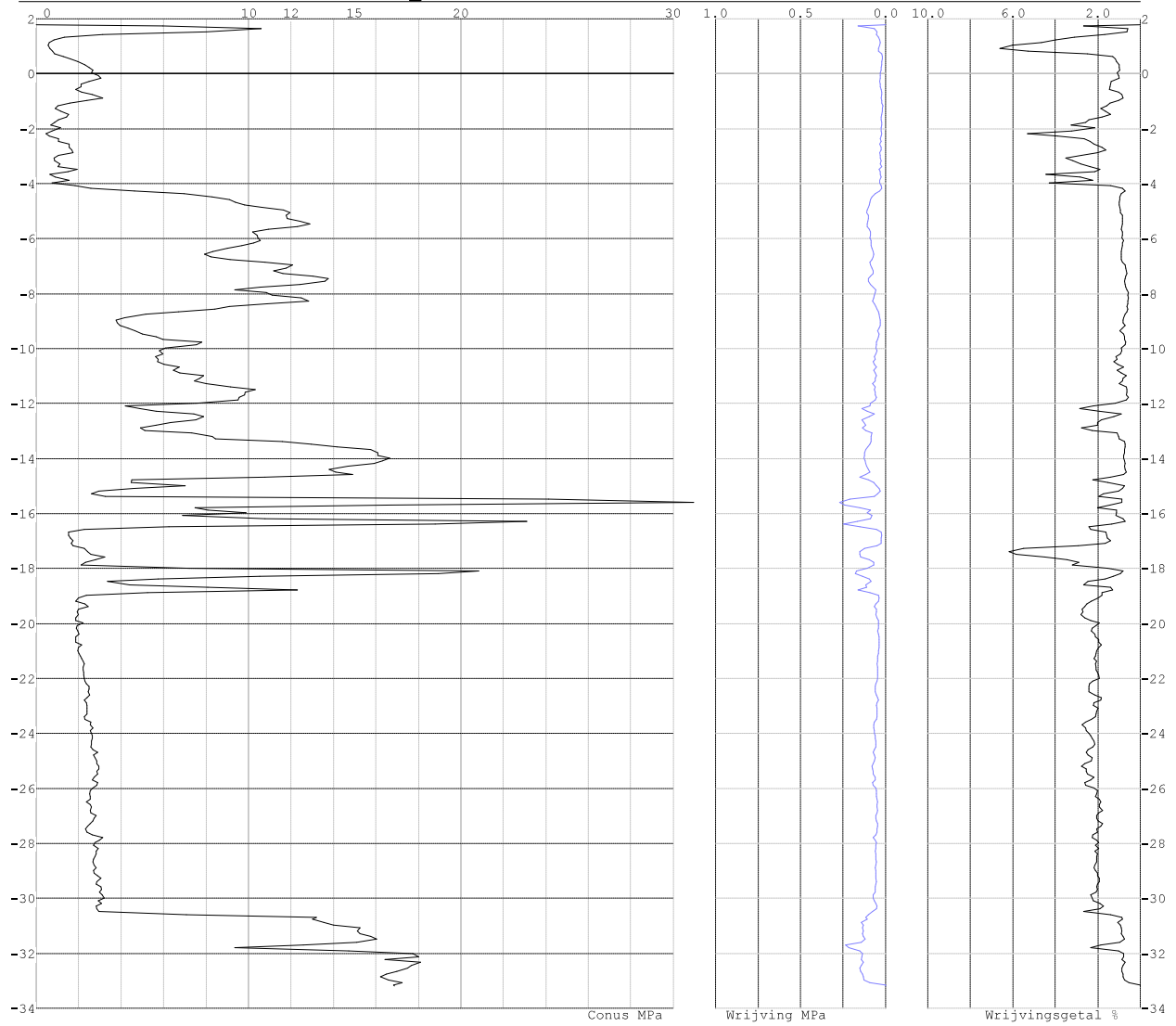


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_21

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 1.78 Bodemprofiel: 19-1008_21
Traject negatieve kleeft : 1.78 tot -4.10 [m]
Traject positieve kleeft : -4.50 tot -33.19 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_21

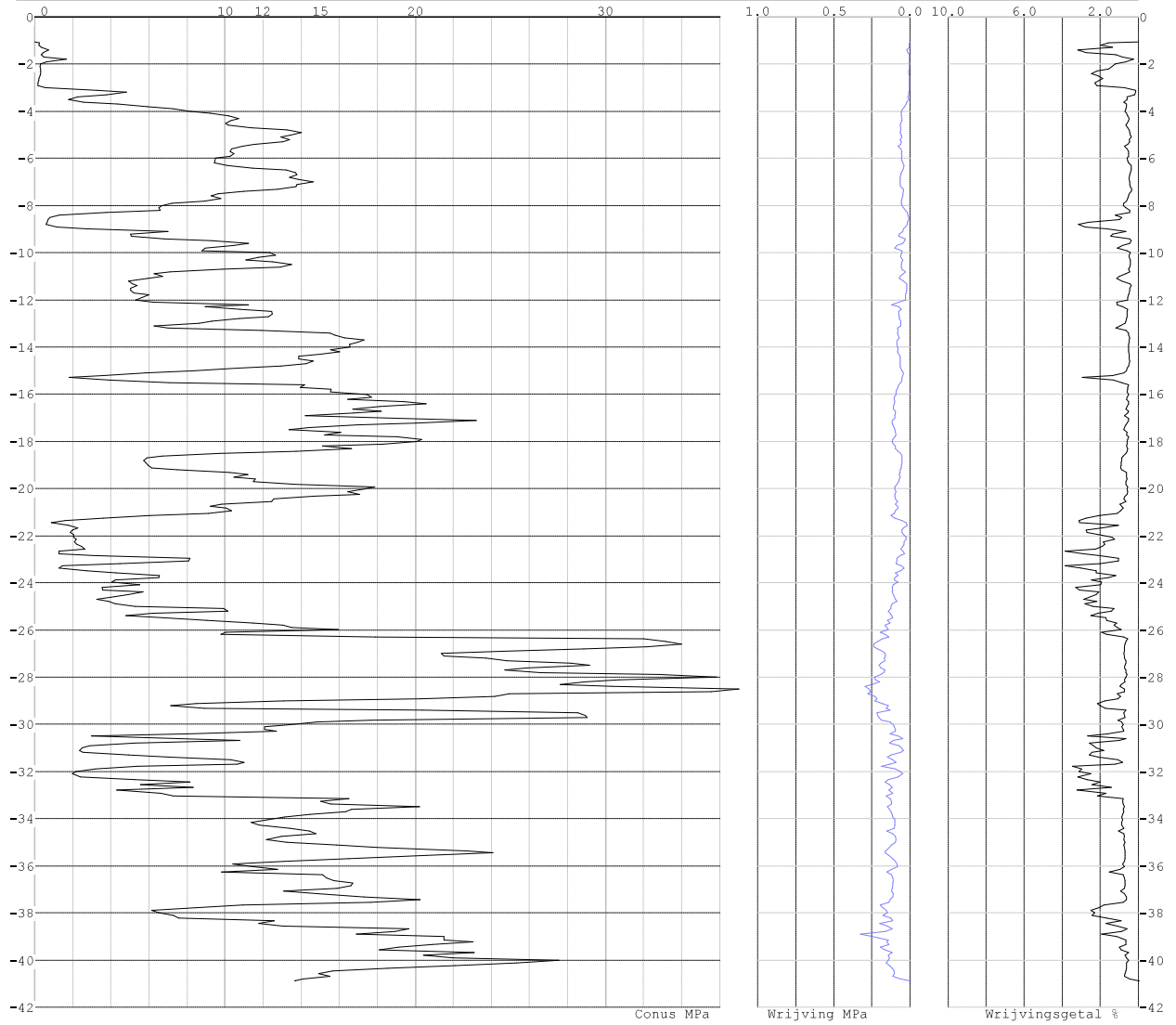


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 251.S01

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : -1.05 Bodemprofiel: 251.S01
Traject negatieve kleeft : -1.05 tot -2.80 [m]
Traject positieve kleeft : -3.30 tot -40.88 [m]

SONDERINGSGEGEVENS GRAFIEK: 251.S01

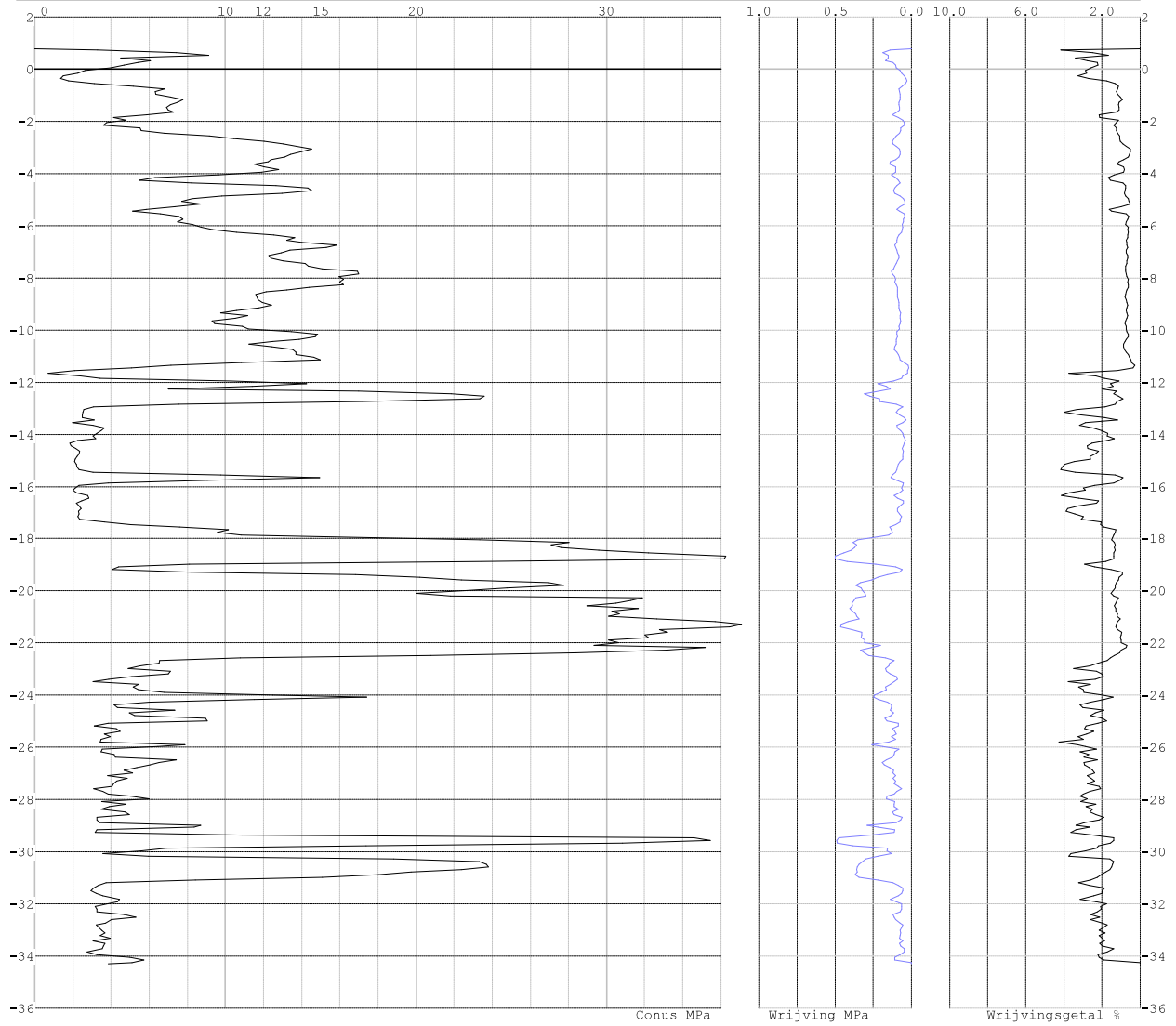


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_29

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 0.79 Bodemprofiel: 19-1008_29
Traject negatieve kleeft : 0.79 tot -0.50 [m]
Traject positieve kleeft : -0.70 tot -34.29 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_29

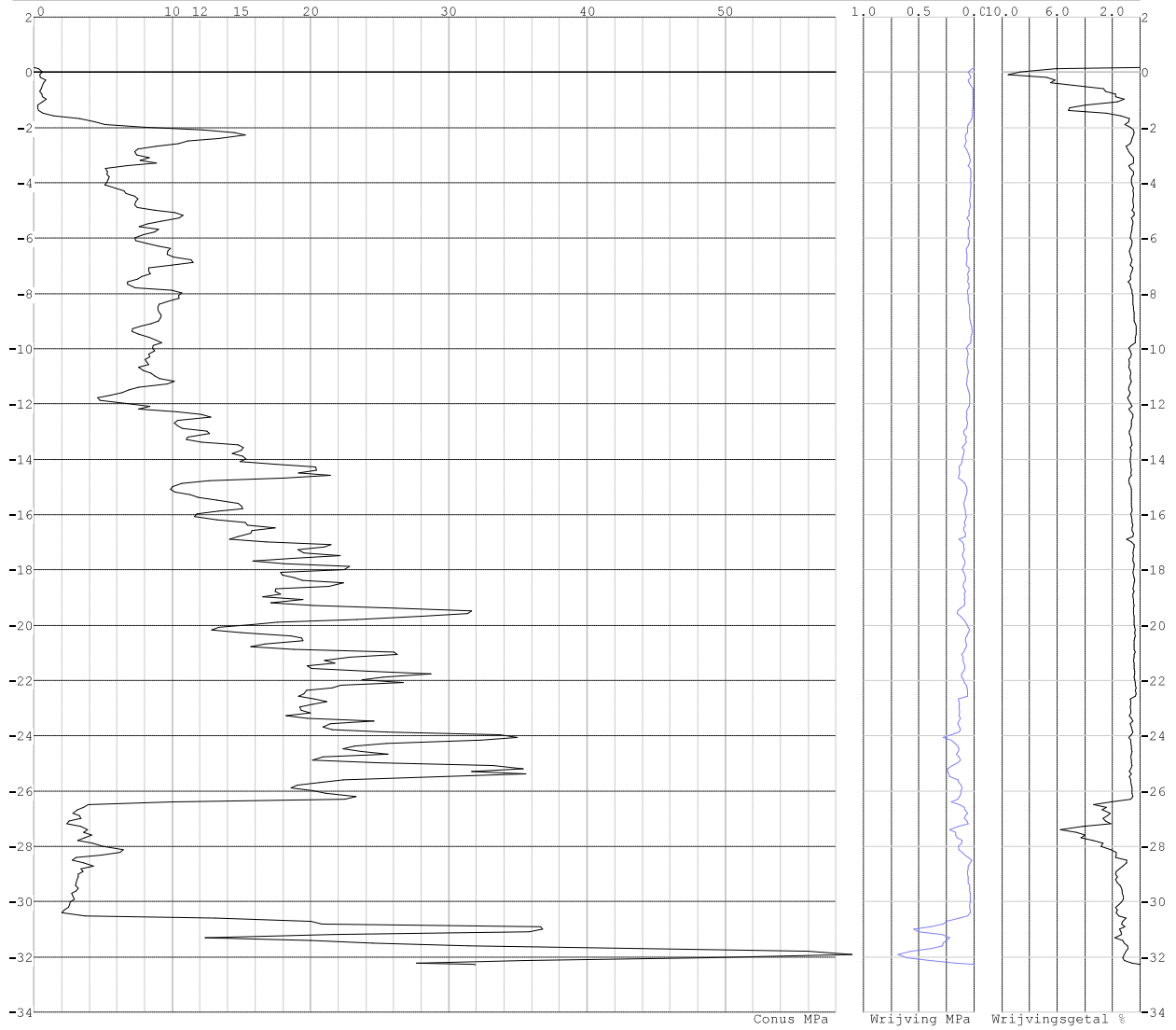


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 283.S02

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 0.17 Bodemprofiel: 283.S02
Traject negatieve kleef : 0.17 tot -1.60 [m]
Traject positieve kleef : -1.70 tot -32.29 [m]

SONDERINGSGEGEVENS GRAFIEK: 283.S02

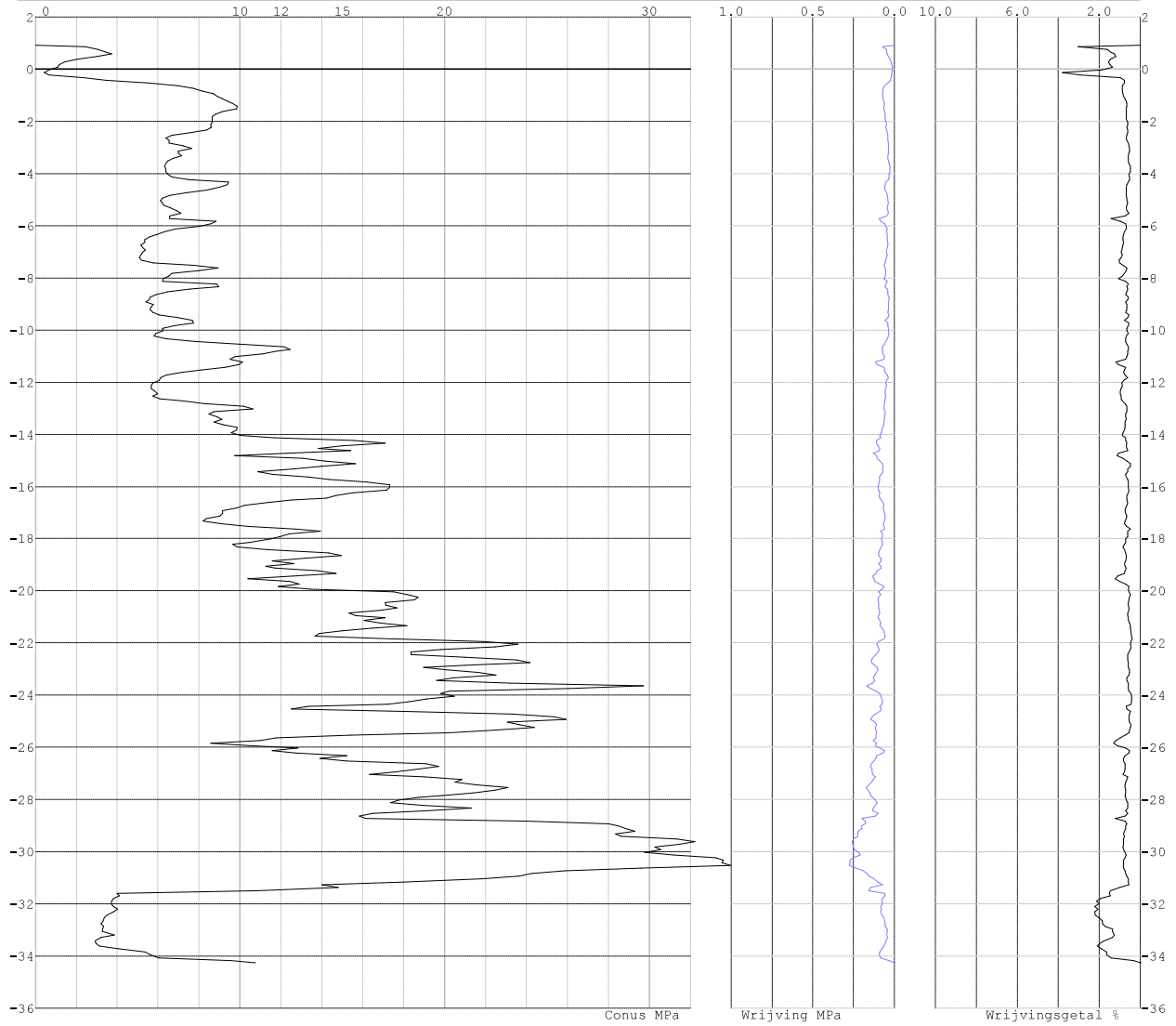


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_35

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 0.92 Bodemprofiel: 19-1008_35
Traject negatieve kleeft : 0.92 tot -0.60 [m]
Traject positieve kleeft : -0.80 tot -34.25 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_35

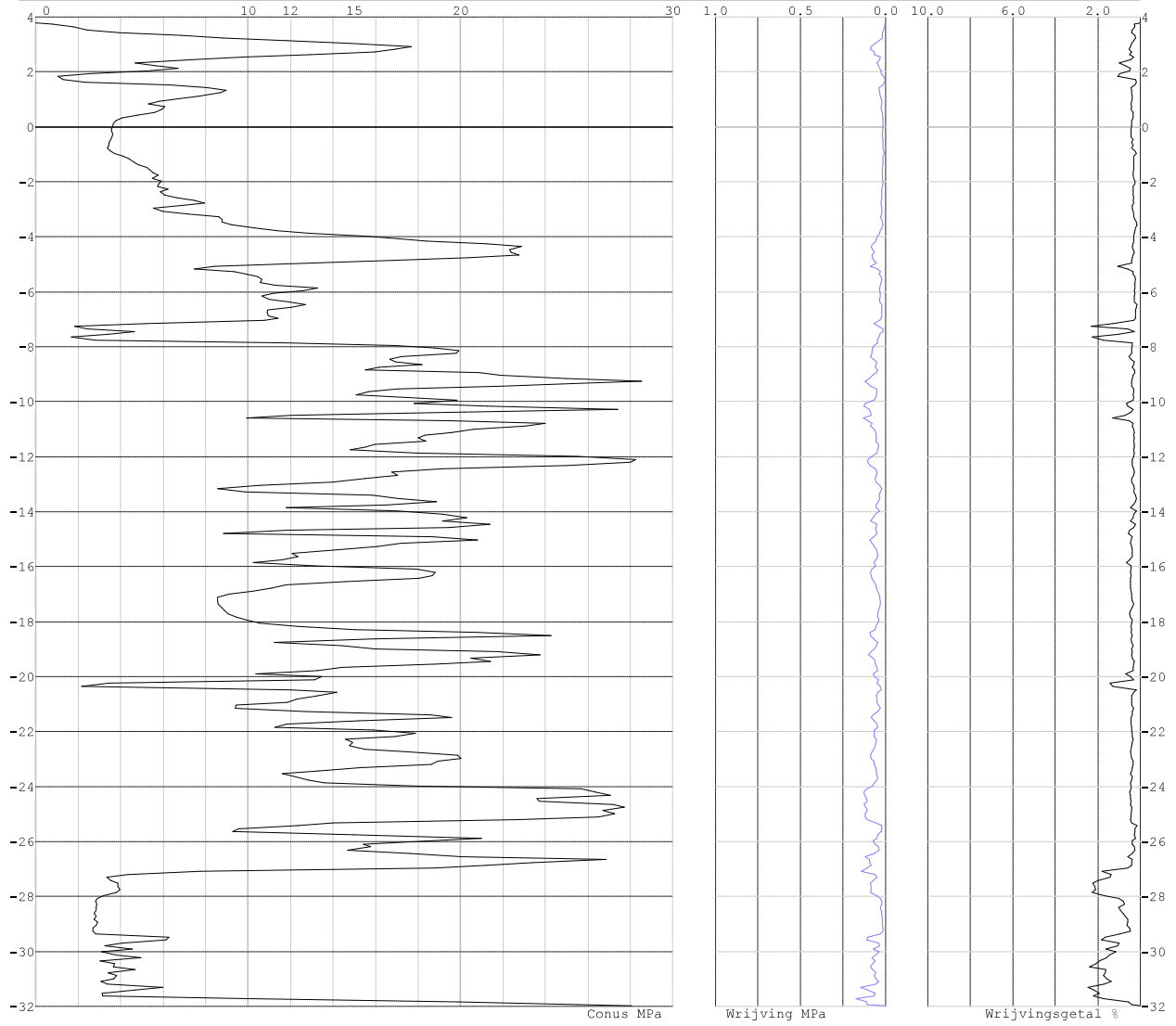


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 312.S03

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 3.78 Bodemprofiel: 312.S03
Traject negatieve kleeft : 3.78 tot 3.30 [m]
Traject positieve kleeft : 3.10 tot -31.97 [m]

SONDERINGSGEGEVENS GRAFIEK: 312.S03

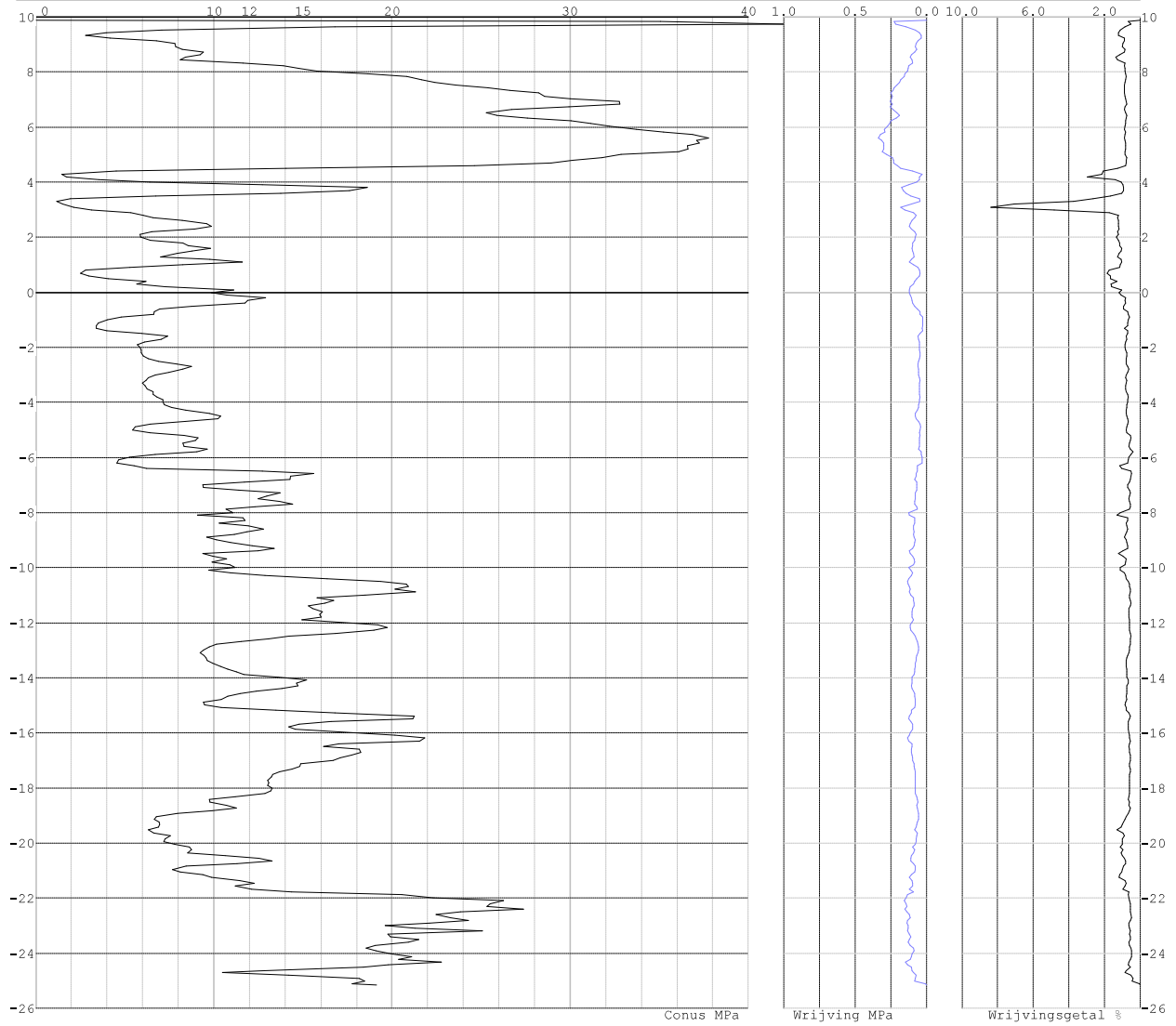


Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 19-1008_43

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
Hoogte maaiveld [m] : 9.88 Bodemprofiel: 19-1008_43
Traject negatieve kleeft : 9.88 tot 9.40 [m]
Traject positieve kleeft : 9.20 tot -25.16 [m]

SONDERINGSGEGEVENS GRAFIEK: 19-1008_43

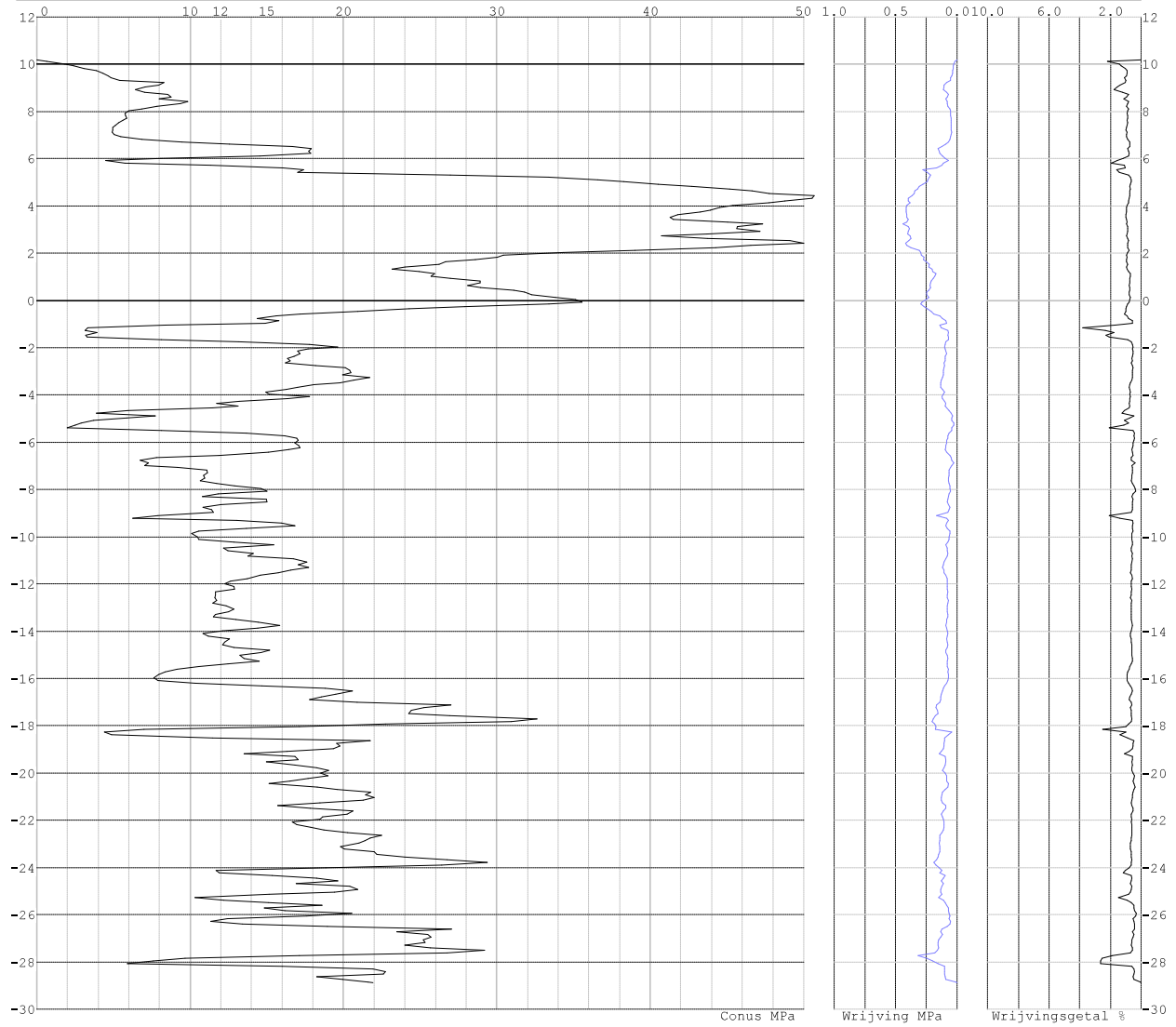


Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

SONDERINGSGEGEVENS ALGEMEEN: 328.S02

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.
 Hoogte maaiveld [m] : 10.17 Bodemprofiel: 328.S02
 Traject negatieve kleeft : 10.17 tot 9.90 [m]
 Traject positieve kleeft : 9.80 tot -28.89 [m]

SONDERINGSGEGEVENS GRAFIEK: 328.S02



REKENGEVENS SI Ø508/670 druk

Berekening : Ontwerpend
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2
 Sondering(en) : 19-1008_1, 19-1008_6, 166.S01, 19-1008_11, 19-1008_12
 : 19-1008_17, 19-1008_20, 19-1008_21, 251.S01, 19-1008_29
 : 283.S02, 19-1008_35, 312.S03, 19-1008_43, 328.S02

Stijf bouwwerk : NEE
 Paalgroep : NEE
 Aantal sonderingen : 15
 Factor ξ_3 (n=1) : 1.39 (handmatig)
 Factor ξ_3 (gem) : 1.39 (handmatig)
 Factor ξ_4 (min) : 1.39 (handmatig)
 Weerstandsfactor γ_R : 1.20
 $\gamma_{f,ink}$: 1.0
 $R_{f,calc,max,ii}$ begrenzen op $0.75 * R_{b,calc,max,ii}$: NEE
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø508/670
 Niveau paalkop [m] : N.A.P. 0.00
 Bovenbel. [kN/m²] : 0.00

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

PAALPUNTNIVEAUS SI Ø508/670

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|--------------------|-------------------|--------------------|
| 1 | -6.00 | -30.00 | 0.50 |

RESULTATEN SI Ø508/670 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Sondering | 19-1008_1 | 19-1008_6 | 166.S01 | 19-1008_11 | 19-1008_12 | 19-1008_17 |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| Niveau [m] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] |
| -6.00 | -71 | 2215 | 1436 | -53 | 1758 | -41 |
| -6.50 | -70 | 2342 | 1620 | -47 | 1420 | 0 |
| -7.00 | -66 | 2413 | 1721 | 32 | 1377 | -50 |
| -7.50 | -25 | 2768 | 1830 | 137 | 1337 | -88 |
| -8.00 | -12 | 2996 | 1954 | 172 | 1291 | -77 |
| -8.50 | -17 | 3209 | 2075 | 202 | 1284 | -51 |
| -9.00 | 85 | 3321 | 2181 | 235 | 1263 | -47 |
| -9.50 | 120 | 3387 | 2442 | 269 | 1281 | 222 |
| -10.00 | 152 | 3811 | 2245 | 269 | 1295 | 89 |
| -10.50 | 199 | 3886 | 2235 | 296 | 1311 | 336 |
| -11.00 | 304 | 3961 | 2170 | 329 | 1301 | 995 |
| -11.50 | 358 | 4027 | 2172 | 346 | 1342 | 1158 |
| -12.00 | 398 | 4091 | 2179 | 321 | 1355 | 1297 |
| -12.50 | 707 | 4121 | 2225 | 722 | 1361 | 1201 |
| -13.00 | 789 | 4150 | 2337 | 1011 | 1382 | 1268 |
| -13.50 | 871 | 4336 | 2644 | 1018 | 1440 | 1346 |
| -14.00 | 1056 | 4411 | 2755 | 1108 | 1474 | 1431 |
| -14.50 | 1220 | 4486 | 2865 | 1190 | 1501 | 1605 |
| -15.00 | 1320 | 4561 | 2968 | 1265 | 1525 | 1802 |
| -15.50 | 1308 | 4396 | 3249 | 1345 | 1575 | 1911 |
| -16.00 | 1481 | 3707 | 3390 | 1511 | 1628 | 1449 |
| -16.50 | 1594 | 3765 | 3510 | 1592 | 1667 | 1406 |
| -17.00 | 1802 | 3773 | 3596 | 1669 | 1712 | 1494 |
| -17.50 | 2613 | 3781 | 3654 | 1931 | 1748 | 1469 |
| -18.00 | 2309 | 3906 | 3758 | 2299 | 1954 | 1465 |
| -18.50 | 2364 | 4606 | 3843 | 2424 | 2032 | 1705 |
| -19.00 | 2078 | 4615 | 3900 | 2519 | 2290 | 1865 |
| -19.50 | 2081 | 4717 | 3939 | 2585 | 2424 | 1881 |
| -20.00 | 2080 | 4827 | 4108 | 2819 | 2650 | 1972 |
| -20.50 | 2185 | 4927 | 0 | 2749 | 2652 | 2102 |
| -21.00 | 2207 | 5058 | 0 | 2432 | 2934 | 2081 |
| -21.50 | 3012 | 5497 | 0 | 2452 | 3061 | 2286 |
| -22.00 | 3906 | 0 | 0 | 2388 | 3190 | 2531 |
| -22.50 | 3981 | 0 | 0 | 2400 | 3275 | 2473 |
| -23.00 | 4056 | 0 | 0 | 2393 | 3489 | 2477 |
| -23.50 | 4131 | 0 | 0 | 2580 | 3418 | 2504 |
| -24.00 | 4206 | 0 | 0 | 2660 | 3156 | 2542 |
| -24.50 | 4281 | 0 | 0 | 2706 | 3119 | 2593 |
| -25.00 | 4356 | 0 | 0 | 2746 | 3103 | 2653 |
| -25.50 | 4431 | 0 | 0 | 3414 | 3053 | 2714 |
| -26.00 | 4506 | 0 | 0 | 3368 | 3118 | 2785 |
| -26.50 | 4581 | 0 | 0 | 3440 | 3177 | 2921 |
| -27.00 | 4656 | 0 | 0 | 3535 | 3228 | 2385 |
| -27.50 | 4731 | 0 | 0 | 3655 | 3268 | 2409 |
| -28.00 | 4806 | 0 | 0 | 3854 | 3621 | 2449 |
| -28.50 | 4881 | 0 | 0 | 4066 | 4017 | 2452 |
| -29.00 | 4956 | 0 | 0 | 4217 | 4128 | 2402 |
| -29.50 | 5031 | 0 | 0 | 4772 | 0 | 2722 |
| -30.00 | 5106 | 0 | 0 | 4933 | 0 | 3140 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø508/670 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | 19-1008_20 | 19-1008_21 | 251.S01 | 19-1008_29 | 283.S02 | 19-1008_35 |
|--------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| [m] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] |
| -6.00 | 327 | 670 | 642 | 1248 | 1011 | 931 |
| -6.50 | 476 | 602 | 547 | 1473 | 1081 | 952 |
| -7.00 | 501 | 617 | 577 | 1492 | 1113 | 979 |
| -7.50 | 557 | 672 | 575 | 1548 | 1179 | 1054 |
| -8.00 | 456 | 721 | 579 | 1620 | 1253 | 1085 |
| -8.50 | 474 | 733 | 563 | 1685 | 1299 | 1108 |
| -9.00 | 502 | 756 | 809 | 1648 | 1335 | 1143 |
| -9.50 | 518 | 870 | 942 | 1220 | 1202 | 1203 |
| -10.00 | 496 | 900 | 1000 | 1260 | 1242 | 1239 |
| -10.50 | 615 | 946 | 1050 | 1293 | 1276 | 1316 |
| -11.00 | 612 | 976 | 1083 | 1308 | 1309 | 1350 |
| -11.50 | 598 | 1016 | 1142 | 1275 | 1307 | 1374 |
| -12.00 | 624 | 1043 | 1336 | 1435 | 1550 | 1400 |
| -12.50 | 652 | 1086 | 1424 | 1445 | 1689 | 1504 |
| -13.00 | 665 | 1120 | 1301 | 1435 | 1830 | 1640 |
| -13.50 | 730 | 1168 | 1365 | 1463 | 1978 | 1731 |
| -14.00 | 762 | 1197 | 1407 | 1491 | 2071 | 1920 |
| -14.50 | 773 | 1186 | 1413 | 1515 | 2127 | 1987 |
| -15.00 | 805 | 1178 | 1374 | 1542 | 2166 | 1992 |
| -15.50 | 829 | 1214 | 1960 | 1608 | 2354 | 2060 |
| -16.00 | 855 | 1233 | 2182 | 1622 | 2507 | 2117 |
| -16.50 | 872 | 1212 | 1983 | 1648 | 2675 | 2134 |
| -17.00 | 903 | 1236 | 2033 | 1691 | 2947 | 2176 |
| -17.50 | 1027 | 1276 | 2110 | 2088 | 3054 | 2342 |
| -18.00 | 1076 | 1358 | 2132 | 2389 | 3055 | 2384 |
| -18.50 | 1104 | 1382 | 2122 | 2412 | 3155 | 2525 |
| -19.00 | 1198 | 1413 | 2033 | 2233 | 3254 | 2589 |
| -19.50 | 1309 | 1427 | 1991 | 3058 | 3337 | 2680 |
| -20.00 | 1310 | 1440 | 1994 | 3420 | 3325 | 2933 |
| -20.50 | 1277 | 1455 | 1999 | 2967 | 3531 | 3025 |
| -21.00 | 1298 | 1477 | 2045 | 2855 | 3781 | 3125 |
| -21.50 | 1325 | 1500 | 2067 | 2709 | 3880 | 3250 |
| -22.00 | 1349 | 1524 | 2080 | 2678 | 3959 | 3544 |
| -22.50 | 1368 | 1545 | 2117 | 2608 | 4042 | 3490 |
| -23.00 | 1627 | 1565 | 2180 | 2641 | 4149 | 3573 |
| -23.50 | 1747 | 1597 | 2274 | 2732 | 4433 | 3360 |
| -24.00 | 1863 | 1625 | 2324 | 2758 | 4215 | 3412 |
| -24.50 | 1967 | 1645 | 2372 | 2791 | 3329 | 3474 |
| -25.00 | 2044 | 1671 | 2548 | 2821 | 3261 | 3519 |
| -25.50 | 2123 | 1694 | 2860 | 2868 | 3180 | 3449 |
| -26.00 | 2197 | 1718 | 3286 | 2908 | 3179 | 3674 |
| -26.50 | 2301 | 1740 | 3903 | 2941 | 3150 | 3983 |
| -27.00 | 2224 | 1761 | 3517 | 2977 | 3188 | 4119 |
| -27.50 | 2292 | 1795 | 3626 | 3025 | 3229 | 4228 |
| -28.00 | 2314 | 1821 | 3651 | 3052 | 3222 | 4313 |
| -28.50 | 2361 | 1845 | 3329 | 3088 | 3243 | 4546 |
| -29.00 | 2402 | 1877 | 3250 | 3257 | 3268 | 4701 |
| -29.50 | 2451 | 1908 | 3263 | 3412 | 3290 | 3968 |
| -30.00 | 2509 | 1934 | 3179 | 3371 | 0 | 3888 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø508/670 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Sondering 312.S03 19-1008_43 328.S02

| Niveau [m] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] |
|---------------|------------------------------|------------------------------|------------------------------|
| -6.00 | 843 | 934 | 1386 |
| -6.50 | 861 | 1260 | 1350 |
| -7.00 | 855 | 1332 | 1479 |
| -7.50 | 1011 | 1405 | 1563 |
| -8.00 | 1675 | 1485 | 1642 |
| -8.50 | 1686 | 1564 | 1698 |
| -9.00 | 1820 | 1645 | 1825 |
| -9.50 | 1890 | 1716 | 1998 |
| -10.00 | 2033 | 1899 | 2160 |
| -10.50 | 2245 | 2053 | 2271 |
| -11.00 | 2175 | 2071 | 2355 |
| -11.50 | 2287 | 2127 | 2428 |
| -12.00 | 2399 | 2187 | 2492 |
| -12.50 | 2394 | 2201 | 2580 |
| -13.00 | 2430 | 2236 | 2673 |
| -13.50 | 2597 | 2355 | 2539 |
| -14.00 | 2667 | 2416 | 2564 |
| -14.50 | 2691 | 2429 | 2621 |
| -15.00 | 2686 | 2732 | 2658 |
| -15.50 | 2733 | 2813 | 2663 |
| -16.00 | 2769 | 2793 | 2765 |
| -16.50 | 2774 | 2774 | 2877 |
| -17.00 | 2793 | 2589 | 2977 |
| -17.50 | 2865 | 2594 | 3018 |
| -18.00 | 2564 | 2641 | 2773 |
| -18.50 | 2622 | 2671 | 3306 |
| -19.00 | 2681 | 2695 | 3396 |
| -19.50 | 2653 | 2763 | 3581 |
| -20.00 | 2623 | 2894 | 3715 |
| -20.50 | 2967 | 2994 | 3919 |
| -21.00 | 3149 | 3107 | 4051 |
| -21.50 | 3269 | 3414 | 4194 |
| -22.00 | 3455 | 3855 | 4138 |
| -22.50 | 3574 | 3661 | 4265 |
| -23.00 | 3668 | 0 | 4215 |
| -23.50 | 3756 | 0 | 4295 |
| -24.00 | 3955 | 0 | 4306 |
| -24.50 | 4047 | 0 | 4382 |
| -25.00 | 3583 | 0 | 4372 |
| -25.50 | 3572 | 0 | 4495 |
| -26.00 | 3530 | 0 | 4292 |
| -26.50 | 3525 | 0 | 4402 |
| -27.00 | 3486 | 0 | 0 |
| -27.50 | 3512 | 0 | 0 |
| -28.00 | 3537 | 0 | 0 |
| -28.50 | 3560 | 0 | 0 |
| -29.00 | 3587 | 0 | 0 |
| -29.50 | 3651 | 0 | 0 |
| -30.00 | 0 | 0 | 0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

SAMENVATTINGSTABEL SI Ø508/670 druk (n=1)

Uitgangspunten

- paal : SI Ø508/670
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie
 - schachtafmeting : 590 mm
 Paalklassefactor α_p : 0.63
 Factor α_c (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
 Correlatiefactor $\xi_{s(n=1)}$: 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezijskdraagvermogen | | | Rekenwaarden | | |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
| | | | $R_{b,real}$ [kN] | $R_{s,real}$ [kN] | $R_{c,real}$ [kN] | $R_{c;d}$ [kN] | $F_{nk;d}$ [kN] | $R_{c,netto;d}$ [kN] |
| 19-1008_1 | 2.12 | -6.00 | 74.1 | 0.0 | 74.1 | 44.5 | -115.4 | -70.9 |
| | | -6.50 | 75.9 | 0.0 | 75.9 | 45.5 | -115.4 | -69.9 |
| | | -7.00 | 83.0 | 0.0 | 83.0 | 49.8 | -115.4 | -65.6 |
| | | -7.50 | 148.9 | 2.4 | 151.2 | 90.7 | -115.4 | -24.7 |
| | | -8.00 | 142.3 | 30.1 | 172.3 | 103.3 | -115.4 | -12.0 |
| | | -8.50 | 103.4 | 61.3 | 164.7 | 98.8 | -115.4 | -16.6 |
| | | -9.00 | 263.4 | 70.8 | 334.1 | 200.3 | -115.4 | 85.0 |
| | | -9.50 | 270.2 | 122.6 | 392.8 | 235.5 | -115.4 | 120.1 |
| | | -10.00 | 277.8 | 168.6 | 446.4 | 267.7 | -115.4 | 152.3 |
| | | -10.50 | 301.0 | 222.6 | 523.6 | 313.9 | -115.4 | 198.5 |
| | | -11.00 | 440.3 | 259.3 | 699.5 | 419.4 | -115.4 | 304.0 |
| | | -11.50 | 467.1 | 322.9 | 790.0 | 473.6 | -115.4 | 358.3 |
| | | -12.00 | 451.3 | 404.9 | 856.2 | 513.3 | -115.4 | 398.0 |
| | | -12.50 | 911.7 | 459.3 | 1371.0 | 821.9 | -115.4 | 706.5 |
| | | -13.00 | 962.1 | 547.0 | 1509.0 | 904.7 | -115.4 | 789.3 |
| | | -13.50 | 1010.3 | 634.6 | 1644.9 | 986.1 | -115.4 | 870.8 |
| | | -14.00 | 1243.4 | 710.1 | 1953.4 | 1171.1 | -115.4 | 1055.8 |
| | | -14.50 | 1417.3 | 809.6 | 2226.8 | 1335.0 | -115.4 | 1219.7 |
| | | -15.00 | 1494.3 | 900.2 | 2394.5 | 1435.5 | -115.4 | 1320.2 |
| | | -15.50 | 1374.5 | 999.5 | 2374.0 | 1423.3 | -115.4 | 1307.9 |
| | | -16.00 | 1578.4 | 1084.5 | 2663.0 | 1596.5 | -115.4 | 1481.1 |
| | | -16.50 | 1672.8 | 1178.2 | 2851.0 | 1709.2 | -115.4 | 1593.9 |
| | | -17.00 | 1925.2 | 1273.5 | 3198.7 | 1917.7 | -115.4 | 1802.3 |
| | | -17.50 | 3165.4 | 1384.9 | 4550.4 | 2728.0 | -115.4 | 2612.7 |
| | | -18.00 | 2533.5 | 1510.0 | 4043.5 | 2424.2 | -115.4 | 2308.8 |
| | | -18.50 | 2500.1 | 1635.1 | 4135.2 | 2479.2 | -115.4 | 2363.8 |
| | | -19.00 | 1897.8 | 1760.3 | 3658.1 | 2193.1 | -115.4 | 2077.7 |
| | | -19.50 | 1777.5 | 1885.4 | 3662.9 | 2196.0 | -115.4 | 2080.6 |
| | | -20.00 | 1622.6 | 2039.8 | 3662.4 | 2195.7 | -115.4 | 2080.3 |
| | | -20.50 | 1637.4 | 2200.1 | 3837.5 | 2300.6 | -115.4 | 2185.3 |
| | | -21.00 | 1506.1 | 2366.9 | 3873.0 | 2321.9 | -115.4 | 2206.6 |
| -21.50 | 2734.1 | 2481.7 | 5215.9 | 3127.0 | -115.4 | 3011.7 | | |
| -22.00 | 4101.0 | 2606.9 | 6707.8 | 4021.5 | -115.4 | 3906.1 | | |
| -22.50 | 4101.0 | 2732.0 | 6832.9 | 4096.5 | -115.4 | 3981.1 | | |
| -23.00 | 4101.0 | 2857.1 | 6958.0 | 4171.5 | -115.4 | 4056.1 | | |
| -23.50 | 4101.0 | 2982.2 | 7083.2 | 4246.5 | -115.4 | 4131.1 | | |
| -24.00 | 4101.0 | 3107.3 | 7208.3 | 4321.5 | -115.4 | 4206.1 | | |
| -24.50 | 4101.0 | 3232.4 | 7333.4 | 4396.5 | -115.4 | 4281.2 | | |
| -25.00 | 4101.0 | 3357.5 | 7458.5 | 4471.5 | -115.4 | 4356.2 | | |
| -25.50 | 4101.0 | 3482.7 | 7583.6 | 4546.5 | -115.4 | 4431.2 | | |
| -26.00 | 4101.0 | 3607.8 | 7708.7 | 4621.5 | -115.4 | 4506.2 | | |
| -26.50 | 4101.0 | 3732.9 | 7833.8 | 4696.5 | -115.4 | 4581.2 | | |
| -27.00 | 4101.0 | 3858.0 | 7959.0 | 4771.6 | -115.4 | 4656.2 | | |
| -27.50 | 4101.0 | 3983.1 | 8084.1 | 4846.6 | -115.4 | 4731.2 | | |
| -28.00 | 4101.0 | 4108.2 | 8209.2 | 4921.6 | -115.4 | 4806.2 | | |
| -28.50 | 4101.0 | 4233.3 | 8334.3 | 4996.6 | -115.4 | 4881.2 | | |
| -29.00 | 4101.0 | 4358.5 | 8459.4 | 5071.6 | -115.4 | 4956.2 | | |
| -29.50 | 4101.0 | 4483.6 | 8584.5 | 5146.6 | -115.4 | 5031.2 | | |
| -30.00 | 4101.0 | 4608.7 | 8709.6 | 5221.6 | -115.4 | 5106.2 | | |
| 19-1008_6 | 11.00 | -6.00 | 2439.0 | 1255.0 | 3694.0 | 2214.6 | 0.0 | 2214.6 |
| | | -6.50 | 2526.9 | 1380.1 | 3907.0 | 2342.3 | 0.0 | 2342.3 |
| | | -7.00 | 2518.9 | 1505.2 | 4024.1 | 2412.6 | 0.0 | 2412.6 |
| | | -7.50 | 2986.5 | 1630.3 | 4616.8 | 2767.9 | 0.0 | 2767.9 |
| | | -8.00 | 3241.8 | 1755.4 | 4997.3 | 2996.0 | 0.0 | 2996.0 |
| | | -8.50 | 3472.2 | 1880.6 | 5352.8 | 3209.1 | 0.0 | 3209.1 |
| | | -9.00 | 3533.5 | 2005.7 | 5539.2 | 3320.9 | 0.0 | 3320.9 |
| | | -9.50 | 3518.5 | 2130.8 | 5649.3 | 3386.9 | 0.0 | 3386.9 |
| | | -10.00 | 4101.0 | 2255.9 | 6356.9 | 3811.1 | 0.0 | 3811.1 |
| | | -10.50 | 4101.0 | 2381.0 | 6482.0 | 3886.1 | 0.0 | 3886.1 |
| | | -11.00 | 4101.0 | 2506.1 | 6607.1 | 3961.1 | 0.0 | 3961.1 |
| | | -11.50 | 4085.8 | 2631.2 | 6717.0 | 4027.0 | 0.0 | 4027.0 |
| | | -12.00 | 4067.7 | 2756.4 | 6824.0 | 4091.1 | 0.0 | 4091.1 |
| | | -12.50 | 3992.6 | 2881.5 | 6874.1 | 4121.2 | 0.0 | 4121.2 |
| | | -13.00 | 3914.8 | 3006.6 | 6921.4 | 4149.5 | 0.0 | 4149.5 |
| | | -13.50 | 4101.0 | 3131.7 | 7232.7 | 4336.1 | 0.0 | 4336.1 |
| | | -14.00 | 4101.0 | 3256.8 | 7357.8 | 4411.1 | 0.0 | 4411.1 |
| | | -14.50 | 4101.0 | 3381.9 | 7482.9 | 4486.1 | 0.0 | 4486.1 |
| | | -15.00 | 4101.0 | 3507.0 | 7608.0 | 4561.1 | 0.0 | 4561.1 |
| | | -15.50 | 3699.8 | 3632.2 | 7331.9 | 4395.6 | 0.0 | 4395.6 |
| | | -16.00 | 2425.7 | 3757.3 | 6183.0 | 3706.8 | 0.0 | 3706.8 |
| -16.50 | 2397.0 | 3882.4 | 6279.4 | 3764.6 | 0.0 | 3764.6 | | |
| -17.00 | 2285.4 | 4007.5 | 6292.9 | 3772.7 | 0.0 | 3772.7 | | |
| -17.50 | 2174.9 | 4132.6 | 6307.5 | 3781.5 | 0.0 | 3781.5 | | |
| -18.00 | 2256.8 | 4257.7 | 6514.5 | 3905.6 | 0.0 | 3905.6 | | |
| -18.50 | 3308.9 | 4374.5 | 7683.3 | 4606.3 | 0.0 | 4606.3 | | |
| -19.00 | 3198.2 | 4499.6 | 7697.8 | 4615.0 | 0.0 | 4615.0 | | |
| -19.50 | 3243.5 | 4624.7 | 7868.2 | 4717.2 | 0.0 | 4717.2 | | |
| -20.00 | 3301.1 | 4749.8 | 8050.9 | 4826.7 | 0.0 | 4826.7 | | |
| -20.50 | 3342.6 | 4874.9 | 8217.5 | 4926.6 | 0.0 | 4926.6 | | |
| -21.00 | 3436.2 | 5000.0 | 8436.3 | 5057.7 | 0.0 | 5057.7 | | |
| -21.50 | 4044.3 | 5125.1 | 9169.5 | 5497.3 | 0.0 | 5497.3 | | |
| 166.S01 | 3.45 | -6.00 | 1838.5 | 571.4 | 2410.0 | 1444.8 | -8.9 | 1435.9 |
| | | -6.50 | 2019.9 | 696.6 | 2716.4 | 1628.5 | -8.9 | 1619.7 |
| | | -7.00 | 2063.9 | 821.7 | 2885.6 | 1730.0 | -8.9 | 1721.1 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld | | Bezijskdraagvermogen | | | Rekenwaarden | | |
|------------|----------|----------|--------------------------|--------------------------|--------------------------|-----------------------|-----------------------|-----------------------------|
| | niveau | paalpunt | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _{b;d} [kN] | F _{h;d} [kN] | R _{c,netto;d} [kN] |
| 166.S01 | 3.45 | -7.50 | 2120.6 | 946.8 | 3067.4 | 1839.0 | -8.9 | 1830.1 |
| | | -8.00 | 2202.7 | 1071.9 | 3274.6 | 1963.2 | -8.9 | 1954.3 |
| | | -8.50 | 2280.3 | 1196.1 | 3476.4 | 2084.1 | -8.9 | 2075.3 |
| | | -9.00 | 2333.3 | 1320.1 | 3653.3 | 2190.2 | -8.9 | 2181.4 |
| | | -9.50 | 2646.1 | 1442.3 | 4088.4 | 2451.1 | -8.9 | 2442.2 |
| | | -10.00 | 2191.9 | 1567.4 | 3759.4 | 2253.8 | -8.9 | 2244.9 |
| | | -10.50 | 2050.8 | 1692.5 | 3743.3 | 2244.2 | -8.9 | 2235.3 |
| | | -11.00 | 1817.1 | 1817.6 | 3634.8 | 2179.1 | -8.9 | 2170.2 |
| | | -11.50 | 1694.2 | 1942.8 | 3636.9 | 2180.4 | -8.9 | 2171.5 |
| | | -12.00 | 1591.2 | 2057.7 | 3648.9 | 2187.6 | -8.9 | 2178.7 |
| | | -12.50 | 1571.1 | 2154.9 | 3726.0 | 2233.8 | -8.9 | 2224.9 |
| | | -13.00 | 1666.9 | 2245.8 | 3912.7 | 2345.7 | -8.9 | 2336.9 |
| | | -13.50 | 2087.6 | 2338.1 | 4425.7 | 2653.3 | -8.9 | 2644.4 |
| | | -14.00 | 2163.8 | 2445.5 | 4609.3 | 2763.4 | -8.9 | 2754.5 |
| | | -14.50 | 2224.6 | 2569.3 | 4794.0 | 2874.1 | -8.9 | 2865.2 |
| | | -15.00 | 2271.1 | 2694.4 | 4965.5 | 2976.9 | -8.9 | 2968.1 |
| | | -15.50 | 2614.1 | 2819.5 | 5433.6 | 3257.6 | -8.9 | 3248.7 |
| | | -16.00 | 2725.3 | 2944.7 | 5670.0 | 3399.3 | -8.9 | 3390.4 |
| | | -16.50 | 2800.2 | 3069.8 | 5870.0 | 3519.2 | -8.9 | 3510.3 |
| | | -17.00 | 2818.7 | 3194.9 | 6013.6 | 3605.3 | -8.9 | 3596.4 |
| | | -17.50 | 2789.5 | 3320.0 | 6109.5 | 3662.8 | -8.9 | 3653.9 |
| -18.00 | 2838.7 | 3445.1 | 6283.9 | 3767.3 | -8.9 | 3758.4 | | |
| -18.50 | 2854.2 | 3570.2 | 6424.4 | 3851.6 | -8.9 | 3842.7 | | |
| -19.00 | 2824.6 | 3695.3 | 6519.9 | 3908.8 | -8.9 | 3899.9 | | |
| -19.50 | 2764.1 | 3820.5 | 6584.6 | 3947.6 | -8.9 | 3938.7 | | |
| -20.00 | 2920.5 | 3945.6 | 6866.1 | 4116.4 | -8.9 | 4107.5 | | |
| 19-1008_11 | 0.62 | -6.00 | 136.3 | 0.0 | 136.3 | 81.7 | -135.0 | -53.3 |
| | | -6.50 | 146.6 | 0.0 | 146.6 | 87.9 | -135.0 | -47.1 |
| | | -7.00 | 273.2 | 5.5 | 278.7 | 167.1 | -135.0 | 32.0 |
| | | -7.50 | 413.9 | 39.6 | 453.5 | 271.9 | -135.0 | 136.9 |
| | | -8.00 | 421.6 | 89.8 | 511.4 | 306.6 | -135.0 | 171.6 |
| | | -8.50 | 426.6 | 135.6 | 562.2 | 337.0 | -135.0 | 202.0 |
| | | -9.00 | 445.6 | 171.0 | 616.7 | 369.7 | -135.0 | 234.7 |
| | | -9.50 | 469.4 | 204.8 | 674.2 | 404.2 | -135.0 | 269.1 |
| | | -10.00 | 434.6 | 239.8 | 674.4 | 404.3 | -135.0 | 269.3 |
| | | -10.50 | 436.3 | 281.8 | 718.1 | 430.5 | -135.0 | 295.5 |
| | | -11.00 | 442.9 | 330.8 | 773.7 | 463.9 | -135.0 | 328.8 |
| | | -11.50 | 413.4 | 389.8 | 803.1 | 481.5 | -135.0 | 346.4 |
| | | -12.00 | 296.8 | 464.1 | 760.9 | 456.2 | -135.0 | 321.1 |
| | | -12.50 | 937.8 | 491.9 | 1429.7 | 857.1 | -135.0 | 722.1 |
| | | -13.00 | 1332.2 | 579.6 | 1911.8 | 1146.2 | -135.0 | 1011.1 |
| | | -13.50 | 1240.8 | 683.1 | 1923.9 | 1153.4 | -135.0 | 1018.4 |
| | | -14.00 | 1284.1 | 788.6 | 2072.7 | 1242.6 | -135.0 | 1107.6 |
| | | -14.50 | 1314.6 | 895.2 | 2209.8 | 1324.8 | -135.0 | 1189.8 |
| | | -15.00 | 1333.3 | 1001.8 | 2335.1 | 1400.0 | -135.0 | 1264.9 |
| | | -15.50 | 1367.1 | 1101.6 | 2468.7 | 1480.1 | -135.0 | 1345.0 |
| | | -16.00 | 1559.2 | 1185.9 | 2745.0 | 1645.7 | -135.0 | 1510.7 |
| | | -16.50 | 1596.3 | 1284.4 | 2880.7 | 1727.0 | -135.0 | 1592.0 |
| | | -17.00 | 1629.7 | 1379.2 | 3008.9 | 1803.9 | -135.0 | 1668.9 |
| | | -17.50 | 1977.8 | 1468.7 | 3446.5 | 2066.2 | -135.0 | 1931.2 |
| | | -18.00 | 2477.9 | 1581.5 | 4059.4 | 2433.7 | -135.0 | 2298.7 |
| | | -18.50 | 2562.5 | 1706.6 | 4269.1 | 2559.4 | -135.0 | 2424.4 |
| | | -19.00 | 2596.0 | 1831.7 | 4427.7 | 2654.5 | -135.0 | 2519.4 |
| | | -19.50 | 2580.8 | 1956.8 | 4537.6 | 2720.4 | -135.0 | 2585.4 |
| | | -20.00 | 2846.1 | 2081.9 | 4928.0 | 2954.4 | -135.0 | 2819.4 |
| | | -20.50 | 2603.4 | 2207.0 | 4810.4 | 2884.0 | -135.0 | 2748.9 |
| -21.00 | 1949.5 | 2332.2 | 4281.6 | 2566.9 | -135.0 | 2431.9 | | |
| -21.50 | 1865.2 | 2450.1 | 4315.3 | 2587.1 | -135.0 | 2452.0 | | |
| -22.00 | 1633.6 | 2575.2 | 4208.8 | 2523.3 | -135.0 | 2388.2 | | |
| -22.50 | 1528.9 | 2700.3 | 4229.2 | 2535.5 | -135.0 | 2400.4 | | |
| -23.00 | 1403.5 | 2813.7 | 4217.2 | 2528.3 | -135.0 | 2393.2 | | |
| -23.50 | 1638.9 | 2889.1 | 4528.0 | 2714.6 | -135.0 | 2579.6 | | |
| -24.00 | 1676.1 | 2986.2 | 4662.3 | 2795.2 | -135.0 | 2660.1 | | |
| -24.50 | 1642.1 | 3096.4 | 4738.5 | 2840.8 | -135.0 | 2705.8 | | |
| -25.00 | 1604.9 | 3201.2 | 4806.0 | 2881.3 | -135.0 | 2746.3 | | |
| -25.50 | 2630.1 | 3289.6 | 5919.7 | 3549.0 | -135.0 | 3413.9 | | |
| -26.00 | 2428.7 | 3414.7 | 5843.4 | 3503.3 | -135.0 | 3368.2 | | |
| -26.50 | 2422.6 | 3539.8 | 5962.4 | 3574.6 | -135.0 | 3439.6 | | |
| -27.00 | 2456.2 | 3664.9 | 6121.1 | 3669.7 | -135.0 | 3534.7 | | |
| -27.50 | 2531.2 | 3790.0 | 6321.3 | 3789.7 | -135.0 | 3654.7 | | |
| -28.00 | 2738.8 | 3915.2 | 6654.0 | 3989.2 | -135.0 | 3854.2 | | |
| -28.50 | 2967.6 | 4040.2 | 7007.8 | 4201.3 | -135.0 | 4066.3 | | |
| -29.00 | 3093.1 | 4165.3 | 7258.4 | 4351.6 | -135.0 | 4216.5 | | |
| -29.50 | 3894.2 | 4290.5 | 8184.6 | 4906.8 | -135.0 | 4771.8 | | |
| -30.00 | 4037.8 | 4415.6 | 8453.4 | 5068.0 | -135.0 | 4933.0 | | |
| 19-1008_12 | 3.57 | -6.00 | 1574.5 | 1357.6 | 2932.1 | 1757.8 | 0.0 | 1757.8 |
| | | -6.50 | 912.3 | 1456.0 | 2368.3 | 1419.8 | 0.0 | 1419.8 |
| | | -7.00 | 718.5 | 1578.0 | 2296.5 | 1376.8 | 0.0 | 1376.8 |
| | | -7.50 | 526.5 | 1703.1 | 2229.6 | 1336.7 | 0.0 | 1336.7 |
| | | -8.00 | 326.8 | 1827.0 | 2153.9 | 1291.3 | 0.0 | 1291.3 |
| | | -8.50 | 250.5 | 1890.8 | 2141.2 | 1283.7 | 0.0 | 1283.7 |
| | | -9.00 | 197.1 | 1909.4 | 2106.5 | 1262.9 | 0.0 | 1262.9 |
| | | -9.50 | 213.2 | 1923.0 | 2136.2 | 1280.7 | 0.0 | 1280.7 |
| | | -10.00 | 209.1 | 1950.1 | 2159.2 | 1294.5 | 0.0 | 1294.5 |
| | | -10.50 | 180.8 | 2005.2 | 2186.0 | 1310.5 | 0.0 | 1310.5 |
| | | -11.00 | 122.7 | 2047.7 | 2170.3 | 1301.2 | 0.0 | 1301.2 |
| | | -11.50 | 181.9 | 2056.0 | 2237.8 | 1341.6 | 0.0 | 1341.6 |
| | | -12.00 | 163.7 | 2095.7 | 2259.4 | 1354.6 | 0.0 | 1354.6 |
| | | -12.50 | 160.4 | 2110.1 | 2270.6 | 1361.3 | 0.0 | 1361.3 |
| | | -13.00 | 183.3 | 2121.4 | 2304.7 | 1381.7 | 0.0 | 1381.7 |
| -13.50 | 266.3 | 2135.4 | 2401.6 | 1439.8 | 0.0 | 1439.8 | | |
| -14.00 | 288.4 | 2169.8 | 2458.2 | 1473.7 | 0.0 | 1473.7 | | |
| -14.50 | 288.5 | 2214.7 | 2503.2 | 1500.7 | 0.0 | 1500.7 | | |
| -15.00 | 298.3 | 2246.2 | 2544.5 | 1525.5 | 0.0 | 1525.5 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziwkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|----------------------------|--------------------------------|
| | | | R _{o,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _{o;d} [kN] | F _{h,k;d} [kN] | R _{o,netto;d} [kN] |
| 19-1008_12 | 3.57 | -15.50 | 356.6 | 2271.0 | 2627.6 | 1575.3 | 0.0 | 1575.3 |
| | | -16.00 | 404.1 | 2311.7 | 2715.7 | 1628.1 | 0.0 | 1628.1 |
| | | -16.50 | 412.6 | 2367.3 | 2779.9 | 1666.6 | 0.0 | 1666.6 |
| | | -17.00 | 443.0 | 2413.4 | 2856.4 | 1712.5 | 0.0 | 1712.5 |
| | | -17.50 | 434.0 | 2482.3 | 2916.3 | 1748.4 | 0.0 | 1748.4 |
| | | -18.00 | 723.7 | 2535.5 | 3259.2 | 1954.0 | 0.0 | 1954.0 |
| | | -18.50 | 730.9 | 2658.7 | 3389.6 | 2032.1 | 0.0 | 2032.1 |
| | | -19.00 | 1048.0 | 2771.4 | 3819.3 | 2289.8 | 0.0 | 2289.8 |
| | | -19.50 | 1169.2 | 2874.4 | 4043.6 | 2424.2 | 0.0 | 2424.2 |
| | | -20.00 | 1457.3 | 2963.3 | 4420.5 | 2650.2 | 0.0 | 2650.2 |
| | | -20.50 | 1360.0 | 3063.3 | 4423.3 | 2651.9 | 0.0 | 2651.9 |
| | | -21.00 | 1736.6 | 3157.0 | 4893.7 | 2933.9 | 0.0 | 2933.9 |
| | | -21.50 | 1834.3 | 3270.7 | 5104.9 | 3060.5 | 0.0 | 3060.5 |
| | | -22.00 | 1926.9 | 3394.0 | 5320.9 | 3190.0 | 0.0 | 3190.0 |
| | | -22.50 | 1945.3 | 3517.2 | 5462.6 | 3274.9 | 0.0 | 3274.9 |
| | | -23.00 | 2189.4 | 3630.1 | 5819.5 | 3488.9 | 0.0 | 3488.9 |
| | | -23.50 | 1962.8 | 3738.8 | 5701.6 | 3418.2 | 0.0 | 3418.2 |
| | | -24.00 | 1409.7 | 3854.2 | 5263.9 | 3155.8 | 0.0 | 3155.8 |
| | | -24.50 | 1223.6 | 3979.3 | 5202.8 | 3119.2 | 0.0 | 3119.2 |
| | | -25.00 | 1071.3 | 4104.4 | 5175.7 | 3102.9 | 0.0 | 3102.9 |
| | | -25.50 | 822.7 | 4269.5 | 5092.2 | 3052.9 | 0.0 | 3052.9 |
| | | -26.00 | 765.4 | 4435.6 | 5200.9 | 3118.1 | 0.0 | 3118.1 |
| | | -26.50 | 767.9 | 4531.2 | 5299.1 | 3176.9 | 0.0 | 3176.9 |
| | | -27.00 | 763.3 | 4620.6 | 5383.8 | 3227.7 | 0.0 | 3227.7 |
| | | -27.50 | 727.5 | 4723.1 | 5450.6 | 3267.7 | 0.0 | 3267.7 |
| | | -28.00 | 1243.1 | 4797.1 | 6040.2 | 3621.2 | 0.0 | 3621.2 |
| | | -28.50 | 1808.9 | 4892.2 | 6701.1 | 4017.4 | 0.0 | 4017.4 |
| | | -29.00 | 1868.1 | 5017.3 | 6885.4 | 4127.9 | 0.0 | 4127.9 |
| 19-1008_17 | 0.20 | -6.00 | 143.4 | 0.0 | 143.4 | 86.0 | -127.5 | -41.5 |
| | | -6.50 | 241.3 | 0.0 | 241.3 | 144.7 | -144.6 | 0.0 |
| | | -7.00 | 194.5 | 0.0 | 194.5 | 116.6 | -166.5 | -49.9 |
| | | -7.50 | 167.9 | 0.0 | 167.9 | 100.7 | -188.6 | -87.9 |
| | | -8.00 | 185.8 | 0.0 | 185.8 | 111.4 | -188.6 | -77.2 |
| | | -8.50 | 230.2 | 0.0 | 230.2 | 138.0 | -188.6 | -50.5 |
| | | -9.00 | 236.1 | 0.0 | 236.1 | 141.6 | -188.6 | -47.0 |
| | | -9.50 | 684.9 | 0.0 | 684.9 | 410.6 | -188.6 | 222.1 |
| | | -10.00 | 463.1 | 0.0 | 463.1 | 277.6 | -188.6 | 89.0 |
| | | -10.50 | 856.2 | 19.2 | 875.4 | 524.8 | -188.6 | 336.2 |
| | | -11.00 | 1875.8 | 97.6 | 1973.5 | 1183.1 | -188.6 | 994.6 |
| | | -11.50 | 2022.6 | 222.8 | 2245.3 | 1346.1 | -188.6 | 1157.6 |
| | | -12.00 | 2130.2 | 347.9 | 2478.1 | 1485.7 | -188.6 | 1297.1 |
| | | -12.50 | 1845.0 | 473.0 | 2317.9 | 1389.7 | -188.6 | 1201.1 |
| | | -13.00 | 1832.0 | 598.1 | 2430.1 | 1456.9 | -188.6 | 1268.3 |
| | | -13.50 | 1836.1 | 723.2 | 2559.3 | 1534.4 | -188.6 | 1345.8 |
| | | -14.00 | 1853.6 | 848.3 | 2701.9 | 1619.8 | -188.6 | 1431.3 |
| | | -14.50 | 2019.0 | 973.4 | 2992.3 | 1794.0 | -188.6 | 1605.4 |
| | | -15.00 | 2230.5 | 1089.0 | 3319.5 | 1990.1 | -188.6 | 1801.5 |
| | | -15.50 | 2288.0 | 1214.1 | 3502.1 | 2099.6 | -188.6 | 1911.0 |
| | | -16.00 | 1392.2 | 1339.2 | 2731.4 | 1637.5 | -188.6 | 1449.0 |
| | | -16.50 | 1196.2 | 1464.3 | 2660.5 | 1595.0 | -188.6 | 1406.4 |
| | | -17.00 | 1222.3 | 1584.3 | 2806.6 | 1682.6 | -188.6 | 1494.0 |
| | | -17.50 | 1051.8 | 1713.8 | 2765.6 | 1658.1 | -188.6 | 1469.5 |
| | | -18.00 | 894.3 | 1864.1 | 2758.4 | 1653.7 | -188.6 | 1465.2 |
| | | -18.50 | 1193.2 | 1964.6 | 3157.8 | 1893.2 | -188.6 | 1704.6 |
| | | -19.00 | 1374.9 | 2051.3 | 3426.2 | 2054.1 | -188.6 | 1865.5 |
| | | -19.50 | 1300.2 | 2151.4 | 3451.6 | 2069.3 | -188.6 | 1880.7 |
| | | -20.00 | 1350.8 | 2252.3 | 3603.1 | 2160.2 | -188.6 | 1971.6 |
| | | -20.50 | 1460.7 | 2359.5 | 3820.2 | 2290.3 | -188.6 | 2101.7 |
| | | -21.00 | 1315.9 | 2470.1 | 3786.0 | 2269.8 | -188.6 | 2081.2 |
| | | -21.50 | 1533.7 | 2594.0 | 4127.7 | 2474.6 | -188.6 | 2286.1 |
| | | -22.00 | 1836.4 | 2700.7 | 4537.0 | 2720.1 | -188.6 | 2531.5 |
| | | -22.50 | 1614.4 | 2825.8 | 4440.2 | 2662.0 | -188.6 | 2473.4 |
| | | -23.00 | 1496.0 | 2950.9 | 4446.9 | 2666.0 | -188.6 | 2477.5 |
| | | -23.50 | 1415.7 | 3076.0 | 4491.7 | 2692.9 | -188.6 | 2504.3 |
| | | -24.00 | 1362.8 | 3191.4 | 4554.2 | 2730.3 | -188.6 | 2541.8 |
| | | -24.50 | 1347.8 | 3291.2 | 4639.0 | 2781.2 | -188.6 | 2592.6 |
| | | -25.00 | 1371.3 | 3369.1 | 4740.4 | 2842.0 | -188.6 | 2653.4 |
| | | -25.50 | 1396.6 | 3444.6 | 4841.2 | 2902.4 | -188.6 | 2713.8 |
| | | -26.00 | 1441.9 | 3518.3 | 4960.2 | 2973.8 | -188.6 | 2785.2 |
| | | -26.50 | 1595.4 | 3591.8 | 5187.2 | 3109.8 | -188.6 | 2921.3 |
| | | -27.00 | 614.4 | 3679.1 | 4293.5 | 2574.0 | -188.6 | 2385.4 |
| | | -27.50 | 559.6 | 3772.6 | 4332.2 | 2597.2 | -188.6 | 2408.7 |
| | | -28.00 | 531.0 | 3867.9 | 4398.9 | 2637.2 | -188.6 | 2448.6 |
| | | -28.50 | 436.8 | 3967.9 | 4404.7 | 2640.7 | -188.6 | 2452.1 |
| | | -29.00 | 248.0 | 4072.8 | 4320.9 | 2590.5 | -188.6 | 2401.9 |
| | | -29.50 | 752.0 | 4102.5 | 4854.4 | 2910.3 | -188.6 | 2721.7 |
| | | -30.00 | 1370.2 | 4182.1 | 5552.3 | 3328.7 | -188.6 | 3140.2 |
| 19-1008_20 | -0.03 | -6.00 | 478.7 | 125.8 | 604.5 | 362.4 | -35.5 | 326.9 |
| | | -6.50 | 686.9 | 166.4 | 853.3 | 511.6 | -35.5 | 476.1 |
| | | -7.00 | 652.0 | 243.5 | 895.5 | 536.9 | -35.5 | 501.3 |
| | | -7.50 | 678.1 | 310.5 | 988.6 | 592.7 | -35.5 | 557.1 |
| | | -8.00 | 457.8 | 362.3 | 820.1 | 491.6 | -35.5 | 456.1 |
| | | -8.50 | 437.1 | 412.7 | 849.9 | 509.5 | -35.5 | 474.0 |
| | | -9.00 | 413.6 | 482.7 | 896.4 | 537.4 | -35.5 | 501.9 |
| | | -9.50 | 384.4 | 539.4 | 923.7 | 553.8 | -35.5 | 518.3 |
| | | -10.00 | 282.1 | 604.8 | 886.9 | 531.7 | -35.5 | 496.2 |
| | | -10.50 | 464.3 | 620.5 | 1084.8 | 650.3 | -35.5 | 614.8 |
| | | -11.00 | 374.9 | 705.4 | 1080.3 | 647.6 | -35.5 | 612.1 |
| | | -11.50 | 260.2 | 797.1 | 1057.3 | 633.8 | -35.5 | 598.3 |
| | | -12.00 | 285.6 | 814.9 | 1100.5 | 659.8 | -35.5 | 624.2 |
| | | -12.50 | 311.3 | 835.4 | 1146.7 | 687.5 | -35.5 | 651.9 |
| | | -13.00 | 293.0 | 874.9 | 1167.9 | 700.2 | -35.5 | 664.6 |
| | | -13.50 | 383.5 | 892.7 | 1276.1 | 765.1 | -35.5 | 729.5 |
| | | -14.00 | 402.7 | 927.5 | 1330.2 | 797.5 | -35.5 | 762.0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziijkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|---------------------------|--------------------------------|
| | | | R _{b,real} [kN] | R _{r,real} [kN] | R _{c,real} [kN] | R _{r,d} [kN] | F _{pk,d} [kN] | R _{c,netto,d} [kN] |
| 19-1008_20 | -0.03 | -14.50 | 355.8 | 992.1 | 1347.9 | 808.1 | -35.5 | 772.5 |
| | | -15.00 | 336.3 | 1065.9 | 1402.2 | 840.6 | -35.5 | 805.1 |
| | | -15.50 | 334.7 | 1107.3 | 1442.1 | 864.5 | -35.5 | 829.0 |
| | | -16.00 | 346.3 | 1138.4 | 1484.7 | 890.1 | -35.5 | 854.6 |
| | | -16.50 | 331.0 | 1182.5 | 1513.6 | 907.4 | -35.5 | 871.9 |
| | | -17.00 | 354.0 | 1211.0 | 1565.1 | 938.3 | -35.5 | 902.8 |
| | | -17.50 | 526.9 | 1246.0 | 1772.9 | 1062.9 | -35.5 | 1027.4 |
| | | -18.00 | 542.0 | 1311.6 | 1853.7 | 1111.3 | -35.5 | 1075.8 |
| | | -18.50 | 511.6 | 1388.4 | 1900.0 | 1139.1 | -35.5 | 1103.6 |
| | | -19.00 | 611.3 | 1445.8 | 2057.1 | 1233.3 | -35.5 | 1197.7 |
| | | -19.50 | 720.2 | 1523.2 | 2243.4 | 1345.0 | -35.5 | 1309.4 |
| | | -20.00 | 642.1 | 1603.0 | 2245.1 | 1346.0 | -35.5 | 1310.4 |
| | | -20.50 | 483.7 | 1705.7 | 2189.4 | 1312.6 | -35.5 | 1277.1 |
| | | -21.00 | 380.9 | 1843.3 | 2224.3 | 1333.5 | -35.5 | 1297.9 |
| | | -21.50 | 367.4 | 1901.7 | 2269.1 | 1360.3 | -35.5 | 1324.8 |
| | | -22.00 | 369.7 | 1940.1 | 2309.8 | 1384.7 | -35.5 | 1349.2 |
| | | -22.50 | 358.2 | 1982.1 | 2340.3 | 1403.0 | -35.5 | 1367.5 |
| | | -23.00 | 758.0 | 2015.9 | 2773.9 | 1663.0 | -35.5 | 1627.5 |
| | | -23.50 | 891.0 | 2081.8 | 2972.8 | 1782.3 | -35.5 | 1746.7 |
| | | -24.00 | 1010.4 | 2155.6 | 3166.1 | 1898.1 | -35.5 | 1862.6 |
| | | -24.50 | 1106.5 | 2233.0 | 3339.5 | 2002.1 | -35.5 | 1966.5 |
| | | -25.00 | 1140.6 | 2328.1 | 3468.8 | 2079.6 | -35.5 | 2044.1 |
| | | -25.50 | 1186.4 | 2414.6 | 3601.1 | 2158.9 | -35.5 | 2123.4 |
| | | -26.00 | 1224.2 | 2499.2 | 3723.4 | 2232.3 | -35.5 | 2196.7 |
| | | -26.50 | 1321.2 | 2575.7 | 3896.9 | 2336.2 | -35.5 | 2300.7 |
| | | -27.00 | 1100.5 | 2668.9 | 3769.4 | 2259.8 | -35.5 | 2224.3 |
| | | -27.50 | 1132.0 | 2750.8 | 3882.8 | 2327.8 | -35.5 | 2292.3 |
| | | -28.00 | 1094.5 | 2824.9 | 3919.4 | 2349.8 | -35.5 | 2314.2 |
| | | -28.50 | 1085.8 | 2911.7 | 3997.6 | 2396.6 | -35.5 | 2361.1 |
| | | -29.00 | 1074.2 | 2992.2 | 4066.4 | 2437.9 | -35.5 | 2402.4 |
| -29.50 | 1090.8 | 3056.9 | 4147.7 | 2486.6 | -35.5 | 2451.1 | | |
| -30.00 | 1105.7 | 3138.6 | 4244.3 | 2544.6 | -35.5 | 2509.0 | | |
| 19-1008_21 | 1.78 | -6.00 | 1028.7 | 273.3 | 1302.1 | 780.6 | -110.9 | 669.7 |
| | | -6.50 | 835.6 | 353.4 | 1189.0 | 712.8 | -110.9 | 601.9 |
| | | -7.00 | 781.9 | 433.1 | 1214.9 | 728.4 | -110.9 | 617.5 |
| | | -7.50 | 775.3 | 531.1 | 1306.4 | 783.2 | -110.9 | 672.3 |
| | | -8.00 | 765.4 | 622.9 | 1388.4 | 832.3 | -110.9 | 721.4 |
| | | -8.50 | 692.8 | 715.6 | 1408.4 | 844.4 | -110.9 | 733.5 |
| | | -9.00 | 682.9 | 763.6 | 1446.5 | 867.2 | -110.9 | 756.3 |
| | | -9.50 | 836.9 | 799.7 | 1636.6 | 981.2 | -110.9 | 870.3 |
| | | -10.00 | 831.9 | 854.7 | 1686.7 | 1011.2 | -110.9 | 900.3 |
| | | -10.50 | 859.1 | 903.0 | 1762.1 | 1056.4 | -110.9 | 945.5 |
| | | -11.00 | 854.9 | 958.4 | 1813.3 | 1087.1 | -110.9 | 976.2 |
| | | -11.50 | 851.4 | 1028.3 | 1879.7 | 1126.9 | -110.9 | 1016.0 |
| | | -12.00 | 818.0 | 1106.8 | 1924.8 | 1153.9 | -110.9 | 1043.0 |
| | | -12.50 | 829.7 | 1167.1 | 1996.8 | 1197.1 | -110.9 | 1086.2 |
| | | -13.00 | 816.0 | 1236.8 | 2052.7 | 1230.7 | -110.9 | 1119.7 |
| | | -13.50 | 819.6 | 1313.9 | 2133.5 | 1279.1 | -110.9 | 1168.2 |
| | | -14.00 | 752.8 | 1428.6 | 2181.4 | 1307.8 | -110.9 | 1196.9 |
| | | -14.50 | 619.8 | 1543.5 | 2163.4 | 1297.0 | -110.9 | 1186.1 |
| | | -15.00 | 521.5 | 1627.6 | 2149.2 | 1288.5 | -110.9 | 1177.6 |
| | | -15.50 | 521.4 | 1689.0 | 2210.3 | 1325.1 | -110.9 | 1214.2 |
| | | -16.00 | 433.7 | 1807.5 | 2241.2 | 1343.7 | -110.9 | 1232.8 |
| | | -16.50 | 280.8 | 1925.9 | 2206.7 | 1323.0 | -110.9 | 1212.0 |
| | | -17.00 | 300.0 | 1946.0 | 2246.1 | 1346.6 | -110.9 | 1235.7 |
| | | -17.50 | 343.9 | 1969.5 | 2313.4 | 1386.9 | -110.9 | 1276.0 |
| | | -18.00 | 435.6 | 2014.4 | 2450.0 | 1468.8 | -110.9 | 1357.9 |
| | | -18.50 | 346.4 | 2144.2 | 2490.6 | 1493.2 | -110.9 | 1382.2 |
| | | -19.00 | 307.6 | 2234.8 | 2542.4 | 1524.2 | -110.9 | 1413.3 |
| | | -19.50 | 307.1 | 2257.8 | 2565.0 | 1537.8 | -110.9 | 1426.9 |
| | | -20.00 | 311.0 | 2276.2 | 2587.2 | 1551.1 | -110.9 | 1440.2 |
| | | -20.50 | 317.7 | 2294.3 | 2612.0 | 1566.0 | -110.9 | 1455.1 |
| -21.00 | 335.4 | 2312.6 | 2648.0 | 1587.5 | -110.9 | 1476.6 | | |
| -21.50 | 352.1 | 2334.7 | 2686.8 | 1610.8 | -110.9 | 1499.9 | | |
| -22.00 | 366.2 | 2360.3 | 2726.5 | 1634.6 | -110.9 | 1523.7 | | |
| -22.50 | 369.7 | 2391.6 | 2761.3 | 1655.4 | -110.9 | 1544.5 | | |
| -23.00 | 372.9 | 2422.6 | 2795.5 | 1676.0 | -110.9 | 1565.1 | | |
| -23.50 | 395.6 | 2452.4 | 2848.0 | 1707.4 | -110.9 | 1596.5 | | |
| -24.00 | 407.2 | 2487.8 | 2895.0 | 1735.6 | -110.9 | 1624.7 | | |
| -24.50 | 405.3 | 2524.1 | 2929.5 | 1756.3 | -110.9 | 1645.4 | | |
| -25.00 | 409.4 | 2562.4 | 2971.8 | 1781.6 | -110.9 | 1670.7 | | |
| -25.50 | 407.9 | 2602.6 | 3010.4 | 1804.8 | -110.9 | 1693.9 | | |
| -26.00 | 408.7 | 2641.0 | 3049.8 | 1828.4 | -110.9 | 1717.5 | | |
| -26.50 | 411.0 | 2675.9 | 3086.8 | 1850.6 | -110.9 | 1739.7 | | |
| -27.00 | 411.3 | 2711.6 | 3122.9 | 1872.2 | -110.9 | 1761.3 | | |
| -27.50 | 433.1 | 2746.6 | 3179.8 | 1906.3 | -110.9 | 1795.4 | | |
| -28.00 | 437.8 | 2784.5 | 3222.3 | 1931.8 | -110.9 | 1820.9 | | |
| -28.50 | 439.6 | 2823.5 | 3263.2 | 1956.3 | -110.9 | 1845.4 | | |
| -29.00 | 453.9 | 2861.4 | 3315.3 | 1987.6 | -110.9 | 1876.7 | | |
| -29.50 | 465.7 | 2901.2 | 3367.0 | 2018.6 | -110.9 | 1907.7 | | |
| -30.00 | 467.8 | 2943.8 | 3411.6 | 2045.3 | -110.9 | 1934.4 | | |
| 251.S01 | -1.05 | -6.00 | 673.9 | 417.3 | 1091.2 | 654.2 | -12.2 | 642.0 |
| | | -6.50 | 430.4 | 503.1 | 933.5 | 559.6 | -12.2 | 547.5 |
| | | -7.00 | 379.8 | 603.2 | 983.0 | 589.3 | -12.2 | 577.1 |
| | | -7.50 | 278.9 | 700.0 | 978.9 | 586.8 | -12.2 | 574.7 |
| | | -8.00 | 196.5 | 788.9 | 985.4 | 590.8 | -12.2 | 578.6 |
| | | -8.50 | 110.3 | 848.8 | 959.1 | 575.0 | -12.2 | 562.8 |
| | | -9.00 | 512.4 | 857.8 | 1370.2 | 821.5 | -12.2 | 809.3 |
| | | -9.50 | 679.2 | 913.1 | 1592.3 | 954.6 | -12.2 | 942.5 |
| | | -10.00 | 691.9 | 997.0 | 1688.9 | 1012.5 | -12.2 | 1000.3 |
| | | -10.50 | 676.5 | 1095.6 | 1772.1 | 1062.4 | -12.2 | 1050.2 |
| | | -11.00 | 657.0 | 1170.4 | 1827.4 | 1095.6 | -12.2 | 1083.4 |
| | | -11.50 | 709.0 | 1215.9 | 1924.9 | 1154.0 | -12.2 | 1141.9 |
| -12.00 | 988.0 | 1261.1 | 2249.1 | 1348.4 | -12.2 | 1336.2 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|--------------------------|--------------------------------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _d [kN] | F _{hkd} [kN] | R _{d,netto;d} [kN] |
| 251.S01 | -1.05 | -12.50 | 1058.4 | 1338.0 | 2396.4 | 1436.7 | -12.2 | 1424.5 |
| | | -13.00 | 761.7 | 1428.8 | 2190.5 | 1313.2 | -12.2 | 1301.1 |
| | | -13.50 | 782.8 | 1514.4 | 2297.2 | 1377.2 | -12.2 | 1365.0 |
| | | -14.00 | 733.8 | 1633.4 | 2367.2 | 1419.2 | -12.2 | 1407.0 |
| | | -14.50 | 624.8 | 1751.7 | 2376.5 | 1424.8 | -12.2 | 1412.6 |
| | | -15.00 | 432.6 | 1879.7 | 2312.3 | 1386.3 | -12.2 | 1374.1 |
| | | -15.50 | 1352.0 | 1937.0 | 3289.0 | 1971.8 | -12.2 | 1959.6 |
| | | -16.00 | 1607.9 | 2052.5 | 3660.4 | 2194.5 | -12.2 | 2182.3 |
| | | -16.50 | 1149.9 | 2177.6 | 3327.5 | 1994.9 | -12.2 | 1982.7 |
| | | -17.00 | 1109.8 | 2301.3 | 3411.2 | 2045.1 | -12.2 | 2032.9 |
| | | -17.50 | 1119.7 | 2419.4 | 3539.2 | 2121.8 | -12.2 | 2109.6 |
| | | -18.00 | 1046.1 | 2531.0 | 3577.1 | 2144.5 | -12.2 | 2132.3 |
| | | -18.50 | 903.9 | 2655.9 | 3559.8 | 2134.2 | -12.2 | 2122.0 |
| | | -19.00 | 680.4 | 2731.0 | 3411.4 | 2045.2 | -12.2 | 2033.0 |
| | | -19.50 | 529.9 | 2811.2 | 3341.1 | 2003.1 | -12.2 | 1990.9 |
| | | -20.00 | 438.1 | 2908.5 | 3346.6 | 2006.3 | -12.2 | 1994.2 |
| | | -20.50 | 310.4 | 3044.6 | 3355.0 | 2011.4 | -12.2 | 1999.2 |
| | | -21.00 | 243.3 | 3187.9 | 3431.2 | 2057.1 | -12.2 | 2044.9 |
| | | -21.50 | 220.6 | 3247.4 | 3468.0 | 2079.1 | -12.2 | 2066.9 |
| | | -22.00 | 223.6 | 3266.0 | 3489.6 | 2092.1 | -12.2 | 2079.9 |
| | | -22.50 | 261.7 | 3290.6 | 3552.3 | 2129.7 | -12.2 | 2117.5 |
| | | -23.00 | 326.4 | 3330.0 | 3656.4 | 2192.1 | -12.2 | 2179.9 |
| | | -23.50 | 432.2 | 3381.6 | 3813.8 | 2286.4 | -12.2 | 2274.3 |
| | | -24.00 | 444.7 | 3451.4 | 3896.1 | 2335.8 | -12.2 | 2323.6 |
| | | -24.50 | 461.6 | 3515.0 | 3976.6 | 2384.1 | -12.2 | 2371.9 |
| | | -25.00 | 698.0 | 3572.7 | 4270.7 | 2560.4 | -12.2 | 2548.2 |
| | | -25.50 | 1114.2 | 3676.3 | 4790.4 | 2872.0 | -12.2 | 2859.8 |
| | | -26.00 | 1673.3 | 3828.1 | 5501.4 | 3298.2 | -12.2 | 3286.0 |
| | | -26.50 | 2555.8 | 3974.3 | 6530.2 | 3915.0 | -12.2 | 3902.8 |
| | | -27.00 | 1787.8 | 4099.5 | 5887.2 | 3529.5 | -12.2 | 3517.3 |
| -27.50 | 1843.6 | 4224.6 | 6068.1 | 3638.0 | -12.2 | 3625.8 | | |
| -28.00 | 1760.1 | 4349.7 | 6109.8 | 3662.9 | -12.2 | 3650.7 | | |
| -28.50 | 1097.7 | 4474.8 | 5572.5 | 3340.8 | -12.2 | 3328.6 | | |
| -29.00 | 841.7 | 4599.7 | 5441.4 | 3262.3 | -12.2 | 3250.1 | | |
| -29.50 | 778.6 | 4683.7 | 5462.3 | 3274.8 | -12.2 | 3262.6 | | |
| -30.00 | 539.7 | 4783.8 | 5323.5 | 3191.5 | -12.2 | 3179.4 | | |
| 19-1008_29 | 0.79 | -6.00 | 1333.7 | 757.2 | 2090.9 | 1253.5 | -5.9 | 1247.6 |
| | | -6.50 | 1620.2 | 846.0 | 2466.2 | 1478.5 | -5.9 | 1472.6 |
| | | -7.00 | 1549.9 | 948.4 | 2498.3 | 1497.8 | -5.9 | 1491.9 |
| | | -7.50 | 1536.4 | 1054.8 | 2591.2 | 1553.5 | -5.9 | 1547.6 |
| | | -8.00 | 1542.4 | 1169.2 | 2711.5 | 1625.6 | -5.9 | 1619.7 |
| | | -8.50 | 1537.2 | 1282.7 | 2819.9 | 1690.6 | -5.9 | 1684.7 |
| | | -9.00 | 1377.8 | 1381.5 | 2759.3 | 1654.3 | -5.9 | 1648.4 |
| | | -9.50 | 571.1 | 1473.7 | 2044.8 | 1225.9 | -5.9 | 1220.0 |
| | | -10.00 | 551.7 | 1559.9 | 2111.6 | 1266.0 | -5.9 | 1260.1 |
| | | -10.50 | 506.4 | 1660.0 | 2166.4 | 1298.8 | -5.9 | 1292.9 |
| | | -11.00 | 431.8 | 1759.3 | 2191.1 | 1313.6 | -5.9 | 1307.7 |
| | | -11.50 | 266.0 | 1870.2 | 2136.2 | 1280.7 | -5.9 | 1274.8 |
| | | -12.00 | 481.0 | 1922.4 | 2403.3 | 1440.8 | -5.9 | 1434.9 |
| | | -12.50 | 383.7 | 2035.6 | 2419.3 | 1450.4 | -5.9 | 1444.5 |
| | | -13.00 | 280.2 | 2122.8 | 2403.0 | 1440.7 | -5.9 | 1434.8 |
| | | -13.50 | 290.8 | 2159.3 | 2450.2 | 1468.9 | -5.9 | 1463.0 |
| | | -14.00 | 294.2 | 2202.4 | 2496.6 | 1496.8 | -5.9 | 1490.9 |
| | | -14.50 | 303.8 | 2232.3 | 2536.1 | 1520.4 | -5.9 | 1514.5 |
| | | -15.00 | 323.7 | 2257.8 | 2581.5 | 1547.7 | -5.9 | 1541.8 |
| | | -15.50 | 403.0 | 2288.6 | 2691.6 | 1613.7 | -5.9 | 1607.8 |
| | | -16.00 | 348.9 | 2367.0 | 2715.8 | 1628.2 | -5.9 | 1622.3 |
| | | -16.50 | 362.4 | 2396.0 | 2758.3 | 1653.7 | -5.9 | 1647.8 |
| | | -17.00 | 405.0 | 2425.2 | 2830.2 | 1696.7 | -5.9 | 1690.8 |
| | | -17.50 | 1025.3 | 2467.5 | 3492.8 | 2094.0 | -5.9 | 2088.1 |
| | | -18.00 | 1424.0 | 2570.8 | 3994.8 | 2395.0 | -5.9 | 2389.1 |
| | | -18.50 | 1337.0 | 2695.9 | 4032.9 | 2417.8 | -5.9 | 2411.9 |
| | | -19.00 | 918.3 | 2817.0 | 3735.3 | 2239.4 | -5.9 | 2233.5 |
| | | -19.50 | 2199.8 | 2910.6 | 5110.3 | 3063.7 | -5.9 | 3057.8 |
| | | -20.00 | 2679.2 | 3035.7 | 5714.9 | 3426.2 | -5.9 | 3420.3 |
| | | -20.50 | 1797.9 | 3160.8 | 4958.7 | 2972.8 | -5.9 | 2966.9 |
| -21.00 | 1486.7 | 3285.9 | 4772.6 | 2861.3 | -5.9 | 2855.4 | | |
| -21.50 | 1117.6 | 3411.0 | 4528.6 | 2715.0 | -5.9 | 2709.1 | | |
| -22.00 | 940.5 | 3536.1 | 4476.6 | 2683.8 | -5.9 | 2677.9 | | |
| -22.50 | 679.3 | 3681.3 | 4360.6 | 2614.3 | -5.9 | 2608.4 | | |
| -23.00 | 625.9 | 3788.5 | 4414.4 | 2646.5 | -5.9 | 2640.6 | | |
| -23.50 | 704.9 | 3862.7 | 4567.6 | 2738.4 | -5.9 | 2732.5 | | |
| -24.00 | 660.0 | 3950.1 | 4610.1 | 2763.8 | -5.9 | 2758.0 | | |
| -24.50 | 625.6 | 4038.9 | 4664.5 | 2796.4 | -5.9 | 2790.5 | | |
| -25.00 | 581.1 | 4133.3 | 4714.4 | 2826.4 | -5.9 | 2820.5 | | |
| -25.50 | 601.9 | 4191.9 | 4793.8 | 2874.0 | -5.9 | 2868.1 | | |
| -26.00 | 601.4 | 4259.3 | 4860.7 | 2914.1 | -5.9 | 2908.2 | | |
| -26.50 | 593.5 | 4322.1 | 4915.7 | 2947.0 | -5.9 | 2941.1 | | |
| -27.00 | 574.7 | 4401.0 | 4975.7 | 2983.1 | -5.9 | 2977.2 | | |
| -27.50 | 594.5 | 4460.6 | 5055.2 | 3030.7 | -5.9 | 3024.8 | | |
| -28.00 | 581.1 | 4518.8 | 5099.8 | 3057.4 | -5.9 | 3051.5 | | |
| -28.50 | 584.6 | 4576.5 | 5161.1 | 3094.2 | -5.9 | 3088.3 | | |
| -29.00 | 803.1 | 4640.1 | 5443.2 | 3263.3 | -5.9 | 3257.4 | | |
| -29.50 | 961.0 | 4740.5 | 5701.6 | 3418.2 | -5.9 | 3412.3 | | |
| -30.00 | 807.4 | 4825.6 | 5633.1 | 3377.1 | -5.9 | 3371.2 | | |
| 283.S02 | 0.17 | -6.00 | 1139.4 | 567.0 | 1706.4 | 1023.0 | -11.9 | 1011.1 |
| | | -6.50 | 1184.4 | 639.1 | 1823.5 | 1093.2 | -11.9 | 1081.3 |
| | | -7.00 | 1149.0 | 726.6 | 1875.7 | 1124.5 | -11.9 | 1112.6 |
| | | -7.50 | 1190.8 | 795.0 | 1985.8 | 1190.5 | -11.9 | 1178.6 |
| | | -8.00 | 1246.8 | 862.6 | 2109.4 | 1264.6 | -11.9 | 1252.8 |
| | | -8.50 | 1241.4 | 944.8 | 2186.2 | 1310.7 | -11.9 | 1298.8 |
| | | -9.00 | 1225.9 | 1020.5 | 2246.3 | 1346.7 | -11.9 | 1334.8 |
| -9.50 | 939.5 | 1084.6 | 2024.2 | 1213.5 | -11.9 | 1201.7 | | |
| -10.00 | 934.9 | 1156.8 | 2091.7 | 1254.0 | -11.9 | 1242.1 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|---------------------------|--------------------------------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _{b;d} [kN] | F _{hk;d} [kN] | R _{c,netto;d} [kN] |
| 283.S02 | 0.17 | -10.50 | 921.1 | 1226.4 | 2147.4 | 1287.4 | -11.9 | 1275.5 |
| | | -11.00 | 908.8 | 1294.4 | 2203.3 | 1320.9 | -11.9 | 1309.0 |
| | | -11.50 | 831.7 | 1367.5 | 2199.1 | 1318.4 | -11.9 | 1306.5 |
| | | -12.00 | 1191.8 | 1414.3 | 2606.0 | 1562.4 | -11.9 | 1550.5 |
| | | -12.50 | 1341.2 | 1495.5 | 2836.7 | 1700.6 | -11.9 | 1688.8 |
| | | -13.00 | 1486.9 | 1585.8 | 3072.7 | 1842.1 | -11.9 | 1830.3 |
| | | -13.50 | 1632.9 | 1686.4 | 3319.3 | 1990.0 | -11.9 | 1978.1 |
| | | -14.00 | 1668.6 | 1805.8 | 3474.4 | 2083.0 | -11.9 | 2071.1 |
| | | -14.50 | 1643.0 | 1925.2 | 3568.2 | 2139.2 | -11.9 | 2127.3 |
| | | -15.00 | 1600.7 | 2031.8 | 3632.5 | 2177.8 | -11.9 | 2165.9 |
| | | -15.50 | 1823.4 | 2123.0 | 3946.4 | 2366.0 | -11.9 | 2354.1 |
| | | -16.00 | 1977.7 | 2223.0 | 4200.7 | 2518.4 | -11.9 | 2506.5 |
| | | -16.50 | 2147.5 | 2334.4 | 4481.9 | 2687.0 | -11.9 | 2675.1 |
| | | -17.00 | 2482.4 | 2453.7 | 4936.2 | 2959.3 | -11.9 | 2947.4 |
| | | -17.50 | 2534.8 | 2578.8 | 5113.6 | 3065.7 | -11.9 | 3053.8 |
| | | -18.00 | 2411.3 | 2703.9 | 5115.2 | 3066.7 | -11.9 | 3054.8 |
| | | -18.50 | 2452.7 | 2829.0 | 5281.8 | 3166.5 | -11.9 | 3154.6 |
| | | -19.00 | 2493.9 | 2954.2 | 5448.1 | 3266.2 | -11.9 | 3254.4 |
| | | -19.50 | 2506.7 | 3079.3 | 5586.0 | 3348.9 | -11.9 | 3337.0 |
| | | -20.00 | 2361.0 | 3204.4 | 5565.4 | 3336.6 | -11.9 | 3324.7 |
| | | -20.50 | 2585.0 | 3323.9 | 5908.9 | 3542.5 | -11.9 | 3530.6 |
| | | -21.00 | 2877.2 | 3449.0 | 6326.2 | 3792.7 | -11.9 | 3780.8 |
| | | -21.50 | 2917.2 | 3574.1 | 6491.3 | 3891.7 | -11.9 | 3879.8 |
| | | -22.00 | 2924.8 | 3699.3 | 6624.0 | 3971.2 | -11.9 | 3959.3 |
| | | -22.50 | 2938.1 | 3824.4 | 6762.5 | 4054.3 | -11.9 | 4042.4 |
| | | -23.00 | 2991.4 | 3949.5 | 6940.9 | 4161.2 | -11.9 | 4149.3 |
| | | -23.50 | 3339.1 | 4074.6 | 7413.7 | 4444.7 | -11.9 | 4432.8 |
| | | -24.00 | 2850.0 | 4199.7 | 7049.7 | 4226.4 | -11.9 | 4214.5 |
| | | -24.50 | 1247.6 | 4324.8 | 5572.5 | 3340.8 | -11.9 | 3328.9 |
| -25.00 | 1009.8 | 4449.9 | 5459.8 | 3273.2 | -11.9 | 3261.3 | | |
| -25.50 | 749.8 | 4575.1 | 5324.9 | 3192.4 | -11.9 | 3180.5 | | |
| -26.00 | 622.3 | 4700.2 | 5322.5 | 3190.9 | -11.9 | 3179.0 | | |
| -26.50 | 441.6 | 4831.9 | 5273.5 | 3161.6 | -11.9 | 3149.7 | | |
| -27.00 | 459.1 | 4877.6 | 5336.7 | 3199.5 | -11.9 | 3187.6 | | |
| -27.50 | 484.7 | 4920.9 | 5405.6 | 3240.8 | -11.9 | 3228.9 | | |
| -28.00 | 418.2 | 4975.4 | 5393.6 | 3233.6 | -11.9 | 3221.7 | | |
| -28.50 | 385.3 | 5044.5 | 5429.8 | 3255.3 | -11.9 | 3243.4 | | |
| -29.00 | 377.2 | 5093.8 | 5471.0 | 3280.0 | -11.9 | 3268.1 | | |
| -29.50 | 370.4 | 5137.1 | 5507.5 | 3301.9 | -11.9 | 3290.0 | | |
| 19-1008_35 | 0.92 | -6.00 | 901.7 | 663.9 | 1565.6 | 938.6 | -7.3 | 931.3 |
| | | -6.50 | 881.9 | 717.6 | 1599.5 | 958.9 | -7.3 | 951.6 |
| | | -7.00 | 884.1 | 761.6 | 1645.7 | 986.6 | -7.3 | 979.3 |
| | | -7.50 | 963.8 | 806.7 | 1770.5 | 1061.4 | -7.3 | 1054.1 |
| | | -8.00 | 953.5 | 869.3 | 1822.8 | 1092.8 | -7.3 | 1085.5 |
| | | -8.50 | 927.8 | 932.4 | 1860.2 | 1115.2 | -7.3 | 1107.9 |
| | | -9.00 | 938.6 | 980.6 | 1919.2 | 1150.6 | -7.3 | 1143.3 |
| | | -9.50 | 990.2 | 1029.2 | 2019.4 | 1210.7 | -7.3 | 1203.4 |
| | | -10.00 | 990.6 | 1087.9 | 2078.5 | 1246.1 | -7.3 | 1238.8 |
| | | -10.50 | 1064.6 | 1142.9 | 2207.5 | 1323.4 | -7.3 | 1316.1 |
| | | -11.00 | 1027.1 | 1237.6 | 2264.6 | 1357.7 | -7.3 | 1350.4 |
| | | -11.50 | 986.2 | 1318.1 | 2304.3 | 1381.5 | -7.3 | 1374.2 |
| | | -12.00 | 973.2 | 1373.9 | 2347.1 | 1407.1 | -7.3 | 1399.8 |
| | | -12.50 | 1098.4 | 1422.0 | 2520.5 | 1511.1 | -7.3 | 1503.8 |
| | | -13.00 | 1260.8 | 1486.3 | 2747.0 | 1646.9 | -7.3 | 1639.6 |
| | | -13.50 | 1337.6 | 1562.0 | 2899.7 | 1738.4 | -7.3 | 1731.1 |
| | | -14.00 | 1573.3 | 1641.2 | 3214.4 | 1927.1 | -7.3 | 1919.8 |
| | | -14.50 | 1588.8 | 1738.3 | 3327.1 | 1994.6 | -7.3 | 1987.3 |
| | | -15.00 | 1499.0 | 1835.4 | 3334.4 | 1999.1 | -7.3 | 1991.7 |
| | | -15.50 | 1514.4 | 1933.9 | 3448.2 | 2067.3 | -7.3 | 2060.0 |
| | | -16.00 | 1508.9 | 2034.7 | 3543.7 | 2124.5 | -7.3 | 2117.2 |
| | | -16.50 | 1435.2 | 2136.1 | 3571.3 | 2141.1 | -7.3 | 2133.8 |
| | | -17.00 | 1418.0 | 2223.1 | 3641.1 | 2182.9 | -7.3 | 2175.6 |
| | | -17.50 | 1621.1 | 2297.0 | 3918.1 | 2349.0 | -7.3 | 2341.7 |
| | | -18.00 | 1593.3 | 2395.2 | 3988.4 | 2391.1 | -7.3 | 2383.8 |
| | | -18.50 | 1740.2 | 2483.8 | 4223.9 | 2532.3 | -7.3 | 2525.0 |
| | | -19.00 | 1747.1 | 2583.6 | 4330.7 | 2596.3 | -7.3 | 2589.0 |
| | | -19.50 | 1800.4 | 2682.3 | 4482.7 | 2687.5 | -7.3 | 2680.1 |
| | | -20.00 | 2120.2 | 2784.1 | 4904.3 | 2940.2 | -7.3 | 2932.9 |
| -20.50 | 2149.0 | 2909.2 | 5058.2 | 3032.5 | -7.3 | 3025.2 | | |
| -21.00 | 2189.8 | 3034.3 | 5224.1 | 3132.0 | -7.3 | 3124.7 | | |
| -21.50 | 2274.2 | 3159.4 | 5433.6 | 3257.6 | -7.3 | 3250.3 | | |
| -22.00 | 2642.9 | 3281.1 | 5924.0 | 3551.6 | -7.3 | 3544.3 | | |
| -22.50 | 2427.0 | 3406.3 | 5833.3 | 3497.2 | -7.3 | 3489.8 | | |
| -23.00 | 2440.1 | 3531.4 | 5971.5 | 3580.0 | -7.3 | 3572.7 | | |
| -23.50 | 1961.0 | 3656.5 | 5617.4 | 3367.8 | -7.3 | 3360.5 | | |
| -24.00 | 1922.6 | 3781.6 | 5704.2 | 3419.8 | -7.3 | 3412.5 | | |
| -24.50 | 1902.3 | 3903.9 | 5806.2 | 3480.9 | -7.3 | 3473.6 | | |
| -25.00 | 1860.3 | 4021.4 | 5881.8 | 3526.2 | -7.3 | 3518.9 | | |
| -25.50 | 1609.6 | 4155.9 | 5765.5 | 3456.5 | -7.3 | 3449.2 | | |
| -26.00 | 1858.7 | 4281.5 | 6140.2 | 3681.2 | -7.3 | 3673.9 | | |
| -26.50 | 2265.9 | 4390.3 | 6656.2 | 3990.6 | -7.3 | 3983.3 | | |
| -27.00 | 2367.7 | 4515.4 | 6883.1 | 4126.6 | -7.3 | 4119.3 | | |
| -27.50 | 2424.7 | 4640.5 | 7065.2 | 4235.7 | -7.3 | 4228.4 | | |
| -28.00 | 2440.4 | 4765.7 | 7206.1 | 4320.2 | -7.3 | 4312.9 | | |
| -28.50 | 2704.0 | 4890.8 | 7594.8 | 4553.2 | -7.3 | 4545.9 | | |
| -29.00 | 2838.3 | 5015.9 | 7854.2 | 4708.7 | -7.3 | 4701.4 | | |
| -29.50 | 1489.9 | 5141.0 | 6630.9 | 3975.3 | -7.3 | 3968.0 | | |
| -30.00 | 1230.7 | 5266.1 | 6496.8 | 3895.0 | -7.3 | 3887.7 | | |
| 312.S03 | 3.78 | -6.00 | 583.8 | 822.7 | 1406.5 | 843.2 | 0.0 | 843.2 |
| | | -6.50 | 518.6 | 917.6 | 1436.3 | 861.1 | 0.0 | 861.1 |
| | | -7.00 | 398.1 | 1028.8 | 1426.9 | 855.5 | 0.0 | 855.5 |
| | | -7.50 | 589.7 | 1096.3 | 1686.0 | 1010.8 | 0.0 | 1010.8 |
| | | -8.00 | 1623.7 | 1169.8 | 2793.5 | 1674.8 | 0.0 | 1674.8 |
| -8.50 | 1517.1 | 1294.9 | 2812.0 | 1685.8 | 0.0 | 1685.8 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|--------------------------|--------------------------------|
| | | | R _{z,real} [kN] | R _{z,real} [kN] | R _{z,real} [kN] | R _{z,d} [kN] | F _{hkd} [kN] | R _{z,netto;d} [kN] |
| 312.S03 | 3.78 | -9.00 | 1615.5 | 1420.0 | 3035.5 | 1819.8 | 0.0 | 1819.8 |
| | | -9.50 | 1607.8 | 1545.1 | 3153.0 | 1890.3 | 0.0 | 1890.3 |
| | | -10.00 | 1720.3 | 1670.3 | 3390.6 | 2032.7 | 0.0 | 2032.7 |
| | | -10.50 | 1950.1 | 1793.9 | 3744.0 | 2244.6 | 0.0 | 2244.6 |
| | | -11.00 | 1717.0 | 1910.5 | 3627.5 | 2174.8 | 0.0 | 2174.8 |
| | | -11.50 | 1778.5 | 2035.6 | 3814.2 | 2286.7 | 0.0 | 2286.7 |
| | | -12.00 | 1840.2 | 2160.7 | 4000.8 | 2398.6 | 0.0 | 2398.6 |
| | | -12.50 | 1707.0 | 2285.8 | 3992.8 | 2393.8 | 0.0 | 2393.8 |
| | | -13.00 | 1645.8 | 2407.3 | 4053.0 | 2429.9 | 0.0 | 2429.9 |
| | | -13.50 | 1836.1 | 2495.5 | 4331.6 | 2596.9 | 0.0 | 2596.9 |
| | | -14.00 | 1852.4 | 2595.6 | 4448.0 | 2666.7 | 0.0 | 2666.7 |
| | | -14.50 | 1792.2 | 2695.7 | 4487.8 | 2690.5 | 0.0 | 2690.5 |
| | | -15.00 | 1688.2 | 2791.4 | 4479.6 | 2685.6 | 0.0 | 2685.6 |
| | | -15.50 | 1667.9 | 2891.5 | 4559.4 | 2733.5 | 0.0 | 2733.5 |
| | | -16.00 | 1630.2 | 2988.3 | 4618.5 | 2768.9 | 0.0 | 2768.9 |
| | | -16.50 | 1539.2 | 3088.4 | 4627.6 | 2774.3 | 0.0 | 2774.3 |
| | | -17.00 | 1477.9 | 3180.9 | 4658.8 | 2793.0 | 0.0 | 2793.0 |
| | | -17.50 | 1525.2 | 3253.2 | 4778.4 | 2864.8 | 0.0 | 2864.8 |
| | | -18.00 | 945.4 | 3330.8 | 4276.2 | 2563.7 | 0.0 | 2563.7 |
| | | -18.50 | 945.7 | 3428.2 | 4374.0 | 2622.3 | 0.0 | 2622.3 |
| | | -19.00 | 940.6 | 3530.6 | 4471.2 | 2680.6 | 0.0 | 2680.6 |
| | | -19.50 | 788.6 | 3636.8 | 4425.5 | 2653.2 | 0.0 | 2653.2 |
| | | -20.00 | 636.3 | 3739.1 | 4375.3 | 2623.1 | 0.0 | 2623.1 |
| | | -20.50 | 1120.5 | 3828.6 | 4949.1 | 2967.1 | 0.0 | 2967.1 |
| | | -21.00 | 1325.4 | 3927.5 | 5252.9 | 3149.2 | 0.0 | 3149.2 |
| | | -21.50 | 1433.6 | 4019.4 | 5453.1 | 3269.2 | 0.0 | 3269.2 |
| | | -22.00 | 1640.1 | 4123.3 | 5763.3 | 3455.2 | 0.0 | 3455.2 |
| | | -22.50 | 1716.0 | 4245.3 | 5961.3 | 3573.9 | 0.0 | 3573.9 |
| | | -23.00 | 1750.6 | 4368.2 | 6118.8 | 3668.3 | 0.0 | 3668.3 |
| | | -23.50 | 1778.2 | 4487.4 | 6265.6 | 3756.4 | 0.0 | 3756.4 |
| -24.00 | 2001.0 | 4596.6 | 6597.6 | 3955.4 | 0.0 | 3955.4 | | |
| -24.50 | 2029.3 | 4721.8 | 6751.1 | 4047.4 | 0.0 | 4047.4 | | |
| -25.00 | 1130.0 | 4846.9 | 5976.9 | 3583.3 | 0.0 | 3583.3 | | |
| -25.50 | 993.6 | 4964.4 | 5958.0 | 3571.9 | 0.0 | 3571.9 | | |
| -26.00 | 818.5 | 5069.4 | 5887.8 | 3529.9 | 0.0 | 3529.9 | | |
| -26.50 | 687.8 | 5191.8 | 5879.6 | 3524.9 | 0.0 | 3524.9 | | |
| -27.00 | 500.1 | 5314.2 | 5814.2 | 3485.7 | 0.0 | 3485.7 | | |
| -27.50 | 478.1 | 5379.8 | 5857.8 | 3511.9 | 0.0 | 3511.9 | | |
| -28.00 | 467.4 | 5431.8 | 5899.2 | 3536.7 | 0.0 | 3536.7 | | |
| -28.50 | 466.1 | 5471.7 | 5937.8 | 3559.8 | 0.0 | 3559.8 | | |
| -29.00 | 471.9 | 5510.9 | 5982.8 | 3586.8 | 0.0 | 3586.8 | | |
| -29.50 | 532.8 | 5556.5 | 6089.3 | 3650.7 | 0.0 | 3650.7 | | |
| 19-1008_43 | 9.88 | -6.00 | 835.3 | 723.2 | 1558.5 | 934.3 | 0.0 | 934.3 |
| | | -6.50 | 1326.8 | 774.2 | 2101.1 | 1259.6 | 0.0 | 1259.6 |
| | | -7.00 | 1350.2 | 871.4 | 2221.6 | 1331.9 | 0.0 | 1331.9 |
| | | -7.50 | 1378.9 | 964.7 | 2343.7 | 1405.1 | 0.0 | 1405.1 |
| | | -8.00 | 1415.6 | 1061.9 | 2477.5 | 1485.3 | 0.0 | 1485.3 |
| | | -8.50 | 1455.9 | 1152.5 | 2608.4 | 1563.8 | 0.0 | 1563.8 |
| | | -9.00 | 1498.9 | 1245.2 | 2744.1 | 1645.1 | 0.0 | 1645.1 |
| | | -9.50 | 1522.3 | 1340.0 | 2862.4 | 1716.0 | 0.0 | 1716.0 |
| | | -10.00 | 1741.3 | 1426.5 | 3167.8 | 1899.2 | 0.0 | 1899.2 |
| | | -10.50 | 1894.4 | 1530.6 | 3425.0 | 2053.4 | 0.0 | 2053.4 |
| | | -11.00 | 1798.3 | 1655.7 | 3454.0 | 2070.8 | 0.0 | 2070.8 |
| | | -11.50 | 1767.6 | 1780.8 | 3548.5 | 2127.4 | 0.0 | 2127.4 |
| | | -12.00 | 1741.4 | 1905.8 | 3647.3 | 2186.6 | 0.0 | 2186.6 |
| | | -12.50 | 1641.5 | 2029.9 | 3671.4 | 2201.1 | 0.0 | 2201.1 |
| | | -13.00 | 1607.4 | 2122.3 | 3729.6 | 2236.0 | 0.0 | 2236.0 |
| | | -13.50 | 1726.0 | 2201.7 | 3927.7 | 2354.7 | 0.0 | 2354.7 |
| | | -14.00 | 1736.1 | 2294.4 | 4030.5 | 2416.4 | 0.0 | 2416.4 |
| | | -14.50 | 1656.3 | 2394.5 | 4050.8 | 2428.5 | 0.0 | 2428.5 |
| | | -15.00 | 2074.2 | 2482.0 | 4556.3 | 2731.6 | 0.0 | 2731.6 |
| | | -15.50 | 2100.7 | 2591.0 | 4691.7 | 2812.8 | 0.0 | 2812.8 |
| -16.00 | 1947.2 | 2711.3 | 4658.5 | 2792.9 | 0.0 | 2792.9 | | |
| -16.50 | 1790.2 | 2836.4 | 4626.6 | 2773.8 | 0.0 | 2773.8 | | |
| -17.00 | 1356.4 | 2961.5 | 4317.9 | 2588.7 | 0.0 | 2588.7 | | |
| -17.50 | 1245.2 | 3082.0 | 4327.2 | 2594.2 | 0.0 | 2594.2 | | |
| -18.00 | 1214.4 | 3191.1 | 4405.5 | 2641.2 | 0.0 | 2641.2 | | |
| -18.50 | 1167.2 | 3288.7 | 4455.9 | 2671.4 | 0.0 | 2671.4 | | |
| -19.00 | 1108.6 | 3386.5 | 4495.1 | 2694.9 | 0.0 | 2694.9 | | |
| -19.50 | 1143.7 | 3465.6 | 4609.3 | 2763.4 | 0.0 | 2763.4 | | |
| -20.00 | 1280.4 | 3547.2 | 4827.6 | 2894.2 | 0.0 | 2894.2 | | |
| -20.50 | 1343.2 | 3650.3 | 4993.5 | 2993.7 | 0.0 | 2993.7 | | |
| -21.00 | 1413.0 | 3769.9 | 5182.9 | 3107.2 | 0.0 | 3107.2 | | |
| -21.50 | 1825.8 | 3868.8 | 5694.6 | 3414.0 | 0.0 | 3414.0 | | |
| -22.00 | 2449.7 | 3980.9 | 6430.6 | 3855.3 | 0.0 | 3855.3 | | |
| -22.50 | 2000.5 | 4106.0 | 6106.5 | 3661.0 | 0.0 | 3661.0 | | |
| 328.S02 | 10.17 | -6.00 | 1077.5 | 1234.9 | 2312.4 | 1386.3 | 0.0 | 1386.3 |
| | | -6.50 | 917.3 | 1335.0 | 2252.3 | 1350.3 | 0.0 | 1350.3 |
| | | -7.00 | 1062.7 | 1403.7 | 2466.4 | 1478.6 | 0.0 | 1478.6 |
| | | -7.50 | 1116.7 | 1490.8 | 2607.5 | 1563.2 | 0.0 | 1563.2 |
| | | -8.00 | 1151.6 | 1586.8 | 2738.4 | 1641.7 | 0.0 | 1641.7 |
| | | -8.50 | 1147.5 | 1685.3 | 2832.8 | 1698.3 | 0.0 | 1698.3 |
| | | -9.00 | 1262.1 | 1781.4 | 3043.5 | 1824.6 | 0.0 | 1824.6 |
| | | -9.50 | 1468.4 | 1863.6 | 3332.0 | 1997.6 | 0.0 | 1997.6 |
| | | -10.00 | 1647.2 | 1956.4 | 3603.6 | 2160.4 | 0.0 | 2160.4 |
| | | -10.50 | 1733.7 | 2053.8 | 3787.5 | 2270.7 | 0.0 | 2270.7 |
| | | -11.00 | 1762.6 | 2165.7 | 3928.3 | 2355.1 | 0.0 | 2355.1 |
| | | -11.50 | 1768.9 | 2280.7 | 4049.6 | 2427.8 | 0.0 | 2427.8 |
| | | -12.00 | 1765.2 | 2391.8 | 4157.0 | 2492.2 | 0.0 | 2492.2 |
| | | -12.50 | 1810.6 | 2492.2 | 4302.8 | 2579.6 | 0.0 | 2579.6 |
| -13.00 | 1868.4 | 2590.1 | 4458.6 | 2673.0 | 0.0 | 2673.0 | | |
| -13.50 | 1546.7 | 2689.2 | 4235.9 | 2539.5 | 0.0 | 2539.5 | | |
| -14.00 | 1487.6 | 2789.2 | 4276.9 | 2564.1 | 0.0 | 2564.1 | | |
| -14.50 | 1485.4 | 2886.4 | 4371.8 | 2621.0 | 0.0 | 2621.0 | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
| | | | $R_{b,real}$ [kN] | $R_{s,real}$ [kN] | $R_{c,real}$ [kN] | $R_{b;d}$ [kN] | $F_{nk;d}$ [kN] | $R_{c,netto;d}$ [kN] |
| 328.S02 | 10.17 | -15.00 | 1446.8 | 2987.5 | 4434.3 | 2658.5 | 0.0 | 2658.5 |
| | | -15.50 | 1354.8 | 3087.4 | 4442.3 | 2663.2 | 0.0 | 2663.2 |
| | | -16.00 | 1425.7 | 3186.6 | 4612.3 | 2765.1 | 0.0 | 2765.1 |
| | | -16.50 | 1507.8 | 3290.3 | 4798.1 | 2876.6 | 0.0 | 2876.6 |
| | | -17.00 | 1550.0 | 3415.5 | 4965.4 | 2976.9 | 0.0 | 2976.9 |
| | | -17.50 | 1493.0 | 3540.6 | 5033.6 | 3017.7 | 0.0 | 3017.7 |
| | | -18.00 | 941.5 | 3684.2 | 4625.7 | 2773.2 | 0.0 | 2773.2 |
| | | -18.50 | 1740.9 | 3773.2 | 5514.1 | 3305.8 | 0.0 | 3305.8 |
| | | -19.00 | 1778.9 | 3885.2 | 5664.2 | 3395.8 | 0.0 | 3395.8 |
| | | -19.50 | 1968.5 | 4004.7 | 5973.2 | 3581.1 | 0.0 | 3581.1 |
| | | -20.00 | 2067.5 | 4129.8 | 6197.3 | 3715.4 | 0.0 | 3715.4 |
| | | -20.50 | 2282.0 | 4254.9 | 6536.9 | 3919.0 | 0.0 | 3919.0 |
| | | -21.00 | 2376.8 | 4380.0 | 6756.8 | 4050.9 | 0.0 | 4050.9 |
| | | -21.50 | 2490.7 | 4505.1 | 6995.9 | 4194.2 | 0.0 | 4194.2 |
| | | -22.00 | 2271.8 | 4630.3 | 6902.0 | 4137.9 | 0.0 | 4137.9 |
| | | -22.50 | 2358.9 | 4755.4 | 7114.3 | 4265.2 | 0.0 | 4265.2 |
| | | -23.00 | 2150.6 | 4880.5 | 7031.1 | 4215.3 | 0.0 | 4215.3 |
| | | -23.50 | 2159.3 | 5005.6 | 7164.9 | 4295.5 | 0.0 | 4295.5 |
| | | -24.00 | 2052.2 | 5130.7 | 7182.9 | 4306.3 | 0.0 | 4306.3 |
| | | -24.50 | 2073.8 | 5235.0 | 7308.8 | 4381.8 | 0.0 | 4381.8 |
| | | -25.00 | 1957.7 | 5335.1 | 7292.8 | 4372.2 | 0.0 | 4372.2 |
| -25.50 | 2064.4 | 5433.2 | 7497.6 | 4494.9 | 0.0 | 4494.9 | | |
| -26.00 | 1625.6 | 5533.3 | 7158.9 | 4291.9 | 0.0 | 4291.9 | | |
| -26.50 | 1703.8 | 5638.9 | 7342.7 | 4402.1 | 0.0 | 4402.1 | | |

REKENGEGEVENS SI Ø610/850 druk

Berekening : Ontwerpend
Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2
Sondering(en) : 19-1008_1, 19-1008_6, 166.S01, 19-1008_11, 19-1008_12
: 19-1008_17, 19-1008_20, 19-1008_21, 251.S01, 19-1008_29
: 283.S02, 19-1008_35, 312.S03, 19-1008_43, 328.S02

Stijf bouwwerk : NEE
Paalgroep : NEE
Aantal sonderingen : 15
Factor $\xi_{3(n-1)}$: 1.39 (handmatig)
Factor $\xi_{3(gem)}$: 1.39 (handmatig)
Factor $\xi_{4(min)}$: 1.39 (handmatig)
Weerstandsfactor γ_R : 1.20
 $\gamma_{F;nk}$: 1.0
 $R_{b,real,max;i}$ begrenzen op $0.75 * R_{b,real,max;i}$: NEE
UGT draagvermogen zonder negatieve kleef : NEE

Paal : SI Ø610/850
Niveau paalkop [m] : N.A.P. 0.00
Bovenbel. [kN/m²] : 0.00

PAALPUNTNIVEAUS SI Ø610/850

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|--------------------|-------------------|--------------------|
| 1 | -7.00 | -30.00 | 0.50 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø610/850 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering | 19-1008_1 | 19-1008_6 | 166.S01 | 19-1008_11 | 19-1008_12 | 19-1008_17 |
|------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| Niveau [m] | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] |
| -7.00 | -67 | 3372 | 2403 | 106 | 1755 | -34 |
| -7.50 | -8 | 3882 | 2529 | 240 | 1722 | -87 |
| -8.00 | 8 | 4221 | 2678 | 279 | 1628 | -59 |
| -8.50 | 17 | 4466 | 2837 | 314 | 1577 | -31 |
| -9.00 | 149 | 4590 | 2887 | 354 | 1597 | -10 |
| -9.50 | 190 | 4714 | 2991 | 356 | 1622 | 387 |
| -10.00 | 232 | 5436 | 2873 | 401 | 1624 | 207 |
| -10.50 | 311 | 5511 | 2925 | 433 | 1652 | 693 |
| -11.00 | 444 | 5502 | 3017 | 475 | 1642 | 1534 |
| -11.50 | 511 | 5629 | 2985 | 492 | 1692 | 1699 |
| -12.00 | 553 | 5716 | 2976 | 455 | 1704 | 1612 |
| -12.50 | 1013 | 5752 | 3029 | 1101 | 1714 | 1756 |
| -13.00 | 1116 | 5798 | 3253 | 1342 | 1751 | 1810 |
| -13.50 | 1259 | 6087 | 3635 | 1453 | 1833 | 1894 |
| -14.00 | 1478 | 6180 | 3778 | 1561 | 1869 | 1990 |
| -14.50 | 1731 | 6272 | 3915 | 1658 | 1900 | 2296 |
| -15.00 | 1836 | 6035 | 4057 | 1742 | 1930 | 2502 |
| -15.50 | 1790 | 5033 | 4455 | 1835 | 2022 | 1857 |
| -16.00 | 2041 | 5019 | 4621 | 2063 | 2071 | 1866 |
| -16.50 | 2198 | 5080 | 4714 | 2158 | 2120 | 1951 |
| -17.00 | 2641 | 5070 | 4780 | 2251 | 2183 | 2064 |
| -17.50 | 3099 | 5062 | 4919 | 2771 | 2292 | 2003 |
| -18.00 | 3189 | 5498 | 5056 | 3232 | 2529 | 1954 |
| -18.50 | 2898 | 6133 | 5186 | 3433 | 2621 | 2358 |
| -19.00 | 2917 | 6248 | 5284 | 3547 | 3006 | 2449 |
| -19.50 | 2887 | 6366 | 5347 | 3616 | 3224 | 2552 |
| -20.00 | 2860 | 6495 | 0 | 3761 | 3505 | 2672 |
| -20.50 | 2992 | 6609 | 0 | 3283 | 3478 | 2851 |
| -21.00 | 3114 | 6890 | 0 | 3352 | 3892 | 2798 |
| -21.50 | 4304 | 0 | 0 | 3371 | 4038 | 3154 |
| -22.00 | 5555 | 0 | 0 | 3242 | 4197 | 3186 |
| -22.50 | 5648 | 0 | 0 | 3239 | 4290 | 3246 |
| -23.00 | 5740 | 0 | 0 | 3221 | 4320 | 3257 |
| -23.50 | 5833 | 0 | 0 | 3495 | 4047 | 3275 |
| -24.00 | 5926 | 0 | 0 | 3581 | 4053 | 3357 |
| -24.50 | 6019 | 0 | 0 | 3628 | 3991 | 3414 |
| -25.00 | 6112 | 0 | 0 | 3691 | 3890 | 3488 |
| -25.50 | 6204 | 0 | 0 | 4470 | 3914 | 3562 |
| -26.00 | 6297 | 0 | 0 | 4567 | 3993 | 3663 |
| -26.50 | 6390 | 0 | 0 | 4643 | 4066 | 2996 |
| -27.00 | 6483 | 0 | 0 | 4755 | 4128 | 3021 |
| -27.50 | 6576 | 0 | 0 | 4906 | 4163 | 3079 |
| -28.00 | 6668 | 0 | 0 | 5270 | 4810 | 3123 |
| -28.50 | 6761 | 0 | 0 | 5485 | 5278 | 3111 |
| -29.00 | 6854 | 0 | 0 | 5847 | 0 | 3015 |
| -29.50 | 6947 | 0 | 0 | 6505 | 0 | 3656 |
| -30.00 | 0 | 0 | 0 | 6706 | 0 | 4113 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø610/850 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | 19-1008_20 | 19-1008_21 | 251.S01 | 19-1008_29 | 283.S02 | 19-1008_35 |
|--------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| [m] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] |
| -7.00 | 644 | 863 | 778 | 2033 | 1532 | 1386 |
| -7.50 | 580 | 924 | 754 | 2154 | 1673 | 1476 |
| -8.00 | 602 | 996 | 746 | 2244 | 1746 | 1510 |
| -8.50 | 647 | 986 | 736 | 2070 | 1802 | 1533 |
| -9.00 | 675 | 1030 | 1137 | 1521 | 1606 | 1588 |
| -9.50 | 692 | 1190 | 1268 | 1589 | 1653 | 1660 |
| -10.00 | 657 | 1258 | 1345 | 1656 | 1701 | 1738 |
| -10.50 | 809 | 1319 | 1397 | 1689 | 1740 | 1811 |
| -11.00 | 819 | 1356 | 1428 | 1694 | 1780 | 1846 |
| -11.50 | 786 | 1403 | 1502 | 1748 | 1783 | 1867 |
| -12.00 | 828 | 1466 | 1784 | 1818 | 2165 | 1896 |
| -12.50 | 861 | 1441 | 1641 | 1831 | 2343 | 2096 |
| -13.00 | 873 | 1529 | 1728 | 1820 | 2549 | 2244 |
| -13.50 | 975 | 1590 | 1809 | 1855 | 2696 | 2371 |
| -14.00 | 980 | 1545 | 1858 | 1888 | 2824 | 2610 |
| -14.50 | 1013 | 1577 | 1854 | 1917 | 2880 | 2617 |
| -15.00 | 1052 | 1676 | 1817 | 1983 | 2947 | 2708 |
| -15.50 | 1081 | 1592 | 2704 | 2046 | 3174 | 2793 |
| -16.00 | 1114 | 1602 | 2534 | 2052 | 3419 | 2858 |
| -16.50 | 1140 | 1549 | 2595 | 2085 | 3628 | 2862 |
| -17.00 | 1186 | 1591 | 2712 | 2194 | 4002 | 2924 |
| -17.50 | 1361 | 1703 | 2781 | 2890 | 4033 | 3147 |
| -18.00 | 1424 | 1732 | 2790 | 3199 | 4179 | 3241 |
| -18.50 | 1476 | 1764 | 2489 | 3209 | 4307 | 3423 |
| -19.00 | 1584 | 1801 | 2533 | 3087 | 4433 | 3502 |
| -19.50 | 1669 | 1818 | 2509 | 4145 | 4533 | 3659 |
| -20.00 | 1665 | 1833 | 2504 | 3788 | 4553 | 3983 |
| -20.50 | 1658 | 1853 | 2528 | 3650 | 4906 | 4094 |
| -21.00 | 1671 | 1884 | 2573 | 3552 | 5158 | 4215 |
| -21.50 | 1702 | 1913 | 2596 | 3486 | 5289 | 4482 |
| -22.00 | 1733 | 1944 | 2612 | 3429 | 5388 | 4582 |
| -22.50 | 1769 | 1973 | 2699 | 3340 | 5484 | 4701 |
| -23.00 | 2148 | 2000 | 2748 | 3376 | 5681 | 4410 |
| -23.50 | 2310 | 2042 | 2887 | 3466 | 4956 | 4475 |
| -24.00 | 2472 | 2071 | 2947 | 3538 | 4283 | 4561 |
| -24.50 | 2603 | 2101 | 3025 | 3563 | 4156 | 4633 |
| -25.00 | 2694 | 2131 | 3263 | 3592 | 4125 | 4681 |
| -25.50 | 2791 | 2162 | 3713 | 3654 | 4032 | 4570 |
| -26.00 | 2907 | 2191 | 4578 | 3696 | 4008 | 4891 |
| -26.50 | 2817 | 2221 | 4481 | 3743 | 3975 | 5319 |
| -27.00 | 2897 | 2250 | 4620 | 3784 | 4034 | 5494 |
| -27.50 | 2940 | 2296 | 4609 | 3834 | 4008 | 5627 |
| -28.00 | 3017 | 2329 | 4253 | 3877 | 4046 | 5723 |
| -28.50 | 3098 | 2359 | 4133 | 3985 | 4081 | 6007 |
| -29.00 | 3161 | 2400 | 4106 | 4351 | 4110 | 5097 |
| -29.50 | 3225 | 2440 | 4067 | 4318 | 0 | 4994 |
| -30.00 | 3139 | 2476 | 4028 | 4271 | 0 | 4864 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø610/850 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Sondering 312.S03 19-1008_43 328.S02

| Niveau [m] | F _{netto;d} [kN] | F _{netto;d} [kN] | F _{netto;d} [kN] |
|---------------|------------------------------|------------------------------|------------------------------|
| -7.00 | 1129 | 1863 | 1995 |
| -7.50 | 1533 | 1963 | 2102 |
| -8.00 | 2177 | 2063 | 2199 |
| -8.50 | 2334 | 2160 | 2261 |
| -9.00 | 2505 | 2260 | 2509 |
| -9.50 | 2576 | 2344 | 2671 |
| -10.00 | 2759 | 2659 | 2873 |
| -10.50 | 2789 | 2723 | 3038 |
| -11.00 | 2922 | 2793 | 3180 |
| -11.50 | 3052 | 2903 | 3252 |
| -12.00 | 3198 | 2998 | 3356 |
| -12.50 | 3160 | 3010 | 3464 |
| -13.00 | 3331 | 3054 | 3287 |
| -13.50 | 3532 | 3216 | 3349 |
| -14.00 | 3603 | 3295 | 3414 |
| -14.50 | 3556 | 3294 | 3494 |
| -15.00 | 3590 | 3732 | 3543 |
| -15.50 | 3638 | 3660 | 3519 |
| -16.00 | 3713 | 3554 | 3672 |
| -16.50 | 3704 | 3386 | 3825 |
| -17.00 | 3718 | 3370 | 3956 |
| -17.50 | 3238 | 3430 | 3997 |
| -18.00 | 3338 | 3481 | 3632 |
| -18.50 | 3411 | 3511 | 4395 |
| -19.00 | 3482 | 3530 | 4499 |
| -19.50 | 3422 | 3625 | 4746 |
| -20.00 | 3443 | 3827 | 4908 |
| -20.50 | 3866 | 3937 | 5184 |
| -21.00 | 4116 | 4121 | 5348 |
| -21.50 | 4319 | 4655 | 5280 |
| -22.00 | 4521 | 4777 | 5436 |
| -22.50 | 4667 | 0 | 5386 |
| -23.00 | 4774 | 0 | 5520 |
| -23.50 | 4944 | 0 | 5590 |
| -24.00 | 5177 | 0 | 5668 |
| -24.50 | 4574 | 0 | 5787 |
| -25.00 | 4521 | 0 | 5707 |
| -25.50 | 4449 | 0 | 5501 |
| -26.00 | 4444 | 0 | 0 |
| -26.50 | 4436 | 0 | 0 |
| -27.00 | 4401 | 0 | 0 |
| -27.50 | 4429 | 0 | 0 |
| -28.00 | 4458 | 0 | 0 |
| -28.50 | 4487 | 0 | 0 |
| -29.00 | 4563 | 0 | 0 |
| -29.50 | 0 | 0 | 0 |
| -30.00 | 0 | 0 | 0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

SAMENVATTINGSTABEL SI Ø610/850 druk (n=1)

Uitgangspunten

- paal : SI Ø610/850
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie
 - schachtafmeting : 730 mm
 Paalklassefactor α_p : 0.63
 Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
 Correlatiefactor $\xi_{s(n=1)}$: 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
| | | | $R_{e,real}$ [kN] | $R_{s,real}$ [kN] | $R_{c,real}$ [kN] | $R_{e;d}$ [kN] | $F_{nk;d}$ [kN] | $R_{z,netto;d}$ [kN] |
| 19-1008_1 | 2.12 | -7.00 | 126.5 | 0.0 | 126.5 | 75.8 | -142.7 | -66.9 |
| | | -7.50 | 221.6 | 2.9 | 224.5 | 134.6 | -142.7 | -8.1 |
| | | -8.00 | 215.1 | 37.2 | 252.2 | 151.2 | -142.7 | 8.5 |
| | | -8.50 | 190.7 | 75.9 | 266.6 | 159.8 | -142.7 | 17.1 |
| | | -9.00 | 399.3 | 87.6 | 486.9 | 291.9 | -142.7 | 149.1 |
| | | -9.50 | 403.0 | 151.7 | 554.7 | 332.5 | -142.7 | 189.8 |
| | | -10.00 | 416.9 | 208.7 | 625.6 | 375.1 | -142.7 | 232.3 |
| | | -10.50 | 481.1 | 275.4 | 756.5 | 453.5 | -142.7 | 310.8 |
| | | -11.00 | 657.5 | 320.8 | 978.2 | 586.5 | -142.7 | 443.7 |
| | | -11.50 | 691.3 | 399.6 | 1090.9 | 654.0 | -142.7 | 511.3 |
| | | -12.00 | 658.8 | 501.0 | 1159.8 | 695.3 | -142.7 | 552.6 |
| | | -12.50 | 1360.0 | 568.3 | 1928.3 | 1156.0 | -142.7 | 1013.3 |
| | | -13.00 | 1422.5 | 676.8 | 2099.3 | 1258.6 | -142.7 | 1115.8 |
| | | -13.50 | 1552.7 | 785.2 | 2337.9 | 1401.6 | -142.7 | 1258.9 |
| | | -14.00 | 1825.6 | 878.6 | 2704.1 | 1621.2 | -142.7 | 1478.4 |
| | | -14.50 | 2124.2 | 1001.7 | 3125.8 | 1874.0 | -142.7 | 1731.3 |
| | | -15.00 | 2186.3 | 1113.8 | 3300.1 | 1978.5 | -142.7 | 1835.7 |
| | | -15.50 | 1986.3 | 1236.7 | 3223.0 | 1932.3 | -142.7 | 1789.5 |
| | | -16.00 | 2300.4 | 1341.9 | 3642.3 | 2183.6 | -142.7 | 2040.9 |
| | | -16.50 | 2446.6 | 1457.8 | 3904.4 | 2340.8 | -142.7 | 2198.0 |
| | | -17.00 | 3066.9 | 1575.6 | 4642.6 | 2783.3 | -142.7 | 2640.6 |
| | | -17.50 | 3693.9 | 1713.5 | 5407.4 | 3241.8 | -142.7 | 3099.1 |
| | | -18.00 | 3688.4 | 1868.3 | 5556.8 | 3331.4 | -142.7 | 3188.7 |
| | | -18.50 | 3048.8 | 2023.2 | 5072.0 | 3040.7 | -142.7 | 2898.0 |
| | | -19.00 | 2925.1 | 2178.0 | 5103.0 | 3059.4 | -142.7 | 2916.6 |
| | | -19.50 | 2721.1 | 2332.8 | 5053.9 | 3029.9 | -142.7 | 2887.2 |
| | | -20.00 | 2484.0 | 2523.8 | 5007.9 | 3002.3 | -142.7 | 2859.6 |
| | | -20.50 | 2506.7 | 2722.1 | 5228.8 | 3134.8 | -142.7 | 2992.0 |
| | | -21.00 | 2503.8 | 2928.5 | 5432.3 | 3256.8 | -142.7 | 3114.1 |
| -21.50 | 4346.4 | 3070.6 | 7417.0 | 4446.6 | -142.7 | 4303.9 | | |
| -22.00 | 6278.1 | 3225.4 | 9503.5 | 5697.6 | -142.7 | 5554.8 | | |
| -22.50 | 6278.1 | 3380.2 | 9658.3 | 5790.4 | -142.7 | 5647.6 | | |
| -23.00 | 6278.1 | 3535.0 | 9813.1 | 5883.2 | -142.7 | 5740.4 | | |
| -23.50 | 6278.1 | 3689.8 | 9967.9 | 5976.0 | -142.7 | 5833.2 | | |
| -24.00 | 6278.1 | 3844.6 | 10122.7 | 6068.8 | -142.7 | 5926.0 | | |
| -24.50 | 6278.1 | 3999.4 | 10277.5 | 6161.6 | -142.7 | 6018.8 | | |
| -25.00 | 6278.1 | 4154.2 | 10432.3 | 6254.4 | -142.7 | 6111.7 | | |
| -25.50 | 6278.1 | 4309.1 | 10587.1 | 6347.2 | -142.7 | 6204.5 | | |
| -26.00 | 6278.1 | 4463.9 | 10741.9 | 6440.0 | -142.7 | 6297.3 | | |
| -26.50 | 6278.1 | 4618.7 | 10896.7 | 6532.8 | -142.7 | 6390.1 | | |
| -27.00 | 6278.1 | 4773.5 | 11051.5 | 6625.6 | -142.7 | 6482.9 | | |
| -27.50 | 6278.1 | 4928.3 | 11206.3 | 6718.4 | -142.7 | 6575.7 | | |
| -28.00 | 6278.1 | 5083.1 | 11361.1 | 6811.2 | -142.7 | 6668.5 | | |
| -28.50 | 6278.1 | 5237.9 | 11515.9 | 6904.0 | -142.7 | 6761.3 | | |
| -29.00 | 6278.1 | 5392.7 | 11670.7 | 6996.8 | -142.7 | 6854.1 | | |
| -29.50 | 6278.1 | 5547.5 | 11825.5 | 7089.7 | -142.7 | 6946.9 | | |
| 19-1008_6 | 11.00 | -7.00 | 3761.5 | 1862.4 | 5623.9 | 3371.7 | 0.0 | 3371.7 |
| | | -7.50 | 4457.9 | 2017.2 | 6475.0 | 3881.9 | 0.0 | 3881.9 |
| | | -8.00 | 4868.9 | 2172.0 | 7040.8 | 4221.1 | 0.0 | 4221.1 |
| | | -8.50 | 5122.0 | 2326.8 | 7448.8 | 4465.7 | 0.0 | 4465.7 |
| | | -9.00 | 5174.4 | 2481.6 | 7656.0 | 4589.9 | 0.0 | 4589.9 |
| | | -9.50 | 5227.2 | 2636.4 | 7863.6 | 4714.4 | 0.0 | 4714.4 |
| | | -10.00 | 6275.5 | 2791.2 | 9066.7 | 5435.6 | 0.0 | 5435.6 |
| | | -10.50 | 6245.8 | 2946.0 | 9191.8 | 5510.7 | 0.0 | 5510.7 |
| | | -11.00 | 6076.5 | 3100.8 | 9177.3 | 5502.0 | 0.0 | 5502.0 |
| | | -11.50 | 6133.6 | 3255.6 | 9389.2 | 5629.0 | 0.0 | 5629.0 |
| | | -12.00 | 6124.0 | 3410.4 | 9534.4 | 5716.0 | 0.0 | 5716.0 |
| | | -12.50 | 6028.9 | 3565.2 | 9594.1 | 5751.9 | 0.0 | 5751.9 |
| | | -13.00 | 5951.5 | 3720.0 | 9671.5 | 5798.3 | 0.0 | 5798.3 |
| | | -13.50 | 6278.1 | 3874.8 | 10152.9 | 6086.9 | 0.0 | 6086.9 |
| | | -14.00 | 6278.1 | 4029.6 | 10307.7 | 6179.7 | 0.0 | 6179.7 |
| | | -14.50 | 6278.1 | 4184.4 | 10462.5 | 6272.5 | 0.0 | 6272.5 |
| | | -15.00 | 5727.2 | 4339.2 | 10066.4 | 6035.0 | 0.0 | 6035.0 |
| | | -15.50 | 3900.7 | 4494.0 | 8394.7 | 5032.8 | 0.0 | 5032.8 |
| | | -16.00 | 3722.5 | 4648.8 | 8371.4 | 5018.8 | 0.0 | 5018.8 |
| | | -16.50 | 3669.6 | 4803.6 | 8473.2 | 5079.8 | 0.0 | 5079.8 |
| | | -17.00 | 3498.7 | 4958.4 | 8457.1 | 5070.2 | 0.0 | 5070.2 |
| | | -17.50 | 3329.5 | 5113.2 | 8442.8 | 5061.6 | 0.0 | 5061.6 |
| | | -18.00 | 3901.9 | 5268.0 | 9170.0 | 5497.6 | 0.0 | 5497.6 |
| | | -18.50 | 4817.8 | 5412.5 | 10230.3 | 6133.3 | 0.0 | 6133.3 |
| | | -19.00 | 4854.7 | 5567.3 | 10421.9 | 6248.2 | 0.0 | 6248.2 |
| | | -19.50 | 4896.6 | 5722.1 | 10618.7 | 6366.1 | 0.0 | 6366.1 |
| | | -20.00 | 4956.5 | 5876.9 | 10833.3 | 6494.8 | 0.0 | 6494.8 |
| | | -20.50 | 4991.8 | 6031.7 | 11023.4 | 6608.8 | 0.0 | 6608.8 |
| | | -21.00 | 5305.8 | 6186.5 | 11492.2 | 6889.8 | 0.0 | 6889.8 |
| 166.S01 | 3.45 | -7.00 | 3009.4 | 1016.6 | 4026.0 | 2413.7 | -11.0 | 2402.7 |
| | | -7.50 | 3065.5 | 1171.5 | 4236.9 | 2540.1 | -11.0 | 2529.1 |
| | | -8.00 | 3159.0 | 1326.3 | 4485.2 | 2689.0 | -11.0 | 2678.0 |
| | | -8.50 | 3269.8 | 1479.9 | 4749.6 | 2847.5 | -11.0 | 2836.5 |
| | | -9.00 | 3201.1 | 1633.3 | 4834.4 | 2898.3 | -11.0 | 2887.3 |
| | | -9.50 | 3223.6 | 1784.5 | 5008.1 | 3002.5 | -11.0 | 2991.5 |
| | | -10.00 | 2871.6 | 1939.3 | 4811.0 | 2884.3 | -11.0 | 2873.3 |
| -10.50 | 2802.8 | 2094.1 | 4896.9 | 2935.8 | -11.0 | 2924.8 | | |
| -11.00 | 2801.0 | 2248.9 | 5049.9 | 3027.5 | -11.0 | 3016.6 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziwkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|---------------------------|--------------------------------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _d [kN] | F _{bk;d} [kN] | R _{c,netto;d} [kN] |
| 166.S01 | 3.45 | -11.50 | 2593.6 | 2403.7 | 4997.3 | 2996.0 | -11.0 | 2985.0 |
| | | -12.00 | 2435.9 | 2546.0 | 4982.0 | 2986.8 | -11.0 | 2975.8 |
| | | -12.50 | 2405.1 | 2666.2 | 5071.3 | 3040.4 | -11.0 | 3029.4 |
| | | -13.00 | 2665.1 | 2778.6 | 5443.7 | 3263.6 | -11.0 | 3252.6 |
| | | -13.50 | 3188.4 | 2892.9 | 6081.2 | 3645.8 | -11.0 | 3634.8 |
| | | -14.00 | 3294.0 | 3025.8 | 6319.9 | 3788.9 | -11.0 | 3777.9 |
| | | -14.50 | 3369.8 | 3179.0 | 6548.8 | 3926.1 | -11.0 | 3915.1 |
| | | -15.00 | 3452.1 | 3333.8 | 6785.9 | 4068.3 | -11.0 | 4057.3 |
| | | -15.50 | 3959.9 | 3488.6 | 7448.5 | 4465.5 | -11.0 | 4454.5 |
| | | -16.00 | 4082.4 | 3643.4 | 7725.8 | 4631.8 | -11.0 | 4620.8 |
| | | -16.50 | 4083.2 | 3798.2 | 7881.4 | 4725.1 | -11.0 | 4714.1 |
| | | -17.00 | 4037.8 | 3953.0 | 7990.8 | 4790.6 | -11.0 | 4779.7 |
| | | -17.50 | 4116.0 | 4107.8 | 8223.8 | 4930.4 | -11.0 | 4919.4 |
| | | -18.00 | 4189.8 | 4262.6 | 8452.4 | 5067.4 | -11.0 | 5056.4 |
| | | -18.50 | 4250.9 | 4417.4 | 8668.3 | 5196.8 | -11.0 | 5185.9 |
| | | -19.00 | 4260.0 | 4572.2 | 8832.2 | 5295.1 | -11.0 | 5284.1 |
| | | -19.50 | 4210.2 | 4727.0 | 8937.2 | 5358.0 | -11.0 | 5347.0 |
| 19-1008_11 | 0.62 | -7.00 | 448.0 | 6.8 | 454.8 | 272.7 | -167.1 | 105.6 |
| | | -7.50 | 629.1 | 49.1 | 678.2 | 406.6 | -167.1 | 239.5 |
| | | -8.00 | 633.3 | 111.2 | 744.4 | 446.3 | -167.1 | 279.2 |
| | | -8.50 | 635.1 | 167.7 | 802.8 | 481.3 | -167.1 | 314.2 |
| | | -9.00 | 658.3 | 211.6 | 869.9 | 521.5 | -167.1 | 354.4 |
| | | -9.50 | 619.0 | 253.4 | 872.4 | 523.0 | -167.1 | 356.0 |
| | | -10.00 | 650.6 | 296.7 | 947.3 | 567.9 | -167.1 | 400.8 |
| | | -10.50 | 651.7 | 348.7 | 1000.3 | 599.7 | -167.1 | 432.6 |
| | | -11.00 | 661.7 | 409.3 | 1071.0 | 642.1 | -167.1 | 475.0 |
| | | -11.50 | 616.5 | 482.3 | 1098.7 | 658.7 | -167.1 | 491.6 |
| | | -12.00 | 463.6 | 574.3 | 1037.9 | 622.2 | -167.1 | 455.1 |
| | | -12.50 | 1506.7 | 608.6 | 2115.3 | 1268.2 | -167.1 | 1101.1 |
| | | -13.00 | 1800.6 | 717.2 | 2517.8 | 1509.5 | -167.1 | 1342.4 |
| | | -13.50 | 1857.0 | 845.2 | 2702.3 | 1620.1 | -167.1 | 1453.0 |
| | | -14.00 | 1907.3 | 975.7 | 2883.0 | 1728.4 | -167.1 | 1561.3 |
| | | -14.50 | 1936.0 | 1107.6 | 3043.7 | 1824.7 | -167.1 | 1657.7 |
| | | -15.00 | 1944.8 | 1239.6 | 3184.4 | 1909.1 | -167.1 | 1742.0 |
| | | -15.50 | 1976.7 | 1363.0 | 3339.8 | 2002.3 | -167.1 | 1835.2 |
| | | -16.00 | 2252.0 | 1467.2 | 3719.2 | 2229.7 | -167.1 | 2062.7 |
| | | -16.50 | 2289.1 | 1589.2 | 3878.3 | 2325.1 | -167.1 | 2158.1 |
| | | -17.00 | 2327.0 | 1706.4 | 4033.4 | 2418.1 | -167.1 | 2251.0 |
| | | -17.50 | 3083.0 | 1817.1 | 4900.2 | 2937.8 | -167.1 | 2770.7 |
| | | -18.00 | 3712.4 | 1956.8 | 5669.2 | 3398.8 | -167.1 | 3231.7 |
| | | -18.50 | 3893.1 | 2111.6 | 6004.6 | 3599.9 | -167.1 | 3432.8 |
| | | -19.00 | 3928.3 | 2266.4 | 6194.6 | 3713.8 | -167.1 | 3546.7 |
| | | -19.50 | 3889.0 | 2421.2 | 6310.1 | 3783.0 | -167.1 | 3616.0 |
| | | -20.00 | 3976.1 | 2576.0 | 6552.1 | 3928.1 | -167.1 | 3761.0 |
| | | -20.50 | 3024.6 | 2730.8 | 5755.3 | 3450.4 | -167.1 | 3283.4 |
| | | -21.00 | 2984.4 | 2885.6 | 5870.0 | 3519.2 | -167.1 | 3352.1 |
| | | -21.50 | 2870.2 | 3031.4 | 5901.6 | 3538.1 | -167.1 | 3371.0 |
| -22.00 | 2500.9 | 3186.2 | 5687.1 | 3409.5 | -167.1 | 3242.5 | | |
| -22.50 | 2340.6 | 3341.0 | 5681.6 | 3406.2 | -167.1 | 3239.2 | | |
| -23.00 | 2170.4 | 3481.4 | 5651.8 | 3388.4 | -167.1 | 3221.3 | | |
| -23.50 | 2534.1 | 3574.6 | 6108.7 | 3662.3 | -167.1 | 3495.2 | | |
| -24.00 | 2557.2 | 3694.8 | 6252.0 | 3748.2 | -167.1 | 3581.1 | | |
| -24.50 | 2499.0 | 3831.1 | 6330.1 | 3795.0 | -167.1 | 3627.9 | | |
| -25.00 | 2474.2 | 3960.8 | 6435.0 | 3857.9 | -167.1 | 3690.8 | | |
| -25.50 | 3664.9 | 4070.2 | 7735.1 | 4637.3 | -167.1 | 4470.3 | | |
| -26.00 | 3671.2 | 4225.0 | 7896.1 | 4733.9 | -167.1 | 4566.8 | | |
| -26.50 | 3643.0 | 4379.8 | 8022.8 | 4809.8 | -167.1 | 4642.8 | | |
| -27.00 | 3675.7 | 4534.6 | 8210.2 | 4922.2 | -167.1 | 4755.1 | | |
| -27.50 | 3771.8 | 4689.4 | 8461.2 | 5072.6 | -167.1 | 4905.6 | | |
| -28.00 | 4225.4 | 4844.2 | 9069.6 | 5437.4 | -167.1 | 5270.3 | | |
| -28.50 | 4428.0 | 4998.9 | 9426.9 | 5651.6 | -167.1 | 5484.5 | | |
| -29.00 | 4877.6 | 5153.7 | 10031.3 | 6014.0 | -167.1 | 5846.9 | | |
| -29.50 | 5819.9 | 5308.5 | 11128.5 | 6671.7 | -167.1 | 6504.7 | | |
| -30.00 | 6001.2 | 5463.3 | 11464.6 | 6873.2 | -167.1 | 6706.2 | | |
| 19-1008_12 | 3.57 | -7.00 | 974.4 | 1952.4 | 2926.8 | 1754.7 | 0.0 | 1754.7 |
| | | -7.50 | 765.6 | 2107.2 | 2872.8 | 1722.3 | 0.0 | 1722.3 |
| | | -8.00 | 454.5 | 2260.6 | 2715.1 | 1627.8 | 0.0 | 1627.8 |
| | | -8.50 | 291.3 | 2339.4 | 2630.8 | 1577.2 | 0.0 | 1577.2 |
| | | -9.00 | 301.8 | 2362.5 | 2664.3 | 1597.3 | 0.0 | 1597.3 |
| | | -9.50 | 326.4 | 2379.3 | 2705.7 | 1622.1 | 0.0 | 1622.1 |
| | | -10.00 | 295.8 | 2412.8 | 2708.6 | 1623.9 | 0.0 | 1623.9 |
| | | -10.50 | 274.2 | 2481.0 | 2755.2 | 1651.8 | 0.0 | 1651.8 |
| | | -11.00 | 204.6 | 2533.5 | 2738.1 | 1641.6 | 0.0 | 1641.6 |
| | | -11.50 | 278.0 | 2543.8 | 2821.8 | 1691.7 | 0.0 | 1691.7 |
| | | -12.00 | 249.3 | 2593.0 | 2842.3 | 1704.0 | 0.0 | 1704.0 |
| | | -12.50 | 248.8 | 2610.8 | 2859.7 | 1714.4 | 0.0 | 1714.4 |
| | | -13.00 | 296.1 | 2624.8 | 2920.8 | 1751.1 | 0.0 | 1751.1 |
| | | -13.50 | 416.0 | 2642.1 | 3058.1 | 1833.4 | 0.0 | 1833.4 |
| | | -14.00 | 432.5 | 2684.6 | 3117.2 | 1868.8 | 0.0 | 1868.8 |
| | | -14.50 | 428.7 | 2740.3 | 3169.0 | 1899.9 | 0.0 | 1899.9 |
| | | -15.00 | 440.0 | 2779.1 | 3219.2 | 1930.0 | 0.0 | 1930.0 |
| | | -15.50 | 562.6 | 2809.9 | 3372.6 | 2021.9 | 0.0 | 2021.9 |
| | | -16.00 | 594.4 | 2860.2 | 3454.6 | 2071.1 | 0.0 | 2071.1 |
| | | -16.50 | 606.9 | 2929.0 | 3535.9 | 2119.9 | 0.0 | 2119.9 |
| | | -17.00 | 654.5 | 2986.1 | 3640.6 | 2182.6 | 0.0 | 2182.6 |
| -17.50 | 752.4 | 3071.3 | 3823.6 | 2292.3 | 0.0 | 2292.3 | | |
| -18.00 | 1080.6 | 3137.2 | 4217.8 | 2528.7 | 0.0 | 2528.7 | | |
| -18.50 | 1082.0 | 3289.6 | 4371.6 | 2620.9 | 0.0 | 2620.9 | | |
| -19.00 | 1585.3 | 3429.0 | 5014.3 | 3006.2 | 0.0 | 3006.2 | | |
| -19.50 | 1820.5 | 3556.5 | 5377.0 | 3223.6 | 0.0 | 3223.6 | | |
| -20.00 | 2180.0 | 3666.4 | 5846.4 | 3505.0 | 0.0 | 3505.0 | | |
| -20.50 | 2010.5 | 3790.2 | 5800.8 | 3477.7 | 0.0 | 3477.7 | | |
| -21.00 | 2586.1 | 3906.2 | 6492.2 | 3892.2 | 0.0 | 3892.2 | | |
| -21.50 | 2689.3 | 4046.7 | 6736.0 | 4038.4 | 0.0 | 4038.4 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|--------------------------|--------------------------------|--------|-------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _{s,d} [kN] | F _{hkd} [kN] | R _{c,netto;d} [kN] | | |
| 19-1008_12 | 3.57 | -22.00 | 2801.9 | 4199.4 | 7001.4 | 4197.5 | 0.0 | 4197.5 | | |
| | | -22.50 | 2804.1 | 4351.8 | 7155.9 | 4290.1 | 0.0 | 4290.1 | | |
| | | -23.00 | 2714.1 | 4491.5 | 7205.7 | 4319.9 | 0.0 | 4319.9 | | |
| | | -23.50 | 2124.5 | 4626.0 | 6750.5 | 4047.0 | 0.0 | 4047.0 | | |
| | | -24.00 | 1991.2 | 4768.7 | 6759.9 | 4052.7 | 0.0 | 4052.7 | | |
| | | -24.50 | 1732.9 | 4923.5 | 6656.4 | 3990.7 | 0.0 | 3990.7 | | |
| | | -25.00 | 1409.9 | 5078.3 | 6488.2 | 3889.8 | 0.0 | 3889.8 | | |
| | | -25.50 | 1246.4 | 5282.6 | 6529.0 | 3914.3 | 0.0 | 3914.3 | | |
| | | -26.00 | 1171.7 | 5488.1 | 6659.7 | 3992.7 | 0.0 | 3992.7 | | |
| | | -26.50 | 1175.6 | 5606.4 | 6782.0 | 4065.9 | 0.0 | 4065.9 | | |
| | | -27.00 | 1168.5 | 5717.0 | 6885.5 | 4128.0 | 0.0 | 4128.0 | | |
| | | -27.50 | 1100.3 | 5843.8 | 6944.1 | 4163.2 | 0.0 | 4163.2 | | |
| | | -28.00 | 2086.8 | 5935.4 | 8022.3 | 4809.5 | 0.0 | 4809.5 | | |
| | | -28.50 | 2751.2 | 6053.0 | 8804.2 | 5278.3 | 0.0 | 5278.3 | | |
| | | 19-1008_17 | 0.20 | -7.00 | 287.1 | 0.0 | 287.1 | 172.1 | -206.0 | -33.9 |
| | | | | -7.50 | 244.4 | 0.0 | 244.4 | 146.6 | -233.3 | -86.8 |
| | | | | -8.00 | 290.5 | 0.0 | 290.5 | 174.2 | -233.3 | -59.2 |
| -8.50 | 337.5 | | | 0.0 | 337.5 | 202.3 | -233.3 | -31.0 | | |
| -9.00 | 372.8 | | | 0.0 | 372.8 | 223.5 | -233.3 | -9.8 | | |
| -9.50 | 1034.2 | | | 0.0 | 1034.2 | 620.0 | -233.3 | 386.7 | | |
| -10.00 | 733.7 | | | 0.0 | 733.7 | 439.9 | -233.3 | 206.6 | | |
| -10.50 | 1520.5 | | | 23.8 | 1544.3 | 925.9 | -233.3 | 692.5 | | |
| -11.00 | 2827.2 | | | 120.8 | 2948.0 | 1767.4 | -233.3 | 1534.1 | | |
| -11.50 | 2946.9 | | | 275.6 | 3222.5 | 1931.9 | -233.3 | 1698.6 | | |
| -12.00 | 2646.9 | | | 430.4 | 3077.3 | 1844.9 | -233.3 | 1611.6 | | |
| -12.50 | 2732.2 | | | 585.2 | 3317.4 | 1988.8 | -233.3 | 1755.5 | | |
| -13.00 | 2668.8 | | | 740.0 | 3408.8 | 2043.6 | -233.3 | 1810.3 | | |
| -13.50 | 2652.8 | | | 894.8 | 3547.6 | 2126.8 | -233.3 | 1893.5 | | |
| -14.00 | 2658.5 | | | 1049.6 | 3708.1 | 2223.1 | -233.3 | 1989.8 | | |
| -14.50 | 3014.4 | | | 1204.3 | 4218.7 | 2529.2 | -233.3 | 2295.9 | | |
| -15.00 | 3215.9 | | | 1347.4 | 4563.3 | 2735.8 | -233.3 | 2502.5 | | |
| -15.50 | 1984.2 | | | 1502.2 | 3486.4 | 2090.2 | -233.3 | 1856.8 | | |
| -16.00 | 1845.2 | | | 1657.0 | 3502.2 | 2099.6 | -233.3 | 1866.3 | | |
| -16.50 | 1831.2 | | | 1811.8 | 3643.0 | 2184.0 | -233.3 | 1950.7 | | |
| -17.00 | 1871.2 | | | 1960.2 | 3831.4 | 2297.0 | -233.3 | 2063.7 | | |
| -17.50 | 1610.2 | | | 2120.5 | 3730.7 | 2236.6 | -233.3 | 2003.3 | | |
| -18.00 | 1341.8 | | | 2306.4 | 3648.2 | 2187.2 | -233.3 | 1953.8 | | |
| -18.50 | 1890.8 | | | 2430.8 | 4321.6 | 2590.9 | -233.3 | 2357.6 | | |
| -19.00 | 1935.5 | | | 2538.0 | 4473.5 | 2682.0 | -233.3 | 2448.6 | | |
| -19.50 | 1984.6 | | | 2661.8 | 4646.5 | 2785.6 | -233.3 | 2552.3 | | |
| -20.00 | 2059.3 | | | 2786.8 | 4846.0 | 2905.3 | -233.3 | 2672.0 | | |
| -20.50 | 2224.7 | | | 2919.3 | 5144.0 | 3084.0 | -233.3 | 2850.6 | | |
| -21.00 | 2000.2 | | | 3056.2 | 5056.4 | 3031.4 | -233.3 | 2798.1 | | |
| -21.50 | 2441.3 | | | 3209.5 | 5650.8 | 3387.7 | -233.3 | 3154.4 | | |
| -22.00 | 2362.0 | 3341.5 | 5703.5 | 3419.4 | -233.3 | 3186.1 | | | | |
| -22.50 | 2306.9 | 3496.3 | 5803.2 | 3479.1 | -233.3 | 3245.8 | | | | |
| -23.00 | 2170.1 | 3651.1 | 5821.2 | 3490.0 | -233.3 | 3256.6 | | | | |
| -23.50 | 2045.6 | 3805.9 | 5851.5 | 3508.1 | -233.3 | 3274.8 | | | | |
| -24.00 | 2039.9 | 3948.6 | 5988.5 | 3590.2 | -233.3 | 3356.9 | | | | |
| -24.50 | 2010.9 | 4072.2 | 6083.1 | 3647.0 | -233.3 | 3413.6 | | | | |
| -25.00 | 2038.0 | 4168.5 | 6206.5 | 3720.9 | -233.3 | 3487.6 | | | | |
| -25.50 | 2067.8 | 4262.0 | 6329.8 | 3794.8 | -233.3 | 3561.5 | | | | |
| -26.00 | 2146.4 | 4353.2 | 6499.6 | 3896.6 | -233.3 | 3663.3 | | | | |
| -26.50 | 942.9 | 4444.1 | 5387.0 | 3229.6 | -233.3 | 2996.3 | | | | |
| -27.00 | 876.6 | 4552.1 | 5428.6 | 3254.6 | -233.3 | 3021.3 | | | | |
| -27.50 | 856.7 | 4667.8 | 5524.5 | 3312.0 | -233.3 | 3078.7 | | | | |
| -28.00 | 812.9 | 4785.7 | 5598.6 | 3356.5 | -233.3 | 3123.2 | | | | |
| -28.50 | 668.7 | 4909.4 | 5578.1 | 3344.2 | -233.3 | 3110.9 | | | | |
| -29.00 | 379.7 | 5039.3 | 5419.0 | 3248.8 | -233.3 | 3015.5 | | | | |
| -29.50 | 1411.6 | 5075.9 | 6487.5 | 3889.4 | -233.3 | 3656.1 | | | | |
| -30.00 | 2075.6 | 5174.4 | 7250.0 | 4346.5 | -233.3 | 4113.2 | | | | |
| 19-1008_20 | -0.03 | -7.00 | 845.8 | 301.3 | 1147.1 | 687.7 | -44.0 | 643.8 | | |
| | | -7.50 | 657.3 | 384.2 | 1041.5 | 624.4 | -44.0 | 580.4 | | |
| | | -8.00 | 629.6 | 448.2 | 1077.9 | 646.2 | -44.0 | 602.2 | | |
| | | -8.50 | 641.2 | 510.6 | 1151.9 | 690.6 | -44.0 | 646.6 | | |
| | | -9.00 | 601.7 | 597.3 | 1198.9 | 718.8 | -44.0 | 674.8 | | |
| | | -9.50 | 560.4 | 667.4 | 1227.7 | 736.1 | -44.0 | 692.1 | | |
| | | -10.00 | 420.2 | 748.3 | 1168.6 | 700.6 | -44.0 | 656.6 | | |
| | | -10.50 | 655.7 | 767.7 | 1423.4 | 853.4 | -44.0 | 809.4 | | |
| | | -11.00 | 567.3 | 872.7 | 1440.0 | 863.3 | -44.0 | 819.3 | | |
| | | -11.50 | 397.9 | 986.2 | 1384.2 | 829.9 | -44.0 | 785.9 | | |
| | | -12.00 | 446.3 | 1008.3 | 1454.7 | 872.1 | -44.0 | 828.1 | | |
| | | -12.50 | 475.7 | 1033.7 | 1509.4 | 904.9 | -44.0 | 860.9 | | |
| | | -13.00 | 447.7 | 1082.5 | 1530.2 | 917.4 | -44.0 | 873.4 | | |
| | | -13.50 | 594.6 | 1104.5 | 1699.1 | 1018.6 | -44.0 | 974.7 | | |
| | | -14.00 | 559.6 | 1147.6 | 1707.3 | 1023.5 | -44.0 | 979.6 | | |
| | | -14.50 | 536.0 | 1227.5 | 1763.5 | 1057.3 | -44.0 | 1013.3 | | |
| | | -15.00 | 509.9 | 1318.8 | 1828.7 | 1096.4 | -44.0 | 1052.4 | | |
| | | -15.50 | 506.7 | 1370.1 | 1876.8 | 1125.2 | -44.0 | 1081.2 | | |
| | | -16.00 | 523.5 | 1408.6 | 1932.1 | 1158.3 | -44.0 | 1114.4 | | |
| | | -16.50 | 512.1 | 1463.1 | 1975.2 | 1184.2 | -44.0 | 1140.2 | | |
| | | -17.00 | 553.2 | 1498.4 | 2051.6 | 1230.0 | -44.0 | 1186.0 | | |
| | | -17.50 | 802.4 | 1541.7 | 2344.1 | 1405.4 | -44.0 | 1361.4 | | |
| | | -18.00 | 825.9 | 1622.8 | 2448.7 | 1468.1 | -44.0 | 1424.1 | | |
| -18.50 | 817.0 | 1717.8 | 2534.9 | 1519.7 | -44.0 | 1475.7 | | | | |
| -19.00 | 926.2 | 1788.9 | 2715.0 | 1627.7 | -44.0 | 1583.8 | | | | |
| -19.50 | 972.7 | 1884.6 | 2857.3 | 1713.0 | -44.0 | 1669.0 | | | | |
| -20.00 | 867.7 | 1983.3 | 2851.0 | 1709.2 | -44.0 | 1665.3 | | | | |
| -20.50 | 729.2 | 2110.5 | 2839.6 | 1702.4 | -44.0 | 1658.4 | | | | |
| -21.00 | 579.8 | 2280.7 | 2860.6 | 1715.0 | -44.0 | 1671.0 | | | | |
| -21.50 | 559.0 | 2352.9 | 2911.9 | 1745.7 | -44.0 | 1701.8 | | | | |
| -22.00 | 564.0 | 2400.5 | 2964.5 | 1777.3 | -44.0 | 1733.3 | | | | |
| -22.50 | 572.3 | 2452.4 | 3024.7 | 1813.4 | -44.0 | 1769.4 | | | | |
| -23.00 | 1162.0 | 2494.3 | 3656.3 | 2192.0 | -44.0 | 2148.0 | | | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziwkdraagvermogen | | | Rekenwaarden | | | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|---------------------------|--------------------------------|--------|-------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _d [kN] | F _{nk;d} [kN] | R _{d,netto;d} [kN] | | |
| 19-1008_20 | -0.03 | -23.50 | 1351.1 | 2575.8 | 3927.0 | 2354.3 | -44.0 | 2310.3 | | |
| | | -24.00 | 1529.0 | 2667.1 | 4196.1 | 2515.7 | -44.0 | 2471.7 | | |
| | | -24.50 | 1651.6 | 2762.8 | 4414.4 | 2646.5 | -44.0 | 2602.6 | | |
| | | -25.00 | 1687.2 | 2880.6 | 4567.7 | 2738.4 | -44.0 | 2694.5 | | |
| | | -25.50 | 1740.6 | 2987.6 | 4728.2 | 2834.6 | -44.0 | 2790.7 | | |
| | | -26.00 | 1830.7 | 3092.3 | 4923.0 | 2951.4 | -44.0 | 2907.5 | | |
| | | -26.50 | 1585.8 | 3186.8 | 4772.6 | 2861.3 | -44.0 | 2817.3 | | |
| | | -27.00 | 1602.6 | 3302.2 | 4904.8 | 2940.5 | -44.0 | 2896.6 | | |
| | | -27.50 | 1573.9 | 3403.6 | 4977.5 | 2984.1 | -44.0 | 2940.1 | | |
| | | -28.00 | 1611.3 | 3495.2 | 5106.5 | 3061.5 | -44.0 | 3017.5 | | |
| | | -28.50 | 1637.7 | 3602.7 | 5240.3 | 3141.7 | -44.0 | 3097.7 | | |
| | | -29.00 | 1644.5 | 3702.2 | 5346.7 | 3205.4 | -44.0 | 3161.5 | | |
| | | -29.50 | 1669.9 | 3782.3 | 5452.2 | 3268.7 | -44.0 | 3224.7 | | |
| | | -30.00 | 1425.7 | 3883.4 | 5309.1 | 3182.9 | -44.0 | 3138.9 | | |
| | | 19-1008_21 | 1.78 | -7.00 | 1133.1 | 535.8 | 1668.9 | 1000.5 | -137.2 | 863.3 |
| | | | | -7.50 | 1113.1 | 657.1 | 1770.2 | 1061.3 | -137.2 | 924.0 |
| | | | | -8.00 | 1119.5 | 770.7 | 1890.2 | 1133.2 | -137.2 | 996.0 |
| -8.50 | 988.3 | | | 885.5 | 1873.7 | 1123.3 | -137.2 | 986.1 | | |
| -9.00 | 1001.5 | | | 944.8 | 1946.3 | 1166.8 | -137.2 | 1029.6 | | |
| -9.50 | 1224.4 | | | 989.5 | 2213.9 | 1327.3 | -137.2 | 1190.1 | | |
| -10.00 | 1270.5 | | | 1057.6 | 2328.1 | 1395.7 | -137.2 | 1258.5 | | |
| -10.50 | 1311.8 | | | 1117.3 | 2429.1 | 1456.3 | -137.2 | 1319.1 | | |
| -11.00 | 1304.2 | | | 1185.8 | 2490.0 | 1492.8 | -137.2 | 1355.6 | | |
| -11.50 | 1297.6 | | | 1272.3 | 2569.9 | 1540.7 | -137.2 | 1403.5 | | |
| -12.00 | 1304.1 | | | 1369.4 | 2673.6 | 1602.9 | -137.2 | 1465.6 | | |
| -12.50 | 1189.1 | | | 1444.0 | 2633.1 | 1578.6 | -137.2 | 1441.4 | | |
| -13.00 | 1249.2 | | | 1530.2 | 2779.4 | 1666.3 | -137.2 | 1529.1 | | |
| -13.50 | 1254.7 | | | 1625.6 | 2880.4 | 1726.8 | -137.2 | 1589.6 | | |
| -14.00 | 1038.3 | | | 1767.6 | 2805.9 | 1682.2 | -137.2 | 1545.0 | | |
| -14.50 | 948.9 | | | 1909.8 | 2858.7 | 1713.9 | -137.2 | 1576.6 | | |
| -15.00 | 1010.8 | | | 2013.9 | 3024.7 | 1813.3 | -137.2 | 1676.1 | | |
| -15.50 | 795.4 | | | 2089.7 | 2885.2 | 1729.7 | -137.2 | 1592.5 | | |
| -16.00 | 663.9 | | | 2236.5 | 2900.4 | 1738.8 | -137.2 | 1601.6 | | |
| -16.50 | 429.8 | | | 2382.9 | 2812.7 | 1686.3 | -137.2 | 1549.1 | | |
| -17.00 | 474.6 | | | 2407.8 | 2882.4 | 1728.1 | -137.2 | 1590.8 | | |
| -17.50 | 633.2 | | | 2436.9 | 3070.0 | 1840.6 | -137.2 | 1703.3 | | |
| -18.00 | 625.1 | | | 2492.4 | 3117.4 | 1869.0 | -137.2 | 1731.7 | | |
| -18.50 | 518.6 | | | 2653.0 | 3171.7 | 1901.5 | -137.2 | 1764.2 | | |
| -19.00 | 467.3 | | | 2765.1 | 3232.4 | 1937.9 | -137.2 | 1800.7 | | |
| -19.50 | 467.3 | | | 2793.6 | 3261.0 | 1955.0 | -137.2 | 1817.8 | | |
| -20.00 | 470.8 | | | 2816.3 | 3287.1 | 1970.7 | -137.2 | 1833.4 | | |
| -20.50 | 480.3 | | | 2838.7 | 3319.0 | 1989.8 | -137.2 | 1852.6 | | |
| -21.00 | 509.7 | | | 2861.4 | 3371.0 | 2021.0 | -137.2 | 1883.8 | | |
| -21.50 | 531.2 | | | 2888.7 | 3419.9 | 2050.3 | -137.2 | 1913.1 | | |
| -22.00 | 551.9 | | | 2920.4 | 3472.2 | 2081.7 | -137.2 | 1944.4 | | |
| -22.50 | 560.0 | | | 2959.1 | 3519.0 | 2109.7 | -137.2 | 1972.5 | | |
| -23.00 | 566.6 | | | 2997.4 | 3564.1 | 2136.7 | -137.2 | 1999.5 | | |
| -23.50 | 601.3 | 3034.3 | 3635.6 | 2179.6 | -137.2 | 2042.4 | | | | |
| -24.00 | 605.4 | 3078.1 | 3683.5 | 2208.3 | -137.2 | 2071.1 | | | | |
| -24.50 | 610.6 | 3123.1 | 3733.6 | 2238.4 | -137.2 | 2101.2 | | | | |
| -25.00 | 612.2 | 3170.4 | 3782.6 | 2267.7 | -137.2 | 2130.5 | | | | |
| -25.50 | 614.3 | 3220.1 | 3834.4 | 2298.8 | -137.2 | 2161.6 | | | | |
| -26.00 | 616.3 | 3267.7 | 3884.1 | 2328.6 | -137.2 | 2191.3 | | | | |
| -26.50 | 623.0 | 3310.8 | 3933.9 | 2358.4 | -137.2 | 2221.2 | | | | |
| -27.00 | 626.7 | 3355.0 | 3981.7 | 2387.1 | -137.2 | 2249.9 | | | | |
| -27.50 | 659.9 | 3398.4 | 4058.3 | 2433.0 | -137.2 | 2295.8 | | | | |
| -28.00 | 667.9 | 3445.2 | 4113.1 | 2465.9 | -137.2 | 2328.7 | | | | |
| -28.50 | 670.2 | 3493.5 | 4163.7 | 2496.2 | -137.2 | 2359.0 | | | | |
| -29.00 | 692.1 | 3540.4 | 4232.5 | 2537.5 | -137.2 | 2400.3 | | | | |
| -29.50 | 709.2 | 3589.7 | 4298.9 | 2577.3 | -137.2 | 2440.1 | | | | |
| -30.00 | 716.9 | 3642.3 | 4359.2 | 2613.4 | -137.2 | 2476.2 | | | | |
| 251.S01 | -1.05 | -7.00 | 575.9 | 746.3 | 1322.2 | 792.7 | -15.1 | 777.6 | | |
| | | -7.50 | 417.2 | 866.1 | 1283.2 | 769.3 | -15.1 | 754.3 | | |
| | | -8.00 | 293.6 | 976.2 | 1269.8 | 761.3 | -15.1 | 746.2 | | |
| | | -8.50 | 202.4 | 1050.3 | 1252.7 | 751.0 | -15.1 | 735.9 | | |
| | | -9.00 | 859.6 | 1061.4 | 1921.0 | 1151.6 | -15.1 | 1136.6 | | |
| | | -9.50 | 1011.0 | 1129.8 | 2140.8 | 1283.4 | -15.1 | 1268.4 | | |
| | | -10.00 | 1035.2 | 1233.5 | 2268.8 | 1360.2 | -15.1 | 1345.1 | | |
| | | -10.50 | 1000.1 | 1355.5 | 2355.6 | 1412.2 | -15.1 | 1397.2 | | |
| | | -11.00 | 958.4 | 1448.2 | 2406.6 | 1442.8 | -15.1 | 1427.7 | | |
| | | -11.50 | 1026.3 | 1504.5 | 2530.8 | 1517.3 | -15.1 | 1502.2 | | |
| | | -12.00 | 1440.9 | 1560.4 | 3001.3 | 1799.3 | -15.1 | 1784.3 | | |
| | | -12.50 | 1107.2 | 1655.4 | 2762.6 | 1656.2 | -15.1 | 1641.2 | | |
| | | -13.00 | 1139.0 | 1767.9 | 2906.9 | 1742.7 | -15.1 | 1727.7 | | |
| | | -13.50 | 1168.1 | 1873.8 | 3041.9 | 1823.7 | -15.1 | 1808.6 | | |
| | | -14.00 | 1103.3 | 2021.0 | 3124.3 | 1873.1 | -15.1 | 1858.0 | | |
| | | -14.50 | 950.3 | 2167.3 | 3117.6 | 1869.1 | -15.1 | 1854.0 | | |
| | | -15.00 | 729.8 | 2325.7 | 3055.5 | 1831.8 | -15.1 | 1816.8 | | |
| | | -15.50 | 2139.0 | 2396.6 | 4535.7 | 2719.2 | -15.1 | 2704.2 | | |
| | | -16.00 | 1712.0 | 2539.5 | 4251.6 | 2548.9 | -15.1 | 2533.8 | | |
| | | -16.50 | 1659.7 | 2694.3 | 4354.0 | 2610.3 | -15.1 | 2595.3 | | |
| | | -17.00 | 1701.0 | 2847.4 | 4548.5 | 2726.9 | -15.1 | 2711.8 | | |
| | | -17.50 | 1669.8 | 2993.5 | 4663.3 | 2795.8 | -15.1 | 2780.7 | | |
| | | -18.00 | 1546.6 | 3131.5 | 4678.1 | 2804.6 | -15.1 | 2789.5 | | |
| -18.50 | 891.3 | 3286.1 | 4177.4 | 2504.5 | -15.1 | 2489.4 | | | | |
| -19.00 | 871.2 | 3379.0 | 4250.2 | 2548.1 | -15.1 | 2533.0 | | | | |
| -19.50 | 731.1 | 3478.3 | 4209.4 | 2523.6 | -15.1 | 2508.5 | | | | |
| -20.00 | 602.8 | 3598.7 | 4201.5 | 2518.9 | -15.1 | 2503.8 | | | | |
| -20.50 | 475.2 | 3767.1 | 4242.2 | 2543.3 | -15.1 | 2528.2 | | | | |
| -21.00 | 372.5 | 3944.4 | 4316.8 | 2588.0 | -15.1 | 2572.9 | | | | |
| -21.50 | 337.7 | 4017.9 | 4355.6 | 2611.3 | -15.1 | 2596.2 | | | | |
| -22.00 | 341.2 | 4040.9 | 4382.1 | 2627.2 | -15.1 | 2612.1 | | | | |
| -22.50 | 455.0 | 4071.4 | 4526.4 | 2713.6 | -15.1 | 2698.6 | | | | |
| -23.00 | 488.4 | 4120.2 | 4608.6 | 2762.9 | -15.1 | 2747.9 | | | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | | | |
|-----------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|---------------------------|--------------------------------|------|--------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _d [kN] | F _{bk;d} [kN] | R _{c,netto;d} [kN] | | |
| 251.S01 | -1.05 | -23.50 | 656.8 | 4184.0 | 4840.8 | 2902.2 | -15.1 | 2887.1 | | |
| | | -24.00 | 669.6 | 4270.4 | 4940.0 | 2961.7 | -15.1 | 2946.6 | | |
| | | -24.50 | 721.5 | 4349.1 | 5070.5 | 3039.9 | -15.1 | 3024.8 | | |
| | | -25.00 | 1047.3 | 4420.5 | 5467.8 | 3278.0 | -15.1 | 3263.0 | | |
| | | -25.50 | 1669.3 | 4548.6 | 6217.9 | 3727.7 | -15.1 | 3712.7 | | |
| | | -26.00 | 2925.2 | 4736.4 | 7661.6 | 4593.3 | -15.1 | 4578.2 | | |
| | | -26.50 | 2582.5 | 4917.4 | 7499.9 | 4496.4 | -15.1 | 4481.3 | | |
| | | -27.00 | 2658.8 | 5072.2 | 7731.0 | 4634.9 | -15.1 | 4619.8 | | |
| | | -27.50 | 2485.5 | 5227.0 | 7712.6 | 4623.8 | -15.1 | 4608.8 | | |
| | | -28.00 | 1737.7 | 5381.8 | 7119.5 | 4268.3 | -15.1 | 4253.2 | | |
| | | -28.50 | 1382.4 | 5536.6 | 6919.0 | 4148.1 | -15.1 | 4133.0 | | |
| | | -29.00 | 1182.9 | 5691.2 | 6874.1 | 4121.2 | -15.1 | 4106.1 | | |
| | | -29.50 | 1013.2 | 5795.1 | 6808.2 | 4081.7 | -15.1 | 4066.6 | | |
| | | -30.00 | 824.8 | 5918.9 | 6743.7 | 4043.0 | -15.1 | 4027.9 | | |
| | | 19-1008_29 | 0.79 | -7.00 | 2229.0 | 1173.4 | 3402.4 | 2039.8 | -7.3 | 2032.5 |
| | | | | -7.50 | 2299.7 | 1305.1 | 3604.9 | 2161.2 | -7.3 | 2153.9 |
| | | | | -8.00 | 2309.4 | 1446.6 | 3756.0 | 2251.8 | -7.3 | 2244.5 |
| -8.50 | 1877.2 | | | 1587.1 | 3464.3 | 2076.9 | -7.3 | 2069.6 | | |
| -9.00 | 839.6 | | | 1709.3 | 2549.0 | 1528.2 | -7.3 | 1520.9 | | |
| -9.50 | 839.3 | | | 1823.4 | 2662.7 | 1596.3 | -7.3 | 1589.1 | | |
| -10.00 | 844.6 | | | 1930.1 | 2774.6 | 1663.5 | -7.3 | 1656.2 | | |
| -10.50 | 775.2 | | | 2053.9 | 2829.2 | 1696.1 | -7.3 | 1688.8 | | |
| -11.00 | 661.1 | | | 2176.8 | 2837.9 | 1701.4 | -7.3 | 1694.1 | | |
| -11.50 | 613.8 | | | 2314.0 | 2927.8 | 1755.3 | -7.3 | 1748.0 | | |
| -12.00 | 666.5 | | | 2378.5 | 3045.0 | 1825.5 | -7.3 | 1818.3 | | |
| -12.50 | 547.2 | | | 2518.6 | 3065.8 | 1838.0 | -7.3 | 1830.7 | | |
| -13.00 | 420.9 | | | 2626.5 | 3047.4 | 1827.0 | -7.3 | 1819.7 | | |
| -13.50 | 434.1 | | | 2671.7 | 3105.9 | 1862.0 | -7.3 | 1854.7 | | |
| -14.00 | 436.2 | | | 2725.0 | 3161.2 | 1895.2 | -7.3 | 1887.9 | | |
| -14.50 | 447.9 | | | 2762.0 | 3209.8 | 1924.3 | -7.3 | 1917.1 | | |
| -15.00 | 525.8 | | | 2793.6 | 3319.4 | 1990.1 | -7.3 | 1982.8 | | |
| -15.50 | 592.6 | | | 2831.7 | 3424.2 | 2052.9 | -7.3 | 2045.6 | | |
| -16.00 | 506.2 | | | 2928.6 | 3434.8 | 2059.3 | -7.3 | 2052.0 | | |
| -16.50 | 526.1 | | | 2964.5 | 3490.6 | 2092.7 | -7.3 | 2085.4 | | |
| -17.00 | 671.2 | | | 3000.7 | 3671.9 | 2201.4 | -7.3 | 2194.1 | | |
| -17.50 | 1779.5 | | | 3053.0 | 4832.5 | 2897.2 | -7.3 | 2889.9 | | |
| -18.00 | 2167.8 | | | 3180.8 | 5348.6 | 3206.6 | -7.3 | 3199.3 | | |
| -18.50 | 2028.6 | | | 3335.6 | 5364.3 | 3216.0 | -7.3 | 3208.7 | | |
| -19.00 | 1676.0 | | | 3485.5 | 5161.5 | 3094.4 | -7.3 | 3087.1 | | |
| -19.50 | 3324.1 | | | 3601.2 | 6925.2 | 4151.8 | -7.3 | 4144.5 | | |
| -20.00 | 2574.3 | | | 3756.0 | 6330.3 | 3795.2 | -7.3 | 3787.9 | | |
| -20.50 | 2190.3 | | | 3910.8 | 6101.1 | 3657.7 | -7.3 | 3650.4 | | |
| -21.00 | 1871.5 | | | 4065.6 | 5937.1 | 3559.4 | -7.3 | 3552.1 | | |
| -21.50 | 1605.6 | | | 4220.4 | 5826.0 | 3492.8 | -7.3 | 3485.5 | | |
| -22.00 | 1356.6 | | | 4375.2 | 5731.8 | 3436.4 | -7.3 | 3429.1 | | |
| -22.50 | 1029.3 | | | 4554.8 | 5584.0 | 3347.7 | -7.3 | 3340.5 | | |
| -23.00 | 956.4 | | | 4687.5 | 5643.9 | 3383.6 | -7.3 | 3376.3 | | |
| -23.50 | 1013.9 | 4779.3 | 5793.2 | 3473.2 | -7.3 | 3465.9 | | | | |
| -24.00 | 1026.1 | 4887.4 | 5913.4 | 3545.2 | -7.3 | 3537.9 | | | | |
| -24.50 | 957.2 | 4997.3 | 5954.5 | 3569.8 | -7.3 | 3562.6 | | | | |
| -25.00 | 888.9 | 5114.1 | 6003.1 | 3599.0 | -7.3 | 3591.7 | | | | |
| -25.50 | 921.0 | 5186.5 | 6107.5 | 3661.6 | -7.3 | 3654.3 | | | | |
| -26.00 | 906.6 | 5270.0 | 6176.6 | 3703.0 | -7.3 | 3695.7 | | | | |
| -26.50 | 907.7 | 5347.7 | 6255.3 | 3750.2 | -7.3 | 3742.9 | | | | |
| -27.00 | 878.9 | 5445.3 | 6324.2 | 3791.5 | -7.3 | 3784.2 | | | | |
| -27.50 | 888.5 | 5519.1 | 6407.6 | 3841.5 | -7.3 | 3834.2 | | | | |
| -28.00 | 888.0 | 5591.0 | 6479.0 | 3884.3 | -7.3 | 3877.0 | | | | |
| -28.50 | 997.3 | 5662.4 | 6659.7 | 3992.6 | -7.3 | 3985.3 | | | | |
| -29.00 | 1529.0 | 5741.1 | 7270.2 | 4358.6 | -7.3 | 4351.3 | | | | |
| -29.50 | 1349.5 | 5865.4 | 7214.9 | 4325.5 | -7.3 | 4318.2 | | | | |
| -30.00 | 1166.1 | 5970.7 | 7136.8 | 4278.6 | -7.3 | 4271.3 | | | | |
| 283.S02 | 0.17 | -7.00 | 1681.2 | 899.0 | 2580.2 | 1546.9 | -14.7 | 1532.2 | | |
| | | -7.50 | 1831.7 | 983.7 | 2815.4 | 1687.9 | -14.7 | 1673.2 | | |
| | | -8.00 | 1870.1 | 1067.3 | 2937.4 | 1761.0 | -14.7 | 1746.3 | | |
| | | -8.50 | 1861.4 | 1169.0 | 3030.4 | 1816.8 | -14.7 | 1802.1 | | |
| | | -9.00 | 1440.6 | 1262.6 | 2703.2 | 1620.6 | -14.7 | 1605.9 | | |
| | | -9.50 | 1440.5 | 1342.0 | 2782.5 | 1668.1 | -14.7 | 1653.4 | | |
| | | -10.00 | 1431.2 | 1431.3 | 2862.5 | 1716.1 | -14.7 | 1701.4 | | |
| | | -10.50 | 1410.0 | 1517.4 | 2927.4 | 1755.0 | -14.7 | 1740.3 | | |
| | | -11.00 | 1391.3 | 1601.6 | 2992.9 | 1794.3 | -14.7 | 1779.6 | | |
| | | -11.50 | 1307.0 | 1692.0 | 2999.0 | 1797.9 | -14.7 | 1783.2 | | |
| | | -12.00 | 1885.6 | 1749.9 | 3635.5 | 2179.5 | -14.7 | 2164.8 | | |
| | | -12.50 | 2081.6 | 1850.4 | 3932.0 | 2357.3 | -14.7 | 2342.6 | | |
| | | -13.00 | 2314.9 | 1962.1 | 4276.9 | 2564.1 | -14.7 | 2549.4 | | |
| | | -13.50 | 2435.3 | 2086.5 | 4521.8 | 2710.9 | -14.7 | 2696.2 | | |
| | | -14.00 | 2500.0 | 2234.3 | 4734.2 | 2838.3 | -14.7 | 2823.6 | | |
| | | -14.50 | 2446.6 | 2382.0 | 4828.6 | 2894.8 | -14.7 | 2880.1 | | |
| | | -15.00 | 2425.4 | 2513.9 | 4939.3 | 2961.2 | -14.7 | 2946.5 | | |
| | | -15.50 | 2692.0 | 2626.8 | 5318.8 | 3188.7 | -14.7 | 3174.0 | | |
| | | -16.00 | 2977.7 | 2750.5 | 5728.2 | 3434.2 | -14.7 | 3419.5 | | |
| | | -16.50 | 3188.2 | 2888.3 | 6076.6 | 3643.0 | -14.7 | 3628.3 | | |
| | | -17.00 | 3663.9 | 3035.9 | 6699.8 | 4016.7 | -14.7 | 4002.0 | | |
| | | -17.50 | 3560.6 | 3190.7 | 6751.4 | 4047.6 | -14.7 | 4032.9 | | |
| | | -18.00 | 3649.7 | 3345.5 | 6995.3 | 4193.8 | -14.7 | 4179.1 | | |
| -18.50 | 3708.5 | 3500.3 | 7208.8 | 4321.8 | -14.7 | 4307.1 | | | | |
| -19.00 | 3763.6 | 3655.2 | 7418.8 | 4447.7 | -14.7 | 4433.0 | | | | |
| -19.50 | 3775.3 | 3810.0 | 7585.2 | 4547.5 | -14.7 | 4532.8 | | | | |
| -20.00 | 3654.2 | 3964.8 | 7618.9 | 4567.7 | -14.7 | 4553.0 | | | | |
| -20.50 | 4095.1 | 4112.6 | 8207.8 | 4920.7 | -14.7 | 4906.0 | | | | |
| -21.00 | 4361.3 | 4267.4 | 8628.7 | 5173.1 | -14.7 | 5158.4 | | | | |
| -21.50 | 4424.7 | 4422.2 | 8846.9 | 5303.9 | -14.7 | 5289.2 | | | | |
| -22.00 | 4434.3 | 4577.1 | 9011.3 | 5402.5 | -14.7 | 5387.8 | | | | |
| -22.50 | 4440.3 | 4731.9 | 9172.1 | 5498.9 | -14.7 | 5484.2 | | | | |
| -23.00 | 4614.6 | 4886.7 | 9501.2 | 5696.2 | -14.7 | 5681.5 | | | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziwkdraagvermogen | | | Rekenwaarden | | | | |
|-----------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|---------------------------|--------------------------------|------|--------|
| | | | R _{b,real} [kN] | R _{r,real} [kN] | R _{c,real} [kN] | R _d [kN] | F _{bk;d} [kN] | R _{z,netto;d} [kN] | | |
| 283.S02 | 0.17 | -23.50 | 3250.3 | 5041.5 | 8291.7 | 4971.1 | -14.7 | 4956.3 | | |
| | | -24.00 | 1973.0 | 5196.3 | 7169.3 | 4298.1 | -14.7 | 4283.4 | | |
| | | -24.50 | 1606.5 | 5351.1 | 6957.6 | 4171.2 | -14.7 | 4156.5 | | |
| | | -25.00 | 1398.4 | 5505.9 | 6904.3 | 4139.3 | -14.7 | 4124.6 | | |
| | | -25.50 | 1089.3 | 5660.7 | 6750.0 | 4046.7 | -14.7 | 4032.0 | | |
| | | -26.00 | 894.5 | 5815.5 | 6709.9 | 4022.7 | -14.7 | 4008.0 | | |
| | | -26.50 | 676.0 | 5978.4 | 6654.5 | 3989.5 | -14.7 | 3974.8 | | |
| | | -27.00 | 718.8 | 6035.0 | 6753.7 | 4049.0 | -14.7 | 4034.3 | | |
| | | -27.50 | 621.9 | 6088.6 | 6710.5 | 4023.1 | -14.7 | 4008.4 | | |
| | | -28.00 | 616.5 | 6156.1 | 6772.6 | 4060.3 | -14.7 | 4045.6 | | |
| | | -28.50 | 589.8 | 6241.5 | 6831.3 | 4095.5 | -14.7 | 4080.8 | | |
| | | -29.00 | 577.4 | 6302.5 | 6879.9 | 4124.7 | -14.7 | 4110.0 | | |
| | | 19-1008_35 | 0.92 | -7.00 | 1384.4 | 942.4 | 2326.8 | 1395.0 | -9.0 | 1385.9 |
| | | | | -7.50 | 1478.2 | 998.1 | 2476.3 | 1484.6 | -9.0 | 1475.5 |
| | | | | -8.00 | 1458.6 | 1075.5 | 2534.1 | 1519.2 | -9.0 | 1510.2 |
| | | | | -8.50 | 1418.7 | 1153.7 | 2572.4 | 1542.2 | -9.0 | 1533.2 |
| -9.00 | 1450.7 | | | 1213.3 | 2664.0 | 1597.1 | -9.0 | 1588.1 | | |
| -9.50 | 1511.3 | | | 1273.4 | 2784.7 | 1669.5 | -9.0 | 1660.4 | | |
| -10.00 | 1568.8 | | | 1346.1 | 2914.9 | 1747.5 | -9.0 | 1738.5 | | |
| -10.50 | 1622.1 | | | 1414.1 | 3036.3 | 1820.3 | -9.0 | 1811.3 | | |
| -11.00 | 1563.2 | | | 1531.2 | 3094.4 | 1855.2 | -9.0 | 1846.1 | | |
| -11.50 | 1499.0 | | | 1630.9 | 3129.9 | 1876.5 | -9.0 | 1867.4 | | |
| -12.00 | 1478.1 | | | 1699.9 | 3178.0 | 1905.3 | -9.0 | 1896.2 | | |
| -12.50 | 1751.7 | | | 1759.5 | 3511.1 | 2105.0 | -9.0 | 2096.0 | | |
| -13.00 | 1918.9 | | | 1838.9 | 3757.9 | 2252.9 | -9.0 | 2243.9 | | |
| -13.50 | 2036.5 | | | 1932.7 | 3969.2 | 2379.6 | -9.0 | 2370.6 | | |
| -14.00 | 2338.6 | | | 2030.6 | 4369.2 | 2619.4 | -9.0 | 2610.4 | | |
| -14.50 | 2229.2 | | | 2150.8 | 4380.0 | 2625.9 | -9.0 | 2616.8 | | |
| -15.00 | 2260.2 | | | 2271.0 | 4531.2 | 2716.6 | -9.0 | 2707.5 | | |
| -15.50 | 2281.8 | | | 2392.7 | 4674.6 | 2802.5 | -9.0 | 2793.5 | | |
| -16.00 | 2265.1 | | | 2517.5 | 4782.6 | 2867.3 | -9.0 | 2858.2 | | |
| -16.50 | 2145.5 | | | 2642.9 | 4788.4 | 2870.8 | -9.0 | 2861.7 | | |
| -17.00 | 2141.3 | | | 2750.7 | 4892.0 | 2932.9 | -9.0 | 2923.8 | | |
| -17.50 | 2422.3 | | | 2842.0 | 5264.3 | 3156.1 | -9.0 | 3147.0 | | |
| -18.00 | 2457.0 | | | 2963.5 | 5420.5 | 3249.7 | -9.0 | 3240.6 | | |
| -18.50 | 2651.5 | | | 3073.2 | 5724.7 | 3432.1 | -9.0 | 3423.0 | | |
| -19.00 | 2659.5 | | | 3196.7 | 5856.2 | 3510.9 | -9.0 | 3501.8 | | |
| -19.50 | 2799.6 | | | 3318.8 | 6118.4 | 3668.1 | -9.0 | 3659.0 | | |
| -20.00 | 3214.7 | | | 3444.7 | 6659.4 | 3992.5 | -9.0 | 3983.4 | | |
| -20.50 | 3244.2 | | | 3599.5 | 6843.7 | 4102.9 | -9.0 | 4093.9 | | |
| -21.00 | 3291.9 | | | 3754.3 | 7046.2 | 4224.4 | -9.0 | 4215.3 | | |
| -21.50 | 3581.5 | | | 3909.1 | 7490.7 | 4490.8 | -9.0 | 4481.8 | | |
| -22.00 | 3597.9 | 4059.7 | 7657.6 | 4590.9 | -9.0 | 4581.8 | | | | |
| -22.50 | 3642.3 | 4214.5 | 7856.9 | 4710.3 | -9.0 | 4701.3 | | | | |
| -23.00 | 3001.5 | 4369.3 | 7370.8 | 4418.9 | -9.0 | 4409.9 | | | | |
| -23.50 | 2956.0 | 4524.1 | 7480.1 | 4484.5 | -9.0 | 4475.4 | | | | |
| -24.00 | 2943.3 | 4678.9 | 7622.2 | 4569.7 | -9.0 | 4560.6 | | | | |
| -24.50 | 2912.2 | 4830.3 | 7742.5 | 4641.8 | -9.0 | 4632.7 | | | | |
| -25.00 | 2848.0 | 4975.7 | 7823.6 | 4690.4 | -9.0 | 4681.4 | | | | |
| -25.50 | 2495.6 | 5142.0 | 7637.6 | 4578.9 | -9.0 | 4569.9 | | | | |
| -26.00 | 2875.9 | 5297.4 | 8173.3 | 4900.1 | -9.0 | 4891.0 | | | | |
| -26.50 | 3455.5 | 5432.1 | 8887.6 | 5328.3 | -9.0 | 5319.3 | | | | |
| -27.00 | 3592.1 | 5586.9 | 9179.0 | 5503.0 | -9.0 | 5493.9 | | | | |
| -27.50 | 3659.8 | 5741.7 | 9401.5 | 5636.4 | -9.0 | 5627.4 | | | | |
| -28.00 | 3664.5 | 5896.5 | 9561.0 | 5732.0 | -9.0 | 5723.0 | | | | |
| -28.50 | 3982.9 | 6051.3 | 10034.2 | 6015.7 | -9.0 | 6006.7 | | | | |
| -29.00 | 2310.2 | 6206.1 | 8516.3 | 5105.7 | -9.0 | 5096.7 | | | | |
| -29.50 | 1983.7 | 6360.9 | 8344.6 | 5002.8 | -9.0 | 4993.7 | | | | |
| -30.00 | 1613.2 | 6515.7 | 8128.9 | 4873.5 | -9.0 | 4864.4 | | | | |
| 312.S03 | 3.78 | -7.00 | 609.5 | 1273.0 | 1882.4 | 1128.5 | 0.0 | 1128.5 | | |
| | | -7.50 | 1199.9 | 1356.5 | 2556.4 | 1532.6 | 0.0 | 1532.6 | | |
| | | -8.00 | 2184.2 | 1447.4 | 3631.6 | 2177.2 | 0.0 | 2177.2 | | |
| | | -8.50 | 2290.5 | 1602.2 | 3892.6 | 2333.7 | 0.0 | 2333.7 | | |
| | | -9.00 | 2421.4 | 1757.0 | 4178.4 | 2505.0 | 0.0 | 2505.0 | | |
| | | -9.50 | 2385.2 | 1911.8 | 4296.9 | 2576.1 | 0.0 | 2576.1 | | |
| | | -10.00 | 2535.2 | 2066.6 | 4601.8 | 2758.9 | 0.0 | 2758.9 | | |
| | | -10.50 | 2432.8 | 2219.5 | 4652.3 | 2789.1 | 0.0 | 2789.1 | | |
| | | -11.00 | 2509.3 | 2363.8 | 4873.2 | 2921.6 | 0.0 | 2921.6 | | |
| | | -11.50 | 2571.4 | 2518.6 | 5090.0 | 3051.6 | 0.0 | 3051.6 | | |
| | | -12.00 | 2661.0 | 2673.4 | 5334.4 | 3198.1 | 0.0 | 3198.1 | | |
| | | -12.50 | 2442.4 | 2828.2 | 5270.6 | 3159.8 | 0.0 | 3159.8 | | |
| | | -13.00 | 2576.8 | 2978.5 | 5555.3 | 3330.5 | 0.0 | 3330.5 | | |
| | | -13.50 | 2803.8 | 3087.6 | 5891.4 | 3532.0 | 0.0 | 3532.0 | | |
| | | -14.00 | 2797.8 | 3211.5 | 6009.3 | 3602.7 | 0.0 | 3602.7 | | |
| | | -14.50 | 2595.7 | 3335.3 | 5931.0 | 3555.7 | 0.0 | 3555.7 | | |
| | | -15.00 | 2533.6 | 3453.8 | 5987.3 | 3589.5 | 0.0 | 3589.5 | | |
| | | -15.50 | 2490.9 | 3577.6 | 6068.5 | 3638.2 | 0.0 | 3638.2 | | |
| | | -16.00 | 2495.6 | 3697.4 | 6193.0 | 3712.8 | 0.0 | 3712.8 | | |
| | | -16.50 | 2356.2 | 3821.2 | 6177.5 | 3703.5 | 0.0 | 3703.5 | | |
| | | -17.00 | 2265.2 | 3935.7 | 6200.9 | 3717.5 | 0.0 | 3717.5 | | |
| | | -17.50 | 1376.2 | 4025.2 | 5401.4 | 3238.2 | 0.0 | 3238.2 | | |
| | | -18.00 | 1447.3 | 4121.2 | 5568.5 | 3338.4 | 0.0 | 3338.4 | | |
| | | -18.50 | 1447.8 | 4241.7 | 5689.5 | 3411.0 | 0.0 | 3411.0 | | |
| -19.00 | 1439.9 | 4368.4 | 5808.3 | 3482.2 | 0.0 | 3482.2 | | | | |
| -19.50 | 1207.3 | 4499.8 | 5707.1 | 3421.5 | 0.0 | 3421.5 | | | | |
| -20.00 | 1116.1 | 4626.3 | 5742.4 | 3442.7 | 0.0 | 3442.7 | | | | |
| -20.50 | 1711.2 | 4737.1 | 6448.3 | 3865.9 | 0.0 | 3865.9 | | | | |
| -21.00 | 2005.5 | 4859.5 | 6865.0 | 4115.7 | 0.0 | 4115.7 | | | | |
| -21.50 | 2231.3 | 4973.2 | 7204.5 | 4319.2 | 0.0 | 4319.2 | | | | |
| -22.00 | 2440.1 | 5101.7 | 7541.8 | 4521.5 | 0.0 | 4521.5 | | | | |
| -22.50 | 2531.2 | 5252.7 | 7783.9 | 4666.6 | 0.0 | 4666.6 | | | | |
| -23.00 | 2558.9 | 5404.7 | 7963.6 | 4774.4 | 0.0 | 4774.4 | | | | |
| -23.50 | 2695.0 | 5552.2 | 8247.2 | 4944.3 | 0.0 | 4944.3 | | | | |
| -24.00 | 2947.9 | 5687.4 | 8635.3 | 5177.1 | 0.0 | 5177.1 | | | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | |
|-----------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|---------------------------|--------------------------------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _{e,d} [kN] | F _{bk,d} [kN] | R _{z,netto,d} [kN] |
| 312.S03 | 3.78 | -24.50 | 1786.5 | 5842.2 | 7628.7 | 4573.6 | 0.0 | 4573.6 |
| | | -25.00 | 1544.0 | 5997.0 | 7541.0 | 4521.0 | 0.0 | 4521.0 |
| | | -25.50 | 1278.2 | 6142.4 | 7420.6 | 4448.8 | 0.0 | 4448.8 |
| | | -26.00 | 1140.4 | 6272.3 | 7412.7 | 4444.1 | 0.0 | 4444.1 |
| | | -26.50 | 976.0 | 6423.7 | 7399.7 | 4436.3 | 0.0 | 4436.3 |
| | | -27.00 | 765.3 | 6575.1 | 7340.5 | 4400.8 | 0.0 | 4400.8 |
| | | -27.50 | 731.8 | 6656.3 | 7388.1 | 4429.3 | 0.0 | 4429.3 |
| | | -28.00 | 715.6 | 6720.7 | 7436.3 | 4458.2 | 0.0 | 4458.2 |
| | | -28.50 | 713.5 | 6770.1 | 7483.6 | 4486.6 | 0.0 | 4486.6 |
| | | -29.00 | 791.7 | 6818.6 | 7610.3 | 4562.5 | 0.0 | 4562.5 |
| | | 19-1008_43 | 9.88 | -7.00 | 2028.6 | 1078.2 | 3106.8 | 1862.6 |
| -7.50 | 2079.8 | | | 1193.7 | 3273.5 | 1962.5 | 0.0 | 1962.5 |
| -8.00 | 2127.5 | | | 1313.8 | 3441.4 | 2063.2 | 0.0 | 2063.2 |
| -8.50 | 2176.4 | | | 1426.0 | 3602.4 | 2159.7 | 0.0 | 2159.7 |
| -9.00 | 2229.5 | | | 1540.6 | 3770.1 | 2260.2 | 0.0 | 2260.2 |
| -9.50 | 2252.4 | | | 1658.0 | 3910.4 | 2344.4 | 0.0 | 2344.4 |
| -10.00 | 2670.3 | | | 1765.0 | 4435.3 | 2659.0 | 0.0 | 2659.0 |
| -10.50 | 2648.9 | | | 1893.8 | 4542.7 | 2723.4 | 0.0 | 2723.4 |
| -11.00 | 2610.7 | | | 2048.6 | 4659.3 | 2793.3 | 0.0 | 2793.3 |
| -11.50 | 2638.7 | | | 2203.4 | 4842.1 | 2903.0 | 0.0 | 2903.0 |
| -12.00 | 2642.2 | | | 2358.1 | 5000.2 | 2997.7 | 0.0 | 2997.7 |
| -12.50 | 2509.7 | | | 2511.6 | 5021.3 | 3010.4 | 0.0 | 3010.4 |
| -13.00 | 2468.3 | | | 2625.8 | 5094.2 | 3054.1 | 0.0 | 3054.1 |
| -13.50 | 2640.5 | | | 2724.2 | 5364.7 | 3216.2 | 0.0 | 3216.2 |
| -14.00 | 2656.9 | | | 2838.9 | 5495.7 | 3294.8 | 0.0 | 3294.8 |
| -14.50 | 2532.2 | | | 2962.7 | 5494.9 | 3294.3 | 0.0 | 3294.3 |
| -15.00 | 3154.3 | | | 3071.0 | 6225.3 | 3732.2 | 0.0 | 3732.2 |
| -15.50 | 2898.5 | | | 3205.8 | 6104.3 | 3659.6 | 0.0 | 3659.6 |
| -16.00 | 2573.9 | | | 3354.6 | 5928.5 | 3554.3 | 0.0 | 3554.3 |
| -16.50 | 2138.4 | | | 3509.4 | 5647.8 | 3386.0 | 0.0 | 3386.0 |
| -17.00 | 1956.4 | | | 3664.2 | 5620.6 | 3369.7 | 0.0 | 3369.7 |
| -17.50 | 1907.4 | 3813.3 | 5720.7 | 3429.7 | 0.0 | 3429.7 | | |
| -18.00 | 1858.6 | 3948.3 | 5806.9 | 3481.4 | 0.0 | 3481.4 | | |
| -18.50 | 1786.9 | 4069.1 | 5856.0 | 3510.8 | 0.0 | 3510.8 | | |
| -19.00 | 1697.2 | 4190.1 | 5887.3 | 3529.5 | 0.0 | 3529.5 | | |
| -19.50 | 1759.3 | 4287.9 | 6047.2 | 3625.4 | 0.0 | 3625.4 | | |
| -20.00 | 1994.8 | 4388.9 | 6383.6 | 3827.1 | 0.0 | 3827.1 | | |
| -20.50 | 2051.0 | 4516.4 | 6567.4 | 3937.3 | 0.0 | 3937.3 | | |
| -21.00 | 2208.6 | 4664.4 | 6873.0 | 4120.5 | 0.0 | 4120.5 | | |
| -21.50 | 2977.5 | 4786.8 | 7764.3 | 4654.9 | 0.0 | 4654.9 | | |
| -22.00 | 3042.6 | 4925.5 | 7968.1 | 4777.0 | 0.0 | 4777.0 | | |
| 328.S02 | 10.17 | -7.00 | 1590.9 | 1736.8 | 3327.6 | 1995.0 | 0.0 | 1995.0 |
| | | -7.50 | 1662.1 | 1844.6 | 3506.6 | 2102.3 | 0.0 | 2102.3 |
| | | -8.00 | 1704.1 | 1963.4 | 3667.4 | 2198.7 | 0.0 | 2198.7 |
| | | -8.50 | 1686.4 | 2085.2 | 3771.6 | 2261.2 | 0.0 | 2261.2 |
| | | -9.00 | 1980.9 | 2204.1 | 4185.0 | 2509.0 | 0.0 | 2509.0 |
| | | -9.50 | 2149.4 | 2305.9 | 4455.3 | 2671.0 | 0.0 | 2671.0 |
| | | -10.00 | 2371.3 | 2420.6 | 4791.9 | 2872.9 | 0.0 | 2872.9 |
| | | -10.50 | 2526.4 | 2541.1 | 5067.5 | 3038.1 | 0.0 | 3038.1 |
| | | -11.00 | 2625.3 | 2679.6 | 5304.9 | 3180.4 | 0.0 | 3180.4 |
| | | -11.50 | 2602.0 | 2821.9 | 5423.9 | 3251.7 | 0.0 | 3251.7 |
| | | -12.00 | 2637.6 | 2959.4 | 5597.0 | 3355.5 | 0.0 | 3355.5 |
| | | -12.50 | 2694.8 | 3083.6 | 5778.4 | 3464.3 | 0.0 | 3464.3 |
| | | -13.00 | 2278.8 | 3204.8 | 5483.5 | 3287.5 | 0.0 | 3287.5 |
| | | -13.50 | 2259.6 | 3327.3 | 5586.8 | 3349.4 | 0.0 | 3349.4 |
| | | -14.00 | 2243.5 | 3451.1 | 5694.6 | 3414.0 | 0.0 | 3414.0 |
| | | -14.50 | 2256.1 | 3571.3 | 5827.4 | 3493.6 | 0.0 | 3493.6 |
| | | -15.00 | 2212.9 | 3696.5 | 5909.4 | 3542.8 | 0.0 | 3542.8 |
| | | -15.50 | 2048.9 | 3820.1 | 5868.9 | 3518.5 | 0.0 | 3518.5 |
| | | -16.00 | 2182.6 | 3942.7 | 6125.3 | 3672.2 | 0.0 | 3672.2 |
| | | -16.50 | 2308.3 | 4071.1 | 6379.4 | 3824.6 | 0.0 | 3824.6 |
| | | -17.00 | 2372.8 | 4225.9 | 6598.7 | 3956.1 | 0.0 | 3956.1 |
| -17.50 | 2285.6 | 4380.7 | 6666.3 | 3996.6 | 0.0 | 3996.6 | | |
| -18.00 | 1500.6 | 4558.4 | 6059.0 | 3632.5 | 0.0 | 3632.5 | | |
| -18.50 | 2662.9 | 4668.6 | 7331.5 | 4395.4 | 0.0 | 4395.4 | | |
| -19.00 | 2697.0 | 4807.2 | 7504.2 | 4498.9 | 0.0 | 4498.9 | | |
| -19.50 | 2960.8 | 4955.0 | 7915.7 | 4745.7 | 0.0 | 4745.7 | | |
| -20.00 | 3076.6 | 5109.8 | 8186.4 | 4907.9 | 0.0 | 4907.9 | | |
| -20.50 | 3383.0 | 5264.6 | 8647.6 | 5184.4 | 0.0 | 5184.4 | | |
| -21.00 | 3500.9 | 5419.4 | 8920.2 | 5347.9 | 0.0 | 5347.9 | | |
| -21.50 | 3232.8 | 5574.2 | 8806.9 | 5279.9 | 0.0 | 5279.9 | | |
| -22.00 | 3339.1 | 5729.0 | 9068.1 | 5436.5 | 0.0 | 5436.5 | | |
| -22.50 | 3099.6 | 5883.8 | 8983.4 | 5385.7 | 0.0 | 5385.7 | | |
| -23.00 | 3168.5 | 6038.6 | 9207.1 | 5519.8 | 0.0 | 5519.8 | | |
| -23.50 | 3130.6 | 6193.4 | 9324.0 | 5589.9 | 0.0 | 5589.9 | | |
| -24.00 | 3105.8 | 6348.2 | 9453.9 | 5667.8 | 0.0 | 5667.8 | | |
| -24.50 | 3174.7 | 6477.2 | 9651.9 | 5786.5 | 0.0 | 5786.5 | | |
| -25.00 | 2918.6 | 6601.1 | 9519.6 | 5707.2 | 0.0 | 5707.2 | | |
| -25.50 | 2454.0 | 6722.4 | 9176.4 | 5501.5 | 0.0 | 5501.5 | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

REKENGEGEVENS SI Ø762/950 druk

Berekening : Ontwerpend
Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2
Sondering(en) : 19-1008_1, 19-1008_6, 166.S01, 19-1008_11, 19-1008_12
: 19-1008_17, 19-1008_20, 19-1008_21, 251.S01, 19-1008_29
: 283.S02, 19-1008_35, 312.S03, 19-1008_43, 328.S02

Stijf bouwwerk : NEE
Paalgroep : NEE
Aantal sonderingen : 15
Factor $\xi_{s(n-1)}$: 1.39 (handmatig)
Factor $\xi_{s(gem)}$: 1.39 (handmatig)
Factor $\xi_{s(min)}$: 1.39 (handmatig)
Weerstandsfactor γ_R : 1.20
 $\gamma_{f,nk}$: 1.0
 $R_{b,calc,max;i}$ begrenzen op $0.75 * R_{b,calc,max;i}$: NEE
UGT draagvermogen zonder negatieve kleef : NEE

Paal : SI Ø762/950
Niveau paalkop [m] : N.A.P. 0.00
Bovenbel. [kN/m²] : 0.00

PAALPUNTNIVEAUS SI Ø762/950

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

Nr Beginniveau Eindniveau Stapgrootte
[m] [m] [m]

| | | | |
|---|-------|--------|------|
| 1 | -8.00 | -30.00 | 0.50 |
|---|-------|--------|------|

RESULTATEN SI Ø762/950 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Sondering | 19-1008_1 | 19-1008_6 | 166.S01 | 19-1008_11 | 19-1008_12 | 19-1008_17 |
|-----------|---------------|---------------|---------------|---------------|---------------|---------------|
| Niveau | $F_{netto;d}$ | $F_{netto;d}$ | $F_{netto;d}$ | $F_{netto;d}$ | $F_{netto;d}$ | $F_{netto;d}$ |
| [m] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] |
| -8.00 | 34 | 5504 | 3437 | 402 | 1871 | -29 |
| -8.50 | 89 | 5803 | 3463 | 440 | 1895 | -4 |
| -9.00 | 223 | 5934 | 3600 | 440 | 1920 | 66 |
| -9.50 | 270 | 6181 | 3531 | 491 | 1924 | 574 |
| -10.00 | 321 | 6752 | 3636 | 546 | 1946 | 351 |
| -10.50 | 448 | 6802 | 3770 | 583 | 1982 | 1161 |
| -11.00 | 596 | 7035 | 3876 | 633 | 1983 | 2105 |
| -11.50 | 677 | 7217 | 3832 | 646 | 2028 | 1986 |
| -12.00 | 738 | 7374 | 3812 | 619 | 2038 | 2190 |
| -12.50 | 1345 | 7450 | 3871 | 1537 | 2050 | 2351 |
| -13.00 | 1464 | 7512 | 4287 | 1790 | 2123 | 2396 |
| -13.50 | 1694 | 7960 | 4717 | 1918 | 2209 | 2479 |
| -14.00 | 1924 | 8070 | 4855 | 2049 | 2251 | 2579 |
| -14.50 | 2207 | 7824 | 5017 | 2156 | 2285 | 3000 |
| -15.00 | 2372 | 6376 | 5251 | 2246 | 2321 | 2233 |
| -15.50 | 2290 | 6420 | 5702 | 2380 | 2437 | 2320 |
| -16.00 | 2619 | 6381 | 5837 | 2642 | 2502 | 2422 |
| -16.50 | 2795 | 6446 | 5930 | 2748 | 2562 | 2516 |
| -17.00 | 3591 | 6413 | 6069 | 2898 | 2636 | 2664 |
| -17.50 | 3961 | 6382 | 6233 | 3654 | 2826 | 2563 |
| -18.00 | 3622 | 7255 | 6394 | 4265 | 3098 | 2481 |
| -18.50 | 3769 | 7834 | 6544 | 4407 | 3220 | 2987 |
| -19.00 | 3778 | 7950 | 6653 | 4596 | 3718 | 3127 |
| -19.50 | 3744 | 8079 | 0 | 4708 | 4107 | 3253 |
| -20.00 | 3681 | 8223 | 0 | 4243 | 4372 | 3402 |
| -20.50 | 3840 | 0 | 0 | 4179 | 4312 | 3632 |
| -21.00 | 4177 | 0 | 0 | 4193 | 4860 | 3495 |
| -21.50 | 5816 | 0 | 0 | 4270 | 5031 | 3888 |
| -22.00 | 7334 | 0 | 0 | 4136 | 5219 | 3956 |
| -22.50 | 7443 | 0 | 0 | 4110 | 5146 | 4032 |
| -23.00 | 7552 | 0 | 0 | 4075 | 4873 | 4025 |
| -23.50 | 7662 | 0 | 0 | 4416 | 4883 | 4084 |
| -24.00 | 7771 | 0 | 0 | 4536 | 4892 | 4172 |
| -24.50 | 7880 | 0 | 0 | 4580 | 4727 | 4232 |
| -25.00 | 7990 | 0 | 0 | 4830 | 4758 | 4327 |
| -25.50 | 8099 | 0 | 0 | 5712 | 4768 | 4418 |
| -26.00 | 8208 | 0 | 0 | 5817 | 4851 | 3567 |
| -26.50 | 8318 | 0 | 0 | 5893 | 4938 | 3598 |
| -27.00 | 8427 | 0 | 0 | 6019 | 5010 | 3670 |
| -27.50 | 8536 | 0 | 0 | 6199 | 5072 | 3735 |
| -28.00 | 8646 | 0 | 0 | 6676 | 6054 | 3782 |
| -28.50 | 8755 | 0 | 0 | 6941 | 0 | 3749 |
| -29.00 | 8864 | 0 | 0 | 7529 | 0 | 3600 |
| -29.50 | 0 | 0 | 0 | 8297 | 0 | 4665 |
| -30.00 | 0 | 0 | 0 | 8455 | 0 | 5110 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø762/950 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | 19-1008_20 | 19-1008_21 | 251.S01 | 19-1008_29 | 283.S02 | 19-1008_35 |
|---------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|
| | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] |
| -8.00 | 776 | 1277 | 910 | 2523 | 2235 | 1962 |
| -8.50 | 828 | 1246 | 955 | 1823 | 2005 | 1984 |
| -9.00 | 854 | 1317 | 1516 | 1901 | 2073 | 2074 |
| -9.50 | 867 | 1508 | 1613 | 1978 | 2129 | 2144 |
| -10.00 | 821 | 1594 | 1702 | 2057 | 2184 | 2281 |
| -10.50 | 1006 | 1694 | 1753 | 2102 | 2228 | 2334 |
| -11.00 | 1030 | 1757 | 1777 | 2079 | 2271 | 2367 |
| -11.50 | 975 | 1814 | 1876 | 2190 | 2308 | 2383 |
| -12.00 | 1036 | 1760 | 1957 | 2190 | 2785 | 2415 |
| -12.50 | 1074 | 1848 | 2060 | 2223 | 3043 | 2702 |
| -13.00 | 1085 | 1958 | 2164 | 2192 | 3311 | 2875 |
| -13.50 | 1188 | 1845 | 2262 | 2234 | 3461 | 3052 |
| -14.00 | 1216 | 1841 | 2310 | 2271 | 3612 | 3247 |
| -14.50 | 1260 | 1977 | 2284 | 2306 | 3664 | 3348 |
| -15.00 | 1301 | 1913 | 2339 | 2417 | 3786 | 3454 |
| -15.50 | 1334 | 1976 | 3062 | 2472 | 4025 | 3556 |
| -16.00 | 1375 | 1970 | 3146 | 2466 | 4340 | 3628 |
| -16.50 | 1404 | 1879 | 3273 | 2506 | 4686 | 3614 |
| -17.00 | 1502 | 1950 | 3391 | 2725 | 4927 | 3724 |
| -17.50 | 1699 | 2066 | 3462 | 3694 | 5102 | 3977 |
| -18.00 | 1775 | 2100 | 2956 | 4025 | 5285 | 4149 |
| -18.50 | 1883 | 2140 | 2990 | 4024 | 5479 | 4321 |
| -19.00 | 1957 | 2178 | 2977 | 4031 | 5663 | 4425 |
| -19.50 | 2011 | 2198 | 2997 | 4591 | 5782 | 4733 |
| -20.00 | 2069 | 2216 | 3009 | 4435 | 5786 | 5081 |
| -20.50 | 2044 | 2241 | 3038 | 4371 | 6364 | 5207 |
| -21.00 | 2040 | 2280 | 3078 | 4325 | 6573 | 5357 |
| -21.50 | 2073 | 2317 | 3101 | 4239 | 6737 | 5631 |
| -22.00 | 2111 | 2354 | 3120 | 4108 | 6860 | 5804 |
| -22.50 | 2233 | 2387 | 3235 | 4050 | 6979 | 5467 |
| -23.00 | 2700 | 2422 | 3317 | 4089 | 5898 | 5542 |
| -23.50 | 2885 | 2474 | 3481 | 4213 | 5202 | 5654 |
| -24.00 | 3120 | 2512 | 3550 | 4278 | 5072 | 5742 |
| -24.50 | 3239 | 2545 | 3716 | 4297 | 4995 | 5824 |
| -25.00 | 3355 | 2582 | 3996 | 4343 | 4963 | 5873 |
| -25.50 | 3466 | 2618 | 4564 | 4421 | 4840 | 5727 |
| -26.00 | 3377 | 2653 | 5368 | 4468 | 4810 | 6175 |
| -26.50 | 3484 | 2688 | 5607 | 4523 | 4768 | 6687 |
| -27.00 | 3517 | 2722 | 5464 | 4568 | 4760 | 6907 |
| -27.50 | 3611 | 2784 | 5147 | 4628 | 4801 | 7062 |
| -28.00 | 3707 | 2825 | 5039 | 4678 | 4844 | 7165 |
| -28.50 | 3800 | 2862 | 4970 | 4772 | 4882 | 6154 |
| -29.00 | 3884 | 2915 | 4859 | 5163 | 0 | 6089 |
| -29.50 | 3787 | 2961 | 4905 | 5195 | 0 | 5950 |
| -30.00 | 3877 | 0 | 4846 | 5132 | 0 | 5792 |

RESULTATEN SI Ø762/950 druk (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | 312.S03 | 19-1008_43 | 328.S02 |
|---------------|-------------------------------|-------------------------------|-------------------------------|
| | F _{nettoord} [kN] | F _{nettoord} [kN] | F _{nettoord} [kN] |
| -8.00 | 2834 | 2663 | 2773 |
| -8.50 | 3020 | 2790 | 2839 |
| -9.00 | 3227 | 2908 | 3161 |
| -9.50 | 3294 | 3003 | 3356 |
| -10.00 | 3391 | 3374 | 3620 |
| -10.50 | 3526 | 3464 | 3819 |
| -11.00 | 3694 | 3562 | 3938 |
| -11.50 | 3804 | 3656 | 4075 |
| -12.00 | 4020 | 3775 | 4230 |
| -12.50 | 3937 | 3807 | 4035 |
| -13.00 | 4203 | 3901 | 4116 |
| -13.50 | 4369 | 4119 | 4213 |
| -14.00 | 4403 | 4213 | 4285 |
| -14.50 | 4466 | 4202 | 4378 |
| -15.00 | 4548 | 4575 | 4276 |
| -15.50 | 4599 | 4362 | 4403 |
| -16.00 | 4688 | 4204 | 4601 |
| -16.50 | 4659 | 4160 | 4796 |
| -17.00 | 3878 | 4213 | 4959 |
| -17.50 | 3988 | 4277 | 4996 |
| -18.00 | 4115 | 4335 | 4615 |
| -18.50 | 4201 | 4361 | 5512 |
| -19.00 | 4283 | 4371 | 5628 |
| -19.50 | 4183 | 4507 | 5935 |
| -20.00 | 4318 | 4759 | 6148 |
| -20.50 | 4767 | 4884 | 6475 |
| -21.00 | 5088 | 5139 | 6380 |
| -21.50 | 5396 | 5826 | 6564 |
| -22.00 | 5596 | 0 | 6512 |
| -22.50 | 5750 | 0 | 6686 |
| -23.00 | 5882 | 0 | 6763 |
| -23.50 | 6132 | 0 | 6903 |
| -24.00 | 5534 | 0 | 6975 |
| -24.50 | 5479 | 0 | 6894 |
| -25.00 | 5347 | 0 | 6650 |
| -25.50 | 5315 | 0 | 0 |
| -26.00 | 5307 | 0 | 0 |
| -26.50 | 5332 | 0 | 0 |
| -27.00 | 5279 | 0 | 0 |
| -27.50 | 5310 | 0 | 0 |
| -28.00 | 5342 | 0 | 0 |
| -28.50 | 5375 | 0 | 0 |
| -29.00 | 0 | 0 | 0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

-29.50 0 0 0
 -30.00 0 0 0

SAMENVATTINGSTABEL SI Ø762/950 druk (n=1)

Uitgangspunten

- paal : SI Ø762/950
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie
 - schachtafmeting : 860 mm
 Paalklassefactor α_p : 0.63
 Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
 Correlatiefactor $\xi_{3(n-1)}$: 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bewijkdraagvermogen | | | Rekenwaarden | | |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
| | | | $R_{b,real}$ [kN] | $R_{s,real}$ [kN] | $R_{z,real}$ [kN] | $R_{b,d}$ [kN] | $F_{nk,d}$ [kN] | $R_{z,netto,d}$ [kN] |
| 19-1008_1 | 2.12 | -8.00 | 294.1 | 43.8 | 337.9 | 202.6 | -168.2 | 34.4 |
| | | -8.50 | 339.6 | 89.4 | 429.0 | 257.2 | -168.2 | 89.0 |
| | | -9.00 | 549.9 | 103.2 | 653.1 | 391.5 | -168.2 | 223.4 |
| | | -9.50 | 552.8 | 178.7 | 731.4 | 438.5 | -168.2 | 270.4 |
| | | -10.00 | 569.5 | 245.8 | 815.3 | 488.8 | -168.2 | 320.6 |
| | | -10.50 | 702.5 | 324.4 | 1026.9 | 615.7 | -168.2 | 447.5 |
| | | -11.00 | 897.4 | 377.9 | 1275.3 | 764.6 | -168.2 | 596.4 |
| | | -11.50 | 938.5 | 470.7 | 1409.2 | 844.8 | -168.2 | 676.7 |
| | | -12.00 | 921.8 | 590.3 | 1512.1 | 906.5 | -168.2 | 738.4 |
| | | -12.50 | 1853.7 | 669.5 | 2523.1 | 1512.7 | -168.2 | 1344.5 |
| | | -13.00 | 1925.9 | 797.3 | 2723.2 | 1632.6 | -168.2 | 1464.5 |
| | | -13.50 | 2181.4 | 925.0 | 3106.5 | 1862.4 | -168.2 | 1694.2 |
| | | -14.00 | 2455.4 | 1035.0 | 3490.4 | 2092.6 | -168.2 | 1924.4 |
| | | -14.50 | 2781.8 | 1180.0 | 3961.8 | 2375.2 | -168.2 | 2207.0 |
| | | -15.00 | 2924.9 | 1312.1 | 4237.0 | 2540.1 | -168.2 | 2372.0 |
| | | -15.50 | 2642.6 | 1456.9 | 4099.5 | 2457.7 | -168.2 | 2289.6 |
| | | -16.00 | 3067.9 | 1580.8 | 4648.8 | 2787.0 | -168.2 | 2618.9 |
| | | -16.50 | 3225.6 | 1717.4 | 4943.0 | 2963.4 | -168.2 | 2795.3 |
| | | -17.00 | 4413.5 | 1856.2 | 6269.7 | 3758.8 | -168.2 | 3590.7 |
| | | -17.50 | 4868.9 | 2018.7 | 6887.6 | 4129.3 | -168.2 | 3961.1 |
| | | -18.00 | 4120.4 | 2201.1 | 6321.5 | 3789.9 | -168.2 | 3621.7 |
| | | -18.50 | 4183.7 | 2383.4 | 6567.2 | 3937.2 | -168.2 | 3769.0 |
| | | -19.00 | 4016.6 | 2565.8 | 6582.4 | 3946.3 | -168.2 | 3778.1 |
| | | -19.50 | 3776.6 | 2748.2 | 6524.7 | 3911.7 | -168.2 | 3743.6 |
| | | -20.00 | 3447.5 | 2973.3 | 6420.8 | 3849.4 | -168.2 | 3681.2 |
| | | -20.50 | 3478.9 | 3206.9 | 6685.8 | 4008.3 | -168.2 | 3840.1 |
| | | -21.00 | 3797.1 | 3450.0 | 7247.1 | 4344.8 | -168.2 | 4176.6 |
| | | -21.50 | 6363.8 | 3617.5 | 9981.2 | 5984.0 | -168.2 | 5815.8 |
| | | -22.00 | 8713.2 | 3799.8 | 12513.0 | 7501.8 | -168.2 | 7333.7 |
| -22.50 | 8713.2 | 3982.2 | 12695.4 | 7611.2 | -168.2 | 7443.0 | | |
| -23.00 | 8713.2 | 4164.6 | 12877.8 | 7720.5 | -168.2 | 7552.3 | | |
| -23.50 | 8713.2 | 4346.9 | 13060.1 | 7829.8 | -168.2 | 7661.7 | | |
| -24.00 | 8713.2 | 4529.3 | 13242.5 | 7939.2 | -168.2 | 7771.0 | | |
| -24.50 | 8713.2 | 4711.7 | 13424.9 | 8048.5 | -168.2 | 7880.3 | | |
| -25.00 | 8713.2 | 4894.0 | 13607.3 | 8157.8 | -168.2 | 7989.7 | | |
| -25.50 | 8713.2 | 5076.4 | 13789.6 | 8267.2 | -168.2 | 8099.0 | | |
| -26.00 | 8713.2 | 5258.8 | 13972.0 | 8376.5 | -168.2 | 8208.3 | | |
| -26.50 | 8713.2 | 5441.2 | 14154.4 | 8485.8 | -168.2 | 8317.7 | | |
| -27.00 | 8713.2 | 5623.5 | 14336.7 | 8595.2 | -168.2 | 8427.0 | | |
| -27.50 | 8713.2 | 5805.9 | 14519.1 | 8704.5 | -168.2 | 8536.3 | | |
| -28.00 | 8713.2 | 5988.3 | 14701.5 | 8813.8 | -168.2 | 8645.7 | | |
| -28.50 | 8713.2 | 6170.6 | 14883.8 | 8923.2 | -168.2 | 8755.0 | | |
| -29.00 | 8713.2 | 6353.0 | 15066.2 | 9032.5 | -168.2 | 8864.3 | | |
| 19-1008_6 | 11.00 | -8.00 | 6622.1 | 2558.8 | 9180.9 | 5504.2 | 0.0 | 5504.2 |
| | | -8.50 | 6937.6 | 2741.2 | 9678.7 | 5802.6 | 0.0 | 5802.6 |
| | | -9.00 | 6973.7 | 2923.5 | 9897.2 | 5933.6 | 0.0 | 5933.6 |
| | | -9.50 | 7204.7 | 3105.9 | 10310.6 | 6181.4 | 0.0 | 6181.4 |
| | | -10.00 | 7974.9 | 3288.3 | 11263.2 | 6752.5 | 0.0 | 6752.5 |
| | | -10.50 | 7875.3 | 3470.6 | 11346.0 | 6802.1 | 0.0 | 6802.1 |
| | | -11.00 | 8082.2 | 3653.0 | 11735.2 | 7035.5 | 0.0 | 7035.5 |
| | | -11.50 | 8203.2 | 3835.4 | 12038.5 | 7217.4 | 0.0 | 7217.4 |
| | | -12.00 | 8282.8 | 4017.7 | 12300.6 | 7374.4 | 0.0 | 7374.4 |
| | | -12.50 | 8226.4 | 4200.1 | 12426.5 | 7449.9 | 0.0 | 7449.9 |
| | | -13.00 | 8148.1 | 4382.5 | 12530.6 | 7512.3 | 0.0 | 7512.3 |
| | | -13.50 | 8713.2 | 4564.8 | 13278.1 | 7960.5 | 0.0 | 7960.5 |
| | | -14.00 | 8713.2 | 4747.2 | 13460.4 | 8069.8 | 0.0 | 8069.8 |
| | | -14.50 | 8120.1 | 4929.6 | 13049.7 | 7823.6 | 0.0 | 7823.6 |
| | | -15.00 | 5522.5 | 5112.0 | 10634.5 | 6375.6 | 0.0 | 6375.6 |
| | | -15.50 | 5413.7 | 5294.3 | 10708.0 | 6419.7 | 0.0 | 6419.7 |
| -16.00 | 5166.4 | 5476.7 | 10643.1 | 6380.8 | 0.0 | 6380.8 | | |
| -16.50 | 5092.9 | 5659.1 | 10752.0 | 6446.0 | 0.0 | 6446.0 | | |
| -17.00 | 4855.8 | 5841.4 | 10697.2 | 6413.2 | 0.0 | 6413.2 | | |
| -17.50 | 4621.0 | 6023.8 | 10644.8 | 6381.8 | 0.0 | 6381.8 | | |
| -18.00 | 5895.7 | 6206.2 | 12101.9 | 7255.3 | 0.0 | 7255.3 | | |
| -18.50 | 6691.2 | 6376.3 | 13067.5 | 7834.2 | 0.0 | 7834.2 | | |
| -19.00 | 6701.8 | 6558.7 | 13260.5 | 7949.9 | 0.0 | 7949.9 | | |
| -19.50 | 6735.0 | 6741.1 | 13476.0 | 8079.2 | 0.0 | 8079.2 | | |
| -20.00 | 6793.1 | 6923.4 | 13716.5 | 8223.3 | 0.0 | 8223.3 | | |
| 166.S01 | 3.45 | -8.00 | 4192.9 | 1562.4 | 5755.3 | 3450.4 | -12.9 | 3437.5 |
| | | -8.50 | 4054.8 | 1743.4 | 5798.2 | 3476.1 | -12.9 | 3463.2 |
| | | -9.00 | 4102.7 | 1924.2 | 6026.8 | 3613.2 | -12.9 | 3600.3 |
| | | -9.50 | 3808.8 | 2102.3 | 5911.1 | 3543.8 | -12.9 | 3530.9 |
| | | -10.00 | 3801.2 | 2284.7 | 6085.9 | 3648.6 | -12.9 | 3635.7 |
| | | -10.50 | 3843.1 | 2467.1 | 6310.1 | 3783.1 | -12.9 | 3770.1 |
| | | -11.00 | 3837.4 | 2649.4 | 6486.8 | 3889.0 | -12.9 | 3876.0 |
| | | -11.50 | 3581.2 | 2831.8 | 6413.1 | 3844.8 | -12.9 | 3831.8 |
| | | -12.00 | 3380.8 | 2999.4 | 6380.2 | 3825.1 | -12.9 | 3812.1 |
| | | -12.50 | 3338.0 | 3141.0 | 6479.0 | 3884.3 | -12.9 | 3871.4 |
| | | -13.00 | 3898.5 | 3273.5 | 7172.0 | 4299.8 | -12.9 | 4286.8 |
| | | -13.50 | 4482.3 | 3408.0 | 7890.3 | 4730.4 | -12.9 | 4717.5 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziijkdraagvermogen | | | Rekenwaarden | | | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|---------------------------|--------------------------------|--------|-------|
| | | | R _{z,real} [kN] | R _{z,real} [kN] | R _{z,real} [kN] | R _{z,d} [kN] | F _{nk,d} [kN] | R _{z,netto,d} [kN] | | |
| 166.S01 | 3.45 | -14.00 | 4555.4 | 3564.7 | 8120.0 | 4868.1 | -12.9 | 4855.2 | | |
| | | -14.50 | 4645.1 | 3745.1 | 8390.2 | 5030.1 | -12.9 | 5017.2 | | |
| | | -15.00 | 4852.6 | 3927.5 | 8780.1 | 5263.8 | -12.9 | 5250.9 | | |
| | | -15.50 | 5422.6 | 4109.8 | 9532.5 | 5714.9 | -12.9 | 5702.0 | | |
| | | -16.00 | 5465.6 | 4292.2 | 9757.8 | 5850.0 | -12.9 | 5837.0 | | |
| | | -16.50 | 5439.0 | 4474.6 | 9913.5 | 5943.4 | -12.9 | 5930.4 | | |
| | | -17.00 | 5487.3 | 4657.0 | 10144.3 | 6081.7 | -12.9 | 6068.8 | | |
| | | -17.50 | 5579.3 | 4839.3 | 10418.6 | 6246.2 | -12.9 | 6233.2 | | |
| | | -18.00 | 5665.6 | 5021.7 | 10687.3 | 6407.3 | -12.9 | 6394.3 | | |
| | | -18.50 | 5733.3 | 5204.1 | 10937.4 | 6557.2 | -12.9 | 6544.2 | | |
| | | -19.00 | 5732.3 | 5386.4 | 11118.7 | 6665.9 | -12.9 | 6653.0 | | |
| | | 19-1008_11 | 0.62 | -8.00 | 868.1 | 130.9 | 999.1 | 599.0 | -196.8 | 402.1 |
| | | | | -8.50 | 865.5 | 197.6 | 1063.1 | 637.3 | -196.8 | 440.5 |
| -9.00 | 813.8 | | | 249.3 | 1063.1 | 637.3 | -196.8 | 440.5 | | |
| -9.50 | 848.0 | | | 298.5 | 1146.5 | 687.4 | -196.8 | 490.5 | | |
| -10.00 | 889.9 | | | 349.5 | 1239.4 | 743.0 | -196.8 | 546.2 | | |
| -10.50 | 889.5 | | | 410.8 | 1300.2 | 779.5 | -196.8 | 582.7 | | |
| -11.00 | 901.4 | | | 482.2 | 1383.6 | 829.5 | -196.8 | 632.7 | | |
| -11.50 | 837.2 | | | 568.1 | 1405.3 | 842.5 | -196.8 | 645.7 | | |
| -12.00 | 683.9 | | | 676.5 | 1360.4 | 815.6 | -196.8 | 618.8 | | |
| -12.50 | 2175.1 | | | 717.0 | 2892.1 | 1733.9 | -196.8 | 1537.0 | | |
| -13.00 | 2468.6 | | | 844.9 | 3313.5 | 1986.5 | -196.8 | 1789.7 | | |
| -13.50 | 2531.7 | | | 995.8 | 3527.4 | 2114.8 | -196.8 | 1917.9 | | |
| -14.00 | 2597.2 | | | 1149.5 | 3746.7 | 2246.2 | -196.8 | 2049.4 | | |
| -14.50 | 2619.3 | | | 1304.9 | 3924.2 | 2352.6 | -196.8 | 2155.8 | | |
| -15.00 | 2614.0 | | | 1460.3 | 4074.3 | 2442.6 | -196.8 | 2245.8 | | |
| -15.50 | 2692.5 | | | 1605.8 | 4298.3 | 2576.9 | -196.8 | 2380.1 | | |
| -16.00 | 3006.1 | | | 1728.5 | 4734.7 | 2838.5 | -196.8 | 2641.7 | | |
| -16.50 | 3040.3 | | | 1872.2 | 4912.6 | 2945.2 | -196.8 | 2748.3 | | |
| -17.00 | 3151.4 | | | 2010.3 | 5161.8 | 3094.6 | -196.8 | 2897.7 | | |
| -17.50 | 4282.9 | | | 2140.8 | 6423.7 | 3851.1 | -196.8 | 3654.3 | | |
| -18.00 | 5137.2 | | | 2305.2 | 7442.5 | 4461.9 | -196.8 | 4265.1 | | |
| -18.50 | 5192.2 | | | 2487.6 | 7679.8 | 4604.2 | -196.8 | 4407.4 | | |
| -19.00 | 5324.3 | | | 2670.0 | 7994.2 | 4792.7 | -196.8 | 4595.9 | | |
| -19.50 | 5329.3 | | | 2852.3 | 8181.6 | 4905.0 | -196.8 | 4708.2 | | |
| -20.00 | 4370.2 | | | 3034.7 | 7404.8 | 4439.4 | -196.8 | 4242.5 | | |
| -20.50 | 4081.6 | | | 3217.1 | 7298.7 | 4375.7 | -196.8 | 4178.9 | | |
| -21.00 | 3922.7 | | | 3399.4 | 7322.1 | 4389.7 | -196.8 | 4192.9 | | |
| -21.50 | 3879.4 | | | 3571.3 | 7450.7 | 4466.8 | -196.8 | 4270.0 | | |
| -22.00 | 3472.8 | | | 3753.7 | 7226.5 | 4332.4 | -196.8 | 4135.6 | | |
| -22.50 | 3248.4 | | | 3936.0 | 7184.4 | 4307.2 | -196.8 | 4110.4 | | |
| -23.00 | 3023.5 | 4101.3 | 7124.8 | 4271.5 | -196.8 | 4074.6 | | | | |
| -23.50 | 3483.0 | 4211.2 | 7694.2 | 4612.8 | -196.8 | 4416.0 | | | | |
| -24.00 | 3541.3 | 4352.8 | 7894.1 | 4732.7 | -196.8 | 4535.9 | | | | |
| -24.50 | 3455.1 | 4513.4 | 7968.5 | 4777.3 | -196.8 | 4580.4 | | | | |
| -25.00 | 3717.8 | 4666.1 | 8383.9 | 5026.3 | -196.8 | 4829.5 | | | | |
| -25.50 | 5061.6 | 4795.0 | 9856.6 | 5909.2 | -196.8 | 5712.4 | | | | |
| -26.00 | 5053.6 | 4977.4 | 10031.0 | 6013.8 | -196.8 | 5817.0 | | | | |
| -26.50 | 4998.0 | 5159.7 | 10157.7 | 6089.8 | -196.8 | 5892.9 | | | | |
| -27.00 | 5026.7 | 5342.1 | 10368.8 | 6216.3 | -196.8 | 6019.5 | | | | |
| -27.50 | 5143.5 | 5524.5 | 10668.0 | 6395.7 | -196.8 | 6198.8 | | | | |
| -28.00 | 5756.5 | 5706.8 | 11463.3 | 6872.5 | -196.8 | 6675.6 | | | | |
| -28.50 | 6016.0 | 5889.1 | 11905.1 | 7137.4 | -196.8 | 6940.5 | | | | |
| -29.00 | 6815.5 | 6071.5 | 12887.0 | 7726.0 | -196.8 | 7529.2 | | | | |
| -29.50 | 7914.3 | 6253.9 | 14168.2 | 8494.1 | -196.8 | 8297.3 | | | | |
| -30.00 | 7994.5 | 6436.2 | 14430.8 | 8651.5 | -196.8 | 8454.7 | | | | |
| 19-1008_12 | 3.57 | -8.00 | 457.8 | 2663.1 | 3120.9 | 1871.0 | 0.0 | 1871.0 | | |
| | | -8.50 | 404.3 | 2756.0 | 3160.4 | 1894.7 | 0.0 | 1894.7 | | |
| | | -9.00 | 418.8 | 2783.2 | 3202.0 | 1919.7 | 0.0 | 1919.7 | | |
| | | -9.50 | 406.0 | 2803.0 | 3209.1 | 1923.9 | 0.0 | 1923.9 | | |
| | | -10.00 | 403.9 | 2842.5 | 3246.4 | 1946.3 | 0.0 | 1946.3 | | |
| | | -10.50 | 382.7 | 2922.8 | 3305.5 | 1981.7 | 0.0 | 1981.7 | | |
| | | -11.00 | 323.6 | 2984.7 | 3308.3 | 1983.4 | 0.0 | 1983.4 | | |
| | | -11.50 | 385.4 | 2996.8 | 3382.3 | 2027.7 | 0.0 | 2027.7 | | |
| | | -12.00 | 344.9 | 3054.8 | 3399.7 | 2038.2 | 0.0 | 2038.2 | | |
| | | -12.50 | 344.0 | 3075.8 | 3419.8 | 2050.3 | 0.0 | 2050.3 | | |
| | | -13.00 | 448.8 | 3092.2 | 3540.9 | 2122.9 | 0.0 | 2122.9 | | |
| | | -13.50 | 572.5 | 3112.6 | 3685.1 | 2209.3 | 0.0 | 2209.3 | | |
| | | -14.00 | 592.3 | 3162.7 | 3755.0 | 2251.2 | 0.0 | 2251.2 | | |
| | | -14.50 | 583.6 | 3228.3 | 3811.9 | 2285.3 | 0.0 | 2285.3 | | |
| | | -15.00 | 596.8 | 3274.1 | 3870.9 | 2320.7 | 0.0 | 2320.7 | | |
| | | -15.50 | 753.8 | 3310.3 | 4064.2 | 2436.5 | 0.0 | 2436.5 | | |
| | | -16.00 | 803.0 | 3369.6 | 4172.6 | 2501.6 | 0.0 | 2501.6 | | |
| | | -16.50 | 822.2 | 3450.6 | 4272.7 | 2561.6 | 0.0 | 2561.6 | | |
| | | -17.00 | 879.3 | 3517.8 | 4397.2 | 2636.2 | 0.0 | 2636.2 | | |
| | | -17.50 | 1096.1 | 3618.2 | 4714.3 | 2826.3 | 0.0 | 2826.3 | | |
| | | -18.00 | 1470.9 | 3695.9 | 5166.8 | 3097.6 | 0.0 | 3097.6 | | |
| | | -18.50 | 1495.0 | 3875.4 | 5370.4 | 3219.7 | 0.0 | 3219.7 | | |
| | | -19.00 | 2162.0 | 4039.6 | 6201.6 | 3718.0 | 0.0 | 3718.0 | | |
| | | -19.50 | 2661.2 | 4189.8 | 6851.0 | 4107.3 | 0.0 | 4107.3 | | |
| | | -20.00 | 2973.1 | 4319.3 | 7292.4 | 4371.9 | 0.0 | 4371.9 | | |
| | | -20.50 | 2727.8 | 4465.2 | 7193.1 | 4312.4 | 0.0 | 4312.4 | | |
| | | -21.00 | 3505.5 | 4601.8 | 8107.3 | 4860.5 | 0.0 | 4860.5 | | |
| | | -21.50 | 3625.1 | 4767.4 | 8392.5 | 5031.5 | 0.0 | 5031.5 | | |
| | | -22.00 | 3757.3 | 4947.2 | 8704.5 | 5218.6 | 0.0 | 5218.6 | | |
| | | -22.50 | 3456.9 | 5126.8 | 8583.7 | 5146.1 | 0.0 | 5146.1 | | |
| -23.00 | 2836.4 | 5291.4 | 8127.8 | 4872.8 | 0.0 | 4872.8 | | | | |
| -23.50 | 2694.3 | 5449.8 | 8144.1 | 4882.6 | 0.0 | 4882.6 | | | | |
| -24.00 | 2542.0 | 5617.9 | 8159.9 | 4892.0 | 0.0 | 4892.0 | | | | |
| -24.50 | 2083.5 | 5800.3 | 7883.8 | 4726.5 | 0.0 | 4726.5 | | | | |
| -25.00 | 1953.1 | 5982.7 | 7935.7 | 4757.6 | 0.0 | 4757.6 | | | | |
| -25.50 | 1729.8 | 6223.4 | 7953.2 | 4768.1 | 0.0 | 4768.1 | | | | |
| -26.00 | 1626.2 | 6465.4 | 8091.5 | 4851.0 | 0.0 | 4851.0 | | | | |
| -26.50 | 1631.5 | 6604.8 | 8236.4 | 4937.9 | 0.0 | 4937.9 | | | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziwkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|----------------------------|--------------------------------|
| | | | R _{z,real} [kN] | R _{z,real} [kN] | R _{z,real} [kN] | R _{z,d} [kN] | F _{hkk;d} [kN] | R _{z,netto;d} [kN] |
| 19-1008_12 | 3.57 | -27.00 | 1621.7 | 6735.1 | 8356.8 | 5010.1 | 0.0 | 5010.1 |
| | | -27.50 | 1575.1 | 6884.5 | 8459.6 | 5071.7 | 0.0 | 5071.7 |
| | | -28.00 | 3106.4 | 6992.4 | 10098.9 | 6054.5 | 0.0 | 6054.5 |
| 19-1008_17 | 0.20 | -8.00 | 409.4 | 0.0 | 409.4 | 245.5 | -274.9 | -29.4 |
| | | -8.50 | 452.5 | 0.0 | 452.5 | 271.3 | -274.9 | -3.6 |
| | | -9.00 | 568.5 | 0.0 | 568.5 | 340.8 | -274.9 | 65.9 |
| | | -9.50 | 1415.9 | 0.0 | 1415.9 | 848.8 | -274.9 | 574.0 |
| | | -10.00 | 1044.0 | 0.0 | 1044.0 | 625.9 | -274.9 | 351.0 |
| | | -10.50 | 2367.5 | 28.0 | 2395.5 | 1436.2 | -274.9 | 1161.3 |
| | | -11.00 | 3827.7 | 142.3 | 3970.0 | 2380.1 | -274.9 | 2105.2 |
| | | -11.50 | 3447.0 | 324.7 | 3771.7 | 2261.2 | -274.9 | 1986.3 |
| | | -12.00 | 3603.8 | 507.1 | 4110.8 | 2464.5 | -274.9 | 2189.7 |
| | | -12.50 | 3690.8 | 689.4 | 4380.2 | 2626.0 | -274.9 | 2351.2 |
| | | -13.00 | 3583.4 | 871.8 | 4455.2 | 2671.0 | -274.9 | 2396.1 |
| | | -13.50 | 3538.8 | 1054.2 | 4593.0 | 2753.6 | -274.9 | 2478.7 |
| | | -14.00 | 3524.2 | 1236.5 | 4760.8 | 2854.2 | -274.9 | 2579.3 |
| | | -14.50 | 4044.0 | 1418.8 | 5462.8 | 3275.1 | -274.9 | 3000.2 |
| | | -15.00 | 2596.0 | 1587.3 | 4183.3 | 2508.0 | -274.9 | 2233.1 |
| | | -15.50 | 2558.0 | 1769.7 | 4327.7 | 2594.5 | -274.9 | 2319.7 |
| | | -16.00 | 2546.2 | 1952.1 | 4498.3 | 2696.8 | -274.9 | 2421.9 |
| | | -16.50 | 2521.3 | 2134.4 | 4655.8 | 2791.2 | -274.9 | 2516.3 |
| | | -17.00 | 2592.5 | 2309.3 | 4901.8 | 2938.7 | -274.9 | 2663.9 |
| | | -17.50 | 2234.8 | 2498.1 | 4732.9 | 2837.5 | -274.9 | 2562.6 |
| | | -18.00 | 1879.8 | 2717.1 | 4596.9 | 2755.9 | -274.9 | 2481.1 |
| | | -18.50 | 2576.5 | 2863.7 | 5440.2 | 3261.5 | -274.9 | 2986.6 |
| | | -19.00 | 2683.6 | 2990.0 | 5673.6 | 3401.4 | -274.9 | 3126.5 |
| | | -19.50 | 2749.2 | 3135.9 | 5885.1 | 3528.2 | -274.9 | 3253.4 |
| | | -20.00 | 2850.4 | 3283.1 | 6133.4 | 3677.1 | -274.9 | 3402.2 |
| | | -20.50 | 3077.5 | 3439.2 | 6516.7 | 3906.9 | -274.9 | 3632.0 |
| | | -21.00 | 2687.2 | 3600.5 | 6287.7 | 3769.6 | -274.9 | 3494.7 |
| | | -21.50 | 3162.9 | 3781.0 | 6944.0 | 4163.1 | -274.9 | 3888.2 |
| | | -22.00 | 3120.4 | 3936.6 | 7057.0 | 4230.8 | -274.9 | 3956.0 |
| | | -22.50 | 3064.6 | 4119.0 | 7183.6 | 4306.7 | -274.9 | 4031.8 |
| -23.00 | 2870.4 | 4301.3 | 7171.8 | 4299.6 | -274.9 | 4024.8 | | |
| -23.50 | 2787.2 | 4483.7 | 7270.9 | 4359.0 | -274.9 | 4084.2 | | |
| -24.00 | 2765.0 | 4651.8 | 7416.8 | 4446.5 | -274.9 | 4171.7 | | |
| -24.50 | 2720.8 | 4797.4 | 7518.2 | 4507.3 | -274.9 | 4232.4 | | |
| -25.00 | 2764.6 | 4910.9 | 7675.4 | 4601.6 | -274.9 | 4326.7 | | |
| -25.50 | 2807.2 | 5020.9 | 7828.1 | 4693.1 | -274.9 | 4418.3 | | |
| -26.00 | 1280.3 | 5128.4 | 6408.7 | 3842.1 | -274.9 | 3567.3 | | |
| -26.50 | 1225.0 | 5235.5 | 6460.5 | 3873.2 | -274.9 | 3598.3 | | |
| -27.00 | 1216.6 | 5362.7 | 6579.3 | 3944.4 | -274.9 | 3669.5 | | |
| -27.50 | 1189.0 | 5499.0 | 6688.0 | 4009.6 | -274.9 | 3734.7 | | |
| -28.00 | 1128.3 | 5637.9 | 6766.2 | 4056.4 | -274.9 | 3781.6 | | |
| -28.50 | 928.1 | 5783.7 | 6711.8 | 4023.8 | -274.9 | 3749.0 | | |
| -29.00 | 526.8 | 5936.7 | 6463.4 | 3875.0 | -274.9 | 3600.1 | | |
| -29.50 | 2260.5 | 5979.8 | 8240.3 | 4940.3 | -274.9 | 4665.4 | | |
| -30.00 | 2886.1 | 6095.9 | 8982.0 | 5384.9 | -274.9 | 5110.0 | | |
| 19-1008_20 | -0.03 | -8.00 | 852.3 | 528.1 | 1380.3 | 827.5 | -51.8 | 775.7 |
| | | -8.50 | 865.2 | 601.6 | 1466.8 | 879.4 | -51.8 | 827.6 |
| | | -9.00 | 807.1 | 703.6 | 1510.8 | 905.7 | -51.8 | 853.9 |
| | | -9.50 | 746.7 | 786.2 | 1532.9 | 919.0 | -51.8 | 867.2 |
| | | -10.00 | 574.9 | 881.6 | 1456.5 | 873.2 | -51.8 | 821.4 |
| | | -10.50 | 859.5 | 904.4 | 1763.9 | 1057.5 | -51.8 | 1005.7 |
| | | -11.00 | 776.6 | 1028.2 | 1804.8 | 1082.0 | -51.8 | 1030.2 |
| | | -11.50 | 550.8 | 1161.9 | 1712.7 | 1026.8 | -51.8 | 975.0 |
| | | -12.00 | 627.1 | 1187.9 | 1815.0 | 1088.1 | -51.8 | 1036.3 |
| | | -12.50 | 659.5 | 1217.8 | 1877.2 | 1125.4 | -51.8 | 1073.6 |
| | | -13.00 | 620.5 | 1275.3 | 1895.8 | 1136.6 | -51.8 | 1084.8 |
| | | -13.50 | 767.2 | 1301.2 | 2068.4 | 1240.1 | -51.8 | 1188.3 |
| | | -14.00 | 762.6 | 1352.0 | 2114.6 | 1267.8 | -51.8 | 1216.0 |
| | | -14.50 | 741.7 | 1446.1 | 2187.8 | 1311.6 | -51.8 | 1259.8 |
| | | -15.00 | 703.4 | 1553.7 | 2257.1 | 1353.2 | -51.8 | 1301.4 |
| | | -15.50 | 698.2 | 1614.1 | 2312.3 | 1386.3 | -51.8 | 1334.5 |
| | | -16.00 | 720.8 | 1659.4 | 2380.2 | 1427.0 | -51.8 | 1375.2 |
| | | -16.50 | 704.2 | 1723.7 | 2427.9 | 1455.6 | -51.8 | 1403.8 |
| | | -17.00 | 826.7 | 1765.3 | 2592.0 | 1553.9 | -51.8 | 1502.1 |
| | | -17.50 | 1104.4 | 1816.3 | 2920.7 | 1751.0 | -51.8 | 1699.2 |
| | | -18.00 | 1135.2 | 1911.8 | 3047.0 | 1826.8 | -51.8 | 1775.0 |
| | | -18.50 | 1203.8 | 2023.8 | 3227.5 | 1935.0 | -51.8 | 1883.2 |
| | | -19.00 | 1242.8 | 2107.5 | 3350.3 | 2008.6 | -51.8 | 1956.8 |
| | | -19.50 | 1219.7 | 2220.2 | 3440.0 | 2062.3 | -51.8 | 2010.5 |
| | | -20.00 | 1200.5 | 2336.5 | 3537.0 | 2120.5 | -51.8 | 2068.7 |
| | | -20.50 | 1009.4 | 2486.3 | 3495.7 | 2095.8 | -51.8 | 2044.0 |
| | | -21.00 | 801.8 | 2686.9 | 3488.7 | 2091.6 | -51.8 | 2039.8 |
| | | -21.50 | 772.5 | 2771.9 | 3544.4 | 2125.0 | -51.8 | 2073.2 |
| | | -22.00 | 779.2 | 2827.9 | 3607.2 | 2162.6 | -51.8 | 2110.8 |
| | | -22.50 | 921.9 | 2889.2 | 3811.1 | 2284.8 | -51.8 | 2233.0 |
| -23.00 | 1650.8 | 2938.5 | 4589.3 | 2751.4 | -51.8 | 2699.6 | | |
| -23.50 | 1863.4 | 3034.5 | 4897.9 | 2936.4 | -51.8 | 2884.6 | | |
| -24.00 | 2148.1 | 3142.1 | 5290.2 | 3171.6 | -51.8 | 3119.8 | | |
| -24.50 | 2233.5 | 3254.9 | 5488.4 | 3290.4 | -51.8 | 3238.6 | | |
| -25.00 | 2289.4 | 3393.5 | 5682.9 | 3407.0 | -51.8 | 3355.2 | | |
| -25.50 | 2348.6 | 3519.6 | 5868.2 | 3518.1 | -51.8 | 3466.3 | | |
| -26.00 | 2076.3 | 3643.0 | 5719.3 | 3428.8 | -51.8 | 3377.0 | | |
| -26.50 | 2142.7 | 3754.4 | 5897.0 | 3535.4 | -51.8 | 3483.6 | | |
| -27.00 | 2062.8 | 3890.3 | 5953.1 | 3569.0 | -51.8 | 3517.2 | | |
| -27.50 | 2100.5 | 4009.7 | 6110.2 | 3663.2 | -51.8 | 3611.4 | | |
| -28.00 | 2152.6 | 4117.7 | 6270.3 | 3759.2 | -51.8 | 3707.4 | | |
| -28.50 | 2180.9 | 4244.2 | 6425.2 | 3852.0 | -51.8 | 3800.2 | | |
| -29.00 | 2202.9 | 4361.5 | 6564.4 | 3935.5 | -51.8 | 3883.7 | | |
| -29.50 | 1947.1 | 4455.9 | 6403.0 | 3838.7 | -51.8 | 3786.9 | | |
| -30.00 | 1978.7 | 4575.0 | 6553.6 | 3929.0 | -51.8 | 3877.2 | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezijsdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
| | | | $R_{b,real}$ [kN] | $R_{s,real}$ [kN] | $R_{c,real}$ [kN] | $R_{s,d}$ [kN] | $F_{pk,d}$ [kN] | $R_{c,netto,d}$ [kN] |
| 19-1008_21 | 1.78 | -8.00 | 1491.2 | 908.0 | 2399.1 | 1438.3 | -161.7 | 1276.7 |
| | | -8.50 | 1304.1 | 1043.1 | 2347.3 | 1407.2 | -161.7 | 1245.6 |
| | | -9.00 | 1352.6 | 1113.1 | 2465.7 | 1478.2 | -161.7 | 1316.5 |
| | | -9.50 | 1619.8 | 1165.7 | 2785.6 | 1670.0 | -161.7 | 1508.3 |
| | | -10.00 | 1682.5 | 1245.9 | 2928.3 | 1755.6 | -161.7 | 1593.9 |
| | | -10.50 | 1778.2 | 1316.3 | 3094.5 | 1855.2 | -161.7 | 1693.6 |
| | | -11.00 | 1803.4 | 1397.0 | 3200.4 | 1918.7 | -161.7 | 1757.1 |
| | | -11.50 | 1795.9 | 1498.9 | 3294.8 | 1975.3 | -161.7 | 1813.6 |
| | | -12.00 | 1591.3 | 1613.3 | 3204.6 | 1921.2 | -161.7 | 1759.5 |
| | | -12.50 | 1650.3 | 1701.2 | 3351.5 | 2009.3 | -161.7 | 1847.6 |
| | | -13.00 | 1733.7 | 1802.7 | 3536.4 | 2120.2 | -161.7 | 1958.5 |
| | | -13.50 | 1431.6 | 1915.1 | 3346.7 | 2006.4 | -161.7 | 1844.8 |
| | | -14.00 | 1257.5 | 2082.3 | 3339.8 | 2002.3 | -161.7 | 1840.6 |
| | | -14.50 | 1317.0 | 2249.9 | 3566.9 | 2138.4 | -161.7 | 1976.7 |
| | | -15.00 | 1088.1 | 2372.5 | 3460.6 | 2074.7 | -161.7 | 1913.0 |
| | | -15.50 | 1104.0 | 2461.9 | 3565.9 | 2137.8 | -161.7 | 1976.1 |
| | | -16.00 | 921.4 | 2634.7 | 3556.2 | 2132.0 | -161.7 | 1970.3 |
| | | -16.50 | 596.5 | 2807.3 | 3403.8 | 2040.7 | -161.7 | 1879.0 |
| | | -17.00 | 684.9 | 2836.6 | 3521.5 | 2111.2 | -161.7 | 1949.5 |
| | | -17.50 | 844.2 | 2870.8 | 3715.1 | 2227.3 | -161.7 | 2065.6 |
| | | -18.00 | 835.6 | 2936.2 | 3771.8 | 2261.3 | -161.7 | 2099.6 |
| | | -18.50 | 714.2 | 3125.5 | 3839.7 | 2302.0 | -161.7 | 2140.3 |
| | | -19.00 | 645.5 | 3257.5 | 3903.0 | 2339.9 | -161.7 | 2178.2 |
| | | -19.50 | 644.7 | 3291.1 | 3935.8 | 2359.6 | -161.7 | 2197.9 |
| | | -20.00 | 648.7 | 3317.8 | 3966.5 | 2378.0 | -161.7 | 2216.3 |
| | | -20.50 | 662.8 | 3344.3 | 4007.1 | 2402.3 | -161.7 | 2240.7 |
| | | -21.00 | 702.3 | 3370.9 | 4073.3 | 2442.0 | -161.7 | 2280.3 |
| | | -21.50 | 731.0 | 3403.2 | 4134.2 | 2478.5 | -161.7 | 2316.8 |
| | | -22.00 | 756.3 | 3440.4 | 4196.7 | 2516.0 | -161.7 | 2354.3 |
| | | -22.50 | 765.7 | 3486.0 | 4251.7 | 2549.0 | -161.7 | 2387.3 |
| -23.00 | 779.0 | 3531.2 | 4310.3 | 2584.1 | -161.7 | 2422.4 | | |
| -23.50 | 821.4 | 3574.7 | 4396.1 | 2635.5 | -161.7 | 2473.9 | | |
| -24.00 | 834.0 | 3626.2 | 4460.2 | 2674.0 | -161.7 | 2512.3 | | |
| -24.50 | 836.1 | 3679.2 | 4515.3 | 2707.0 | -161.7 | 2545.4 | | |
| -25.00 | 841.4 | 3735.0 | 4576.4 | 2743.6 | -161.7 | 2582.0 | | |
| -25.50 | 843.1 | 3793.6 | 4636.7 | 2779.8 | -161.7 | 2618.1 | | |
| -26.00 | 845.1 | 3849.7 | 4694.8 | 2814.6 | -161.7 | 2653.0 | | |
| -26.50 | 853.2 | 3900.4 | 4753.7 | 2849.9 | -161.7 | 2688.2 | | |
| -27.00 | 857.3 | 3952.5 | 4809.7 | 2883.5 | -161.7 | 2721.9 | | |
| -27.50 | 909.1 | 4003.6 | 4912.7 | 2945.3 | -161.7 | 2783.6 | | |
| -28.00 | 923.2 | 4058.7 | 4981.9 | 2986.7 | -161.7 | 2825.1 | | |
| -28.50 | 927.5 | 4115.7 | 5043.2 | 3023.5 | -161.7 | 2861.8 | | |
| -29.00 | 961.0 | 4170.9 | 5131.9 | 3076.7 | -161.7 | 2915.0 | | |
| -29.50 | 979.5 | 4228.9 | 5208.4 | 3122.6 | -161.7 | 2960.9 | | |
| 251.S01 | -1.05 | -8.00 | 397.9 | 1150.0 | 1547.9 | 928.0 | -17.8 | 910.3 |
| | | -8.50 | 385.3 | 1237.3 | 1622.6 | 972.8 | -17.8 | 955.0 |
| | | -9.00 | 1307.1 | 1250.4 | 2557.5 | 1533.3 | -17.8 | 1515.5 |
| | | -9.50 | 1388.7 | 1331.0 | 2719.7 | 1630.5 | -17.8 | 1612.8 |
| | | -10.00 | 1415.6 | 1453.2 | 2868.8 | 1719.9 | -17.8 | 1702.2 |
| | | -10.50 | 1356.4 | 1596.9 | 2953.4 | 1770.6 | -17.8 | 1752.8 |
| | | -11.00 | 1288.3 | 1706.1 | 2994.4 | 1795.2 | -17.8 | 1777.5 |
| | | -11.50 | 1386.5 | 1772.4 | 3158.9 | 1893.8 | -17.8 | 1876.1 |
| | | -12.00 | 1456.4 | 1838.2 | 3294.6 | 1975.2 | -17.8 | 1957.4 |
| | | -12.50 | 1515.7 | 1950.2 | 3465.9 | 2077.9 | -17.8 | 2060.1 |
| | | -13.00 | 1557.0 | 2082.7 | 3639.6 | 2182.0 | -17.8 | 2164.3 |
| | | -13.50 | 1594.4 | 2207.4 | 3801.9 | 2279.3 | -17.8 | 2261.5 |
| | | -14.00 | 1501.5 | 2380.9 | 3882.5 | 2327.6 | -17.8 | 2309.9 |
| | | -14.50 | 1286.3 | 2553.3 | 3839.6 | 2301.9 | -17.8 | 2284.2 |
| | | -15.00 | 1191.7 | 2739.9 | 3931.6 | 2357.1 | -17.8 | 2339.3 |
| | | -15.50 | 2313.0 | 2823.4 | 5136.4 | 3079.4 | -17.8 | 3061.6 |
| | | -16.00 | 2285.3 | 2991.8 | 5277.1 | 3163.7 | -17.8 | 3146.0 |
| | | -16.50 | 2314.4 | 3174.1 | 5488.5 | 3290.5 | -17.8 | 3272.7 |
| | | -17.00 | 2330.9 | 3354.5 | 5685.4 | 3408.5 | -17.8 | 3390.7 |
| | | -17.50 | 2278.3 | 3526.6 | 5804.9 | 3480.1 | -17.8 | 3462.4 |
| | | -18.00 | 1271.1 | 3689.2 | 4960.3 | 2973.8 | -17.8 | 2956.1 |
| | | -18.50 | 1145.8 | 3871.3 | 5017.1 | 3007.9 | -17.8 | 2990.1 |
| | | -19.00 | 1013.8 | 3980.8 | 4994.6 | 2994.4 | -17.8 | 2976.6 |
| | | -19.50 | 930.4 | 4097.7 | 5028.2 | 3014.5 | -17.8 | 2996.7 |
| | | -20.00 | 809.4 | 4239.5 | 5048.9 | 3026.9 | -17.8 | 3009.2 |
| | | -20.50 | 659.5 | 4437.9 | 5097.4 | 3056.0 | -17.8 | 3038.2 |
| | | -21.00 | 516.9 | 4646.8 | 5163.7 | 3095.7 | -17.8 | 3078.0 |
| | | -21.50 | 468.6 | 4733.4 | 5202.1 | 3118.7 | -17.8 | 3101.0 |
| | | -22.00 | 472.6 | 4760.6 | 5233.2 | 3137.4 | -17.8 | 3119.6 |
| | | -22.50 | 629.6 | 4796.4 | 5426.0 | 3253.0 | -17.8 | 3235.2 |
| -23.00 | 708.0 | 4853.9 | 5561.9 | 3334.5 | -17.8 | 3316.7 | | |
| -23.50 | 907.3 | 4929.1 | 5836.4 | 3499.1 | -17.8 | 3481.3 | | |
| -24.00 | 919.5 | 5030.9 | 5950.4 | 3567.4 | -17.8 | 3549.6 | | |
| -24.50 | 1104.5 | 5123.6 | 6228.1 | 3733.9 | -17.8 | 3716.1 | | |
| -25.00 | 1486.9 | 5207.7 | 6694.7 | 4013.6 | -17.8 | 3995.8 | | |
| -25.50 | 2284.5 | 5358.6 | 7643.2 | 4582.2 | -17.8 | 4564.5 | | |
| -26.00 | 3403.7 | 5579.9 | 8983.6 | 5385.8 | -17.8 | 5368.1 | | |
| -26.50 | 3588.9 | 5793.1 | 9382.0 | 5624.7 | -17.8 | 5607.0 | | |
| -27.00 | 3168.6 | 5975.5 | 9144.0 | 5482.0 | -17.8 | 5464.3 | | |
| -27.50 | 2457.4 | 6157.8 | 8615.3 | 5165.0 | -17.8 | 5147.3 | | |
| -28.00 | 2094.1 | 6340.2 | 8434.4 | 5056.6 | -17.8 | 5038.8 | | |
| -28.50 | 1796.6 | 6522.6 | 8319.2 | 4987.5 | -17.8 | 4969.8 | | |
| -29.00 | 1429.6 | 6704.7 | 8134.4 | 4876.7 | -17.8 | 4859.0 | | |
| -29.50 | 1383.3 | 6827.1 | 8210.4 | 4922.3 | -17.8 | 4904.5 | | |
| -30.00 | 1139.3 | 6973.0 | 8112.3 | 4863.5 | -17.8 | 4845.8 | | |
| 19-1008_29 | 0.79 | -8.00 | 2518.7 | 1704.2 | 4222.9 | 2531.7 | -8.6 | 2523.1 |
| | | -8.50 | 1184.7 | 1869.7 | 3054.4 | 1831.2 | -8.6 | 1822.6 |
| | | -9.00 | 1172.0 | 2013.7 | 3185.7 | 1909.9 | -8.6 | 1901.3 |
| | | -9.50 | 1164.8 | 2148.1 | 3313.0 | 1986.2 | -8.6 | 1977.6 |
| | | -10.00 | 1172.1 | 2273.8 | 3445.9 | 2065.9 | -8.6 | 2057.3 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziwkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|---------------------------|--------------------------------|
| | | | R _{b,real} [kN] | R _{r,real} [kN] | R _{c,real} [kN] | R _d [kN] | F _{nk;d} [kN] | R _{c,netto;d} [kN] |
| 19-1008_29 | 0.79 | -10.50 | 1101.1 | 2419.7 | 3520.8 | 2110.8 | -8.6 | 2102.2 |
| | | -11.00 | 917.5 | 2564.4 | 3481.9 | 2087.5 | -8.6 | 2078.9 |
| | | -11.50 | 941.3 | 2726.1 | 3667.4 | 2198.7 | -8.6 | 2190.1 |
| | | -12.00 | 865.6 | 2802.1 | 3667.7 | 2198.9 | -8.6 | 2190.3 |
| | | -12.50 | 754.4 | 2967.1 | 3721.5 | 2231.1 | -8.6 | 2222.5 |
| | | -13.00 | 577.0 | 3094.3 | 3671.3 | 2201.0 | -8.6 | 2192.4 |
| | | -13.50 | 592.7 | 3147.5 | 3740.2 | 2242.3 | -8.6 | 2233.8 |
| | | -14.00 | 592.9 | 3210.3 | 3803.2 | 2280.1 | -8.6 | 2271.5 |
| | | -14.50 | 606.3 | 3253.8 | 3860.1 | 2314.2 | -8.6 | 2305.6 |
| | | -15.00 | 754.1 | 3291.1 | 4045.2 | 2425.2 | -8.6 | 2416.6 |
| | | -15.50 | 800.9 | 3335.9 | 4136.8 | 2480.1 | -8.6 | 2471.5 |
| | | -16.00 | 677.9 | 3450.1 | 4128.1 | 2474.9 | -8.6 | 2466.3 |
| | | -16.50 | 702.2 | 3492.4 | 4194.6 | 2514.8 | -8.6 | 2506.2 |
| | | -17.00 | 1024.8 | 3535.1 | 4559.9 | 2733.7 | -8.6 | 2725.1 |
| | | -17.50 | 2579.3 | 3596.6 | 6176.0 | 3702.6 | -8.6 | 3694.0 |
| | | -18.00 | 2980.8 | 3747.2 | 6728.0 | 4033.6 | -8.6 | 4025.0 |
| | | -18.50 | 2797.5 | 3929.6 | 6727.1 | 4033.0 | -8.6 | 4024.5 |
| | | -19.00 | 2631.6 | 4106.2 | 6737.8 | 4039.5 | -8.6 | 4030.9 |
| | | -19.50 | 3429.5 | 4242.5 | 7672.0 | 4599.5 | -8.6 | 4590.9 |
| | | -20.00 | 2986.5 | 4424.9 | 7411.3 | 4443.2 | -8.6 | 4434.6 |
| | | -20.50 | 2697.4 | 4607.2 | 7304.7 | 4379.3 | -8.6 | 4370.7 |
| | | -21.00 | 2439.2 | 4789.6 | 7228.8 | 4333.8 | -8.6 | 4325.2 |
| | | -21.50 | 2112.4 | 4972.0 | 7084.4 | 4247.2 | -8.6 | 4238.6 |
| | | -22.00 | 1712.4 | 5154.3 | 6866.7 | 4116.7 | -8.6 | 4108.1 |
| | | -22.50 | 1404.5 | 5365.9 | 6770.3 | 4059.0 | -8.6 | 4050.4 |
| | | -23.00 | 1312.4 | 5522.2 | 6834.7 | 4097.5 | -8.6 | 4088.9 |
| | | -23.50 | 1411.5 | 5630.4 | 7041.9 | 4221.8 | -8.6 | 4213.2 |
| | | -24.00 | 1392.2 | 5757.7 | 7149.9 | 4286.5 | -8.6 | 4277.9 |
| | | -24.50 | 1294.2 | 5887.2 | 7181.4 | 4305.4 | -8.6 | 4296.8 |
| | | -25.00 | 1233.2 | 6024.8 | 7258.0 | 4351.3 | -8.6 | 4342.7 |
| | | -25.50 | 1277.7 | 6110.2 | 7387.9 | 4429.2 | -8.6 | 4420.6 |
| -26.00 | 1257.7 | 6208.5 | 7466.2 | 4476.1 | -8.6 | 4467.5 | | |
| -26.50 | 1259.0 | 6300.0 | 7559.1 | 4531.8 | -8.6 | 4523.2 | | |
| -27.00 | 1219.0 | 6415.1 | 7634.1 | 4576.8 | -8.6 | 4568.2 | | |
| -27.50 | 1232.3 | 6502.0 | 7734.2 | 4636.8 | -8.6 | 4628.2 | | |
| -28.00 | 1231.1 | 6586.7 | 7817.7 | 4686.9 | -8.6 | 4678.3 | | |
| -28.50 | 1303.8 | 6670.8 | 7974.6 | 4780.9 | -8.6 | 4772.3 | | |
| -29.00 | 1863.1 | 6763.5 | 8626.6 | 5171.8 | -8.6 | 5163.2 | | |
| -29.50 | 1769.5 | 6910.0 | 8679.4 | 5203.5 | -8.6 | 5194.9 | | |
| -30.00 | 1540.6 | 7034.0 | 8574.6 | 5140.6 | -8.6 | 5132.0 | | |
| 283.S02 | 0.17 | -8.00 | 2500.0 | 1257.4 | 3757.4 | 2252.6 | -17.3 | 2235.3 |
| | | -8.50 | 1995.9 | 1377.2 | 3373.0 | 2022.2 | -17.3 | 2004.9 |
| | | -9.00 | 1999.4 | 1487.4 | 3486.8 | 2090.4 | -17.3 | 2073.1 |
| | | -9.50 | 1999.2 | 1581.0 | 3580.2 | 2146.4 | -17.3 | 2129.1 |
| | | -10.00 | 1986.3 | 1686.1 | 3672.5 | 2201.7 | -17.3 | 2184.4 |
| | | -10.50 | 1956.9 | 1787.6 | 3744.5 | 2244.9 | -17.3 | 2227.6 |
| | | -11.00 | 1931.0 | 1886.8 | 3817.8 | 2288.8 | -17.3 | 2271.5 |
| | | -11.50 | 1886.2 | 1993.3 | 3879.4 | 2325.8 | -17.3 | 2308.5 |
| | | -12.00 | 2613.4 | 2061.5 | 4674.9 | 2802.7 | -17.3 | 2785.3 |
| | | -12.50 | 2924.0 | 2179.9 | 5103.9 | 3059.9 | -17.3 | 3042.5 |
| | | -13.00 | 3239.9 | 2311.5 | 5551.4 | 3328.2 | -17.3 | 3310.8 |
| | | -13.50 | 3344.1 | 2458.1 | 5802.2 | 3478.5 | -17.3 | 3461.2 |
| | | -14.00 | 3421.5 | 2632.1 | 6053.6 | 3629.3 | -17.3 | 3611.9 |
| | | -14.50 | 3334.9 | 2806.2 | 6141.1 | 3681.7 | -17.3 | 3664.4 |
| | | -15.00 | 3381.9 | 2961.6 | 6343.5 | 3803.1 | -17.3 | 3785.7 |
| | | -15.50 | 3648.3 | 3094.6 | 6742.9 | 4042.5 | -17.3 | 4025.2 |
| | | -16.00 | 4028.2 | 3240.4 | 7268.5 | 4357.6 | -17.3 | 4340.3 |
| | | -16.50 | 4443.0 | 3402.7 | 7845.7 | 4703.7 | -17.3 | 4686.3 |
| | | -17.00 | 4670.5 | 3576.6 | 8247.1 | 4944.3 | -17.3 | 4927.0 |
| | | -17.50 | 4779.4 | 3759.0 | 8538.3 | 5118.9 | -17.3 | 5101.6 |
| | | -18.00 | 4903.6 | 3941.3 | 8844.9 | 5302.7 | -17.3 | 5285.4 |
| | | -18.50 | 5043.6 | 4123.7 | 9167.3 | 5496.0 | -17.3 | 5478.6 |
| | | -19.00 | 5169.2 | 4306.1 | 9475.3 | 5680.6 | -17.3 | 5663.3 |
| | | -19.50 | 5184.6 | 4488.4 | 9673.0 | 5799.2 | -17.3 | 5781.8 |
| | | -20.00 | 5009.4 | 4670.8 | 9680.3 | 5803.5 | -17.3 | 5786.2 |
| | | -20.50 | 5799.2 | 4845.0 | 10644.2 | 6381.4 | -17.3 | 6364.1 |
| | | -21.00 | 5964.6 | 5027.4 | 10992.0 | 6589.9 | -17.3 | 6572.6 |
| | | -21.50 | 6056.4 | 5209.8 | 11266.2 | 6754.3 | -17.3 | 6737.0 |
| | | -22.00 | 6079.0 | 5392.1 | 11471.1 | 6877.2 | -17.3 | 6859.8 |
| -22.50 | 6095.5 | 5574.5 | 11670.0 | 6996.4 | -17.3 | 6979.1 | | |
| -23.00 | 4109.8 | 5756.9 | 9866.7 | 5915.3 | -17.3 | 5898.0 | | |
| -23.50 | 2766.9 | 5939.2 | 8706.1 | 5219.5 | -17.3 | 5202.2 | | |
| -24.00 | 2367.6 | 6121.6 | 8489.2 | 5089.5 | -17.3 | 5072.1 | | |
| -24.50 | 2055.8 | 6304.0 | 8359.8 | 5011.8 | -17.3 | 4994.5 | | |
| -25.00 | 1820.6 | 6486.4 | 8306.9 | 4980.2 | -17.3 | 4962.8 | | |
| -25.50 | 1433.1 | 6668.7 | 8101.8 | 4857.2 | -17.3 | 4839.9 | | |
| -26.00 | 1201.2 | 6851.1 | 8052.3 | 4827.5 | -17.3 | 4810.2 | | |
| -26.50 | 938.2 | 7043.1 | 7981.3 | 4785.0 | -17.3 | 4767.6 | | |
| -27.00 | 858.5 | 7109.7 | 7968.2 | 4777.1 | -17.3 | 4759.8 | | |
| -27.50 | 863.5 | 7172.9 | 8036.4 | 4818.0 | -17.3 | 4800.6 | | |
| -28.00 | 855.7 | 7252.3 | 8108.0 | 4860.9 | -17.3 | 4843.6 | | |
| -28.50 | 818.6 | 7353.0 | 8171.6 | 4899.1 | -17.3 | 4881.7 | | |
| 19-1008_35 | 0.92 | -8.00 | 2023.3 | 1267.1 | 3290.3 | 1972.6 | -10.6 | 1962.0 |
| | | -8.50 | 1967.2 | 1359.1 | 3326.3 | 1994.2 | -10.6 | 1983.6 |
| | | -9.00 | 2047.7 | 1429.4 | 3477.1 | 2084.6 | -10.6 | 2073.9 |
| | | -9.50 | 2093.4 | 1500.2 | 3593.6 | 2154.4 | -10.6 | 2143.8 |
| | | -10.00 | 2236.6 | 1585.8 | 3822.4 | 2291.6 | -10.6 | 2281.0 |
| | | -10.50 | 2244.6 | 1666.0 | 3910.5 | 2344.5 | -10.6 | 2333.8 |
| | | -11.00 | 2161.4 | 1803.9 | 3965.3 | 2377.3 | -10.6 | 2366.6 |
| | | -11.50 | 2071.0 | 1921.4 | 3992.3 | 2393.5 | -10.6 | 2382.8 |
| | | -12.00 | 2043.4 | 2002.6 | 4046.0 | 2425.7 | -10.6 | 2415.0 |
| | | -12.50 | 2451.7 | 2072.8 | 4524.5 | 2712.5 | -10.6 | 2701.9 |
| | | -13.00 | 2646.9 | 2166.4 | 4813.3 | 2885.7 | -10.6 | 2875.0 |
| | | -13.50 | 2832.3 | 2276.9 | 5109.1 | 3063.0 | -10.6 | 3052.4 |

Project : ZWO380 Funderingen
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Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Beziijkdraagvermogen | | | Rekenwaarden | | |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|---------------------------|--------------------------------|
| | | | R _{b,real} [kN] | R _{s,real} [kN] | R _{c,real} [kN] | R _{s,d} [kN] | F _{nk;d} [kN] | R _{c,netto;d} [kN] |
| 19-1008_35 | 0.92 | -14.00 | 3041.8 | 2392.2 | 5434.1 | 3257.9 | -10.6 | 3247.2 |
| | | -14.50 | 3068.2 | 2533.8 | 5602.0 | 3358.5 | -10.6 | 3347.9 |
| | | -15.00 | 3103.3 | 2675.4 | 5778.7 | 3464.4 | -10.6 | 3453.8 |
| | | -15.50 | 3131.0 | 2818.8 | 5949.8 | 3567.1 | -10.6 | 3556.4 |
| | | -16.00 | 3103.8 | 2965.9 | 6069.7 | 3638.9 | -10.6 | 3628.2 |
| | | -16.50 | 2932.0 | 3113.6 | 6045.6 | 3624.4 | -10.6 | 3613.8 |
| | | -17.00 | 2988.6 | 3240.5 | 6229.1 | 3734.5 | -10.6 | 3723.8 |
| | | -17.50 | 3303.5 | 3348.1 | 6651.6 | 3987.8 | -10.6 | 3977.2 |
| | | -18.00 | 3447.8 | 3491.3 | 6939.0 | 4160.1 | -10.6 | 4149.4 |
| | | -18.50 | 3604.2 | 3620.4 | 7224.6 | 4331.3 | -10.6 | 4320.7 |
| | | -19.00 | 3632.7 | 3766.0 | 7398.7 | 4435.7 | -10.6 | 4425.0 |
| | | -19.50 | 4001.9 | 3909.8 | 7911.7 | 4743.2 | -10.6 | 4732.6 |
| | | -20.00 | 4434.1 | 4058.2 | 8492.2 | 5091.3 | -10.6 | 5080.6 |
| | | -20.50 | 4462.0 | 4240.5 | 8702.6 | 5217.4 | -10.6 | 5206.7 |
| | | -21.00 | 4529.9 | 4422.9 | 8952.8 | 5367.4 | -10.6 | 5356.8 |
| | | -21.50 | 4804.9 | 4605.3 | 9410.2 | 5641.6 | -10.6 | 5631.0 |
| | | -22.00 | 4915.9 | 4782.7 | 9698.6 | 5814.5 | -10.6 | 5803.8 |
| | | -22.50 | 4171.3 | 4965.0 | 9136.4 | 5477.5 | -10.6 | 5466.8 |
| | | -23.00 | 4114.3 | 5147.4 | 9261.7 | 5552.6 | -10.6 | 5541.9 |
| | | -23.50 | 4118.3 | 5329.8 | 9448.1 | 5664.3 | -10.6 | 5653.7 |
| | | -24.00 | 4082.6 | 5512.2 | 9594.8 | 5752.3 | -10.6 | 5741.6 |
| | | -24.50 | 4041.8 | 5690.4 | 9732.2 | 5834.7 | -10.6 | 5824.0 |
| | | -25.00 | 3952.6 | 5861.7 | 9814.3 | 5883.9 | -10.6 | 5873.3 |
| | | -25.50 | 3513.3 | 6057.7 | 9571.0 | 5738.0 | -10.6 | 5727.4 |
| | | -26.00 | 4076.2 | 6240.8 | 10316.9 | 6185.2 | -10.6 | 6174.6 |
| | | -26.50 | 4771.9 | 6399.5 | 11171.4 | 6697.5 | -10.6 | 6686.8 |
| | | -27.00 | 4956.5 | 6581.8 | 11538.3 | 6917.5 | -10.6 | 6906.8 |
| | | -27.50 | 5033.4 | 6764.2 | 11797.5 | 7072.9 | -10.6 | 7062.2 |
| | | -28.00 | 5022.7 | 6946.6 | 11969.2 | 7175.8 | -10.6 | 7165.2 |
| | | -28.50 | 3153.3 | 7128.9 | 10282.2 | 6164.4 | -10.6 | 6153.7 |
| -29.00 | 2862.1 | 7311.3 | 10173.4 | 6099.2 | -10.6 | 6088.5 | | |
| -29.50 | 2448.6 | 7493.7 | 9942.2 | 5960.6 | -10.6 | 5949.9 | | |
| -30.00 | 2003.0 | 7676.0 | 9679.0 | 5802.8 | -10.6 | 5792.1 | | |
| 312.S03 | 3.78 | -8.00 | 3022.7 | 1705.1 | 4727.8 | 2834.4 | 0.0 | 2834.4 |
| | | -8.50 | 3150.6 | 1887.5 | 5038.1 | 3020.4 | 0.0 | 3020.4 |
| | | -9.00 | 3312.7 | 2069.9 | 5382.6 | 3227.0 | 0.0 | 3227.0 |
| | | -9.50 | 3242.9 | 2252.2 | 5495.1 | 3294.4 | 0.0 | 3294.4 |
| | | -10.00 | 3221.5 | 2434.6 | 5656.1 | 3390.9 | 0.0 | 3390.9 |
| | | -10.50 | 3267.0 | 2614.8 | 5881.8 | 3526.3 | 0.0 | 3526.3 |
| | | -11.00 | 3377.3 | 2784.8 | 6162.1 | 3694.3 | 0.0 | 3694.3 |
| | | -11.50 | 3378.2 | 2967.2 | 6345.4 | 3804.2 | 0.0 | 3804.2 |
| | | -12.00 | 3555.2 | 3149.4 | 6704.6 | 4019.6 | 0.0 | 4019.6 |
| | | -12.50 | 3235.5 | 3331.8 | 6567.3 | 3937.2 | 0.0 | 3937.2 |
| | | -13.00 | 3501.0 | 3508.9 | 7009.9 | 4202.6 | 0.0 | 4202.6 |
| | | -13.50 | 3650.2 | 3637.5 | 7287.7 | 4369.1 | 0.0 | 4369.1 |
| | | -14.00 | 3560.3 | 3783.4 | 7343.7 | 4402.7 | 0.0 | 4402.7 |
| | | -14.50 | 3519.5 | 3929.3 | 7448.8 | 4465.7 | 0.0 | 4465.7 |
| | | -15.00 | 3517.0 | 4068.8 | 7585.9 | 4547.9 | 0.0 | 4547.9 |
| | | -15.50 | 3457.0 | 4214.7 | 7671.8 | 4599.4 | 0.0 | 4599.4 |
| | | -16.00 | 3463.5 | 4355.8 | 7819.4 | 4687.9 | 0.0 | 4687.9 |
| | | -16.50 | 3270.1 | 4501.7 | 7771.9 | 4659.4 | 0.0 | 4659.4 |
| | | -17.00 | 1832.2 | 4636.6 | 6468.7 | 3878.1 | 0.0 | 3878.1 |
| | | -17.50 | 1910.0 | 4742.0 | 6652.0 | 3988.0 | 0.0 | 3988.0 |
| | | -18.00 | 2008.7 | 4855.1 | 6863.8 | 4115.0 | 0.0 | 4115.0 |
| | | -18.50 | 2009.4 | 4997.1 | 7006.5 | 4200.5 | 0.0 | 4200.5 |
| | | -19.00 | 1998.4 | 5146.3 | 7144.7 | 4283.4 | 0.0 | 4283.4 |
| | | -19.50 | 1675.6 | 5301.1 | 6976.7 | 4182.7 | 0.0 | 4182.7 |
| | | -20.00 | 1752.0 | 5450.2 | 7202.2 | 4317.9 | 0.0 | 4317.9 |
| | | -20.50 | 2371.4 | 5580.7 | 7952.0 | 4767.4 | 0.0 | 4767.4 |
| | | -21.00 | 2762.6 | 5724.9 | 8487.5 | 5088.5 | 0.0 | 5088.5 |
| | | -21.50 | 3142.0 | 5858.8 | 9000.8 | 5396.2 | 0.0 | 5396.2 |
| | | -22.00 | 3324.2 | 6010.2 | 9334.4 | 5596.2 | 0.0 | 5596.2 |
| | | -22.50 | 3403.5 | 6188.1 | 9591.6 | 5750.3 | 0.0 | 5750.3 |
| -23.00 | 3444.5 | 6367.2 | 9811.6 | 5882.3 | 0.0 | 5882.3 | | |
| -23.50 | 3686.7 | 6540.9 | 10227.6 | 6131.7 | 0.0 | 6131.7 | | |
| -24.00 | 2530.6 | 6700.2 | 9230.8 | 5534.0 | 0.0 | 5534.0 | | |
| -24.50 | 2255.7 | 6882.6 | 9138.3 | 5478.6 | 0.0 | 5478.6 | | |
| -25.00 | 1854.5 | 7064.9 | 8919.5 | 5347.4 | 0.0 | 5347.4 | | |
| -25.50 | 1629.5 | 7236.3 | 8865.7 | 5315.2 | 0.0 | 5315.2 | | |
| -26.00 | 1463.5 | 7389.2 | 8852.8 | 5307.4 | 0.0 | 5307.4 | | |
| -26.50 | 1326.2 | 7567.7 | 8893.9 | 5332.1 | 0.0 | 5332.1 | | |
| -27.00 | 1059.1 | 7746.1 | 8805.1 | 5278.8 | 0.0 | 5278.8 | | |
| -27.50 | 1015.7 | 7841.7 | 8857.4 | 5310.2 | 0.0 | 5310.2 | | |
| -28.00 | 993.1 | 7917.6 | 8910.7 | 5342.1 | 0.0 | 5342.1 | | |
| -28.50 | 990.3 | 7975.7 | 8966.0 | 5375.3 | 0.0 | 5375.3 | | |
| 19-1008_43 | 9.88 | -8.00 | 2894.8 | 1547.8 | 4442.6 | 2663.4 | 0.0 | 2663.4 |
| | | -8.50 | 2974.3 | 1679.9 | 4654.2 | 2790.3 | 0.0 | 2790.3 |
| | | -9.00 | 3035.7 | 1815.0 | 4850.7 | 2908.1 | 0.0 | 2908.1 |
| | | -9.50 | 3056.0 | 1953.3 | 5009.3 | 3003.2 | 0.0 | 3003.2 |
| | | -10.00 | 3548.2 | 2079.3 | 5627.5 | 3373.8 | 0.0 | 3373.8 |
| | | -10.50 | 3546.7 | 2231.1 | 5777.8 | 3463.9 | 0.0 | 3463.9 |
| | | -11.00 | 3527.3 | 2413.4 | 5940.8 | 3561.6 | 0.0 | 3561.6 |
| | | -11.50 | 3503.0 | 2595.8 | 6098.8 | 3656.3 | 0.0 | 3656.3 |
| | | -12.00 | 3518.0 | 2778.0 | 6296.0 | 3774.6 | 0.0 | 3774.6 |
| | | -12.50 | 3390.7 | 2958.9 | 6349.6 | 3806.7 | 0.0 | 3806.7 |
| | | -13.00 | 3413.1 | 3093.5 | 6506.5 | 3900.8 | 0.0 | 3900.8 |
| | | -13.50 | 3660.9 | 3209.3 | 6870.2 | 4118.8 | 0.0 | 4118.8 |
| | | -14.00 | 3683.0 | 3344.4 | 7027.5 | 4213.1 | 0.0 | 4213.1 |
| | | -14.50 | 3519.4 | 3490.3 | 7009.7 | 4202.5 | 0.0 | 4202.5 |
| | | -15.00 | 4013.7 | 3617.9 | 7631.6 | 4575.3 | 0.0 | 4575.3 |
| -15.50 | 3499.4 | 3776.7 | 7276.1 | 4362.2 | 0.0 | 4362.2 | | |
| -16.00 | 3060.5 | 3952.0 | 7012.5 | 4204.1 | 0.0 | 4204.1 | | |
| -16.50 | 2804.5 | 4134.4 | 6938.9 | 4160.0 | 0.0 | 4160.0 | | |
| -17.00 | 2711.3 | 4316.8 | 7028.1 | 4213.5 | 0.0 | 4213.5 | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | Rekenwaarden | | | | |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|---------------------|-------------------------|-----|--------|
| | | | $R_{b,real}$ [kN] | $R_{s,real}$ [kN] | $R_{c,real}$ [kN] | $R_{b;d}$ [kN] | $F_{b;k;d}$ [kN] | $R_{c,netto;d}$ [kN] | | |
| 19-1008_43 | 9.88 | -17.50 | 2642.2 | 4492.4 | 7134.6 | 4277.4 | 0.0 | 4277.4 | | |
| | | -18.00 | 2579.6 | 4651.4 | 7231.0 | 4335.1 | 0.0 | 4335.1 | | |
| | | -18.50 | 2480.0 | 4793.7 | 7273.7 | 4360.7 | 0.0 | 4360.7 | | |
| | | -19.00 | 2355.2 | 4936.3 | 7291.5 | 4371.4 | 0.0 | 4371.4 | | |
| | | -19.50 | 2465.4 | 5051.5 | 7516.9 | 4506.5 | 0.0 | 4506.5 | | |
| | | -20.00 | 2767.0 | 5170.5 | 7937.4 | 4758.6 | 0.0 | 4758.6 | | |
| | | -20.50 | 2825.6 | 5320.7 | 8146.3 | 4883.9 | 0.0 | 4883.9 | | |
| | | -21.00 | 3077.2 | 5495.1 | 8572.3 | 5139.2 | 0.0 | 5139.2 | | |
| | | -21.50 | 4078.0 | 5639.2 | 9717.3 | 5825.7 | 0.0 | 5825.7 | | |
| | | 328.S02 | 10.17 | -8.00 | 2313.0 | 2313.0 | 4626.0 | 2773.4 | 0.0 | 2773.4 |
| | | | | -8.50 | 2278.4 | 2456.5 | 4735.0 | 2838.7 | 0.0 | 2838.7 |
| -9.00 | 2676.5 | | | 2596.6 | 5273.1 | 3161.3 | 0.0 | 3161.3 | | |
| -9.50 | 2880.6 | | | 2716.5 | 5597.1 | 3355.6 | 0.0 | 3355.6 | | |
| -10.00 | 3186.1 | | | 2851.7 | 6037.8 | 3619.8 | 0.0 | 3619.8 | | |
| -10.50 | 3377.1 | | | 2993.6 | 6370.8 | 3819.4 | 0.0 | 3819.4 | | |
| -11.00 | 3411.4 | | | 3156.8 | 6568.1 | 3937.7 | 0.0 | 3937.7 | | |
| -11.50 | 3473.1 | | | 3324.4 | 6797.5 | 4075.2 | 0.0 | 4075.2 | | |
| -12.00 | 3568.4 | | | 3486.4 | 7054.8 | 4229.5 | 0.0 | 4229.5 | | |
| -12.50 | 3097.1 | | | 3632.7 | 6729.8 | 4034.7 | 0.0 | 4034.7 | | |
| -13.00 | 3090.5 | | | 3775.5 | 6866.0 | 4116.3 | 0.0 | 4116.3 | | |
| -13.50 | 3107.3 | | | 3919.8 | 7027.1 | 4212.9 | 0.0 | 4212.9 | | |
| -14.00 | 3081.6 | | | 4065.7 | 7147.3 | 4285.0 | 0.0 | 4285.0 | | |
| -14.50 | 3095.8 | | | 4207.3 | 7303.0 | 4378.3 | 0.0 | 4378.3 | | |
| -15.00 | 2778.0 | | | 4354.7 | 7132.7 | 4276.2 | 0.0 | 4276.2 | | |
| -15.50 | 2843.6 | | | 4500.3 | 7343.9 | 4402.8 | 0.0 | 4402.8 | | |
| -16.00 | 3029.1 | | | 4644.8 | 7674.0 | 4600.7 | 0.0 | 4600.7 | | |
| -16.50 | 3203.6 | | | 4796.1 | 7999.7 | 4796.0 | 0.0 | 4796.0 | | |
| -17.00 | 3293.2 | | | 4978.5 | 8271.7 | 4959.0 | 0.0 | 4959.0 | | |
| -17.50 | 3172.1 | | | 5160.8 | 8332.9 | 4995.8 | 0.0 | 4995.8 | | |
| -18.00 | 2328.0 | | | 5370.1 | 7698.1 | 4615.2 | 0.0 | 4615.2 | | |
| -18.50 | 3693.9 | | | 5500.0 | 9193.8 | 5511.9 | 0.0 | 5511.9 | | |
| -19.00 | 3724.9 | | | 5663.2 | 9388.1 | 5628.4 | 0.0 | 5628.4 | | |
| -19.50 | 4062.5 | | | 5837.4 | 9899.9 | 5935.2 | 0.0 | 5935.2 | | |
| -20.00 | 4234.7 | | | 6019.7 | 10254.5 | 6147.8 | 0.0 | 6147.8 | | |
| -20.50 | 4597.6 | 6202.1 | 10799.7 | 6474.6 | 0.0 | 6474.6 | | | | |
| -21.00 | 4258.1 | 6384.4 | 10642.6 | 6380.4 | 0.0 | 6380.4 | | | | |
| -21.50 | 4381.3 | 6566.8 | 10948.1 | 6563.6 | 0.0 | 6563.6 | | | | |
| -22.00 | 4113.1 | 6749.2 | 10862.3 | 6512.2 | 0.0 | 6512.2 | | | | |
| -22.50 | 4221.0 | 6931.6 | 11152.5 | 6686.2 | 0.0 | 6686.2 | | | | |
| -23.00 | 4166.3 | 7113.9 | 11280.2 | 6762.7 | 0.0 | 6762.7 | | | | |
| -23.50 | 4217.2 | 7296.3 | 11513.5 | 6902.6 | 0.0 | 6902.6 | | | | |
| -24.00 | 4155.4 | 7478.7 | 11634.0 | 6974.8 | 0.0 | 6974.8 | | | | |
| -24.50 | 3869.0 | 7630.7 | 11499.7 | 6894.3 | 0.0 | 6894.3 | | | | |
| -25.00 | 3316.0 | 7776.6 | 11092.6 | 6650.2 | 0.0 | 6650.2 | | | | |

PAALGEGEVENS SI Ø508/670

Type : In de grond gevormde geschroefde paal; groutinjectie
Wijze van installeren : Schroeven
Wijze van terugwinnen : n.v.t.
Diameter [m] : 0.590
Elasticiteitsmodulus [N/mm²] : 20000
Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
Factor α_t (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
Paalklassefactor α_p : 0.63
Paalvoetvormfactor β : 1.00
Type lastzakingsdiagram : Grondverdringende paal
Verm.factor * $\varphi'_{j,k}$: 1.00
Groutomhulling : JA

PAALGEGEVENS SI Ø610/850

Type : In de grond gevormde geschroefde paal; groutinjectie
Wijze van installeren : Schroeven
Wijze van terugwinnen : n.v.t.
Diameter [m] : 0.730
Elasticiteitsmodulus [N/mm²] : 20000
Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
Factor α_t (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
Paalklassefactor α_p : 0.63
Paalvoetvormfactor β : 1.00
Type lastzakingsdiagram : Grondverdringende paal
Verm.factor * $\varphi'_{j,k}$: 1.00
Groutomhulling : JA

PAALGEGEVENS SI Ø762/950

Type : In de grond gevormde geschroefde paal; groutinjectie
Wijze van installeren : Schroeven
Wijze van terugwinnen : n.v.t.
Diameter [m] : 0.860
Elasticiteitsmodulus [N/mm²] : 20000
Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
Factor α_t (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
Paalklassefactor α_p : 0.63
Paalvoetvormfactor β : 1.00
Type lastzakingsdiagram : Grondverdringende paal
Verm.factor * $\varphi'_{j,k}$: 1.00
Groutomhulling : JA

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

OVERZICHT NETTO DRAAGVERMOGEN DRUKPALEN

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld niveau | paalpunt niveau | R _{d, netto, d} [kN] | | |
|-----------|--------------------|--------------------|-------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| 19-1008_1 | 2.12 | -6.00 | -71 | | |
| | | -6.50 | -70 | | |
| | | -7.00 | -66 | -67 | |
| | | -7.50 | -25 | -9 | |
| | | -8.00 | -13 | 8 | 34 |
| | | -8.50 | -17 | 17 | 89 |
| | | -9.00 | 84 | 149 | 223 |
| | | -9.50 | 120 | 189 | 270 |
| | | -10.00 | 152 | 232 | 320 |
| | | -10.50 | 198 | 310 | 447 |
| | | -11.00 | 304 | 443 | 596 |
| | | -11.50 | 358 | 511 | 676 |
| | | -12.00 | 397 | 552 | 738 |
| | | -12.50 | 706 | 1013 | 1344 |
| | | -13.00 | 789 | 1115 | 1464 |
| | | -13.50 | 870 | 1258 | 1694 |
| | | -14.00 | 1055 | 1478 | 1924 |
| | | -14.50 | 1219 | 1731 | 2207 |
| | | -15.00 | 1320 | 1835 | 2371 |
| | | -15.50 | 1307 | 1789 | 2289 |
| | | -16.00 | 1481 | 2040 | 2618 |
| | | -16.50 | 1593 | 2198 | 2795 |
| | | -17.00 | 1802 | 2640 | 3590 |
| | | -17.50 | 2612 | 3099 | 3961 |
| | | -18.00 | 2308 | 3188 | 3621 |
| | | -18.50 | 2363 | 2898 | 3769 |
| | | -19.00 | 2077 | 2916 | 3778 |
| | | -19.50 | 2080 | 2887 | 3743 |
| | | -20.00 | 2080 | 2859 | 3681 |
| | | -20.50 | 2185 | 2992 | 3840 |
| -21.00 | 2206 | 3114 | 4176 | | |
| -21.50 | 3011 | 4303 | 5815 | | |
| -22.00 | 3906 | 5554 | 7333 | | |
| -22.50 | 3981 | 5647 | 7442 | | |
| -23.00 | 4056 | 5740 | 7552 | | |
| -23.50 | 4131 | 5833 | 7661 | | |
| -24.00 | 4206 | 5926 | 7771 | | |
| -24.50 | 4281 | 6018 | 7880 | | |
| -25.00 | 4356 | 6111 | 7989 | | |
| -25.50 | 4431 | 6204 | 8099 | | |
| -26.00 | 4506 | 6297 | 8208 | | |
| -26.50 | 4581 | 6390 | 8317 | | |
| -27.00 | 4656 | 6482 | 8427 | | |
| -27.50 | 4731 | 6575 | 8536 | | |
| -28.00 | 4806 | 6668 | 8645 | | |
| -28.50 | 4881 | 6761 | 8755 | | |
| -29.00 | 4956 | 6854 | 8864 | | |
| -29.50 | 5031 | 6946 | | | |
| -30.00 | 5106 | | | | |
| 19-1008_6 | 11.00 | -6.00 | 2214 | | |
| | | -6.50 | 2342 | | |
| | | -7.00 | 2412 | 3371 | |
| | | -7.50 | 2767 | 3881 | |
| | | -8.00 | 2995 | 4221 | 5504 |
| | | -8.50 | 3209 | 4465 | 5802 |
| | | -9.00 | 3320 | 4589 | 5933 |
| | | -9.50 | 3386 | 4714 | 6181 |
| | | -10.00 | 3811 | 5435 | 6752 |
| | | -10.50 | 3886 | 5510 | 6802 |
| | | -11.00 | 3961 | 5501 | 7035 |
| | | -11.50 | 4026 | 5629 | 7217 |
| | | -12.00 | 4091 | 5716 | 7374 |
| | | -12.50 | 4121 | 5751 | 7449 |
| | | -13.00 | 4149 | 5798 | 7512 |
| | | -13.50 | 4336 | 6086 | 7960 |
| | | -14.00 | 4411 | 6179 | 8069 |
| | | -14.50 | 4486 | 6272 | 7823 |
| | | -15.00 | 4561 | 6035 | 6375 |
| | | -15.50 | 4395 | 5032 | 6419 |
| -16.00 | 3706 | 5018 | 6380 | | |
| -16.50 | 3764 | 5079 | 6446 | | |
| -17.00 | 3772 | 5070 | 6413 | | |
| -17.50 | 3781 | 5061 | 6381 | | |
| -18.00 | 3905 | 5497 | 7255 | | |
| -18.50 | 4606 | 6133 | 7834 | | |
| -19.00 | 4615 | 6248 | 7949 | | |
| -19.50 | 4717 | 6366 | 8079 | | |
| -20.00 | 4826 | 6494 | 8223 | | |
| -20.50 | 4926 | 6608 | | | |
| -21.00 | 5057 | 6889 | | | |
| -21.50 | 5497 | | | | |
| 166.S01 | 3.45 | -6.00 | 1435 | | |
| | | -6.50 | 1619 | | |
| | | -7.00 | 1721 | 2402 | |
| | | -7.50 | 1830 | 2529 | |
| | | -8.00 | 1954 | 2678 | 3437 |
| | | -8.50 | 2075 | 2836 | 3463 |
| | | -9.00 | 2181 | 2887 | 3600 |
| | | -9.50 | 2442 | 2991 | 3530 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | niveau | maalveld niveau | R _{n, netto;d} [kN] | | |
|------------|--------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -10.00 | 2244 | 2873 | 3635 | |
| | -10.50 | 2235 | 2924 | 3770 | |
| | -11.00 | 2170 | 3016 | 3876 | |
| | -11.50 | 2171 | 2985 | 3831 | |
| | -12.00 | 2178 | 2975 | 3812 | |
| | -12.50 | 2224 | 3029 | 3871 | |
| | -13.00 | 2336 | 3252 | 4286 | |
| | -13.50 | 2644 | 3634 | 4717 | |
| | -14.00 | 2754 | 3777 | 4855 | |
| | -14.50 | 2865 | 3915 | 5017 | |
| | -15.00 | 2968 | 4057 | 5250 | |
| | -15.50 | 3248 | 4454 | 5701 | |
| | -16.00 | 3390 | 4620 | 5837 | |
| | -16.50 | 3510 | 4714 | 5930 | |
| | -17.00 | 3596 | 4779 | 6068 | |
| | -17.50 | 3653 | 4919 | 6233 | |
| | -18.00 | 3758 | 5056 | 6394 | |
| | -18.50 | 3842 | 5185 | 6544 | |
| | -19.00 | 3899 | 5284 | 6652 | |
| | -19.50 | 3938 | 5347 | | |
| | -20.00 | 4107 | | | |
| 19-1008_11 | 0.62 | -6.00 | -54 | | |
| | | -6.50 | -48 | | |
| | | -7.00 | 32 | 105 | |
| | | -7.50 | 136 | 239 | |
| | | -8.00 | 171 | 279 | 402 |
| | | -8.50 | 201 | 314 | 440 |
| | | -9.00 | 234 | 354 | 440 |
| | | -9.50 | 269 | 355 | 490 |
| | | -10.00 | 269 | 400 | 546 |
| | | -10.50 | 295 | 432 | 582 |
| | | -11.00 | 328 | 474 | 632 |
| | | -11.50 | 346 | 491 | 645 |
| | | -12.00 | 321 | 455 | 618 |
| | | -12.50 | 722 | 1101 | 1537 |
| | | -13.00 | 1011 | 1342 | 1789 |
| | | -13.50 | 1018 | 1452 | 1917 |
| | | -14.00 | 1107 | 1561 | 2049 |
| | | -14.50 | 1189 | 1657 | 2155 |
| | | -15.00 | 1264 | 1742 | 2245 |
| | | -15.50 | 1345 | 1835 | 2380 |
| | | -16.00 | 1510 | 2062 | 2641 |
| | | -16.50 | 1592 | 2158 | 2748 |
| | | -17.00 | 1668 | 2251 | 2897 |
| | | -17.50 | 1931 | 2770 | 3654 |
| | | -18.00 | 2298 | 3231 | 4265 |
| | | -18.50 | 2424 | 3432 | 4407 |
| | | -19.00 | 2519 | 3546 | 4595 |
| | | -19.50 | 2585 | 3615 | 4708 |
| | | -20.00 | 2819 | 3761 | 4242 |
| | | -20.50 | 2748 | 3283 | 4178 |
| | | -21.00 | 2431 | 3352 | 4192 |
| | | -21.50 | 2452 | 3371 | 4269 |
| | | -22.00 | 2388 | 3242 | 4135 |
| | | -22.50 | 2400 | 3239 | 4110 |
| | | -23.00 | 2393 | 3221 | 4074 |
| | | -23.50 | 2579 | 3495 | 4415 |
| | | -24.00 | 2660 | 3581 | 4535 |
| | | -24.50 | 2705 | 3627 | 4580 |
| | | -25.00 | 2746 | 3690 | 4829 |
| | | -25.50 | 3413 | 4470 | 5712 |
| | | -26.00 | 3368 | 4566 | 5816 |
| | | -26.50 | 3439 | 4642 | 5892 |
| | | -27.00 | 3534 | 4755 | 6019 |
| | | -27.50 | 3654 | 4905 | 6198 |
| | | -28.00 | 3854 | 5270 | 6675 |
| | | -28.50 | 4066 | 5484 | 6940 |
| | | -29.00 | 4216 | 5846 | 7529 |
| | | -29.50 | 4771 | 6504 | 8297 |
| | | -30.00 | 4932 | 6706 | 8454 |
| 19-1008_12 | 3.57 | -6.00 | 1757 | | |
| | | -6.50 | 1419 | | |
| | | -7.00 | 1376 | 1754 | |
| | | -7.50 | 1336 | 1722 | |
| | | -8.00 | 1291 | 1627 | 1871 |
| | | -8.50 | 1283 | 1577 | 1894 |
| | | -9.00 | 1262 | 1597 | 1919 |
| | | -9.50 | 1280 | 1622 | 1923 |
| | | -10.00 | 1294 | 1623 | 1946 |
| | | -10.50 | 1310 | 1651 | 1981 |
| | | -11.00 | 1301 | 1641 | 1983 |
| | | -11.50 | 1341 | 1691 | 2027 |
| | | -12.00 | 1354 | 1704 | 2038 |
| | | -12.50 | 1361 | 1714 | 2050 |
| | | -13.00 | 1381 | 1751 | 2122 |
| | | -13.50 | 1439 | 1833 | 2209 |
| | | -14.00 | 1473 | 1868 | 2251 |
| | | -14.50 | 1500 | 1899 | 2285 |
| | | -15.00 | 1525 | 1929 | 2320 |
| | | -15.50 | 1575 | 2021 | 2436 |
| | | -16.00 | 1628 | 2071 | 2501 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paaldragvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld niveau | paalpunt niveau | R _{z, netto;d} [kN] | | |
|------------|--------------------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | | -16.50 | 1666 | 2119 | 2561 |
| | | -17.00 | 1712 | 2182 | 2636 |
| | | -17.50 | 1748 | 2292 | 2826 |
| | | -18.00 | 1953 | 2528 | 3097 |
| | | -18.50 | 2032 | 2620 | 3219 |
| | | -19.00 | 2289 | 3006 | 3718 |
| | | -19.50 | 2424 | 3223 | 4107 |
| | | -20.00 | 2650 | 3505 | 4371 |
| | | -20.50 | 2651 | 3477 | 4312 |
| | | -21.00 | 2933 | 3892 | 4860 |
| | | -21.50 | 3060 | 4038 | 5031 |
| | | -22.00 | 3189 | 4197 | 5218 |
| | | -22.50 | 3274 | 4290 | 5146 |
| | | -23.00 | 3488 | 4319 | 4872 |
| | | -23.50 | 3418 | 4047 | 4882 |
| | | -24.00 | 3155 | 4052 | 4892 |
| | | -24.50 | 3119 | 3990 | 4726 |
| | | -25.00 | 3102 | 3889 | 4757 |
| | | -25.50 | 3052 | 3914 | 4768 |
| | | -26.00 | 3118 | 3992 | 4851 |
| | | -26.50 | 3176 | 4065 | 4937 |
| | | -27.00 | 3227 | 4127 | 5010 |
| | | -27.50 | 3267 | 4163 | 5071 |
| | | -28.00 | 3621 | 4809 | 6054 |
| | | -28.50 | 4017 | 5278 | |
| | | -29.00 | 4127 | | |
| 19-1008_17 | 0.20 | -6.00 | -42 | | |
| | | -6.50 | 0 | | |
| | | -7.00 | -50 | -34 | |
| | | -7.50 | -88 | -87 | |
| | | -8.00 | -78 | -60 | -30 |
| | | -8.50 | -51 | -32 | -4 |
| | | -9.00 | -48 | -10 | 65 |
| | | -9.50 | 222 | 386 | 573 |
| | | -10.00 | 89 | 206 | 351 |
| | | -10.50 | 336 | 692 | 1161 |
| | | -11.00 | 994 | 1534 | 2105 |
| | | -11.50 | 1157 | 1698 | 1986 |
| | | -12.00 | 1297 | 1611 | 2189 |
| | | -12.50 | 1201 | 1755 | 2351 |
| | | -13.00 | 1268 | 1810 | 2396 |
| | | -13.50 | 1345 | 1893 | 2478 |
| | | -14.00 | 1431 | 1989 | 2579 |
| | | -14.50 | 1605 | 2295 | 3000 |
| | | -15.00 | 1801 | 2502 | 2233 |
| | | -15.50 | 1911 | 1856 | 2319 |
| | | -16.00 | 1448 | 1866 | 2421 |
| | | -16.50 | 1406 | 1950 | 2516 |
| | | -17.00 | 1494 | 2063 | 2663 |
| | | -17.50 | 1469 | 2003 | 2562 |
| | | -18.00 | 1465 | 1953 | 2481 |
| | | -18.50 | 1704 | 2357 | 2986 |
| | | -19.00 | 1865 | 2448 | 3126 |
| | | -19.50 | 1880 | 2552 | 3253 |
| | | -20.00 | 1971 | 2671 | 3402 |
| | | -20.50 | 2101 | 2850 | 3632 |
| | | -21.00 | 2081 | 2798 | 3494 |
| | | -21.50 | 2286 | 3154 | 3888 |
| | | -22.00 | 2531 | 3186 | 3955 |
| | | -22.50 | 2473 | 3245 | 4031 |
| | | -23.00 | 2477 | 3256 | 4024 |
| | | -23.50 | 2504 | 3274 | 4084 |
| | | -24.00 | 2541 | 3356 | 4171 |
| | | -24.50 | 2592 | 3413 | 4232 |
| | | -25.00 | 2653 | 3487 | 4326 |
| | | -25.50 | 2713 | 3561 | 4418 |
| | | -26.00 | 2785 | 3663 | 3567 |
| | | -26.50 | 2921 | 2996 | 3598 |
| | | -27.00 | 2385 | 3021 | 3669 |
| | | -27.50 | 2408 | 3078 | 3734 |
| | | -28.00 | 2448 | 3123 | 3781 |
| | | -28.50 | 2452 | 3110 | 3748 |
| | | -29.00 | 2401 | 3015 | 3600 |
| | | -29.50 | 2721 | 3656 | 4665 |
| | | -30.00 | 3140 | 4113 | 5110 |
| 19-1008_20 | -0.03 | -6.00 | 326 | | |
| | | -6.50 | 476 | | |
| | | -7.00 | 501 | 643 | |
| | | -7.50 | 557 | 580 | |
| | | -8.00 | 456 | 602 | 775 |
| | | -8.50 | 473 | 646 | 827 |
| | | -9.00 | 501 | 674 | 853 |
| | | -9.50 | 518 | 692 | 867 |
| | | -10.00 | 496 | 656 | 821 |
| | | -10.50 | 614 | 809 | 1005 |
| | | -11.00 | 612 | 819 | 1030 |
| | | -11.50 | 598 | 785 | 974 |
| | | -12.00 | 624 | 828 | 1036 |
| | | -12.50 | 651 | 860 | 1073 |
| | | -13.00 | 664 | 873 | 1084 |
| | | -13.50 | 729 | 974 | 1188 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld niveau | paalpunt niveau | R _{z, netto;d} [kN] | | |
|------------|--------------------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -14.00 | 761 | 979 | 1215 | |
| | -14.50 | 772 | 1013 | 1259 | |
| | -15.00 | 805 | 1052 | 1301 | |
| | -15.50 | 829 | 1081 | 1334 | |
| | -16.00 | 854 | 1114 | 1375 | |
| | -16.50 | 871 | 1140 | 1403 | |
| | -17.00 | 902 | 1186 | 1502 | |
| | -17.50 | 1027 | 1361 | 1699 | |
| | -18.00 | 1075 | 1424 | 1774 | |
| | -18.50 | 1103 | 1475 | 1883 | |
| | -19.00 | 1197 | 1583 | 1956 | |
| | -19.50 | 1309 | 1669 | 2010 | |
| | -20.00 | 1310 | 1665 | 2068 | |
| | -20.50 | 1277 | 1658 | 2043 | |
| | -21.00 | 1297 | 1671 | 2039 | |
| | -21.50 | 1324 | 1701 | 2073 | |
| | -22.00 | 1349 | 1733 | 2110 | |
| | -22.50 | 1367 | 1769 | 2233 | |
| | -23.00 | 1627 | 2148 | 2699 | |
| | -23.50 | 1746 | 2310 | 2884 | |
| | -24.00 | 1862 | 2471 | 3119 | |
| | -24.50 | 1966 | 2602 | 3238 | |
| | -25.00 | 2044 | 2694 | 3355 | |
| | -25.50 | 2123 | 2790 | 3466 | |
| | -26.00 | 2196 | 2907 | 3377 | |
| | -26.50 | 2300 | 2817 | 3483 | |
| | -27.00 | 2224 | 2896 | 3517 | |
| | -27.50 | 2292 | 2940 | 3611 | |
| | -28.00 | 2314 | 3017 | 3707 | |
| | -28.50 | 2361 | 3097 | 3800 | |
| | -29.00 | 2402 | 3161 | 3883 | |
| | -29.50 | 2451 | 3224 | 3786 | |
| | -30.00 | 2509 | 3138 | 3877 | |
| 19-1008_21 | 1.78 | -6.00 | 669 | | |
| | | -6.50 | 601 | | |
| | | -7.00 | 617 | 863 | |
| | | -7.50 | 672 | 924 | |
| | | -8.00 | 721 | 995 | 1276 |
| | | -8.50 | 733 | 986 | 1245 |
| | | -9.00 | 756 | 1029 | 1316 |
| | | -9.50 | 870 | 1190 | 1508 |
| | | -10.00 | 900 | 1258 | 1593 |
| | | -10.50 | 945 | 1319 | 1693 |
| | | -11.00 | 976 | 1355 | 1757 |
| | | -11.50 | 1015 | 1403 | 1813 |
| | | -12.00 | 1043 | 1465 | 1759 |
| | | -12.50 | 1086 | 1441 | 1847 |
| | | -13.00 | 1119 | 1529 | 1958 |
| | | -13.50 | 1168 | 1589 | 1844 |
| | | -14.00 | 1196 | 1544 | 1840 |
| | | -14.50 | 1186 | 1576 | 1976 |
| | | -15.00 | 1177 | 1676 | 1913 |
| | | -15.50 | 1214 | 1592 | 1976 |
| | | -16.00 | 1232 | 1601 | 1970 |
| | | -16.50 | 1212 | 1549 | 1878 |
| | | -17.00 | 1235 | 1590 | 1949 |
| | | -17.50 | 1276 | 1703 | 2065 |
| | | -18.00 | 1357 | 1731 | 2099 |
| | | -18.50 | 1382 | 1764 | 2140 |
| | | -19.00 | 1413 | 1800 | 2178 |
| | | -19.50 | 1426 | 1817 | 2197 |
| | | -20.00 | 1440 | 1833 | 2216 |
| | | -20.50 | 1455 | 1852 | 2240 |
| | | -21.00 | 1476 | 1883 | 2280 |
| | | -21.50 | 1499 | 1913 | 2316 |
| | | -22.00 | 1523 | 1944 | 2354 |
| | | -22.50 | 1544 | 1972 | 2387 |
| | | -23.00 | 1565 | 1999 | 2422 |
| | | -23.50 | 1596 | 2042 | 2473 |
| | | -24.00 | 1624 | 2071 | 2512 |
| | | -24.50 | 1645 | 2101 | 2545 |
| | | -25.00 | 1670 | 2130 | 2581 |
| | | -25.50 | 1693 | 2161 | 2618 |
| | | -26.00 | 1717 | 2191 | 2652 |
| | | -26.50 | 1739 | 2221 | 2688 |
| | | -27.00 | 1761 | 2249 | 2721 |
| | | -27.50 | 1795 | 2295 | 2783 |
| | | -28.00 | 1820 | 2328 | 2825 |
| | | -28.50 | 1845 | 2359 | 2861 |
| | | -29.00 | 1876 | 2400 | 2914 |
| | | -29.50 | 1907 | 2440 | 2960 |
| | | -30.00 | 1934 | 2476 | |
| 251.S01 | -1.05 | -6.00 | 642 | | |
| | | -6.50 | 547 | | |
| | | -7.00 | 577 | 777 | |
| | | -7.50 | 574 | 754 | |
| | | -8.00 | 578 | 746 | 910 |
| | | -8.50 | 562 | 735 | 955 |
| | | -9.00 | 809 | 1136 | 1515 |
| | | -9.50 | 942 | 1268 | 1612 |
| | | -10.00 | 1000 | 1345 | 1702 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld paalpunt | | R _{z, netto, d} [kN] | | |
|------------|-------------------|--------|-------------------------------|-----------|-----------|
| | niveau | niveau | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -10.50 | 1050 | 1397 | 1752 | |
| | -11.00 | 1083 | 1427 | 1777 | |
| | -11.50 | 1141 | 1502 | 1876 | |
| | -12.00 | 1336 | 1784 | 1957 | |
| | -12.50 | 1424 | 1641 | 2060 | |
| | -13.00 | 1301 | 1727 | 2164 | |
| | -13.50 | 1365 | 1808 | 2261 | |
| | -14.00 | 1407 | 1858 | 2309 | |
| | -14.50 | 1412 | 1854 | 2284 | |
| | -15.00 | 1374 | 1816 | 2339 | |
| | -15.50 | 1959 | 2704 | 3061 | |
| | -16.00 | 2182 | 2533 | 3145 | |
| | -16.50 | 1982 | 2595 | 3272 | |
| | -17.00 | 2032 | 2711 | 3390 | |
| | -17.50 | 2109 | 2780 | 3462 | |
| | -18.00 | 2132 | 2789 | 2956 | |
| | -18.50 | 2122 | 2489 | 2990 | |
| | -19.00 | 2033 | 2533 | 2976 | |
| | -19.50 | 1990 | 2508 | 2996 | |
| | -20.00 | 1994 | 2503 | 3009 | |
| | -20.50 | 1999 | 2528 | 3038 | |
| | -21.00 | 2044 | 2572 | 3077 | |
| | -21.50 | 2066 | 2596 | 3100 | |
| | -22.00 | 2079 | 2612 | 3119 | |
| | -22.50 | 2117 | 2698 | 3235 | |
| | -23.00 | 2179 | 2747 | 3316 | |
| | -23.50 | 2274 | 2887 | 3481 | |
| | -24.00 | 2323 | 2946 | 3549 | |
| | -24.50 | 2371 | 3024 | 3716 | |
| | -25.00 | 2548 | 3262 | 3995 | |
| | -25.50 | 2859 | 3712 | 4564 | |
| | -26.00 | 3286 | 4578 | 5368 | |
| | -26.50 | 3902 | 4481 | 5606 | |
| | -27.00 | 3517 | 4619 | 5464 | |
| | -27.50 | 3625 | 4608 | 5147 | |
| | -28.00 | 3650 | 4253 | 5038 | |
| | -28.50 | 3328 | 4132 | 4969 | |
| | -29.00 | 3250 | 4106 | 4858 | |
| | -29.50 | 3262 | 4066 | 4904 | |
| | -30.00 | 3179 | 4027 | 4845 | |
| 19-1008_29 | 0.79 | -6.00 | 1247 | | |
| | | -6.50 | 1472 | | |
| | | -7.00 | 1491 | 2032 | |
| | | -7.50 | 1547 | 2153 | |
| | | -8.00 | 1619 | 2244 | 2523 |
| | | -8.50 | 1684 | 2069 | 1822 |
| | | -9.00 | 1648 | 1520 | 1901 |
| | | -9.50 | 1219 | 1589 | 1977 |
| | | -10.00 | 1260 | 1656 | 2057 |
| | | -10.50 | 1292 | 1688 | 2102 |
| | | -11.00 | 1307 | 1694 | 2078 |
| | | -11.50 | 1274 | 1747 | 2190 |
| | | -12.00 | 1434 | 1818 | 2190 |
| | | -12.50 | 1444 | 1830 | 2222 |
| | | -13.00 | 1434 | 1819 | 2192 |
| | | -13.50 | 1463 | 1854 | 2233 |
| | | -14.00 | 1490 | 1887 | 2271 |
| | | -14.50 | 1514 | 1917 | 2305 |
| | | -15.00 | 1541 | 1982 | 2416 |
| | | -15.50 | 1607 | 2045 | 2471 |
| | | -16.00 | 1622 | 2051 | 2466 |
| | | -16.50 | 1647 | 2085 | 2506 |
| | | -17.00 | 1690 | 2194 | 2725 |
| | | -17.50 | 2088 | 2889 | 3694 |
| | | -18.00 | 2389 | 3199 | 4024 |
| | | -18.50 | 2411 | 3208 | 4024 |
| | | -19.00 | 2233 | 3087 | 4030 |
| | | -19.50 | 3057 | 4144 | 4590 |
| | | -20.00 | 3420 | 3787 | 4434 |
| | | -20.50 | 2966 | 3650 | 4370 |
| | | -21.00 | 2855 | 3552 | 4325 |
| | | -21.50 | 2709 | 3485 | 4238 |
| | | -22.00 | 2677 | 3429 | 4108 |
| | | -22.50 | 2608 | 3340 | 4050 |
| | | -23.00 | 2640 | 3376 | 4088 |
| | | -23.50 | 2732 | 3465 | 4213 |
| | | -24.00 | 2757 | 3537 | 4277 |
| | | -24.50 | 2790 | 3562 | 4296 |
| | | -25.00 | 2820 | 3591 | 4342 |
| | | -25.50 | 2868 | 3654 | 4420 |
| | | -26.00 | 2908 | 3695 | 4467 |
| | | -26.50 | 2941 | 3742 | 4523 |
| | | -27.00 | 2977 | 3784 | 4568 |
| | | -27.50 | 3024 | 3834 | 4628 |
| | | -28.00 | 3051 | 3876 | 4678 |
| | | -28.50 | 3088 | 3985 | 4772 |
| | | -29.00 | 3257 | 4351 | 5163 |
| | | -29.50 | 3412 | 4318 | 5194 |
| | | -30.00 | 3371 | 4271 | 5132 |
| 283.S02 | 0.17 | -6.00 | 1011 | | |
| | | -6.50 | 1081 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld niveau | paalpunt niveau | R _{z, netto;d} [kN] | | |
|------------|--------------------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -7.00 | 1112 | 1532 | | |
| | -7.50 | 1178 | 1673 | | |
| | -8.00 | 1252 | 1746 | 2235 | |
| | -8.50 | 1298 | 1802 | 2004 | |
| | -9.00 | 1334 | 1605 | 2073 | |
| | -9.50 | 1201 | 1653 | 2129 | |
| | -10.00 | 1242 | 1701 | 2184 | |
| | -10.50 | 1275 | 1740 | 2227 | |
| | -11.00 | 1309 | 1779 | 2271 | |
| | -11.50 | 1306 | 1783 | 2308 | |
| | -12.00 | 1550 | 2164 | 2785 | |
| | -12.50 | 1688 | 2342 | 3042 | |
| | -13.00 | 1830 | 2549 | 3310 | |
| | -13.50 | 1978 | 2696 | 3461 | |
| | -14.00 | 2071 | 2823 | 3611 | |
| | -14.50 | 2127 | 2880 | 3664 | |
| | -15.00 | 2165 | 2946 | 3785 | |
| | -15.50 | 2354 | 3174 | 4025 | |
| | -16.00 | 2506 | 3419 | 4340 | |
| | -16.50 | 2675 | 3628 | 4686 | |
| | -17.00 | 2947 | 4001 | 4926 | |
| | -17.50 | 3053 | 4032 | 5101 | |
| | -18.00 | 3054 | 4179 | 5285 | |
| | -18.50 | 3154 | 4307 | 5478 | |
| | -19.00 | 3254 | 4432 | 5663 | |
| | -19.50 | 3337 | 4532 | 5781 | |
| | -20.00 | 3324 | 4552 | 5786 | |
| | -20.50 | 3530 | 4906 | 6364 | |
| | -21.00 | 3780 | 5158 | 6572 | |
| | -21.50 | 3879 | 5289 | 6736 | |
| | -22.00 | 3959 | 5387 | 6859 | |
| | -22.50 | 4042 | 5484 | 6979 | |
| | -23.00 | 4149 | 5681 | 5897 | |
| | -23.50 | 4432 | 4956 | 5202 | |
| | -24.00 | 4214 | 4283 | 5072 | |
| | -24.50 | 3328 | 4156 | 4994 | |
| | -25.00 | 3261 | 4124 | 4962 | |
| | -25.50 | 3180 | 4032 | 4839 | |
| | -26.00 | 3179 | 4008 | 4810 | |
| | -26.50 | 3149 | 3974 | 4767 | |
| | -27.00 | 3187 | 4034 | 4759 | |
| | -27.50 | 3228 | 4008 | 4800 | |
| | -28.00 | 3221 | 4045 | 4843 | |
| | -28.50 | 3243 | 4080 | 4881 | |
| | -29.00 | 3268 | 4109 | | |
| | -29.50 | 3289 | | | |
| 19-1008_35 | 0.92 | -6.00 | 931 | | |
| | | -6.50 | 951 | | |
| | | -7.00 | 979 | 1385 | |
| | | -7.50 | 1054 | 1475 | |
| | | -8.00 | 1085 | 1510 | 1961 |
| | | -8.50 | 1107 | 1533 | 1983 |
| | | -9.00 | 1143 | 1588 | 2073 |
| | | -9.50 | 1203 | 1660 | 2143 |
| | | -10.00 | 1238 | 1738 | 2280 |
| | | -10.50 | 1316 | 1811 | 2333 |
| | | -11.00 | 1350 | 1846 | 2366 |
| | | -11.50 | 1374 | 1867 | 2382 |
| | | -12.00 | 1399 | 1896 | 2415 |
| | | -12.50 | 1503 | 2095 | 2701 |
| | | -13.00 | 1639 | 2243 | 2875 |
| | | -13.50 | 1731 | 2370 | 3052 |
| | | -14.00 | 1919 | 2610 | 3247 |
| | | -14.50 | 1987 | 2616 | 3347 |
| | | -15.00 | 1991 | 2707 | 3453 |
| | | -15.50 | 2059 | 2793 | 3556 |
| | | -16.00 | 2117 | 2858 | 3628 |
| | | -16.50 | 2133 | 2861 | 3613 |
| | | -17.00 | 2175 | 2923 | 3723 |
| | | -17.50 | 2341 | 3147 | 3977 |
| | | -18.00 | 2383 | 3240 | 4149 |
| | | -18.50 | 2525 | 3423 | 4320 |
| | | -19.00 | 2589 | 3501 | 4425 |
| | | -19.50 | 2680 | 3659 | 4732 |
| | | -20.00 | 2932 | 3983 | 5080 |
| | | -20.50 | 3025 | 4093 | 5206 |
| | | -21.00 | 3124 | 4215 | 5356 |
| | | -21.50 | 3250 | 4481 | 5630 |
| | | -22.00 | 3544 | 4581 | 5803 |
| | | -22.50 | 3489 | 4701 | 5466 |
| | | -23.00 | 3572 | 4409 | 5541 |
| | | -23.50 | 3360 | 4475 | 5653 |
| | | -24.00 | 3412 | 4560 | 5741 |
| | | -24.50 | 3473 | 4632 | 5824 |
| | | -25.00 | 3518 | 4681 | 5873 |
| | | -25.50 | 3449 | 4569 | 5727 |
| | | -26.00 | 3673 | 4891 | 6174 |
| | | -26.50 | 3983 | 5319 | 6686 |
| | | -27.00 | 4119 | 5493 | 6906 |
| | | -27.50 | 4228 | 5627 | 7062 |
| | | -28.00 | 4312 | 5722 | 7165 |
| | | -28.50 | 4545 | 6006 | 6153 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paaldragvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld niveau | paalpunt niveau | R _{z, netto,z} [kN] | | |
|------------|--------------------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | | -29.00 | 4701 | 5096 | 6088 |
| | | -29.50 | 3968 | 4993 | 5949 |
| | | -30.00 | 3887 | 4864 | 5792 |
| 312.S03 | 3.78 | -6.00 | 843 | | |
| | | -6.50 | 861 | | |
| | | -7.00 | 855 | 1128 | |
| | | -7.50 | 1010 | 1532 | |
| | | -8.00 | 1674 | 2177 | 2834 |
| | | -8.50 | 1685 | 2333 | 3020 |
| | | -9.00 | 1819 | 2505 | 3226 |
| | | -9.50 | 1890 | 2576 | 3294 |
| | | -10.00 | 2032 | 2758 | 3390 |
| | | -10.50 | 2244 | 2789 | 3526 |
| | | -11.00 | 2174 | 2921 | 3694 |
| | | -11.50 | 2286 | 3051 | 3804 |
| | | -12.00 | 2398 | 3198 | 4019 |
| | | -12.50 | 2393 | 3159 | 3937 |
| | | -13.00 | 2429 | 3330 | 4202 |
| | | -13.50 | 2596 | 3532 | 4369 |
| | | -14.00 | 2666 | 3602 | 4402 |
| | | -14.50 | 2690 | 3555 | 4465 |
| | | -15.00 | 2685 | 3589 | 4547 |
| | | -15.50 | 2733 | 3638 | 4599 |
| | | -16.00 | 2768 | 3712 | 4687 |
| | | -16.50 | 2774 | 3703 | 4659 |
| | | -17.00 | 2793 | 3717 | 3878 |
| | | -17.50 | 2864 | 3238 | 3988 |
| | | -18.00 | 2563 | 3338 | 4114 |
| | | -18.50 | 2622 | 3410 | 4200 |
| | | -19.00 | 2680 | 3482 | 4283 |
| | | -19.50 | 2653 | 3421 | 4182 |
| | | -20.00 | 2623 | 3442 | 4317 |
| | | -20.50 | 2967 | 3865 | 4767 |
| | | -21.00 | 3149 | 4115 | 5088 |
| | | -21.50 | 3269 | 4319 | 5396 |
| | | -22.00 | 3455 | 4521 | 5596 |
| | | -22.50 | 3573 | 4666 | 5750 |
| | | -23.00 | 3668 | 4774 | 5882 |
| | | -23.50 | 3756 | 4944 | 6131 |
| | | -24.00 | 3955 | 5177 | 5534 |
| | | -24.50 | 4047 | 4573 | 5478 |
| | | -25.00 | 3583 | 4520 | 5347 |
| | | -25.50 | 3571 | 4448 | 5315 |
| | | -26.00 | 3529 | 4444 | 5307 |
| | | -26.50 | 3524 | 4436 | 5332 |
| | | -27.00 | 3485 | 4400 | 5278 |
| | | -27.50 | 3511 | 4429 | 5310 |
| | | -28.00 | 3536 | 4458 | 5342 |
| | | -28.50 | 3559 | 4486 | 5375 |
| | | -29.00 | 3586 | 4562 | |
| | | -29.50 | 3650 | | |
| 19-1008_43 | 9.88 | -6.00 | 934 | | |
| | | -6.50 | 1259 | | |
| | | -7.00 | 1331 | 1862 | |
| | | -7.50 | 1405 | 1962 | |
| | | -8.00 | 1485 | 2063 | 2663 |
| | | -8.50 | 1563 | 2159 | 2790 |
| | | -9.00 | 1645 | 2260 | 2908 |
| | | -9.50 | 1716 | 2344 | 3003 |
| | | -10.00 | 1899 | 2659 | 3373 |
| | | -10.50 | 2053 | 2723 | 3463 |
| | | -11.00 | 2070 | 2793 | 3561 |
| | | -11.50 | 2127 | 2902 | 3656 |
| | | -12.00 | 2186 | 2997 | 3774 |
| | | -12.50 | 2201 | 3010 | 3806 |
| | | -13.00 | 2235 | 3054 | 3900 |
| | | -13.50 | 2354 | 3216 | 4118 |
| | | -14.00 | 2416 | 3294 | 4213 |
| | | -14.50 | 2428 | 3294 | 4202 |
| | | -15.00 | 2731 | 3732 | 4575 |
| | | -15.50 | 2812 | 3659 | 4362 |
| | | -16.00 | 2792 | 3554 | 4204 |
| | | -16.50 | 2773 | 3385 | 4160 |
| | | -17.00 | 2588 | 3369 | 4213 |
| | | -17.50 | 2594 | 3429 | 4277 |
| | | -18.00 | 2641 | 3481 | 4335 |
| | | -18.50 | 2671 | 3510 | 4360 |
| | | -19.00 | 2694 | 3529 | 4371 |
| | | -19.50 | 2763 | 3625 | 4506 |
| | | -20.00 | 2894 | 3827 | 4758 |
| | | -20.50 | 2993 | 3937 | 4883 |
| | | -21.00 | 3107 | 4120 | 5139 |
| | | -21.50 | 3414 | 4654 | 5825 |
| | | -22.00 | 3855 | 4777 | |
| | | -22.50 | 3660 | | |
| 328.S02 | 10.17 | -6.00 | 1386 | | |
| | | -6.50 | 1350 | | |
| | | -7.00 | 1478 | 1994 | |
| | | -7.50 | 1563 | 2102 | |
| | | -8.00 | 1641 | 2198 | 2773 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld paalpunt | | R _{n, netto;d} [kN] | | |
|-----------|-------------------|--------|------------------------------|-----------|-----------|
| | niveau | niveau | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -8.50 | 1698 | 2261 | 2838 | |
| | -9.00 | 1824 | 2508 | 3161 | |
| | -9.50 | 1997 | 2671 | 3355 | |
| | -10.00 | 2160 | 2872 | 3619 | |
| | -10.50 | 2270 | 3038 | 3819 | |
| | -11.00 | 2355 | 3180 | 3937 | |
| | -11.50 | 2427 | 3251 | 4075 | |
| | -12.00 | 2492 | 3355 | 4229 | |
| | -12.50 | 2579 | 3464 | 4034 | |
| | -13.00 | 2673 | 3287 | 4116 | |
| | -13.50 | 2539 | 3349 | 4212 | |
| | -14.00 | 2564 | 3414 | 4284 | |
| | -14.50 | 2620 | 3493 | 4378 | |
| | -15.00 | 2658 | 3542 | 4276 | |
| | -15.50 | 2663 | 3518 | 4402 | |
| | -16.00 | 2765 | 3672 | 4600 | |
| | -16.50 | 2876 | 3824 | 4795 | |
| | -17.00 | 2976 | 3956 | 4959 | |
| | -17.50 | 3017 | 3996 | 4995 | |
| | -18.00 | 2773 | 3632 | 4615 | |
| | -18.50 | 3305 | 4395 | 5511 | |
| | -19.00 | 3395 | 4498 | 5628 | |
| | -19.50 | 3581 | 4745 | 5935 | |
| | -20.00 | 3715 | 4907 | 6147 | |
| | -20.50 | 3918 | 5184 | 6474 | |
| | -21.00 | 4050 | 5347 | 6380 | |
| | -21.50 | 4194 | 5279 | 6563 | |
| | -22.00 | 4137 | 5436 | 6512 | |
| | -22.50 | 4265 | 5385 | 6686 | |
| | -23.00 | 4215 | 5519 | 6762 | |
| | -23.50 | 4295 | 5589 | 6902 | |
| | -24.00 | 4306 | 5667 | 6974 | |
| | -24.50 | 4381 | 5786 | 6894 | |
| | -25.00 | 4372 | 5707 | 6650 | |
| | -25.50 | 4494 | 5501 | | |
| | -26.00 | 4291 | | | |
| | -26.50 | 4402 | | | |

ALGEMENE GEGEVENS

Project : ZW0380 Funderingen
 Onderdeel : RLL-TBG380
 Datum : 27-03-2021
 Bestand : P:\EANL_Projects\10124719 - TenneT Engineering
 ZW380 kV Oost\2 Content\007 DO
 vakwerkmasten\TS Paalfunderingen\ZW0380
 steunmast DO.pvw
 Berekeningstype : Verticaal belaste paal
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Toegepaste normen volgens Eurocode met Nederlandse NB

Geotechniek EN 1997-1:2004 AC:2009
 NEN-EN 1997-1:2005 C1+A1:2013 NB:2016
 NEN 9997-1:2016 C2:2017

REKENGEDEVENS SI Ø508/670 trek

Berekening : Ontwerpend
 Rekenmethode : Trekpalen volgens NEN-EN 1997-1, art. 7.6.3
 Sondering(en) : 19-1008_1, 19-1008_6, 166.S01, 19-1008_11, 19-1008_12
 : 19-1008_17, 19-1008_20, 19-1008_21, 251.S01, 19-1008_29
 : 283.S02, 19-1008_35, 312.S03, 19-1008_43, 328.S02
 Let op: trekcapaciteit t.p.v. negatief kleefttraject is meegerkend.

Stijf bouwwerk : NEE
 Paalgroep : NEE
 Aantal sonderingen : 15
 Factor $\xi_{3(n=1)}$: 1.39 (handmatig)
 Factor $\xi_{3(gem)}$: 1.39 (handmatig)
 Factor $\xi_{4(min)}$: 1.39 (handmatig)
 Weerstandsfactor γ_R : 1.35
 $\gamma_{m,variabe}$: 1.50
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø508/670
 Niveau paalkop [m] : N.A.P. 0.00
 Bovenbel. [kN/m²] : 0.00

PAALPUNTNIVEAUS SI Ø508/670

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|-----------------|----------------|-----------------|
| 1 | -6.00 | -30.00 | 0.50 |

RESULTATEN SI Ø508/670 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering | 19-1008_1 | 19-1008_6 | 166.S01 | 19-1008_11 | 19-1008_12 | 19-1008_17 |
|------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| Niveau [m] | $F_{nettozt}$ [kN] | $F_{nettozt}$ [kN] | $F_{nettozt}$ [kN] | $F_{nettozt}$ [kN] | $F_{nettozt}$ [kN] | $F_{nettozt}$ [kN] |
| -6.00 | 46 | 393 | 231 | 159 | 419 | 68 |
| -6.50 | 50 | 439 | 278 | 164 | 456 | 74 |
| -7.00 | 53 | 485 | 324 | 169 | 501 | 99 |
| -7.50 | 56 | 531 | 370 | 183 | 547 | 111 |
| -8.00 | 68 | 577 | 416 | 202 | 593 | 116 |
| -8.50 | 81 | 623 | 461 | 220 | 617 | 123 |
| -9.00 | 86 | 669 | 507 | 234 | 625 | 134 |
| -9.50 | 106 | 715 | 552 | 248 | 631 | 142 |
| -10.00 | 124 | 761 | 598 | 262 | 643 | 177 |
| -10.50 | 144 | 807 | 644 | 279 | 664 | 195 |
| -11.00 | 159 | 854 | 690 | 298 | 681 | 224 |
| -11.50 | 183 | 900 | 736 | 320 | 685 | 270 |
| -12.00 | 214 | 946 | 779 | 348 | 701 | 317 |
| -12.50 | 235 | 992 | 816 | 360 | 708 | 363 |
| -13.00 | 268 | 1038 | 850 | 393 | 713 | 409 |
| -13.50 | 300 | 1084 | 884 | 431 | 720 | 455 |
| -14.00 | 329 | 1130 | 924 | 470 | 734 | 501 |
| -14.50 | 366 | 1176 | 970 | 510 | 751 | 547 |
| -15.00 | 400 | 1222 | 1016 | 549 | 764 | 590 |
| -15.50 | 437 | 1268 | 1062 | 586 | 774 | 636 |
| -16.00 | 469 | 1314 | 1108 | 618 | 791 | 682 |
| -16.50 | 504 | 1360 | 1154 | 655 | 812 | 728 |
| -17.00 | 539 | 1406 | 1200 | 690 | 830 | 772 |
| -17.50 | 580 | 1452 | 1246 | 724 | 856 | 820 |
| -18.00 | 626 | 1498 | 1292 | 766 | 877 | 875 |
| -18.50 | 672 | 1542 | 1338 | 812 | 922 | 912 |
| -19.00 | 719 | 1588 | 1384 | 858 | 964 | 945 |
| -19.50 | 765 | 1634 | 1430 | 904 | 1002 | 982 |
| -20.00 | 823 | 1680 | 1476 | 950 | 1035 | 1019 |
| -20.50 | 881 | 1726 | 1522 | 996 | 1072 | 1059 |
| -21.00 | 942 | 1772 | 1569 | 1042 | 1107 | 1100 |
| -21.50 | 986 | 1818 | 1615 | 1086 | 1149 | 1146 |
| -22.00 | 1032 | 1864 | 1661 | 1132 | 1195 | 1186 |
| -22.50 | 1078 | 1910 | 1707 | 1178 | 1240 | 1232 |
| -23.00 | 1124 | 1956 | 0 | 1220 | 1282 | 1278 |
| -23.50 | 1170 | 2002 | 0 | 1249 | 1322 | 1324 |
| -24.00 | 1216 | 0 | 0 | 1285 | 1365 | 1367 |
| -24.50 | 1262 | 0 | 0 | 1326 | 1411 | 1404 |
| -25.00 | 1308 | 0 | 0 | 1365 | 1457 | 1433 |
| -25.50 | 1354 | 0 | 0 | 1398 | 1517 | 1462 |
| -26.00 | 1400 | 0 | 0 | 1444 | 1578 | 1490 |
| -26.50 | 1446 | 0 | 0 | 1490 | 1614 | 1517 |
| -27.00 | 1492 | 0 | 0 | 1536 | 1647 | 1550 |
| -27.50 | 1538 | 0 | 0 | 1582 | 1685 | 1585 |
| -28.00 | 1584 | 0 | 0 | 1628 | 1713 | 1620 |
| -28.50 | 1630 | 0 | 0 | 1675 | 1748 | 1658 |
| -29.00 | 1676 | 0 | 0 | 1721 | 1794 | 1697 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

| | | | | | | |
|--------|------|---|---|------|------|------|
| -29.50 | 1723 | 0 | 0 | 1767 | 1840 | 1709 |
| -30.00 | 1769 | 0 | 0 | 1813 | 1886 | 1739 |

RESULTATEN SI Ø508/670 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | F _{nettozt} [kN] | F _{nettozt} [kN] | F _{nettozt} [kN] | F _{nettozt} [kN] | 283.S02 F _{nettozt} [kN] | 19-1008_35 F _{nettozt} [kN] |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|---|--|
| -6.00 | 86 | 154 | 185 | 278 | 225 | 245 |
| -6.50 | 102 | 184 | 217 | 311 | 252 | 266 |
| -7.00 | 131 | 214 | 254 | 349 | 285 | 283 |
| -7.50 | 157 | 250 | 290 | 388 | 311 | 301 |
| -8.00 | 177 | 284 | 323 | 431 | 336 | 325 |
| -8.50 | 196 | 319 | 346 | 473 | 367 | 349 |
| -9.00 | 223 | 338 | 351 | 509 | 396 | 368 |
| -9.50 | 244 | 352 | 372 | 544 | 420 | 386 |
| -10.00 | 269 | 373 | 404 | 576 | 447 | 409 |
| -10.50 | 277 | 392 | 440 | 613 | 474 | 430 |
| -11.00 | 309 | 413 | 469 | 650 | 500 | 465 |
| -11.50 | 343 | 440 | 486 | 691 | 527 | 496 |
| -12.00 | 351 | 469 | 504 | 712 | 545 | 517 |
| -12.50 | 360 | 492 | 533 | 755 | 576 | 536 |
| -13.00 | 375 | 519 | 567 | 788 | 610 | 560 |
| -13.50 | 383 | 548 | 599 | 802 | 647 | 589 |
| -14.00 | 397 | 590 | 643 | 819 | 691 | 618 |
| -14.50 | 422 | 633 | 687 | 831 | 735 | 655 |
| -15.00 | 450 | 664 | 734 | 842 | 775 | 691 |
| -15.50 | 466 | 689 | 756 | 855 | 809 | 727 |
| -16.00 | 479 | 734 | 798 | 885 | 846 | 765 |
| -16.50 | 496 | 779 | 844 | 897 | 887 | 803 |
| -17.00 | 508 | 787 | 890 | 909 | 931 | 835 |
| -17.50 | 522 | 797 | 934 | 925 | 978 | 863 |
| -18.00 | 547 | 815 | 975 | 964 | 1024 | 900 |
| -18.50 | 575 | 863 | 1021 | 1010 | 1070 | 933 |
| -19.00 | 597 | 897 | 1049 | 1056 | 1116 | 970 |
| -19.50 | 627 | 907 | 1079 | 1091 | 1162 | 1007 |
| -20.00 | 657 | 915 | 1116 | 1137 | 1208 | 1045 |
| -20.50 | 695 | 923 | 1166 | 1183 | 1252 | 1091 |
| -21.00 | 745 | 931 | 1218 | 1229 | 1298 | 1137 |
| -21.50 | 768 | 941 | 1241 | 1275 | 1344 | 1183 |
| -22.00 | 783 | 952 | 1249 | 1321 | 1390 | 1228 |
| -22.50 | 800 | 964 | 1259 | 1374 | 1436 | 1274 |
| -23.00 | 813 | 977 | 1275 | 1415 | 1482 | 1320 |
| -23.50 | 838 | 989 | 1295 | 1443 | 1528 | 1366 |
| -24.00 | 866 | 1003 | 1321 | 1475 | 1574 | 1412 |
| -24.50 | 895 | 1018 | 1346 | 1509 | 1620 | 1457 |
| -25.00 | 931 | 1033 | 1368 | 1544 | 1667 | 1501 |
| -25.50 | 963 | 1049 | 1406 | 1566 | 1713 | 1550 |
| -26.00 | 995 | 1064 | 1462 | 1592 | 1759 | 1597 |
| -26.50 | 1023 | 1078 | 1516 | 1616 | 1808 | 1637 |
| -27.00 | 1058 | 1093 | 1562 | 1645 | 1826 | 1683 |
| -27.50 | 1089 | 1107 | 1608 | 1668 | 1843 | 1729 |
| -28.00 | 1117 | 1122 | 1654 | 1690 | 1864 | 1776 |
| -28.50 | 1149 | 1137 | 1700 | 1713 | 1890 | 1822 |
| -29.00 | 1180 | 1152 | 1747 | 1737 | 1909 | 1868 |
| -29.50 | 1204 | 1168 | 1778 | 1774 | 1926 | 1914 |
| -30.00 | 1235 | 1185 | 1816 | 1807 | 1942 | 1960 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø508/670 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Sondering 312.S03 19-1008_43 328.S02

| Niveau [m] | F _{netto:st} [kN] | F _{netto:st} [kN] | F _{netto:st} [kN] |
|---------------|-------------------------------|-------------------------------|-------------------------------|
| -6.00 | 291 | 225 | 371 |
| -6.50 | 326 | 244 | 408 |
| -7.00 | 368 | 280 | 434 |
| -7.50 | 393 | 315 | 467 |
| -8.00 | 421 | 351 | 503 |
| -8.50 | 467 | 385 | 539 |
| -9.00 | 513 | 420 | 575 |
| -9.50 | 559 | 455 | 606 |
| -10.00 | 605 | 487 | 641 |
| -10.50 | 651 | 526 | 677 |
| -11.00 | 695 | 572 | 718 |
| -11.50 | 741 | 618 | 761 |
| -12.00 | 787 | 664 | 802 |
| -12.50 | 833 | 710 | 839 |
| -13.00 | 878 | 745 | 876 |
| -13.50 | 911 | 774 | 913 |
| -14.00 | 948 | 809 | 950 |
| -14.50 | 985 | 846 | 986 |
| -15.00 | 1021 | 879 | 1024 |
| -15.50 | 1059 | 919 | 1061 |
| -16.00 | 1095 | 964 | 1097 |
| -16.50 | 1132 | 1010 | 1136 |
| -17.00 | 1167 | 1056 | 1182 |
| -17.50 | 1194 | 1100 | 1228 |
| -18.00 | 1223 | 1141 | 1281 |
| -18.50 | 1259 | 1177 | 1314 |
| -19.00 | 1298 | 1213 | 1356 |
| -19.50 | 1337 | 1243 | 1400 |
| -20.00 | 1375 | 1274 | 1446 |
| -20.50 | 1409 | 1312 | 1492 |
| -21.00 | 1445 | 1356 | 1538 |
| -21.50 | 1480 | 1393 | 1584 |
| -22.00 | 1518 | 1434 | 1630 |
| -22.50 | 1563 | 1480 | 1676 |
| -23.00 | 1609 | 1526 | 1722 |
| -23.50 | 1653 | 1573 | 1769 |
| -24.00 | 1693 | 1619 | 1815 |
| -24.50 | 1739 | 1665 | 1854 |
| -25.00 | 1785 | 1704 | 1891 |
| -25.50 | 1829 | 0 | 1928 |
| -26.00 | 1868 | 0 | 1965 |
| -26.50 | 1913 | 0 | 2004 |
| -27.00 | 1958 | 0 | 2050 |
| -27.50 | 1983 | 0 | 2096 |
| -28.00 | 2003 | 0 | 2135 |
| -28.50 | 2019 | 0 | 2170 |
| -29.00 | 2035 | 0 | 0 |
| -29.50 | 2052 | 0 | 0 |
| -30.00 | 2076 | 0 | 0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

SAMENVATTINGSTABEL SI Ø508/670 trek (n=1)
Uitgangspunten

- paal : SI Ø508/670
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie
 - schachtafmeting : 590 mm
 Paalklassefactor α_p : 0.63
 Factor α_s (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
 Correlatiefactor $\xi_{s(n=1)}$: 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt | | Bewijkdraagvermogen | | |
|-----------|-------------------|--------|----------------------|-------------------|-------------------------|
| | niveau | niveau | $R_{t,calc}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_1 | 2.12 | -6.00 | 46.3 | 46.3 | 46.3 |
| | | -6.50 | 49.6 | 49.6 | 49.6 |
| | | -7.00 | 52.9 | 52.9 | 52.9 |
| | | -7.50 | 56.4 | 56.4 | 56.4 |
| | | -8.00 | 67.8 | 67.8 | 67.8 |
| | | -8.50 | 80.6 | 80.6 | 80.6 |
| | | -9.00 | 85.5 | 85.5 | 85.5 |
| | | -9.50 | 105.6 | 105.6 | 105.6 |
| | | -10.00 | 123.5 | 123.5 | 123.5 |
| | | -10.50 | 144.3 | 144.3 | 144.3 |
| | | -11.00 | 159.0 | 159.0 | 159.0 |
| | | -11.50 | 183.2 | 183.2 | 183.2 |
| | | -12.00 | 213.9 | 213.9 | 213.9 |
| | | -12.50 | 234.9 | 234.9 | 234.9 |
| | | -13.00 | 267.7 | 267.7 | 267.7 |
| | | -13.50 | 300.5 | 300.5 | 300.5 |
| | | -14.00 | 328.9 | 328.9 | 328.9 |
| | | -14.50 | 365.9 | 365.9 | 365.9 |
| | | -15.00 | 400.0 | 400.0 | 400.0 |
| | | -15.50 | 436.9 | 436.9 | 436.9 |
| | | -16.00 | 468.7 | 468.7 | 468.7 |
| | | -16.50 | 503.7 | 503.7 | 503.7 |
| | | -17.00 | 539.1 | 539.1 | 539.1 |
| | | -17.50 | 580.4 | 580.4 | 580.4 |
| | | -18.00 | 626.4 | 626.4 | 626.4 |
| | | -18.50 | 672.5 | 672.5 | 672.5 |
| | | -19.00 | 718.5 | 718.5 | 718.5 |
| | | -19.50 | 764.6 | 764.6 | 764.6 |
| | | -20.00 | 822.5 | 822.5 | 822.5 |
| | | -20.50 | 881.2 | 881.2 | 881.2 |
| -21.00 | 942.1 | 942.1 | 942.1 | | |
| -21.50 | 985.5 | 985.5 | 985.5 | | |
| -22.00 | 1031.6 | 1031.6 | 1031.6 | | |
| -22.50 | 1077.7 | 1077.7 | 1077.7 | | |
| -23.00 | 1123.7 | 1123.7 | 1123.7 | | |
| -23.50 | 1169.8 | 1169.8 | 1169.8 | | |
| -24.00 | 1215.8 | 1215.8 | 1215.8 | | |
| -24.50 | 1261.9 | 1261.9 | 1261.9 | | |
| -25.00 | 1308.0 | 1308.0 | 1308.0 | | |
| -25.50 | 1354.0 | 1354.0 | 1354.0 | | |
| -26.00 | 1400.1 | 1400.1 | 1400.1 | | |
| -26.50 | 1446.2 | 1446.2 | 1446.2 | | |
| -27.00 | 1492.2 | 1492.2 | 1492.2 | | |
| -27.50 | 1538.3 | 1538.3 | 1538.3 | | |
| -28.00 | 1584.4 | 1584.4 | 1584.4 | | |
| -28.50 | 1630.4 | 1630.4 | 1630.4 | | |
| -29.00 | 1676.5 | 1676.5 | 1676.5 | | |
| -29.50 | 1722.6 | 1722.6 | 1722.6 | | |
| -30.00 | 1768.6 | 1768.6 | 1768.6 | | |
| 19-1008_6 | 11.00 | -6.00 | 392.7 | 392.7 | 392.7 |
| | | -6.50 | 439.0 | 439.0 | 439.0 |
| | | -7.00 | 485.0 | 485.0 | 485.0 |
| | | -7.50 | 531.1 | 531.1 | 531.1 |
| | | -8.00 | 577.1 | 577.1 | 577.1 |
| | | -8.50 | 623.2 | 623.2 | 623.2 |
| | | -9.00 | 669.3 | 669.3 | 669.3 |
| | | -9.50 | 715.3 | 715.3 | 715.3 |
| | | -10.00 | 761.4 | 761.4 | 761.4 |
| | | -10.50 | 807.5 | 807.5 | 807.5 |
| | | -11.00 | 853.5 | 853.5 | 853.5 |
| | | -11.50 | 899.6 | 899.6 | 899.6 |
| | | -12.00 | 945.7 | 945.7 | 945.7 |
| | | -12.50 | 991.7 | 991.7 | 991.7 |
| | | -13.00 | 1037.8 | 1037.8 | 1037.8 |
| | | -13.50 | 1083.9 | 1083.9 | 1083.9 |
| | | -14.00 | 1129.9 | 1129.9 | 1129.9 |
| | | -14.50 | 1176.0 | 1176.0 | 1176.0 |
| | | -15.00 | 1222.1 | 1222.1 | 1222.1 |
| | | -15.50 | 1268.1 | 1268.1 | 1268.1 |
| | | -16.00 | 1314.2 | 1314.2 | 1314.2 |
| | | -16.50 | 1360.3 | 1360.3 | 1360.3 |
| | | -17.00 | 1406.3 | 1406.3 | 1406.3 |
| -17.50 | 1452.4 | 1452.4 | 1452.4 | | |
| -18.00 | 1498.4 | 1498.4 | 1498.4 | | |
| -18.50 | 1541.6 | 1541.6 | 1541.6 | | |
| -19.00 | 1587.6 | 1587.6 | 1587.6 | | |
| -19.50 | 1633.7 | 1633.7 | 1633.7 | | |
| -20.00 | 1679.8 | 1679.8 | 1679.8 | | |
| -20.50 | 1725.8 | 1725.8 | 1725.8 | | |
| -21.00 | 1771.9 | 1771.9 | 1771.9 | | |
| -21.50 | 1818.0 | 1818.0 | 1818.0 | | |
| -22.00 | 1864.0 | 1864.0 | 1864.0 | | |
| -22.50 | 1910.1 | 1910.1 | 1910.1 | | |
| -23.00 | 1956.1 | 1956.1 | 1956.1 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt | | Bezuikdraagvermogen | Rekenwaarden | | |
|------------|-------------------|--------|---------------------|---------------------|-------------------|-------------------------|
| | niveau | niveau | | $R_{t,ca1}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_6 | 11.00 | -23.50 | 2002.2 | 2002.2 | 2002.2 | |
| 166.S01 | 3.45 | -6.00 | 231.5 | 231.5 | 231.5 | |
| | | -6.50 | 277.5 | 277.5 | 277.5 | |
| | | -7.00 | 323.6 | 323.6 | 323.6 | |
| | | -7.50 | 369.7 | 369.7 | 369.7 | |
| | | -8.00 | 415.7 | 415.7 | 415.7 | |
| | | -8.50 | 461.5 | 461.5 | 461.5 | |
| | | -9.00 | 507.2 | 507.2 | 507.2 | |
| | | -9.50 | 552.2 | 552.2 | 552.2 | |
| | | -10.00 | 598.3 | 598.3 | 598.3 | |
| | | -10.50 | 644.3 | 644.3 | 644.3 | |
| | | -11.00 | 690.4 | 690.4 | 690.4 | |
| | | -11.50 | 736.5 | 736.5 | 736.5 | |
| | | -12.00 | 779.3 | 779.3 | 779.3 | |
| | | -12.50 | 815.5 | 815.5 | 815.5 | |
| | | -13.00 | 849.6 | 849.6 | 849.6 | |
| | | -13.50 | 884.1 | 884.1 | 884.1 | |
| | | -14.00 | 923.8 | 923.8 | 923.8 | |
| | | -14.50 | 969.7 | 969.7 | 969.7 | |
| | | -15.00 | 1015.7 | 1015.7 | 1015.7 | |
| | | -15.50 | 1061.8 | 1061.8 | 1061.8 | |
| | | -16.00 | 1107.9 | 1107.9 | 1107.9 | |
| -16.50 | 1153.9 | 1153.9 | 1153.9 | | | |
| -17.00 | 1200.0 | 1200.0 | 1200.0 | | | |
| -17.50 | 1246.1 | 1246.1 | 1246.1 | | | |
| -18.00 | 1292.1 | 1292.1 | 1292.1 | | | |
| -18.50 | 1338.2 | 1338.2 | 1338.2 | | | |
| -19.00 | 1384.3 | 1384.3 | 1384.3 | | | |
| -19.50 | 1430.3 | 1430.3 | 1430.3 | | | |
| -20.00 | 1476.4 | 1476.4 | 1476.4 | | | |
| -20.50 | 1522.5 | 1522.5 | 1522.5 | | | |
| -21.00 | 1568.5 | 1568.5 | 1568.5 | | | |
| -21.50 | 1614.6 | 1614.6 | 1614.6 | | | |
| -22.00 | 1660.7 | 1660.7 | 1660.7 | | | |
| -22.50 | 1706.7 | 1706.7 | 1706.7 | | | |
| 19-1008_11 | 0.62 | -6.00 | 159.1 | 159.1 | 159.1 | |
| | | -6.50 | 163.7 | 163.7 | 163.7 | |
| | | -7.00 | 169.1 | 169.1 | 169.1 | |
| | | -7.50 | 182.8 | 182.8 | 182.8 | |
| | | -8.00 | 202.3 | 202.3 | 202.3 | |
| | | -8.50 | 220.1 | 220.1 | 220.1 | |
| | | -9.00 | 234.3 | 234.3 | 234.3 | |
| | | -9.50 | 247.9 | 247.9 | 247.9 | |
| | | -10.00 | 262.0 | 262.0 | 262.0 | |
| | | -10.50 | 278.5 | 278.5 | 278.5 | |
| | | -11.00 | 297.6 | 297.6 | 297.6 | |
| | | -11.50 | 320.1 | 320.1 | 320.1 | |
| | | -12.00 | 348.2 | 348.2 | 348.2 | |
| | | -12.50 | 359.6 | 359.6 | 359.6 | |
| | | -13.00 | 392.6 | 392.6 | 392.6 | |
| | | -13.50 | 431.0 | 431.0 | 431.0 | |
| | | -14.00 | 470.0 | 470.0 | 470.0 | |
| | | -14.50 | 509.5 | 509.5 | 509.5 | |
| | | -15.00 | 549.0 | 549.0 | 549.0 | |
| | | -15.50 | 586.2 | 586.2 | 586.2 | |
| | | -16.00 | 617.7 | 617.7 | 617.7 | |
| | | -16.50 | 654.6 | 654.6 | 654.6 | |
| | | -17.00 | 690.2 | 690.2 | 690.2 | |
| | | -17.50 | 723.9 | 723.9 | 723.9 | |
| | | -18.00 | 765.9 | 765.9 | 765.9 | |
| | | -18.50 | 812.0 | 812.0 | 812.0 | |
| | | -19.00 | 858.1 | 858.1 | 858.1 | |
| | | -19.50 | 904.1 | 904.1 | 904.1 | |
| | | -20.00 | 950.2 | 950.2 | 950.2 | |
| | | -20.50 | 996.3 | 996.3 | 996.3 | |
| | | -21.00 | 1042.3 | 1042.3 | 1042.3 | |
| -21.50 | 1085.9 | 1085.9 | 1085.9 | | | |
| -22.00 | 1132.0 | 1132.0 | 1132.0 | | | |
| -22.50 | 1178.0 | 1178.0 | 1178.0 | | | |
| -23.00 | 1220.2 | 1220.2 | 1220.2 | | | |
| -23.50 | 1248.6 | 1248.6 | 1248.6 | | | |
| -24.00 | 1284.8 | 1284.8 | 1284.8 | | | |
| -24.50 | 1325.5 | 1325.5 | 1325.5 | | | |
| -25.00 | 1364.5 | 1364.5 | 1364.5 | | | |
| -25.50 | 1397.5 | 1397.5 | 1397.5 | | | |
| -26.00 | 1444.2 | 1444.2 | 1444.2 | | | |
| -26.50 | 1490.3 | 1490.3 | 1490.3 | | | |
| -27.00 | 1536.3 | 1536.3 | 1536.3 | | | |
| -27.50 | 1582.4 | 1582.4 | 1582.4 | | | |
| -28.00 | 1628.4 | 1628.4 | 1628.4 | | | |
| -28.50 | 1674.5 | 1674.5 | 1674.5 | | | |
| -29.00 | 1720.6 | 1720.6 | 1720.6 | | | |
| -29.50 | 1766.6 | 1766.6 | 1766.6 | | | |
| -30.00 | 1812.7 | 1812.7 | 1812.7 | | | |
| 19-1008_12 | 3.57 | -6.00 | 419.1 | 419.1 | 419.1 | |
| | | -6.50 | 455.7 | 455.7 | 455.7 | |
| | | -7.00 | 500.7 | 500.7 | 500.7 | |
| | | -7.50 | 546.8 | 546.8 | 546.8 | |
| | | -8.00 | 592.5 | 592.5 | 592.5 | |
| | | -8.50 | 616.8 | 616.8 | 616.8 | |
| | | -9.00 | 625.0 | 625.0 | 625.0 | |
| | | -9.50 | 631.5 | 631.5 | 631.5 | |
| | | -10.00 | 642.7 | 642.7 | 642.7 | |
| | | -10.50 | 663.9 | 663.9 | 663.9 | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maai- veld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|-------------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_12 | 3.57 | -11.00 | 680.6 | 680.6 | 680.6 |
| | | -11.50 | 685.2 | 685.2 | 685.2 |
| | | -12.00 | 700.9 | 700.9 | 700.9 |
| | | -12.50 | 707.6 | 707.6 | 707.6 |
| | | -13.00 | 713.3 | 713.3 | 713.3 |
| | | -13.50 | 719.8 | 719.8 | 719.8 |
| | | -14.00 | 733.7 | 733.7 | 733.7 |
| | | -14.50 | 751.3 | 751.3 | 751.3 |
| | | -15.00 | 764.0 | 764.0 | 764.0 |
| | | -15.50 | 774.5 | 774.5 | 774.5 |
| | | -16.00 | 790.6 | 790.6 | 790.6 |
| | | -16.50 | 811.9 | 811.9 | 811.9 |
| | | -17.00 | 829.9 | 829.9 | 829.9 |
| | | -17.50 | 856.0 | 856.0 | 856.0 |
| | | -18.00 | 876.5 | 876.5 | 876.5 |
| | | -18.50 | 921.9 | 921.9 | 921.9 |
| | | -19.00 | 963.6 | 963.6 | 963.6 |
| | | -19.50 | 1001.9 | 1001.9 | 1001.9 |
| | | -20.00 | 1035.1 | 1035.1 | 1035.1 |
| | | -20.50 | 1072.3 | 1072.3 | 1072.3 |
| | | -21.00 | 1107.2 | 1107.2 | 1107.2 |
| | | -21.50 | 1149.3 | 1149.3 | 1149.3 |
| | | -22.00 | 1194.7 | 1194.7 | 1194.7 |
| | | -22.50 | 1240.1 | 1240.1 | 1240.1 |
| | | -23.00 | 1281.9 | 1281.9 | 1281.9 |
| | | -23.50 | 1322.1 | 1322.1 | 1322.1 |
| | | -24.00 | 1364.9 | 1364.9 | 1364.9 |
| | | -24.50 | 1411.0 | 1411.0 | 1411.0 |
| | | -25.00 | 1457.1 | 1457.1 | 1457.1 |
| | | -25.50 | 1517.3 | 1517.3 | 1517.3 |
| -26.00 | 1578.0 | 1578.0 | 1578.0 | | |
| -26.50 | 1613.6 | 1613.6 | 1613.6 | | |
| -27.00 | 1646.9 | 1646.9 | 1646.9 | | |
| -27.50 | 1684.9 | 1684.9 | 1684.9 | | |
| -28.00 | 1712.9 | 1712.9 | 1712.9 | | |
| -28.50 | 1748.3 | 1748.3 | 1748.3 | | |
| -29.00 | 1794.4 | 1794.4 | 1794.4 | | |
| -29.50 | 1840.5 | 1840.5 | 1840.5 | | |
| -30.00 | 1885.7 | 1885.7 | 1885.7 | | |
| 19-1008_17 | 0.20 | -6.00 | 68.1 | 68.1 | 68.1 |
| | | -6.50 | 73.8 | 73.8 | 73.8 |
| | | -7.00 | 99.0 | 99.0 | 99.0 |
| | | -7.50 | 110.8 | 110.8 | 110.8 |
| | | -8.00 | 116.4 | 116.4 | 116.4 |
| | | -8.50 | 122.9 | 122.9 | 122.9 |
| | | -9.00 | 133.9 | 133.9 | 133.9 |
| | | -9.50 | 142.5 | 142.5 | 142.5 |
| | | -10.00 | 176.9 | 176.9 | 176.9 |
| | | -10.50 | 194.7 | 194.7 | 194.7 |
| | | -11.00 | 224.4 | 224.4 | 224.4 |
| | | -11.50 | 270.5 | 270.5 | 270.5 |
| | | -12.00 | 316.5 | 316.5 | 316.5 |
| | | -12.50 | 362.6 | 362.6 | 362.6 |
| | | -13.00 | 408.7 | 408.7 | 408.7 |
| | | -13.50 | 454.7 | 454.7 | 454.7 |
| | | -14.00 | 500.8 | 500.8 | 500.8 |
| | | -14.50 | 546.8 | 546.8 | 546.8 |
| | | -15.00 | 589.6 | 589.6 | 589.6 |
| | | -15.50 | 635.7 | 635.7 | 635.7 |
| | | -16.00 | 681.7 | 681.7 | 681.7 |
| | | -16.50 | 727.8 | 727.8 | 727.8 |
| | | -17.00 | 772.1 | 772.1 | 772.1 |
| | | -17.50 | 819.7 | 819.7 | 819.7 |
| | | -18.00 | 874.7 | 874.7 | 874.7 |
| | | -18.50 | 912.1 | 912.1 | 912.1 |
| | | -19.00 | 944.6 | 944.6 | 944.6 |
| | | -19.50 | 981.8 | 981.8 | 981.8 |
| | | -20.00 | 1019.4 | 1019.4 | 1019.4 |
| | | -20.50 | 1059.1 | 1059.1 | 1059.1 |
| -21.00 | 1100.0 | 1100.0 | 1100.0 | | |
| -21.50 | 1146.2 | 1146.2 | 1146.2 | | |
| -22.00 | 1185.9 | 1185.9 | 1185.9 | | |
| -22.50 | 1231.9 | 1231.9 | 1231.9 | | |
| -23.00 | 1278.0 | 1278.0 | 1278.0 | | |
| -23.50 | 1324.0 | 1324.0 | 1324.0 | | |
| -24.00 | 1366.9 | 1366.9 | 1366.9 | | |
| -24.50 | 1404.0 | 1404.0 | 1404.0 | | |
| -25.00 | 1433.3 | 1433.3 | 1433.3 | | |
| -25.50 | 1461.8 | 1461.8 | 1461.8 | | |
| -26.00 | 1489.6 | 1489.6 | 1489.6 | | |
| -26.50 | 1517.3 | 1517.3 | 1517.3 | | |
| -27.00 | 1549.9 | 1549.9 | 1549.9 | | |
| -27.50 | 1584.8 | 1584.8 | 1584.8 | | |
| -28.00 | 1620.4 | 1620.4 | 1620.4 | | |
| -28.50 | 1657.6 | 1657.6 | 1657.6 | | |
| -29.00 | 1696.6 | 1696.6 | 1696.6 | | |
| -29.50 | 1708.7 | 1708.7 | 1708.7 | | |
| -30.00 | 1738.7 | 1738.7 | 1738.7 | | |
| 19-1008_20 | -0.03 | -6.00 | 86.3 | 86.3 | 86.3 |
| | | -6.50 | 102.3 | 102.3 | 102.3 |
| | | -7.00 | 131.3 | 131.3 | 131.3 |
| | | -7.50 | 156.7 | 156.7 | 156.7 |
| | | -8.00 | 176.7 | 176.7 | 176.7 |
| | | -8.50 | 196.3 | 196.3 | 196.3 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt | | Bezwijkdraagvermogen | | |
|------------|-------------------|--------|----------------------|-------------------|-------------------------|
| | niveau | niveau | $R_{t,ca1}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_20 | -0.03 | -9.00 | 222.8 | 222.8 | 222.8 |
| | | -9.50 | 244.5 | 244.5 | 244.5 |
| | | -10.00 | 269.4 | 269.4 | 269.4 |
| | | -10.50 | 276.5 | 276.5 | 276.5 |
| | | -11.00 | 308.5 | 308.5 | 308.5 |
| | | -11.50 | 342.8 | 342.8 | 342.8 |
| | | -12.00 | 350.7 | 350.7 | 350.7 |
| | | -12.50 | 359.6 | 359.6 | 359.6 |
| | | -13.00 | 375.3 | 375.3 | 375.3 |
| | | -13.50 | 383.2 | 383.2 | 383.2 |
| | | -14.00 | 397.2 | 397.2 | 397.2 |
| | | -14.50 | 421.7 | 421.7 | 421.7 |
| | | -15.00 | 449.6 | 449.6 | 449.6 |
| | | -15.50 | 465.9 | 465.9 | 465.9 |
| | | -16.00 | 478.6 | 478.6 | 478.6 |
| | | -16.50 | 495.8 | 495.8 | 495.8 |
| | | -17.00 | 507.6 | 507.6 | 507.6 |
| | | -17.50 | 521.6 | 521.6 | 521.6 |
| | | -18.00 | 546.6 | 546.6 | 546.6 |
| | | -18.50 | 575.5 | 575.5 | 575.5 |
| | | -19.00 | 597.5 | 597.5 | 597.5 |
| | | -19.50 | 626.6 | 626.6 | 626.6 |
| | | -20.00 | 656.7 | 656.7 | 656.7 |
| | | -20.50 | 694.8 | 694.8 | 694.8 |
| | | -21.00 | 745.4 | 745.4 | 745.4 |
| | | -21.50 | 767.7 | 767.7 | 767.7 |
| | | -22.00 | 783.0 | 783.0 | 783.0 |
| | | -22.50 | 799.5 | 799.5 | 799.5 |
| | | -23.00 | 813.1 | 813.1 | 813.1 |
| | | -23.50 | 838.2 | 838.2 | 838.2 |
| -24.00 | 866.0 | 866.0 | 866.0 | | |
| -24.50 | 895.1 | 895.1 | 895.1 | | |
| -25.00 | 930.6 | 930.6 | 930.6 | | |
| -25.50 | 963.0 | 963.0 | 963.0 | | |
| -26.00 | 994.7 | 994.7 | 994.7 | | |
| -26.50 | 1023.4 | 1023.4 | 1023.4 | | |
| -27.00 | 1058.3 | 1058.3 | 1058.3 | | |
| -27.50 | 1089.0 | 1089.0 | 1089.0 | | |
| -28.00 | 1117.0 | 1117.0 | 1117.0 | | |
| -28.50 | 1149.4 | 1149.4 | 1149.4 | | |
| -29.00 | 1179.6 | 1179.6 | 1179.6 | | |
| -29.50 | 1204.3 | 1204.3 | 1204.3 | | |
| -30.00 | 1234.9 | 1234.9 | 1234.9 | | |
| 19-1008_21 | 1.78 | -6.00 | 153.6 | 153.6 | 153.6 |
| | | -6.50 | 183.6 | 183.6 | 183.6 |
| | | -7.00 | 213.5 | 213.5 | 213.5 |
| | | -7.50 | 250.0 | 250.0 | 250.0 |
| | | -8.00 | 284.3 | 284.3 | 284.3 |
| | | -8.50 | 319.0 | 319.0 | 319.0 |
| | | -9.00 | 337.7 | 337.7 | 337.7 |
| | | -9.50 | 352.1 | 352.1 | 352.1 |
| | | -10.00 | 373.3 | 373.3 | 373.3 |
| | | -10.50 | 392.0 | 392.0 | 392.0 |
| | | -11.00 | 413.3 | 413.3 | 413.3 |
| | | -11.50 | 439.8 | 439.8 | 439.8 |
| | | -12.00 | 469.3 | 469.3 | 469.3 |
| | | -12.50 | 492.3 | 492.3 | 492.3 |
| | | -13.00 | 518.7 | 518.7 | 518.7 |
| | | -13.50 | 547.7 | 547.7 | 547.7 |
| | | -14.00 | 590.1 | 590.1 | 590.1 |
| | | -14.50 | 632.6 | 632.6 | 632.6 |
| | | -15.00 | 664.1 | 664.1 | 664.1 |
| | | -15.50 | 689.1 | 689.1 | 689.1 |
| | | -16.00 | 733.7 | 733.7 | 733.7 |
| | | -16.50 | 778.5 | 778.5 | 778.5 |
| | | -17.00 | 787.3 | 787.3 | 787.3 |
| | | -17.50 | 797.2 | 797.2 | 797.2 |
| | | -18.00 | 814.8 | 814.8 | 814.8 |
| | | -18.50 | 863.5 | 863.5 | 863.5 |
| | | -19.00 | 897.3 | 897.3 | 897.3 |
| | | -19.50 | 907.1 | 907.1 | 907.1 |
| | | -20.00 | 915.2 | 915.2 | 915.2 |
| | | -20.50 | 923.3 | 923.3 | 923.3 |
| -21.00 | 931.4 | 931.4 | 931.4 | | |
| -21.50 | 940.9 | 940.9 | 940.9 | | |
| -22.00 | 951.6 | 951.6 | 951.6 | | |
| -22.50 | 964.3 | 964.3 | 964.3 | | |
| -23.00 | 976.9 | 976.9 | 976.9 | | |
| -23.50 | 989.1 | 989.1 | 989.1 | | |
| -24.00 | 1003.3 | 1003.3 | 1003.3 | | |
| -24.50 | 1017.9 | 1017.9 | 1017.9 | | |
| -25.00 | 1033.1 | 1033.1 | 1033.1 | | |
| -25.50 | 1049.0 | 1049.0 | 1049.0 | | |
| -26.00 | 1064.2 | 1064.2 | 1064.2 | | |
| -26.50 | 1078.2 | 1078.2 | 1078.2 | | |
| -27.00 | 1092.5 | 1092.5 | 1092.5 | | |
| -27.50 | 1106.6 | 1106.6 | 1106.6 | | |
| -28.00 | 1121.7 | 1121.7 | 1121.7 | | |
| -28.50 | 1137.2 | 1137.2 | 1137.2 | | |
| -29.00 | 1152.2 | 1152.2 | 1152.2 | | |
| -29.50 | 1168.0 | 1168.0 | 1168.0 | | |
| -30.00 | 1184.7 | 1184.7 | 1184.7 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt | | Bewijkdraagvermogen | | |
|------------|-------------------|--------|----------------------------|--------------------------|--------------------------------|
| | niveau | niveau | R _{t,ca1} [kN] | R _{t,d} [kN] | R _{t,netto,d} [kN] |
| 251.S01 | -1.05 | -6.00 | 184.5 | 184.5 | 184.5 |
| | | -6.50 | 216.7 | 216.7 | 216.7 |
| | | -7.00 | 253.9 | 253.9 | 253.9 |
| | | -7.50 | 290.0 | 290.0 | 290.0 |
| | | -8.00 | 323.2 | 323.2 | 323.2 |
| | | -8.50 | 346.1 | 346.1 | 346.1 |
| | | -9.00 | 350.9 | 350.9 | 350.9 |
| | | -9.50 | 372.2 | 372.2 | 372.2 |
| | | -10.00 | 403.6 | 403.6 | 403.6 |
| | | -10.50 | 440.3 | 440.3 | 440.3 |
| | | -11.00 | 468.6 | 468.6 | 468.6 |
| | | -11.50 | 486.4 | 486.4 | 486.4 |
| | | -12.00 | 504.0 | 504.0 | 504.0 |
| | | -12.50 | 533.0 | 533.0 | 533.0 |
| | | -13.00 | 566.9 | 566.9 | 566.9 |
| | | -13.50 | 599.0 | 599.0 | 599.0 |
| | | -14.00 | 642.9 | 642.9 | 642.9 |
| | | -14.50 | 686.6 | 686.6 | 686.6 |
| | | -15.00 | 733.7 | 733.7 | 733.7 |
| | | -15.50 | 755.7 | 755.7 | 755.7 |
| | | -16.00 | 798.4 | 798.4 | 798.4 |
| | | -16.50 | 844.5 | 844.5 | 844.5 |
| | | -17.00 | 890.1 | 890.1 | 890.1 |
| | | -17.50 | 933.7 | 933.7 | 933.7 |
| | | -18.00 | 975.0 | 975.0 | 975.0 |
| | | -18.50 | 1021.0 | 1021.0 | 1021.0 |
| | | -19.00 | 1049.3 | 1049.3 | 1049.3 |
| | | -19.50 | 1079.4 | 1079.4 | 1079.4 |
| | | -20.00 | 1115.6 | 1115.6 | 1115.6 |
| | | -20.50 | 1165.6 | 1165.6 | 1165.6 |
| -21.00 | 1218.1 | 1218.1 | 1218.1 | | |
| -21.50 | 1240.9 | 1240.9 | 1240.9 | | |
| -22.00 | 1249.1 | 1249.1 | 1249.1 | | |
| -22.50 | 1259.5 | 1259.5 | 1259.5 | | |
| -23.00 | 1275.1 | 1275.1 | 1275.1 | | |
| -23.50 | 1295.0 | 1295.0 | 1295.0 | | |
| -24.00 | 1321.5 | 1321.5 | 1321.5 | | |
| -24.50 | 1345.7 | 1345.7 | 1345.7 | | |
| -25.00 | 1367.8 | 1367.8 | 1367.8 | | |
| -25.50 | 1406.2 | 1406.2 | 1406.2 | | |
| -26.00 | 1461.8 | 1461.8 | 1461.8 | | |
| -26.50 | 1516.2 | 1516.2 | 1516.2 | | |
| -27.00 | 1562.3 | 1562.3 | 1562.3 | | |
| -27.50 | 1608.4 | 1608.4 | 1608.4 | | |
| -28.00 | 1654.4 | 1654.4 | 1654.4 | | |
| -28.50 | 1700.5 | 1700.5 | 1700.5 | | |
| -29.00 | 1746.6 | 1746.6 | 1746.6 | | |
| -29.50 | 1778.3 | 1778.3 | 1778.3 | | |
| -30.00 | 1815.5 | 1815.5 | 1815.5 | | |
| 19-1008_29 | 0.79 | -6.00 | 277.7 | 277.7 | 277.7 |
| | | -6.50 | 310.9 | 310.9 | 310.9 |
| | | -7.00 | 348.9 | 348.9 | 348.9 |
| | | -7.50 | 388.4 | 388.4 | 388.4 |
| | | -8.00 | 430.6 | 430.6 | 430.6 |
| | | -8.50 | 472.6 | 472.6 | 472.6 |
| | | -9.00 | 509.3 | 509.3 | 509.3 |
| | | -9.50 | 543.7 | 543.7 | 543.7 |
| | | -10.00 | 576.0 | 576.0 | 576.0 |
| | | -10.50 | 613.2 | 613.2 | 613.2 |
| | | -11.00 | 650.2 | 650.2 | 650.2 |
| | | -11.50 | 691.4 | 691.4 | 691.4 |
| | | -12.00 | 711.5 | 711.5 | 711.5 |
| | | -12.50 | 754.5 | 754.5 | 754.5 |
| | | -13.00 | 787.7 | 787.7 | 787.7 |
| | | -13.50 | 802.3 | 802.3 | 802.3 |
| | | -14.00 | 819.3 | 819.3 | 819.3 |
| | | -14.50 | 831.5 | 831.5 | 831.5 |
| | | -15.00 | 842.2 | 842.2 | 842.2 |
| | | -15.50 | 854.7 | 854.7 | 854.7 |
| | | -16.00 | 884.9 | 884.9 | 884.9 |
| | | -16.50 | 896.8 | 896.8 | 896.8 |
| | | -17.00 | 908.8 | 908.8 | 908.8 |
| | | -17.50 | 925.5 | 925.5 | 925.5 |
| | | -18.00 | 964.1 | 964.1 | 964.1 |
| | | -18.50 | 1010.2 | 1010.2 | 1010.2 |
| -19.00 | 1055.7 | 1055.7 | 1055.7 | | |
| -19.50 | 1090.7 | 1090.7 | 1090.7 | | |
| -20.00 | 1136.8 | 1136.8 | 1136.8 | | |
| -20.50 | 1182.9 | 1182.9 | 1182.9 | | |
| -21.00 | 1228.9 | 1228.9 | 1228.9 | | |
| -21.50 | 1275.0 | 1275.0 | 1275.0 | | |
| -22.00 | 1321.1 | 1321.1 | 1321.1 | | |
| -22.50 | 1374.2 | 1374.2 | 1374.2 | | |
| -23.00 | 1414.8 | 1414.8 | 1414.8 | | |
| -23.50 | 1442.8 | 1442.8 | 1442.8 | | |
| -24.00 | 1475.5 | 1475.5 | 1475.5 | | |
| -24.50 | 1508.7 | 1508.7 | 1508.7 | | |
| -25.00 | 1543.8 | 1543.8 | 1543.8 | | |
| -25.50 | 1566.3 | 1566.3 | 1566.3 | | |
| -26.00 | 1591.8 | 1591.8 | 1591.8 | | |
| -26.50 | 1615.8 | 1615.8 | 1615.8 | | |
| -27.00 | 1645.4 | 1645.4 | 1645.4 | | |
| -27.50 | 1668.2 | 1668.2 | 1668.2 | | |
| -28.00 | 1690.5 | 1690.5 | 1690.5 | | |
| -28.50 | 1712.6 | 1712.6 | 1712.6 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|--------------------|--------------------|----------------------------|--------------------------|---------------------------------|
| | | | R _{z,ca1} [kN] | R _{z,d} [kN] | R _{z,netto,zd} [kN] |
| 19-1008_29 | 0.79 | -29.00 | 1736.8 | 1736.8 | 1736.8 |
| | | -29.50 | 1774.1 | 1774.1 | 1774.1 |
| | | -30.00 | 1806.7 | 1806.7 | 1806.7 |
| 283.S02 | 0.17 | -6.00 | 225.0 | 225.0 | 225.0 |
| | | -6.50 | 252.2 | 252.2 | 252.2 |
| | | -7.00 | 284.9 | 284.9 | 284.9 |
| | | -7.50 | 310.9 | 310.9 | 310.9 |
| | | -8.00 | 336.5 | 336.5 | 336.5 |
| | | -8.50 | 367.3 | 367.3 | 367.3 |
| | | -9.00 | 395.8 | 395.8 | 395.8 |
| | | -9.50 | 420.2 | 420.2 | 420.2 |
| | | -10.00 | 447.5 | 447.5 | 447.5 |
| | | -10.50 | 473.8 | 473.8 | 473.8 |
| | | -11.00 | 499.6 | 499.6 | 499.6 |
| | | -11.50 | 527.2 | 527.2 | 527.2 |
| | | -12.00 | 545.4 | 545.4 | 545.4 |
| | | -12.50 | 575.9 | 575.9 | 575.9 |
| | | -13.00 | 609.7 | 609.7 | 609.7 |
| | | -13.50 | 647.2 | 647.2 | 647.2 |
| | | -14.00 | 691.2 | 691.2 | 691.2 |
| | | -14.50 | 735.2 | 735.2 | 735.2 |
| | | -15.00 | 774.9 | 774.9 | 774.9 |
| | | -15.50 | 808.9 | 808.9 | 808.9 |
| | | -16.00 | 846.1 | 846.1 | 846.1 |
| | | -16.50 | 887.4 | 887.4 | 887.4 |
| | | -17.00 | 931.4 | 931.4 | 931.4 |
| | | -17.50 | 977.5 | 977.5 | 977.5 |
| | | -18.00 | 1023.6 | 1023.6 | 1023.6 |
| | | -18.50 | 1069.6 | 1069.6 | 1069.6 |
| | | -19.00 | 1115.7 | 1115.7 | 1115.7 |
| | | -19.50 | 1161.8 | 1161.8 | 1161.8 |
| | | -20.00 | 1207.8 | 1207.8 | 1207.8 |
| | | -20.50 | 1252.0 | 1252.0 | 1252.0 |
| -21.00 | 1298.0 | 1298.0 | 1298.0 | | |
| -21.50 | 1344.1 | 1344.1 | 1344.1 | | |
| -22.00 | 1390.2 | 1390.2 | 1390.2 | | |
| -22.50 | 1436.2 | 1436.2 | 1436.2 | | |
| -23.00 | 1482.3 | 1482.3 | 1482.3 | | |
| -23.50 | 1528.4 | 1528.4 | 1528.4 | | |
| -24.00 | 1574.4 | 1574.4 | 1574.4 | | |
| -24.50 | 1620.5 | 1620.5 | 1620.5 | | |
| -25.00 | 1666.6 | 1666.6 | 1666.6 | | |
| -25.50 | 1712.6 | 1712.6 | 1712.6 | | |
| -26.00 | 1758.7 | 1758.7 | 1758.7 | | |
| -26.50 | 1808.1 | 1808.1 | 1808.1 | | |
| -27.00 | 1826.0 | 1826.0 | 1826.0 | | |
| -27.50 | 1843.0 | 1843.0 | 1843.0 | | |
| -28.00 | 1864.0 | 1864.0 | 1864.0 | | |
| -28.50 | 1890.1 | 1890.1 | 1890.1 | | |
| -29.00 | 1909.3 | 1909.3 | 1909.3 | | |
| -29.50 | 1926.3 | 1926.3 | 1926.3 | | |
| -30.00 | 1942.2 | 1942.2 | 1942.2 | | |
| 19-1008_35 | 0.92 | -6.00 | 245.4 | 245.4 | 245.4 |
| | | -6.50 | 266.1 | 266.1 | 266.1 |
| | | -7.00 | 283.4 | 283.4 | 283.4 |
| | | -7.50 | 301.0 | 301.0 | 301.0 |
| | | -8.00 | 324.8 | 324.8 | 324.8 |
| | | -8.50 | 348.9 | 348.9 | 348.9 |
| | | -9.00 | 367.6 | 367.6 | 367.6 |
| | | -9.50 | 386.5 | 386.5 | 386.5 |
| | | -10.00 | 409.0 | 409.0 | 409.0 |
| | | -10.50 | 430.1 | 430.1 | 430.1 |
| | | -11.00 | 465.4 | 465.4 | 465.4 |
| | | -11.50 | 495.6 | 495.6 | 495.6 |
| | | -12.00 | 517.1 | 517.1 | 517.1 |
| | | -12.50 | 535.8 | 535.8 | 535.8 |
| | | -13.00 | 560.2 | 560.2 | 560.2 |
| | | -13.50 | 588.8 | 588.8 | 588.8 |
| | | -14.00 | 618.5 | 618.5 | 618.5 |
| | | -14.50 | 654.6 | 654.6 | 654.6 |
| | | -15.00 | 690.8 | 690.8 | 690.8 |
| | | -15.50 | 727.5 | 727.5 | 727.5 |
| | | -16.00 | 765.0 | 765.0 | 765.0 |
| | | -16.50 | 802.6 | 802.6 | 802.6 |
| | | -17.00 | 835.2 | 835.2 | 835.2 |
| | | -17.50 | 863.0 | 863.0 | 863.0 |
| | | -18.00 | 899.6 | 899.6 | 899.6 |
| | | -18.50 | 932.8 | 932.8 | 932.8 |
| -19.00 | 969.9 | 969.9 | 969.9 | | |
| -19.50 | 1006.7 | 1006.7 | 1006.7 | | |
| -20.00 | 1044.6 | 1044.6 | 1044.6 | | |
| -20.50 | 1090.8 | 1090.8 | 1090.8 | | |
| -21.00 | 1136.9 | 1136.9 | 1136.9 | | |
| -21.50 | 1182.9 | 1182.9 | 1182.9 | | |
| -22.00 | 1227.9 | 1227.9 | 1227.9 | | |
| -22.50 | 1274.0 | 1274.0 | 1274.0 | | |
| -23.00 | 1320.1 | 1320.1 | 1320.1 | | |
| -23.50 | 1366.1 | 1366.1 | 1366.1 | | |
| -24.00 | 1412.2 | 1412.2 | 1412.2 | | |
| -24.50 | 1457.4 | 1457.4 | 1457.4 | | |
| -25.00 | 1501.0 | 1501.0 | 1501.0 | | |
| -25.50 | 1550.4 | 1550.4 | 1550.4 | | |
| -26.00 | 1596.7 | 1596.7 | 1596.7 | | |
| -26.50 | 1637.3 | 1637.3 | 1637.3 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_35 | 0.92 | -27.00 | 1683.4 | 1683.4 | 1683.4 |
| | | -27.50 | 1729.5 | 1729.5 | 1729.5 |
| | | -28.00 | 1775.5 | 1775.5 | 1775.5 |
| | | -28.50 | 1821.6 | 1821.6 | 1821.6 |
| | | -29.00 | 1867.7 | 1867.7 | 1867.7 |
| | | -29.50 | 1913.7 | 1913.7 | 1913.7 |
| | | -30.00 | 1959.8 | 1959.8 | 1959.8 |
| 312.S03 | 3.78 | -6.00 | 291.0 | 291.0 | 291.0 |
| | | -6.50 | 326.4 | 326.4 | 326.4 |
| | | -7.00 | 367.5 | 367.5 | 367.5 |
| | | -7.50 | 393.1 | 393.1 | 393.1 |
| | | -8.00 | 421.1 | 421.1 | 421.1 |
| | | -8.50 | 467.1 | 467.1 | 467.1 |
| | | -9.00 | 513.2 | 513.2 | 513.2 |
| | | -9.50 | 559.3 | 559.3 | 559.3 |
| | | -10.00 | 605.3 | 605.3 | 605.3 |
| | | -10.50 | 651.2 | 651.2 | 651.2 |
| | | -11.00 | 694.9 | 694.9 | 694.9 |
| | | -11.50 | 740.9 | 740.9 | 740.9 |
| | | -12.00 | 787.0 | 787.0 | 787.0 |
| | | -12.50 | 833.1 | 833.1 | 833.1 |
| | | -13.00 | 877.9 | 877.9 | 877.9 |
| | | -13.50 | 911.1 | 911.1 | 911.1 |
| | | -14.00 | 948.3 | 948.3 | 948.3 |
| | | -14.50 | 985.5 | 985.5 | 985.5 |
| | | -15.00 | 1021.5 | 1021.5 | 1021.5 |
| | | -15.50 | 1058.6 | 1058.6 | 1058.6 |
| | | -16.00 | 1094.9 | 1094.9 | 1094.9 |
| | | -16.50 | 1132.0 | 1132.0 | 1132.0 |
| | | -17.00 | 1166.5 | 1166.5 | 1166.5 |
| | | -17.50 | 1193.8 | 1193.8 | 1193.8 |
| | | -18.00 | 1223.0 | 1223.0 | 1223.0 |
| | | -18.50 | 1259.3 | 1259.3 | 1259.3 |
| | | -19.00 | 1297.5 | 1297.5 | 1297.5 |
| | | -19.50 | 1336.9 | 1336.9 | 1336.9 |
| | | -20.00 | 1375.0 | 1375.0 | 1375.0 |
| | | -20.50 | 1408.6 | 1408.6 | 1408.6 |
| -21.00 | 1445.4 | 1445.4 | 1445.4 | | |
| -21.50 | 1479.7 | 1479.7 | 1479.7 | | |
| -22.00 | 1518.3 | 1518.3 | 1518.3 | | |
| -22.50 | 1563.3 | 1563.3 | 1563.3 | | |
| -23.00 | 1608.6 | 1608.6 | 1608.6 | | |
| -23.50 | 1652.6 | 1652.6 | 1652.6 | | |
| -24.00 | 1693.2 | 1693.2 | 1693.2 | | |
| -24.50 | 1739.2 | 1739.2 | 1739.2 | | |
| -25.00 | 1785.3 | 1785.3 | 1785.3 | | |
| -25.50 | 1828.7 | 1828.7 | 1828.7 | | |
| -26.00 | 1867.6 | 1867.6 | 1867.6 | | |
| -26.50 | 1912.7 | 1912.7 | 1912.7 | | |
| -27.00 | 1957.8 | 1957.8 | 1957.8 | | |
| -27.50 | 1983.2 | 1983.2 | 1983.2 | | |
| -28.00 | 2003.3 | 2003.3 | 2003.3 | | |
| -28.50 | 2019.1 | 2019.1 | 2019.1 | | |
| -29.00 | 2034.7 | 2034.7 | 2034.7 | | |
| -29.50 | 2052.5 | 2052.5 | 2052.5 | | |
| -30.00 | 2076.2 | 2076.2 | 2076.2 | | |
| 19-1008_43 | 9.88 | -6.00 | 224.5 | 224.5 | 224.5 |
| | | -6.50 | 244.3 | 244.3 | 244.3 |
| | | -7.00 | 280.5 | 280.5 | 280.5 |
| | | -7.50 | 315.3 | 315.3 | 315.3 |
| | | -8.00 | 351.4 | 351.4 | 351.4 |
| | | -8.50 | 385.2 | 385.2 | 385.2 |
| | | -9.00 | 419.8 | 419.8 | 419.8 |
| | | -9.50 | 455.1 | 455.1 | 455.1 |
| | | -10.00 | 487.5 | 487.5 | 487.5 |
| | | -10.50 | 526.2 | 526.2 | 526.2 |
| | | -11.00 | 572.3 | 572.3 | 572.3 |
| | | -11.50 | 618.3 | 618.3 | 618.3 |
| | | -12.00 | 664.4 | 664.4 | 664.4 |
| | | -12.50 | 710.1 | 710.1 | 710.1 |
| | | -13.00 | 744.5 | 744.5 | 744.5 |
| | | -13.50 | 774.4 | 774.4 | 774.4 |
| | | -14.00 | 809.0 | 809.0 | 809.0 |
| | | -14.50 | 846.1 | 846.1 | 846.1 |
| | | -15.00 | 878.9 | 878.9 | 878.9 |
| | | -15.50 | 919.3 | 919.3 | 919.3 |
| | | -16.00 | 963.6 | 963.6 | 963.6 |
| | | -16.50 | 1009.7 | 1009.7 | 1009.7 |
| | | -17.00 | 1055.8 | 1055.8 | 1055.8 |
| | | -17.50 | 1100.2 | 1100.2 | 1100.2 |
| -18.00 | 1140.6 | 1140.6 | 1140.6 | | |
| -18.50 | 1176.9 | 1176.9 | 1176.9 | | |
| -19.00 | 1213.2 | 1213.2 | 1213.2 | | |
| -19.50 | 1242.9 | 1242.9 | 1242.9 | | |
| -20.00 | 1273.5 | 1273.5 | 1273.5 | | |
| -20.50 | 1311.8 | 1311.8 | 1311.8 | | |
| -21.00 | 1356.1 | 1356.1 | 1356.1 | | |
| -21.50 | 1392.8 | 1392.8 | 1392.8 | | |
| -22.00 | 1434.3 | 1434.3 | 1434.3 | | |
| -22.50 | 1480.4 | 1480.4 | 1480.4 | | |
| -23.00 | 1526.4 | 1526.4 | 1526.4 | | |
| -23.50 | 1572.5 | 1572.5 | 1572.5 | | |
| -24.00 | 1618.6 | 1618.6 | 1618.6 | | |
| -24.50 | 1664.6 | 1664.6 | 1664.6 | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt | | Bewijkdraagvermogen | Rekenwaarden | | |
|------------|-------------------|--------|---------------------|---------------------|-------------------|-------------------------|
| | niveau | niveau | | $R_{t,ca1}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_43 | 9.88 | -25.00 | 1703.7 | 1703.7 | 1703.7 | |
| 328.S02 | 10.17 | -6.00 | 371.0 | 371.0 | 371.0 | |
| | | -6.50 | 408.2 | 408.2 | 408.2 | |
| | | -7.00 | 434.2 | 434.2 | 434.2 | |
| | | -7.50 | 466.8 | 466.8 | 466.8 | |
| | | -8.00 | 502.5 | 502.5 | 502.5 | |
| | | -8.50 | 539.3 | 539.3 | 539.3 | |
| | | -9.00 | 575.0 | 575.0 | 575.0 | |
| | | -9.50 | 605.9 | 605.9 | 605.9 | |
| | | -10.00 | 640.7 | 640.7 | 640.7 | |
| | | -10.50 | 677.0 | 677.0 | 677.0 | |
| | | -11.00 | 718.4 | 718.4 | 718.4 | |
| | | -11.50 | 760.8 | 760.8 | 760.8 | |
| | | -12.00 | 802.0 | 802.0 | 802.0 | |
| | | -12.50 | 839.3 | 839.3 | 839.3 | |
| | | -13.00 | 875.7 | 875.7 | 875.7 | |
| | | -13.50 | 912.6 | 912.6 | 912.6 | |
| | | -14.00 | 949.8 | 949.8 | 949.8 | |
| | | -14.50 | 986.0 | 986.0 | 986.0 | |
| | | -15.00 | 1023.5 | 1023.5 | 1023.5 | |
| | | -15.50 | 1060.7 | 1060.7 | 1060.7 | |
| | | -16.00 | 1097.5 | 1097.5 | 1097.5 | |
| | | -16.50 | 1136.0 | 1136.0 | 1136.0 | |
| | | -17.00 | 1182.1 | 1182.1 | 1182.1 | |
| | | -17.50 | 1228.1 | 1228.1 | 1228.1 | |
| | | -18.00 | 1280.8 | 1280.8 | 1280.8 | |
| | | -18.50 | 1314.2 | 1314.2 | 1314.2 | |
| | | -19.00 | 1355.8 | 1355.8 | 1355.8 | |
| | | -19.50 | 1400.0 | 1400.0 | 1400.0 | |
| | | -20.00 | 1446.1 | 1446.1 | 1446.1 | |
| | | -20.50 | 1492.2 | 1492.2 | 1492.2 | |
| | | -21.00 | 1538.2 | 1538.2 | 1538.2 | |
| | | -21.50 | 1584.3 | 1584.3 | 1584.3 | |
| | | -22.00 | 1630.4 | 1630.4 | 1630.4 | |
| | | -22.50 | 1676.4 | 1676.4 | 1676.4 | |
| | | -23.00 | 1722.5 | 1722.5 | 1722.5 | |
| | | -23.50 | 1768.6 | 1768.6 | 1768.6 | |
| | | -24.00 | 1814.6 | 1814.6 | 1814.6 | |
| | | -24.50 | 1853.8 | 1853.8 | 1853.8 | |
| | | -25.00 | 1891.0 | 1891.0 | 1891.0 | |
| | | -25.50 | 1927.6 | 1927.6 | 1927.6 | |
| | | -26.00 | 1964.8 | 1964.8 | 1964.8 | |
| | | -26.50 | 2004.2 | 2004.2 | 2004.2 | |
| | | -27.00 | 2050.2 | 2050.2 | 2050.2 | |
| | | -27.50 | 2096.3 | 2096.3 | 2096.3 | |
| | | -28.00 | 2135.4 | 2135.4 | 2135.4 | |
| | | -28.50 | 2169.6 | 2169.6 | 2169.6 | |

REKENGEGEVENS SI Ø610/850 trek

Berekening : Ontwerpend
Rekenmethode : Trekpalen volgens NEN-EN 1997-1, art. 7.6.3
Sondering(en) : 19-1008_1, 19-1008_6, 166.S01, 19-1008_11, 19-1008_12
: 19-1008_17, 19-1008_20, 19-1008_21, 251.S01, 19-1008_29
: 283.S02, 19-1008_35, 312.S03, 19-1008_43, 328.S02

Let op: trekcapaciteit t.p.v. negatief kleeftraject is meegerekend.

Stijf bouwwerk : NEE
Paalgroep : NEE
Aantal sonderingen : 15
Factor $\xi_3 (n=1)$: 1.39 (handmatig)
Factor $\xi_3 (g=0)$: 1.39 (handmatig)
Factor $\xi_3 (min)$: 1.39 (handmatig)
Weerstandsfactor γ_R : 1.35
 $\gamma_{m,verleg}$: 1.50
UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø610/850
Niveau paalkop [m] : N.A.P. 0.00
Bovenbel. [kN/m²] : 0.00

PAALPUNTNIVEAUS SI Ø610/850

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|--------------------|-------------------|--------------------|
| 1 | -7.00 | -30.00 | 0.50 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø610/850 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering | 19-1008_1 | 19-1008_6 | 166.S01 | 19-1008_11 | 19-1008_12 | 19-1008_17 |
|-----------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| Niveau | F _{netto:tt} | F _{netto:tt} | F _{netto:tt} | F _{netto:tt} | F _{netto:tt} | F _{netto:tt} |
| [m] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] |
| -7.00 | 72 | 607 | 407 | 216 | 626 | 130 |
| -7.50 | 77 | 664 | 464 | 234 | 684 | 145 |
| -8.00 | 92 | 722 | 522 | 258 | 741 | 152 |
| -8.50 | 108 | 779 | 579 | 281 | 771 | 161 |
| -9.00 | 114 | 837 | 636 | 299 | 782 | 175 |
| -9.50 | 140 | 894 | 692 | 316 | 790 | 186 |
| -10.00 | 162 | 952 | 750 | 334 | 805 | 229 |
| -10.50 | 189 | 1009 | 807 | 355 | 831 | 251 |
| -11.00 | 207 | 1067 | 865 | 379 | 853 | 289 |
| -11.50 | 238 | 1124 | 922 | 407 | 859 | 346 |
| -12.00 | 276 | 1181 | 976 | 442 | 879 | 404 |
| -12.50 | 302 | 1239 | 1021 | 457 | 887 | 461 |
| -13.00 | 344 | 1296 | 1064 | 498 | 895 | 519 |
| -13.50 | 385 | 1354 | 1107 | 546 | 903 | 576 |
| -14.00 | 420 | 1411 | 1156 | 595 | 921 | 634 |
| -14.50 | 466 | 1469 | 1214 | 644 | 943 | 691 |
| -15.00 | 509 | 1526 | 1271 | 694 | 960 | 744 |
| -15.50 | 555 | 1584 | 1328 | 740 | 973 | 802 |
| -16.00 | 595 | 1641 | 1386 | 780 | 993 | 859 |
| -16.50 | 639 | 1699 | 1443 | 826 | 1020 | 917 |
| -17.00 | 683 | 1756 | 1501 | 870 | 1043 | 972 |
| -17.50 | 735 | 1814 | 1558 | 913 | 1076 | 1031 |
| -18.00 | 792 | 1871 | 1616 | 965 | 1102 | 1100 |
| -18.50 | 850 | 1925 | 1673 | 1023 | 1158 | 1147 |
| -19.00 | 907 | 1982 | 1731 | 1080 | 1210 | 1187 |
| -19.50 | 965 | 2040 | 1788 | 1137 | 1258 | 1234 |
| -20.00 | 1037 | 2097 | 1846 | 1195 | 1300 | 1281 |
| -20.50 | 1110 | 2155 | 1903 | 1252 | 1346 | 1330 |
| -21.00 | 1186 | 2212 | 1961 | 1310 | 1390 | 1382 |
| -21.50 | 1240 | 2270 | 2018 | 1364 | 1442 | 1439 |
| -22.00 | 1297 | 2327 | 2076 | 1422 | 1499 | 1489 |
| -22.50 | 1355 | 2385 | 2133 | 1479 | 1556 | 1546 |
| -23.00 | 1412 | 2442 | 0 | 1532 | 1608 | 1604 |
| -23.50 | 1470 | 2500 | 0 | 1568 | 1658 | 1661 |
| -24.00 | 1527 | 0 | 0 | 1613 | 1712 | 1715 |
| -24.50 | 1585 | 0 | 0 | 1664 | 1769 | 1761 |
| -25.00 | 1642 | 0 | 0 | 1712 | 1827 | 1798 |
| -25.50 | 1700 | 0 | 0 | 1754 | 1902 | 1833 |
| -26.00 | 1757 | 0 | 0 | 1812 | 1977 | 1868 |
| -26.50 | 1814 | 0 | 0 | 1869 | 2022 | 1903 |
| -27.00 | 1872 | 0 | 0 | 1927 | 2063 | 1944 |
| -27.50 | 1929 | 0 | 0 | 1984 | 2111 | 1988 |
| -28.00 | 1987 | 0 | 0 | 2042 | 2146 | 2032 |
| -28.50 | 2044 | 0 | 0 | 2099 | 2190 | 2079 |
| -29.00 | 2102 | 0 | 0 | 2157 | 2248 | 2127 |
| -29.50 | 2159 | 0 | 0 | 2214 | 2305 | 2143 |
| -30.00 | 2217 | 0 | 0 | 2272 | 2362 | 2180 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø610/850 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | 19-1008_20 | 19-1008_21 | 251.S01 | 19-1008_29 | 283.S02 | 19-1008_35 |
|--------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|
| [m] | F _{netto:rt} [kN] | F _{netto:rt} [kN] | F _{netto:rt} [kN] | F _{netto:rt} [kN] | F _{netto:rt} [kN] | F _{netto:rt} [kN] |
| -7.00 | 170 | 271 | 322 | 438 | 360 | 357 |
| -7.50 | 202 | 316 | 368 | 488 | 392 | 380 |
| -8.00 | 227 | 359 | 409 | 541 | 425 | 410 |
| -8.50 | 252 | 403 | 438 | 593 | 463 | 440 |
| -9.00 | 285 | 426 | 444 | 639 | 499 | 463 |
| -9.50 | 312 | 445 | 471 | 682 | 530 | 487 |
| -10.00 | 344 | 471 | 510 | 722 | 564 | 516 |
| -10.50 | 353 | 495 | 556 | 769 | 597 | 542 |
| -11.00 | 393 | 522 | 592 | 815 | 629 | 586 |
| -11.50 | 436 | 555 | 614 | 867 | 664 | 624 |
| -12.00 | 446 | 592 | 637 | 892 | 687 | 651 |
| -12.50 | 458 | 621 | 673 | 946 | 725 | 675 |
| -13.00 | 477 | 654 | 715 | 987 | 767 | 706 |
| -13.50 | 488 | 690 | 756 | 1006 | 814 | 741 |
| -14.00 | 506 | 743 | 810 | 1027 | 869 | 779 |
| -14.50 | 536 | 796 | 865 | 1043 | 924 | 824 |
| -15.00 | 571 | 836 | 924 | 1056 | 974 | 869 |
| -15.50 | 592 | 867 | 951 | 1072 | 1016 | 915 |
| -16.00 | 608 | 923 | 1005 | 1110 | 1063 | 962 |
| -16.50 | <u>630</u> | 979 | 1062 | 1125 | 1114 | 1009 |
| -17.00 | <u>645</u> | 990 | 1119 | 1141 | 1169 | 1050 |
| -17.50 | <u>663</u> | 1003 | 1174 | 1162 | 1227 | 1084 |
| -18.00 | <u>694</u> | 1025 | 1225 | 1210 | 1284 | 1130 |
| -18.50 | <u>730</u> | 1086 | 1282 | 1268 | 1342 | 1172 |
| -19.00 | <u>758</u> | 1128 | 1318 | 1324 | 1399 | 1218 |
| -19.50 | <u>795</u> | 1141 | 1356 | 1368 | 1457 | 1264 |
| -20.00 | <u>832</u> | 1151 | 1401 | 1426 | 1514 | 1312 |
| -20.50 | <u>880</u> | 1162 | 1463 | 1483 | 1569 | 1369 |
| -21.00 | <u>943</u> | 1172 | 1529 | 1541 | 1627 | 1427 |
| -21.50 | <u>971</u> | 1185 | 1557 | 1598 | 1684 | 1484 |
| -22.00 | <u>990</u> | 1198 | 1568 | 1656 | 1742 | 1540 |
| -22.50 | <u>1011</u> | 1214 | 1581 | 1722 | 1799 | 1598 |
| -23.00 | 1029 | 1231 | 1601 | 1773 | 1857 | 1655 |
| -23.50 | 1060 | 1246 | 1626 | 1808 | 1914 | 1713 |
| -24.00 | 1095 | 1264 | 1659 | 1849 | 1971 | 1770 |
| -24.50 | 1132 | 1283 | 1690 | 1890 | 2029 | 1827 |
| -25.00 | 1176 | 1302 | 1718 | 1934 | 2086 | 1881 |
| -25.50 | 1216 | 1322 | 1766 | 1962 | 2144 | 1943 |
| -26.00 | 1256 | 1341 | 1835 | 1994 | 2201 | 2000 |
| -26.50 | 1292 | 1359 | 1903 | 2024 | 2263 | 2051 |
| -27.00 | 1336 | 1377 | 1960 | 2062 | 2286 | 2109 |
| -27.50 | 1374 | 1395 | 2018 | 2090 | 2307 | 2166 |
| -28.00 | 1409 | 1414 | 2075 | 2118 | 2333 | 2223 |
| -28.50 | 1450 | 1434 | 2133 | 2146 | 2366 | 2281 |
| -29.00 | 1488 | 1453 | 2190 | 2177 | 2390 | 2338 |
| -29.50 | 1519 | 1473 | 2230 | 2223 | 2412 | 2396 |
| -30.00 | 1557 | 1494 | 2276 | 2264 | 2432 | 2453 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø610/850 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Sondering 312.S03 19-1008_43 328.S02

| Niveau [m] | F _{netto:st} [kN] | F _{netto:st} [kN] | F _{netto:st} [kN] |
|---------------|-------------------------------|-------------------------------|-------------------------------|
| -7.00 | 461 | 354 | 544 |
| -7.50 | 494 | 397 | 585 |
| -8.00 | 529 | 442 | 629 |
| -8.50 | 586 | 485 | 675 |
| -9.00 | 644 | 528 | 720 |
| -9.50 | 701 | 572 | 759 |
| -10.00 | 758 | 613 | 802 |
| -10.50 | 816 | 661 | 848 |
| -11.00 | 870 | 719 | 899 |
| -11.50 | 928 | 776 | 952 |
| -12.00 | 985 | 833 | 1004 |
| -12.50 | 1043 | 890 | 1050 |
| -13.00 | 1099 | 934 | 1096 |
| -13.50 | 1140 | 971 | 1142 |
| -14.00 | 1187 | 1014 | 1188 |
| -14.50 | 1233 | 1061 | 1234 |
| -15.00 | 1278 | 1102 | 1281 |
| -15.50 | 1325 | 1152 | 1327 |
| -16.00 | 1370 | 1207 | 1373 |
| -16.50 | 1416 | 1265 | 1421 |
| -17.00 | 1459 | 1322 | 1479 |
| -17.50 | 1494 | 1378 | 1536 |
| -18.00 | 1530 | 1428 | 1602 |
| -18.50 | 1576 | 1474 | 1644 |
| -19.00 | 1623 | 1519 | 1696 |
| -19.50 | 1673 | 1556 | 1751 |
| -20.00 | 1720 | 1595 | 1808 |
| -20.50 | 1762 | 1642 | 1866 |
| -21.00 | 1808 | 1698 | 1923 |
| -21.50 | 1851 | 1744 | 1981 |
| -22.00 | 1899 | 1796 | 2038 |
| -22.50 | 1956 | 1853 | 2096 |
| -23.00 | 2012 | 1910 | 2153 |
| -23.50 | 2067 | 1968 | 2211 |
| -24.00 | 2118 | 2025 | 2268 |
| -24.50 | 2175 | 2083 | 2317 |
| -25.00 | 2233 | 2132 | 2363 |
| -25.50 | 2287 | 0 | 2409 |
| -26.00 | 2335 | 0 | 2456 |
| -26.50 | 2392 | 0 | 2505 |
| -27.00 | 2448 | 0 | 2562 |
| -27.50 | 2480 | 0 | 2620 |
| -28.00 | 2505 | 0 | 2669 |
| -28.50 | 2525 | 0 | 2711 |
| -29.00 | 2545 | 0 | 0 |
| -29.50 | 2568 | 0 | 0 |
| -30.00 | 2597 | 0 | 0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

SAMENVATTINGSTABEL SI Ø610/850 trek (n=1)
Uitgangspunten

- paal : SI Ø610/850
 - paaltype : In de grond gevormde geschroefde paal; groutinjection
 - schachtafmeting : 730 mm
 Paalklassefactor α_p : 0.63
 Factor α_s (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
 Correlatiefactor $\xi_{s(n=1)}$: 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt | | Bewijkdraagvermogen | | |
|-----------|-------------------|--------|----------------------|-------------------|-------------------------|
| | niveau | niveau | $R_{t,calc}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_1 | 2.12 | -7.00 | 72.1 | 72.1 | 72.1 |
| | | -7.50 | 76.9 | 76.9 | 76.9 |
| | | -8.00 | 91.5 | 91.5 | 91.5 |
| | | -8.50 | 107.7 | 107.7 | 107.7 |
| | | -9.00 | 114.4 | 114.4 | 114.4 |
| | | -9.50 | 139.6 | 139.6 | 139.6 |
| | | -10.00 | 162.3 | 162.3 | 162.3 |
| | | -10.50 | 188.5 | 188.5 | 188.5 |
| | | -11.00 | 207.1 | 207.1 | 207.1 |
| | | -11.50 | 237.6 | 237.6 | 237.6 |
| | | -12.00 | 276.1 | 276.1 | 276.1 |
| | | -12.50 | 302.5 | 302.5 | 302.5 |
| | | -13.00 | 343.6 | 343.6 | 343.6 |
| | | -13.50 | 384.6 | 384.6 | 384.6 |
| | | -14.00 | 420.2 | 420.2 | 420.2 |
| | | -14.50 | 466.5 | 466.5 | 466.5 |
| | | -15.00 | 509.1 | 509.1 | 509.1 |
| | | -15.50 | 555.3 | 555.3 | 555.3 |
| | | -16.00 | 595.1 | 595.1 | 595.1 |
| | | -16.50 | 638.8 | 638.8 | 638.8 |
| | | -17.00 | 683.2 | 683.2 | 683.2 |
| | | -17.50 | 734.7 | 734.7 | 734.7 |
| | | -18.00 | 792.1 | 792.1 | 792.1 |
| | | -18.50 | 849.6 | 849.6 | 849.6 |
| | | -19.00 | 907.1 | 907.1 | 907.1 |
| | | -19.50 | 964.5 | 964.5 | 964.5 |
| | | -20.00 | 1036.7 | 1036.7 | 1036.7 |
| | | -20.50 | 1109.8 | 1109.8 | 1109.8 |
| | | -21.00 | 1185.6 | 1185.6 | 1185.6 |
| | | -21.50 | 1239.8 | 1239.8 | 1239.8 |
| | | -22.00 | 1297.2 | 1297.2 | 1297.2 |
| -22.50 | 1354.7 | 1354.7 | 1354.7 | | |
| -23.00 | 1412.2 | 1412.2 | 1412.2 | | |
| -23.50 | 1469.7 | 1469.7 | 1469.7 | | |
| -24.00 | 1527.1 | 1527.1 | 1527.1 | | |
| -24.50 | 1584.6 | 1584.6 | 1584.6 | | |
| -25.00 | 1642.1 | 1642.1 | 1642.1 | | |
| -25.50 | 1699.5 | 1699.5 | 1699.5 | | |
| -26.00 | 1757.0 | 1757.0 | 1757.0 | | |
| -26.50 | 1814.5 | 1814.5 | 1814.5 | | |
| -27.00 | 1871.9 | 1871.9 | 1871.9 | | |
| -27.50 | 1929.4 | 1929.4 | 1929.4 | | |
| -28.00 | 1986.9 | 1986.9 | 1986.9 | | |
| -28.50 | 2044.4 | 2044.4 | 2044.4 | | |
| -29.00 | 2101.8 | 2101.8 | 2101.8 | | |
| -29.50 | 2159.3 | 2159.3 | 2159.3 | | |
| -30.00 | 2216.8 | 2216.8 | 2216.8 | | |
| 19-1008_6 | 11.00 | -7.00 | 606.7 | 606.7 | 606.7 |
| | | -7.50 | 664.2 | 664.2 | 664.2 |
| | | -8.00 | 721.7 | 721.7 | 721.7 |
| | | -8.50 | 779.2 | 779.2 | 779.2 |
| | | -9.00 | 836.6 | 836.6 | 836.6 |
| | | -9.50 | 894.1 | 894.1 | 894.1 |
| | | -10.00 | 951.6 | 951.6 | 951.6 |
| | | -10.50 | 1009.0 | 1009.0 | 1009.0 |
| | | -11.00 | 1066.5 | 1066.5 | 1066.5 |
| | | -11.50 | 1124.0 | 1124.0 | 1124.0 |
| | | -12.00 | 1181.4 | 1181.4 | 1181.4 |
| | | -12.50 | 1238.9 | 1238.9 | 1238.9 |
| | | -13.00 | 1296.4 | 1296.4 | 1296.4 |
| | | -13.50 | 1353.9 | 1353.9 | 1353.9 |
| | | -14.00 | 1411.3 | 1411.3 | 1411.3 |
| | | -14.50 | 1468.8 | 1468.8 | 1468.8 |
| | | -15.00 | 1526.3 | 1526.3 | 1526.3 |
| | | -15.50 | 1583.7 | 1583.7 | 1583.7 |
| | | -16.00 | 1641.2 | 1641.2 | 1641.2 |
| | | -16.50 | 1698.7 | 1698.7 | 1698.7 |
| | | -17.00 | 1756.1 | 1756.1 | 1756.1 |
| -17.50 | 1813.6 | 1813.6 | 1813.6 | | |
| -18.00 | 1871.1 | 1871.1 | 1871.1 | | |
| -18.50 | 1924.9 | 1924.9 | 1924.9 | | |
| -19.00 | 1982.4 | 1982.4 | 1982.4 | | |
| -19.50 | 2039.8 | 2039.8 | 2039.8 | | |
| -20.00 | 2097.3 | 2097.3 | 2097.3 | | |
| -20.50 | 2154.8 | 2154.8 | 2154.8 | | |
| -21.00 | 2212.3 | 2212.3 | 2212.3 | | |
| -21.50 | 2269.7 | 2269.7 | 2269.7 | | |
| -22.00 | 2327.2 | 2327.2 | 2327.2 | | |
| -22.50 | 2384.7 | 2384.7 | 2384.7 | | |
| -23.00 | 2442.1 | 2442.1 | 2442.1 | | |
| -23.50 | 2499.6 | 2499.6 | 2499.6 | | |
| 166.S01 | 3.45 | -7.00 | 407.0 | 407.0 | 407.0 |
| | | -7.50 | 464.5 | 464.5 | 464.5 |
| | | -8.00 | 522.0 | 522.0 | 522.0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|--------------------|--------------------|----------------------------|--------------------------|---------------------------------|
| | | | R _{z,ca1} [kN] | R _{z,d} [kN] | R _{z,netto,zd} [kN] |
| 166.S01 | 3.45 | -8.50 | 579.0 | 579.0 | 579.0 |
| | | -9.00 | 636.0 | 636.0 | 636.0 |
| | | -9.50 | 692.2 | 692.2 | 692.2 |
| | | -10.00 | 749.7 | 749.7 | 749.7 |
| | | -10.50 | 807.2 | 807.2 | 807.2 |
| | | -11.00 | 864.6 | 864.6 | 864.6 |
| | | -11.50 | 922.1 | 922.1 | 922.1 |
| | | -12.00 | 975.6 | 975.6 | 975.6 |
| | | -12.50 | 1020.9 | 1020.9 | 1020.9 |
| | | -13.00 | 1063.6 | 1063.6 | 1063.6 |
| | | -13.50 | 1106.6 | 1106.6 | 1106.6 |
| | | -14.00 | 1156.3 | 1156.3 | 1156.3 |
| | | -14.50 | 1213.5 | 1213.5 | 1213.5 |
| | | -15.00 | 1271.0 | 1271.0 | 1271.0 |
| | | -15.50 | 1328.5 | 1328.5 | 1328.5 |
| | | -16.00 | 1385.9 | 1385.9 | 1385.9 |
| | | -16.50 | 1443.4 | 1443.4 | 1443.4 |
| | | -17.00 | 1500.9 | 1500.9 | 1500.9 |
| | | -17.50 | 1558.3 | 1558.3 | 1558.3 |
| | | -18.00 | 1615.8 | 1615.8 | 1615.8 |
| | | -18.50 | 1673.3 | 1673.3 | 1673.3 |
| -19.00 | 1730.8 | 1730.8 | 1730.8 | | |
| -19.50 | 1788.2 | 1788.2 | 1788.2 | | |
| -20.00 | 1845.7 | 1845.7 | 1845.7 | | |
| -20.50 | 1903.2 | 1903.2 | 1903.2 | | |
| -21.00 | 1960.6 | 1960.6 | 1960.6 | | |
| -21.50 | 2018.1 | 2018.1 | 2018.1 | | |
| -22.00 | 2075.6 | 2075.6 | 2075.6 | | |
| -22.50 | 2133.0 | 2133.0 | 2133.0 | | |
| 19-1008_11 | 0.62 | -7.00 | 216.1 | 216.1 | 216.1 |
| | | -7.50 | 233.6 | 233.6 | 233.6 |
| | | -8.00 | 258.1 | 258.1 | 258.1 |
| | | -8.50 | 280.7 | 280.7 | 280.7 |
| | | -9.00 | 298.8 | 298.8 | 298.8 |
| | | -9.50 | 316.1 | 316.1 | 316.1 |
| | | -10.00 | 333.9 | 333.9 | 333.9 |
| | | -10.50 | 354.9 | 354.9 | 354.9 |
| | | -11.00 | 378.9 | 378.9 | 378.9 |
| | | -11.50 | 407.3 | 407.3 | 407.3 |
| | | -12.00 | 442.5 | 442.5 | 442.5 |
| | | -12.50 | 457.1 | 457.1 | 457.1 |
| | | -13.00 | 498.4 | 498.4 | 498.4 |
| | | -13.50 | 546.3 | 546.3 | 546.3 |
| | | -14.00 | 595.1 | 595.1 | 595.1 |
| | | -14.50 | 644.5 | 644.5 | 644.5 |
| | | -15.00 | 693.8 | 693.8 | 693.8 |
| | | -15.50 | 740.3 | 740.3 | 740.3 |
| | | -16.00 | 779.8 | 779.8 | 779.8 |
| | | -16.50 | 825.8 | 825.8 | 825.8 |
| | | -17.00 | 870.5 | 870.5 | 870.5 |
| | | -17.50 | 912.6 | 912.6 | 912.6 |
| | | -18.00 | 965.1 | 965.1 | 965.1 |
| | | -18.50 | 1022.5 | 1022.5 | 1022.5 |
| | | -19.00 | 1080.0 | 1080.0 | 1080.0 |
| | | -19.50 | 1137.5 | 1137.5 | 1137.5 |
| | | -20.00 | 1194.9 | 1194.9 | 1194.9 |
| | | -20.50 | 1252.4 | 1252.4 | 1252.4 |
| | | -21.00 | 1309.9 | 1309.9 | 1309.9 |
| | | -21.50 | 1364.3 | 1364.3 | 1364.3 |
| -22.00 | 1421.7 | 1421.7 | 1421.7 | | |
| -22.50 | 1479.2 | 1479.2 | 1479.2 | | |
| -23.00 | 1531.9 | 1531.9 | 1531.9 | | |
| -23.50 | 1567.5 | 1567.5 | 1567.5 | | |
| -24.00 | 1612.7 | 1612.7 | 1612.7 | | |
| -24.50 | 1663.6 | 1663.6 | 1663.6 | | |
| -25.00 | 1712.3 | 1712.3 | 1712.3 | | |
| -25.50 | 1753.6 | 1753.6 | 1753.6 | | |
| -26.00 | 1811.8 | 1811.8 | 1811.8 | | |
| -26.50 | 1869.3 | 1869.3 | 1869.3 | | |
| -27.00 | 1926.8 | 1926.8 | 1926.8 | | |
| -27.50 | 1984.3 | 1984.3 | 1984.3 | | |
| -28.00 | 2041.7 | 2041.7 | 2041.7 | | |
| -28.50 | 2099.2 | 2099.2 | 2099.2 | | |
| -29.00 | 2156.7 | 2156.7 | 2156.7 | | |
| -29.50 | 2214.1 | 2214.1 | 2214.1 | | |
| -30.00 | 2271.6 | 2271.6 | 2271.6 | | |
| 19-1008_12 | 3.57 | -7.00 | 626.1 | 626.1 | 626.1 |
| | | -7.50 | 683.6 | 683.6 | 683.6 |
| | | -8.00 | 740.7 | 740.7 | 740.7 |
| | | -8.50 | 771.2 | 771.2 | 771.2 |
| | | -9.00 | 781.9 | 781.9 | 781.9 |
| | | -9.50 | 790.3 | 790.3 | 790.3 |
| | | -10.00 | 804.7 | 804.7 | 804.7 |
| | | -10.50 | 831.4 | 831.4 | 831.4 |
| | | -11.00 | 852.5 | 852.5 | 852.5 |
| | | -11.50 | 858.7 | 858.7 | 858.7 |
| | | -12.00 | 878.6 | 878.6 | 878.6 |
| | | -12.50 | 887.4 | 887.4 | 887.4 |
| | | -13.00 | 894.8 | 894.8 | 894.8 |
| | | -13.50 | 903.5 | 903.5 | 903.5 |
| | | -14.00 | 921.0 | 921.0 | 921.0 |
| -14.50 | 943.3 | 943.3 | 943.3 | | |
| -15.00 | 959.6 | 959.6 | 959.6 | | |
| -15.50 | 973.0 | 973.0 | 973.0 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_12 | 3.57 | -16.00 | 993.3 | 993.3 | 993.3 |
| | | -16.50 | 1020.2 | 1020.2 | 1020.2 |
| | | -17.00 | 1043.0 | 1043.0 | 1043.0 |
| | | -17.50 | 1075.7 | 1075.7 | 1075.7 |
| | | -18.00 | 1101.6 | 1101.6 | 1101.6 |
| | | -18.50 | 1158.3 | 1158.3 | 1158.3 |
| | | -19.00 | 1210.3 | 1210.3 | 1210.3 |
| | | -19.50 | 1258.2 | 1258.2 | 1258.2 |
| | | -20.00 | 1299.7 | 1299.7 | 1299.7 |
| | | -20.50 | 1346.2 | 1346.2 | 1346.2 |
| | | -21.00 | 1389.9 | 1389.9 | 1389.9 |
| | | -21.50 | 1442.4 | 1442.4 | 1442.4 |
| | | -22.00 | 1499.1 | 1499.1 | 1499.1 |
| | | -22.50 | 1555.8 | 1555.8 | 1555.8 |
| | | -23.00 | 1607.9 | 1607.9 | 1607.9 |
| | | -23.50 | 1658.1 | 1658.1 | 1658.1 |
| | | -24.00 | 1711.6 | 1711.6 | 1711.6 |
| | | -24.50 | 1769.0 | 1769.0 | 1769.0 |
| | | -25.00 | 1826.5 | 1826.5 | 1826.5 |
| | | -25.50 | 1901.6 | 1901.6 | 1901.6 |
| | | -26.00 | 1977.0 | 1977.0 | 1977.0 |
| | | -26.50 | 2021.6 | 2021.6 | 2021.6 |
| | | -27.00 | 2063.3 | 2063.3 | 2063.3 |
| | | -27.50 | 2110.9 | 2110.9 | 2110.9 |
| | | -28.00 | 2145.9 | 2145.9 | 2145.9 |
| | | -28.50 | 2190.2 | 2190.2 | 2190.2 |
| | | -29.00 | 2247.7 | 2247.7 | 2247.7 |
| | | -29.50 | 2305.2 | 2305.2 | 2305.2 |
| | | -30.00 | 2361.6 | 2361.6 | 2361.6 |
| | | 19-1008_17 | 0.20 | -7.00 | 129.7 |
| -7.50 | 144.9 | | | 144.9 | 144.9 |
| -8.00 | 152.3 | | | 152.3 | 152.3 |
| -8.50 | 160.8 | | | 160.8 | 160.8 |
| -9.00 | 174.8 | | | 174.8 | 174.8 |
| -9.50 | 186.0 | | | 186.0 | 186.0 |
| -10.00 | 229.0 | | | 229.0 | 229.0 |
| -10.50 | 251.5 | | | 251.5 | 251.5 |
| -11.00 | 288.7 | | | 288.7 | 288.7 |
| -11.50 | 346.2 | | | 346.2 | 346.2 |
| -12.00 | 403.7 | | | 403.7 | 403.7 |
| -12.50 | 461.1 | | | 461.1 | 461.1 |
| -13.00 | 518.6 | | | 518.6 | 518.6 |
| -13.50 | 576.1 | | | 576.1 | 576.1 |
| -14.00 | 633.5 | | | 633.5 | 633.5 |
| -14.50 | 691.0 | | | 691.0 | 691.0 |
| -15.00 | 744.4 | | | 744.4 | 744.4 |
| -15.50 | 801.9 | | | 801.9 | 801.9 |
| -16.00 | 859.3 | | | 859.3 | 859.3 |
| -16.50 | 916.8 | | | 916.8 | 916.8 |
| -17.00 | 972.1 | | | 972.1 | 972.1 |
| -17.50 | 1031.5 | | | 1031.5 | 1031.5 |
| -18.00 | 1100.0 | | | 1100.0 | 1100.0 |
| -18.50 | 1146.7 | | | 1146.7 | 1146.7 |
| -19.00 | 1187.4 | | | 1187.4 | 1187.4 |
| -19.50 | 1233.9 | | | 1233.9 | 1233.9 |
| -20.00 | 1280.9 | | | 1280.9 | 1280.9 |
| -20.50 | 1330.5 | | | 1330.5 | 1330.5 |
| -21.00 | 1381.6 | | | 1381.6 | 1381.6 |
| -21.50 | 1439.2 | | | 1439.2 | 1439.2 |
| -22.00 | 1488.8 | 1488.8 | 1488.8 | | |
| -22.50 | 1546.2 | 1546.2 | 1546.2 | | |
| -23.00 | 1603.7 | 1603.7 | 1603.7 | | |
| -23.50 | 1661.2 | 1661.2 | 1661.2 | | |
| -24.00 | 1714.6 | 1714.6 | 1714.6 | | |
| -24.50 | 1761.1 | 1761.1 | 1761.1 | | |
| -25.00 | 1797.8 | 1797.8 | 1797.8 | | |
| -25.50 | 1833.4 | 1833.4 | 1833.4 | | |
| -26.00 | 1868.3 | 1868.3 | 1868.3 | | |
| -26.50 | 1903.1 | 1903.1 | 1903.1 | | |
| -27.00 | 1943.9 | 1943.9 | 1943.9 | | |
| -27.50 | 1987.5 | 1987.5 | 1987.5 | | |
| -28.00 | 2032.1 | 2032.1 | 2032.1 | | |
| -28.50 | 2078.6 | 2078.6 | 2078.6 | | |
| -29.00 | 2127.3 | 2127.3 | 2127.3 | | |
| -29.50 | 2142.8 | 2142.8 | 2142.8 | | |
| -30.00 | 2180.3 | 2180.3 | 2180.3 | | |
| 19-1008_20 | -0.03 | -7.00 | 169.9 | 169.9 | 169.9 |
| | | -7.50 | 201.8 | 201.8 | 201.8 |
| | | -8.00 | 227.1 | 227.1 | 227.1 |
| | | -8.50 | 251.7 | 251.7 | 251.7 |
| | | -9.00 | 285.0 | 285.0 | 285.0 |
| | | -9.50 | 312.4 | 312.4 | 312.4 |
| | | -10.00 | 343.6 | 343.6 | 343.6 |
| | | -10.50 | 352.9 | 352.9 | 352.9 |
| | | -11.00 | 393.0 | 393.0 | 393.0 |
| | | -11.50 | 435.8 | 435.8 | 435.8 |
| | | -12.00 | 446.2 | 446.2 | 446.2 |
| | | -12.50 | 457.6 | 457.6 | 457.6 |
| | | -13.00 | 477.5 | 477.5 | 477.5 |
| | | -13.50 | 487.7 | 487.7 | 487.7 |
| | | -14.00 | 505.5 | 505.5 | 505.5 |
| -14.50 | 536.4 | 536.4 | 536.4 | | |
| -15.00 | 571.3 | 571.3 | 571.3 | | |
| -15.50 | 592.0 | 592.0 | 592.0 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,ca1}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_20 | -0.03 | -16.00 | 608.1 | 608.1 | 608.1 |
| | | -16.50 | 630.0 | 630.0 | 630.0 |
| | | -17.00 | 645.0 | 645.0 | 645.0 |
| | | -17.50 | 662.9 | 662.9 | 662.9 |
| | | -18.00 | 694.2 | 694.2 | 694.2 |
| | | -18.50 | 730.4 | 730.4 | 730.4 |
| | | -19.00 | 758.1 | 758.1 | 758.1 |
| | | -19.50 | 794.6 | 794.6 | 794.6 |
| | | -20.00 | 832.3 | 832.3 | 832.3 |
| | | -20.50 | 879.9 | 879.9 | 879.9 |
| | | -21.00 | 943.0 | 943.0 | 943.0 |
| | | -21.50 | 971.1 | 971.1 | 971.1 |
| | | -22.00 | 990.5 | 990.5 | 990.5 |
| | | -22.50 | 1011.4 | 1011.4 | 1011.4 |
| | | -23.00 | 1028.7 | 1028.7 | 1028.7 |
| | | -23.50 | 1060.2 | 1060.2 | 1060.2 |
| | | -24.00 | 1095.1 | 1095.1 | 1095.1 |
| | | -24.50 | 1131.6 | 1131.6 | 1131.6 |
| | | -25.00 | 1176.0 | 1176.0 | 1176.0 |
| | | -25.50 | 1216.5 | 1216.5 | 1216.5 |
| | | -26.00 | 1256.2 | 1256.2 | 1256.2 |
| | | -26.50 | 1292.2 | 1292.2 | 1292.2 |
| | | -27.00 | 1335.9 | 1335.9 | 1335.9 |
| | | -27.50 | 1374.4 | 1374.4 | 1374.4 |
| | | -28.00 | 1409.4 | 1409.4 | 1409.4 |
| | | -28.50 | 1450.0 | 1450.0 | 1450.0 |
| | | -29.00 | 1487.9 | 1487.9 | 1487.9 |
| | | -29.50 | 1518.8 | 1518.8 | 1518.8 |
| | | -30.00 | 1557.2 | 1557.2 | 1557.2 |
| | | 19-1008_21 | 1.78 | -7.00 | 270.9 |
| -7.50 | 316.4 | | | 316.4 | 316.4 |
| -8.00 | 359.3 | | | 359.3 | 359.3 |
| -8.50 | 402.8 | | | 402.8 | 402.8 |
| -9.00 | 426.3 | | | 426.3 | 426.3 |
| -9.50 | 444.7 | | | 444.7 | 444.7 |
| -10.00 | 471.3 | | | 471.3 | 471.3 |
| -10.50 | 495.0 | | | 495.0 | 495.0 |
| -11.00 | 521.8 | | | 521.8 | 521.8 |
| -11.50 | 555.0 | | | 555.0 | 555.0 |
| -12.00 | 592.0 | | | 592.0 | 592.0 |
| -12.50 | 621.0 | | | 621.0 | 621.0 |
| -13.00 | 654.1 | | | 654.1 | 654.1 |
| -13.50 | 690.5 | | | 690.5 | 690.5 |
| -14.00 | 743.4 | | | 743.4 | 743.4 |
| -14.50 | 796.4 | | | 796.4 | 796.4 |
| -15.00 | 836.0 | | | 836.0 | 836.0 |
| -15.50 | 867.3 | | | 867.3 | 867.3 |
| -16.00 | 923.0 | | | 923.0 | 923.0 |
| -16.50 | 978.9 | | | 978.9 | 978.9 |
| -17.00 | 990.2 | | | 990.2 | 990.2 |
| -17.50 | 1003.0 | | | 1003.0 | 1003.0 |
| -18.00 | 1025.2 | | | 1025.2 | 1025.2 |
| -18.50 | 1085.9 | | | 1085.9 | 1085.9 |
| -19.00 | 1128.2 | | | 1128.2 | 1128.2 |
| -19.50 | 1140.9 | | | 1140.9 | 1140.9 |
| -20.00 | 1151.4 | | | 1151.4 | 1151.4 |
| -20.50 | 1161.8 | | | 1161.8 | 1161.8 |
| -21.00 | 1172.3 | | | 1172.3 | 1172.3 |
| -21.50 | 1184.5 | | | 1184.5 | 1184.5 |
| -22.00 | 1198.2 | 1198.2 | 1198.2 | | |
| -22.50 | 1214.5 | 1214.5 | 1214.5 | | |
| -23.00 | 1230.6 | 1230.6 | 1230.6 | | |
| -23.50 | 1246.2 | 1246.2 | 1246.2 | | |
| -24.00 | 1264.2 | 1264.2 | 1264.2 | | |
| -24.50 | 1282.6 | 1282.6 | 1282.6 | | |
| -25.00 | 1301.9 | 1301.9 | 1301.9 | | |
| -25.50 | 1322.1 | 1322.1 | 1322.1 | | |
| -26.00 | 1341.4 | 1341.4 | 1341.4 | | |
| -26.50 | 1359.2 | 1359.2 | 1359.2 | | |
| -27.00 | 1377.4 | 1377.4 | 1377.4 | | |
| -27.50 | 1395.3 | 1395.3 | 1395.3 | | |
| -28.00 | 1414.4 | 1414.4 | 1414.4 | | |
| -28.50 | 1434.0 | 1434.0 | 1434.0 | | |
| -29.00 | 1453.2 | 1453.2 | 1453.2 | | |
| -29.50 | 1473.1 | 1473.1 | 1473.1 | | |
| -30.00 | 1494.3 | 1494.3 | 1494.3 | | |
| 251.S01 | -1.05 | -7.00 | 322.4 | 322.4 | 322.4 |
| | | -7.50 | 367.5 | 367.5 | 367.5 |
| | | -8.00 | 409.1 | 409.1 | 409.1 |
| | | -8.50 | 437.9 | 437.9 | 437.9 |
| | | -9.00 | 444.3 | 444.3 | 444.3 |
| | | -9.50 | 471.1 | 471.1 | 471.1 |
| | | -10.00 | 510.5 | 510.5 | 510.5 |
| | | -10.50 | 556.3 | 556.3 | 556.3 |
| | | -11.00 | 591.8 | 591.8 | 591.8 |
| | | -11.50 | 614.3 | 614.3 | 614.3 |
| | | -12.00 | 636.6 | 636.6 | 636.6 |
| | | -12.50 | 672.9 | 672.9 | 672.9 |
| | | -13.00 | 715.4 | 715.4 | 715.4 |
| | | -13.50 | 755.6 | 755.6 | 755.6 |
| | | -14.00 | 810.4 | 810.4 | 810.4 |
| -14.50 | 864.9 | 864.9 | 864.9 | | |
| -15.00 | 923.7 | 923.7 | 923.7 | | |
| -15.50 | 951.4 | 951.4 | 951.4 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|-----------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,ca1}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 251.S01 | -1.05 | -16.00 | 1004.7 | 1004.7 | 1004.7 |
| | | -16.50 | 1062.2 | 1062.2 | 1062.2 |
| | | -17.00 | 1119.1 | 1119.1 | 1119.1 |
| | | -17.50 | 1173.5 | 1173.5 | 1173.5 |
| | | -18.00 | 1225.0 | 1225.0 | 1225.0 |
| | | -18.50 | 1282.4 | 1282.4 | 1282.4 |
| | | -19.00 | 1317.9 | 1317.9 | 1317.9 |
| | | -19.50 | 1355.7 | 1355.7 | 1355.7 |
| | | -20.00 | 1400.9 | 1400.9 | 1400.9 |
| | | -20.50 | 1463.3 | 1463.3 | 1463.3 |
| | | -21.00 | 1528.8 | 1528.8 | 1528.8 |
| | | -21.50 | 1557.4 | 1557.4 | 1557.4 |
| | | -22.00 | 1568.0 | 1568.0 | 1568.0 |
| | | -22.50 | 1581.3 | 1581.3 | 1581.3 |
| | | -23.00 | 1601.1 | 1601.1 | 1601.1 |
| | | -23.50 | 1626.3 | 1626.3 | 1626.3 |
| | | -24.00 | 1659.4 | 1659.4 | 1659.4 |
| | | -24.50 | 1689.9 | 1689.9 | 1689.9 |
| | | -25.00 | 1717.7 | 1717.7 | 1717.7 |
| | | -25.50 | 1765.7 | 1765.7 | 1765.7 |
| | | -26.00 | 1835.0 | 1835.0 | 1835.0 |
| | | -26.50 | 1902.8 | 1902.8 | 1902.8 |
| | | -27.00 | 1960.3 | 1960.3 | 1960.3 |
| | | -27.50 | 2017.7 | 2017.7 | 2017.7 |
| | | -28.00 | 2075.2 | 2075.2 | 2075.2 |
| | | -28.50 | 2132.7 | 2132.7 | 2132.7 |
| | | -29.00 | 2190.1 | 2190.1 | 2190.1 |
| | | -29.50 | 2229.9 | 2229.9 | 2229.9 |
| | | -30.00 | 2276.4 | 2276.4 | 2276.4 |
| | | 19-1008_29 | 0.79 | -7.00 | 438.4 |
| -7.50 | 487.8 | | | 487.8 | 487.8 |
| -8.00 | 540.5 | | | 540.5 | 540.5 |
| -8.50 | 593.0 | | | 593.0 | 593.0 |
| -9.00 | 638.9 | | | 638.9 | 638.9 |
| -9.50 | 681.9 | | | 681.9 | 681.9 |
| -10.00 | 722.3 | | | 722.3 | 722.3 |
| -10.50 | 768.9 | | | 768.9 | 768.9 |
| -11.00 | 815.1 | | | 815.1 | 815.1 |
| -11.50 | 866.5 | | | 866.5 | 866.5 |
| -12.00 | 891.9 | | | 891.9 | 891.9 |
| -12.50 | 945.6 | | | 945.6 | 945.6 |
| -13.00 | 987.2 | | | 987.2 | 987.2 |
| -13.50 | 1005.7 | | | 1005.7 | 1005.7 |
| -14.00 | 1027.1 | | | 1027.1 | 1027.1 |
| -14.50 | 1042.7 | | | 1042.7 | 1042.7 |
| -15.00 | 1056.4 | | | 1056.4 | 1056.4 |
| -15.50 | 1072.4 | | | 1072.4 | 1072.4 |
| -16.00 | 1110.2 | | | 1110.2 | 1110.2 |
| -16.50 | 1125.4 | | | 1125.4 | 1125.4 |
| -17.00 | 1140.8 | | | 1140.8 | 1140.8 |
| -17.50 | 1161.8 | | | 1161.8 | 1161.8 |
| -18.00 | 1210.1 | | | 1210.1 | 1210.1 |
| -18.50 | 1267.6 | | | 1267.6 | 1267.6 |
| -19.00 | 1324.5 | | | 1324.5 | 1324.5 |
| -19.50 | 1368.2 | | | 1368.2 | 1368.2 |
| -20.00 | 1425.7 | | | 1425.7 | 1425.7 |
| -20.50 | 1483.2 | | | 1483.2 | 1483.2 |
| -21.00 | 1540.6 | | | 1540.6 | 1540.6 |
| -21.50 | 1598.1 | | | 1598.1 | 1598.1 |
| -22.00 | 1655.6 | 1655.6 | 1655.6 | | |
| -22.50 | 1721.9 | 1721.9 | 1721.9 | | |
| -23.00 | 1772.6 | 1772.6 | 1772.6 | | |
| -23.50 | 1807.7 | 1807.7 | 1807.7 | | |
| -24.00 | 1848.5 | 1848.5 | 1848.5 | | |
| -24.50 | 1890.1 | 1890.1 | 1890.1 | | |
| -25.00 | 1934.1 | 1934.1 | 1934.1 | | |
| -25.50 | 1962.3 | 1962.3 | 1962.3 | | |
| -26.00 | 1994.4 | 1994.4 | 1994.4 | | |
| -26.50 | 2024.5 | 2024.5 | 2024.5 | | |
| -27.00 | 2061.6 | 2061.6 | 2061.6 | | |
| -27.50 | 2090.3 | 2090.3 | 2090.3 | | |
| -28.00 | 2118.3 | 2118.3 | 2118.3 | | |
| -28.50 | 2146.2 | 2146.2 | 2146.2 | | |
| -29.00 | 2176.6 | 2176.6 | 2176.6 | | |
| -29.50 | 2223.3 | 2223.3 | 2223.3 | | |
| -30.00 | 2264.1 | 2264.1 | 2264.1 | | |
| 283.S02 | 0.17 | -7.00 | 359.9 | 359.9 | 359.9 |
| | | -7.50 | 392.4 | 392.4 | 392.4 |
| | | -8.00 | 424.6 | 424.6 | 424.6 |
| | | -8.50 | 463.2 | 463.2 | 463.2 |
| | | -9.00 | 498.9 | 498.9 | 498.9 |
| | | -9.50 | 529.6 | 529.6 | 529.6 |
| | | -10.00 | 563.8 | 563.8 | 563.8 |
| | | -10.50 | 596.9 | 596.9 | 596.9 |
| | | -11.00 | 629.2 | 629.2 | 629.2 |
| | | -11.50 | 663.8 | 663.8 | 663.8 |
| | | -12.00 | 686.9 | 686.9 | 686.9 |
| | | -12.50 | 725.1 | 725.1 | 725.1 |
| | | -13.00 | 767.4 | 767.4 | 767.4 |
| | | -13.50 | 814.2 | 814.2 | 814.2 |
| | | -14.00 | 869.2 | 869.2 | 869.2 |
| -14.50 | 924.1 | 924.1 | 924.1 | | |
| -15.00 | 973.6 | 973.6 | 973.6 | | |
| -15.50 | 1016.2 | 1016.2 | 1016.2 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bewijkdraagvermogen | | |
|-----------|--------------------|--------------------|---------------------|-------------------|-------------------------|
| | | | $R_{t,ca1}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 283.S02 | 0.17 | -16.00 | 1062.7 | 1062.7 | 1062.7 |
| | | -16.50 | 1114.2 | 1114.2 | 1114.2 |
| | | -17.00 | 1169.2 | 1169.2 | 1169.2 |
| | | -17.50 | 1226.7 | 1226.7 | 1226.7 |
| | | -18.00 | 1284.2 | 1284.2 | 1284.2 |
| | | -18.50 | 1341.7 | 1341.7 | 1341.7 |
| | | -19.00 | 1399.1 | 1399.1 | 1399.1 |
| | | -19.50 | 1456.6 | 1456.6 | 1456.6 |
| | | -20.00 | 1514.1 | 1514.1 | 1514.1 |
| | | -20.50 | 1569.2 | 1569.2 | 1569.2 |
| | | -21.00 | 1626.6 | 1626.6 | 1626.6 |
| | | -21.50 | 1684.1 | 1684.1 | 1684.1 |
| | | -22.00 | 1741.6 | 1741.6 | 1741.6 |
| | | -22.50 | 1799.0 | 1799.0 | 1799.0 |
| | | -23.00 | 1856.5 | 1856.5 | 1856.5 |
| | | -23.50 | 1914.0 | 1914.0 | 1914.0 |
| | | -24.00 | 1971.5 | 1971.5 | 1971.5 |
| | | -24.50 | 2028.9 | 2028.9 | 2028.9 |
| | | -25.00 | 2086.4 | 2086.4 | 2086.4 |
| | | -25.50 | 2143.9 | 2143.9 | 2143.9 |
| | | -26.00 | 2201.3 | 2201.3 | 2201.3 |
| | | -26.50 | 2263.0 | 2263.0 | 2263.0 |
| | | -27.00 | 2285.5 | 2285.5 | 2285.5 |
| | | -27.50 | 2307.1 | 2307.1 | 2307.1 |
| | | -28.00 | 2333.5 | 2333.5 | 2333.5 |
| | | -28.50 | 2366.3 | 2366.3 | 2366.3 |
| | | -29.00 | 2390.5 | 2390.5 | 2390.5 |
| | | -29.50 | 2412.0 | 2412.0 | 2412.0 |
| | | -30.00 | 2432.2 | 2432.2 | 2432.2 |
| | | 19-1008_35 | 0.92 | -7.00 | 357.3 |
| -7.50 | 379.6 | | | 379.6 | 379.6 |
| -8.00 | 409.6 | | | 409.6 | 409.6 |
| -8.50 | 439.8 | | | 439.8 | 439.8 |
| -9.00 | 463.5 | | | 463.5 | 463.5 |
| -9.50 | 487.3 | | | 487.3 | 487.3 |
| -10.00 | 515.6 | | | 515.6 | 515.6 |
| -10.50 | 542.2 | | | 542.2 | 542.2 |
| -11.00 | 586.3 | | | 586.3 | 586.3 |
| -11.50 | 624.2 | | | 624.2 | 624.2 |
| -12.00 | 651.2 | | | 651.2 | 651.2 |
| -12.50 | 674.8 | | | 674.8 | 674.8 |
| -13.00 | 705.5 | | | 705.5 | 705.5 |
| -13.50 | 741.3 | | | 741.3 | 741.3 |
| -14.00 | 778.6 | | | 778.6 | 778.6 |
| -14.50 | 823.8 | | | 823.8 | 823.8 |
| -15.00 | 869.1 | | | 869.1 | 869.1 |
| -15.50 | 914.9 | | | 914.9 | 914.9 |
| -16.00 | 961.7 | | | 961.7 | 961.7 |
| -16.50 | 1008.8 | | | 1008.8 | 1008.8 |
| -17.00 | 1049.6 | | | 1049.6 | 1049.6 |
| -17.50 | 1084.5 | | | 1084.5 | 1084.5 |
| -18.00 | 1130.2 | | | 1130.2 | 1130.2 |
| -18.50 | 1171.7 | | | 1171.7 | 1171.7 |
| -19.00 | 1218.2 | | | 1218.2 | 1218.2 |
| -19.50 | 1264.2 | | | 1264.2 | 1264.2 |
| -20.00 | 1311.5 | | | 1311.5 | 1311.5 |
| -20.50 | 1369.2 | | | 1369.2 | 1369.2 |
| -21.00 | 1426.6 | | | 1426.6 | 1426.6 |
| -21.50 | 1484.1 | | | 1484.1 | 1484.1 |
| -22.00 | 1540.2 | 1540.2 | 1540.2 | | |
| -22.50 | 1597.7 | 1597.7 | 1597.7 | | |
| -23.00 | 1655.2 | 1655.2 | 1655.2 | | |
| -23.50 | 1712.6 | 1712.6 | 1712.6 | | |
| -24.00 | 1770.1 | 1770.1 | 1770.1 | | |
| -24.50 | 1826.6 | 1826.6 | 1826.6 | | |
| -25.00 | 1880.9 | 1880.9 | 1880.9 | | |
| -25.50 | 1942.5 | 1942.5 | 1942.5 | | |
| -26.00 | 2000.4 | 2000.4 | 2000.4 | | |
| -26.50 | 2051.1 | 2051.1 | 2051.1 | | |
| -27.00 | 2108.5 | 2108.5 | 2108.5 | | |
| -27.50 | 2166.0 | 2166.0 | 2166.0 | | |
| -28.00 | 2223.5 | 2223.5 | 2223.5 | | |
| -28.50 | 2280.9 | 2280.9 | 2280.9 | | |
| -29.00 | 2338.4 | 2338.4 | 2338.4 | | |
| -29.50 | 2395.9 | 2395.9 | 2395.9 | | |
| -30.00 | 2453.4 | 2453.4 | 2453.4 | | |
| 312.S03 | 3.78 | -7.00 | 461.4 | 461.4 | 461.4 |
| | | -7.50 | 493.5 | 493.5 | 493.5 |
| | | -8.00 | 528.6 | 528.6 | 528.6 |
| | | -8.50 | 586.1 | 586.1 | 586.1 |
| | | -9.00 | 643.5 | 643.5 | 643.5 |
| | | -9.50 | 701.0 | 701.0 | 701.0 |
| | | -10.00 | 758.5 | 758.5 | 758.5 |
| | | -10.50 | 815.7 | 815.7 | 815.7 |
| | | -11.00 | 870.2 | 870.2 | 870.2 |
| | | -11.50 | 927.7 | 927.7 | 927.7 |
| | | -12.00 | 985.1 | 985.1 | 985.1 |
| | | -12.50 | 1042.6 | 1042.6 | 1042.6 |
| | | -13.00 | 1098.6 | 1098.6 | 1098.6 |
| | | -13.50 | 1140.1 | 1140.1 | 1140.1 |
| | | -14.00 | 1186.6 | 1186.6 | 1186.6 |
| -14.50 | 1233.1 | 1233.1 | 1233.1 | | |
| -15.00 | 1278.1 | 1278.1 | 1278.1 | | |
| -15.50 | 1324.5 | 1324.5 | 1324.5 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|-----------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 312.S03 | 3.78 | -16.00 | 1369.8 | 1369.8 | 1369.8 |
| | | -16.50 | 1416.3 | 1416.3 | 1416.3 |
| | | -17.00 | 1459.5 | 1459.5 | 1459.5 |
| | | -17.50 | 1493.7 | 1493.7 | 1493.7 |
| | | -18.00 | 1530.3 | 1530.3 | 1530.3 |
| | | -18.50 | 1575.6 | 1575.6 | 1575.6 |
| | | -19.00 | 1623.4 | 1623.4 | 1623.4 |
| | | -19.50 | 1672.6 | 1672.6 | 1672.6 |
| | | -20.00 | 1720.2 | 1720.2 | 1720.2 |
| | | -20.50 | 1762.3 | 1762.3 | 1762.3 |
| | | -21.00 | 1808.2 | 1808.2 | 1808.2 |
| | | -21.50 | 1851.2 | 1851.2 | 1851.2 |
| | | -22.00 | 1899.5 | 1899.5 | 1899.5 |
| | | -22.50 | 1955.6 | 1955.6 | 1955.6 |
| | | -23.00 | 2012.1 | 2012.1 | 2012.1 |
| | | -23.50 | 2067.0 | 2067.0 | 2067.0 |
| | | -24.00 | 2117.7 | 2117.7 | 2117.7 |
| | | -24.50 | 2175.2 | 2175.2 | 2175.2 |
| | | -25.00 | 2232.6 | 2232.6 | 2232.6 |
| | | -25.50 | 2286.8 | 2286.8 | 2286.8 |
| | | -26.00 | 2335.4 | 2335.4 | 2335.4 |
| | | -26.50 | 2391.7 | 2391.7 | 2391.7 |
| | | -27.00 | 2448.0 | 2448.0 | 2448.0 |
| | | -27.50 | 2479.9 | 2479.9 | 2479.9 |
| | | -28.00 | 2505.3 | 2505.3 | 2505.3 |
| | | -28.50 | 2525.3 | 2525.3 | 2525.3 |
| | | -29.00 | 2545.0 | 2545.0 | 2545.0 |
| | | -29.50 | 2567.5 | 2567.5 | 2567.5 |
| | | -30.00 | 2597.3 | 2597.3 | 2597.3 |
| | | 19-1008_43 | 9.88 | -7.00 | 353.6 |
| -7.50 | 397.2 | | | 397.2 | 397.2 |
| -8.00 | 442.4 | | | 442.4 | 442.4 |
| -8.50 | 484.7 | | | 484.7 | 484.7 |
| -9.00 | 527.9 | | | 527.9 | 527.9 |
| -9.50 | 572.1 | | | 572.1 | 572.1 |
| -10.00 | 612.6 | | | 612.6 | 612.6 |
| -10.50 | 661.0 | | | 661.0 | 661.0 |
| -11.00 | 718.5 | | | 718.5 | 718.5 |
| -11.50 | 776.0 | | | 776.0 | 776.0 |
| -12.00 | 833.4 | | | 833.4 | 833.4 |
| -12.50 | 890.5 | | | 890.5 | 890.5 |
| -13.00 | 933.6 | | | 933.6 | 933.6 |
| -13.50 | 971.0 | | | 971.0 | 971.0 |
| -14.00 | 1014.2 | | | 1014.2 | 1014.2 |
| -14.50 | 1060.7 | | | 1060.7 | 1060.7 |
| -15.00 | 1101.7 | | | 1101.7 | 1101.7 |
| -15.50 | 1152.1 | | | 1152.1 | 1152.1 |
| -16.00 | 1207.5 | | | 1207.5 | 1207.5 |
| -16.50 | 1264.9 | | | 1264.9 | 1264.9 |
| -17.00 | 1322.4 | | | 1322.4 | 1322.4 |
| -17.50 | 1377.8 | | | 1377.8 | 1377.8 |
| -18.00 | 1428.3 | | | 1428.3 | 1428.3 |
| -18.50 | 1473.7 | | | 1473.7 | 1473.7 |
| -19.00 | 1519.1 | | | 1519.1 | 1519.1 |
| -19.50 | 1556.4 | | | 1556.4 | 1556.4 |
| -20.00 | 1594.7 | | | 1594.7 | 1594.7 |
| -20.50 | 1642.5 | | | 1642.5 | 1642.5 |
| -21.00 | 1697.8 | | | 1697.8 | 1697.8 |
| -21.50 | 1743.7 | | | 1743.7 | 1743.7 |
| -22.00 | 1795.5 | 1795.5 | 1795.5 | | |
| -22.50 | 1853.0 | 1853.0 | 1853.0 | | |
| -23.00 | 1910.5 | 1910.5 | 1910.5 | | |
| -23.50 | 1967.9 | 1967.9 | 1967.9 | | |
| -24.00 | 2025.4 | 2025.4 | 2025.4 | | |
| -24.50 | 2082.9 | 2082.9 | 2082.9 | | |
| -25.00 | 2131.7 | 2131.7 | 2131.7 | | |
| 328.S02 | 10.17 | -7.00 | 543.9 | 543.9 | 543.9 |
| | | -7.50 | 584.7 | 584.7 | 584.7 |
| | | -8.00 | 629.4 | 629.4 | 629.4 |
| | | -8.50 | 675.3 | 675.3 | 675.3 |
| | | -9.00 | 720.0 | 720.0 | 720.0 |
| | | -9.50 | 758.7 | 758.7 | 758.7 |
| | | -10.00 | 802.2 | 802.2 | 802.2 |
| | | -10.50 | 847.6 | 847.6 | 847.6 |
| | | -11.00 | 899.3 | 899.3 | 899.3 |
| | | -11.50 | 952.3 | 952.3 | 952.3 |
| | | -12.00 | 1003.6 | 1003.6 | 1003.6 |
| | | -12.50 | 1050.3 | 1050.3 | 1050.3 |
| | | -13.00 | 1095.9 | 1095.9 | 1095.9 |
| | | -13.50 | 1142.0 | 1142.0 | 1142.0 |
| | | -14.00 | 1188.5 | 1188.5 | 1188.5 |
| | | -14.50 | 1233.7 | 1233.7 | 1233.7 |
| | | -15.00 | 1280.6 | 1280.6 | 1280.6 |
| | | -15.50 | 1327.1 | 1327.1 | 1327.1 |
| | | -16.00 | 1373.1 | 1373.1 | 1373.1 |
| | | -16.50 | 1421.2 | 1421.2 | 1421.2 |
| | | -17.00 | 1478.7 | 1478.7 | 1478.7 |
| | | -17.50 | 1536.1 | 1536.1 | 1536.1 |
| | | -18.00 | 1601.7 | 1601.7 | 1601.7 |
| | | -18.50 | 1643.6 | 1643.6 | 1643.6 |
| | | -19.00 | 1695.5 | 1695.5 | 1695.5 |
| | | -19.50 | 1750.7 | 1750.7 | 1750.7 |
| | | -20.00 | 1808.2 | 1808.2 | 1808.2 |
| | | -20.50 | 1865.7 | 1865.7 | 1865.7 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bewijkdraagvermogen | | | Rekenwaarden | | |
|-----------|--------------------|--------------------|----------------------|-------------------|-------------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,calc}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] | $R_{t,calc}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 328.S02 | 10.17 | -21.00 | 1923.2 | 1923.2 | 1923.2 | 1923.2 | 1923.2 | |
| | | -21.50 | 1980.6 | 1980.6 | 1980.6 | 1980.6 | 1980.6 | |
| | | -22.00 | 2038.1 | 2038.1 | 2038.1 | 2038.1 | 2038.1 | |
| | | -22.50 | 2095.6 | 2095.6 | 2095.6 | 2095.6 | 2095.6 | |
| | | -23.00 | 2153.0 | 2153.0 | 2153.0 | 2153.0 | 2153.0 | |
| | | -23.50 | 2210.5 | 2210.5 | 2210.5 | 2210.5 | 2210.5 | |
| | | -24.00 | 2268.0 | 2268.0 | 2268.0 | 2268.0 | 2268.0 | |
| | | -24.50 | 2316.9 | 2316.9 | 2316.9 | 2316.9 | 2316.9 | |
| | | -25.00 | 2363.4 | 2363.4 | 2363.4 | 2363.4 | 2363.4 | |
| | | -25.50 | 2409.2 | 2409.2 | 2409.2 | 2409.2 | 2409.2 | |
| | | -26.00 | 2455.7 | 2455.7 | 2455.7 | 2455.7 | 2455.7 | |
| | | -26.50 | 2504.9 | 2504.9 | 2504.9 | 2504.9 | 2504.9 | |
| | | -27.00 | 2562.3 | 2562.3 | 2562.3 | 2562.3 | 2562.3 | |
| | | -27.50 | 2619.8 | 2619.8 | 2619.8 | 2619.8 | 2619.8 | |
| | | -28.00 | 2668.6 | 2668.6 | 2668.6 | 2668.6 | 2668.6 | |
| | | -28.50 | 2711.4 | 2711.4 | 2711.4 | 2711.4 | 2711.4 | |

REKENGEDEGENS SI Ø762/950 trek

Berekening : Ontwerpend
 Rekenmethode : Trekpalen volgens NEN-EN 1997-1, art. 7.6.3
 Sondering(en) : 19-1008_1, 19-1008_6, 166.S01, 19-1008_11, 19-1008_12
 : 19-1008_17, 19-1008_20, 19-1008_21, 251.S01, 19-1008_29
 : 283.S02, 19-1008_35, 312.S03, 19-1008_43, 328.S02

Let op: trekcapaciteit t.p.v. negatief kleefttraject is meegerekend.

Stijf bouwwerk : NEE
 Paalgroep : NEE
 Aantal sonderingen : 15
 Factor $\xi_{s(n-1)}$: 1.39 (handmatig)
 Factor $\xi_{s(qem)}$: 1.39 (handmatig)
 Factor $\xi_{s(min)}$: 1.39 (handmatig)
 Weerstandsfactor γ_R : 1.35
 $\gamma_{n,variabe}$: 1.50
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø762/950
 Niveau paalkop [m] : N.A.P. 0.00
 Bovenbel. [kN/m²] : 0.00

PAALPUNTNIVEAUS SI Ø762/950

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|--------------------|-------------------|--------------------|
| 1 | -8.00 | -30.00 | 0.50 |

RESULTATEN SI Ø762/950 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering | 19-1008_1 | 19-1008_6 | 166.S01 | 19-1008_11 | 19-1008_12 | 19-1008_17 |
|---------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| Niveau [m] | $F_{netto,t}$ [kN] | $F_{netto,t}$ [kN] | $F_{netto,t}$ [kN] | $F_{netto,t}$ [kN] | $F_{netto,t}$ [kN] | $F_{netto,t}$ [kN] |
| -8.00 | 116 | 859 | 623 | 313 | 881 | 188 |
| -8.50 | 136 | 927 | 691 | 340 | 917 | 199 |
| -9.00 | 144 | 995 | 759 | 362 | 930 | 216 |
| -9.50 | 174 | 1063 | 825 | 383 | 941 | 230 |
| -10.00 | 202 | 1131 | 894 | 404 | 958 | 281 |
| -10.50 | 233 | 1200 | 962 | 429 | 990 | 308 |
| -11.00 | 255 | 1268 | 1030 | 458 | 1016 | 352 |
| -11.50 | 292 | 1336 | 1098 | 492 | 1024 | 420 |
| -12.00 | 338 | 1404 | 1162 | 534 | 1048 | 489 |
| -12.50 | 369 | 1473 | 1216 | 552 | 1058 | 557 |
| -13.00 | 418 | 1541 | 1266 | 601 | 1068 | 625 |
| -13.50 | 467 | 1609 | 1318 | 658 | 1078 | 693 |
| -14.00 | 510 | 1677 | 1377 | 716 | 1100 | 762 |
| -14.50 | 565 | 1745 | 1445 | 775 | 1126 | 830 |
| -15.00 | 615 | 1814 | 1513 | 833 | 1146 | 893 |
| -15.50 | 670 | 1882 | 1581 | 889 | 1162 | 961 |
| -16.00 | 718 | 1950 | 1649 | 936 | 1187 | 1030 |
| -16.50 | 770 | 2018 | 1718 | 990 | 1219 | 1098 |
| -17.00 | 822 | 2087 | 1786 | 1043 | 1246 | 1164 |
| -17.50 | 884 | 2155 | 1854 | 1094 | 1285 | 1234 |
| -18.00 | 952 | 2223 | 1922 | 1156 | 1316 | 1315 |
| -18.50 | 1020 | 2287 | 1990 | 1224 | 1384 | 1371 |
| -19.00 | 1088 | 2355 | 2059 | 1292 | 1446 | 1419 |
| -19.50 | 1157 | 2423 | 2127 | 1361 | 1502 | 1475 |
| -20.00 | 1242 | 2492 | 2195 | 1429 | 1552 | 1530 |
| -20.50 | 1329 | 2560 | 2263 | 1497 | 1607 | 1589 |
| -21.00 | 1419 | 2628 | 2332 | 1565 | 1659 | 1650 |
| -21.50 | 1483 | 2696 | 2400 | 1630 | 1722 | 1719 |
| -22.00 | 1551 | 2764 | 2468 | 1698 | 1789 | 1777 |
| -22.50 | 1619 | 2833 | 2536 | 1766 | 1856 | 1846 |
| -23.00 | 1688 | 2901 | 0 | 1829 | 1918 | 1914 |
| -23.50 | 1756 | 2969 | 0 | 1871 | 1978 | 1982 |
| -24.00 | 1824 | 0 | 0 | 1925 | 2041 | 2046 |
| -24.50 | 1892 | 0 | 0 | 1986 | 2109 | 2101 |
| -25.00 | 1960 | 0 | 0 | 2044 | 2178 | 2145 |
| -25.50 | 2029 | 0 | 0 | 2093 | 2267 | 2187 |
| -26.00 | 2097 | 0 | 0 | 2162 | 2356 | 2229 |
| -26.50 | 2165 | 0 | 0 | 2230 | 2409 | 2270 |
| -27.00 | 2233 | 0 | 0 | 2298 | 2459 | 2319 |
| -27.50 | 2302 | 0 | 0 | 2366 | 2515 | 2371 |
| -28.00 | 2370 | 0 | 0 | 2435 | 2557 | 2424 |
| -28.50 | 2438 | 0 | 0 | 2503 | 2610 | 2479 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

| | | | | | | |
|--------|------|---|---|------|------|------|
| -29.00 | 2506 | 0 | 0 | 2571 | 2678 | 2537 |
| -29.50 | 2574 | 0 | 0 | 2639 | 2746 | 2556 |
| -30.00 | 2643 | 0 | 0 | 2708 | 2813 | 2600 |

RESULTATEN SI Ø762/950 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering | 19-1008_20 | 19-1008_21 | 251.801 | 19-1008_29 | 283.502 | 19-1008_35 |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| Niveau [m] | F _{nettozt} [kN] | F _{nettozt} [kN] | F _{nettozt} [kN] | F _{nettozt} [kN] | F _{nettozt} [kN] | F _{nettozt} [kN] |
| -8.00 | 277 | 432 | 492 | 645 | 509 | 491 |
| -8.50 | 306 | 483 | 527 | 708 | 555 | 527 |
| -9.00 | 346 | 512 | 535 | 762 | 598 | 555 |
| -9.50 | 379 | 534 | 567 | 813 | 635 | 584 |
| -10.00 | 416 | 566 | 614 | 861 | 675 | 618 |
| -10.50 | 428 | 594 | 668 | 917 | 715 | 650 |
| -11.00 | 475 | 626 | 710 | 972 | 753 | 702 |
| -11.50 | 526 | 666 | 737 | 1033 | 795 | 747 |
| -12.00 | 539 | 710 | 764 | 1063 | 822 | 780 |
| -12.50 | 553 | 745 | 808 | 1127 | 868 | 808 |
| -13.00 | 577 | 784 | 858 | 1177 | 918 | 845 |
| -13.50 | 590 | 827 | 906 | 1199 | 974 | 887 |
| -14.00 | 611 | 890 | 971 | 1225 | 1039 | 932 |
| -14.50 | 648 | 953 | 1036 | 1244 | 1104 | 986 |
| -15.00 | 690 | 1000 | 1106 | 1260 | 1163 | 1039 |
| -15.50 | 714 | 1038 | 1139 | 1280 | 1214 | 1094 |
| -16.00 | 734 | 1104 | 1202 | 1325 | 1269 | 1150 |
| -16.50 | 760 | 1170 | 1270 | 1343 | 1331 | 1206 |
| -17.00 | 778 | 1184 | 1338 | 1362 | 1396 | 1254 |
| -17.50 | 800 | 1200 | 1402 | 1387 | 1464 | 1296 |
| -18.00 | 837 | 1226 | 1464 | 1445 | 1532 | 1350 |
| -18.50 | 881 | 1299 | 1532 | 1513 | 1601 | 1400 |
| -19.00 | 914 | 1349 | 1574 | 1580 | 1669 | 1455 |
| -19.50 | 957 | 1364 | 1619 | 1632 | 1737 | 1510 |
| -20.00 | 1002 | 1377 | 1673 | 1701 | 1805 | 1566 |
| -20.50 | 1059 | 1390 | 1747 | 1769 | 1871 | 1634 |
| -21.00 | 1134 | 1403 | 1825 | 1837 | 1939 | 1703 |
| -21.50 | 1167 | 1418 | 1859 | 1905 | 2007 | 1771 |
| -22.00 | 1191 | 1434 | 1872 | 1973 | 2075 | 1837 |
| -22.50 | 1216 | 1454 | 1888 | 2052 | 2144 | 1906 |
| -23.00 | 1237 | 1474 | 1912 | 2112 | 2212 | 1974 |
| -23.50 | 1274 | 1492 | 1942 | 2154 | 2280 | 2042 |
| -24.00 | 1316 | 1514 | 1982 | 2203 | 2348 | 2110 |
| -24.50 | 1359 | 1536 | 2018 | 2252 | 2416 | 2177 |
| -25.00 | 1412 | 1560 | 2051 | 2305 | 2485 | 2242 |
| -25.50 | 1460 | 1584 | 2108 | 2338 | 2553 | 2315 |
| -26.00 | 1508 | 1607 | 2191 | 2377 | 2621 | 2384 |
| -26.50 | 1551 | 1629 | 2271 | 2413 | 2694 | 2444 |
| -27.00 | 1603 | 1651 | 2339 | 2457 | 2721 | 2512 |
| -27.50 | 1649 | 1672 | 2407 | 2491 | 2747 | 2580 |
| -28.00 | 1690 | 1695 | 2476 | 2525 | 2779 | 2649 |
| -28.50 | 1739 | 1719 | 2544 | 2558 | 2818 | 2717 |
| -29.00 | 1784 | 1742 | 2612 | 2595 | 2847 | 2785 |
| -29.50 | 1821 | 1766 | 2659 | 2650 | 2873 | 2853 |
| -30.00 | 1867 | 1792 | 2715 | 2699 | 2897 | 2921 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

RESULTATEN SI Ø762/950 trek (n=1)

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Sondering 312.S03 19-1008_43 328.S02

| Niveau [m] | F _{netto,t} [kN] | F _{netto,t} [kN] | F _{netto,t} [kN] |
|---------------|------------------------------|------------------------------|------------------------------|
| -8.00 | 631 | 529 | 750 |
| -8.50 | 699 | 580 | 804 |
| -9.00 | 767 | 631 | 858 |
| -9.50 | 836 | 684 | 904 |
| -10.00 | 904 | 732 | 955 |
| -10.50 | 972 | 790 | 1009 |
| -11.00 | 1037 | 858 | 1071 |
| -11.50 | 1105 | 926 | 1134 |
| -12.00 | 1173 | 994 | 1195 |
| -12.50 | 1241 | 1062 | 1250 |
| -13.00 | 1308 | 1113 | 1305 |
| -13.50 | 1357 | 1158 | 1359 |
| -14.00 | 1412 | 1209 | 1415 |
| -14.50 | 1468 | 1265 | 1468 |
| -15.00 | 1521 | 1313 | 1524 |
| -15.50 | 1577 | 1373 | 1579 |
| -16.00 | 1630 | 1439 | 1634 |
| -16.50 | 1686 | 1507 | 1691 |
| -17.00 | 1737 | 1576 | 1760 |
| -17.50 | 1778 | 1641 | 1828 |
| -18.00 | 1822 | 1701 | 1906 |
| -18.50 | 1875 | 1755 | 1956 |
| -19.00 | 1932 | 1809 | 2017 |
| -19.50 | 1991 | 1854 | 2083 |
| -20.00 | 2047 | 1899 | 2151 |
| -20.50 | 2097 | 1956 | 2219 |
| -21.00 | 2152 | 2022 | 2287 |
| -21.50 | 2203 | 2077 | 2356 |
| -22.00 | 2261 | 2138 | 2424 |
| -22.50 | 2327 | 2206 | 2492 |
| -23.00 | 2394 | 2275 | 2560 |
| -23.50 | 2460 | 2343 | 2629 |
| -24.00 | 2520 | 2411 | 2697 |
| -24.50 | 2588 | 2479 | 2755 |
| -25.00 | 2656 | 2537 | 2810 |
| -25.50 | 2721 | 0 | 2865 |
| -26.00 | 2778 | 0 | 2920 |
| -26.50 | 2845 | 0 | 2978 |
| -27.00 | 2912 | 0 | 3047 |
| -27.50 | 2950 | 0 | 3115 |
| -28.00 | 2980 | 0 | 3173 |
| -28.50 | 3005 | 0 | 3224 |
| -29.00 | 3028 | 0 | 0 |
| -29.50 | 3055 | 0 | 0 |
| -30.00 | 3091 | 0 | 0 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

SAMENVATTINGSTABEL SI Ø762/950 trek (n=1)
Uitgangspunten

- paal : SI Ø762/950
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie
 - schachtafmeting : 860 mm
 Paalklassefactor α_p : 0.63
 Factor α_s (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
 Correlatiefactor $\xi_{s(n=1)}$: 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bewijkdraagvermogen | | |
|-----------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,calc}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_1 | 2.12 | -8.00 | 116.1 | 116.1 | 116.1 |
| | | -8.50 | 135.8 | 135.8 | 135.8 |
| | | -9.00 | 144.1 | 144.1 | 144.1 |
| | | -9.50 | 174.3 | 174.3 | 174.3 |
| | | -10.00 | 201.6 | 201.6 | 201.6 |
| | | -10.50 | 233.0 | 233.0 | 233.0 |
| | | -11.00 | 255.4 | 255.4 | 255.4 |
| | | -11.50 | 291.8 | 291.8 | 291.8 |
| | | -12.00 | 337.7 | 337.7 | 337.7 |
| | | -12.50 | 369.3 | 369.3 | 369.3 |
| | | -13.00 | 418.3 | 418.3 | 418.3 |
| | | -13.50 | 467.1 | 467.1 | 467.1 |
| | | -14.00 | 509.6 | 509.6 | 509.6 |
| | | -14.50 | 564.6 | 564.6 | 564.6 |
| | | -15.00 | 615.4 | 615.4 | 615.4 |
| | | -15.50 | 670.3 | 670.3 | 670.3 |
| | | -16.00 | 717.7 | 717.7 | 717.7 |
| | | -16.50 | 769.7 | 769.7 | 769.7 |
| | | -17.00 | 822.5 | 822.5 | 822.5 |
| | | -17.50 | 883.7 | 883.7 | 883.7 |
| | | -18.00 | 951.9 | 951.9 | 951.9 |
| | | -18.50 | 1020.1 | 1020.1 | 1020.1 |
| | | -19.00 | 1088.3 | 1088.3 | 1088.3 |
| | | -19.50 | 1156.5 | 1156.5 | 1156.5 |
| | | -20.00 | 1242.0 | 1242.0 | 1242.0 |
| | | -20.50 | 1328.7 | 1328.7 | 1328.7 |
| | | -21.00 | 1418.5 | 1418.5 | 1418.5 |
| | | -21.50 | 1482.9 | 1482.9 | 1482.9 |
| | | -22.00 | 1551.1 | 1551.1 | 1551.1 |
| | | -22.50 | 1619.3 | 1619.3 | 1619.3 |
| -23.00 | 1687.5 | 1687.5 | 1687.5 | | |
| -23.50 | 1755.8 | 1755.8 | 1755.8 | | |
| -24.00 | 1824.0 | 1824.0 | 1824.0 | | |
| -24.50 | 1892.2 | 1892.2 | 1892.2 | | |
| -25.00 | 1960.4 | 1960.4 | 1960.4 | | |
| -25.50 | 2028.7 | 2028.7 | 2028.7 | | |
| -26.00 | 2096.9 | 2096.9 | 2096.9 | | |
| -26.50 | 2165.1 | 2165.1 | 2165.1 | | |
| -27.00 | 2233.3 | 2233.3 | 2233.3 | | |
| -27.50 | 2301.5 | 2301.5 | 2301.5 | | |
| -28.00 | 2369.8 | 2369.8 | 2369.8 | | |
| -28.50 | 2438.0 | 2438.0 | 2438.0 | | |
| -29.00 | 2506.2 | 2506.2 | 2506.2 | | |
| -29.50 | 2574.4 | 2574.4 | 2574.4 | | |
| -30.00 | 2642.7 | 2642.7 | 2642.7 | | |
| 19-1008_6 | 11.00 | -8.00 | 858.5 | 858.5 | 858.5 |
| | | -8.50 | 926.7 | 926.7 | 926.7 |
| | | -9.00 | 995.0 | 995.0 | 995.0 |
| | | -9.50 | 1063.2 | 1063.2 | 1063.2 |
| | | -10.00 | 1131.4 | 1131.4 | 1131.4 |
| | | -10.50 | 1199.6 | 1199.6 | 1199.6 |
| | | -11.00 | 1267.8 | 1267.8 | 1267.8 |
| | | -11.50 | 1336.1 | 1336.1 | 1336.1 |
| | | -12.00 | 1404.3 | 1404.3 | 1404.3 |
| | | -12.50 | 1472.5 | 1472.5 | 1472.5 |
| | | -13.00 | 1540.7 | 1540.7 | 1540.7 |
| | | -13.50 | 1609.0 | 1609.0 | 1609.0 |
| | | -14.00 | 1677.2 | 1677.2 | 1677.2 |
| | | -14.50 | 1745.4 | 1745.4 | 1745.4 |
| | | -15.00 | 1813.6 | 1813.6 | 1813.6 |
| | | -15.50 | 1881.9 | 1881.9 | 1881.9 |
| | | -16.00 | 1950.1 | 1950.1 | 1950.1 |
| | | -16.50 | 2018.3 | 2018.3 | 2018.3 |
| | | -17.00 | 2086.5 | 2086.5 | 2086.5 |
| | | -17.50 | 2154.7 | 2154.7 | 2154.7 |
| -18.00 | 2223.0 | 2223.0 | 2223.0 | | |
| -18.50 | 2286.9 | 2286.9 | 2286.9 | | |
| -19.00 | 2355.1 | 2355.1 | 2355.1 | | |
| -19.50 | 2423.3 | 2423.3 | 2423.3 | | |
| -20.00 | 2491.6 | 2491.6 | 2491.6 | | |
| -20.50 | 2559.8 | 2559.8 | 2559.8 | | |
| -21.00 | 2628.0 | 2628.0 | 2628.0 | | |
| -21.50 | 2696.2 | 2696.2 | 2696.2 | | |
| -22.00 | 2764.5 | 2764.5 | 2764.5 | | |
| -22.50 | 2832.7 | 2832.7 | 2832.7 | | |
| -23.00 | 2900.9 | 2900.9 | 2900.9 | | |
| -23.50 | 2969.1 | 2969.1 | 2969.1 | | |
| 166.S01 | 3.45 | -8.00 | 623.2 | 623.2 | 623.2 |
| | | -8.50 | 691.0 | 691.0 | 691.0 |
| | | -9.00 | 758.6 | 758.6 | 758.6 |
| | | -9.50 | 825.4 | 825.4 | 825.4 |
| | | -10.00 | 893.6 | 893.6 | 893.6 |
| | | -10.50 | 961.8 | 961.8 | 961.8 |
| -11.00 | 1030.0 | 1030.0 | 1030.0 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 166.S01 | 3.45 | -11.50 | 1098.3 | 1098.3 | 1098.3 |
| | | -12.00 | 1161.8 | 1161.8 | 1161.8 |
| | | -12.50 | 1215.7 | 1215.7 | 1215.7 |
| | | -13.00 | 1266.5 | 1266.5 | 1266.5 |
| | | -13.50 | 1317.7 | 1317.7 | 1317.7 |
| | | -14.00 | 1376.8 | 1376.8 | 1376.8 |
| | | -14.50 | 1444.7 | 1444.7 | 1444.7 |
| | | -15.00 | 1512.9 | 1512.9 | 1512.9 |
| | | -15.50 | 1581.1 | 1581.1 | 1581.1 |
| | | -16.00 | 1649.4 | 1649.4 | 1649.4 |
| | | -16.50 | 1717.6 | 1717.6 | 1717.6 |
| | | -17.00 | 1785.8 | 1785.8 | 1785.8 |
| | | -17.50 | 1854.0 | 1854.0 | 1854.0 |
| | | -18.00 | 1922.2 | 1922.2 | 1922.2 |
| | | -18.50 | 1990.5 | 1990.5 | 1990.5 |
| | | -19.00 | 2058.7 | 2058.7 | 2058.7 |
| | | -19.50 | 2126.9 | 2126.9 | 2126.9 |
| | | -20.00 | 2195.1 | 2195.1 | 2195.1 |
| | | -20.50 | 2263.4 | 2263.4 | 2263.4 |
| | | -21.00 | 2331.6 | 2331.6 | 2331.6 |
| | | -21.50 | 2399.8 | 2399.8 | 2399.8 |
| -22.00 | 2468.0 | 2468.0 | 2468.0 | | |
| -22.50 | 2536.3 | 2536.3 | 2536.3 | | |
| 19-1008_11 | 0.62 | -8.00 | 312.7 | 312.7 | 312.7 |
| | | -8.50 | 339.9 | 339.9 | 339.9 |
| | | -9.00 | 361.6 | 361.6 | 361.6 |
| | | -9.50 | 382.6 | 382.6 | 382.6 |
| | | -10.00 | 404.1 | 404.1 | 404.1 |
| | | -10.50 | 429.3 | 429.3 | 429.3 |
| | | -11.00 | 458.1 | 458.1 | 458.1 |
| | | -11.50 | 492.1 | 492.1 | 492.1 |
| | | -12.00 | 534.0 | 534.0 | 534.0 |
| | | -12.50 | 551.9 | 551.9 | 551.9 |
| | | -13.00 | 600.9 | 600.9 | 600.9 |
| | | -13.50 | 658.0 | 658.0 | 658.0 |
| | | -14.00 | 716.0 | 716.0 | 716.0 |
| | | -14.50 | 774.6 | 774.6 | 774.6 |
| | | -15.00 | 833.3 | 833.3 | 833.3 |
| | | -15.50 | 888.6 | 888.6 | 888.6 |
| | | -16.00 | 935.6 | 935.6 | 935.6 |
| | | -16.50 | 990.4 | 990.4 | 990.4 |
| | | -17.00 | 1043.4 | 1043.4 | 1043.4 |
| | | -17.50 | 1093.6 | 1093.6 | 1093.6 |
| | | -18.00 | 1155.9 | 1155.9 | 1155.9 |
| | | -18.50 | 1224.2 | 1224.2 | 1224.2 |
| | | -19.00 | 1292.4 | 1292.4 | 1292.4 |
| | | -19.50 | 1360.6 | 1360.6 | 1360.6 |
| | | -20.00 | 1428.8 | 1428.8 | 1428.8 |
| | | -20.50 | 1497.0 | 1497.0 | 1497.0 |
| | | -21.00 | 1565.3 | 1565.3 | 1565.3 |
| | | -21.50 | 1629.8 | 1629.8 | 1629.8 |
| | | -22.00 | 1698.1 | 1698.1 | 1698.1 |
| | | -22.50 | 1766.3 | 1766.3 | 1766.3 |
| -23.00 | 1828.9 | 1828.9 | 1828.9 | | |
| -23.50 | 1871.4 | 1871.4 | 1871.4 | | |
| -24.00 | 1925.1 | 1925.1 | 1925.1 | | |
| -24.50 | 1985.6 | 1985.6 | 1985.6 | | |
| -25.00 | 2043.5 | 2043.5 | 2043.5 | | |
| -25.50 | 2092.7 | 2092.7 | 2092.7 | | |
| -26.00 | 2161.8 | 2161.8 | 2161.8 | | |
| -26.50 | 2230.0 | 2230.0 | 2230.0 | | |
| -27.00 | 2298.3 | 2298.3 | 2298.3 | | |
| -27.50 | 2366.5 | 2366.5 | 2366.5 | | |
| -28.00 | 2434.7 | 2434.7 | 2434.7 | | |
| -28.50 | 2502.9 | 2502.9 | 2502.9 | | |
| -29.00 | 2571.2 | 2571.2 | 2571.2 | | |
| -29.50 | 2639.4 | 2639.4 | 2639.4 | | |
| -30.00 | 2707.6 | 2707.6 | 2707.6 | | |
| 19-1008_12 | 3.57 | -8.00 | 880.9 | 880.9 | 880.9 |
| | | -8.50 | 917.4 | 917.4 | 917.4 |
| | | -9.00 | 930.4 | 930.4 | 930.4 |
| | | -9.50 | 940.9 | 940.9 | 940.9 |
| | | -10.00 | 958.4 | 958.4 | 958.4 |
| | | -10.50 | 990.3 | 990.3 | 990.3 |
| | | -11.00 | 1015.8 | 1015.8 | 1015.8 |
| | | -11.50 | 1023.5 | 1023.5 | 1023.5 |
| | | -12.00 | 1047.5 | 1047.5 | 1047.5 |
| | | -12.50 | 1058.4 | 1058.4 | 1058.4 |
| | | -13.00 | 1067.7 | 1067.7 | 1067.7 |
| | | -13.50 | 1078.4 | 1078.4 | 1078.4 |
| | | -14.00 | 1099.6 | 1099.6 | 1099.6 |
| | | -14.50 | 1126.3 | 1126.3 | 1126.3 |
| | | -15.00 | 1146.0 | 1146.0 | 1146.0 |
| | | -15.50 | 1162.3 | 1162.3 | 1162.3 |
| | | -16.00 | 1186.8 | 1186.8 | 1186.8 |
| | | -16.50 | 1219.0 | 1219.0 | 1219.0 |
| | | -17.00 | 1246.4 | 1246.4 | 1246.4 |
| | | -17.50 | 1285.4 | 1285.4 | 1285.4 |
| | | -18.00 | 1316.5 | 1316.5 | 1316.5 |
| -18.50 | 1383.7 | 1383.7 | 1383.7 | | |
| -19.00 | 1445.5 | 1445.5 | 1445.5 | | |
| -19.50 | 1502.5 | 1502.5 | 1502.5 | | |
| -20.00 | 1551.9 | 1551.9 | 1551.9 | | |
| -20.50 | 1607.2 | 1607.2 | 1607.2 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | |
|------------|--------------------|--------------------|----------------------|-------------------|-------------------------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 19-1008_12 | 3.57 | -21.00 | 1659.2 | 1659.2 | 1659.2 |
| | | -21.50 | 1721.6 | 1721.6 | 1721.6 |
| | | -22.00 | 1788.9 | 1788.9 | 1788.9 |
| | | -22.50 | 1856.2 | 1856.2 | 1856.2 |
| | | -23.00 | 1918.1 | 1918.1 | 1918.1 |
| | | -23.50 | 1977.8 | 1977.8 | 1977.8 |
| | | -24.00 | 2041.3 | 2041.3 | 2041.3 |
| | | -24.50 | 2109.5 | 2109.5 | 2109.5 |
| | | -25.00 | 2177.7 | 2177.7 | 2177.7 |
| | | -25.50 | 2266.7 | 2266.7 | 2266.7 |
| | | -26.00 | 2356.1 | 2356.1 | 2356.1 |
| | | -26.50 | 2409.1 | 2409.1 | 2409.1 |
| | | -27.00 | 2458.8 | 2458.8 | 2458.8 |
| | | -27.50 | 2515.3 | 2515.3 | 2515.3 |
| | | -28.00 | 2557.1 | 2557.1 | 2557.1 |
| | | -28.50 | 2609.9 | 2609.9 | 2609.9 |
| | | -29.00 | 2678.1 | 2678.1 | 2678.1 |
| | | -29.50 | 2746.3 | 2746.3 | 2746.3 |
| | | -30.00 | 2813.3 | 2813.3 | 2813.3 |
| 19-1008_17 | 0.20 | -8.00 | 188.4 | 188.4 | 188.4 |
| | | -8.50 | 198.9 | 198.9 | 198.9 |
| | | -9.00 | 216.0 | 216.0 | 216.0 |
| | | -9.50 | 229.6 | 229.6 | 229.6 |
| | | -10.00 | 280.8 | 280.8 | 280.8 |
| | | -10.50 | 307.8 | 307.8 | 307.8 |
| | | -11.00 | 352.2 | 352.2 | 352.2 |
| | | -11.50 | 420.5 | 420.5 | 420.5 |
| | | -12.00 | 488.7 | 488.7 | 488.7 |
| | | -12.50 | 556.9 | 556.9 | 556.9 |
| | | -13.00 | 625.1 | 625.1 | 625.1 |
| | | -13.50 | 693.4 | 693.4 | 693.4 |
| | | -14.00 | 761.6 | 761.6 | 761.6 |
| | | -14.50 | 829.8 | 829.8 | 829.8 |
| | | -15.00 | 893.2 | 893.2 | 893.2 |
| | | -15.50 | 961.4 | 961.4 | 961.4 |
| | | -16.00 | 1029.7 | 1029.7 | 1029.7 |
| | | -16.50 | 1097.9 | 1097.9 | 1097.9 |
| | | -17.00 | 1163.5 | 1163.5 | 1163.5 |
| | | -17.50 | 1234.0 | 1234.0 | 1234.0 |
| | | -18.00 | 1315.3 | 1315.3 | 1315.3 |
| -18.50 | 1370.8 | 1370.8 | 1370.8 | | |
| -19.00 | 1419.3 | 1419.3 | 1419.3 | | |
| -19.50 | 1474.6 | 1474.6 | 1474.6 | | |
| -20.00 | 1530.5 | 1530.5 | 1530.5 | | |
| -20.50 | 1589.4 | 1589.4 | 1589.4 | | |
| -21.00 | 1650.1 | 1650.1 | 1650.1 | | |
| -21.50 | 1718.5 | 1718.5 | 1718.5 | | |
| -22.00 | 1777.4 | 1777.4 | 1777.4 | | |
| -22.50 | 1845.6 | 1845.6 | 1845.6 | | |
| -23.00 | 1913.9 | 1913.9 | 1913.9 | | |
| -23.50 | 1982.1 | 1982.1 | 1982.1 | | |
| -24.00 | 2045.6 | 2045.6 | 2045.6 | | |
| -24.50 | 2100.8 | 2100.8 | 2100.8 | | |
| -25.00 | 2144.6 | 2144.6 | 2144.6 | | |
| -25.50 | 2187.1 | 2187.1 | 2187.1 | | |
| -26.00 | 2228.7 | 2228.7 | 2228.7 | | |
| -26.50 | 2270.2 | 2270.2 | 2270.2 | | |
| -27.00 | 2318.8 | 2318.8 | 2318.8 | | |
| -27.50 | 2370.7 | 2370.7 | 2370.7 | | |
| -28.00 | 2423.7 | 2423.7 | 2423.7 | | |
| -28.50 | 2479.0 | 2479.0 | 2479.0 | | |
| -29.00 | 2536.9 | 2536.9 | 2536.9 | | |
| -29.50 | 2555.7 | 2555.7 | 2555.7 | | |
| -30.00 | 2600.4 | 2600.4 | 2600.4 | | |
| 19-1008_20 | -0.03 | -8.00 | 276.7 | 276.7 | 276.7 |
| | | -8.50 | 306.3 | 306.3 | 306.3 |
| | | -9.00 | 346.0 | 346.0 | 346.0 |
| | | -9.50 | 378.7 | 378.7 | 378.7 |
| | | -10.00 | 416.1 | 416.1 | 416.1 |
| | | -10.50 | 427.6 | 427.6 | 427.6 |
| | | -11.00 | 475.3 | 475.3 | 475.3 |
| | | -11.50 | 526.3 | 526.3 | 526.3 |
| | | -12.00 | 539.0 | 539.0 | 539.0 |
| | | -12.50 | 553.0 | 553.0 | 553.0 |
| | | -13.00 | 576.9 | 576.9 | 576.9 |
| | | -13.50 | 589.5 | 589.5 | 589.5 |
| | | -14.00 | 611.0 | 611.0 | 611.0 |
| | | -14.50 | 647.9 | 647.9 | 647.9 |
| | | -15.00 | 689.5 | 689.5 | 689.5 |
| | | -15.50 | 714.4 | 714.4 | 714.4 |
| | | -16.00 | 733.9 | 733.9 | 733.9 |
| | | -16.50 | 760.2 | 760.2 | 760.2 |
| | | -17.00 | 778.4 | 778.4 | 778.4 |
| -17.50 | 800.0 | 800.0 | 800.0 | | |
| -18.00 | 837.4 | 837.4 | 837.4 | | |
| -18.50 | 880.5 | 880.5 | 880.5 | | |
| -19.00 | 913.7 | 913.7 | 913.7 | | |
| -19.50 | 957.2 | 957.2 | 957.2 | | |
| -20.00 | 1002.1 | 1002.1 | 1002.1 | | |
| -20.50 | 1058.8 | 1058.8 | 1058.8 | | |
| -21.00 | 1133.6 | 1133.6 | 1133.6 | | |
| -21.50 | 1167.2 | 1167.2 | 1167.2 | | |
| -22.00 | 1190.6 | 1190.6 | 1190.6 | | |
| -22.50 | 1215.8 | 1215.8 | 1215.8 | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | | |
|------------|--------------------|--------------------|----------------------------|--------------------------|---------------------------------|-------|-------|
| | | | R _{z,ca1} [kN] | R _{z,d} [kN] | R _{z,netto,zd} [kN] | | |
| 19-1008_20 | -0.03 | -23.00 | 1236.7 | 1236.7 | 1236.7 | | |
| | | -23.50 | 1274.3 | 1274.3 | 1274.3 | | |
| | | -24.00 | 1315.9 | 1315.9 | 1315.9 | | |
| | | -24.50 | 1359.4 | 1359.4 | 1359.4 | | |
| | | -25.00 | 1412.3 | 1412.3 | 1412.3 | | |
| | | -25.50 | 1460.5 | 1460.5 | 1460.5 | | |
| | | -26.00 | 1507.7 | 1507.7 | 1507.7 | | |
| | | -26.50 | 1550.8 | 1550.8 | 1550.8 | | |
| | | -27.00 | 1602.7 | 1602.7 | 1602.7 | | |
| | | -27.50 | 1648.6 | 1648.6 | 1648.6 | | |
| | | -28.00 | 1690.4 | 1690.4 | 1690.4 | | |
| | | -28.50 | 1738.8 | 1738.8 | 1738.8 | | |
| | | -29.00 | 1783.8 | 1783.8 | 1783.8 | | |
| | | -29.50 | 1820.8 | 1820.8 | 1820.8 | | |
| | | -30.00 | 1866.5 | 1866.5 | 1866.5 | | |
| | | 19-1008_21 | 1.78 | -8.00 | 431.6 | 431.6 | 431.6 |
| | | | | -8.50 | 483.3 | 483.3 | 483.3 |
| -9.00 | 511.6 | | | 511.6 | 511.6 | | |
| -9.50 | 533.7 | | | 533.7 | 533.7 | | |
| -10.00 | 565.6 | | | 565.6 | 565.6 | | |
| -10.50 | 594.1 | | | 594.1 | 594.1 | | |
| -11.00 | 626.2 | | | 626.2 | 626.2 | | |
| -11.50 | 665.8 | | | 665.8 | 665.8 | | |
| -12.00 | 709.9 | | | 709.9 | 709.9 | | |
| -12.50 | 744.5 | | | 744.5 | 744.5 | | |
| -13.00 | 784.1 | | | 784.1 | 784.1 | | |
| -13.50 | 827.4 | | | 827.4 | 827.4 | | |
| -14.00 | 890.3 | | | 890.3 | 890.3 | | |
| -14.50 | 953.3 | | | 953.3 | 953.3 | | |
| -15.00 | 1000.4 | | | 1000.4 | 1000.4 | | |
| -15.50 | 1037.8 | | | 1037.8 | 1037.8 | | |
| -16.00 | 1103.9 | | | 1103.9 | 1103.9 | | |
| -16.50 | 1170.3 | | | 1170.3 | 1170.3 | | |
| -17.00 | 1184.2 | | | 1184.2 | 1184.2 | | |
| -17.50 | 1199.8 | | | 1199.8 | 1199.8 | | |
| -18.00 | 1226.5 | | | 1226.5 | 1226.5 | | |
| -18.50 | 1298.5 | | | 1298.5 | 1298.5 | | |
| -19.00 | 1348.9 | | | 1348.9 | 1348.9 | | |
| -19.50 | 1364.3 | | | 1364.3 | 1364.3 | | |
| -20.00 | 1377.2 | | | 1377.2 | 1377.2 | | |
| -20.50 | 1390.0 | | | 1390.0 | 1390.0 | | |
| -21.00 | 1402.9 | | | 1402.9 | 1402.9 | | |
| -21.50 | 1417.8 | | | 1417.8 | 1417.8 | | |
| -22.00 | 1434.5 | | | 1434.5 | 1434.5 | | |
| -22.50 | 1454.1 | | | 1454.1 | 1454.1 | | |
| -23.00 | 1473.6 | | | 1473.6 | 1473.6 | | |
| -23.50 | 1492.5 | | | 1492.5 | 1492.5 | | |
| -24.00 | 1514.2 | | | 1514.2 | 1514.2 | | |
| -24.50 | 1536.5 | 1536.5 | 1536.5 | | | | |
| -25.00 | 1559.7 | 1559.7 | 1559.7 | | | | |
| -25.50 | 1584.0 | 1584.0 | 1584.0 | | | | |
| -26.00 | 1607.3 | 1607.3 | 1607.3 | | | | |
| -26.50 | 1628.8 | 1628.8 | 1628.8 | | | | |
| -27.00 | 1650.7 | 1650.7 | 1650.7 | | | | |
| -27.50 | 1672.3 | 1672.3 | 1672.3 | | | | |
| -28.00 | 1695.3 | 1695.3 | 1695.3 | | | | |
| -28.50 | 1719.0 | 1719.0 | 1719.0 | | | | |
| -29.00 | 1742.0 | 1742.0 | 1742.0 | | | | |
| -29.50 | 1766.1 | 1766.1 | 1766.1 | | | | |
| -30.00 | 1791.6 | 1791.6 | 1791.6 | | | | |
| 251.S01 | -1.05 | -8.00 | 492.1 | 492.1 | 492.1 | | |
| | | -8.50 | 526.5 | 526.5 | 526.5 | | |
| | | -9.00 | 534.6 | 534.6 | 534.6 | | |
| | | -9.50 | 566.7 | 566.7 | 566.7 | | |
| | | -10.00 | 613.5 | 613.5 | 613.5 | | |
| | | -10.50 | 668.1 | 668.1 | 668.1 | | |
| | | -11.00 | 710.4 | 710.4 | 710.4 | | |
| | | -11.50 | 737.4 | 737.4 | 737.4 | | |
| | | -12.00 | 764.3 | 764.3 | 764.3 | | |
| | | -12.50 | 807.5 | 807.5 | 807.5 | | |
| | | -13.00 | 858.1 | 858.1 | 858.1 | | |
| | | -13.50 | 906.0 | 906.0 | 906.0 | | |
| | | -14.00 | 971.1 | 971.1 | 971.1 | | |
| | | -14.50 | 1035.8 | 1035.8 | 1035.8 | | |
| | | -15.00 | 1105.6 | 1105.6 | 1105.6 | | |
| | | -15.50 | 1138.7 | 1138.7 | 1138.7 | | |
| | | -16.00 | 1202.0 | 1202.0 | 1202.0 | | |
| | | -16.50 | 1270.2 | 1270.2 | 1270.2 | | |
| | | -17.00 | 1337.8 | 1337.8 | 1337.8 | | |
| | | -17.50 | 1402.5 | 1402.5 | 1402.5 | | |
| | | -18.00 | 1463.7 | 1463.7 | 1463.7 | | |
| | | -18.50 | 1531.8 | 1531.8 | 1531.8 | | |
| | | -19.00 | 1574.1 | 1574.1 | 1574.1 | | |
| | | -19.50 | 1619.1 | 1619.1 | 1619.1 | | |
| -20.00 | 1673.0 | 1673.0 | 1673.0 | | | | |
| -20.50 | 1746.9 | 1746.9 | 1746.9 | | | | |
| -21.00 | 1824.6 | 1824.6 | 1824.6 | | | | |
| -21.50 | 1858.8 | 1858.8 | 1858.8 | | | | |
| -22.00 | 1871.9 | 1871.9 | 1871.9 | | | | |
| -22.50 | 1888.1 | 1888.1 | 1888.1 | | | | |
| -23.00 | 1911.9 | 1911.9 | 1911.9 | | | | |
| -23.50 | 1942.1 | 1942.1 | 1942.1 | | | | |
| -24.00 | 1981.7 | 1981.7 | 1981.7 | | | | |
| -24.50 | 2018.0 | 2018.0 | 2018.0 | | | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bezwijkdraagvermogen | | | | |
|-----------|--------------------|--------------------|----------------------|-------------------|-------------------------|-------|-------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] | | |
| 251.S01 | -1.05 | -25.00 | 2051.3 | 2051.3 | 2051.3 | | |
| | | -25.50 | 2108.4 | 2108.4 | 2108.4 | | |
| | | -26.00 | 2190.5 | 2190.5 | 2190.5 | | |
| | | -26.50 | 2271.0 | 2271.0 | 2271.0 | | |
| | | -27.00 | 2339.2 | 2339.2 | 2339.2 | | |
| | | -27.50 | 2407.4 | 2407.4 | 2407.4 | | |
| | | -28.00 | 2475.6 | 2475.6 | 2475.6 | | |
| | | -28.50 | 2543.8 | 2543.8 | 2543.8 | | |
| | | -29.00 | 2612.1 | 2612.1 | 2612.1 | | |
| | | -29.50 | 2659.5 | 2659.5 | 2659.5 | | |
| | | -30.00 | 2714.7 | 2714.7 | 2714.7 | | |
| | | 19-1008_29 | 0.79 | -8.00 | 645.3 | 645.3 | 645.3 |
| | | | | -8.50 | 707.6 | 707.6 | 707.6 |
| -9.00 | 762.2 | | | 762.2 | 762.2 | | |
| -9.50 | 813.4 | | | 813.4 | 813.4 | | |
| -10.00 | 861.5 | | | 861.5 | 861.5 | | |
| -10.50 | 916.9 | | | 916.9 | 916.9 | | |
| -11.00 | 971.8 | | | 971.8 | 971.8 | | |
| -11.50 | 1032.9 | | | 1032.9 | 1032.9 | | |
| -12.00 | 1063.4 | | | 1063.4 | 1063.4 | | |
| -12.50 | 1127.2 | | | 1127.2 | 1127.2 | | |
| -13.00 | 1176.6 | | | 1176.6 | 1176.6 | | |
| -13.50 | 1199.0 | | | 1199.0 | 1199.0 | | |
| -14.00 | 1224.7 | | | 1224.7 | 1224.7 | | |
| -14.50 | 1243.6 | | | 1243.6 | 1243.6 | | |
| -15.00 | 1260.3 | | | 1260.3 | 1260.3 | | |
| -15.50 | 1279.7 | | | 1279.7 | 1279.7 | | |
| -16.00 | 1324.7 | | | 1324.7 | 1324.7 | | |
| -16.50 | 1343.2 | | | 1343.2 | 1343.2 | | |
| -17.00 | 1361.8 | | | 1361.8 | 1361.8 | | |
| -17.50 | 1387.1 | | | 1387.1 | 1387.1 | | |
| -18.00 | 1444.5 | | | 1444.5 | 1444.5 | | |
| -18.50 | 1512.7 | | | 1512.7 | 1512.7 | | |
| -19.00 | 1580.2 | | | 1580.2 | 1580.2 | | |
| -19.50 | 1632.3 | | | 1632.3 | 1632.3 | | |
| -20.00 | 1700.5 | | | 1700.5 | 1700.5 | | |
| -20.50 | 1768.8 | | | 1768.8 | 1768.8 | | |
| -21.00 | 1837.0 | | | 1837.0 | 1837.0 | | |
| -21.50 | 1905.2 | | | 1905.2 | 1905.2 | | |
| -22.00 | 1973.4 | | | 1973.4 | 1973.4 | | |
| -22.50 | 2052.0 | | | 2052.0 | 2052.0 | | |
| -23.00 | 2112.3 | 2112.3 | 2112.3 | | | | |
| -23.50 | 2154.2 | 2154.2 | 2154.2 | | | | |
| -24.00 | 2202.8 | 2202.8 | 2202.8 | | | | |
| -24.50 | 2252.3 | 2252.3 | 2252.3 | | | | |
| -25.00 | 2304.6 | 2304.6 | 2304.6 | | | | |
| -25.50 | 2338.4 | 2338.4 | 2338.4 | | | | |
| -26.00 | 2376.7 | 2376.7 | 2376.7 | | | | |
| -26.50 | 2412.7 | 2412.7 | 2412.7 | | | | |
| -27.00 | 2457.0 | 2457.0 | 2457.0 | | | | |
| -27.50 | 2491.3 | 2491.3 | 2491.3 | | | | |
| -28.00 | 2524.8 | 2524.8 | 2524.8 | | | | |
| -28.50 | 2558.1 | 2558.1 | 2558.1 | | | | |
| -29.00 | 2594.5 | 2594.5 | 2594.5 | | | | |
| -29.50 | 2650.0 | 2650.0 | 2650.0 | | | | |
| -30.00 | 2698.6 | 2698.6 | 2698.6 | | | | |
| 283.S02 | 0.17 | -8.00 | 509.2 | 509.2 | 509.2 | | |
| | | -8.50 | 555.2 | 555.2 | 555.2 | | |
| | | -9.00 | 597.8 | 597.8 | 597.8 | | |
| | | -9.50 | 634.5 | 634.5 | 634.5 | | |
| | | -10.00 | 675.3 | 675.3 | 675.3 | | |
| | | -10.50 | 714.8 | 714.8 | 714.8 | | |
| | | -11.00 | 753.4 | 753.4 | 753.4 | | |
| | | -11.50 | 794.7 | 794.7 | 794.7 | | |
| | | -12.00 | 822.4 | 822.4 | 822.4 | | |
| | | -12.50 | 867.9 | 867.9 | 867.9 | | |
| | | -13.00 | 918.2 | 918.2 | 918.2 | | |
| | | -13.50 | 973.9 | 973.9 | 973.9 | | |
| | | -14.00 | 1039.2 | 1039.2 | 1039.2 | | |
| | | -14.50 | 1104.5 | 1104.5 | 1104.5 | | |
| | | -15.00 | 1163.3 | 1163.3 | 1163.3 | | |
| | | -15.50 | 1214.0 | 1214.0 | 1214.0 | | |
| | | -16.00 | 1269.2 | 1269.2 | 1269.2 | | |
| | | -16.50 | 1330.5 | 1330.5 | 1330.5 | | |
| | | -17.00 | 1395.8 | 1395.8 | 1395.8 | | |
| | | -17.50 | 1464.1 | 1464.1 | 1464.1 | | |
| | | -18.00 | 1532.3 | 1532.3 | 1532.3 | | |
| | | -18.50 | 1600.5 | 1600.5 | 1600.5 | | |
| | | -19.00 | 1668.7 | 1668.7 | 1668.7 | | |
| | | -19.50 | 1737.0 | 1737.0 | 1737.0 | | |
| | | -20.00 | 1805.2 | 1805.2 | 1805.2 | | |
| | | -20.50 | 1870.6 | 1870.6 | 1870.6 | | |
| -21.00 | 1938.8 | 1938.8 | 1938.8 | | | | |
| -21.50 | 2007.1 | 2007.1 | 2007.1 | | | | |
| -22.00 | 2075.3 | 2075.3 | 2075.3 | | | | |
| -22.50 | 2143.5 | 2143.5 | 2143.5 | | | | |
| -23.00 | 2211.7 | 2211.7 | 2211.7 | | | | |
| -23.50 | 2279.9 | 2279.9 | 2279.9 | | | | |
| -24.00 | 2348.2 | 2348.2 | 2348.2 | | | | |
| -24.50 | 2416.4 | 2416.4 | 2416.4 | | | | |
| -25.00 | 2484.6 | 2484.6 | 2484.6 | | | | |
| -25.50 | 2552.8 | 2552.8 | 2552.8 | | | | |
| -26.00 | 2621.1 | 2621.1 | 2621.1 | | | | |
| -26.50 | 2694.2 | 2694.2 | 2694.2 | | | | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld niveau | paalpunt niveau | Bewijkdraagvermogen | | | | |
|-----------|--------------------|--------------------|----------------------|-------------------|-------------------------|-------|-------|
| | | | $R_{t,caal}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] | | |
| 283.S02 | 0.17 | -27.00 | 2721.3 | 2721.3 | 2721.3 | | |
| | | -27.50 | 2747.2 | 2747.2 | 2747.2 | | |
| | | -28.00 | 2778.8 | 2778.8 | 2778.8 | | |
| | | -28.50 | 2818.0 | 2818.0 | 2818.0 | | |
| | | -29.00 | 2847.0 | 2847.0 | 2847.0 | | |
| | | -29.50 | 2872.9 | 2872.9 | 2872.9 | | |
| | | -30.00 | 2897.2 | 2897.2 | 2897.2 | | |
| | | 19-1008_35 | 0.92 | -8.00 | 490.9 | 490.9 | 490.9 |
| | | | | -8.50 | 527.0 | 527.0 | 527.0 |
| | | | | -9.00 | 555.4 | 555.4 | 555.4 |
| -9.50 | 584.0 | | | 584.0 | 584.0 | | |
| -10.00 | 617.8 | | | 617.8 | 617.8 | | |
| -10.50 | 649.8 | | | 649.8 | 649.8 | | |
| -11.00 | 702.2 | | | 702.2 | 702.2 | | |
| -11.50 | 747.4 | | | 747.4 | 747.4 | | |
| -12.00 | 779.7 | | | 779.7 | 779.7 | | |
| -12.50 | 808.1 | | | 808.1 | 808.1 | | |
| -13.00 | 844.7 | | | 844.7 | 844.7 | | |
| -13.50 | 887.4 | | | 887.4 | 887.4 | | |
| -14.00 | 931.8 | | | 931.8 | 931.8 | | |
| -14.50 | 985.6 | | | 985.6 | 985.6 | | |
| -15.00 | 1039.5 | | | 1039.5 | 1039.5 | | |
| -15.50 | 1093.9 | | | 1093.9 | 1093.9 | | |
| -16.00 | 1149.7 | | | 1149.7 | 1149.7 | | |
| -16.50 | 1205.6 | | | 1205.6 | 1205.6 | | |
| -17.00 | 1254.2 | | | 1254.2 | 1254.2 | | |
| -17.50 | 1295.8 | | | 1295.8 | 1295.8 | | |
| -18.00 | 1350.2 | | | 1350.2 | 1350.2 | | |
| -18.50 | 1399.6 | | | 1399.6 | 1399.6 | | |
| -19.00 | 1454.9 | | | 1454.9 | 1454.9 | | |
| -19.50 | 1509.6 | | | 1509.6 | 1509.6 | | |
| -20.00 | 1565.9 | | | 1565.9 | 1565.9 | | |
| -20.50 | 1634.3 | | | 1634.3 | 1634.3 | | |
| -21.00 | 1702.5 | | | 1702.5 | 1702.5 | | |
| -21.50 | 1770.8 | | | 1770.8 | 1770.8 | | |
| -22.00 | 1837.4 | | | 1837.4 | 1837.4 | | |
| -22.50 | 1905.6 | | | 1905.6 | 1905.6 | | |
| -23.00 | 1973.9 | 1973.9 | 1973.9 | | | | |
| -23.50 | 2042.1 | 2042.1 | 2042.1 | | | | |
| -24.00 | 2110.3 | 2110.3 | 2110.3 | | | | |
| -24.50 | 2177.4 | 2177.4 | 2177.4 | | | | |
| -25.00 | 2241.9 | 2241.9 | 2241.9 | | | | |
| -25.50 | 2315.0 | 2315.0 | 2315.0 | | | | |
| -26.00 | 2383.6 | 2383.6 | 2383.6 | | | | |
| -26.50 | 2443.9 | 2443.9 | 2443.9 | | | | |
| -27.00 | 2512.1 | 2512.1 | 2512.1 | | | | |
| -27.50 | 2580.3 | 2580.3 | 2580.3 | | | | |
| -28.00 | 2648.6 | 2648.6 | 2648.6 | | | | |
| -28.50 | 2716.8 | 2716.8 | 2716.8 | | | | |
| -29.00 | 2785.0 | 2785.0 | 2785.0 | | | | |
| -29.50 | 2853.2 | 2853.2 | 2853.2 | | | | |
| -30.00 | 2921.5 | 2921.5 | 2921.5 | | | | |
| 312.S03 | 3.78 | -8.00 | 631.0 | 631.0 | 631.0 | | |
| | | -8.50 | 699.2 | 699.2 | 699.2 | | |
| | | -9.00 | 767.5 | 767.5 | 767.5 | | |
| | | -9.50 | 835.7 | 835.7 | 835.7 | | |
| | | -10.00 | 903.9 | 903.9 | 903.9 | | |
| | | -10.50 | 971.9 | 971.9 | 971.9 | | |
| | | -11.00 | 1036.6 | 1036.6 | 1036.6 | | |
| | | -11.50 | 1104.8 | 1104.8 | 1104.8 | | |
| | | -12.00 | 1173.0 | 1173.0 | 1173.0 | | |
| | | -12.50 | 1241.3 | 1241.3 | 1241.3 | | |
| | | -13.00 | 1307.7 | 1307.7 | 1307.7 | | |
| | | -13.50 | 1357.2 | 1357.2 | 1357.2 | | |
| | | -14.00 | 1412.4 | 1412.4 | 1412.4 | | |
| | | -14.50 | 1467.7 | 1467.7 | 1467.7 | | |
| | | -15.00 | 1521.2 | 1521.2 | 1521.2 | | |
| | | -15.50 | 1576.5 | 1576.5 | 1576.5 | | |
| | | -16.00 | 1630.4 | 1630.4 | 1630.4 | | |
| | | -16.50 | 1685.7 | 1685.7 | 1685.7 | | |
| | | -17.00 | 1737.0 | 1737.0 | 1737.0 | | |
| | | -17.50 | 1777.9 | 1777.9 | 1777.9 | | |
| | | -18.00 | 1821.5 | 1821.5 | 1821.5 | | |
| | | -18.50 | 1875.4 | 1875.4 | 1875.4 | | |
| | | -19.00 | 1932.3 | 1932.3 | 1932.3 | | |
| | | -19.50 | 1990.7 | 1990.7 | 1990.7 | | |
| | | -20.00 | 2047.3 | 2047.3 | 2047.3 | | |
| | | -20.50 | 2097.3 | 2097.3 | 2097.3 | | |
| | | -21.00 | 2152.1 | 2152.1 | 2152.1 | | |
| | | -21.50 | 2203.2 | 2203.2 | 2203.2 | | |
| -22.00 | 2260.5 | 2260.5 | 2260.5 | | | | |
| -22.50 | 2327.2 | 2327.2 | 2327.2 | | | | |
| -23.00 | 2394.3 | 2394.3 | 2394.3 | | | | |
| -23.50 | 2459.5 | 2459.5 | 2459.5 | | | | |
| -24.00 | 2519.7 | 2519.7 | 2519.7 | | | | |
| -24.50 | 2588.0 | 2588.0 | 2588.0 | | | | |
| -25.00 | 2656.2 | 2656.2 | 2656.2 | | | | |
| -25.50 | 2720.5 | 2720.5 | 2720.5 | | | | |
| -26.00 | 2778.3 | 2778.3 | 2778.3 | | | | |
| -26.50 | 2845.1 | 2845.1 | 2845.1 | | | | |
| -27.00 | 2912.0 | 2912.0 | 2912.0 | | | | |
| -27.50 | 2950.1 | 2950.1 | 2950.1 | | | | |
| -28.00 | 2980.5 | 2980.5 | 2980.5 | | | | |
| -28.50 | 3004.6 | 3004.6 | 3004.6 | | | | |

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld | | Bezuikdraagvermogen | Rekenwaarden | | |
|------------|----------|--------------------|---------------------|---------------------|-------------------|-------------------------|
| | niveau | paalpunt niveau | | $R_{t,ca1}$ [kN] | $R_{t,d}$ [kN] | $R_{t,netto,d}$ [kN] |
| 312.S03 | 3.78 | -29.00 | 3028.3 | 3028.3 | 3028.3 | |
| | | -29.50 | 3055.3 | 3055.3 | 3055.3 | |
| | | -30.00 | 3091.0 | 3091.0 | 3091.0 | |
| | | | | | | |
| 19-1008_43 | 9.88 | -8.00 | 529.5 | 529.5 | 529.5 | |
| | | -8.50 | 579.8 | 579.8 | 579.8 | |
| | | -9.00 | 631.3 | 631.3 | 631.3 | |
| | | -9.50 | 683.9 | 683.9 | 683.9 | |
| | | -10.00 | 732.1 | 732.1 | 732.1 | |
| | | -10.50 | 789.7 | 789.7 | 789.7 | |
| | | -11.00 | 857.9 | 857.9 | 857.9 | |
| | | -11.50 | 926.1 | 926.1 | 926.1 | |
| | | -12.00 | 994.3 | 994.3 | 994.3 | |
| | | -12.50 | 1062.0 | 1062.0 | 1062.0 | |
| | | -13.00 | 1113.3 | 1113.3 | 1113.3 | |
| | | -13.50 | 1157.9 | 1157.9 | 1157.9 | |
| | | -14.00 | 1209.3 | 1209.3 | 1209.3 | |
| | | -14.50 | 1264.6 | 1264.6 | 1264.6 | |
| | | -15.00 | 1313.4 | 1313.4 | 1313.4 | |
| | | -15.50 | 1373.3 | 1373.3 | 1373.3 | |
| | | -16.00 | 1439.1 | 1439.1 | 1439.1 | |
| | | -16.50 | 1507.3 | 1507.3 | 1507.3 | |
| | | -17.00 | 1575.5 | 1575.5 | 1575.5 | |
| | | -17.50 | 1641.4 | 1641.4 | 1641.4 | |
| | | -18.00 | 1701.3 | 1701.3 | 1701.3 | |
| | | -18.50 | 1755.3 | 1755.3 | 1755.3 | |
| | | -19.00 | 1809.4 | 1809.4 | 1809.4 | |
| | | -19.50 | 1853.8 | 1853.8 | 1853.8 | |
| | | -20.00 | 1899.5 | 1899.5 | 1899.5 | |
| | | -20.50 | 1956.3 | 1956.3 | 1956.3 | |
| | | -21.00 | 2021.9 | 2021.9 | 2021.9 | |
| | | -21.50 | 2076.6 | 2076.6 | 2076.6 | |
| -22.00 | 2138.1 | 2138.1 | 2138.1 | | | |
| -22.50 | 2206.3 | 2206.3 | 2206.3 | | | |
| -23.00 | 2274.6 | 2274.6 | 2274.6 | | | |
| -23.50 | 2342.8 | 2342.8 | 2342.8 | | | |
| -24.00 | 2411.0 | 2411.0 | 2411.0 | | | |
| -24.50 | 2479.2 | 2479.2 | 2479.2 | | | |
| -25.00 | 2537.3 | 2537.3 | 2537.3 | | | |
| 328.S02 | 10.17 | -8.00 | 749.8 | 749.8 | 749.8 | |
| | | -8.50 | 804.4 | 804.4 | 804.4 | |
| | | -9.00 | 857.6 | 857.6 | 857.6 | |
| | | -9.50 | 903.7 | 903.7 | 903.7 | |
| | | -10.00 | 955.5 | 955.5 | 955.5 | |
| | | -10.50 | 1009.4 | 1009.4 | 1009.4 | |
| | | -11.00 | 1070.8 | 1070.8 | 1070.8 | |
| | | -11.50 | 1133.8 | 1133.8 | 1133.8 | |
| | | -12.00 | 1194.8 | 1194.8 | 1194.8 | |
| | | -12.50 | 1250.3 | 1250.3 | 1250.3 | |
| | | -13.00 | 1304.5 | 1304.5 | 1304.5 | |
| | | -13.50 | 1359.4 | 1359.4 | 1359.4 | |
| | | -14.00 | 1414.6 | 1414.6 | 1414.6 | |
| | | -14.50 | 1468.5 | 1468.5 | 1468.5 | |
| | | -15.00 | 1524.3 | 1524.3 | 1524.3 | |
| | | -15.50 | 1579.5 | 1579.5 | 1579.5 | |
| | | -16.00 | 1634.2 | 1634.2 | 1634.2 | |
| | | -16.50 | 1691.4 | 1691.4 | 1691.4 | |
| | | -17.00 | 1759.6 | 1759.6 | 1759.6 | |
| | | -17.50 | 1827.9 | 1827.9 | 1827.9 | |
| | | -18.00 | 1905.7 | 1905.7 | 1905.7 | |
| | | -18.50 | 1955.5 | 1955.5 | 1955.5 | |
| | | -19.00 | 2017.2 | 2017.2 | 2017.2 | |
| | | -19.50 | 2082.8 | 2082.8 | 2082.8 | |
| | | -20.00 | 2151.0 | 2151.0 | 2151.0 | |
| | | -20.50 | 2219.2 | 2219.2 | 2219.2 | |
| | | -21.00 | 2287.4 | 2287.4 | 2287.4 | |
| | | -21.50 | 2355.6 | 2355.6 | 2355.6 | |
| -22.00 | 2423.9 | 2423.9 | 2423.9 | | | |
| -22.50 | 2492.1 | 2492.1 | 2492.1 | | | |
| -23.00 | 2560.3 | 2560.3 | 2560.3 | | | |
| -23.50 | 2628.5 | 2628.5 | 2628.5 | | | |
| -24.00 | 2696.8 | 2696.8 | 2696.8 | | | |
| -24.50 | 2754.9 | 2754.9 | 2754.9 | | | |
| -25.00 | 2810.2 | 2810.2 | 2810.2 | | | |
| -25.50 | 2864.7 | 2864.7 | 2864.7 | | | |
| -26.00 | 2920.0 | 2920.0 | 2920.0 | | | |
| -26.50 | 2978.5 | 2978.5 | 2978.5 | | | |
| -27.00 | 3046.7 | 3046.7 | 3046.7 | | | |
| -27.50 | 3114.9 | 3114.9 | 3114.9 | | | |
| -28.00 | 3172.9 | 3172.9 | 3172.9 | | | |
| -28.50 | 3223.8 | 3223.8 | 3223.8 | | | |

PAALGEGEVENS SI Ø508/670

Type : In de grond gevormde geschroefde paal; groutinjectie
 Wijze van installeren : Schroeven
 Wijze van terugwinnen : n.v.t.
 Diameter [m] : 0.590
 Elasticiteitsmodulus [N/mm²] : 20000
 Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
 Factor α_c (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
 Paalklassefactor α_p : 0.63
 Paalvoetvormfactor β : 1.00
 Type lastzakingsdiagram : Grondverdringende paal
 Verm.factor * $\phi_{j,k}$: 1.00
 Groutomhulling : JA

Project : ZWO380 Funderingen
Onderdeel : RLL-TBG380

PAALGEGEVENS SI Ø610/850

Type : In de grond gevormde geschroefde paal; groutinjectie
Wijze van installeren : Schroeven
Wijze van terugwinnen : n.v.t.
Diameter [m] : 0.730
Elasticiteitsmodulus [N/mm²] : 20000
Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
Factor α_c (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
Paalklassefactor α_p : 0.63
Paalvoetvormfactor β : 1.00
Type lastzakkingsdiagram : Grondverdringende paal
Verm.factor * $\phi'_{j,k}$: 1.00
Groutomhulling : JA

PAALGEGEVENS SI Ø762/950

Type : In de grond gevormde geschroefde paal; groutinjectie
Wijze van installeren : Schroeven
Wijze van terugwinnen : n.v.t.
Diameter [m] : 0.860
Elasticiteitsmodulus [N/mm²] : 20000
Factor α_s (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)
Factor α_c (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)
Paalklassefactor α_p : 0.63
Paalvoetvormfactor β : 1.00
Type lastzakkingsdiagram : Grondverdringende paal
Verm.factor * $\phi'_{j,k}$: 1.00
Groutomhulling : JA

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

OVERZICHT NETTO DRAAGVERMOGEN TREKPALEN (n=1)

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld niveau | paalpunt niveau | R _{netto;d} [kN] | | |
|-----------|--------------------|--------------------|---------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| 19-1008_1 | 2.12 | -6.00 | 46 | | |
| | | -6.50 | 49 | | |
| | | -7.00 | 52 | 72 | |
| | | -7.50 | 56 | 76 | |
| | | -8.00 | 67 | 91 | 116 |
| | | -8.50 | 80 | 107 | 135 |
| | | -9.00 | 85 | 114 | 144 |
| | | -9.50 | 105 | 139 | 174 |
| | | -10.00 | 123 | 162 | 201 |
| | | -10.50 | 144 | 188 | 232 |
| | | -11.00 | 158 | 207 | 255 |
| | | -11.50 | 183 | 237 | 291 |
| | | -12.00 | 213 | 276 | 337 |
| | | -12.50 | 234 | 302 | 369 |
| | | -13.00 | 267 | 343 | 418 |
| | | -13.50 | 300 | 384 | 467 |
| | | -14.00 | 328 | 420 | 509 |
| | | -14.50 | 365 | 466 | 564 |
| | | -15.00 | 399 | 509 | 615 |
| | | -15.50 | 436 | 555 | 670 |
| | | -16.00 | 468 | 595 | 717 |
| | | -16.50 | 503 | 638 | 769 |
| | | -17.00 | 539 | 683 | 822 |
| | | -17.50 | 580 | 734 | 883 |
| | | -18.00 | 626 | 792 | 951 |
| | | -18.50 | 672 | 849 | 1020 |
| | | -19.00 | 718 | 907 | 1088 |
| | | -19.50 | 764 | 964 | 1156 |
| | | -20.00 | 822 | 1036 | 1242 |
| | | -20.50 | 881 | 1109 | 1328 |
| -21.00 | 942 | 1185 | 1418 | | |
| -21.50 | 985 | 1239 | 1482 | | |
| -22.00 | 1031 | 1297 | 1551 | | |
| -22.50 | 1077 | 1354 | 1619 | | |
| -23.00 | 1123 | 1412 | 1687 | | |
| -23.50 | 1169 | 1469 | 1755 | | |
| -24.00 | 1215 | 1527 | 1823 | | |
| -24.50 | 1261 | 1584 | 1892 | | |
| -25.00 | 1307 | 1642 | 1960 | | |
| -25.50 | 1354 | 1699 | 2028 | | |
| -26.00 | 1400 | 1757 | 2096 | | |
| -26.50 | 1446 | 1814 | 2165 | | |
| -27.00 | 1492 | 1871 | 2233 | | |
| -27.50 | 1538 | 1929 | 2301 | | |
| -28.00 | 1584 | 1986 | 2369 | | |
| -28.50 | 1630 | 2044 | 2437 | | |
| -29.00 | 1676 | 2101 | 2506 | | |
| -29.50 | 1722 | 2159 | 2574 | | |
| -30.00 | 1768 | 2216 | 2642 | | |
| 19-1008_6 | 11.00 | -6.00 | 392 | | |
| | | -6.50 | 438 | | |
| | | -7.00 | 485 | 606 | |
| | | -7.50 | 531 | 664 | |
| | | -8.00 | 577 | 721 | 858 |
| | | -8.50 | 623 | 779 | 926 |
| | | -9.00 | 669 | 836 | 994 |
| | | -9.50 | 715 | 894 | 1063 |
| | | -10.00 | 761 | 951 | 1131 |
| | | -10.50 | 807 | 1009 | 1199 |
| | | -11.00 | 853 | 1066 | 1267 |
| | | -11.50 | 899 | 1123 | 1336 |
| | | -12.00 | 945 | 1181 | 1404 |
| | | -12.50 | 991 | 1238 | 1472 |
| | | -13.00 | 1037 | 1296 | 1540 |
| | | -13.50 | 1083 | 1353 | 1608 |
| | | -14.00 | 1129 | 1411 | 1677 |
| | | -14.50 | 1175 | 1468 | 1745 |
| | | -15.00 | 1222 | 1526 | 1813 |
| | | -15.50 | 1268 | 1583 | 1881 |
| -16.00 | 1314 | 1641 | 1950 | | |
| -16.50 | 1360 | 1698 | 2018 | | |
| -17.00 | 1406 | 1756 | 2086 | | |
| -17.50 | 1452 | 1813 | 2154 | | |
| -18.00 | 1498 | 1871 | 2222 | | |
| -18.50 | 1541 | 1924 | 2286 | | |
| -19.00 | 1587 | 1982 | 2355 | | |
| -19.50 | 1633 | 2039 | 2423 | | |
| -20.00 | 1679 | 2097 | 2491 | | |
| -20.50 | 1725 | 2154 | 2559 | | |
| -21.00 | 1771 | 2212 | 2628 | | |
| -21.50 | 1817 | 2269 | 2696 | | |
| -22.00 | 1864 | 2327 | 2764 | | |
| -22.50 | 1910 | 2384 | 2832 | | |
| -23.00 | 1956 | 2442 | 2900 | | |
| -23.50 | 2002 | 2499 | 2969 | | |
| 166.S01 | 3.45 | -6.00 | 231 | | |
| | | -6.50 | 277 | | |
| | | -7.00 | 323 | 407 | |
| | | -7.50 | 369 | 464 | |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | niveau | maalveld niveau | R _{n, netto;d} [kN] | | |
|------------|--------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -8.00 | | 415 | 521 | 623 |
| | -8.50 | | 461 | 579 | 690 |
| | -9.00 | | 507 | 636 | 758 |
| | -9.50 | | 552 | 692 | 825 |
| | -10.00 | | 598 | 749 | 893 |
| | -10.50 | | 644 | 807 | 961 |
| | -11.00 | | 690 | 864 | 1030 |
| | -11.50 | | 736 | 922 | 1098 |
| | -12.00 | | 779 | 975 | 1161 |
| | -12.50 | | 815 | 1020 | 1215 |
| | -13.00 | | 849 | 1063 | 1266 |
| | -13.50 | | 884 | 1106 | 1317 |
| | -14.00 | | 923 | 1156 | 1376 |
| | -14.50 | | 969 | 1213 | 1444 |
| | -15.00 | | 1015 | 1270 | 1512 |
| | -15.50 | | 1061 | 1328 | 1581 |
| | -16.00 | | 1107 | 1385 | 1649 |
| | -16.50 | | 1153 | 1443 | 1717 |
| | -17.00 | | 1200 | 1500 | 1785 |
| | -17.50 | | 1246 | 1558 | 1854 |
| | -18.00 | | 1292 | 1615 | 1922 |
| | -18.50 | | 1338 | 1673 | 1990 |
| | -19.00 | | 1384 | 1730 | 2058 |
| | -19.50 | | 1430 | 1788 | 2126 |
| | -20.00 | | 1476 | 1845 | 2195 |
| | -20.50 | | 1522 | 1903 | 2263 |
| | -21.00 | | 1568 | 1960 | 2331 |
| | -21.50 | | 1614 | 2018 | 2399 |
| | -22.00 | | 1660 | 2075 | 2468 |
| | -22.50 | | 1706 | 2133 | 2536 |
| 19-1008_11 | 0.62 | -6.00 | 159 | | |
| | | -6.50 | 163 | | |
| | | -7.00 | 169 | 216 | |
| | | -7.50 | 182 | 233 | |
| | | -8.00 | 202 | 258 | 312 |
| | | -8.50 | 220 | 280 | 339 |
| | | -9.00 | 234 | 298 | 361 |
| | | -9.50 | 247 | 316 | 382 |
| | | -10.00 | 261 | 333 | 404 |
| | | -10.50 | 278 | 354 | 429 |
| | | -11.00 | 297 | 378 | 458 |
| | | -11.50 | 320 | 407 | 492 |
| | | -12.00 | 348 | 442 | 534 |
| | | -12.50 | 359 | 457 | 551 |
| | | -13.00 | 392 | 498 | 600 |
| | | -13.50 | 430 | 546 | 657 |
| | | -14.00 | 470 | 595 | 715 |
| | | -14.50 | 509 | 644 | 774 |
| | | -15.00 | 549 | 693 | 833 |
| | | -15.50 | 586 | 740 | 888 |
| | | -16.00 | 617 | 779 | 935 |
| | | -16.50 | 654 | 825 | 990 |
| | | -17.00 | 690 | 870 | 1043 |
| | | -17.50 | 723 | 912 | 1093 |
| | | -18.00 | 765 | 965 | 1155 |
| | | -18.50 | 811 | 1022 | 1224 |
| | | -19.00 | 858 | 1079 | 1292 |
| | | -19.50 | 904 | 1137 | 1360 |
| | | -20.00 | 950 | 1194 | 1428 |
| | | -20.50 | 996 | 1252 | 1497 |
| | | -21.00 | 1042 | 1309 | 1565 |
| | | -21.50 | 1085 | 1364 | 1629 |
| | | -22.00 | 1131 | 1421 | 1698 |
| | | -22.50 | 1178 | 1479 | 1766 |
| | | -23.00 | 1220 | 1531 | 1828 |
| | | -23.50 | 1248 | 1567 | 1871 |
| | | -24.00 | 1284 | 1612 | 1925 |
| | | -24.50 | 1325 | 1663 | 1985 |
| | | -25.00 | 1364 | 1712 | 2043 |
| | | -25.50 | 1397 | 1753 | 2092 |
| | | -26.00 | 1444 | 1811 | 2161 |
| | | -26.50 | 1490 | 1869 | 2230 |
| | | -27.00 | 1536 | 1926 | 2298 |
| | | -27.50 | 1582 | 1984 | 2366 |
| | | -28.00 | 1628 | 2041 | 2434 |
| | | -28.50 | 1674 | 2099 | 2502 |
| | | -29.00 | 1720 | 2156 | 2571 |
| | | -29.50 | 1766 | 2214 | 2639 |
| | | -30.00 | 1812 | 2271 | 2707 |
| 19-1008_12 | 3.57 | -6.00 | 419 | | |
| | | -6.50 | 455 | | |
| | | -7.00 | 500 | 626 | |
| | | -7.50 | 546 | 683 | |
| | | -8.00 | 592 | 740 | 880 |
| | | -8.50 | 616 | 771 | 917 |
| | | -9.00 | 625 | 781 | 930 |
| | | -9.50 | 631 | 790 | 940 |
| | | -10.00 | 642 | 804 | 958 |
| | | -10.50 | 663 | 831 | 990 |
| | | -11.00 | 680 | 852 | 1015 |
| | | -11.50 | 685 | 858 | 1023 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | niveau | R _{n, netto;d} [kN] | |
|------------|--------|------------------------------|-----------|
| | | SI Ø508/6 | SI Ø610/8 |
| | -12.00 | 700 | 878 |
| | -12.50 | 707 | 887 |
| | -13.00 | 713 | 894 |
| | -13.50 | 719 | 903 |
| | -14.00 | 733 | 921 |
| | -14.50 | 751 | 943 |
| | -15.00 | 764 | 959 |
| | -15.50 | 774 | 972 |
| | -16.00 | 790 | 993 |
| | -16.50 | 811 | 1020 |
| | -17.00 | 829 | 1042 |
| | -17.50 | 855 | 1075 |
| | -18.00 | 876 | 1101 |
| | -18.50 | 921 | 1158 |
| | -19.00 | 963 | 1210 |
| | -19.50 | 1001 | 1258 |
| | -20.00 | 1035 | 1299 |
| | -20.50 | 1072 | 1346 |
| | -21.00 | 1107 | 1389 |
| | -21.50 | 1149 | 1442 |
| | -22.00 | 1194 | 1499 |
| | -22.50 | 1240 | 1555 |
| | -23.00 | 1281 | 1607 |
| | -23.50 | 1322 | 1658 |
| | -24.00 | 1364 | 1711 |
| | -24.50 | 1410 | 1769 |
| | -25.00 | 1457 | 1826 |
| | -25.50 | 1517 | 1901 |
| | -26.00 | 1577 | 1977 |
| | -26.50 | 1613 | 2021 |
| | -27.00 | 1646 | 2063 |
| | -27.50 | 1684 | 2110 |
| | -28.00 | 1712 | 2145 |
| | -28.50 | 1748 | 2190 |
| | -29.00 | 1794 | 2247 |
| | -29.50 | 1840 | 2305 |
| | -30.00 | 1885 | 2361 |
| 19-1008_17 | 0.20 | -6.00 | 68 |
| | | -6.50 | 73 |
| | | -7.00 | 98 |
| | | -7.50 | 110 |
| | | -8.00 | 116 |
| | | -8.50 | 122 |
| | | -9.00 | 133 |
| | | -9.50 | 142 |
| | | -10.00 | 176 |
| | | -10.50 | 194 |
| | | -11.00 | 224 |
| | | -11.50 | 270 |
| | | -12.00 | 316 |
| | | -12.50 | 362 |
| | | -13.00 | 408 |
| | | -13.50 | 454 |
| | | -14.00 | 500 |
| | | -14.50 | 546 |
| | | -15.00 | 589 |
| | | -15.50 | 635 |
| | | -16.00 | 681 |
| | | -16.50 | 727 |
| | | -17.00 | 772 |
| | | -17.50 | 819 |
| | | -18.00 | 874 |
| | | -18.50 | 912 |
| | | -19.00 | 944 |
| | | -19.50 | 981 |
| | | -20.00 | 1019 |
| | | -20.50 | 1059 |
| | | -21.00 | 1100 |
| | | -21.50 | 1146 |
| | | -22.00 | 1185 |
| | | -22.50 | 1231 |
| | | -23.00 | 1277 |
| | | -23.50 | 1324 |
| | | -24.00 | 1366 |
| | | -24.50 | 1404 |
| | | -25.00 | 1433 |
| | | -25.50 | 1461 |
| | | -26.00 | 1489 |
| | | -26.50 | 1517 |
| | | -27.00 | 1549 |
| | | -27.50 | 1584 |
| | | -28.00 | 1620 |
| | | -28.50 | 1657 |
| | | -29.00 | 1696 |
| | | -29.50 | 1708 |
| | | -30.00 | 1738 |
| 19-1008_20 | -0.03 | -6.00 | 86 |
| | | -6.50 | 102 |
| | | -7.00 | 131 |
| | | -7.50 | 156 |
| | | -8.00 | 176 |

Project : ZWO380 Funderingen
 Onderdeel : RLL-TBG380

Netto paaldragvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld paalpunt | | R _{n, netto, d} [kN] | | |
|------------|-------------------|--------|-------------------------------|-----------|-----------|
| | niveau | niveau | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -8.50 | 196 | 251 | 306 | |
| | -9.00 | 222 | 284 | 345 | |
| | -9.50 | 244 | 312 | 378 | |
| | -10.00 | 269 | 343 | 416 | |
| | -10.50 | 276 | 352 | 427 | |
| | -11.00 | 308 | 393 | 475 | |
| | -11.50 | 342 | 435 | 526 | |
| | -12.00 | 350 | 446 | 538 | |
| | -12.50 | 359 | 457 | 553 | |
| | -13.00 | 375 | 477 | 576 | |
| | -13.50 | 383 | 487 | 589 | |
| | -14.00 | 397 | 505 | 610 | |
| | -14.50 | 421 | 536 | 647 | |
| | -15.00 | 449 | 571 | 689 | |
| | -15.50 | 465 | 591 | 714 | |
| | -16.00 | 478 | 608 | 733 | |
| | -16.50 | 495 | 629 | 760 | |
| | -17.00 | 507 | 644 | 778 | |
| | -17.50 | 521 | 662 | 799 | |
| | -18.00 | 546 | 694 | 837 | |
| | -18.50 | 575 | 730 | 880 | |
| | -19.00 | 597 | 758 | 913 | |
| | -19.50 | 626 | 794 | 957 | |
| | -20.00 | 656 | 832 | 1002 | |
| | -20.50 | 694 | 879 | 1058 | |
| | -21.00 | 745 | 942 | 1133 | |
| | -21.50 | 767 | 971 | 1167 | |
| | -22.00 | 782 | 990 | 1190 | |
| | -22.50 | 799 | 1011 | 1215 | |
| | -23.00 | 813 | 1028 | 1236 | |
| | -23.50 | 838 | 1060 | 1274 | |
| | -24.00 | 866 | 1095 | 1315 | |
| | -24.50 | 895 | 1131 | 1359 | |
| | -25.00 | 930 | 1175 | 1412 | |
| | -25.50 | 962 | 1216 | 1460 | |
| | -26.00 | 994 | 1256 | 1507 | |
| | -26.50 | 1023 | 1292 | 1550 | |
| | -27.00 | 1058 | 1335 | 1602 | |
| | -27.50 | 1089 | 1374 | 1648 | |
| | -28.00 | 1116 | 1409 | 1690 | |
| | -28.50 | 1149 | 1450 | 1738 | |
| | -29.00 | 1179 | 1487 | 1783 | |
| | -29.50 | 1204 | 1518 | 1820 | |
| | -30.00 | 1234 | 1557 | 1866 | |
| 19-1008_21 | 1.78 | -6.00 | 153 | | |
| | | -6.50 | 183 | | |
| | | -7.00 | 213 | 270 | |
| | | -7.50 | 250 | 316 | |
| | | -8.00 | 284 | 359 | 431 |
| | | -8.50 | 319 | 402 | 483 |
| | | -9.00 | 337 | 426 | 511 |
| | | -9.50 | 352 | 444 | 533 |
| | | -10.00 | 373 | 471 | 565 |
| | | -10.50 | 392 | 495 | 594 |
| | | -11.00 | 413 | 521 | 626 |
| | | -11.50 | 439 | 555 | 665 |
| | | -12.00 | 469 | 592 | 709 |
| | | -12.50 | 492 | 620 | 744 |
| | | -13.00 | 518 | 654 | 784 |
| | | -13.50 | 547 | 690 | 827 |
| | | -14.00 | 590 | 743 | 890 |
| | | -14.50 | 632 | 796 | 953 |
| | | -15.00 | 664 | 835 | 1000 |
| | | -15.50 | 689 | 867 | 1037 |
| | | -16.00 | 733 | 922 | 1103 |
| | | -16.50 | 778 | 978 | 1170 |
| | | -17.00 | 787 | 990 | 1184 |
| | | -17.50 | 797 | 1003 | 1199 |
| | | -18.00 | 814 | 1025 | 1226 |
| | | -18.50 | 863 | 1085 | 1298 |
| | | -19.00 | 897 | 1128 | 1348 |
| | | -19.50 | 907 | 1140 | 1364 |
| | | -20.00 | 915 | 1151 | 1377 |
| | | -20.50 | 923 | 1161 | 1390 |
| | | -21.00 | 931 | 1172 | 1402 |
| | | -21.50 | 940 | 1184 | 1417 |
| | | -22.00 | 951 | 1198 | 1434 |
| | | -22.50 | 964 | 1214 | 1454 |
| | | -23.00 | 976 | 1230 | 1473 |
| | | -23.50 | 989 | 1246 | 1492 |
| | | -24.00 | 1003 | 1264 | 1514 |
| | | -24.50 | 1017 | 1282 | 1536 |
| | | -25.00 | 1033 | 1301 | 1559 |
| | | -25.50 | 1048 | 1322 | 1583 |
| | | -26.00 | 1064 | 1341 | 1607 |
| | | -26.50 | 1078 | 1359 | 1628 |
| | | -27.00 | 1092 | 1377 | 1650 |
| | | -27.50 | 1106 | 1395 | 1672 |
| | | -28.00 | 1121 | 1414 | 1695 |
| | | -28.50 | 1137 | 1434 | 1718 |
| | | -29.00 | 1152 | 1453 | 1742 |
| | | -29.50 | 1167 | 1473 | 1766 |

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| sondering | niveau | maalveld niveau | R _{n, netto;d} [kN] | | |
|------------|--------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | | -30.00 | 1184 | 1494 | 1791 |
| 251.S01 | -1.05 | -6.00 | 184 | | |
| | | -6.50 | 216 | | |
| | | -7.00 | 253 | 322 | |
| | | -7.50 | 289 | 367 | |
| | | -8.00 | 323 | 409 | 492 |
| | | -8.50 | 346 | 437 | 526 |
| | | -9.00 | 350 | 444 | 534 |
| | | -9.50 | 372 | 471 | 566 |
| | | -10.00 | 403 | 510 | 613 |
| | | -10.50 | 440 | 556 | 668 |
| | | -11.00 | 468 | 591 | 710 |
| | | -11.50 | 486 | 614 | 737 |
| | | -12.00 | 504 | 636 | 764 |
| | | -12.50 | 532 | 672 | 807 |
| | | -13.00 | 566 | 715 | 858 |
| | | -13.50 | 599 | 755 | 905 |
| | | -14.00 | 642 | 810 | 971 |
| | | -14.50 | 686 | 864 | 1035 |
| | | -15.00 | 733 | 923 | 1105 |
| | | -15.50 | 755 | 951 | 1138 |
| | | -16.00 | 798 | 1004 | 1202 |
| | | -16.50 | 844 | 1062 | 1270 |
| | | -17.00 | 890 | 1119 | 1337 |
| | | -17.50 | 933 | 1173 | 1402 |
| | | -18.00 | 974 | 1225 | 1463 |
| | | -18.50 | 1020 | 1282 | 1531 |
| | | -19.00 | 1049 | 1317 | 1574 |
| | | -19.50 | 1079 | 1355 | 1619 |
| | | -20.00 | 1115 | 1400 | 1672 |
| | | -20.50 | 1165 | 1463 | 1746 |
| | | -21.00 | 1218 | 1528 | 1824 |
| | | -21.50 | 1240 | 1557 | 1858 |
| | | -22.00 | 1249 | 1568 | 1871 |
| | | -22.50 | 1259 | 1581 | 1888 |
| | | -23.00 | 1275 | 1601 | 1911 |
| | | -23.50 | 1295 | 1626 | 1942 |
| | | -24.00 | 1321 | 1659 | 1981 |
| | | -24.50 | 1345 | 1689 | 2018 |
| | | -25.00 | 1367 | 1717 | 2051 |
| | | -25.50 | 1406 | 1765 | 2108 |
| | | -26.00 | 1461 | 1834 | 2190 |
| | | -26.50 | 1516 | 1902 | 2270 |
| | | -27.00 | 1562 | 1960 | 2339 |
| | | -27.50 | 1608 | 2017 | 2407 |
| | | -28.00 | 1654 | 2075 | 2475 |
| | | -28.50 | 1700 | 2132 | 2543 |
| | | -29.00 | 1746 | 2190 | 2612 |
| | | -29.50 | 1778 | 2229 | 2659 |
| | | -30.00 | 1815 | 2276 | 2714 |
| 19-1008_29 | 0.79 | -6.00 | 277 | | |
| | | -6.50 | 310 | | |
| | | -7.00 | 348 | 438 | |
| | | -7.50 | 388 | 487 | |
| | | -8.00 | 430 | 540 | 645 |
| | | -8.50 | 472 | 592 | 707 |
| | | -9.00 | 509 | 638 | 762 |
| | | -9.50 | 543 | 681 | 813 |
| | | -10.00 | 575 | 722 | 861 |
| | | -10.50 | 613 | 768 | 916 |
| | | -11.00 | 650 | 815 | 971 |
| | | -11.50 | 691 | 866 | 1032 |
| | | -12.00 | 711 | 891 | 1063 |
| | | -12.50 | 754 | 945 | 1127 |
| | | -13.00 | 787 | 987 | 1176 |
| | | -13.50 | 802 | 1005 | 1198 |
| | | -14.00 | 819 | 1027 | 1224 |
| | | -14.50 | 831 | 1042 | 1243 |
| | | -15.00 | 842 | 1056 | 1260 |
| | | -15.50 | 854 | 1072 | 1279 |
| | | -16.00 | 884 | 1110 | 1324 |
| | | -16.50 | 896 | 1125 | 1343 |
| | | -17.00 | 908 | 1140 | 1361 |
| | | -17.50 | 925 | 1161 | 1387 |
| | | -18.00 | 964 | 1210 | 1444 |
| | | -18.50 | 1010 | 1267 | 1512 |
| | | -19.00 | 1055 | 1324 | 1580 |
| | | -19.50 | 1090 | 1368 | 1632 |
| | | -20.00 | 1136 | 1425 | 1700 |
| | | -20.50 | 1182 | 1483 | 1768 |
| | | -21.00 | 1228 | 1540 | 1836 |
| | | -21.50 | 1275 | 1598 | 1905 |
| | | -22.00 | 1321 | 1655 | 1973 |
| | | -22.50 | 1374 | 1721 | 2052 |
| | | -23.00 | 1414 | 1772 | 2112 |
| | | -23.50 | 1442 | 1807 | 2154 |
| | | -24.00 | 1475 | 1848 | 2202 |
| | | -24.50 | 1508 | 1890 | 2252 |
| | | -25.00 | 1543 | 1934 | 2304 |
| | | -25.50 | 1566 | 1962 | 2338 |
| | | -26.00 | 1591 | 1994 | 2376 |

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| sondering | maalveld paalpunt | | R _{n, netto;d} [kN] | | |
|------------|-------------------|--------|------------------------------|-----------|-----------|
| | niveau | niveau | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | -26.50 | | 1615 | 2024 | 2412 |
| | -27.00 | | 1645 | 2061 | 2456 |
| | -27.50 | | 1668 | 2090 | 2491 |
| | -28.00 | | 1690 | 2118 | 2524 |
| | -28.50 | | 1712 | 2146 | 2558 |
| | -29.00 | | 1736 | 2176 | 2594 |
| | -29.50 | | 1774 | 2223 | 2649 |
| | -30.00 | | 1806 | 2264 | 2698 |
| 283.S02 | 0.17 | -6.00 | 224 | | |
| | | -6.50 | 252 | | |
| | | -7.00 | 284 | 359 | |
| | | -7.50 | 310 | 392 | |
| | | -8.00 | 336 | 424 | 509 |
| | | -8.50 | 367 | 463 | 555 |
| | | -9.00 | 395 | 498 | 597 |
| | | -9.50 | 420 | 529 | 634 |
| | | -10.00 | 447 | 563 | 675 |
| | | -10.50 | 473 | 596 | 714 |
| | | -11.00 | 499 | 629 | 753 |
| | | -11.50 | 527 | 663 | 794 |
| | | -12.00 | 545 | 686 | 822 |
| | | -12.50 | 575 | 725 | 867 |
| | | -13.00 | 609 | 767 | 918 |
| | | -13.50 | 647 | 814 | 973 |
| | | -14.00 | 691 | 869 | 1039 |
| | | -14.50 | 735 | 924 | 1104 |
| | | -15.00 | 774 | 973 | 1163 |
| | | -15.50 | 808 | 1016 | 1214 |
| | | -16.00 | 846 | 1062 | 1269 |
| | | -16.50 | 887 | 1114 | 1330 |
| | | -17.00 | 931 | 1169 | 1395 |
| | | -17.50 | 977 | 1226 | 1464 |
| | | -18.00 | 1023 | 1284 | 1532 |
| | | -18.50 | 1069 | 1341 | 1600 |
| | | -19.00 | 1115 | 1399 | 1668 |
| | | -19.50 | 1161 | 1456 | 1736 |
| | | -20.00 | 1207 | 1514 | 1805 |
| | | -20.50 | 1251 | 1569 | 1870 |
| | | -21.00 | 1298 | 1626 | 1938 |
| | | -21.50 | 1344 | 1684 | 2007 |
| | | -22.00 | 1390 | 1741 | 2075 |
| | | -22.50 | 1436 | 1799 | 2143 |
| | | -23.00 | 1482 | 1856 | 2211 |
| | | -23.50 | 1528 | 1913 | 2279 |
| | | -24.00 | 1574 | 1971 | 2348 |
| | | -24.50 | 1620 | 2028 | 2416 |
| | | -25.00 | 1666 | 2086 | 2484 |
| | | -25.50 | 1712 | 2143 | 2552 |
| | | -26.00 | 1758 | 2201 | 2621 |
| | | -26.50 | 1808 | 2262 | 2694 |
| | | -27.00 | 1825 | 2285 | 2721 |
| | | -27.50 | 1842 | 2307 | 2747 |
| | | -28.00 | 1863 | 2333 | 2778 |
| | | -28.50 | 1890 | 2366 | 2818 |
| | | -29.00 | 1909 | 2390 | 2847 |
| | | -29.50 | 1926 | 2411 | 2872 |
| | | -30.00 | 1942 | 2432 | 2897 |
| 19-1008_35 | 0.92 | -6.00 | 245 | | |
| | | -6.50 | 266 | | |
| | | -7.00 | 283 | 357 | |
| | | -7.50 | 300 | 379 | |
| | | -8.00 | 324 | 409 | 490 |
| | | -8.50 | 348 | 439 | 527 |
| | | -9.00 | 367 | 463 | 555 |
| | | -9.50 | 386 | 487 | 583 |
| | | -10.00 | 408 | 515 | 617 |
| | | -10.50 | 430 | 542 | 649 |
| | | -11.00 | 465 | 586 | 702 |
| | | -11.50 | 495 | 624 | 747 |
| | | -12.00 | 517 | 651 | 779 |
| | | -12.50 | 535 | 674 | 808 |
| | | -13.00 | 560 | 705 | 844 |
| | | -13.50 | 588 | 741 | 887 |
| | | -14.00 | 618 | 778 | 931 |
| | | -14.50 | 654 | 823 | 985 |
| | | -15.00 | 690 | 869 | 1039 |
| | | -15.50 | 727 | 914 | 1093 |
| | | -16.00 | 764 | 961 | 1149 |
| | | -16.50 | 802 | 1008 | 1205 |
| | | -17.00 | 835 | 1049 | 1254 |
| | | -17.50 | 863 | 1084 | 1295 |
| | | -18.00 | 899 | 1130 | 1350 |
| | | -18.50 | 932 | 1171 | 1399 |
| | | -19.00 | 969 | 1218 | 1454 |
| | | -19.50 | 1006 | 1264 | 1509 |
| | | -20.00 | 1044 | 1311 | 1565 |
| | | -20.50 | 1090 | 1369 | 1634 |
| | | -21.00 | 1136 | 1426 | 1702 |
| | | -21.50 | 1182 | 1484 | 1770 |
| | | -22.00 | 1227 | 1540 | 1837 |
| | | -22.50 | 1273 | 1597 | 1905 |

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| sondering | maalveld niveau | paalpunt niveau | R _{n, netto;d} [kN] | | |
|------------|--------------------|--------------------|------------------------------|-----------|-----------|
| | | | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | | -23.00 | 1320 | 1655 | 1973 |
| | | -23.50 | 1366 | 1712 | 2042 |
| | | -24.00 | 1412 | 1770 | 2110 |
| | | -24.50 | 1457 | 1826 | 2177 |
| | | -25.00 | 1500 | 1880 | 2241 |
| | | -25.50 | 1550 | 1942 | 2314 |
| | | -26.00 | 1596 | 2000 | 2383 |
| | | -26.50 | 1637 | 2051 | 2443 |
| | | -27.00 | 1683 | 2108 | 2512 |
| | | -27.50 | 1729 | 2166 | 2580 |
| | | -28.00 | 1775 | 2223 | 2648 |
| | | -28.50 | 1821 | 2280 | 2716 |
| | | -29.00 | 1867 | 2338 | 2785 |
| | | -29.50 | 1913 | 2395 | 2853 |
| | | -30.00 | 1959 | 2453 | 2921 |
| 312.S03 | 3.78 | -6.00 | 291 | | |
| | | -6.50 | 326 | | |
| | | -7.00 | 367 | 461 | |
| | | -7.50 | 393 | 493 | |
| | | -8.00 | 421 | 528 | 631 |
| | | -8.50 | 467 | 586 | 699 |
| | | -9.00 | 513 | 643 | 767 |
| | | -9.50 | 559 | 700 | 835 |
| | | -10.00 | 605 | 758 | 903 |
| | | -10.50 | 651 | 815 | 971 |
| | | -11.00 | 694 | 870 | 1036 |
| | | -11.50 | 740 | 927 | 1104 |
| | | -12.00 | 787 | 985 | 1173 |
| | | -12.50 | 833 | 1042 | 1241 |
| | | -13.00 | 877 | 1098 | 1307 |
| | | -13.50 | 911 | 1140 | 1357 |
| | | -14.00 | 948 | 1186 | 1412 |
| | | -14.50 | 985 | 1233 | 1467 |
| | | -15.00 | 1021 | 1278 | 1521 |
| | | -15.50 | 1058 | 1324 | 1576 |
| | | -16.00 | 1094 | 1369 | 1630 |
| | | -16.50 | 1132 | 1416 | 1685 |
| | | -17.00 | 1166 | 1459 | 1736 |
| | | -17.50 | 1193 | 1493 | 1777 |
| | | -18.00 | 1223 | 1530 | 1821 |
| | | -18.50 | 1259 | 1575 | 1875 |
| | | -19.00 | 1297 | 1623 | 1932 |
| | | -19.50 | 1336 | 1672 | 1990 |
| | | -20.00 | 1374 | 1720 | 2047 |
| | | -20.50 | 1408 | 1762 | 2097 |
| | | -21.00 | 1445 | 1808 | 2152 |
| | | -21.50 | 1479 | 1851 | 2203 |
| | | -22.00 | 1518 | 1899 | 2260 |
| | | -22.50 | 1563 | 1955 | 2327 |
| | | -23.00 | 1608 | 2012 | 2394 |
| | | -23.50 | 1652 | 2067 | 2459 |
| | | -24.00 | 1693 | 2117 | 2519 |
| | | -24.50 | 1739 | 2175 | 2587 |
| | | -25.00 | 1785 | 2232 | 2656 |
| | | -25.50 | 1828 | 2286 | 2720 |
| | | -26.00 | 1867 | 2335 | 2778 |
| | | -26.50 | 1912 | 2391 | 2845 |
| | | -27.00 | 1957 | 2447 | 2911 |
| | | -27.50 | 1983 | 2479 | 2950 |
| | | -28.00 | 2003 | 2505 | 2980 |
| | | -28.50 | 2019 | 2525 | 3004 |
| | | -29.00 | 2034 | 2544 | 3028 |
| | | -29.50 | 2052 | 2567 | 3055 |
| | | -30.00 | 2076 | 2597 | 3090 |
| 19-1008_43 | 9.88 | -6.00 | 224 | | |
| | | -6.50 | 244 | | |
| | | -7.00 | 280 | 353 | |
| | | -7.50 | 315 | 397 | |
| | | -8.00 | 351 | 442 | 529 |
| | | -8.50 | 385 | 484 | 579 |
| | | -9.00 | 419 | 527 | 631 |
| | | -9.50 | 455 | 572 | 683 |
| | | -10.00 | 487 | 612 | 732 |
| | | -10.50 | 526 | 661 | 789 |
| | | -11.00 | 572 | 718 | 857 |
| | | -11.50 | 618 | 775 | 926 |
| | | -12.00 | 664 | 833 | 994 |
| | | -12.50 | 710 | 890 | 1062 |
| | | -13.00 | 744 | 933 | 1113 |
| | | -13.50 | 774 | 970 | 1157 |
| | | -14.00 | 808 | 1014 | 1209 |
| | | -14.50 | 846 | 1060 | 1264 |
| | | -15.00 | 878 | 1101 | 1313 |
| | | -15.50 | 919 | 1152 | 1373 |
| | | -16.00 | 963 | 1207 | 1439 |
| | | -16.50 | 1009 | 1264 | 1507 |
| | | -17.00 | 1055 | 1322 | 1575 |
| | | -17.50 | 1100 | 1377 | 1641 |
| | | -18.00 | 1140 | 1428 | 1701 |
| | | -18.50 | 1176 | 1473 | 1755 |
| | | -19.00 | 1213 | 1519 | 1809 |

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 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | niveau | maalveld paalpunt | | R _{n, netto;d} [kN] | | |
|-----------|--------|-------------------|--------|------------------------------|-----------|-----------|
| | | niveau | niveau | SI Ø508/6 | SI Ø610/8 | SI Ø762/9 |
| | | -19.50 | 1242 | | 1556 | 1853 |
| | | -20.00 | 1273 | | 1594 | 1899 |
| | | -20.50 | 1311 | | 1642 | 1956 |
| | | -21.00 | 1356 | | 1697 | 2021 |
| | | -21.50 | 1392 | | 1743 | 2076 |
| | | -22.00 | 1434 | | 1795 | 2138 |
| | | -22.50 | 1480 | | 1852 | 2206 |
| | | -23.00 | 1526 | | 1910 | 2274 |
| | | -23.50 | 1572 | | 1967 | 2342 |
| | | -24.00 | 1618 | | 2025 | 2411 |
| | | -24.50 | 1664 | | 2082 | 2479 |
| | | -25.00 | 1703 | | 2131 | 2537 |
| 328.S02 | 10.17 | -6.00 | 371 | | | |
| | | -6.50 | 408 | | | |
| | | -7.00 | 434 | 543 | | |
| | | -7.50 | 466 | 584 | | |
| | | -8.00 | 502 | 629 | 749 | |
| | | -8.50 | 539 | 675 | 804 | |
| | | -9.00 | 575 | 720 | 857 | |
| | | -9.50 | 605 | 758 | 903 | |
| | | -10.00 | 640 | 802 | 955 | |
| | | -10.50 | 676 | 847 | 1009 | |
| | | -11.00 | 718 | 899 | 1070 | |
| | | -11.50 | 760 | 952 | 1133 | |
| | | -12.00 | 801 | 1003 | 1194 | |
| | | -12.50 | 839 | 1050 | 1250 | |
| | | -13.00 | 875 | 1095 | 1304 | |
| | | -13.50 | 912 | 1142 | 1359 | |
| | | -14.00 | 949 | 1188 | 1414 | |
| | | -14.50 | 985 | 1233 | 1468 | |
| | | -15.00 | 1023 | 1280 | 1524 | |
| | | -15.50 | 1060 | 1327 | 1579 | |
| | | -16.00 | 1097 | 1373 | 1634 | |
| | | -16.50 | 1135 | 1421 | 1691 | |
| | | -17.00 | 1182 | 1478 | 1759 | |
| | | -17.50 | 1228 | 1536 | 1827 | |
| | | -18.00 | 1280 | 1601 | 1905 | |
| | | -18.50 | 1314 | 1643 | 1955 | |
| | | -19.00 | 1355 | 1695 | 2017 | |
| | | -19.50 | 1400 | 1750 | 2082 | |
| | | -20.00 | 1446 | 1808 | 2150 | |
| | | -20.50 | 1492 | 1865 | 2219 | |
| | | -21.00 | 1538 | 1923 | 2287 | |
| | | -21.50 | 1584 | 1980 | 2355 | |
| | | -22.00 | 1630 | 2038 | 2423 | |
| | | -22.50 | 1676 | 2095 | 2492 | |
| | | -23.00 | 1722 | 2153 | 2560 | |
| | | -23.50 | 1768 | 2210 | 2628 | |
| | | -24.00 | 1814 | 2267 | 2696 | |
| | | -24.50 | 1853 | 2316 | 2754 | |
| | | -25.00 | 1890 | 2363 | 2810 | |
| | | -25.50 | 1927 | 2409 | 2864 | |
| | | -26.00 | 1964 | 2455 | 2920 | |
| | | -26.50 | 2004 | 2504 | 2978 | |
| | | -27.00 | 2050 | 2562 | 3046 | |
| | | -27.50 | 2096 | 2619 | 3114 | |
| | | -28.00 | 2135 | 2668 | 3172 | |
| | | -28.50 | 2169 | 2711 | 3223 | |

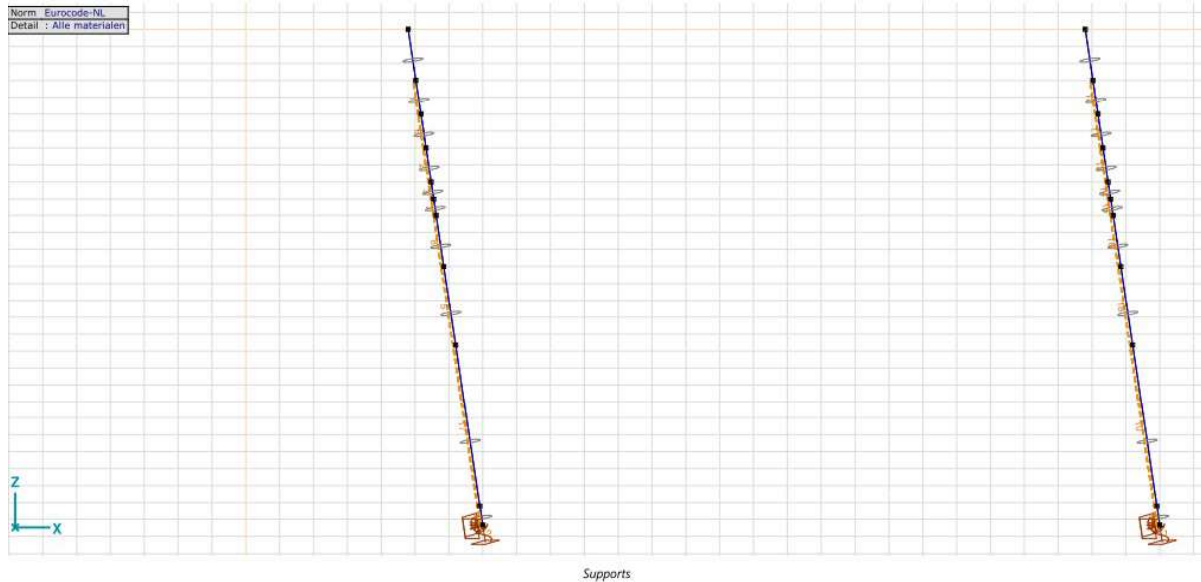
APPENDIX E

Berekening horizontale afdracht

In deze Appendix wordt de horizontale krachtsafdracht van de enkelpaalsfundering aangetoond.

Schematisering

De constructie wordt geschematiseerd als een elastisch ondersteunde ligger met begrensde beddingweerstand tot de passieve gronddruk met dwarsbelasting op de paalkop.



Figuur 10 Rekenmodel

In paragraaf 2.8.6 zijn de uitgangspunten gegeven voor de beddingen tegen de palen. Er is in het kader van de berekening voldoende nauwkeurigheid als onderscheid wordt gemaakt in beddingwaarde voor drie grondsoorten. Er zijn twee berekeningen uitgevoerd: een met lage veerwaarde (k gedeeld door $\sqrt{2}$) en een met hoge veerwaarde (k maal $\sqrt{2}$).

Tabel 16 Beddingwaarden

| Paal | Grond | k_h [kN/m ³] | schelp [-] | Diameter [m] | Gem. [kN/m] | Laag [kN/m] | Hoog [kN/m] |
|----------|-------|-------------------------------|---------------|-----------------|----------------|----------------|----------------|
| Ø610/850 | Veen | 1500 | 1,2 | 0,61 | 1098 | 776 | 1553 |
| | Klei | 3000 | 1,3 | 0,61 | 2379 | 1682 | 3364 |
| | Zand | 15000 | 2,0 | 0,85 | 25500 | 18031 | 36062 |

Het maatgevende bodemprofiel van sondering 2019-1008-17 is gebruikt, zie Tabel 16.

Tabel 17 Gehanteerd bodemprofiel

| Van [m] | Tot [m] | Omschrijving |
|------------|------------|--------------|
| 0,0 | -4,5 | Klei |
| -4,5 | -5,0 | Zand |
| -5,0 | -6,5 | Klei |
| -6,5 | -30,0 | Zand |

De maximale weerstand die in rekening mag worden gebracht kan niet groter zijn dan de passieve gronddruk. Over de bovenste meters waar de grootste verplaatsingen optreden, is vanuit die overweging de maximale reactie van de lijnondersteuning aan de paal in de berekening begrensd. Er is uitgegaan van een volumiek gewicht van 17 kN/m³, een grondwaterstand van 0,5 m beneden maaiveld.

De methode van Bijlage C van NEN 1997-1 is gevolgd. De factor voor passieve gronddruk is voor klei of veen op 2 aangehouden, voor zand op 3. Onderstaand zijn de maximale grondweerstand samengevat die zijn toegekend aan de elastische ondersteuning van de palen.

Tabel 18 Begrenzing passieve gronddruk

| Paal | Grond | Niveau [m] | p [kN/m ³] | k _{pa} [kN/m ³] | schelp [-] | Diameter [m] | Max. druk [kN] | Max. druk [kN] 50% |
|------|-------|---------------|---------------------------|---|---------------|-----------------|-------------------|-----------------------|
| Ø610 | Klei | 0 | 0 | | | | | |
| | | -1 | 12 | 2 | 1,3 | 0,61 | 9,5 | 4,8 |
| | | -2 | 19 | 2 | 1,3 | 0,61 | 24,6 | 12,3 |
| | | -3 | 26 | 2 | 1,3 | 0,61 | 35,7 | 17,8 |

Belasting

De belastingen zijn ontleend aan PLS-TOWER en opgenomen in Appendix A. De belastingen in de lokale richting van de paal zijn ingevoerd.

De belastingen van masttype S+12_c, S+18_s, S+24_s onderscheiden zich door een hoge "spatkracht" naar buiten in combinatie met extreme trek of drukbelasting. De belasting is zodanig dat dit tot te grote verplaatsingen leidt bij het maatgevende grondprofiel. Voor deze masttypes is voor het DO uitgaan van een tweepaalspoer. De maatgevende mast ten aanzien van horizontale belastingen over de overige masttypes is S+3_c, zie hiervoor het blad "trekbelasting lokaal" in Appendix A. In combinatie max. trek is de combinatie van Reta en R_{xi,lok} het grootst. De groen gearceerde belastingen zijn in AxisVM ingevoerd.

Tabel 19 Belastingen S+3_c

| Belasting | Combinatie | R _x [kN] | R _y [kN] | R _z [kN] | R _n [kN] | R _t [kN] | R _{t,lok} [kN] | R _{z,lok} [kN] |
|-------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk | ULS 1a_45 | -274 | -267 | -1838 | 5 | -382 | -8 | -1878 |
| Max. trek | ULS 1a_0,9_0,9_90 | 222 | -175 | 1433 | 33 | 281 | 23 | 1461 |
| Max. pos. torsie | ULS 5a Ah 11_bouwfase | 13 | -97 | -364 | 59 | -78 | 1 | -372 |
| Max. neg. torsie | ULS 5a Ba 11_bouwfase | -13 | -97 | -364 | -59 | -78 | 1 | -372 |
| Comb. trek+torsie | ULS 1a_0,9_0,9_90 | 222 | -175 | 1433 | 33 | 281 | 23 | 1461 |

Toetsing

De volgende aspecten zijn getoetst:

- Horizontale verplaatsing < 1/400 x b
- Buigspanning in de paal < f_y

De gronddruk wordt niet getoetst, deze is immers reeds begrensd.

Verplaatsingseisen worden gesteld voor de karakteristieke belastingen, zonder belastingfactoren. In de berekening is gewerkt met rekenwaarden. Als de berekening wordt uitgevoerd met belastingfactor (ULS of SpLS) moet om terug te rekenen worden gedeeld door de belastingfactor. De methode wordt hier toegelicht.

Er wordt gerekend met een verhouding ULS/SLS van 1,35. Voor de load case ULS-5a met maximale torsiebelasting wordt een factor 1,0 gerekend aangezien de belastingfactor in dat geval 1,0 bedraagt.

Onder de belasting door torsie verplaatsen beide poten in dezelfde richting, theoretisch wordt dan altijd voldaan aan de eis. Gekozen is om ook hier het uitgangspunt te hanteren van 1/400 x b. In de overige load cases met maximale wind (ULS-1a) kunnen beide poten tegengesteld vervormen. De toelaatbare vervorming is in die gevallen 50% van de toelaatbare waarde. De eisen zijn in Tabel 19 samengevat. De pootspreiding van maatgevende mast S+3_c is gebruikt.

Tabel 20 Toelaatbare horizontale belasting

| Mast | Basiseis | | Eis voor berekeningsresultaten | | | |
|-----------------------|----------|------------|--------------------------------|-----------------|-----------------|-------------|
| | b [m] | eis [-] | Eis [mm] | Factor 1 [-] | Factor 2 [-] | Eis [mm] |
| Extr. wind load cases | | 10,24 | 1/400 | 25,6 | 1,35 | 0,50 |
| Torsie load case | | 10,24 | 1/400 | 25,6 | 1,00 | 1,00 |

Resultaten

Zie berekening AxisVM:

Tabel 21 Resultaten

| | Berekend | Toelaatbaar | Unity-check |
|---------------------------|----------|-----------------------|-------------|
| Spanningscheck buispaal | 121 | 355 N/mm ² | 0,34 OK |
| Verplaatsing ULS-1a ex/ey | 15,4 | 17,3 mm | 0,89 OK |
| Verplaatsing ULS-5a ex/ey | 20,8 | 25,6 mm | 0,81 OK |

Conclusie: de enkelpaalsfundering voldoet.

Bijlage: rapport AxisVM

Project

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| [II], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Vz, Lijnen (gevuld), Vooraanzicht | | 19 |
| Staafkrachten [Non-lin., Omhullende (UGT)] | | 20 |
| [II], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, eX, Lijnen | | 22 |
| [II], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, eY, Lijnen | | 23 |
| [II], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, eZ, Lijnen, Vooraanzicht | | 24 |
| [II], > S 355, Non-lin., Co #1 [1] (1,000), Onmiddellijke doorbuiging, eY, Lijnen | | 25 |
| [II], > S 355, Non-lin., Co #3 [1] (1,000), Onmiddellijke doorbuiging, eY, Lijnen | | 26 |
| Knoopverplaatsingen [Non-lin., Omhullende (UGT), S 355] | | 27 |
| [II], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Rx (knoopopl.), Lijnen, Vooraanzicht | | 28 |
| [II], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Ry (lijnopp.), Lijnen (gevuld), Vooraanzicht | | 29 |
| [II], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Rz (lijnopp.), Lijnen (gevuld), Vooraanzicht | | 30 |
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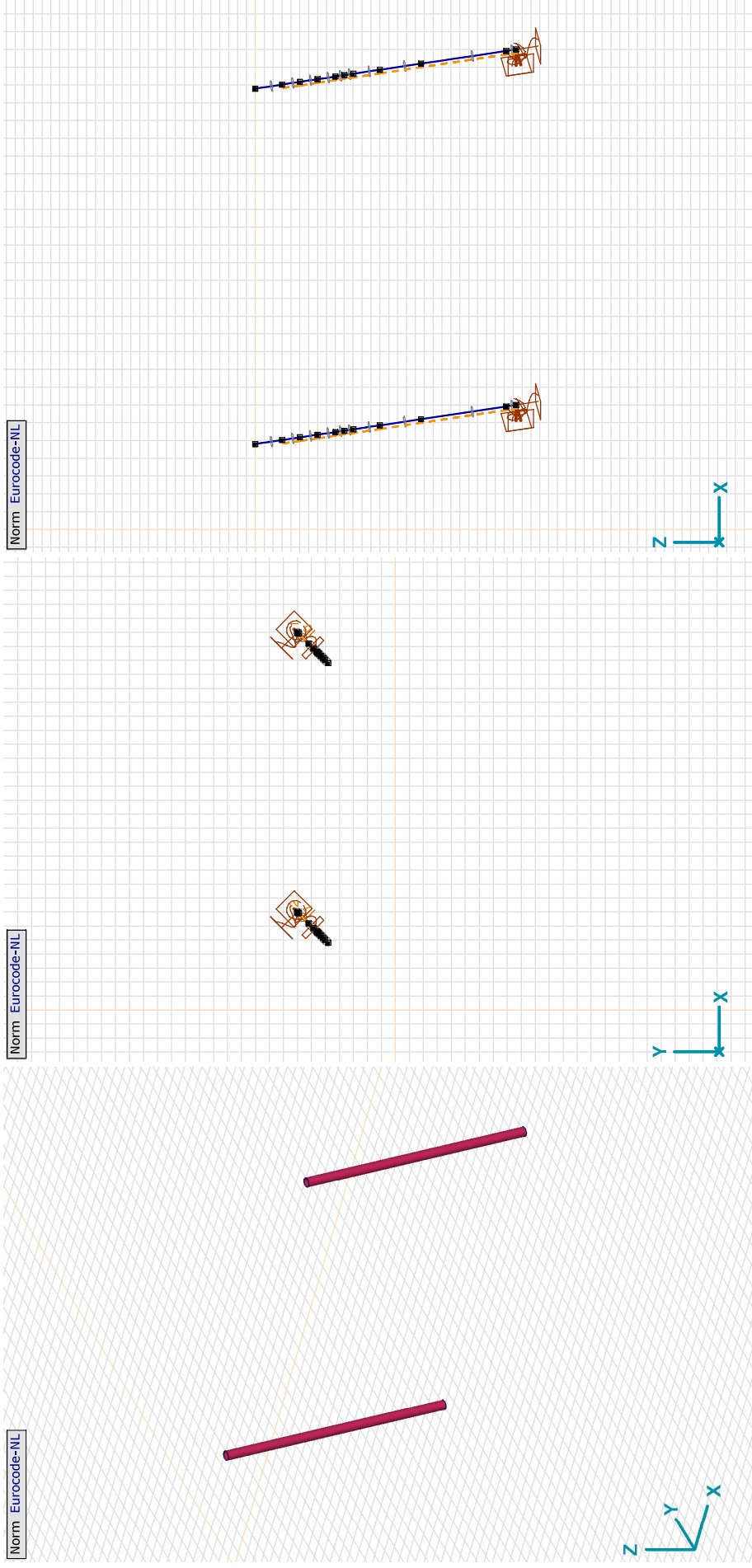
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Geometry

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Materialen

| Naam | Type | Nationale norm | Materiaalnorm | Model | E_x [N/mm ²] | E_y [N/mm ²] | ν | α_T [1/°C] | ρ [kg/m ³] | Materiaal kleur | Contour kleur | Structuur | P_1 |
|------|-------|----------------|---------------|---------|----------------------------|----------------------------|--------|-------------------|-----------------------------|-----------------|---------------|-----------|--|
| 1 | S 355 | Staal | Eurocode-NL | 10025-2 | Lineair | 210000 | 210000 | 0,30 | 1,2E-5 | 7850 | | Steel | f_{yk} [N/mm ²] = 355,00 |

| Naam | P_2 | P_3 | P_4 | P_5 | P_6 | P_7 | P_8 | P_9 | P_{10} | P_{11} | P_{12} | P_{13} | P_{14} |
|------|-------|--|--|--|-------|-------|-------|-------|----------|----------|----------|----------|----------|
| 1 | S 355 | f_{tk} [N/mm ²] = 510,00 | f_{yk} [N/mm ²] = 335,00 | f_{t0} [N/mm ²] = 470,00 | | | | | | | | | |

Naam: Materiaalnaam; **Type:** Type materiaal; **Model:** Materiaal model; **E_x :** Elasticiteitsmodulus in lokale x richting; **E_y :** Elasticiteitsmodulus in lokale y richting; **ν :** Poisson's verhouding; **α_T :** Warmteuitzettingscoëfficiënt; **ρ :** Dichtheid; **Materiaal kleur:** Materiaalkleur; **Contour kleur:** Contourkleur; **$P_1, P_2, P_3, P_4, P_5, P_6, P_7, P_8, P_9, P_{10}, P_{11}, P_{12}, P_{13}, P_{14}$:** Ontwerpparameter.

Profielen

| Naam | Tekening | Productie | Vorm | h [mm] | b [mm] | tw [mm] | tf [mm] | r_1 [mm] | r_2 [mm] | r_3 [mm] | Ax [mm ²] | Ay [mm ²] | Az [mm ²] | I_x [mm ⁴] | I_y [mm ⁴] | I_z [mm ⁴] |
|------|------------------|-----------|------|----------|----------|-----------|-----------|------------|------------|------------|-------------------------|-------------------------|-------------------------|--------------------------|--------------------------|--------------------------|
| 1 | ROR 610,00* 10,0 | Gewalst | Buis | 610,0 | 610,0 | 10,0 | 10,0 | 0 | 0 | 0 | 18825,65 | 9417,10 | 9417,19 | 1,7E+09 | 8,46E+08 | 8,46E+08 |
| 2 | O 610x9 | Gewalst | Buis | 610,0 | 610,0 | 9,2 | 9,2 | 0 | 0 | 0 | 17361,19 | 8683,87 | 8683,99 | 1,57E+09 | 7,83E+08 | 7,83E+08 |

| Naam | I_yz [mm ⁴] | I_1 [mm ⁴] | I_2 [mm ⁴] | α [°] | $I\omega$ [mm ⁶] | $W_{1,elit}$ [mm ³] | $W_{1,elb}$ [mm ³] | $W_{2,elb}$ [mm ³] | $W_{1,pl}$ [mm ³] | $W_{2,pl}$ [mm ³] | i_y [mm] | i_z [mm] | H_y [mm] | H_z [mm] |
|------|---------------------------|--------------------------|--------------------------|--------------|------------------------------|---------------------------------|--------------------------------|--------------------------------|-------------------------------|-------------------------------|------------|------------|------------|------------|
| 1 | ROR 610,00* 10,0 | 0 | 8,46E+08 | 8,46E+08 | 0 | 0 | 2774803,00 | 2774803,00 | 2774803,00 | 2774803,00 | 2774803,00 | 2774803,00 | 3593483,00 | 3593483,00 |
| 2 | O 610x9 | 0 | 7,83E+08 | 7,83E+08 | 0 | 0 | 2568402,00 | 2568402,00 | 2568402,00 | 2568402,00 | 2568402,00 | 2568402,00 | 3320108,00 | 3320108,00 |

| Naam | Y_G [mm] | Z_G [mm] | Y_s [mm] | Z_s [mm] | β_y [mm] | β_z [mm] | β_w [mm] | S.p. |
|------|------------------|------------|------------|------------|----------------|----------------|----------------|------|
| 1 | ROR 610,00* 10,0 | 305,0 | 305,0 | 0 | 0 | 0 | 1,8 | 5 |
| 2 | O 610x9 | 305,0 | 305,0 | 0 | 0 | 0 | 0 | 5 |

Naam: Doorsnede naam; **Productieproces:** Vorm; **Profiel:** h: Doorsnede hoogte; **b:** Doorsnede breedte; **tw:** Lijfdikte; **tf:** Flensdikte; **r_1, r_2, r_3 :** Afrondingswaarde; **Ax:** Doorsnede-oppervlak; **Ay:** Az: Afschuivingsoppervlak; **Ix:** Torietraagheidsmoment; **Iy:** Iz: Buigtraagheidsmoment; **Iyz:** Centrifugaal traagheidsmoment; **I_1, I_2 :** Hoofdbuigtraagheidsmoment; **I_1, I_2 :** Hoofdbuigtraagheidsmoment; **α :** Hoofdrichtingen; **I ω :** Krommingsconstante; **$W_{1,elit}, W_{1,elb}, W_{2,elit}, W_{2,elb}$:** Elastisch weerstandsmoment; **$W_{1,pl}, W_{2,pl}$:** Plastisch weerstandsmoment; **i_y, i_z :** Traagheidsstraal; **H_y, H_z :** Afmeting in lokale Y-richting; **H_z :** Afmeting in lokale Z-richting; **Y_G, Z_G :** Z-coördinaat van het zwaartepunt; **Y_s, Z_s :** Z-coördinaat van het afschuivingsmiddelpunt (toisie); **z_0 :** Z-coördinaat van het afschuivingsmiddelpunt (torsie); **$\beta_y, \beta_z, \beta_w$:** Wagner's coëfficiënt; **S.p.:** Spanningspunten;

Project

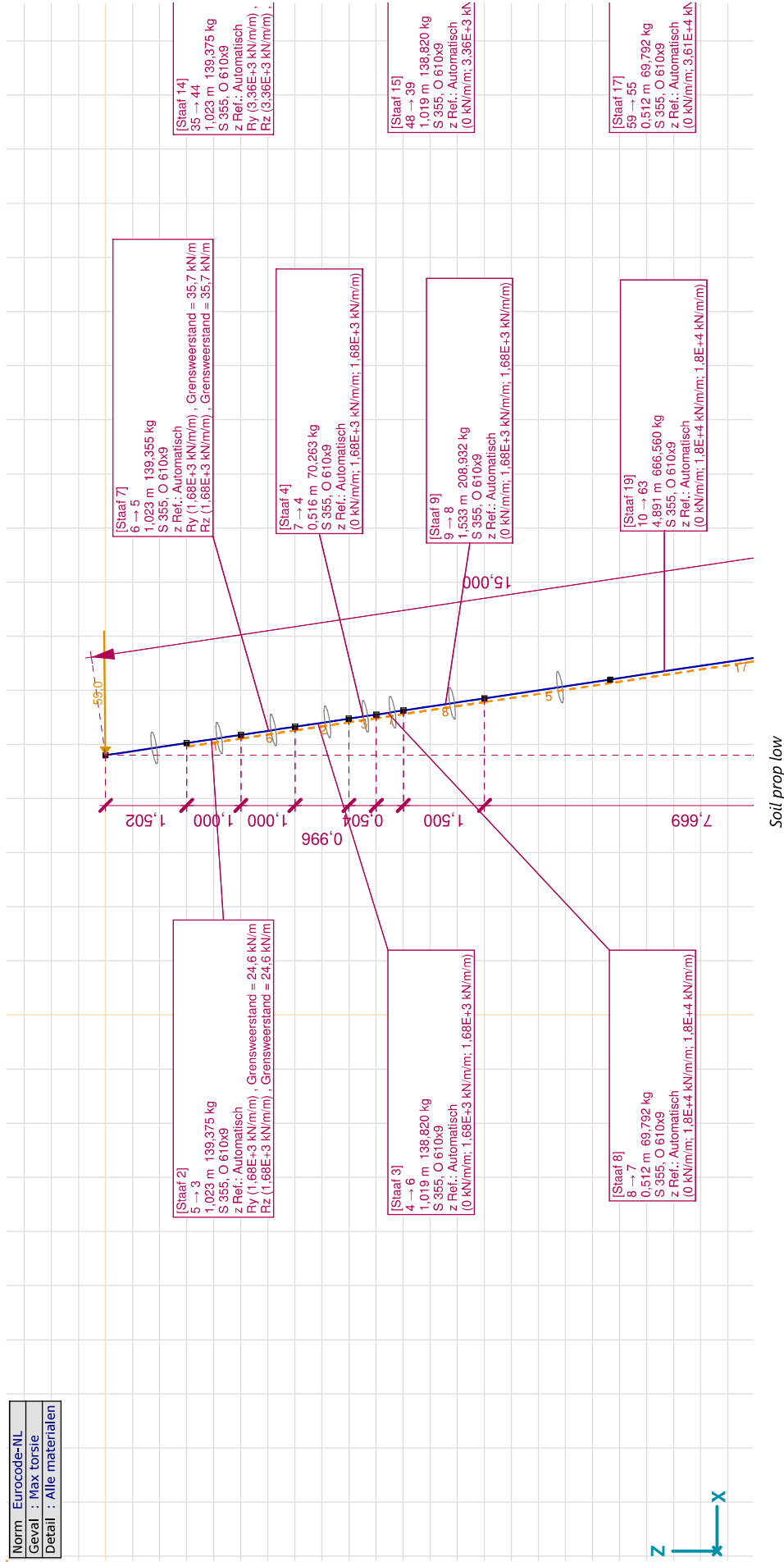
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| | |
|--------|-----------------|
| Norm | Eurocode-NL |
| Geval | Max torsie |
| Detail | Alle materialen |



Project

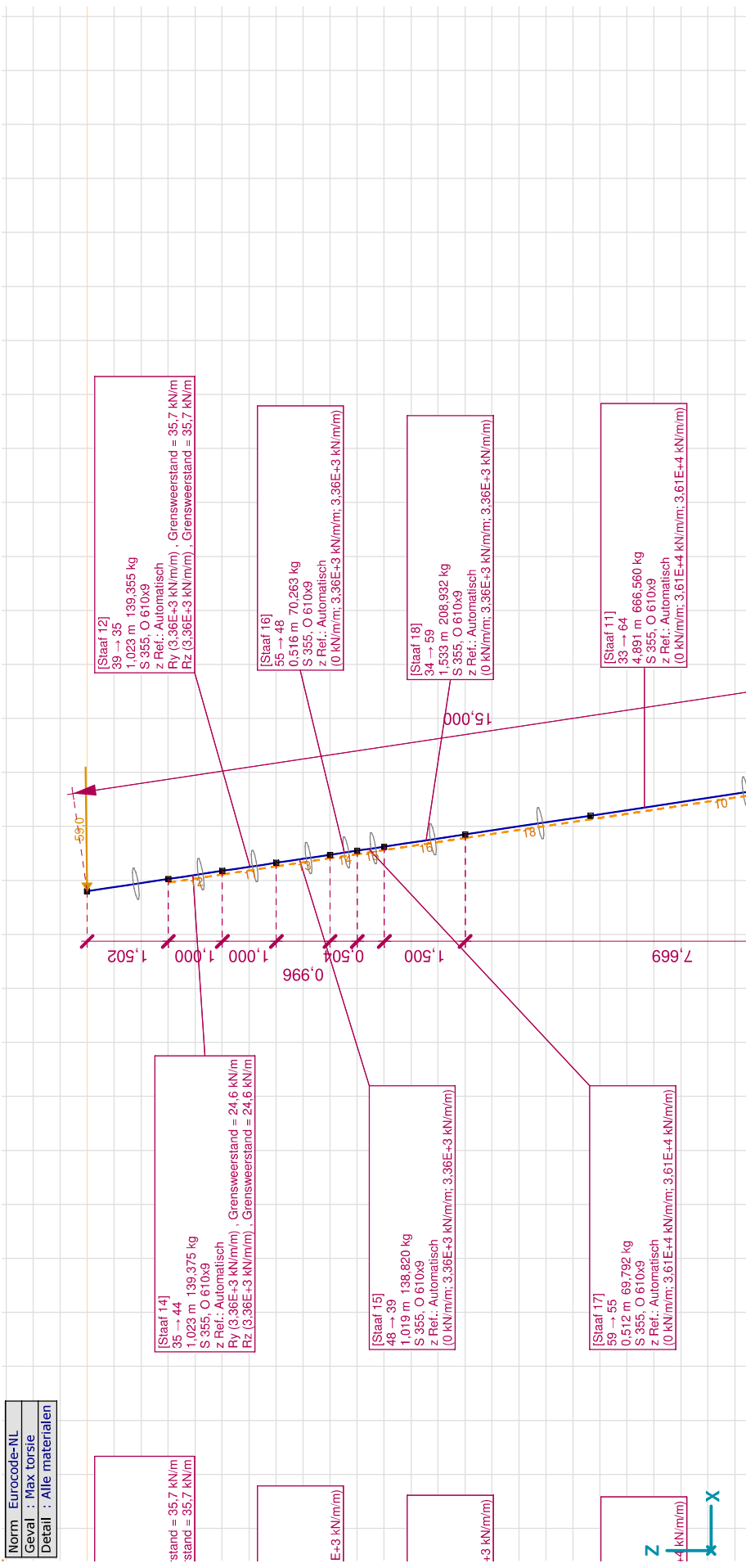
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| | |
|--------|-------------------|
| Norm | Eurocode-NL |
| Geval | : Max torsie |
| Detail | : Alle materialen |



stand = 35.7 kN/m
stand = 35.7 kN/m

E+3 kN/m(m)

+3 kN/m(m)

Z
+4 kN/m(m)



Project

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Veereigenschappen

| | Naam | Type | Vrijheidsgraden | Model | K | K_v | NL | Grenswaarde | K_T | K_C |
|---|-----------------------|------|-----------------|--------------|---------------|---------------|------------------|-------------|---------------|---------------|
| 1 | Verend - translatie | N-N | translatie | Lineair | 1E+0 kN/m | 1E+0 kN/m | Symmetrisch | — | 1E+0 kN/m | 1E+0 kN/m |
| 2 | Rigid - Translational | N-N | translatie | Lineair | 1E+10 kN/m | 1E+10 kN/m | Symmetrisch | — | 1E+10 kN/m | 1E+10 kN/m |
| 3 | Verend - rotatie | N-N | rotatie | Lineair | 1E+0 kNm/rad | 1E+0 kNm/rad | Symmetrisch | — | 1E+0 kNm/rad | 1E+0 kNm/rad |
| 4 | Vast - rotatie | N-N | rotatie | Lineair | 1E+10 kNm/rad | 1E+10 kNm/rad | Symmetrisch | — | 1E+10 kNm/rad | 1E+10 kNm/rad |
| 5 | Rigid_comp_only | N-N | translatie | NL elastisch | 1E+10 kN/m | 1E+10 kN/m | Druk Alleen druk | 2415,0 kN | 0 kN/m | 1E+10 kN/m |
| 6 | Linear 5E+2 kNm/rad | N-N | rotatie | Lineair | 5E+2 kNm/rad | 5E+2 kNm/rad | Symmetrisch | — | 5E+2 kNm/rad | 5E+2 kNm/rad |
| 7 | Linear 1E+1 kNm/rad | N-N | rotatie | Lineair | 1E+1 kNm/rad | 1E+1 kNm/rad | Symmetrisch | — | 1E+1 kNm/rad | 1E+1 kNm/rad |
| 8 | Linear 1E+5 kN/m | N-N | translatie | Lineair | 1E+5 kN/m | 1E+5 kN/m | Symmetrisch | — | 1E+5 kN/m | 1E+5 kN/m |
| 9 | Linear 3,3E+5 kN/m | N-N | translatie | Lineair | 3,3E+5 kN/m | 3,3E+5 kN/m | Symmetrisch | — | 3,3E+5 kN/m | 3,3E+5 kN/m |

Naam: Naam van de veereigenschappen; **Model:** Materiaal model; **K:** Initiële stijfheid; **K_v :** Trillingsstijfheid; **NL:** Niet-lineaire parameters; **K_T :** Initiële stijfheid, onder trek; **K_C :** Initiële stijfheid, onder druk;

Referenties

| | Naam | Type | X_1 [m] | Y_1 [m] | Z_1 [m] | X_2 [m] | Y_2 [m] | Z_2 [m] | X_3 [m] | Y_3 [m] | Z_3 [m] |
|---|------|------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 1 | R1 | Ve | 5,571 | 5,571 | 0 | 4,864 | 6,278 | -0,009 | | | |
| 2 | R2 | Ve | 5,571 | 5,571 | 0 | 5,718 | 5,718 | -0,978 | | | |
| 3 | R3 | Ve | 4,800 | 4,800 | 0 | 5,507 | 5,507 | 0 | | | |

Naam: Referentie naam; **Type:** Type van %s;

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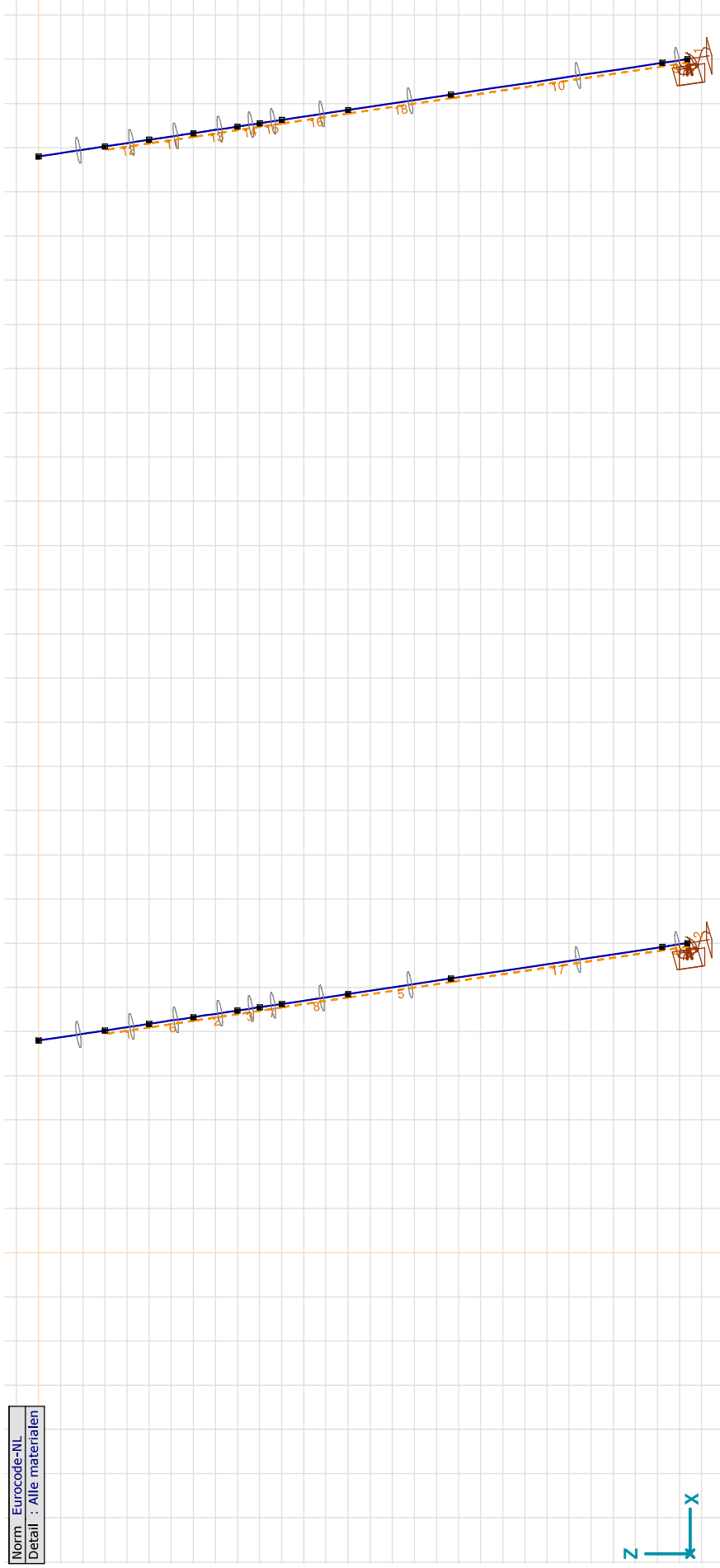
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Norm Eurocode-NL
Detail : Alle materialen



Supports

Project

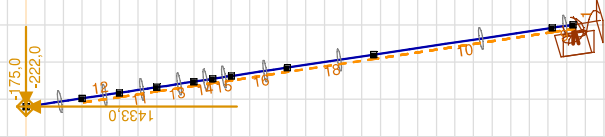
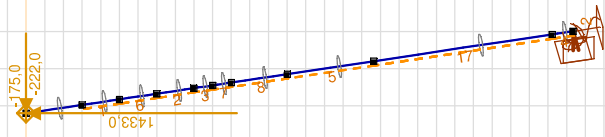
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| | |
|-------|-------------|
| Norm | Eurocode-NL |
| Geval | : Max trek |



Max trek



Project

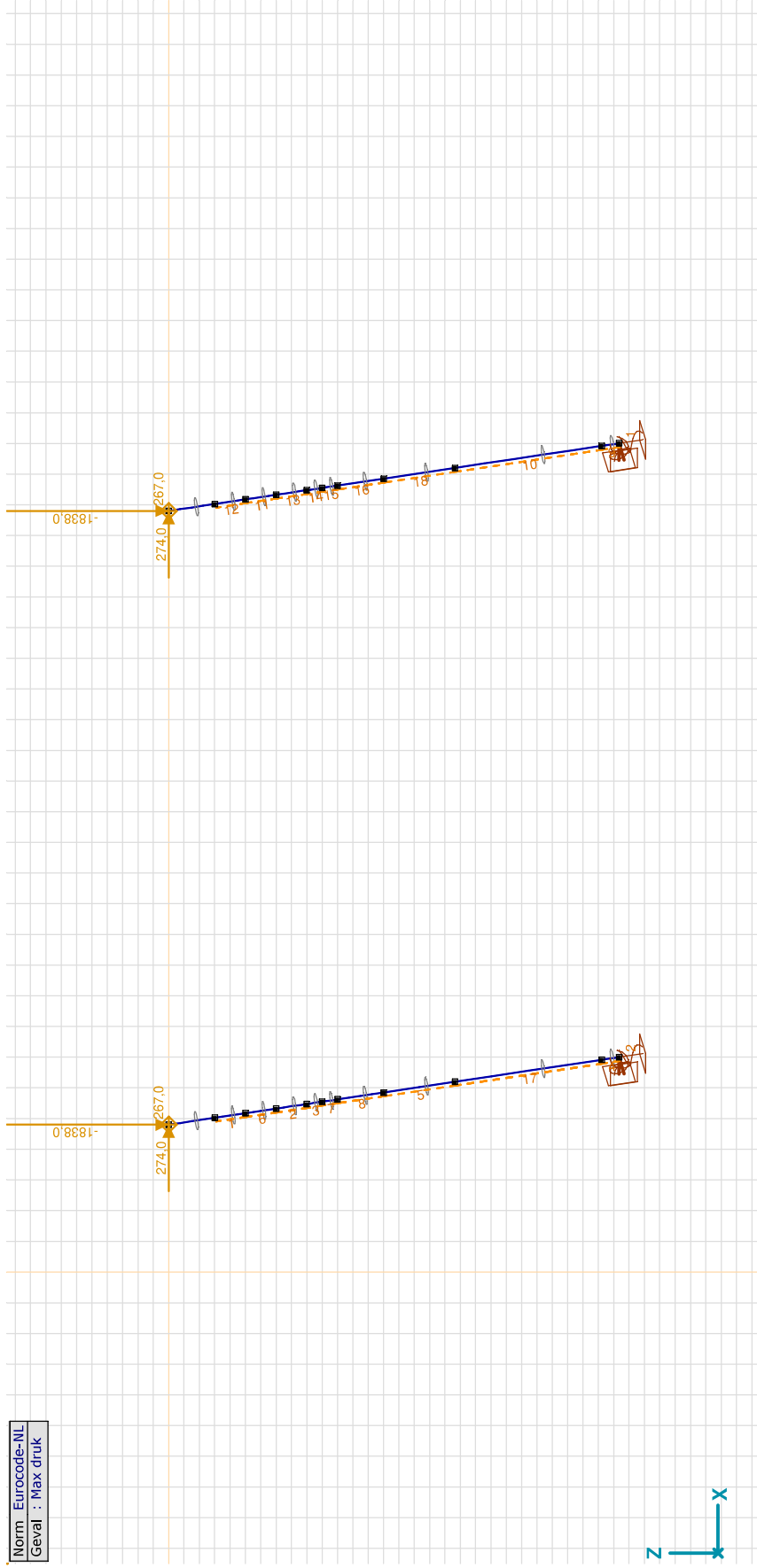
Analysis by

Model: **ZWO380 20210927 1-p rev1.axs**

Max trek: Knoopbelastingen

| Richting | F _x [kN] | F _y [kN] | F _z [kN] | M _x [kNm] | M _y [kNm] | M _z [kNm] |
|----------|---------------------|---------------------|---------------------|----------------------|----------------------|----------------------|
| 1 | -222,0 | -175,0 | 1433,0 | 0 | 0 | 0 |
| 40 | -222,0 | -175,0 | 1433,0 | 0 | 0 | 0 |

F_x, F_y, F_z: Belastingkracht component; M_x, M_y, M_z: Belastingmoment component;



Max druk

Project

Analysis by

Model: **ZWO380 20210927 1-p rev1.axs**

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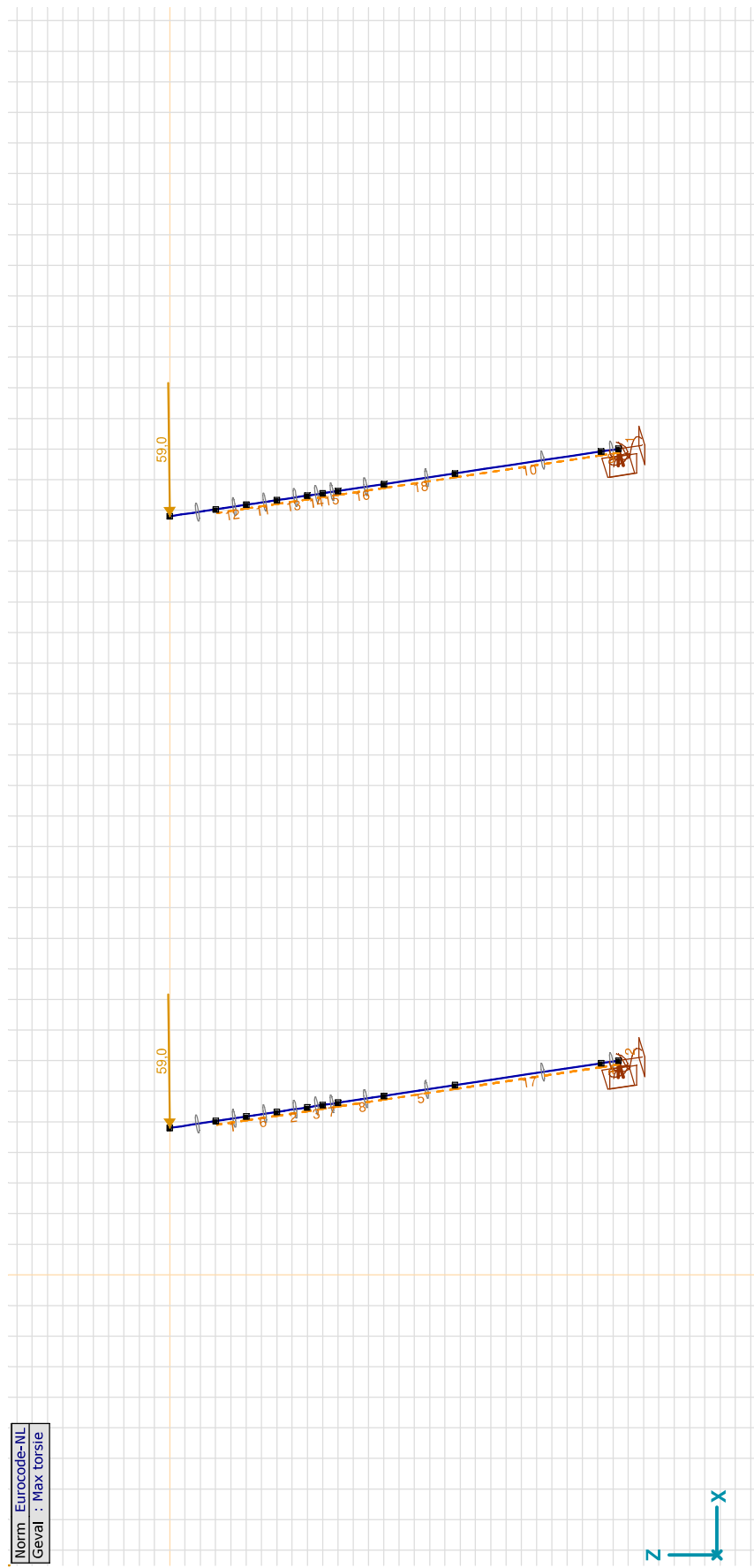
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Max druk: Knoopbelastingen

| | Richting | Fx [kN] | Fy [kN] | Fz [kN] | Mx [kNm] | My [kNm] | Mz [kNm] |
|----|----------|------------|------------|------------|-------------|-------------|-------------|
| 1 | Globaal | 274,0 | 267,0 | -1838,0 | 0 | 0 | 0 |
| 40 | Globaal | 274,0 | 267,0 | -1838,0 | 0 | 0 | 0 |

Fx, Fy, Fz: Belastingkracht component; Mx, My, Mz: Belastingmoment component;

Norm Eurocode-NL
Geval : Max torsie



Max torsie

Project

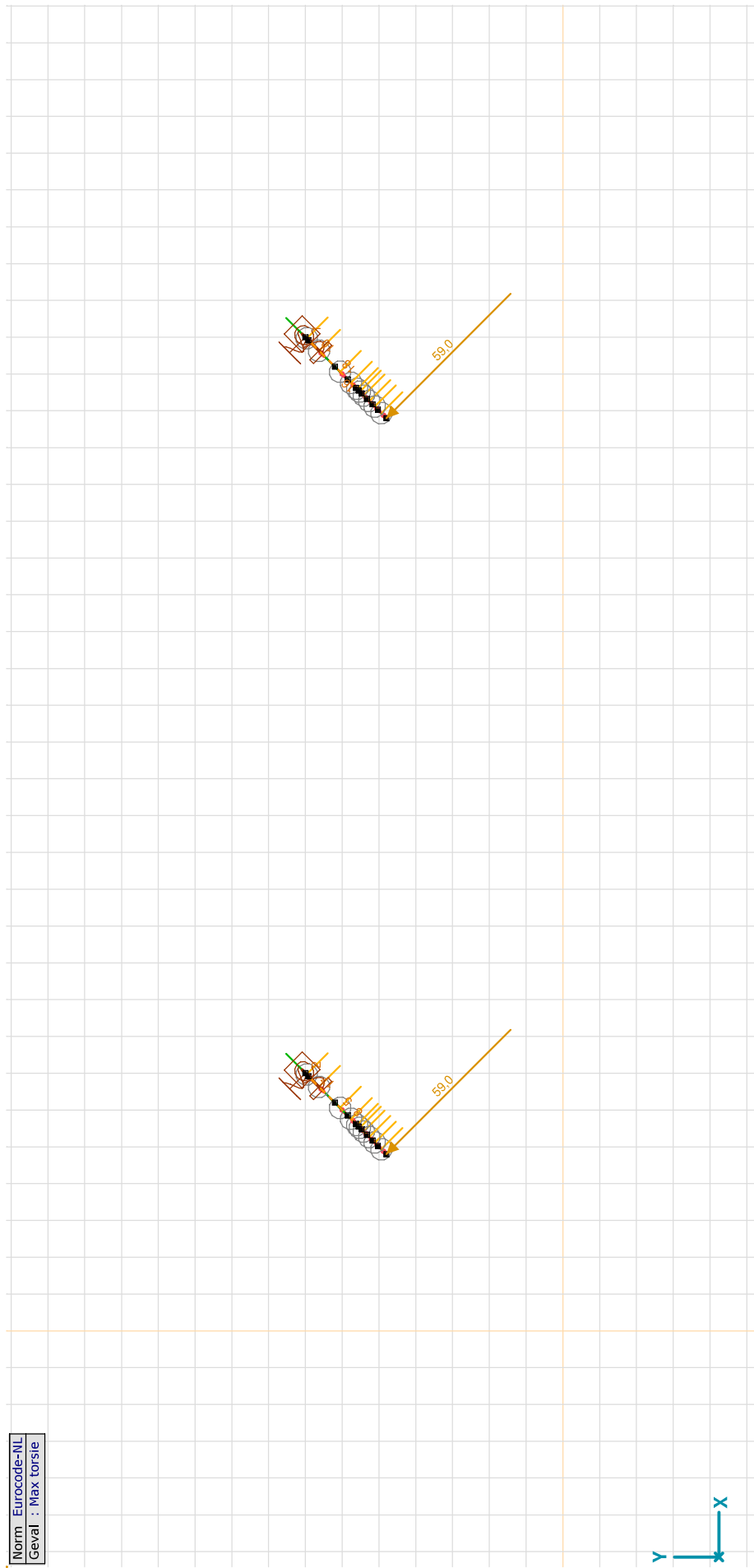
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Norm Eurocode-NL
Geval : Max torsie



Max torsie, Bovenaanzicht

Project

Analysis by

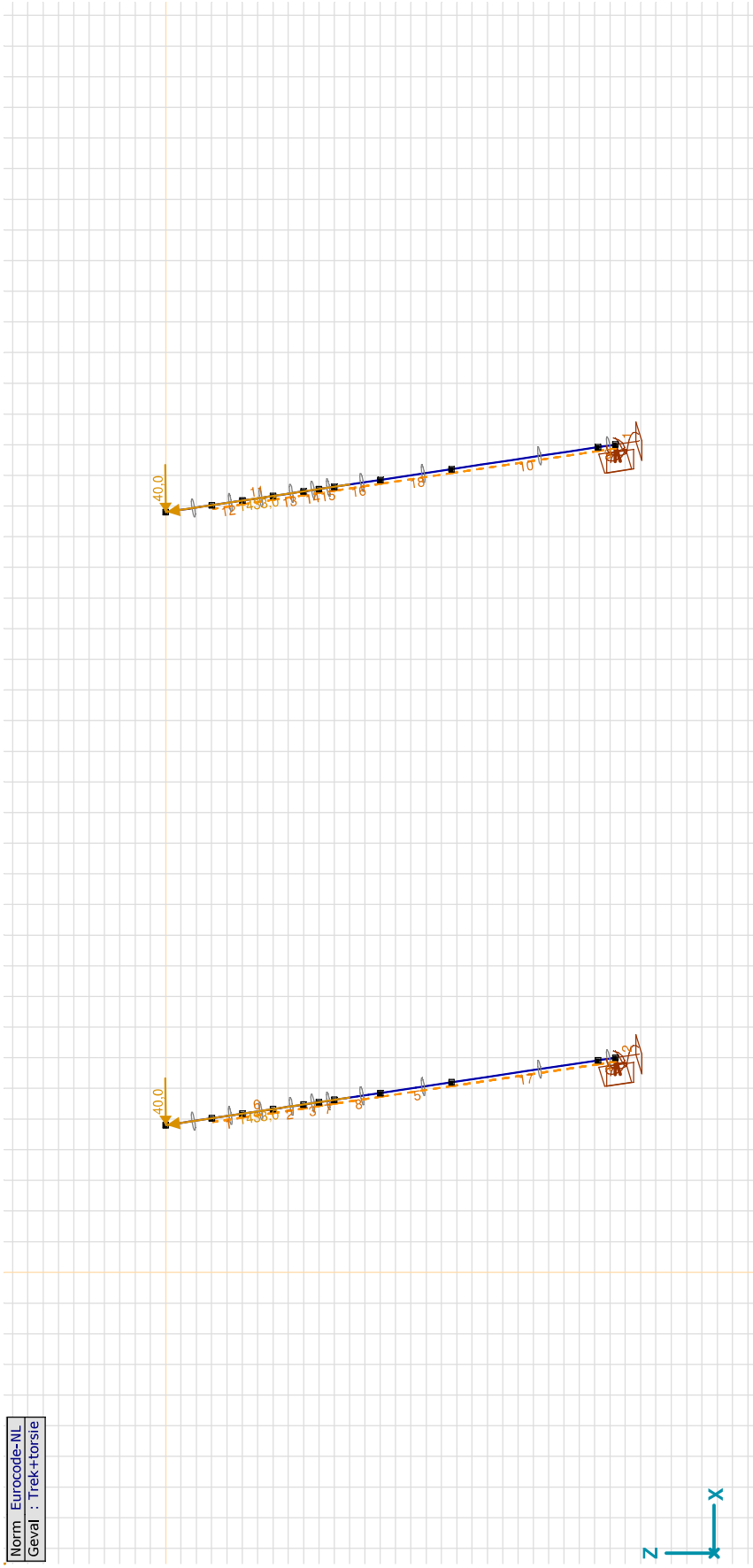
Model: **ZWO380 20210927 1-p rev1.axs**

Max torsie: Knoopbelastingen [S 355]

| | Richting | F _x [kN] | F _y [kN] | F _z [kN] | M _x [kNm] | M _y [kNm] | M _z [kNm] |
|----|----------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| 1 | R1 | 59,0 | | | 0 | | |
| 40 | R1 | 59,0 | | | 0 | | |

F_x, F_y, F_z: Belastingkracht component; M_x, M_y, M_z: Belastingmoment component;

Norm Eurocode-NL
Geval : Trek+torsie



Trek+torsie

Project

Analysis by

Model: **ZWO380 20210927 1-p rev1.axs**

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Trek+torsie: Knoopbelastingen [S 355]

| Richting | F _x [kN] | F _y [kN] | F _z [kN] | M _x [kNm] | M _y [kNm] | M _z [kNm] |
|----------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| 1 | 40,0 | | | 0 | | |
| 40 | 40,0 | | 0 | | | |

F_x, F_y, F_z: Belastingkracht component; **M_x, M_y, M_z:** Belastingmoment component;**Trek+torsie: Gecentreerde belastingen op staven [S 355]**

| Type | Lengte [m] | a/d | Pos. | F _x [kN] | F _y [kN] | F _z [kN] | M _x [kNm] | M _y [kNm] | M _z [kNm] | Excentriciteit | e _y [mm] | e _z [mm] |
|------|---------------|-----|-------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|---------------------|------------------------|------------------------|
| 1 | 1,535 | d | 1,500 | 1433,0 | 0 | 0 | 0 | 0 | 0 | Geen excentriciteit | | |
| 13 | 1,535 | d | 1,500 | 1433,0 | 0 | 0 | 0 | 0 | 0 | Geen excentriciteit | | |

Type: Belastingtype; **Lengte:** Elementlengte; **a/d:** Positie als verhouding (a) of lengte (d); **Pos.:** Positie; **F_x, F_y, F_z:** Belastingkracht component; **M_x, M_y, M_z:** Belastingmoment component;**Gebruiker gedefinieerde belastingcombinaties uit belastinggevallen**

| Naam | Type | Max trek | Max druk | Max torsie | Trek+torsie | Commentaar |
|------|-------|----------|----------|------------|-------------|------------|
| 1 | Co #1 | UGT | 1,00 | 0 | 0 | |
| 2 | Co #2 | UGT | 0 | 1,00 | 0 | |
| 3 | Co #3 | UGT | 0 | 0 | 1,00 | |
| 4 | Co #4 | UGT | 0 | 0 | 0 | 1,00 |

Naam: Naam belastingcombinatie; **Type:** Type belastingcombinatie; **Max trek, Max druk, Max torsie, Trek+torsie:** Factor;

Project

Analysis by

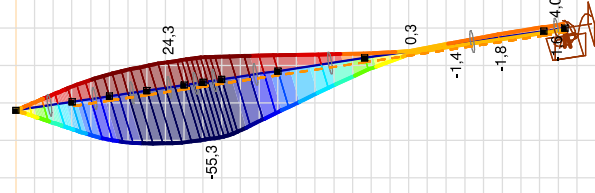
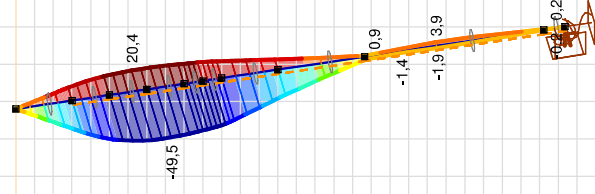
Model: ZWO380 20210927 1-p rev1.axs

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| | |
|--------------------------|-----------------------|
| Niet-lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : My [kNm] |
| Detail Max | : 24,3 |
| Detail Min | : -55,3 |
| Detail | : Alle materialen |

| | |
|----------|-------|
| My [kNm] | 24,3 |
| | 18,6 |
| | 12,9 |
| | 7,2 |
| | 1,5 |
| | -4,1 |
| | -9,8 |
| | -15,5 |
| | -21,2 |
| | -26,9 |
| | -32,6 |
| | -38,3 |
| | -44,0 |
| | -49,6 |
| | -55,3 |



[III], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, My, Lijnen (gevuld), Vooraanzicht

Project

Analysis by

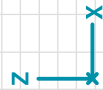
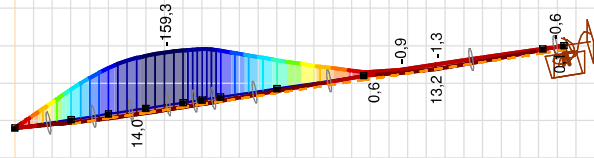
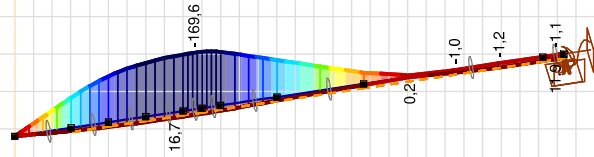
Model: ZWO380 20210927 1-p rev1.axs

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| Niet-lineaire berekening | |
|--------------------------|-----------------------|
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Mz [kNm] |
| Detail Max | : 16,7 |
| Detail Min | : -169,6 |
| Detail | : Alle materialen |

| Mz [kNm] |
|----------|
| 16,7 |
| 3,4 |
| -9,9 |
| -23,2 |
| -36,5 |
| -49,8 |
| -63,1 |
| -76,4 |
| -89,8 |
| -103,1 |
| -116,4 |
| -129,7 |
| -143,0 |
| -156,3 |
| -169,6 |



[III], > S 355; Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Mz, Lijnen (gevuld), Vooraanzicht

Project

Analysis by

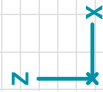
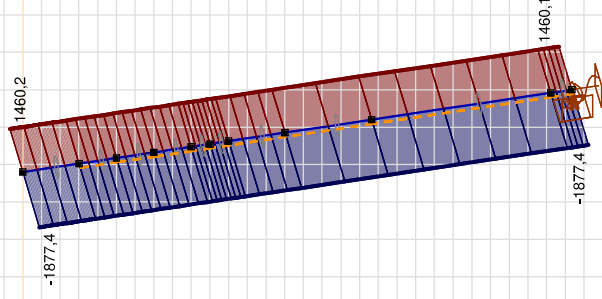
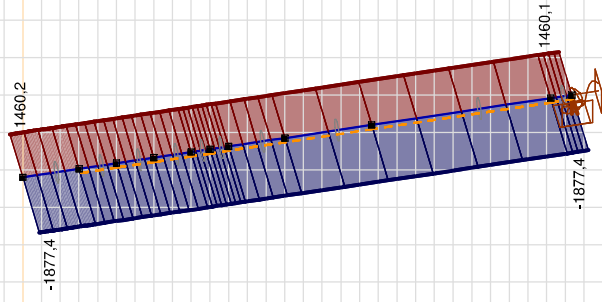
Model: ZWO380 20210927 1-p rev1.axs

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Pag. 17

| Niet-lineaire berekening | |
|--------------------------|-----------------------|
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Nx [kN] |
| Detail Max | : 1460,2 |
| Detail Min | : -1877,4 |
| Detail | : Alle materialen |

| Nx [kN] |
|---------|
| 1460,2 |
| 1221,8 |
| 983,4 |
| 745,0 |
| 506,6 |
| 268,2 |
| 29,8 |
| -208,6 |
| -447,0 |
| -685,4 |
| -923,8 |
| -1162,2 |
| -1400,6 |
| -1639,0 |
| -1877,4 |



[III], > S 355; Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Nx, Lijnen (gevuld), Vooraanzicht

Project

Analysis by

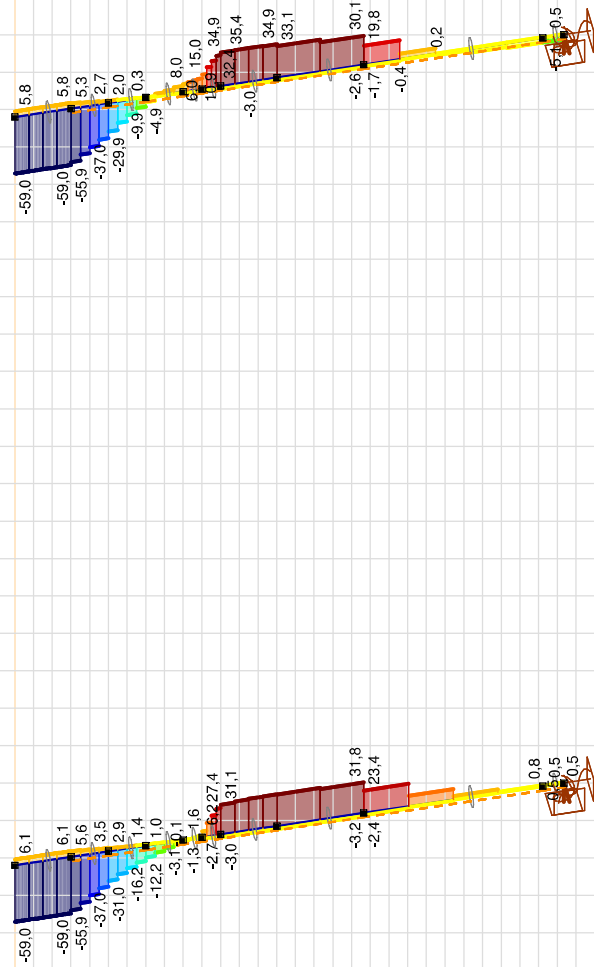
Model: ZWO380 20210927 1-p rev1.axs

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Pag. 18

| | |
|--------------------------|-----------------------|
| Niet-lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Vy [kN] |
| Detail Max | : 35,4 |
| Detail Min | : -59,0 |
| Detail | : Alle materialen |

| | |
|---------|--|
| Vy [kN] | |
| 35,4 | |
| 28,7 | |
| 21,9 | |
| 15,2 | |
| 8,4 | |
| 1,7 | |
| -5,1 | |
| -11,8 | |
| -18,5 | |
| -25,3 | |
| -32,0 | |
| -38,8 | |
| -45,5 | |
| -52,3 | |
| -59,0 | |



[III], > S 355; Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Vy, Lijnen (gevuld), Vooraanzicht

Project

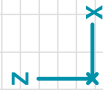
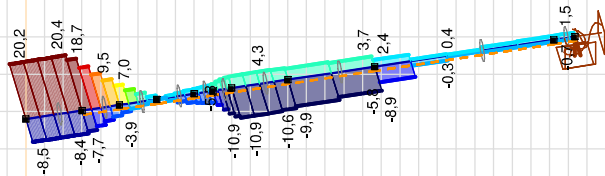
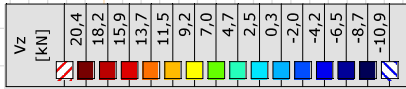
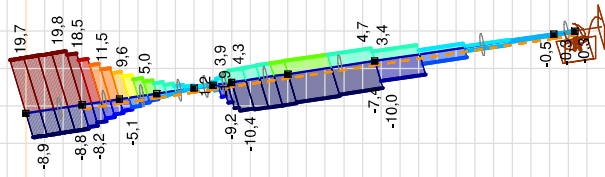
Analysis by

Model: ZWO380 20210927 1-p rev1.axs

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Pag. 19

| | |
|--------------------------|-----------------------|
| Niet-lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Vz [kN] |
| Detail Max | : 20,4 |
| Detail Min | : -10,9 |
| Detail | : Alle materialen |



[III], > S 355; Non-lin., Omhullende (Standaard), Ommiddellijke doorbuiging, Vz, Lijnen (gevuld), Vooraanzicht

Project

Analysis by

Model: **ZWO380 20210927 1-p rev1.axis**

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Staaftkrachten [Non-lin., Omhullende (UGT)]

| Ext. | Prof. | Doorsnede naam | C | min. max. | Geval | Pos. [m] | Knoop | Nx [kN] | Vy [kN] | Vz [kN] | Tx [kNm] | My [kNm] | Mz [kNm] | B [kNm ²] |
|------|-------|----------------|----|--------------|-------------------|----------|-------|---------|---------|---------|----------|----------|----------|-----------------------|
| 1 | 2 | O 610x9 | Nx | min | Co #2 [1] (1,000) | 0 | (3) | -1877,4 | 6,1 | -8,8 | 0 | 13,6 | 9,4 | 0 |
| 2 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (5) | -1877,4 | 3,5 | -5,1 | 0 | 20,4 | 14,0 | 0 |
| 3 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (4) | -1877,4 | 0,1 | -0,1 | 0 | 24,3 | 16,7 | 0 |
| 4 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (7) | -1877,4 | -0,5 | 0,7 | 0 | 24,1 | 16,6 | 0 |
| 5 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (2) | -1877,4 | 0,1 | -0,2 | 0 | -1,6 | -1,1 | 0 |
| 6 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 1,187 | (65) | -1877,4 | -3,3 | 4,8 | 0 | 10,0 | 6,9 | 0 |
| 7 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (6) | -1877,4 | 1,4 | -2,1 | 0 | 23,5 | 16,2 | 0 |
| 8 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (8) | -1877,4 | -2,7 | 3,9 | 0 | 22,7 | 15,6 | 0 |
| 9 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 1,150 | (29) | -1877,4 | -3,0 | 4,3 | 0 | 21,1 | 14,5 | 0 |
| 10 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (32) | -1877,4 | 0,5 | -0,7 | 0 | 0,2 | 0,1 | 0 |
| 11 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (33) | -1877,4 | 0,5 | -0,7 | 0 | -0,2 | -0,1 | 0 |
| 12 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (39) | -1877,4 | 0,3 | -0,4 | 0 | 20,4 | 14,0 | 0 |
| 13 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (44) | -1877,4 | 5,8 | -8,4 | 0 | 13,0 | 8,9 | 0 |
| 14 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (35) | -1877,4 | 2,7 | -3,9 | 0 | 18,8 | 12,9 | 0 |
| 15 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (48) | -1877,4 | -1,0 | 1,5 | 0 | 19,5 | 13,4 | 0 |
| 16 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (55) | -1877,4 | -1,5 | 2,1 | 0 | 18,5 | 12,7 | 0 |
| 17 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (59) | -1877,4 | -2,8 | 4,0 | 0 | 16,8 | 11,6 | 0 |
| 18 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 1,150 | (60) | -1877,4 | -2,9 | 4,3 | 0 | 15,2 | 10,4 | 0 |
| 19 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (10) | -1877,4 | 0,1 | -0,1 | 0 | -1,7 | -1,2 | 0 |
| 20 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 1,187 | (73) | -1877,4 | -2,8 | 4,1 | 0 | 5,3 | 3,7 | 0 |
| 1 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 1,152 | (14) | 1460,2 | -28,7 | 19,7 | 0 | -7,6 | -11,0 | 0 |
| 2 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,767 | (17) | 1460,2 | -27,1 | 18,5 | 0 | -35,1 | -51,2 | 0 |
| 3 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,764 | (22) | 1460,1 | -5,5 | 3,7 | 0 | -53,9 | -78,7 | 0 |
| 4 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,387 | (23) | 1460,1 | -0,7 | 0,5 | 0 | -55,3 | -80,8 | 0 |
| 5 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0 | (2) | 1460,1 | 0,4 | -0,3 | 0 | 4,0 | 5,8 | 0 |
| 6 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0 | (63) | 1460,1 | 14,6 | -10,0 | 0 | -11,5 | -16,8 | 0 |
| 7 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,767 | (11) | 1460,1 | -14,0 | 9,6 | 0 | -48,0 | -70,2 | 0 |
| 8 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,384 | (26) | 1460,1 | 2,7 | -1,9 | 0 | -55,0 | -80,4 | 0 |
| 9 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0 | (9) | 1460,0 | 15,8 | -10,8 | 0 | -36,0 | -52,5 | 0 |
| 10 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0 | (32) | 1460,1 | -2,1 | 1,5 | 0 | -0,2 | -0,2 | 0 |
| 11 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 3,913 | (72) | 1460,1 | 8,4 | -5,8 | 0 | 2,4 | 3,5 | 0 |
| 12 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,767 | (36) | 1460,1 | -10,2 | 7,0 | 0 | -47,2 | -68,9 | 0 |
| 13 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 1,152 | (41) | 1460,2 | -29,6 | 20,2 | 0 | -7,8 | -11,4 | 0 |
| 14 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,767 | (45) | 1460,2 | -27,3 | 18,7 | 0 | -36,0 | -52,5 | 0 |
| 15 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,764 | (51) | 1460,1 | 0 | 0 | 0 | -49,5 | -72,3 | 0 |
| 16 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,387 | (52) | 1460,1 | 5,0 | -3,4 | 0 | -47,5 | -69,3 | 0 |

Project

Analysis by

Model: **ZWO380 20210927 1-p rev1.axs**

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Staaftkrachten [Non-lin., Omhullende (UGT)]

| | Prof. | Doorsnede naam | C | min. max. | Geval | Pos. [m] | Knoop | Nx [kN] | Vy [kN] | Vz [kN] | Tx [kNm] | My [kNm] | Mz [kNm] | B [kNm ²] |
|----|-------|----------------|----|--------------|-------------------|----------|-------|---------------|--------------|--------------|----------|--------------|---------------|-----------------------|
| 17 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,384 | (56) | 1460,1 | 7,7 | -5,3 | 0 | -45,3 | -66,1 | 0 |
| 18 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0 | (34) | 1460,1 | 15,4 | -10,6 | 0 | -25,3 | -36,9 | 0 |
| 19 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 3,668 | (68) | 1460,1 | 10,8 | -7,4 | 0 | -2,5 | -3,7 | 0 |
| 20 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0 | (64) | 1460,1 | 12,9 | -8,9 | 0 | -3,1 | -4,5 | 0 |
| 1 | 2 | O 610x9 | Vy | min | Co #3 [1] (1,000) | 1,152 | (14) | -0,1 | -59,0 | -0,1 | 0 | 0 | -22,6 | 0 |
| 13 | 2 | O 610x9 | | min | Co #3 [1] (1,000) | 1,152 | (41) | -0,2 | -59,0 | -0,1 | 0 | 0 | -22,6 | 0 |
| 18 | 2 | O 610x9 | | max | Co #3 [1] (1,000) | 0,767 | (61) | -0,5 | 35,4 | 0,1 | 0 | 0,2 | -112,6 | 0 |
| 18 | 2 | O 610x9 | Vz | min | Co #1 [1] (1,000) | 0,767 | (61) | 1460,0 | 16,0 | -10,9 | 0 | -33,5 | -48,9 | 0 |
| 13 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0 | (44) | 1460,2 | -29,8 | 20,4 | 0 | -31,2 | -45,6 | 0 |
| 14 | 2 | O 610x9 | Tx | min | Co #3 [1] (1,000) | 0,767 | (45) | -0,2 | -55,9 | -0,1 | 0 | 0,2 | -104,9 | 0 |
| 20 | 2 | O 610x9 | | max | Co #3 [1] (1,000) | 1,187 | (73) | -0,5 | 33,1 | 0,1 | 0 | 0,1 | -46,3 | 0 |
| 4 | 2 | O 610x9 | My | min | Co #1 [1] (1,000) | 0,258 | (24) | 1460,1 | 0,2 | -0,1 | 0 | -55,3 | -80,8 | 0 |
| 3 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 0 | (4) | -1877,4 | 0,1 | -0,1 | 0 | 24,3 | 16,7 | 0 |
| 4 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 0,516 | (4) | -1877,4 | -0,1 | 0,2 | 0 | 24,3 | 16,7 | 0 |
| 4 | 2 | O 610x9 | Mz | min | Co #3 [1] (1,000) | 0,258 | (24) | -0,5 | 0,7 | 0 | 0 | 0,3 | -169,6 | 0 |
| 3 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 0 | (4) | -1877,4 | 0,1 | -0,1 | 0 | 24,3 | 16,7 | 0 |
| 4 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 0,516 | (4) | -1877,4 | -0,1 | 0,2 | 0 | 24,3 | 16,7 | 0 |

Prof.: Profiel; **C:** Extreme component; **min. max.:** Extreme type; **Geval:** Belastinggeval van de extreme; **Pos.:** Lokale X-positie van de doorsnede op de staaf; **Nx:** Normalkracht; **Vy:** Dwarskracht in lokale y-richting; **Vz:** Dwarskracht in lokale z-richting; **Tx:** Torsiemoment; **My:** Buigend moment in lokale y-richting; **Mz:** Buigend moment in lokale z-richting.

Project

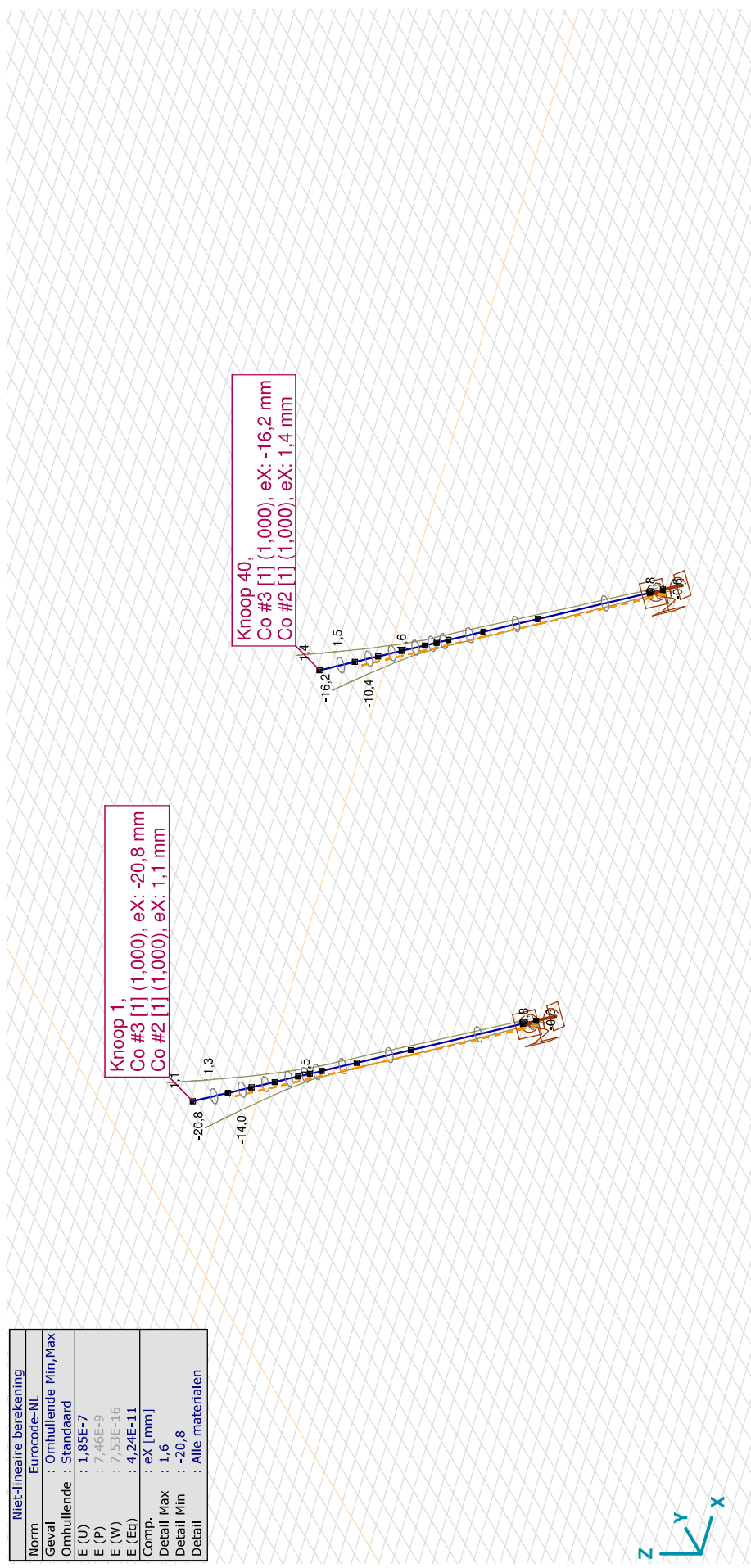
Analysis by

Model: ZWO380 20210927 1-p rev1.axs

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| | |
|--------------------------|-----------------------|
| Niet-lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : eX [mm] |
| Detail Max | : 1,6 |
| Detail Min | : -20,8 |
| Detail | : Alle materialen |



III, > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, eX, Lijnen

Project

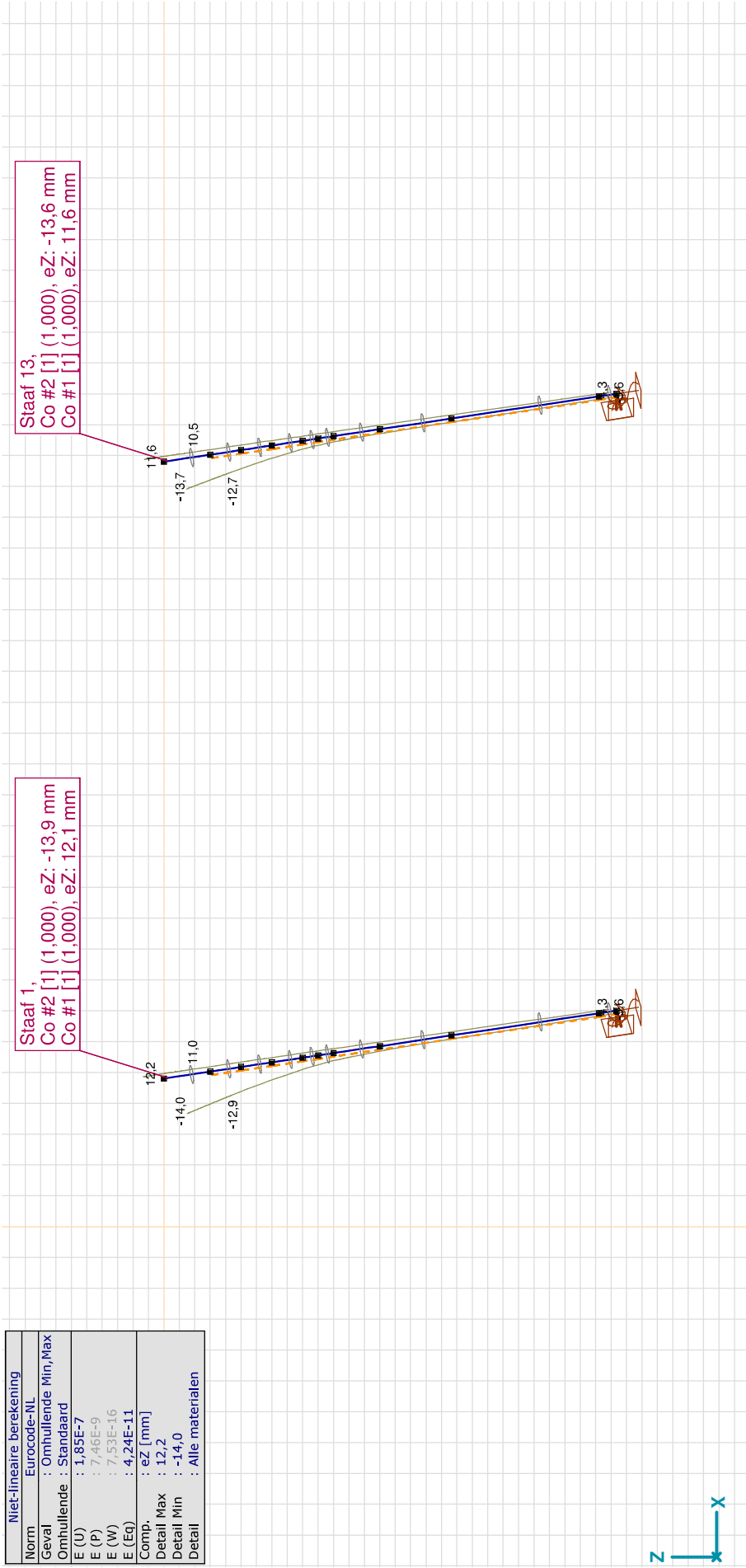
Analysis by

Model: ZWO380 20210927 1-p rev1.axs

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| Niet-lineaire berekening | |
|--------------------------|-----------------------|
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : eZ [mm] |
| Detail Max | : 12,2 |
| Detail Min | : -14,0 |
| Detail | : Alle materialen |



IIIJ. > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, eZ, Lijnen, Vooraanzicht

Project

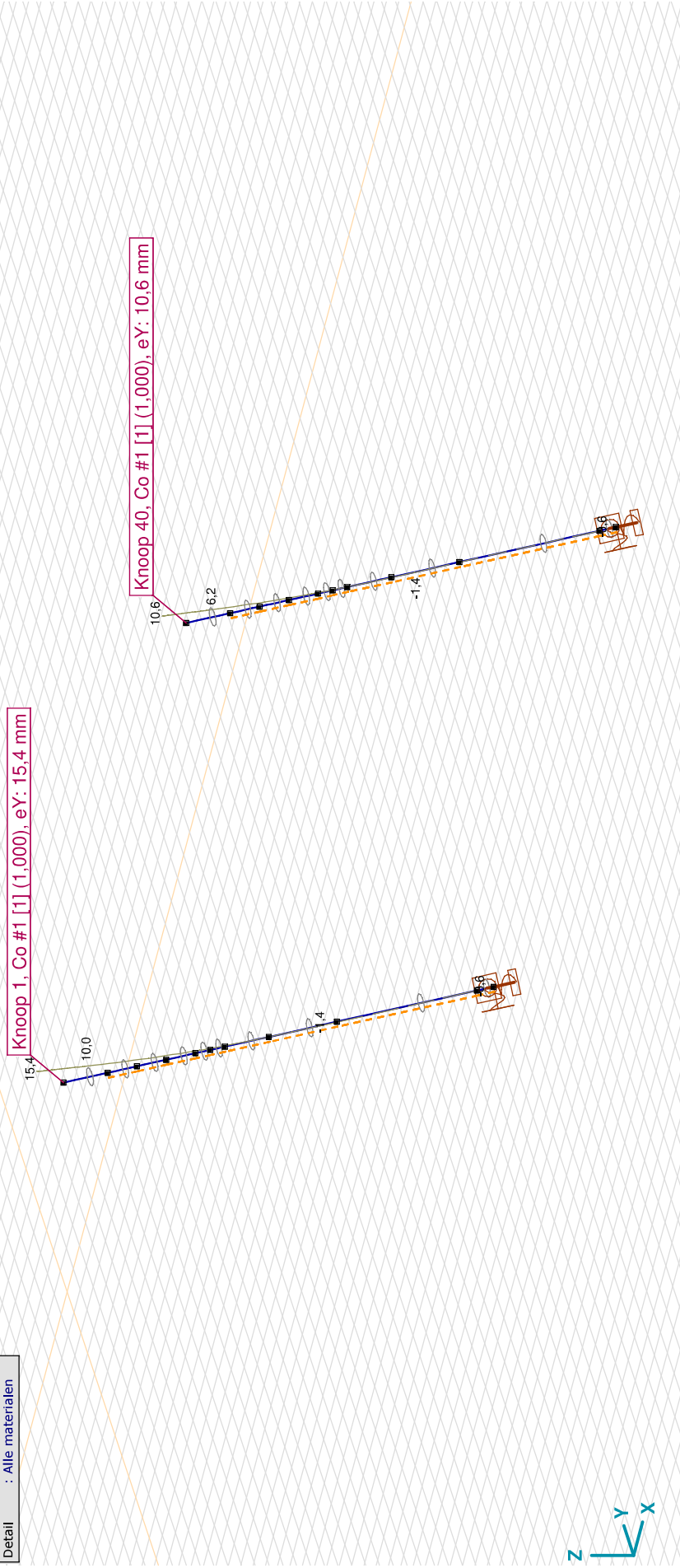
Analysis by

Model: ZWO380 20210927 1-p rev1.axs

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| Niet-lineaire berekening | |
|--------------------------|---------------------|
| Norm | Eurocode-NL |
| Geval | : Co #1 [1] (1,000) |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E+9 |
| E (W) | : 7,53E+16 |
| E (Eq) | : 4,24E+11 |
| Comp. | : eY [mm] |
| Detail Max | : 15,4 |
| Detail Min | : -1,4 |
| Detail | : Alle materialen |



[1], > S 355, Non-lin., Co #1 [1] (1,000), Onmiddellijke doorbuiging, eY, Lijnen

Project

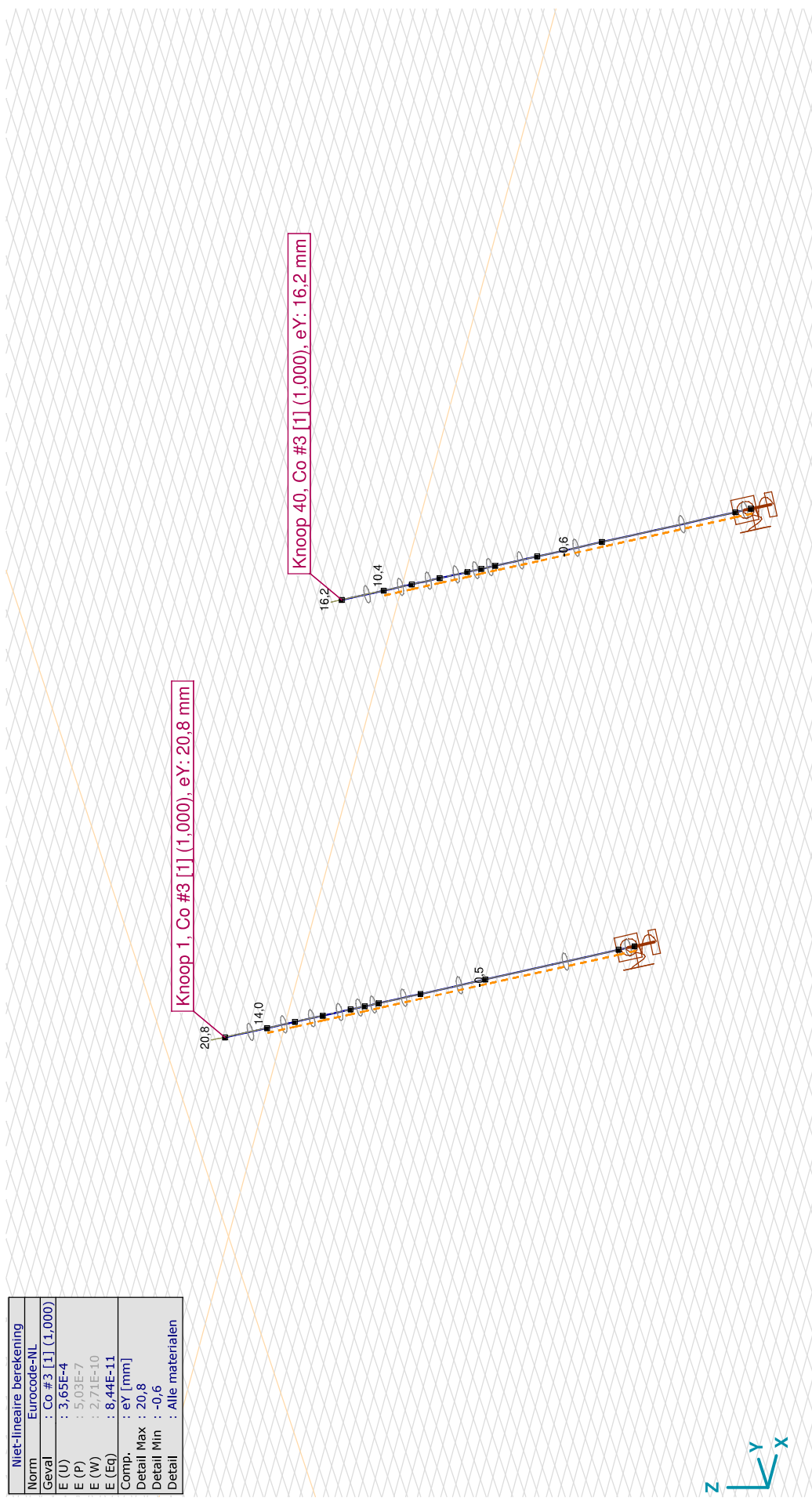
Analysis by

Model: ZWO380 20210927 1-p rev1.axs

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| Niet-lineaire berekening | |
|--------------------------|---------------------|
| Norm | Eurocode-NL |
| Geval | : Co #3 [1] (1,000) |
| E (U) | : 3,65E-4 |
| E (P) | : 5,03E-7 |
| E (W) | : 2,71E-10 |
| E (Eq) | : 8,44E-11 |
| Comp. | : eY [mm] |
| Detail Max | : 20,8 |
| Detail Min | : -0,6 |
| Detail | : Alle materialen |



[1], > S 355, Non-lin., Co #3 [1] (1,000), Onmiddellijke doorbuiging, eY, Lijnen

Project

Analysis by

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Knoopverplaatsingen [Non-lin., Omhullende (UGT), S 355]

| C | min. max. | Geval | eX [mm] | eY [mm] | eZ [mm] | eR [mm] | fX [rad] | fY [rad] | fZ [rad] | fR [rad] |
|------|--------------|-------------------|--------------|-------------|--------------|-------------|-------------|-------------|-------------|-------------|
| Ext. | | | | | | | | | | |
| 1 | eX | Co #3 [1] (1,000) | -20,8 | 20,8 | -0,1 | 29,4 | -0,0044 | -0,0044 | -0,0013 | 0,0064 |
| 39 | max | Co #2 [1] (1,000) | 1,6 | 0,9 | -11,4 | 11,6 | 0,0005 | -0,0001 | 0,0001 | 0,0005 |
| 49 | max | Co #2 [1] (1,000) | 1,6 | 1,2 | -11,0 | 11,2 | 0,0004 | -0,0001 | 0 | 0,0004 |
| 50 | max | Co #2 [1] (1,000) | 1,6 | 1,1 | -11,2 | 11,3 | 0,0004 | -0,0001 | 0 | 0,0004 |
| 51 | max | Co #2 [1] (1,000) | 1,6 | 1,0 | -11,3 | 11,5 | 0,0004 | -0,0001 | 0,0001 | 0,0005 |
| 1 | eY | Co #2 [1] (1,000) | 1,1 | -2,8 | -14,0 | 14,3 | 0,0011 | -0,0002 | 0,0001 | 0,0011 |
| 1 | max | Co #3 [1] (1,000) | -20,8 | 20,8 | -0,1 | 29,4 | -0,0044 | -0,0044 | -0,0013 | 0,0064 |
| 1 | eZ | Co #2 [1] (1,000) | 1,1 | -2,8 | -14,0 | 14,3 | 0,0011 | -0,0002 | 0,0001 | 0,0011 |
| 1 | max | Co #1 [1] (1,000) | -4,9 | 15,4 | 12,2 | 20,2 | -0,0036 | -0,0006 | -0,0006 | 0,0037 |
| 54 | eR | Co #3 [1] (1,000) | -1,4 | 1,4 | 0 | 2,0 | -0,0014 | -0,0014 | -0,0004 | 0,0021 |
| 1 | max | Co #3 [1] (1,000) | -20,8 | 20,8 | -0,1 | 29,4 | -0,0044 | -0,0044 | -0,0013 | 0,0064 |

C: Extreme component; **min.**: Extreme type; **Geval**: Belastinggeval van de extreme; **eX**: Verplaatsing in X-richting; **eY**: Verplaatsing in Y-richting; **eZ**: Verplaatsing in Z-richting; **eR**: Resulterende verplaatsing; **fX**: Rotatie in X-richting; **fY**: Rotatie in Y-richting; **fZ**: Rotatie in Z-richting; **fR**: Resulterende rotatie;

Project

Analysis by

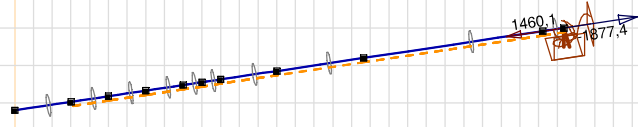
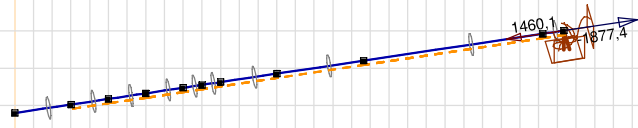
Model: ZWO380 20210927 1-p rev1.axs

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| Niet-lineaire berekening | |
|--------------------------|-----------------------|
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Rx [kN] |
| Detail Max | : 1460,1 |
| Detail Min | : -1877,4 |
| Detail | : Alle materialen |

| Rx [kN] |
|---------|
| 1460,1 |
| 1221,7 |
| 983,3 |
| 744,9 |
| 506,5 |
| 268,1 |
| 29,7 |
| -208,6 |
| -447,0 |
| -685,4 |
| -923,8 |
| -1162,2 |
| -1400,6 |
| -1639,0 |
| -1877,4 |



[I], > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Rx (knoopopl.), Lijnen, Vooraanzicht

Project

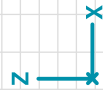
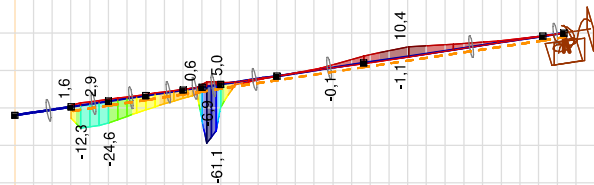
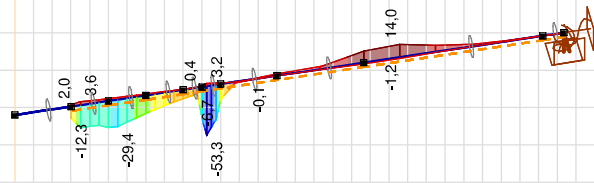
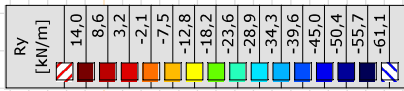
Analysis by

Model: ZWO380 20210927 1-p rev1.axs

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| | |
|--------------------------|-----------------------|
| Niet-lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Ry [kN/m] |
| Detail Max | : 14,0 |
| Detail Min | : -61,1 |
| Detail | : Alle materialen |



III, > S 355, Non-It., Omhullende (Standaard), Onmiddellijke doorbuiging, Ry (lijnopp.), Lijnen (gevuld), Vooraanzicht

Project

Analysis by

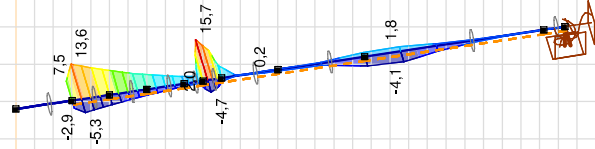
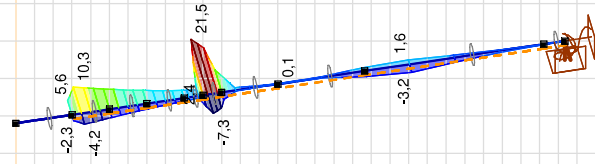
Model: ZWO380 20210927 1-p rev1.axs

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| | |
|--------------------------|-----------------------|
| Niet-lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Rz [kN/m] |
| Detail Max | : 21,5 |
| Detail Min | : -7,3 |
| Detail | : Alle materialen |

| | |
|------|--------|
| Rz | [kN/m] |
| 21,5 | |
| 19,5 | |
| 17,4 | |
| 15,3 | |
| 13,3 | |
| 11,2 | |
| 9,2 | |
| 7,1 | |
| 5,0 | |
| 3,0 | |
| 0,9 | |
| -1,1 | |
| -3,2 | |
| -5,3 | |
| -7,3 | |



III, > S 355, Non-It., Omhullende (Standaard), Onmiddellijke doorbuiging, Rz (lijnopp.), Lijnen (gevuld), Vooraanzicht

Project

Analysis by

Model: **ZWO380 20210927 1-p rev1.axs**

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Interne krachten knooppoplegging [Non-lin., Omhullende (Standaard), S 355]

| Ext. | Knoop | X [m] | Y [m] | Z [m] | Type | C | min. max. | Geval | Rx [kN] | Ry [kN] | Rz [kN] | Rr [kN] | Rxx [kNm] | Ryy [kNm] | Rzz [kNm] | Rrr [kNm] | αR |
|------|-------|-------|--------|-------|---------|-----------|--------------|-------------------|----------------|------------|------------|------------|--------------|--------------|--------------|--------------|------------|
| | 1 | 32 | 27,001 | 7,001 | -14,673 | Staaft r. | Rx | min | -1877,4 | 0,5 | -0,7 | 1877,4 | 0 | 0,2 | 0,1 | 0,3 | -2570,203 |
| | 2 | 2 | 7,001 | 7,001 | -14,673 | Staaft r. | | min | -1877,4 | 0,1 | -0,2 | 1877,4 | 0 | -1,6 | -1,1 | 1,9 | -9818,083 |
| | 1 | 32 | 27,001 | 7,001 | -14,673 | Staaft r. | max | Co #1 [1] (1,000) | 1460,1 | -2,1 | 1,5 | 1460,1 | 0 | -0,2 | -0,2 | 0,3 | 996,293 |
| | 2 | 2 | 7,001 | 7,001 | -14,673 | Staaft r. | max | Co #1 [1] (1,000) | 1460,1 | 0,5 | -0,3 | 1460,1 | 0 | 4,0 | 5,8 | 7,0 | -4712,829 |

Knoop: Ondersteunde knoop; **Type:** Opleggingsstype; **C:** Extreme component; **min. max.:** Belastinggeval van de extreme; **Rx:** X-component opleggingsreactiekracht; **Ry:** Y-component opleggingsreactiekracht; **Rz:** Z-component opleggingsreactiekracht;
Rr: Resulterende opleggingsreactiekracht; **Rxx:** X-component opleggingsreactiemoment; **Ryy:** Y-component opleggingsreactiemoment; **Rzz:** Z-component opleggingsreactiemoment; **Rrr:** Resulterende opleggingsreactiemoment;
 αR : Verhouding verticale oplegkracht / horizontale oplegkracht

Project

Analysis by

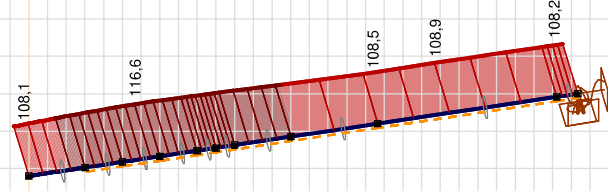
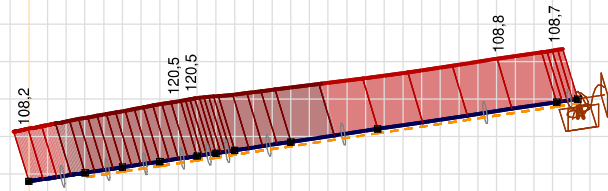
Model: ZWO380 20210927 1-p rev1.axs

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| | |
|--------------------------|---------------------------------|
| Niet-lineaire berekening | |
| Norm | Eurocode-NL |
| Geval | : Omhullende Min, Max |
| Omhullende | : Standaard |
| E (U) | : 1,85E-7 |
| E (P) | : 7,46E-9 |
| E (W) | : 7,53E-16 |
| E (Eq) | : 4,24E-11 |
| Comp. | : Sominmax [N/mm ²] |
| Detail Max | : 120,5 |
| Detail Min | : 0 |
| Detail | : Alle materialen |

| | |
|-------------------------------|--|
| Sominmax [N/mm ²] | |
| 120,5 | |
| 111,9 | |
| 103,3 | |
| 94,7 | |
| 86,1 | |
| 77,5 | |
| 68,9 | |
| 60,3 | |
| 51,7 | |
| 43,0 | |
| 34,4 | |
| 25,8 | |
| 17,2 | |
| 8,6 | |
| 0 | |



[II] > S 355, Non-lin., Omhullende (Standaard), Onmiddellijke doorbuiging, Sominmax, Lijnen (gevuld), Voorraanzicht

Project

Analysis by

Model: **ZWO380 20210927 1-p rev1.axs**

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Staafspanningen [Non-lin., Omhullende (Standaard), S 355]

| Ext. | Prof. | Doorsnede naam | C | min. max. | Geval | Pos. [m] | Knoop | S _x :min [N/mm ²] | S _x :max [N/mm ²] | V _{min} [N/mm ²] | V _{max} [N/mm ²] | S _o :min [N/mm ²] | S _o :max [N/mm ²] | V _y :gem [N/mm ²] | V _z :gem [N/mm ²] |
|------|-------|----------------|---------------------|-----------|-------------------|----------|-------|--|--|---------------------------------------|---------------------------------------|--|--|--|--|
| 3 | 2 | O 610x9 | S _x :min | min | Co #2 [1] (1,000) | 0 | (4) | -117,6 | -98,7 | 0 | 0 | 98,7 | 117,6 | 0 | 0 |
| 4 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0,516 | (4) | -117,6 | -98,7 | 0 | 0 | 98,7 | 117,6 | 0 | 0 |
| 8 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0,512 | (7) | -117,5 | -98,8 | 0 | 0,1 | 98,8 | 117,5 | 0 | 0,1 |
| 1 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 1,535 | (1) | 84,1 | 84,1 | 0 | 3,3 | 84,1 | 84,3 | -1,7 | 1,1 |
| 10 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 0,144 | (77) | 84,1 | 84,1 | 0 | 0,2 | 84,1 | 84,1 | -0,1 | 0,1 |
| 13 | 2 | O 610x9 | | max | Co #1 [1] (1,000) | 1,535 | (40) | 84,1 | 84,1 | 0 | 3,4 | 84,1 | 84,3 | -1,7 | 1,2 |
| 1 | 2 | O 610x9 | S _x :max | min | Co #2 [1] (1,000) | 1,535 | (1) | -108,1 | -108,1 | 0 | 1,0 | 108,1 | 108,2 | 0,4 | -0,5 |
| 10 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0,287 | (78) | -108,1 | -108,1 | 0 | 0,1 | 108,1 | 108,1 | 0 | 0 |
| 11 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 0 | (33) | -108,2 | -108,1 | 0 | 0,1 | 108,1 | 108,2 | 0 | 0 |
| 13 | 2 | O 610x9 | | min | Co #2 [1] (1,000) | 1,535 | (40) | -108,1 | -108,1 | 0 | 1,0 | 108,1 | 108,1 | 0,3 | -0,5 |
| 3 | 2 | O 610x9 | | max | Co #4 [1] (1,000) | 0 | (4) | 44,6 | 120,5 | 0 | 0,2 | 44,6 | 120,5 | -0,1 | 0 |
| 4 | 2 | O 610x9 | | max | Co #4 [1] (1,000) | 0,258 | (24) | 44,5 | 120,5 | 0 | 0 | 44,5 | 120,5 | 0 | 0 |
| 8 | 2 | O 610x9 | | max | Co #4 [1] (1,000) | 0,512 | (7) | 44,6 | 120,5 | 0 | 0,4 | 44,6 | 120,5 | 0,2 | 0 |
| 10 | 2 | O 610x9 | S _o :min | min | Co #3 [1] (1,000) | 0,144 | (77) | -0,1 | 0 | 0 | 0,6 | 0 | 1,0 | -0,3 | 0 |
| 1 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 1,535 | (1) | -108,1 | -108,1 | 0 | 1,0 | 108,1 | 108,2 | 0,4 | -0,5 |
| 10 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 0,287 | (78) | -108,1 | -108,1 | 0 | 0,1 | 108,1 | 108,1 | 0 | 0 |
| 11 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 0 | (33) | -108,2 | -108,1 | 0 | 0,1 | 108,1 | 108,2 | 0 | 0 |
| 13 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 1,535 | (40) | -108,1 | -108,1 | 0 | 1,0 | 108,1 | 108,1 | 0,3 | -0,5 |
| 19 | 2 | O 610x9 | | max | Co #2 [1] (1,000) | 3,668 | (68) | -108,2 | -108,0 | 0 | 0,4 | 108,0 | 108,2 | -0,1 | 0,2 |
| 11 | 2 | O 610x9 | S _o :max | min | Co #3 [1] (1,000) | 0 | (33) | -0,9 | 0,9 | 0 | 0,6 | 0 | 1,0 | -0,3 | 0 |
| 3 | 2 | O 610x9 | | max | Co #4 [1] (1,000) | 0 | (4) | 44,6 | 120,5 | 0 | 0,2 | 44,6 | 120,5 | -0,1 | 0 |
| 4 | 2 | O 610x9 | | max | Co #4 [1] (1,000) | 0,258 | (24) | 44,5 | 120,5 | 0 | 0 | 44,5 | 120,5 | 0 | 0 |
| 8 | 2 | O 610x9 | | max | Co #4 [1] (1,000) | 0,512 | (7) | 44,6 | 120,5 | 0 | 0,4 | 44,6 | 120,5 | 0,2 | 0 |

Prof.: Profiel; **C:** Extreem type; **min. max.:** Extreem type; **Geval:** Belastinggeval van de extreme; **Pos.:** Lokale X-positie van de doorsnede op de staaf; **S_x:min:** Doorsnede minimum normaalspanning; **S_x:max:** Doorsnede maximum normaalspanning;

V_{min}: Doorsnede minimum afschuifspanning; **V_{max}:** Doorsnede maximum afschuifspanning; **S_o:min:** Doorsnede minimum Von Mises spanning; **S_o:max:** Doorsnede maximum Von Mises spanning; **V_y:gem:** Afschuifspanning in lokale Y-richting;

V_z:gem: Afschuifspanning in lokale Z-richting;



About DNV

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Whether assessing a new ship design, optimizing the performance of a wind farm, analyzing sensor data from a gas pipeline or certifying a food company's supply chain, DNV enables its customers and their stakeholders to make critical decisions with confidence.

Driven by its purpose, to safeguard life, property, and the environment, DNV helps tackle the challenges and global transformations facing its customers and the world today and is a trusted voice for many of the world's most successful and forward-thinking companies.