

*380 kV reconstructiemasten*

B.9 Mastrapportage hoekmasten reconstructie

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ZUID-WEST 380 KV OOST VERBINDINGEN

# Mastrapportage GT-RLL HA+0/n en HA+5/n

TenneT TSO B.V.

Meridian doc.nr.: 002.678.00.0934571

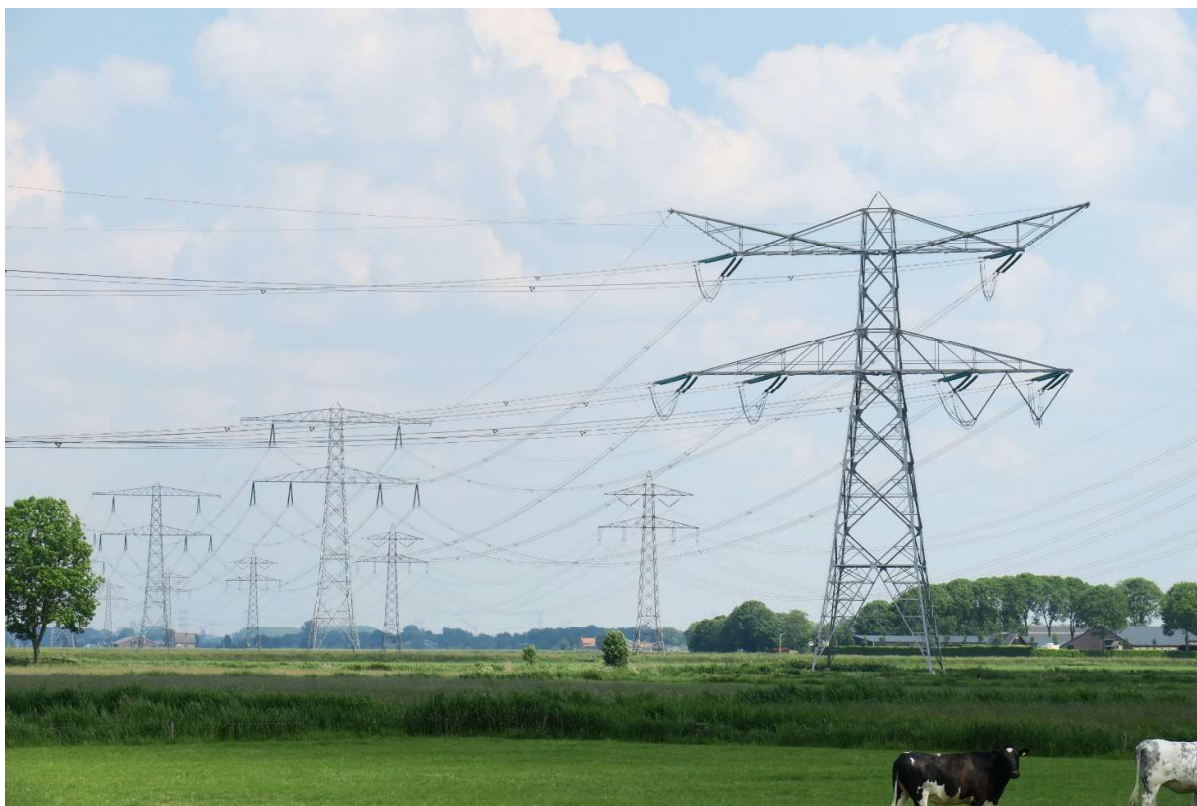
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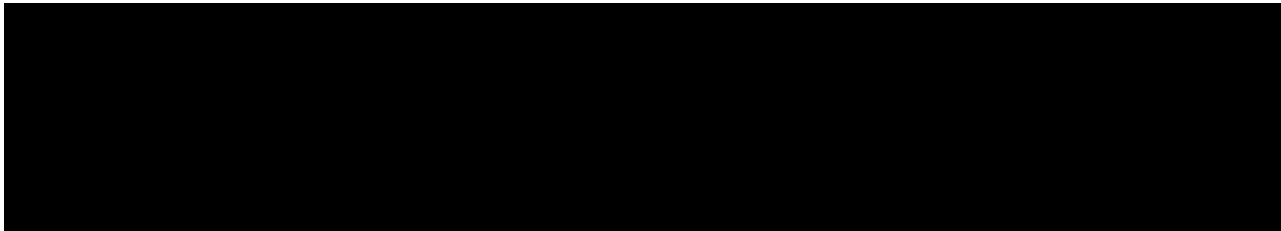




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## 1 INLEIDING

In het basisontwerp van de vakwerkmasten voor de verbinding RLL-TLB380 in het project Zuid-West 380 kV-Oost zijn voor het vaststellen van de haalbaarheid constructieve berekeningen uitgevoerd aan de masten en fundaties. In de Definitief Ontwerpfase, moeten berekeningen verder worden uitgewerkt om te kunnen dienen voor de benodigde vergunningsdocumentatie, voor de aanbesteding en als voorbereiding voor de uitvoeringsfase. Het DO omvat het ontwerp van de mastconstructies, de fundaties en de opstijpunten in de verbinding.

Deze rapportage bevat de resultaten van de toetsing van masttype HA+0/n en HA+5/n t.b.v de reconstructie. Deze mast is gebaseerd op de bestaande HA+0/n en HA+5/n masten uit de verbinding GT-RLL380 met de aanpassingen om te voldoen aan de belasting uit de nieuwe situatie.

In deze rapportage is de toetsing van de mast van de steunmast HA+5/n opgenomen. De toetsing bestaat uit controle van:

- de profielen en boutverbindingen onderdeel van de hoofddraagconstructie
- de knikverkorters
- de liggers voor de isolatorkettingen
- de verbinding met de fundatie via blokdeuvels
- de toetsing op galloping

Buiten de scope van dit DO-rapport valt de controle van de schetsplaten en overige verbindingdetails in de constructie. Dit moet in de UO-fase worden uitgewerkt. Ook de voorzieningen voor de high-step rail en bordessen vallen onder uitwerking in UO-fase.

In hoofdstuk 2 zijn de uitgangspunten en randvoorwaarden vanuit de van toepassing zijnde normen en TenneT-specificaties opgenomen. Hoofdstuk 3 beschrijft de gevolgde aanpak van de berekening. In hoofdstuk 4 is de toetsing opgenomen.

## 2 UITGANGSPUNTEN EN RANDVOORWAARDEN

### 2.1 Normen

Er is gebruik gemaakt van de normen volgens Tabel 1.

**Tabel 1 Gebruikgemaakte normen, voorschriften en richtlijnen**

| Norm                                       | Titel  |
|--|--|
| NEN-EN 50341-1:2013                        | “Overhead electrical lines exceeding AC 1 kV - Part 1: General requirements – Common”                        |
| NEN-EN 50341-2-15:2019                     | “Overhead electrical lines exceeding AC 1 kV Part 2 National Normative Aspects (NNA) for THE NETHERLANDS”    |
| NEN-EN 1990+A1+A1/C2:2019/NB:2019nl        | “Grondslagen van het ontwerp”  |
| NEN-EN 1991-1-4+A1+C2:2011/NB:2019+C1:2020 | “Deel 1-4: Windbelasting op constructies”  |
| NEN-EN 1992-1-1+C2:2011/NB:2016+A1:2020    | “Eurocode 2: Ontwerp en berekening van betonconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-1-1+C2+A1:2016 nl              | “Eurocode 3: Ontwerp en berekening van staalconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-3-1:2007/NB:2011 nl            | “Deel 3-1: Torens, masten en schoorstenen - Torens en masten”  |
| NEN-EN 1993-1-8+C2:2011/NB:2011 nl         | “Ontwerp en berekening van staalconstructies, deel 1-8: ontwerp en berekening van verbindingen”              |

### 2.2 TenneT-specificaties

In Tabel 2 zijn de documenten opgenomen die relevant zijn voor de berekeningen en toetsingen die binnen dit project in de mastrapportage uitgevoerd zullen worden.

**Tabel 2 Relevante documenten t.b.v. mechanische rapportages**

| Nummer          | Onderwerp                           |
|-----------------|-------------------------------------|
| PVE.05.000 v3.2 | PvE Lijnen                          |
| sPVE.05.001     | sPvE Lijnen                         |
| SPE.05.346 v1.3 | Algemene specificatie stalen masten |

### 2.3 Eisenverificatie

Voor de eisenverificatie wordt verwezen naar het rapport “Verificatierapport eisen reconstructies”.

### 2.4 Ontwerprapporten

Voor de achtergrond van het ontwerp wordt verwezen naar het uitgangspuntenrapport “D1.3 Uitgangspunten reconstructies”, DNV GL rapport 21-0702, Meridiannummer 002.678.00 0927721.

### 2.5 Materialen

Voor het ontwerp van de mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 3.

**Tabel 3 Materialen aangepaste constructie**

|                |   |
|----------------|---|
| Staalsoort     | S355J0 (t≤16 mm)<br>S355J2 (16<t≤40 mm) |
| Boutkwaliteit  | 8.8 gerolde draad                       |
| Betonkwaliteit | C30/37                                  |
| Wapeningsstaal | B500                                    |



Voor de constructie geldt conform TenneT-specificatie:

- Toe te passen bouten: M16/M20/M24;
- Voor hoekstaal is de minimale afmeting L50x5 mm;
- Minimale plaatdikte 6 mm.

Mocht het noodzakelijk zijn M30 toe te passen, bij grote plaatdiktes is dit als afwijking door TenneT toegestaan.

## 2.6 Software

De gebruikte software wordt benoemd in Tabel 4.

**Tabel 4 Toegepaste software**

| Software              |           | Versie |
|-----------------------|-----------|--------|
| Mastontwerp           | PLS-CADD  | 16.65  |
| Mastberekeningen      | PLS-TOWER | 16.65  |
| Constructieve analyse | AxisVM    | X5 R4h |

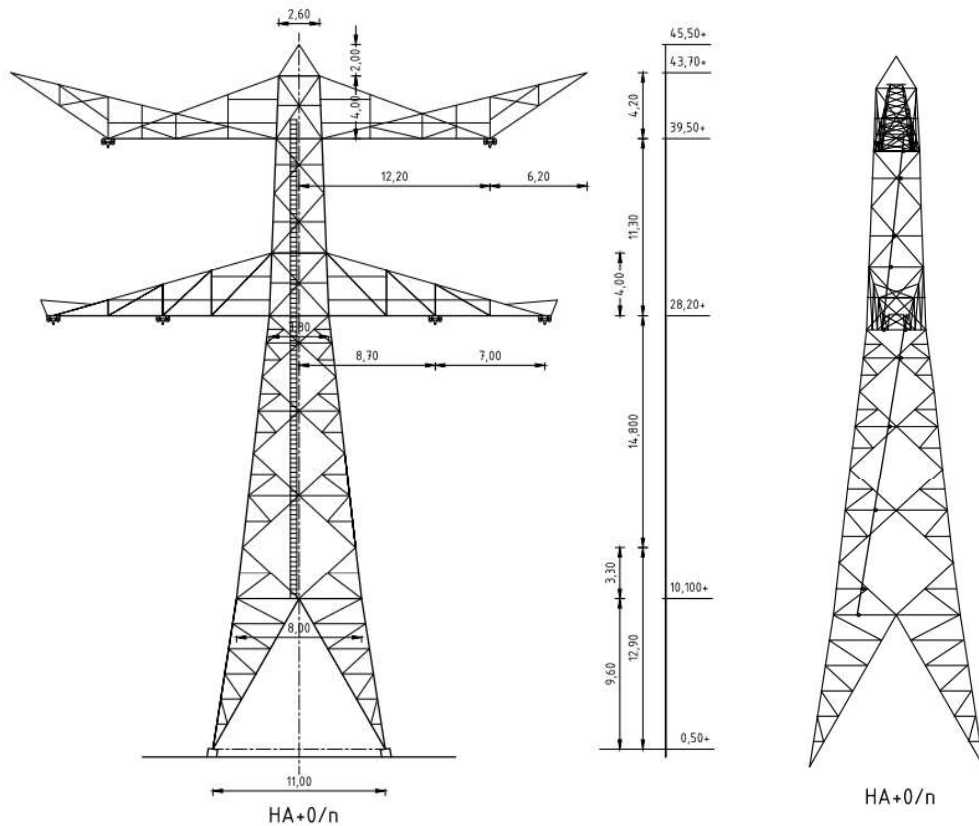
### 3 MASTONTWERP

#### 3.1 Mastbeelden

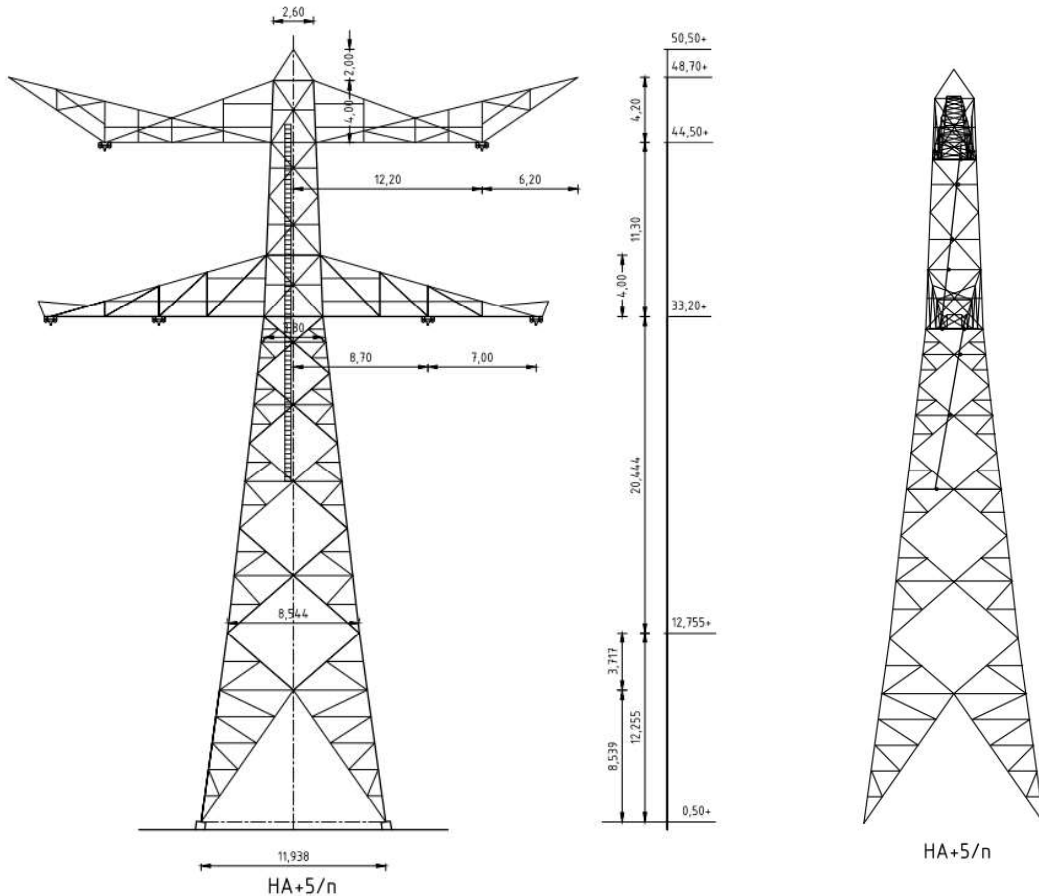
In dit hoofdstuk worden de mastbeelden weergegeven met de belangrijkste maatvoering, de figuren zijn ontleend aan de bij deze rapportage horende tekeningen van de masttypen. Het gaat om de volgende tekeningen:

- Overzichtstekening HA+0/n, Meridiannummer 002.678.00 0934585
- Overzichtstekening HA+5/n, Meridiannummer 002.678.00 0934586.

Masttype reconstructie HA+0/n en HA+5/n is een hoekmast voor twee circuits 380 kV.



Figuur 1 Mastbeeld masttype HA+0/n



**Figuur 2 Mastbeeld masttype HA+5/n**

### 3.2 Verschillen HA+0\_n en HA+5\_n

Masttype HA+0\_n en HA+5\_n delen dezelfde mastkop. Dat wil zeggen het mastgedeelte boven het niveau van de ondertraverse; de traveses en het bovenstuk van het mastlichaam.

Het onderstuk met de drie diagonaalkruisen tussen ondertraverse en broekstuk is ogenschijnlijk gelijk uitgevoerd, echter de geometrie (hellingsverandering) verschilt tussen beide masttypes. In dit mastgedeelte bevindt zich een horizontaalverband dat in beide types op een verschillende positie zit. Bij masttype HA+5 begint de ladder bij dat verband.

Het broekstuk van masttype HA+5 is afwijkend van vorm dan dat van HA+0, het loopt vanaf de fundatie tot het knooppunt met de hoofddiagonaal (12,755+ in bovenstaande figuur) terwijl het zich bij HA+0 tot het niveau van 10,100+ bevindt. De hellingsverandering bij masttype HA+5 is bij de overgang broekstuk -tussenstuk erg klein. In de UO-fase moet hier aandacht aan worden besteed dat dit niet gemist wordt.



### 3.3 Uitgangspunten berekening

De uitgangspunten volgens Tabel 5 zijn van toepassing.

**Tabel 5 Uitgangspunten**

|                           |                       |
|---------------------------|-----------------------|
| Norm                      | NEN-EN50341-2-15:2019 |
| Gevolgklasse initieel     | CC2                   |
| Betrouwbaarheidsniveau    | Nieuwbouw             |
| Referentieperiode         | 50 jaar               |
| Windgebied                | III                   |
| Windsnelheid (m/s)        | 24,5                  |
| Terreincategorie          | II                    |
| Reductiefactor $c_{dir}$  | 1,00                  |
| IJsgebied fasegeleider    | B                     |
| IJsgebied bliksemgeleider | A                     |

### 3.4 Mastenlijst

In Tabel 6 tot en met Tabel 7 zijn alle masten in het tracé van het type HA+0/n en HA+5/n opgenomen. De mast met grootste wind span is vetgedrukt aangegeven. Het masttype zal niet met deze wind en weight span worden berekend maar met generieke wind en weight span, zie uitgangspuntenrapport.

**Tabel 6 Mastenlijst HA+0/n**

| Mast-nummer | Masttype | Lijnhoek (°) | Wind span (m) | Weight span (m) | Hoogteverschil ba+ah (m) | Hoogteverschil back (m) | Hoogteverschil ahead (m) |
|-------------|----------|--------------|---------------|-----------------|--------------------------|-------------------------|--------------------------|
| 76N         | HA+0/n   | 172,4        | 355,5         | 336,1           | -4,9                     | -4,5                    | -0,4                     |
| 73N         | HA+0/n   | 180,0        | 368,5         | 253,3           | -32,8                    | -0,3                    | -32,5                    |
| <b>25N</b>  | HA+0/n   | 170,2        | 335,0         | 313,8           | -5,2                     | -5,4                    | 0,2                      |
| 24N         | HA+0/n   | 180,0        | 335,6         | 333,1           | -0,6                     | -0,2                    | -0,4                     |
| 16AN        | HA+0/n   | 180,0        | 233,3         | 214,2           | -3,1                     | -1,6                    | -1,6                     |

**Tabel 7 Mastenlijst HA+5**

| Mast-nummer | Masttype | Lijnhoek (°) | Wind span (m) | Weight span (m) | Hoogteverschil ba+ah (m) | Hoogteverschil back (m) | Hoogteverschil ahead (m) |
|-------------|----------|--------------|---------------|-----------------|--------------------------|-------------------------|--------------------------|
| 70N         | HA+5/n   | 180,0        | 297,1         | 165,3           | -28,1                    | -27,5                   | -0,6                     |
| <b>18N</b>  | HA+5/n   | 164,5        | 363,2         | 396,7           | 8,7                      | 4,5                     | 4,2                      |

### 3.5 Geleiderbelastingen

De berekening is uitgevoerd met het geleiderbelastingprogramma van DNV GL. De belastingen op de mastconstructie zijn bepaald op basis van de modellering in PLS-TOWER (staafoppervlaktes). Voor de toeslagen op eigen gewicht en windoppervlakte wordt verwezen naar het uitgangspuntenrapport. In Appendix A zijn de resultaten van de geleiderbelastingen samengevat.

### 3.6 Reacties op de fundering

De oplegreacties op de fundering worden ontleend aan de uitvoer van het geleiderbelastingenprogramma. Zie Appendix A.

### 3.7 Modelling

Op basis van de ontwerptekeningen is de mast in PLS-TOWER ingevoerd. De toetsing wordt per staafgroep uitgevoerd. De hoofdelementen zijn gemodelleerd, niet-dragende profielen als knikverkorters zijn weggelaten, deze worden separaat getoetst. De profielen zijn in PLS-TOWER inclusief de boutverbindingen ingevoerd en getoetst, de controle van de schetsplaten en andere detailverbindingen valt buiten de scope.

De geleiderbelastingen vanuit het geleiderbelastingenprogramma zijn als invoer voor de belastingen gebruikt.

De gewichts- en windbelasting op de mastconstructie wordt door PLS-TOWER automatisch bepaald. Via toeslagfactoren wordt de invloed van niet gemodelleerde elementen als knikverkorters, bordesconstructies en klimvoorzieningen meegenomen. Voor schetsplaten, zinklaag en bouten is een aanvullende toeslag op het gewicht van 20% toeslag gerekend.

Diagonalen in voor- en achtervlak respectievelijk de twee zijvlakken zijn samengenomen in een groep.

### 3.8 Overige controles

In PLS-TOWER zijn niet alle elementen getoetst. Knikverkortersprofielen en overige profielen voor beloopbaarheid worden separaat getoetst. In Appendix C is dit opgenomen. De verbinding met de fundatie bestaat uit ingestorte profielen voorzien van blokdeuvels. Dit is in Appendix D opgenomen. De liggers van isolatorkettingen zijn gebaseerd op Moldaumasten en hebben geen aanvullende controle op buiging nodig vanwege aanmerkelijk lagere belastingen. Appendix E is derhalve niet ingevuld bij dit masttype maar vanwege consistentie met andere rapporten hier opgenomen. Appendix F omvat de toetsing op galloping.

### 3.9 Mastgewicht

Het totale mastgewicht per masttype is met de uitgangspunten van paragraaf 3.6 bepaald op:

Het gewicht van masttype HA+0/n is bepaald op 46,3 ton.

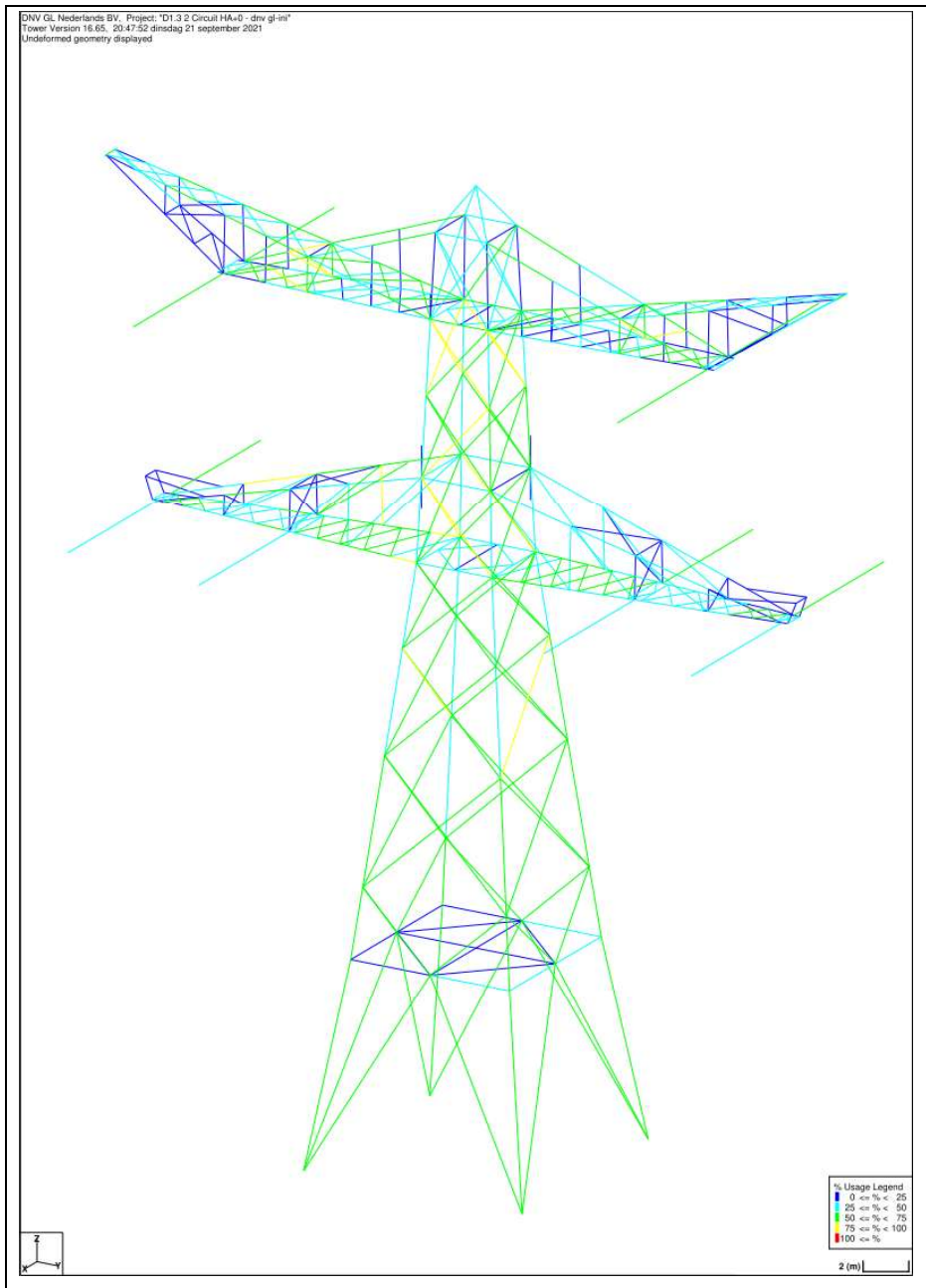
Het gewicht van masttype HA+5/n is bepaald op 50,3 ton.

## 4 TOETSING

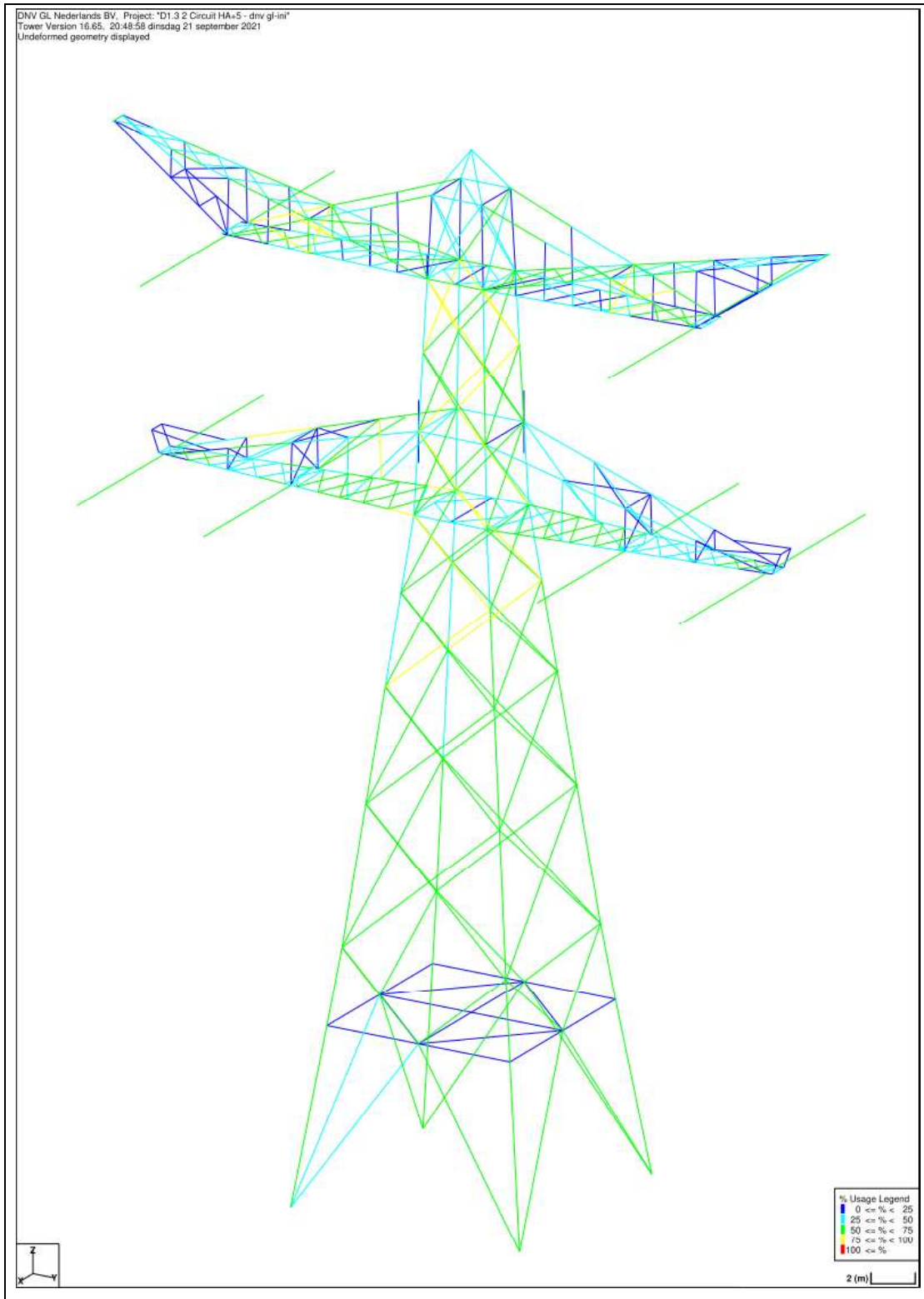
### 4.1 Resultaat PLS-TOWER

Het resultaat van de toetsing met PLS-TOWER is per masttype weergegeven in Figuur 3 en Figuur 4. Voor elk masttype zijn de belastingen apart bepaald. Alléén voor masttype HA+5/n, bepalend voor het ontwerp van de mastkop, zijn deze ook inclusief afspannen.

De uitnutting van de constructie loopt op van blauw (0-25%) tot geel (75-100%). Uit de figuur wordt geconcludeerd dat alle profielen en boutverbindingen voldoen.



**Figuur 3 Resultaat PLS-TOWER voor de steunmast HA+0/n**



**Figuur 4 Resultaat PLS-TOWER voor de steunmast HA+5/n**

## 4.2 Toetsing overige onderdelen

In Tabel 8 zijn de resultaten van de uitgevoerde toetsingen weergegeven.

**Tabel 8 Samenvatting uitgevoerde controles**

| Controle van          | Beoordeling | Referentie                         |
|-----------------------|-------------|------------------------------------|
| Profielen             | Voldoen     | Figuur 4<br>Figuur 3<br>Appendix B |
| Knikverkorters        | Voldoen     | Appendix C                         |
| Blokdeuvels randstijl | Voldoen     | Appendix D                         |
| Galloping             | Voldoet     | Appendix F                         |



## APPENDIX A

### Geleiderbelastingen

---

Geleiderbelastingen opgenomen:

- Masttype HA+0/n
- Masttype HA+5/n



Project: GT-RLL380  
 Tower: HA+0\_n  
 Number: 25N

Auteur: TBR  
 Versie: v12.0

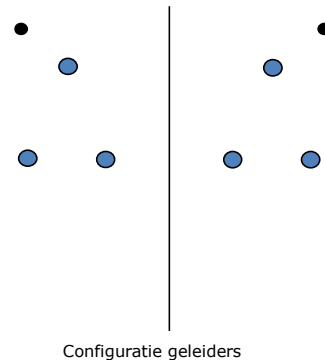
### Geleiderbelastingen

#### Algemeen

Benaming HA+0\_n  
 Masttype Hoekmast  
 Aantal circuits 2  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 2

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 50 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 50 jaar  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsg gebied fasegeleider B  
 IJsg gebied bliksemgeleider A



#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A           | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A           | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging     | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Circuit 2      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Bliksemdraad 1 | Afspanketting | 0,10         | 0,20       | 0,10                       |
| Bliksemdraad 2 | Afspanketting | 0,10         | 0,20       | 0,10                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 27,7 m       | 27,7 m       | -15,7 m                                |
| Circuit 1      | 11         | 380ct1f2 | 27,7 m       | 27,7 m       | -8,7 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 39,0 m       | 39,0 m       | -12,2 m                                |
| Circuit 2      | 20         | 380ct2f1 | 27,7 m       | 27,7 m       | 8,7 m                                  |
| Circuit 2      | 21         | 380ct2f2 | 27,7 m       | 27,7 m       | 15,7 m                                 |
| Circuit 2      | 22         | 380ct2f3 | 39,0 m       | 39,0 m       | 12,2 m                                 |
| Bliksemdraad 1 | 1          | bl1      | 43,2 m       | 43,2 m       | -18,4 m                                |
| Bliksemdraad 2 | 3          | bl2      | 43,2 m       | 43,2 m       | 18,4 m                                 |



Project: GT-RLL380  
 Tower: HA+0\_n  
 Number: 25N

**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead  |   |
|------------------------------------|---------------------------|--------|---|
| Verhoging voor windbelasting       | 32,0 m                    | 0,0 m  | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -5,0 m                    | -5,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |        |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

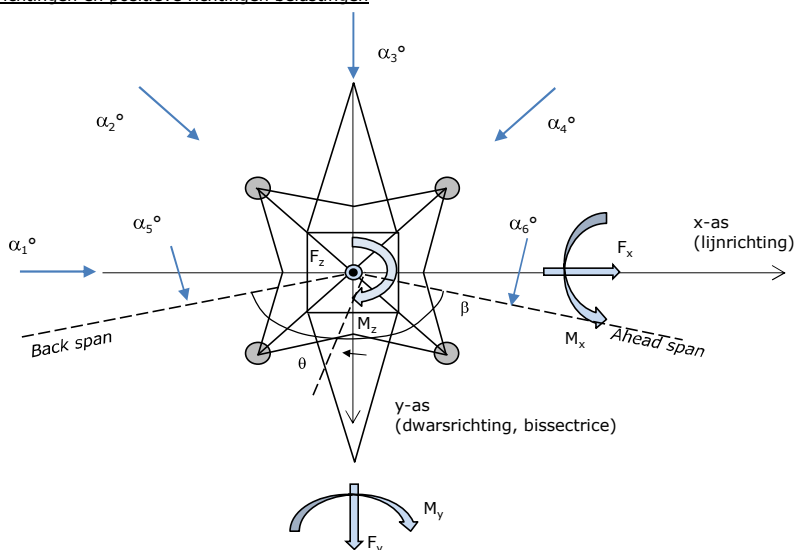
| Circuits       | Aanduiding | Nummer   | Hoogteverschil  |                  | Richtingsverandering |                  |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
|                |            |          | $\Delta h$ back | $\Delta h$ ahead | $\Delta y$ back      | $\Delta y$ ahead |
| Circuit 1      | 10         | 380ct1f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 11         | 380ct1f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 12         | 380ct1f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 20         | 380ct2f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 21         | 380ct2f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 22         | 380ct2f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 1 | 1          | bl1      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 2 | 3          | bl2      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek                                   | $\beta$    | 160 °   |
| Rotatie mast t.o.v. bissectrice            | $\theta$   | 0 °     |
| Vaklengte                                  | 400        | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 45 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 135 °   |
|  | $\alpha_5$ | 80 °    |
|  | $\alpha_6$ | 100 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



Beschouwd aantal windrichtingen

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

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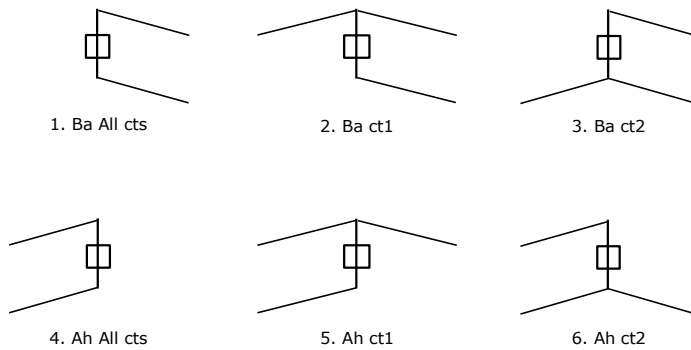
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | b2       | 0             | 1    | 1                        | 0    | 1                  | 0    |

### Belastingsituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

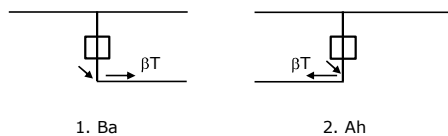
Principe belastingssituaties:



### Belastingsituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



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### Belastingsituaties 6. Bouw- en onderhoud

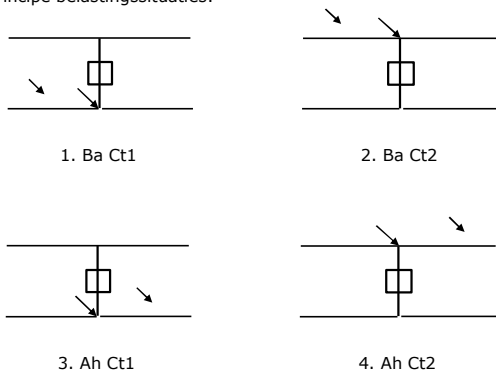
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



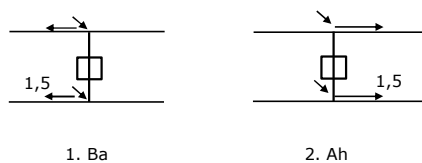
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: Geen (bestaande constructie)

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingsspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

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## Mastconstructie

### Eigenschappen

|   |          |         |
|---|----------|---------|
| Masttype                                    | Hoekmast |         |
| Mastbenaming                                | HA+0_n   |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m    |         |
| Masthoogte t.o.v. voetplaat                 | 45,0 m   |         |
| Gewicht mast                                | 455,0 kN |         |
| <i>Breedte en helling mast bij fundatie</i> |          |         |
|   | x-ri.    | y-ri.   |
| Pootsprei                                   | 11,00    | 11,00 m |
| Helling van de randstijl                    | 0,156    | 0,156 - |
| Factor spatkracht                           | 1,3      | 1,3 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,00 ( <i>Masthoogte &lt; 60 m</i> )  |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 9,60     | 11,00                 | 8,00                  | 9,60      | 0,156                 | 91,20                               | 15,71                               | 0,17                                      | 3,05           |
| Tussenstuk1   | 18,90    | 8,00                  | 5,84                  | 9,30      | 0,116                 | 64,37                               | 13,16                               | 0,20                                      | 2,91           |
| Tussenstuk2   | 27,70    | 5,84                  | 3,80                  | 8,80      | 0,116                 | 42,42                               | 11,52                               | 0,27                                      | 2,64           |
| Bovenstuk1    | 35,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 8,91                                | 0,34                                      | 2,40           |
| Bovenstuk2    | 43,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 5,97                                | 0,29                                      | 2,57           |
| Topstuk       | 45,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse | 27,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,76                                | 0,24                                      | 2,77           |
| Boventraverse | 39,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 8,36                                | 0,23                                      | 2,78           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 9,60     | 11,00                 | 8,00                  | 9,60      | 0,156                 | 91,20                               | 15,71                               | 0,17                                      | 3,05           |
| Tussenstuk1   | 18,90    | 8,00                  | 5,84                  | 9,30      | 0,116                 | 64,37                               | 13,16                               | 0,20                                      | 2,91           |
| Tussenstuk2   | 27,70    | 5,84                  | 3,80                  | 8,80      | 0,116                 | 42,42                               | 11,52                               | 0,27                                      | 2,64           |
| Bovenstuk1    | 35,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 8,91                                | 0,34                                      | 2,40           |
| Bovenstuk2    | 43,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 5,97                                | 0,29                                      | 2,57           |
| Topstuk       | 45,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse | 27,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,76                                | 0,24                                      | 2,77           |
| Boventraverse | 39,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 8,36                                | 0,23                                      | 2,78           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

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#### Windoppervlak feeders telecominstallaties

| Onderdeel   | A (m <sup>2</sup> /m) | Factor | Δh  | A <sub>1</sub> |
|-------------|-----------------------|--------|-----|----------------|
| Broekstuk   | 0,20                  | 0,71   | 9,6 | 1,4            |
| Tussenstuk1 | 0,20                  | 0,71   | 9,3 | 1,3            |
| Tussenstuk2 | 0,20                  | 0,71   | 8,8 | 1,2            |
| Bovenstuk1  | 0,20                  | 0,71   | 7,8 | 1,1            |
| Bovenstuk2  |                       |        |     |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>i</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,6                 | 31,7  | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 33,6                    | 28,5                    | 0,0                     | -28,5                   | 4,8                    | 161,5                    | 137,0                    | 0,0                      | -137,0                   |
| Tussenstuk1   | 0,79                                   | 30,2                    | 25,7                    | 0,0                     | -25,7                   | 14,3                   | 430,9                    | 365,6                    | 0,0                      | -365,6                   |
| Tussenstuk2   | 0,92                                   | 27,9                    | 23,7                    | 0,0                     | -23,7                   | 23,3                   | 651,0                    | 552,4                    | 0,0                      | -552,4                   |
| Bovenstuk1    | 1,01                                   | 21,5                    | 18,3                    | 0,0                     | -18,3                   | 31,6                   | 680,1                    | 577,1                    | 0,0                      | -577,1                   |
| Bovenstuk2    | 1,06                                   | 16,4                    | 13,9                    | 0,0                     | -13,9                   | 39,3                   | 642,6                    | 545,3                    | 0,0                      | -545,3                   |
| Topstuk       | 1,10                                   | 1,4                     | 1,2                     | 0,0                     | -1,2                    | 44,0                   | 60,8                     | 51,6                     | 0,0                      | -51,6                    |
| Ondertraverse | 0,98                                   | 36,7                    | 21,8                    | 0,0                     | -21,8                   | 29,0                   | 1065,5                   | 632,9                    | 0,0                      | -632,9                   |
| Boventraverse | 1,07                                   | 49,9                    | 29,6                    | 0,0                     | -29,6                   | 40,4                   | 2016,5                   | 1197,8                   | 0,0                      | -1197,8                  |

|               |              |              |            |               |  |  |               |               |            |                |
|---------------|--------------|--------------|------------|---------------|--|--|---------------|---------------|------------|----------------|
| <b>Totaal</b> | <b>217,7</b> | <b>162,7</b> | <b>0,0</b> | <b>-162,7</b> |  |  | <b>5709,0</b> | <b>4059,7</b> | <b>0,0</b> | <b>-4059,7</b> |
|---------------|--------------|--------------|------------|---------------|--|--|---------------|---------------|------------|----------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 0,0                     | 28,5                    | 33,6                    | 28,5                    | 4,8                    | 0,0                      | 137,0                    | 161,5                    | 137,0                    |
| Tussenstuk1   | 0,79                                   | 0,0                     | 25,7                    | 30,2                    | 25,7                    | 14,3                   | 0,0                      | 365,6                    | 430,9                    | 365,6                    |
| Tussenstuk2   | 0,92                                   | 0,0                     | 23,7                    | 27,9                    | 23,7                    | 23,3                   | 0,0                      | 552,4                    | 651,0                    | 552,4                    |
| Bovenstuk1    | 1,01                                   | 0,0                     | 18,3                    | 21,5                    | 18,3                    | 31,6                   | 0,0                      | 577,1                    | 680,1                    | 577,1                    |
| Bovenstuk2    | 1,06                                   | 0,0                     | 13,9                    | 16,4                    | 13,9                    | 39,3                   | 0,0                      | 545,3                    | 642,6                    | 545,3                    |
| Topstuk       | 1,10                                   | 0,0                     | 1,2                     | 1,4                     | 1,2                     | 44,0                   | 0,0                      | 51,6                     | 60,8                     | 51,6                     |
| Ondertraverse | 0,98                                   | 0,0                     | 21,8                    | 14,7                    | 21,8                    | 29,0                   | 0,0                      | 632,9                    | 426,2                    | 632,9                    |
| Boventraverse | 1,07                                   | 0,0                     | 29,6                    | 20,0                    | 29,6                    | 40,4                   | 0,0                      | 1197,8                   | 806,6                    | 1197,8                   |

|               |            |              |              |              |  |  |            |               |               |               |
|---------------|------------|--------------|--------------|--------------|--|--|------------|---------------|---------------|---------------|
| <b>Totaal</b> | <b>0,0</b> | <b>162,7</b> | <b>165,7</b> | <b>162,7</b> |  |  | <b>0,0</b> | <b>4059,7</b> | <b>3859,7</b> | <b>4059,7</b> |
|---------------|------------|--------------|--------------|--------------|--|--|------------|---------------|---------------|---------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting     | 0                      | 0                      | 455                    | 0                       | 0                       | 0                       |
| Windrichting 0°          | 225                    | 0                      | 0                      | 0                       | 5929                    | 0                       |
| Windrichting 45°         | 168                    | 168                    | 0                      | 4215                    | 4215                    | 0                       |
| Windrichting 90°         | 0                      | 173                    | 0                      | 4079                    | 0                       | 0                       |
| Windrichting 135°        | -168                   | 168                    | 0                      | 4215                    | -4215                   | 0                       |

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### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 28,20             | 0,97                             | 1,2               | 2,33                |
| 380ct1f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 28,20             | 0,97                             | 1,2               | 2,33                |
| 380ct1f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 39,50             | 1,07                             | 1,2               | 2,56                |
| 380ct2f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 28,20             | 0,97                             | 1,2               | 2,33                |
| 380ct2f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 28,20             | 0,97                             | 1,2               | 2,33                |
| 380ct2f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 39,50             | 1,07                             | 1,2               | 2,56                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 43,70             | 1,10                             | 1,2               | 0,13                |
| bl2      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 43,70             | 1,10                             | 1,2               | 0,13                |

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#### Windbelasting back

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 35,9   | 1,04                 | 0,59           | 0,65          | 1,09  | 28,25         | 56,5  | 62,2        | 46,9              | 103,8       | 114,2           |
| 380ct1f2 | 35,9   | 1,04                 | 0,59           | 0,65          | 1,09  | 28,25         | 56,5  | 62,2        | 46,9              | 103,8       | 114,2           |
| 380ct1f3 | 47,2   | 1,12                 | 0,61           | 0,67          | 1,06  | 28,25         | 61,8  | 68,0        | 46,9              | 115,8       | 127,3           |
| 380ct2f1 | 35,9   | 1,04                 | 0,59           | 0,65          | 1,09  | 28,25         | 56,5  | 62,2        | 46,9              | 103,8       | 114,2           |
| 380ct2f2 | 35,9   | 1,04                 | 0,59           | 0,65          | 1,09  | 28,25         | 56,5  | 62,2        | 46,9              | 103,8       | 114,2           |
| 380ct2f3 | 47,2   | 1,12                 | 0,61           | 0,67          | 1,06  | 28,25         | 61,8  | 68,0        | 46,9              | 115,8       | 127,3           |
| bl1      | 51,4   | 1,14                 | 0,62           | 0,68          | 1,18  | 22,24         | 18,6  | 20,5        | 63,1              | 53,7        | 59,0            |
| bl2      | 51,4   | 1,14                 | 0,62           | 0,68          | 1,19  | 22,13         | 18,6  | 20,4        | 63,0              | 53,6        | 58,9            |

#### Windbelasting ahead

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 19,9   | 0,88                 | 0,54           | 0,60          | 1,13  | 28,25         | 45,8  | 50,4        | 46,9              | 80,6        | 88,8            |
| 380ct1f2 | 19,9   | 0,88                 | 0,54           | 0,60          | 1,13  | 28,25         | 45,8  | 50,4        | 46,9              | 80,6        | 88,8            |
| 380ct1f3 | 31,2   | 1,00                 | 0,58           | 0,64          | 1,10  | 28,25         | 53,9  | 59,3        | 46,9              | 98,0        | 107,8           |
| 380ct2f1 | 19,9   | 0,88                 | 0,54           | 0,60          | 1,13  | 28,25         | 45,8  | 50,4        | 46,9              | 80,6        | 88,8            |
| 380ct2f2 | 19,9   | 0,88                 | 0,54           | 0,60          | 1,13  | 28,25         | 45,8  | 50,4        | 46,9              | 80,6        | 88,8            |
| 380ct2f3 | 31,2   | 1,00                 | 0,58           | 0,64          | 1,10  | 28,25         | 53,9  | 59,3        | 46,9              | 98,0        | 107,8           |
| bl1      | 35,4   | 1,03                 | 0,59           | 0,65          | 1,20  | 22,24         | 16,3  | 17,9        | 63,1              | 46,3        | 50,9            |
| bl2      | 35,4   | 1,03                 | 0,59           | 0,65          | 1,20  | 22,13         | 16,2  | 17,9        | 63,0              | 46,2        | 50,9            |

NB: belastingen  $w_v$  gelden voor bundel

Project: GT-RL380  
 Masttype: HA+0\_n  
 Mast: 25N

Auteur: TBR  
 Versie: v12.0

**Geleiderbelastingen**

**Uitgangspunten**  
 Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 50 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |              |                  |            |          |          |                     |  |
|--|---------------------------|------------------------------|--------------|------------------|------------|----------|----------|---------------------|--|
| Belastingsgeval  | omschrijving              | Temp<br>°C                   | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |  |
|  |                           |                              | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |  |
| ULS 1a   | Wind                      | 10°                          | 1,20         | 1,20             | 0,00       | 1,50     | 0,00     | 0,0                 |  |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90         | 1,20             | 0,00       | 1,50     | 0,00     | 0,0                 |  |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90         | 0,90             | 0,00       | 1,50     | 0,00     | 0,0                 |  |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20         | 1,20             | 0,00       | 0,45     | 1,50     | 0,0                 |  |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20             | 0,00       | 0,45     | 1,50     | 0,0                 |  |
| ULS 4  | Koude+wind                | -20°                         | 1,20         | 1,20             | 0,00       | 0,30     | 0,00     | 0,0                 |  |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90         | 1,20             | 0,00       | 0,30     | 0,00     | 0,0                 |  |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00         | 1,00             | 1,00       | 0,00     | 0,00     | 1,0                 |  |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00         | 1,00             | 0,00       | 0,00     | 0,00     | 1,0                 |  |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 1,50       | 0,30     | 0,00     | 0,0                 |  |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 0,00       | 0,30     | 0,00     | 0,0                 |  |
| ULS 7  | Permanent                 | 10°                          | 1,35         | 1,35             | 0,00       | 0,00     | 0,00     | 0,0                 |  |
| ULS 8  | Special                   | 10°                          | 1,00         | 1,00             | 0,00       | 0,00     | 0,00     | 1,0                 |  |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |  |
|  |                           |                              | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |  |
| SPLS 1a  | Wind                      | 10°                          | 1,20         | 1,20             | 0,0        | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90         | 1,20             | 0,0        | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90         | 0,90             | 0,0        | 0,78     | 0,00     | 0,0                 |  |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20         | 1,20             | 0,0        | 0,36     | 0,34     | 0,0                 |  |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20             | 0,0        | 0,36     | 0,34     | 0,0                 |  |
| SPLS 4   | Koude+wind                | -20°                         | 1,20         | 1,20             | 0,0        | 0,24     | 0,00     | 0,0                 |  |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90         | 1,20             | 0,0        | 0,24     | 0,00     | 0,0                 |  |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 1,2        | 0,24     | 0,0      | 0,0                 |  |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 0,0        | 0,24     | 0,0      | 0,0                 |  |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              | $G_k$        |                  | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |  |
| SLS 1a   | Wind                      | 10°                          | 1,00         | 1,00             | 0,0        | 1,00     | 0,0      | 0,0                 |  |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00         | 1,00             | 0,0        | 0,30     | 1,00     | 0,0                 |  |
| SLS 4  | Wind                      | -20°                         | 1,00         | 1,00             | 0,0        | 0,20     | 0,0      | 0,0                 |  |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00         | 1,00             | 0,0        | 0,20     | 0,0      | 0,0                 |  |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00         | 1,00             | 0,0        | 0,00     | 0,0      | 0,0                 |  |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 54  
 Aantal belastingcombinaties SPLS 222  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 4656



Project: GT-RLL380  
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### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -62,0         | 60,7          | 15,9          | 15,0          | 10,3          | 10,3          |
| bl2      | -61,2         | 59,9          | 15,8          | 14,8          | 10,2          | 10,2          |
| 380ct1f1 | -156,9        | 151,6         | 46,7          | 40,5          | 28,8          | 28,7          |
| 380ct1f2 | -156,9        | 151,6         | 46,7          | 40,5          | 28,8          | 28,7          |
| 380ct1f3 | -160,0        | 155,5         | 49,8          | 45,2          | 28,8          | 28,8          |
| 380ct2f1 | -156,9        | 151,6         | 46,7          | 40,5          | 28,8          | 28,7          |
| 380ct2f2 | -156,9        | 151,6         | 46,7          | 40,5          | 28,8          | 28,7          |
| 380ct2f3 | -160,0        | 155,5         | 49,8          | 45,2          | 28,8          | 28,8          |

#### Min. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 440,1  | 447,2 | 440,0 |
| bl2      | 440,1  | 447,4 | 440,0 |
| 380ct1f1 | 440,0  | 445,4 | 440,0 |
| 380ct1f2 | 440,0  | 445,4 | 440,0 |
| 380ct1f3 | 440,0  | 445,7 | 440,0 |
| 380ct2f1 | 440,0  | 445,4 | 440,0 |
| 380ct2f2 | 440,0  | 445,4 | 440,0 |
| 380ct2f3 | 440,0  | 445,7 | 440,0 |

#### Max. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 486,7  | 433,4 |
| bl2      | 487,9  | 433,2 |
| 380ct1f1 | 464,4  | 440,2 |
| 380ct1f2 | 464,4  | 440,2 |
| 380ct1f3 | 469,2  | 441,1 |
| 380ct2f1 | 464,4  | 440,2 |
| 380ct2f2 | 464,4  | 440,2 |
| 380ct2f3 | 469,2  | 441,1 |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

| Voor alle geleiders | Wind / Weight span verhouding |
|---------------------|-------------------------------|
| Max. weight span    | 487,9 m                       |
| Min. weight span    | 7,4 m                         |
|                     | 1,220 -                       |
|                     | 0,018 -                       |

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**Maximale waarden back+ahead span      Maximale waarden trekkracht geleider**

| Geleider | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN] | Ft_ah<br>[kN] |
|----------|------------|------------|------------|---------------|---------------|
| bl1      | 35,3       | 30,5       | 10,3       | -63,9         | 62,4          |
| bl2      | 34,8       | 30,2       | 10,2       | -63,0         | 61,5          |
| 380ct1f1 | 118,3      | 85,2       | 28,8       | -161,2        | 155,4         |
| 380ct1f2 | 118,3      | 85,2       | 28,8       | -161,2        | 155,4         |
| 380ct1f3 | 119,9      | 92,7       | 28,8       | -164,5        | 159,6         |
| 380ct2f1 | 118,3      | 85,2       | 28,8       | -161,2        | 155,4         |
| 380ct2f2 | 118,3      | 85,2       | 28,8       | -161,2        | 155,4         |
| 380ct2f3 | 119,9      | 92,7       | 28,8       | -164,5        | 159,6         |

**EDS-belastingen geleiders**

| Geleider | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN] | Ft_ah<br>[kN] |
|----------|------------|------------|------------|---------------|---------------|
| bl1      | 15,1       | 2,7        | 2,2        | -15,3         | 15,3          |
| bl2      | 14,7       | 2,6        | 2,1        | -14,9         | 14,9          |
| 380ct1f1 | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct1f2 | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct1f3 | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct2f1 | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct2f2 | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct2f3 | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |

**Controle uplift SLS-wind**

| Combinati | Geleider | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-----------|----------|---------------|---------------|
| SLS 4     | bl1      | 0,0           | 0,0           |
|           | bl2      | 0,0           | 0,0           |
|           | 380ct1f1 | 0,0           | 0,0           |
|           | 380ct1f2 | 0,0           | 0,0           |
|           | 380ct1f3 | 0,0           | 0,0           |
|           | 380ct2f1 | 0,0           | 0,0           |
|           | 380ct2f2 | 0,0           | 0,0           |
|           | 380ct2f3 | 0,0           | 0,0           |

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**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -96           | 574           | 252           | 18745          | -3026          | 0              |
| ULS 1a_0,9_0      |             | 1             | 192           | 184           | 6198           | 37             | 0              |
| ULS 1a_0,9_0,9_90 |             | -104          | 557           | 95            | 18191          | -3294          | 0              |
| ULS 3_0           |             | 1             | 344           | 384           | 11300          | 23             | 0              |
| SLS 7             |             | 0             | 163           | 202           | 5260           | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

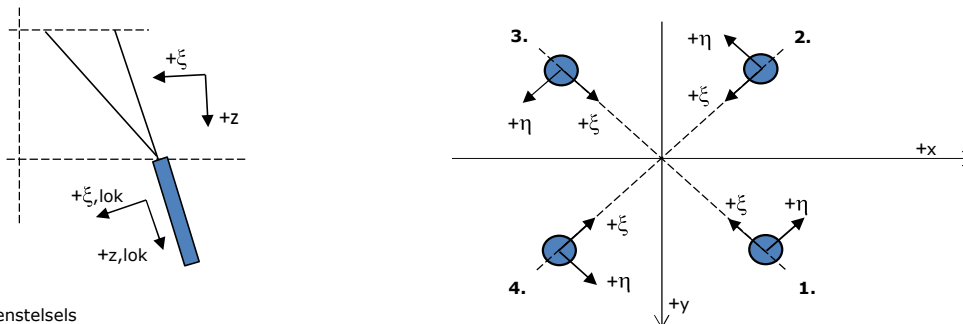
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -96           | 833           | 798           | 24864          | -3026          | 0              |
| ULS 1a_0,9_0,9_90 | -104          | 816           | 504           | 24310          | -3294          | 0              |
| SLS 7             | 0             | 163           | 657           | 5260           | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie                | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_90             | -96           | 833           | 557           | <b>24865</b>   | -3026          | 0              |
| SPLS 3_90 Ah All Cts      | -770          | 235           | 726           | 7105           | <b>-25083</b>  | 8              |
| SPLS 3_80 Ba Ct1          | 345           | 304           | 772           | 9916           | 11108          | <b>-4957</b>   |
| SPLS 1a_0,9_90 Ah All Cts | -694          | 338           | 510           | <b>9784</b>    | <b>-22511</b>  | 7              |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie           | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|----------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_90 Ba All Cts | 283           | 314           | <b>1576</b>   | -22              | -422            | -74                   | 1614                |
| 2     | SPLS 3_0 Ba All Cts  | 187           | -223          | <b>1071</b>   | 25               | -290            | -53                   | 1097                |
| 3     | SPLS 3_90 Ah All Cts | -164          | -209          | <b>999</b>    | -32              | -264            | -43                   | 1023                |
| 4     | SPLS 3_80 Ah All Cts | -294          | 328           | <b>1646</b>   | 24               | -440            | -76                   | 1686                |

**Maximale trekbelasting**

| Stijl | Combinatie                | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_90 Ah All Cts  | -100          | -147          | <b>-688</b>   | 33               | 175             | 23                    | -705                |
| 2     | SPLS 1a_0,9_90 Ah All Cts | -238          | 266           | <b>-1341</b>  | -20              | 357             | 60                    | -1373               |
| 3     | SPLS 3_0,9_90 Ba All Cts  | 217           | 247           | <b>-1250</b>  | 22               | 328             | 52                    | -1280               |
| 4     | SPLS 3_0,9_0 Ba All Cts   | 120           | -157          | <b>-745</b>   | -26              | 196             | 31                    | -763                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ba Ct1 | 125           | -128          | -29           | <b>179</b>       | 2               | -4                    | -29                 |
| 2     | SPLS 3_0,9_80 Ba Ct2     | -81           | -169          | 233           | <b>177</b>       | -62             | -10                   | 238                 |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | 10            | 247           | -695          | <b>168</b>       | 182             | 28                    | -711                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -97           | 329           | 1124          | <b>164</b>       | -301            | -53                   | 1151                |

**Maximale torsiebelasting (negatief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 94            | 328           | 1112          | <b>-165</b>      | -298            | -53                   | 1139                |
| 2     | SPLS 6a_90 Ah Ct2 Ba Ct2 | -13           | 249           | -707          | <b>-167</b>      | 185             | 29                    | -724                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 40            | -208          | 444           | <b>-175</b>      | -118            | -20                   | 454                 |
| 4     | SPLS 3_80 Ba Ct1         | -157          | -100          | 139           | <b>-182</b>      | -40             | -10                   | 142                 |

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#### Combinatie Ftrek+Fhor

| Stijl | Combinatie               | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|--------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_90 Ah All Cts | -100                   | -147                   | <b>-688</b>            | <b>33</b>              | 175                    | 23                         | -705                       |
| 2     | SPLS 3_0,9_80 Ah All Cts | -232                   | 264                    | <b>-1336</b>           | <b>-23</b>             | 351                    | 55                         | -1368                      |
| 3     | SPLS 3_0,9_90 Ba All Cts | 217                    | 247                    | <b>-1250</b>           | <b>22</b>              | 328                    | 52                         | -1280                      |
| 4     | SPLS 3_0,9_0 Ba All Cts  | 120                    | -157                   | <b>-745</b>            | <b>-26</b>             | 196                    | 31                         | -763                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 82                     | 74                     | 403                    | 5                      | -110                   | -21                        | 413                        |
| 2     | SLS 7      | -15                    | 7                      | -75                    | 5                      | 16                     | -1                         | -77                        |
| 3     | SLS 7      | 15                     | 7                      | -75                    | -5                     | 16                     | -1                         | -77                        |
| 4     | SLS 7      | -82                    | 74                     | 403                    | -5                     | -110                   | -21                        | 413                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | SPLS 3_80 Ah All Cts      | -294                   | 328                    | <b>1646</b>            | 24                     | -440                   | -76                        | 1686                       |
| Max. trek         | SPLS 1a_0,9_90 Ah All Cts | -238                   | 266                    | <b>-1341</b>           | -20                    | 357                    | 60                         | -1373                      |
| Max. pos. torsie  | SPLS 6a_90 Ah Ct1 Ba Ct1  | 125                    | -128                   | -29                    | <b>179</b>             | 2                      | -4                         | -29                        |
| Max. neg. torsie  | SPLS 3_80 Ba Ct1          | -157                   | -100                   | 139                    | <b>-182</b>            | -40                    | -10                        | 142                        |
| Comb. trek+torsie | SPLS 3_0,9_80 Ah All Cts  | -232                   | 264                    | <b>-1336</b>           | <b>-23</b>             | 351                    | 55                         | -1368                      |

#### Maximale trekbelasting SLS

| Stijl | Combinatie               | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|--------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_80 Ah All Cts | -98                    | -146                   | <b>-682</b>            | 33                     | 173                    | 22                         | -698                       |
| 2     | SPLS 3_0,9_80 Ah All Cts | -232                   | 264                    | <b>-1336</b>           | -23                    | 351                    | 55                         | -1368                      |
| 3     | SPLS 1a_0,9_100 Ba Ct2   | 61                     | 262                    | <b>-859</b>            | 142                    | 228                    | 39                         | -880                       |
| 4     | SPLS 3_0,9_100 Ba Ct2    | 81                     | 108                    | <b>43</b>              | 134                    | -19                    | -10                        | 44                         |

#### Maximale drukbelasting SLS

| Stijl | Combinatie           | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_100 Ba Ct2   | 318                    | 137                    | <b>1172</b>            | 128                    | -321                   | -62                        | 1200                       |
| 2     | SPLS 3_100 Ba Ct2    | -63                    | -178                   | <b>318</b>             | 171                    | -81                    | -11                        | 326                        |
| 3     | SPLS 3_80 Ah All Cts | -162                   | -208                   | <b>993</b>             | -33                    | -262                   | -42                        | 1016                       |
| 4     | SPLS 3_80 Ah All Cts | -294                   | 328                    | <b>1646</b>            | 24                     | -440                   | -76                        | 1686                       |

Project: GT-RL380  
Masttype: HA+0\_n  
Mast: 25N





Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

Auteur: TBR  
 Versie: v12.0

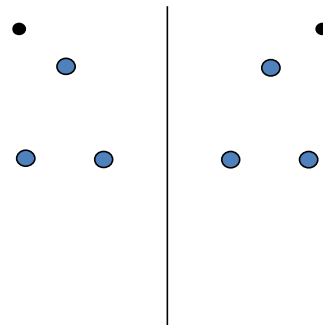
### Geleiderbelastingen

#### Algemeen

Benaming HA\_n (bouwfase)  
 Masttype Hoekmast  
 Aantal circuits 1  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 1

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 15 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsg gebied fasegeleider B  
 IJsg gebied bliksemgeleider A



Configuratie geleiders

#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging     | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Bliksemdraad 1 | Afspanketting | 0,10         | 0,20       | 0,10                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 32,7 m       | 32,7 m       | -15,7 m                                |
| Circuit 1      | 11         | 380ct1f2 | 32,7 m       | 32,7 m       | -8,7 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 44,0 m       | 44,0 m       | -12,2 m                                |
| Bliksemdraad 1 | 1          | bl1      | 48,2 m       | 48,2 m       | -18,4 m                                |

Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead  |   |
|------------------------------------|---------------------------|--------|---|
| Verhoging voor windbelasting       | 32,0 m                    | 0,0 m  | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -5,0 m                    | -5,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |        |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

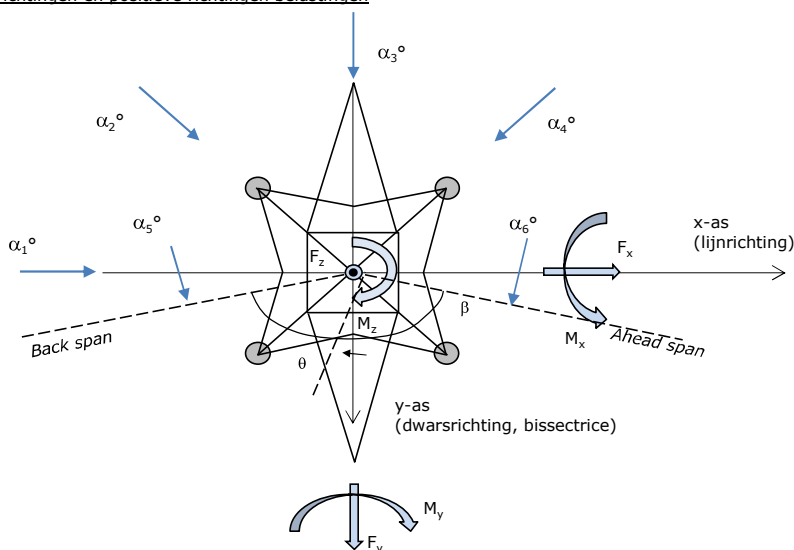
| Circuits       | Aanduiding | Nummer   | Hoogteverschil    |                    | Richtingsverandering |                    |       |
|----------------|------------|----------|-------------------|--------------------|----------------------|--------------------|-------|
|                |            |          | $\Delta h_{back}$ | $\Delta h_{ahead}$ | $\Delta y_{back}$    | $\Delta y_{ahead}$ |       |
| Circuit 1      | 10         | 380ct1f1 | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |
| Circuit 1      | 11         | 380ct1f2 | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |
| Circuit 1      | 12         | 380ct1f3 | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |
| Bliksemdraad 1 | 1          | bl1      | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek                                   | $\beta$    | 160 °   |
| Rotatie mast t.o.v. bissectrice            | $\theta$   | 0 °     |
| Vaklengte                                  | 400        | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 80 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 100 °   |
|  | $\alpha_5$ | 225 °   |
|  | $\alpha_6$ | 270 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



Beschouwd aantal windrichtingen

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |



Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

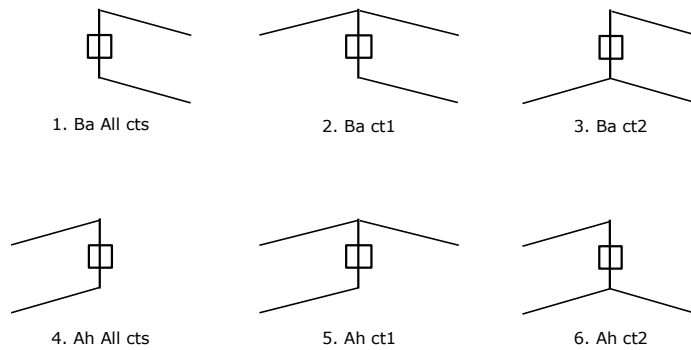
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |

### Belastingsituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

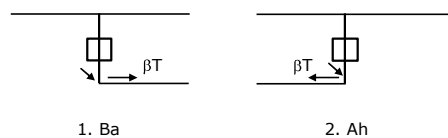
Principe belastingssituaties:



### Belastingsituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

### Belastingsituaties 6. Bouw- en onderhoud

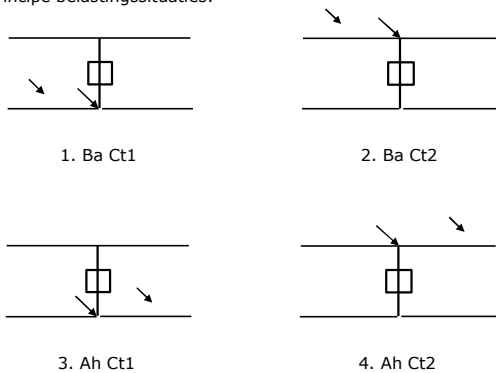
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



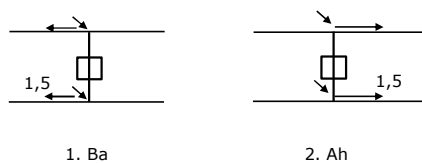
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

## Mastconstructie

### Eigenschappen

|   |                 |         |
|---|-----------------|---------|
| Masttype                                    | Hoekmast        |         |
| Mastbenaming                                | HA_n (bouwfase) |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m           |         |
| Masthoogte t.o.v. voetplaat                 | 50,0 m          |         |
| Gewicht mast                                | 492,0 kN        |         |
| <i>Breedte en helling mast bij fundatie</i> |                 |         |
|   | x-ri.           | y-ri.   |
| Pootsprei                                   | 11,58           | 11,58 m |
| Helling van de randstijl                    | 0,399           | 0,399 - |
| Factor spatkracht                           | 1,3             | 1,3 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,00 ( <i>Masthoogte &lt; 60 m</i> )  |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 8,54     | 11,58                 | 4,77                  | 8,54      | 0,399                 | 69,81                               | 13,53                               | 0,19                                      | 2,96           |
| Tussenstuk1   | 19,03    | 4,77                  | 6,96                  | 10,49     | -0,104                | 61,52                               | 13,15                               | 0,21                                      | 2,87           |
| Tussenstuk2   | 32,70    | 6,96                  | 3,80                  | 13,67     | 0,116                 | 73,54                               | 16,36                               | 0,22                                      | 2,83           |
| Bovenstuk1    | 40,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 7,84                                | 0,30                                      | 2,54           |
| Bovenstuk2    | 48,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 4,92                                | 0,24                                      | 2,77           |
| Topstuk       | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,43                                | 0,17                                      | 3,09           |
| Ondertraverse | 32,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,40                                | 0,23                                      | 2,82           |
| Boventraverse | 44,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 7,96                                | 0,22                                      | 2,83           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 8,54     | 11,58                 | 4,77                  | 8,54      | 0,399                 | 69,81                               | 13,53                               | 0,19                                      | 2,96           |
| Tussenstuk1   | 19,03    | 4,77                  | 6,96                  | 10,49     | -0,104                | 61,52                               | 13,15                               | 0,21                                      | 2,87           |
| Tussenstuk2   | 32,70    | 6,96                  | 3,80                  | 13,67     | 0,116                 | 73,54                               | 16,36                               | 0,22                                      | 2,83           |
| Bovenstuk1    | 40,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 7,84                                | 0,30                                      | 2,54           |
| Bovenstuk2    | 48,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 4,92                                | 0,24                                      | 2,77           |
| Topstuk       | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,43                                | 0,17                                      | 3,09           |
| Ondertraverse | 32,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,40                                | 0,23                                      | 2,82           |
| Boventraverse | 44,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 7,96                                | 0,22                                      | 2,83           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

#### Windoppervlak feeders telecominstallaties

| Onderdeel   | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------|-----------------------|--------|------|----------------|
| Broekstuk   | 0,20                  | 0,71   | 8,5  | 1,2            |
| Tussenstuk1 | 0,20                  | 0,71   | 10,5 | 1,5            |
| Tussenstuk2 | 0,20                  | 0,71   | 13,7 | 1,9            |
| Bovenstuk1  | 0,20                  | 0,71   | 7,8  | 1,1            |
| Bovenstuk2  |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>r</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,6                 | 31,7  | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 28,1                    | 5,0                     | 0,0                     | -5,0                    | 4,3                    | 119,8                    | 21,3                     | 0,0                      | -21,3                    |
| Tussenstuk1   | 0,78                                   | 29,5                    | 5,2                     | 0,0                     | -5,2                    | 13,8                   | 406,5                    | 72,2                     | 0,0                      | -72,2                    |
| Tussenstuk2   | 0,95                                   | 43,9                    | 7,8                     | 0,0                     | -7,8                    | 25,9                   | 1136,4                   | 201,9                    | 0,0                      | -201,9                   |
| Bovenstuk1    | 1,05                                   | 20,9                    | 3,7                     | 0,0                     | -3,7                    | 36,6                   | 763,2                    | 135,6                    | 0,0                      | -135,6                   |
| Bovenstuk2    | 1,10                                   | 15,0                    | 2,7                     | 0,0                     | -2,7                    | 44,3                   | 663,6                    | 117,9                    | 0,0                      | -117,9                   |
| Topstuk       | 1,13                                   | 1,5                     | 0,3                     | 0,0                     | -0,3                    | 49,0                   | 73,3                     | 13,0                     | 0,0                      | -13,0                    |
| Ondertraverse | 1,02                                   | 37,0                    | 2,7                     | 0,0                     | -2,7                    | 34,0                   | 1259,1                   | 93,6                     | 0,0                      | -93,6                    |
| Boventraverse | 1,11                                   | 49,9                    | 3,7                     | 0,0                     | -3,7                    | 45,4                   | 2264,4                   | 168,2                    | 0,0                      | -168,2                   |

|               |              |             |            |              |  |               |              |            |               |
|---------------|--------------|-------------|------------|--------------|--|---------------|--------------|------------|---------------|
| <b>Totaal</b> | <b>225,7</b> | <b>31,1</b> | <b>0,0</b> | <b>-31,1</b> |  | <b>6686,3</b> | <b>823,9</b> | <b>0,0</b> | <b>-823,9</b> |
|---------------|--------------|-------------|------------|--------------|--|---------------|--------------|------------|---------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 0,0                     | 28,3                    | 28,1                    | 28,3                    | 4,3                    | 0,0                      | 120,8                    | 119,8                    | 120,8                    |
| Tussenstuk1   | 0,78                                   | 0,0                     | 29,7                    | 29,5                    | 29,7                    | 13,8                   | 0,0                      | 409,7                    | 406,5                    | 409,7                    |
| Tussenstuk2   | 0,95                                   | 0,0                     | 44,3                    | 43,9                    | 44,3                    | 25,9                   | 0,0                      | 1145,3                   | 1136,4                   | 1145,3                   |
| Bovenstuk1    | 1,05                                   | 0,0                     | 21,0                    | 20,9                    | 21,0                    | 36,6                   | 0,0                      | 769,2                    | 763,2                    | 769,2                    |
| Bovenstuk2    | 1,10                                   | 0,0                     | 15,1                    | 15,0                    | 15,1                    | 44,3                   | 0,0                      | 668,9                    | 663,6                    | 668,9                    |
| Topstuk       | 1,13                                   | 0,0                     | 1,5                     | 1,5                     | 1,5                     | 49,0                   | 0,0                      | 73,9                     | 73,3                     | 73,9                     |
| Ondertraverse | 1,02                                   | 0,0                     | 15,6                    | 14,8                    | 15,6                    | 34,0                   | 0,0                      | 530,5                    | 503,6                    | 530,5                    |
| Boventraverse | 1,11                                   | 0,0                     | 21,0                    | 20,0                    | 21,0                    | 45,4                   | 0,0                      | 954,1                    | 905,8                    | 954,1                    |

|               |            |              |              |              |  |            |               |               |               |
|---------------|------------|--------------|--------------|--------------|--|------------|---------------|---------------|---------------|
| <b>Totaal</b> | <b>0,0</b> | <b>176,5</b> | <b>173,6</b> | <b>176,5</b> |  | <b>0,0</b> | <b>4672,4</b> | <b>4572,3</b> | <b>4672,4</b> |
|---------------|------------|--------------|--------------|--------------|--|------------|---------------|---------------|---------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting     | 0                      | 0                      | 492                    | 0                       | 0                       | 0                       |
| Windrichting 0°          | 233                    | 0                      | 0                      | 0                       | 6906                    | 0                       |
| Windrichting 80°         | 32                     | 183                    | 0                      | 4889                    | 862                     | 0                       |
| Windrichting 90°         | 0                      | 181                    | 0                      | 4792                    | 0                       | 0                       |
| Windrichting 100°        | -32                    | 183                    | 0                      | 4889                    | -862                    | 0                       |

Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $w_{z,G}$<br>[N/m] | IJsgebied | Formule | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $w_{z,G}$<br>[N/m] | IJsgebied | Formule | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 48,70             | 1,13                             | 1,2               | 0,14                |

Project: GT-RLL380  
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 Number: 18N

**Windbelasting back**

| Geleider | hoogte      |                                  | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $W_y$ | $W_{y,vak}$ | $D_{ijs,toeslag}$ | $W_{y,ijs}$ | $W_{y,ijs,vak}$ |
|----------|-------------|----------------------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] |                |               |       |               |       |             |                   |             |                 |
| 380ct1f1 | 40,9        | 1,08                             | 0,60           | 0,66          | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct1f2 | 40,9        | 1,08                             | 0,60           | 0,66          | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct1f3 | 52,2        | 1,15                             | 0,62           | 0,68          | 1,06  | 28,25         | 63,8  | 70,1        | 46,9              | 120,4       | 132,3           |
| bl1      | 56,4        | 1,17                             | 0,63           | 0,69          | 1,18  | 22,24         | 19,2  | 21,1        | 63,1              | 55,6        | 61,1            |

**Windbelasting ahead**

| Geleider | hoogte      |                                  | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $W_y$ | $W_{y,vak}$ | $D_{ijs,toeslag}$ | $W_{y,ijs}$ | $W_{y,ijs,vak}$ |
|----------|-------------|----------------------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] |                |               |       |               |       |             |                   |             |                 |
| 380ct1f1 | 24,9        | 0,94                             | 0,56           | 0,62          | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct1f2 | 24,9        | 0,94                             | 0,56           | 0,62          | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct1f3 | 36,2        | 1,04                             | 0,59           | 0,65          | 1,08  | 28,25         | 56,7  | 62,4        | 46,9              | 104,2       | 114,6           |
| bl1      | 40,4        | 1,07                             | 0,60           | 0,66          | 1,20  | 22,24         | 17,2  | 18,9        | 63,1              | 48,8        | 53,7            |

NB: belastingen  $w_v$  gelden voor bundel

Project: GT-RL380  
 Masttype: HA\_n (bouwfase)  
 Mast: 18N

Auteur: TBR  
 Versie: v12.0

### Geleiderbelastingen

**Uitgangspunten**  
 Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 15 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |              |                     |  |          |          |                     |  |
|--|---------------------------|------------------------------|--------------|---------------------|--|----------|----------|---------------------|--|
| Belastingsgeval  | omschrijving              | Temp<br>°C                   | $\gamma_G$   |                     | $\gamma_Q$                               |          |          | $\gamma_a$<br>$A_k$ |  |
|  |                           |                              | $G_{k,mast}$ | $G_{k,geleider}$    | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ |                     |  |
| ULS 1a   | Wind                      | 10°                          | 1,20         | 1,20                | 0,00                                     | 1,25     | 0,00     | 0,0                 |  |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90         | 1,20                | 0,00                                     | 1,25     | 0,00     | 0,0                 |  |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90         | 0,90                | 0,00                                     | 1,25     | 0,00     | 0,0                 |  |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20         | 1,20                | 0,00                                     | 0,38     | 1,07     | 0,0                 |  |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20                | 0,00                                     | 0,38     | 1,07     | 0,0                 |  |
| ULS 4  | Koude+wind                | -20°                         | 1,20         | 1,20                | 0,00                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90         | 1,20                | 0,00                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00         | 1,00                | 1,00                                     | 0,00     | 0,00     | 1,0                 |  |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |  |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 1,50                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 0,00                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 7  | Permanent                 | 10°                          | 1,35         | 1,35                | 0,00                                     | 0,00     | 0,00     | 0,0                 |  |
| ULS 8  | Special                   | 10°                          | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |  |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              |              | $\gamma_G$<br>$G_k$ | $\gamma_Q$<br>$Q_{pk}$ $Q_{wk}$ $Q_{ik}$ |          |          | $A_k$               |  |
| SPLS 1a  | Wind                      | 10°                          | 1,20         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90         | 0,90                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |  |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |  |
| SPLS 4   | Koude+wind                | -20°                         | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |  |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |  |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 1,2                                      | 0,24     | 0,0      | 0,0                 |  |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,0      | 0,0                 |  |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              |              | $G_k$               | $Q_{pk}$ $Q_{wk}$ $Q_{ik}$               |          |          | $A_k$               |  |
| SLS 1a   | Wind                      | 10°                          | 1,00         | 1,00                | 0,0                                      | 0,87     | 0,0      | 0,0                 |  |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00         | 1,00                | 0,0                                      | 0,26     | 0,71     | 0,0                 |  |
| SLS 4  | Wind                      | -20°                         | 1,00         | 1,00                | 0,0                                      | 0,17     | 0,0      | 0,0                 |  |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00         | 1,00                | 0,0                                      | 0,17     | 0,0      | 0,0                 |  |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00         | 1,00                | 0,0                                      | 0,00     | 0,0      | 0,0                 |  |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 54  
 Aantal belastingcombinaties SPLS 210  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 2232

Project: GT-RLL380  
 Masttype: HA\_n (bouwfase)  
 Mast: 18N

### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -51,7         | 50,3          | 13,2          | 12,5          | 7,6           | 7,6           |
| 380ct1f1 | -143,3        | 138,9         | 42,1          | 37,6          | 27,3          | 27,3          |
| 380ct1f2 | -143,3        | 138,9         | 42,1          | 37,6          | 27,3          | 27,3          |
| 380ct1f3 | -145,9        | 142,1         | 44,4          | 40,9          | 27,3          | 27,3          |

#### Min. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 440,1  | 446,7 | 440,0 |
| 380ct1f1 | 440,0  | 445,3 | 440,0 |
| 380ct1f2 | 440,0  | 445,3 | 440,0 |
| 380ct1f3 | 440,0  | 445,5 | 440,0 |

#### Max. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 479,0  | 437,2 |
| 380ct1f1 | 460,3  | 441,4 |
| 380ct1f2 | 460,3  | 441,4 |
| 380ct1f3 | 463,7  | 442,2 |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

Max. weight span 479,0 m  
 Min. weight span 53,5 m

Wind / Weight span verhouding

1,197 -  
 0,134 -



Project: GT-RLL380  
 Masttype: HA\_n (bouwfase)  
 Mast: 18N

| Geleider | Maximale waarden back+ahead span |            |            | Maximale waarden trekkracht geleider |               |
|----------|----------------------------------|------------|------------|--------------------------------------|---------------|
|          | Fx<br>[kN]                       | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN]                        | Ft_ah<br>[kN] |
| bl1      | 36,0                             | 25,4       | 7,6        | -52,2                                | 50,7          |
| 380ct1f1 | 118,9                            | 77,9       | 27,3       | -144,7                               | 140,3         |
| 380ct1f2 | 118,9                            | 77,9       | 27,3       | -144,7                               | 140,3         |
| 380ct1f3 | 122,0                            | 83,4       | 27,3       | -147,5                               | 143,5         |

| EDS-belastingen geleiders |            |            |            |               |               |
|---------------------------|------------|------------|------------|---------------|---------------|
| Geleider                  | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN] | Ft_ah<br>[kN] |
| bl1                       | 15,1       | 2,7        | 2,2        | -15,3         | 15,3          |
| 380ct1f1                  | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct1f2                  | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct1f3                  | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |

| Controle uplift SLS-wind |          |          |               |               |
|--------------------------|----------|----------|---------------|---------------|
| Combinati                |          | Geleider | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
| SLS 4                    | bl1      |          | 0,0           | 0,0           |
|                          | 380ct1f1 |          | 0,0           | 0,0           |
|                          | 380ct1f2 |          | 0,0           | 0,0           |
|                          | 380ct1f3 |          | 0,0           | 0,0           |

Project: GT-RLL380  
 Masttype: HA\_n (bouwfase)  
 Mast: 18N

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -34           | 261           | 125           | 8246           | -1257          | 432            |
| ULS 1a_0,9_0      |             | 1             | 96            | 92            | 2438           | 20             | -7             |
| ULS 1a_0,9_0,9_90 |             | -38           | 251           | 51            | 8820           | -1391          | 479            |
| ULS 3_0           |             | 0             | 152           | 171           | 3556           | 11             | -4             |
| SLS 7             |             | 0             | 82            | 101           | 1784           | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

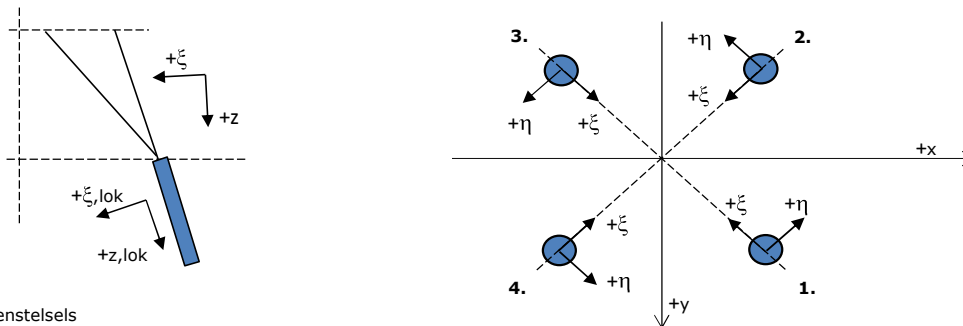
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -34           | 487           | 715           | 14250          | -1257          | 432            |
| ULS 1a_0,9_0,9_90 | -38           | 477           | 494           | 14824          | -1391          | 479            |
| SLS 7             | 0             | 82            | 593           | 1784           | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie                 | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|----------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_90              | -34           | 487           | 520           | <b>14858</b>   | -1257          | 432            |
| SPLS 1a_225 Ah All Cts     | -458          | -106          | 673           | -3774          | <b>-15883</b>  | 4076           |
| SPLS 3_270 Ah All Cts      | -396          | -15           | 680           | -953           | -14874         | <b>5050</b>    |
| SPLS 1a_0,9_100 Ah All Cts | -365          | 242           | 493           | <b>6901</b>    | <b>-13402</b>  | 4311           |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie             | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 1a_80 Ba All Cts  | 226           | 522           | <b>991</b>    | -209             | -528            | 31                    | 1138                |
| 2     | SPLS 1a_270 Ba All Cts | 356           | -312          | <b>896</b>    | -31              | -472            | 33                    | 1028                |
| 3     | SPLS 1a_225 Ah All Cts | -374          | -381          | <b>1017</b>   | -5               | -534            | 39                    | 1168                |
| 4     | SPLS 1a_100 Ah All Cts | -231          | 541           | <b>1027</b>   | 219              | -546            | 34                    | 1179                |

**Maximale trekbelasting**

| Stijl | Combinatie                 | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|----------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 1a_0,9_225 Ah All Cts | -38           | -406          | <b>-708</b>   | 260              | 314             | -85                   | -813                |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -275          | 203           | <b>-753</b>   | 51               | 338             | -86                   | -865                |
| 3     | SPLS 1a_0,9_80 Ba All Cts  | 250           | 189           | <b>-695</b>   | -43              | 310             | -82                   | -798                |
| 4     | SPLS 1a_0,9_270 Ba All Cts | 11            | -346          | <b>-595</b>   | -237             | 252             | -83                   | -683                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_80 Ah All Cts | 177           | -329          | -309          | <b>358</b>       | 108             | -66                   | -354                |
| 2     | ULS 1a_0,9_0,9_80        | -292          | 69            | -576          | <b>158</b>       | 255             | -70                   | -661                |
| 3     | ULS 1a_0                 | 27            | 126           | -286          | <b>70</b>        | 108             | -53                   | -329                |
| 4     | SPLS 1a_225 Ah All Cts   | -29           | 504           | 691           | <b>336</b>       | -377            | 13                    | 793                 |

**Maximale torsiebelasting (negatief)**

| Stijl | Combinatie                | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_270 Ba All Cts     | 56            | 507           | 741           | <b>-318</b>      | -398            | 20                    | 851                 |
| 2     | ULS 1a_225                | 115           | 55            | 8             | <b>-120</b>      | -42             | -38                   | 9                   |
| 3     | ULS 1a_0,9_0,9_100        | 251           | 28            | -455          | <b>-158</b>      | 197             | -60                   | -522                |
| 4     | SPLS 3_0,9_100 Ba All Cts | -167          | -307          | -298          | <b>-335</b>      | 99              | -69                   | -342                |

Project: GT-RLL380  
 Masttype: HA\_n (bouwfase)  
 Mast: 18N

#### Combinatie Ftrek+Fhor

| Stijl | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_0,9_225 Ah All Cts | -38                    | -406                   | <b>-708</b>            | <b>260</b>             | 314                    | -85                        | -813                       |
| 2     | ULS 1a_0,9_0,9_80          | -292                   | 69                     | <b>-576</b>            | <b>158</b>             | 255                    | -70                        | -661                       |
| 3     | ULS 1a_0,9_0,9_100         | 251                    | 28                     | <b>-455</b>            | <b>-158</b>            | 197                    | -60                        | -522                       |
| 4     | SPLS 3_0,9_270 Ba All Cts  | -57                    | -358                   | <b>-522</b>            | <b>-294</b>            | 213                    | -82                        | -600                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 117                    | 97                     | 225                    | 14                     | -151                   | -24                        | 259                        |
| 2     | SLS 7      | 37                     | -56                    | 71                     | 14                     | -66                    | -26                        | 82                         |
| 3     | SLS 7      | -37                    | -56                    | 71                     | -14                    | -66                    | -26                        | 82                         |
| 4     | SLS 7      | -117                   | 97                     | 225                    | -14                    | -151                   | -24                        | 259                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | SPLS 1a_100 Ah All Cts     | -231                   | 541                    | <b>1027</b>            | 219                    | -546                   | 34                         | 1179                       |
| Max. trek         | SPLS 1a_0,9_100 Ah All Cts | -275                   | 203                    | <b>-753</b>            | 51                     | 338                    | -86                        | -865                       |
| Max. pos. torsie  | SPLS 3_0,9_80 Ah All Cts   | 177                    | -329                   | -309                   | <b>358</b>             | 108                    | -66                        | -354                       |
| Max. neg. torsie  | SPLS 3_0,9_100 Ba All Cts  | -167                   | -307                   | -298                   | <b>-335</b>            | 99                     | -69                        | -342                       |
| Comb. trek+torsie | SPLS 1a_0,9_225 Ah All Cts | -38                    | -406                   | <b>-708</b>            | <b>260</b>             | 314                    | -85                        | -813                       |

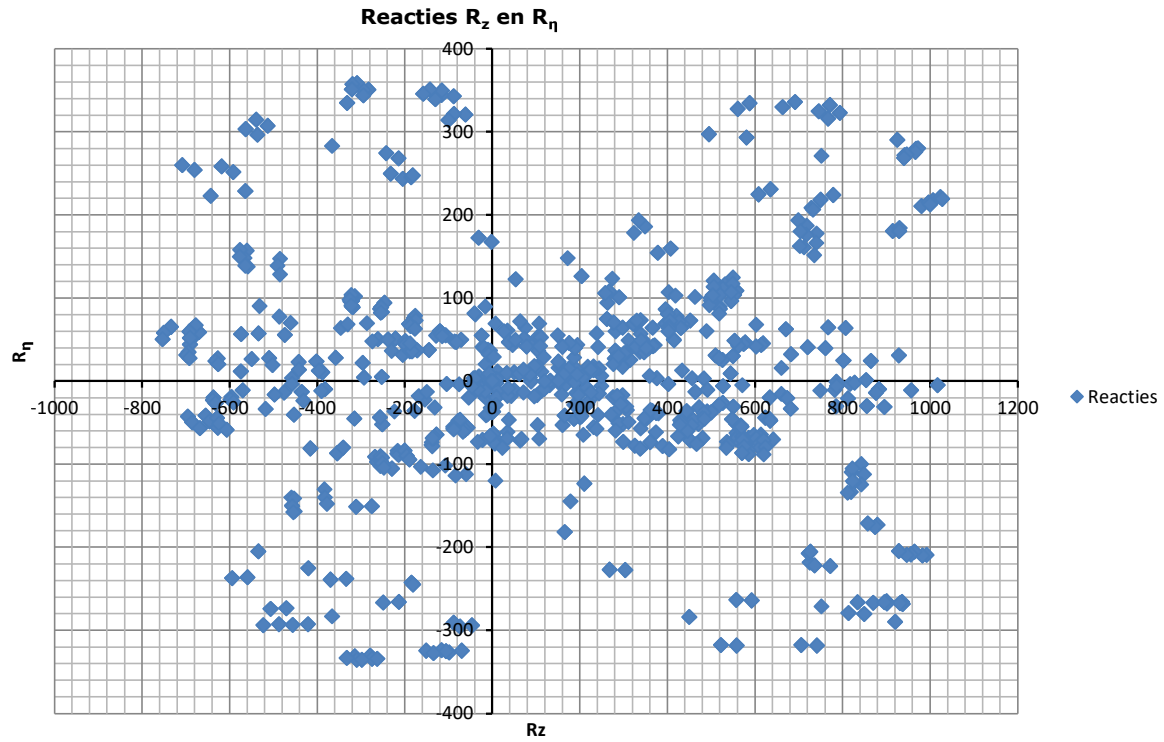
#### Maximale trekbelasting SLS

| Stijl | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_100 Ah All Cts  | 167                    | -329                   | <b>-321</b>            | 351                    | 115                    | -66                        | -368                       |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -275                   | 203                    | <b>-753</b>            | 51                     | 338                    | -86                        | -865                       |
| 3     | SPLS 1a_0,9_80 Ba Ct2      | 140                    | 11                     | <b>-268</b>            | -91                    | 107                    | -44                        | -308                       |
| 4     | SLS 1a_0                   | -67                    | -37                    | <b>-33</b>             | -73                    | -21                    | -40                        | -38                        |

#### Maximale drukbelasting SLS

| Stijl | Combinatie             | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_80 Ba Ct2      | 308                    | 154                    | <b>557</b>             | 109                    | -327                   | -13                        | 640                        |
| 2     | SLS 1a_0               | 87                     | -190                   | <b>330</b>             | 73                     | -196                   | -10                        | 379                        |
| 3     | SPLS 3_100 Ah All Cts  | -205                   | -272                   | <b>635</b>             | -48                    | -338                   | 20                         | 729                        |
| 4     | SPLS 1a_100 Ah All Cts | -231                   | 541                    | <b>1027</b>            | 219                    | -546                   | 34                         | 1179                       |

Project: GT-RL380  
Masttype: HA\_n (bouwfase)  
Mast: 18N



**Belastinggeval - afspannen**

Date: 2021-07-27  
Author: TBR  
Version: 1.1

RLL-TLB  
HA\_n

Invoergegevens
**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

| Circuits       | Aanduiding | Nummer   | Hoogteverschil |          | Richtingsverandering |          |
|----------------|------------|----------|----------------|----------|----------------------|----------|
|                |            |          | Dh_back        | Dh_ahead | Dy_back              | Dy_ahead |
| Circuit 1      | 10         | 380ct1f1 | -32,7          | 0,0 m    | 0,0                  | 0,0 m    |
| Circuit 1      | 11         | 380ct1f2 | -32,7          | 0,0 m    | 0,0                  | 0,0 m    |
| Circuit 1      | 12         | 380ct1f3 | -44,0          | 0,0 m    | 0,0                  | 0,0 m    |
| Bliksemdraad 1 | 1          | bl1      | -48,2          | 0,0 m    | 0,0                  | 0,0 m    |

**Lijn- en mastgegevens**

|                                       |          |  | Back  | Ahead   |
|---------------------------------------|----------|--|-------|---------|
| Ruling span $\sqrt{(SL3/SL)}$         |          |  | 66,0  | 400,0 m |
| Lijnhoek                              | $\beta$  |  | 180 ° |         |
| Rotatie mast t.o.v. bissectrice       | $\theta$ |  | 10 °  |         |
| Vaklengte                             |          |  | 66    | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld |          |  | 0,5 m |         |
| Beschouwde windrichtingen             | a1       |  | 0 °   |         |
| Windrichtingen volgens:               | a2       |  | 45 °  |         |
| <i>Geleiderbelastingen</i>            | a3       |  | 90 °  |         |
|                                       | a4       |  | 135 ° |         |
|                                       | a5       |  | 80 °  |         |
|                                       | a6       |  | 80 °  |         |

*Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.*

In onderstaande tabel zijn de optredende belastingen weergegeven, voor deze situatie geldt:

- belasting op geleider 1 en 10 t/m 12 zijn permanent aanwezig
- van de belasting op de overige geleiders is er telkens één aanwezig per belastingcombinatie

Uitvoer geleiderbelastingen

| Belastingcombi   | nummer | Fxtotaal     | Fytotaal     | Fztotaal    | Ftrekahead | Ftrekback |
|------------------|--------|--------------|--------------|-------------|------------|-----------|
| <b>ULS 6b_90</b> | 13     | <b>-83,5</b> | <b>15,8</b>  | <b>57,6</b> | 0,0        | -85,0     |
|                  | 10     | <b>88,8</b>  | <b>-12,4</b> | <b>19,3</b> | 89,6       | 0,0       |
|                  | 14     | <b>-83,5</b> | <b>15,8</b>  | <b>57,6</b> | 0,0        | -85,0     |
|                  | 11     | <b>88,8</b>  | <b>-12,4</b> | <b>19,3</b> | 89,6       | 0,0       |
|                  | 15     | <b>-83,6</b> | <b>15,8</b>  | <b>72,2</b> | 0,0        | -85,0     |
|                  | 12     | <b>89,5</b>  | <b>-12,2</b> | <b>19,3</b> | 90,2       | 0,0       |
|                  | 4      | <b>-17,4</b> | <b>3,3</b>   | <b>14,8</b> | 0,0        | -17,7     |
|                  | 1      | <b>19,2</b>  | <b>-2,4</b>  | <b>2,7</b>  | 19,4       | 0,0       |



Project: GT-RLL380  
 Tower: HA+5\_n  
 Number: 18N

Auteur: TBR  
 Versie: v12.0

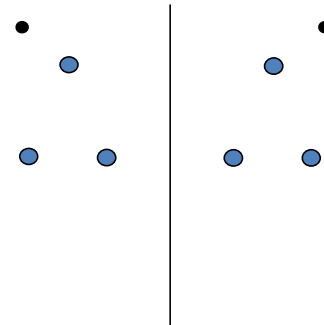
### Geleiderbelastingen

#### Algemeen

Benaming HA+5\_n  
 Masttype Hoekmast  
 Aantal circuits 2  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 2

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 50 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 50 jaar  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsg gebied fasegeleider B  
 IJsg gebied bliksemgeleider A



Configuratie geleiders

#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A           | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A           | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging     | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Circuit 2      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Bliksemdraad 1 | Afspanketting | 0,10         | 0,20       | 0,10                       |
| Bliksemdraad 2 | Afspanketting | 0,10         | 0,20       | 0,10                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 32,7 m       | 32,7 m       | -15,7 m                                |
| Circuit 1      | 11         | 380ct1f2 | 32,7 m       | 32,7 m       | -8,7 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 44,0 m       | 44,0 m       | -12,2 m                                |
| Circuit 2      | 20         | 380ct2f1 | 32,7 m       | 32,7 m       | 8,7 m                                  |
| Circuit 2      | 21         | 380ct2f2 | 32,7 m       | 32,7 m       | 15,7 m                                 |
| Circuit 2      | 22         | 380ct2f3 | 44,0 m       | 44,0 m       | 12,2 m                                 |
| Bliksemdraad 1 | 1          | bl1      | 48,2 m       | 48,2 m       | -18,4 m                                |
| Bliksemdraad 2 | 3          | bl2      | 48,2 m       | 48,2 m       | 18,4 m                                 |

Project: GT-RLL380  
 Tower: HA+5\_n  
 Number: 18N

**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead  |   |
|------------------------------------|---------------------------|--------|---|
| Verhoging voor windbelasting       | 32,0 m                    | 0,0 m  | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -5,0 m                    | -5,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |        |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

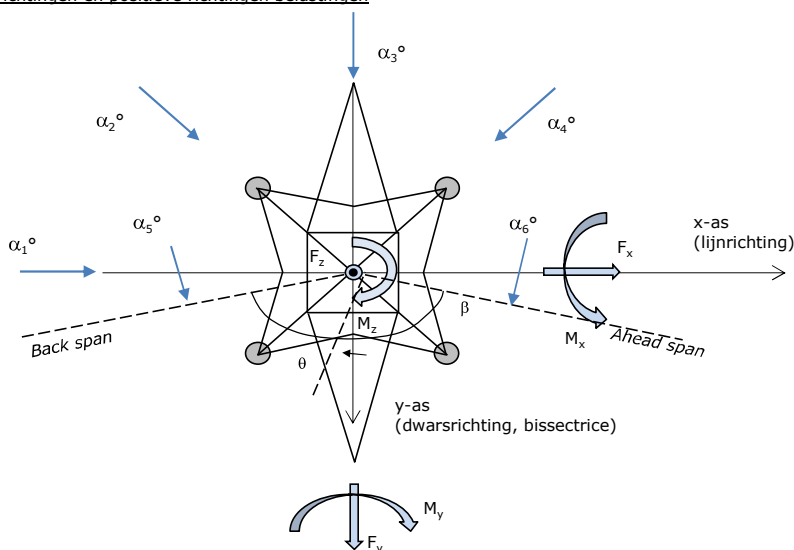
| Circuits       | Aanduiding | Nummer   | Hoogteverschil  |                  | Richtingsverandering |                  |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
|                |            |          | $\Delta h$ back | $\Delta h$ ahead | $\Delta y$ back      | $\Delta y$ ahead |
| Circuit 1      | 10         | 380ct1f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 11         | 380ct1f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 12         | 380ct1f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 20         | 380ct2f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 21         | 380ct2f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 22         | 380ct2f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 1 | 1          | bl1      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 2 | 3          | bl2      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek $\beta$                           | 160 °      |         |
| Rotatie mast t.o.v. bissectrice $\theta$   | 0 °        |         |
| Vaklengte                                  | 400        | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 45 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 135 °   |
|  | $\alpha_5$ | 80 °    |
|  | $\alpha_6$ | 100 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



Beschouwd aantal windrichtingen

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |



Project: GT-RLL380  
 Tower: HA+5\_n  
 Number: 18N

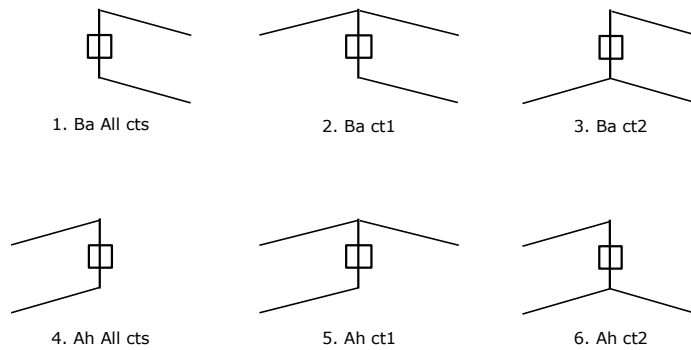
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | b2       | 0             | 1    | 1                        | 0    | 1                  | 0    |

### Belastingsituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

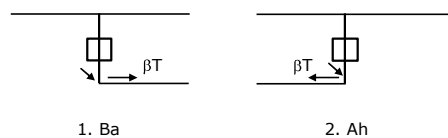
Principe belastingssituaties:



### Belastingsituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



Project: GT-RLL380  
 Tower: HA+5\_n  
 Number: 18N

### Belastingsituaties 6. Bouw- en onderhoud

Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht.

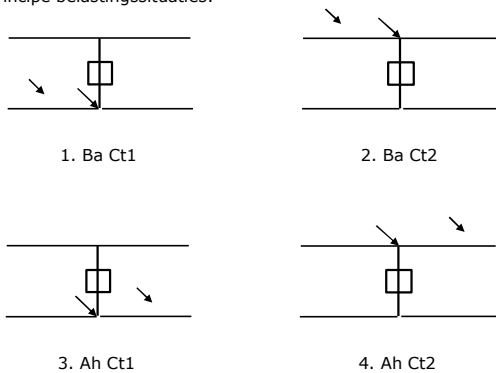
Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



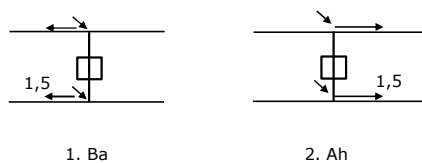
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingsspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

Project: GT-RLL380  
 Tower: HA+5\_n  
 Number: 18N

## Mastconstructie

### Eigenschappen

|   |          |         |
|---|----------|---------|
| Masttype                                    | Hoekmast |         |
| Mastbenaming                                | HA+5_n   |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m    |         |
| Masthoogte t.o.v. voetplaat                 | 50,0 m   |         |
| Gewicht mast                                | 492,0 kN |         |
| <i>Breedte en helling mast bij fundatie</i> |          |         |
|   | x-ri.    | y-ri.   |
| Pootsprei                                   | 11,94    | 11,94 m |
| Helling van de randstijl                    | 0,135    | 0,135 - |
| Factor spatkracht                           | 1,3      | 1,3 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,00 ( <i>Masthoogte &lt; 60 m</i> )  |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 12,25    | 11,94                 | 8,63                  | 12,25     | 0,135                 | 125,97                              | 18,34                               | 0,15                                      | 3,18           |
| Tussenstuk1   | 24,56    | 8,63                  | 5,68                  | 12,31     | 0,120                 | 88,08                               | 15,61                               | 0,18                                      | 3,03           |
| Tussenstuk2   | 32,70    | 5,68                  | 3,80                  | 8,14      | 0,116                 | 38,59                               | 12,57                               | 0,33                                      | 2,45           |
| Bovenstuk1    | 40,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 8,91                                | 0,34                                      | 2,40           |
| Bovenstuk2    | 48,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 5,97                                | 0,29                                      | 2,57           |
| Topstuk       | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse | 32,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,76                                | 0,24                                      | 2,77           |
| Boventraverse | 44,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 8,36                                | 0,23                                      | 2,78           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 12,25    | 11,94                 | 8,63                  | 12,25     | 0,135                 | 125,97                              | 18,34                               | 0,15                                      | 3,18           |
| Tussenstuk1   | 24,56    | 8,63                  | 5,68                  | 12,31     | 0,120                 | 88,08                               | 15,61                               | 0,18                                      | 3,03           |
| Tussenstuk2   | 32,70    | 5,68                  | 3,80                  | 8,14      | 0,116                 | 38,59                               | 12,57                               | 0,33                                      | 2,45           |
| Bovenstuk1    | 40,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 8,91                                | 0,34                                      | 2,40           |
| Bovenstuk2    | 48,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 5,97                                | 0,29                                      | 2,57           |
| Topstuk       | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse | 32,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,76                                | 0,24                                      | 2,77           |
| Boventraverse | 44,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 8,36                                | 0,23                                      | 2,78           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

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#### Windoppervlak feeders telecominstallaties

| Onderdeel   | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------|-----------------------|--------|------|----------------|
| Broekstuk   | 0,20                  | 0,71   | 12,3 | 1,7            |
| Tussenstuk1 | 0,20                  | 0,71   | 12,3 | 1,7            |
| Tussenstuk2 | 0,20                  | 0,71   | 8,1  | 1,2            |
| Bovenstuk1  | 0,20                  | 0,71   | 7,8  | 1,1            |
| Bovenstuk2  |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>i</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,6                 | 31,7  | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 40,9                    | 34,7                    | 0,0                     | -34,7                   | 6,1                    | 250,4                    | 212,5                    | 0,0                      | -212,5                   |
| Tussenstuk1   | 0,86                                   | 40,5                    | 34,4                    | 0,0                     | -34,4                   | 18,4                   | 745,3                    | 632,4                    | 0,0                      | -632,4                   |
| Tussenstuk2   | 0,98                                   | 30,0                    | 25,4                    | 0,0                     | -25,4                   | 28,6                   | 858,5                    | 728,5                    | 0,0                      | -728,5                   |
| Bovenstuk1    | 1,05                                   | 22,4                    | 19,0                    | 0,0                     | -19,0                   | 36,6                   | 819,9                    | 695,7                    | 0,0                      | -695,7                   |
| Bovenstuk2    | 1,10                                   | 16,9                    | 14,3                    | 0,0                     | -14,3                   | 44,3                   | 748,1                    | 634,8                    | 0,0                      | -634,8                   |
| Topstuk       | 1,13                                   | 1,4                     | 1,2                     | 0,0                     | -1,2                    | 49,0                   | 69,7                     | 59,1                     | 0,0                      | -59,1                    |
| Ondertraverse | 1,02                                   | 38,4                    | 22,8                    | 0,0                     | -22,8                   | 34,0                   | 1306,0                   | 775,7                    | 0,0                      | -775,7                   |
| Boventraverse | 1,11                                   | 51,5                    | 30,6                    | 0,0                     | -30,6                   | 45,4                   | 2337,9                   | 1388,6                   | 0,0                      | -1388,6                  |

|               |              |              |            |               |  |  |               |               |            |                |
|---------------|--------------|--------------|------------|---------------|--|--|---------------|---------------|------------|----------------|
| <b>Totaal</b> | <b>242,0</b> | <b>182,4</b> | <b>0,0</b> | <b>-182,4</b> |  |  | <b>7135,8</b> | <b>5127,3</b> | <b>0,0</b> | <b>-5127,3</b> |
|---------------|--------------|--------------|------------|---------------|--|--|---------------|---------------|------------|----------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 0,0                     | 34,7                    | 40,9                    | 34,7                    | 6,1                    | 0,0                      | 212,5                    | 250,4                    | 212,5                    |
| Tussenstuk1   | 0,86                                   | 0,0                     | 34,4                    | 40,5                    | 34,4                    | 18,4                   | 0,0                      | 632,4                    | 745,3                    | 632,4                    |
| Tussenstuk2   | 0,98                                   | 0,0                     | 25,4                    | 30,0                    | 25,4                    | 28,6                   | 0,0                      | 728,5                    | 858,5                    | 728,5                    |
| Bovenstuk1    | 1,05                                   | 0,0                     | 19,0                    | 22,4                    | 19,0                    | 36,6                   | 0,0                      | 695,7                    | 819,9                    | 695,7                    |
| Bovenstuk2    | 1,10                                   | 0,0                     | 14,3                    | 16,9                    | 14,3                    | 44,3                   | 0,0                      | 634,8                    | 748,1                    | 634,8                    |
| Topstuk       | 1,13                                   | 0,0                     | 1,2                     | 1,4                     | 1,2                     | 49,0                   | 0,0                      | 59,1                     | 69,7                     | 59,1                     |
| Ondertraverse | 1,02                                   | 0,0                     | 22,8                    | 15,3                    | 22,8                    | 34,0                   | 0,0                      | 775,7                    | 522,4                    | 775,7                    |
| Boventraverse | 1,11                                   | 0,0                     | 30,6                    | 20,6                    | 30,6                    | 45,4                   | 0,0                      | 1388,6                   | 935,1                    | 1388,6                   |

|               |            |              |              |              |  |  |            |               |               |               |
|---------------|------------|--------------|--------------|--------------|--|--|------------|---------------|---------------|---------------|
| <b>Totaal</b> | <b>0,0</b> | <b>182,4</b> | <b>188,0</b> | <b>182,4</b> |  |  | <b>0,0</b> | <b>5127,3</b> | <b>4949,5</b> | <b>5127,3</b> |
|---------------|------------|--------------|--------------|--------------|--|--|------------|---------------|---------------|---------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting     | 0                      | 0                      | 492                    | 0                       | 0                       | 0                       |
| Windrichting 0°          | 249                    | 0                      | 0                      | 0                       | 7355                    | 0                       |
| Windrichting 45°         | 187                    | 187                    | 0                      | 5283                    | 5283                    | 0                       |
| Windrichting 90°         | 0                      | 195                    | 0                      | 5169                    | 0                       | 0                       |
| Windrichting 135°        | -187                   | 187                    | 0                      | 5283                    | -5283                   | 0                       |

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### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| 380ct2f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct2f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct2f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 48,70             | 1,13                             | 1,2               | 0,14                |
| bl2      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 48,70             | 1,13                             | 1,2               | 0,14                |

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#### Windbelasting back

| Geleider | hoogte      |                                  | $G_{c,dwars}$ | $G_{c,trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|-------------|----------------------------------|---------------|--------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] |               |              |       |               |       |             |                   |             |                 |
| 380ct1f1 | 40,9        | 1,08                             | 0,60          | 0,66         | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct1f2 | 40,9        | 1,08                             | 0,60          | 0,66         | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct1f3 | 52,2        | 1,15                             | 0,62          | 0,68         | 1,06  | 28,25         | 63,8  | 70,1        | 46,9              | 120,4       | 132,3           |
| 380ct2f1 | 40,9        | 1,08                             | 0,60          | 0,66         | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct2f2 | 40,9        | 1,08                             | 0,60          | 0,66         | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct2f3 | 52,2        | 1,15                             | 0,62          | 0,68         | 1,06  | 28,25         | 63,8  | 70,1        | 46,9              | 120,4       | 132,3           |
| bl1      | 56,4        | 1,17                             | 0,63          | 0,69         | 1,18  | 22,24         | 19,2  | 21,1        | 63,1              | 55,6        | 61,1            |
| bl2      | 56,4        | 1,17                             | 0,63          | 0,69         | 1,18  | 22,13         | 19,2  | 21,1        | 63,0              | 55,5        | 61,0            |

#### Windbelasting ahead

| Geleider | hoogte      |                                  | $G_{c,dwars}$ | $G_{c,trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|-------------|----------------------------------|---------------|--------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] |               |              |       |               |       |             |                   |             |                 |
| 380ct1f1 | 24,9        | 0,94                             | 0,56          | 0,62         | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct1f2 | 24,9        | 0,94                             | 0,56          | 0,62         | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct1f3 | 36,2        | 1,04                             | 0,59          | 0,65         | 1,08  | 28,25         | 56,7  | 62,4        | 46,9              | 104,2       | 114,6           |
| 380ct2f1 | 24,9        | 0,94                             | 0,56          | 0,62         | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct2f2 | 24,9        | 0,94                             | 0,56          | 0,62         | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct2f3 | 36,2        | 1,04                             | 0,59          | 0,65         | 1,08  | 28,25         | 56,7  | 62,4        | 46,9              | 104,2       | 114,6           |
| bl1      | 40,4        | 1,07                             | 0,60          | 0,66         | 1,20  | 22,24         | 17,2  | 18,9        | 63,1              | 48,8        | 53,7            |
| bl2      | 40,4        | 1,07                             | 0,60          | 0,66         | 1,20  | 22,13         | 17,1  | 18,8        | 63,0              | 48,8        | 53,6            |

NB: belastingen  $w_v$  gelden voor bundel

Project: GT-RL380  
 Masttype: HA+5\_n  
 Mast: 18N

Auteur: TBR  
 Versie: v12.0

### Geleiderbelastingen

**Uitgangspunten**  
 Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 50 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |              |                     |  |          |          |                     |  |
|--|---------------------------|------------------------------|--------------|---------------------|--|----------|----------|---------------------|--|
| Belastingsgeval  | omschrijving              | Temp<br>°C                   | $\gamma_G$   |                     | $\gamma_Q$                               |          |          | $\gamma_a$<br>$A_k$ |  |
|  |                           |                              | $G_{k,mast}$ | $G_{k,geleider}$    | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ |                     |  |
| ULS 1a   | Wind                      | 10°                          | 1,20         | 1,20                | 0,00                                     | 1,50     | 0,00     | 0,0                 |  |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90         | 1,20                | 0,00                                     | 1,50     | 0,00     | 0,0                 |  |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90         | 0,90                | 0,00                                     | 1,50     | 0,00     | 0,0                 |  |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20         | 1,20                | 0,00                                     | 0,45     | 1,50     | 0,0                 |  |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20                | 0,00                                     | 0,45     | 1,50     | 0,0                 |  |
| ULS 4  | Koude+wind                | -20°                         | 1,20         | 1,20                | 0,00                                     | 0,30     | 0,00     | 0,0                 |  |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90         | 1,20                | 0,00                                     | 0,30     | 0,00     | 0,0                 |  |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00         | 1,00                | 1,00                                     | 0,00     | 0,00     | 1,0                 |  |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |  |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 1,50                                     | 0,30     | 0,00     | 0,0                 |  |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 0,00                                     | 0,30     | 0,00     | 0,0                 |  |
| ULS 7  | Permanent                 | 10°                          | 1,35         | 1,35                | 0,00                                     | 0,00     | 0,00     | 0,0                 |  |
| ULS 8  | Special                   | 10°                          | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |  |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              |              | $\gamma_G$<br>$G_k$ | $\gamma_Q$<br>$Q_{pk}$ $Q_{wk}$ $Q_{ik}$ |          |          | $A_k$               |  |
| SPLS 1a  | Wind                      | 10°                          | 1,20         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90         | 0,90                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |  |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |  |
| SPLS 4   | Koude+wind                | -20°                         | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |  |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |  |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 1,2                                      | 0,24     | 0,0      | 0,0                 |  |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,0      | 0,0                 |  |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              |              | $G_k$               | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |  |
| SLS 1a   | Wind                      | 10°                          | 1,00         | 1,00                | 0,0                                      | 1,00     | 0,0      | 0,0                 |  |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00         | 1,00                | 0,0                                      | 0,30     | 1,00     | 0,0                 |  |
| SLS 4  | Wind                      | -20°                         | 1,00         | 1,00                | 0,0                                      | 0,20     | 0,0      | 0,0                 |  |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00         | 1,00                | 0,0                                      | 0,20     | 0,0      | 0,0                 |  |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00         | 1,00                | 0,0                                      | 0,00     | 0,0      | 0,0                 |  |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 72  
 Aantal belastingcombinaties SPLS 222  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 4944

Project: GT-RLL380  
 Masttype: HA+5\_n  
 Mast: 18N

### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -62,4         | 61,1          | 16,1          | 15,3          | 10,3          | 10,3          |
| bl2      | -61,6         | 60,3          | 16,0          | 15,2          | 10,3          | 10,2          |
| 380ct1f1 | -158,3        | 153,4         | 48,3          | 42,9          | 28,8          | 28,8          |
| 380ct1f2 | -158,3        | 153,4         | 48,3          | 42,9          | 28,8          | 28,8          |
| 380ct1f3 | -161,3        | 157,0         | 51,1          | 46,9          | 28,9          | 28,8          |
| 380ct2f1 | -158,3        | 153,4         | 48,3          | 42,9          | 28,8          | 28,8          |
| 380ct2f2 | -158,3        | 153,4         | 48,3          | 42,9          | 28,8          | 28,8          |
| 380ct2f3 | -161,3        | 157,0         | 51,1          | 46,9          | 28,9          | 28,8          |

#### Min. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 440,1  | 447,4 | 440,0 |
| bl2      | 440,1  | 447,6 | 440,0 |
| 380ct1f1 | 440,0  | 445,6 | 440,0 |
| 380ct1f2 | 440,0  | 445,6 | 440,0 |
| 380ct1f3 | 440,0  | 445,8 | 440,0 |
| 380ct2f1 | 440,0  | 445,6 | 440,0 |
| 380ct2f2 | 440,0  | 445,6 | 440,0 |
| 380ct2f3 | 440,0  | 445,8 | 440,0 |

#### Max. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 489,1  | 433,6 |
| bl2      | 490,4  | 433,4 |
| 380ct1f1 | 466,7  | 440,7 |
| 380ct1f2 | 466,7  | 440,7 |
| 380ct1f3 | 470,9  | 441,5 |
| 380ct2f1 | 466,7  | 440,7 |
| 380ct2f2 | 466,7  | 440,7 |
| 380ct2f3 | 470,9  | 441,5 |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

| Voor alle geleiders | Wind / Weight span verhouding |
|---------------------|-------------------------------|
| Max. weight span    | 490,4 m / 1,226 -             |
| Min. weight span    | -1,5 m / -0,004 -             |



Project: GT-RLL380  
 Masttype: HA+5\_n  
 Mast: 18N

**Maximale waarden back+ahead span      Maximale waarden trekkracht geleider**

| Geleider | Maximale waarden back+ahead span |            |            | Maximale waarden trekkracht geleider |               |
|----------|----------------------------------|------------|------------|--------------------------------------|---------------|
|          | Fx<br>[kN]                       | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN]                        | Ft_ah<br>[kN] |
| bl1      | 36,0                             | 31,1       | 10,3       | -64,3                                | 62,9          |
| bl2      | 35,5                             | 30,8       | 10,3       | -63,4                                | 62,0          |
| 380ct1f1 | 118,5                            | 89,1       | 28,8       | -162,7                               | 157,4         |
| 380ct1f2 | 118,5                            | 89,1       | 28,8       | -162,7                               | 157,4         |
| 380ct1f3 | 121,2                            | 95,7       | 28,9       | -165,9                               | 161,3         |
| 380ct2f1 | 118,5                            | 89,1       | 28,8       | -162,7                               | 157,4         |
| 380ct2f2 | 118,5                            | 89,1       | 28,8       | -162,7                               | 157,4         |
| 380ct2f3 | 121,2                            | 95,7       | 28,9       | -165,9                               | 161,3         |

**EDS-belastingen geleiders**

| Geleider | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|----------|------|------|------|-------|-------|
|          | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1      | 15,1 | 2,7  | 2,2  | -15,3 | 15,3  |
| bl2      | 14,7 | 2,6  | 2,1  | -14,9 | 14,9  |
| 380ct1f1 | 72,2 | 12,7 | 16,1 | -73,3 | 73,3  |
| 380ct1f2 | 72,2 | 12,7 | 16,1 | -73,3 | 73,3  |
| 380ct1f3 | 72,2 | 12,7 | 16,1 | -73,3 | 73,3  |
| 380ct2f1 | 72,2 | 12,7 | 16,1 | -73,3 | 73,3  |
| 380ct2f2 | 72,2 | 12,7 | 16,1 | -73,3 | 73,3  |
| 380ct2f3 | 72,2 | 12,7 | 16,1 | -73,3 | 73,3  |

**Controle uplift SLS-wind**

| Combinati | Geleider | Fz_ba | Fz_ah |
|-----------|----------|-------|-------|
|           |          | [kN]  | [kN]  |
| SLS 4     | bl1      | 0,0   | 0,0   |
|           | bl2      | 0,0   | 0,0   |
|           | 380ct1f1 | 0,0   | 0,0   |
|           | 380ct1f2 | 0,0   | 0,0   |
|           | 380ct1f3 | 0,0   | 0,0   |
|           | 380ct2f1 | 0,0   | 0,0   |
|           | 380ct2f2 | 0,0   | 0,0   |
|           | 380ct2f3 | 0,0   | 0,0   |

Project: GT-RLL380  
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 Mast: 18N

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -84           | 598           | 252           | 22476          | -3073          | 0              |
| ULS 1a_0,9_0      |             | 1             | 192           | 184           | 7158           | 46             | 0              |
| ULS 1a_0,9_0,9_90 |             | -91           | 581           | 93            | 21866          | -3323          | 0              |
| ULS 3_0           |             | 1             | 344           | 384           | 13021          | 28             | 0              |
| SLS 7             |             | 0             | 163           | 202           | 6076           | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

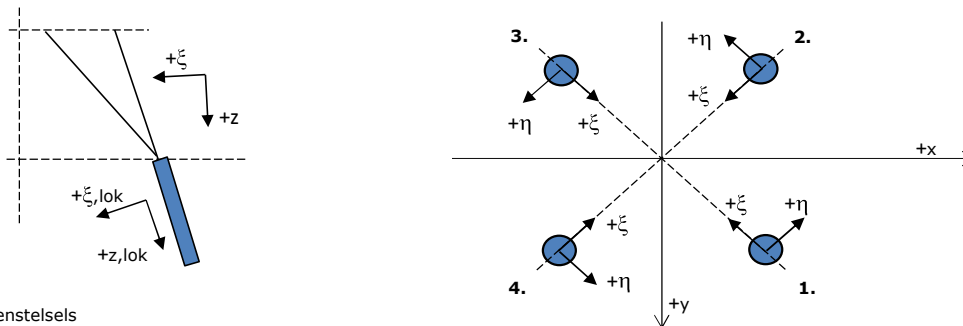
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -84           | 890           | 843           | 30230          | -3073          | 0              |
| ULS 1a_0,9_0,9_90 | -91           | 873           | 535           | 29620          | -3323          | 0              |
| SLS 7             | 0             | 163           | 694           | 6076           | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie                | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_90             | -84           | 890           | 589           | <b>30231</b>   | -3073          | 0              |
| SPLS 3_90 Ah All Cts      | -779          | 247           | 770           | 8483           | <b>-29292</b>  | 8              |
| SPLS 3_80 Ba Ct1          | 352           | 317           | 816           | 11712          | 13048          | <b>-5022</b>   |
| SPLS 1a_0,9_90 Ah All Cts | -704          | 361           | 542           | <b>11839</b>   | <b>-26354</b>  | 7              |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie            | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|-----------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 1a_90 Ba All Cts | 283           | 304           | <b>1709</b>   | -15              | -415            | -88                   | 1740                |
| 2     | SPLS 3_0 Ba All Cts   | 189           | -204          | <b>1147</b>   | 11               | -278            | -59                   | 1167                |
| 3     | SPLS 3_90 Ah All Cts  | -166          | -187          | <b>1064</b>   | -15              | -250            | -47                   | 1083                |
| 4     | SPLS 1a_90 Ah All Cts | -296          | 317           | <b>1789</b>   | 15               | -434            | -92                   | 1821                |

**Maximale trekbelasting**

| Stijl | Combinatie                | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_90 Ah All Cts  | -108          | -130          | <b>-734</b>   | 15               | 168             | 28                    | -748                |
| 2     | SPLS 1a_0,9_90 Ah All Cts | -239          | 260           | <b>-1464</b>  | -15              | 353             | 73                    | -1491               |
| 3     | SPLS 1a_0,9_90 Ba All Cts | 224           | 244           | <b>-1370</b>  | 14               | 331             | 69                    | -1395               |
| 4     | SPLS 3_0,9_0 Ba All Cts   | 128           | -144          | <b>-801</b>   | -11              | 192             | 39                    | -816                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ba Ct1 | 108           | -112          | -26           | <b>156</b>       | 2               | -3                    | -26                 |
| 2     | SPLS 3_0,9_80 Ba Ct2     | -71           | -149          | 240           | <b>155</b>       | -55             | -9                    | 244                 |
| 3     | SPLS 3_80 Ba Ct2         | 24            | 244           | -783          | <b>155</b>       | 190             | 40                    | -797                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -98           | 309           | 1200          | <b>150</b>       | -288            | -59                   | 1222                |

**Maximale torsiebelasting (negatief)**

| Stijl<br>Index | Combinatie<br>Combination | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|----------------|---------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1              | SPLS 3_0,9_80 Ba Ct1      | 93            | 308           | 1173          | <b>-152</b>      | -283            | -59                   | 1194                |
| 2              | SPLS 6a_90 Ah Ct2 Ba Ct2  | -21           | 236           | -762          | <b>-152</b>      | 182             | 36                    | -776                |
| 3              | SPLS 6a_90 Ah Ct2 Ba Ct2  | 32            | -184          | 461           | <b>-153</b>      | -108            | -20                   | 470                 |
| 4              | SPLS 3_80 Ba Ct1          | -139          | -86           | 148           | <b>-159</b>      | -38             | -9                    | 151                 |

Project: GT-RLL380  
 Masttype: HA+5\_n  
 Mast: 18N

#### Combinatie Ftrek+Fhor

| Stijl | Combinatie                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_90 Ah All Cts  | -108                   | -130                   | <b>-734</b>            | <b>15</b>              | 168                    | 28                         | -748                       |
| 2     | SPLS 1a_0,9_90 Ah All Cts | -239                   | 260                    | <b>-1464</b>           | <b>-15</b>             | 353                    | 73                         | -1491                      |
| 3     | SPLS 1a_0,9_90 Ba All Cts | 224                    | 244                    | <b>-1370</b>           | <b>14</b>              | 331                    | 69                         | -1395                      |
| 4     | SPLS 3_0,9_0 Ba All Cts   | 128                    | -144                   | <b>-801</b>            | <b>-11</b>             | 192                    | 39                         | -816                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 75                     | 71                     | 428                    | 3                      | -104                   | -22                        | 436                        |
| 2     | SLS 7      | -14                    | 10                     | -81                    | 3                      | 17                     | 2                          | -83                        |
| 3     | SLS 7      | 14                     | 10                     | -81                    | -3                     | 17                     | 2                          | -83                        |
| 4     | SLS 7      | -75                    | 71                     | 428                    | -3                     | -104                   | -22                        | 436                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | SPLS 1a_90 Ah All Cts     | -296                   | 317                    | <b>1789</b>            | 15                     | -434                   | -92                        | 1821                       |
| Max. trek         | SPLS 1a_0,9_90 Ah All Cts | -239                   | 260                    | <b>-1464</b>           | -15                    | 353                    | 73                         | -1491                      |
| Max. pos. torsie  | SPLS 6a_90 Ah Ct1 Ba Ct1  | 108                    | -112                   | -26                    | <b>156</b>             | 2                      | -3                         | -26                        |
| Max. neg. torsie  | SPLS 3_80 Ba Ct1          | -139                   | -86                    | 148                    | <b>-159</b>            | -38                    | -9                         | 151                        |
| Comb. trek+torsie | SPLS 1a_0,9_90 Ah All Cts | -239                   | 260                    | <b>-1464</b>           | <b>-15</b>             | 353                    | 73                         | -1491                      |

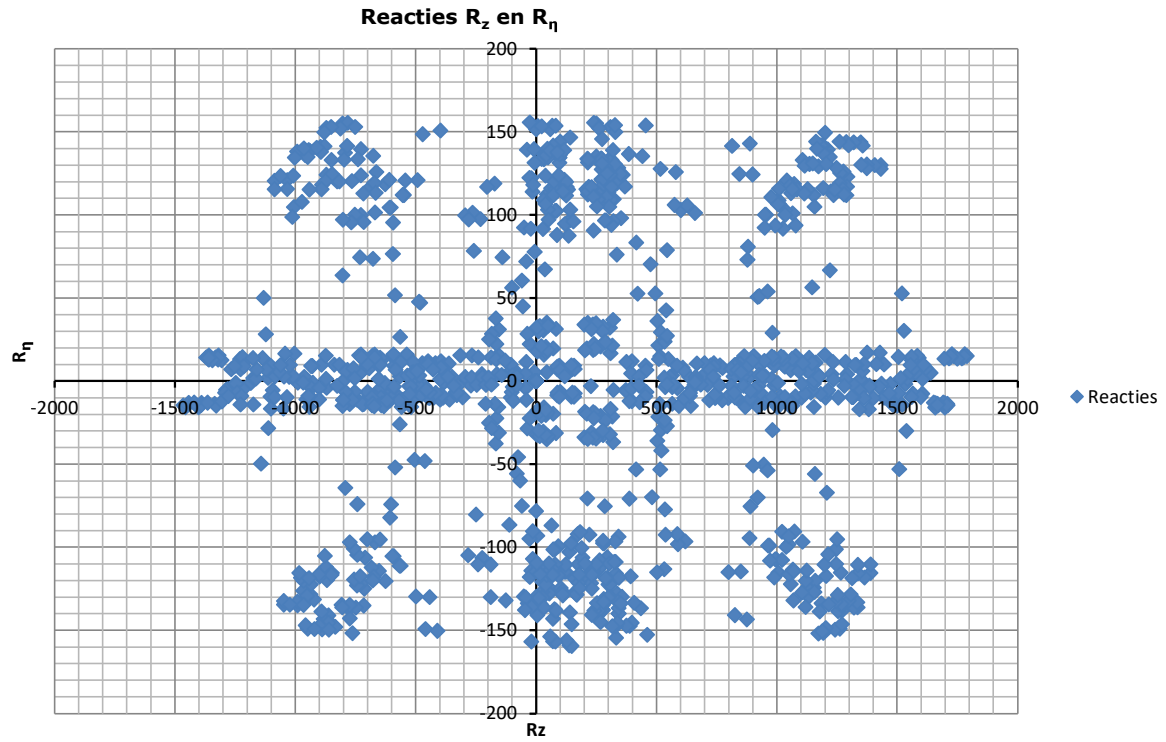
#### Maximale trekbelasting SLS

| Stijl | Combinatie                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_80 Ah All Cts  | -106                   | -129                   | <b>-727</b>            | 16                     | 166                    | 27                         | -740                       |
| 2     | SPLS 1a_0,9_80 Ah All Cts | -236                   | 258                    | <b>-1455</b>           | -16                    | 350                    | 72                         | -1482                      |
| 3     | SPLS 1a_0,9_100 Ba Ct2    | 68                     | 260                    | <b>-958</b>            | 136                    | 232                    | 49                         | -975                       |
| 4     | SPLS 3_0,9_100 Ba Ct2     | 82                     | 108                    | <b>50</b>              | 135                    | -19                    | -9                         | 51                         |

#### Maximale drukbelasting SLS

| Stijl | Combinatie            | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_100 Ba Ct2    | 307                    | 141                    | <b>1291</b>            | 117                    | -317                   | -70                        | 1315                       |
| 2     | SPLS 3_100 Ba Ct2     | -54                    | -158                   | <b>329</b>             | 150                    | -73                    | -10                        | 335                        |
| 3     | SPLS 3_80 Ah All Cts  | -164                   | -186                   | <b>1057</b>            | -16                    | -248                   | -46                        | 1076                       |
| 4     | SPLS 1a_80 Ah All Cts | -293                   | 316                    | <b>1780</b>            | 16                     | -430                   | -90                        | 1812                       |

Project: GT-RL380  
Masttype: HA+5\_n  
Mast: 18N





Project: GT-RLL380  
 Tower: HA\_n (bouwfase)  
 Number: 18N

Auteur: TBR  
 Versie: v12.0

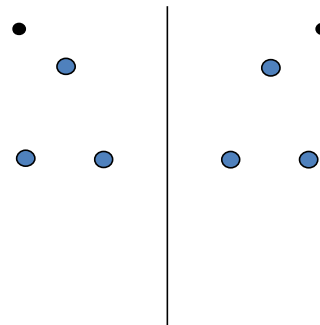
### Geleiderbelastingen

#### Algemeen

Benaming HA\_n (bouwfase)  
 Masttype Hoekmast  
 Aantal circuits 1  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 1

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 15 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsg gebied fasegeleider B  
 IJsg gebied bliksemgeleider A



Configuratie geleiders

#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging     | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Bliksemdraad 1 | Afspanketting | 0,10         | 0,20       | 0,10                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 32,7 m       | 32,7 m       | -15,7 m                                |
| Circuit 1      | 11         | 380ct1f2 | 32,7 m       | 32,7 m       | -8,7 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 44,0 m       | 44,0 m       | -12,2 m                                |
| Bliksemdraad 1 | 1          | bl1      | 48,2 m       | 48,2 m       | -18,4 m                                |

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**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead  |   |
|------------------------------------|---------------------------|--------|---|
| Verhoging voor windbelasting       | 32,0 m                    | 0,0 m  | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -5,0 m                    | -5,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |        |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

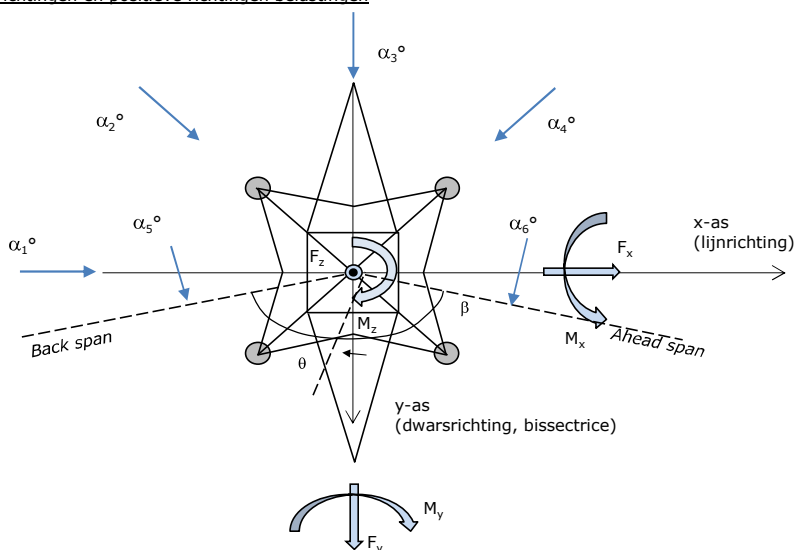
| Circuits       | Aanduiding | Nummer   | Hoogteverschil    |                    | Richtingsverandering |                    |       |
|----------------|------------|----------|-------------------|--------------------|----------------------|--------------------|-------|
|                |            |          | $\Delta h_{back}$ | $\Delta h_{ahead}$ | $\Delta y_{back}$    | $\Delta y_{ahead}$ |       |
| Circuit 1      | 10         | 380ct1f1 | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |
| Circuit 1      | 11         | 380ct1f2 | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |
| Circuit 1      | 12         | 380ct1f3 | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |
| Bliksemdraad 1 | 1          | bl1      | 0,0               | 0,0 m              | 0,0                  | 0,0                | 0,0 m |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek                                   | $\beta$    | 160 °   |
| Rotatie mast t.o.v. bissectrice            | $\theta$   | 0 °     |
| Vaklengte                                  | 400        | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 80 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 100 °   |
|  | $\alpha_5$ | 225 °   |
|  | $\alpha_6$ | 270 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



Beschouwd aantal windrichtingen

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

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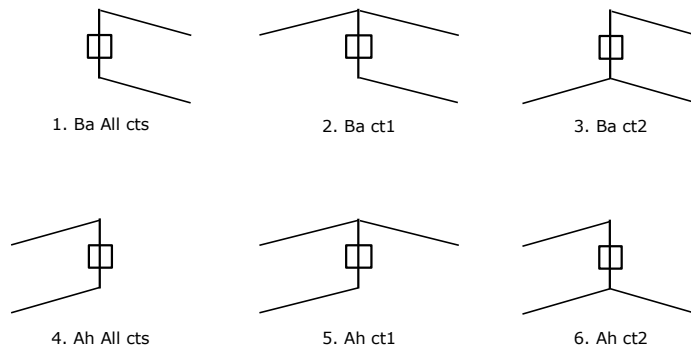
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |

### Belastingssituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

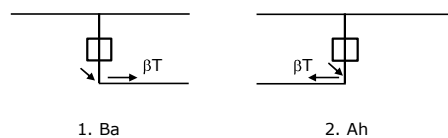
Principe belastingssituaties:



### Belastingssituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:





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### Belastingsituaties 6. Bouw- en onderhoud

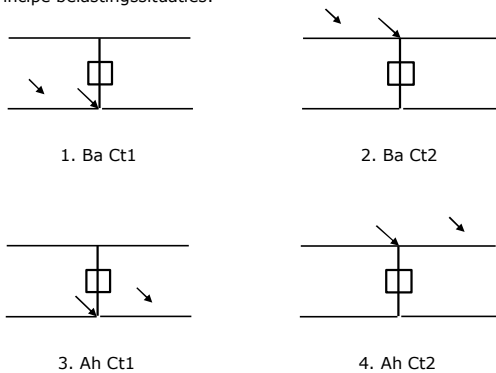
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



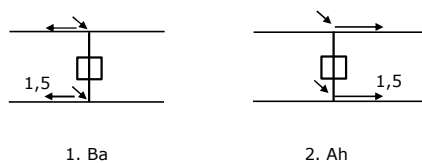
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

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## Mastconstructie

### Eigenschappen

|   |                 |         |
|---|-----------------|---------|
| Masttype                                    | Hoekmast        |         |
| Mastbenaming                                | HA_n (bouwfase) |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m           |         |
| Masthoogte t.o.v. voetplaat                 | 50,0 m          |         |
| Gewicht mast                                | 492,0 kN        |         |
| <i>Breedte en helling mast bij fundatie</i> |                 |         |
|   | x-ri.           | y-ri.   |
| Pootsprei                                   | 11,58           | 11,58 m |
| Helling van de randstijl                    | 0,399           | 0,399 - |
| Factor spatkracht                           | 1,3             | 1,3 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,00 (Masthoogte < 60 m)              |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 8,54     | 11,58                 | 4,77                  | 8,54      | 0,399                 | 69,81                               | 13,53                               | 0,19                                      | 2,96           |
| Tussenstuk1   | 19,03    | 4,77                  | 6,96                  | 10,49     | -0,104                | 61,52                               | 13,15                               | 0,21                                      | 2,87           |
| Tussenstuk2   | 32,70    | 6,96                  | 3,80                  | 13,67     | 0,116                 | 73,54                               | 16,36                               | 0,22                                      | 2,83           |
| Bovenstuk1    | 40,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 7,84                                | 0,30                                      | 2,54           |
| Bovenstuk2    | 48,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 4,92                                | 0,24                                      | 2,77           |
| Topstuk       | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,43                                | 0,17                                      | 3,09           |
| Ondertraverse | 32,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,40                                | 0,23                                      | 2,82           |
| Boventraverse | 44,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 7,96                                | 0,22                                      | 2,83           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving  | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|---------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk     | 8,54     | 11,58                 | 4,77                  | 8,54      | 0,399                 | 69,81                               | 13,53                               | 0,19                                      | 2,96           |
| Tussenstuk1   | 19,03    | 4,77                  | 6,96                  | 10,49     | -0,104                | 61,52                               | 13,15                               | 0,21                                      | 2,87           |
| Tussenstuk2   | 32,70    | 6,96                  | 3,80                  | 13,67     | 0,116                 | 73,54                               | 16,36                               | 0,22                                      | 2,83           |
| Bovenstuk1    | 40,50    | 3,80                  | 2,91                  | 7,80      | 0,057                 | 26,18                               | 7,84                                | 0,30                                      | 2,54           |
| Bovenstuk2    | 48,00    | 2,91                  | 2,60                  | 7,50      | 0,021                 | 20,68                               | 4,92                                | 0,24                                      | 2,77           |
| Topstuk       | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,43                                | 0,17                                      | 3,09           |
| Ondertraverse | 32,70    | 14,20                 |                       | 4,00      |                       | 28,40                               | 6,40                                | 0,23                                      | 2,82           |
| Boventraverse | 44,00    | 16,94                 |                       | 4,20      |                       | 35,57                               | 7,96                                | 0,22                                      | 2,83           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

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#### Windoppervlak feeders telecominstallaties

| Onderdeel   | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------|-----------------------|--------|------|----------------|
| Broekstuk   | 0,20                  | 0,71   | 8,5  | 1,2            |
| Tussenstuk1 | 0,20                  | 0,71   | 10,5 | 1,5            |
| Tussenstuk2 | 0,20                  | 0,71   | 13,7 | 1,9            |
| Bovenstuk1  | 0,20                  | 0,71   | 7,8  | 1,1            |
| Bovenstuk2  |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>r</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,6                 | 31,7  | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 28,1                    | 5,0                     | 0,0                     | -5,0                    | 4,3                    | 119,8                    | 21,3                     | 0,0                      | -21,3                    |
| Tussenstuk1   | 0,78                                   | 29,5                    | 5,2                     | 0,0                     | -5,2                    | 13,8                   | 406,5                    | 72,2                     | 0,0                      | -72,2                    |
| Tussenstuk2   | 0,95                                   | 43,9                    | 7,8                     | 0,0                     | -7,8                    | 25,9                   | 1136,4                   | 201,9                    | 0,0                      | -201,9                   |
| Bovenstuk1    | 1,05                                   | 20,9                    | 3,7                     | 0,0                     | -3,7                    | 36,6                   | 763,2                    | 135,6                    | 0,0                      | -135,6                   |
| Bovenstuk2    | 1,10                                   | 15,0                    | 2,7                     | 0,0                     | -2,7                    | 44,3                   | 663,6                    | 117,9                    | 0,0                      | -117,9                   |
| Topstuk       | 1,13                                   | 1,5                     | 0,3                     | 0,0                     | -0,3                    | 49,0                   | 73,3                     | 13,0                     | 0,0                      | -13,0                    |
| Ondertraverse | 1,02                                   | 37,0                    | 2,7                     | 0,0                     | -2,7                    | 34,0                   | 1259,1                   | 93,6                     | 0,0                      | -93,6                    |
| Boventraverse | 1,11                                   | 49,9                    | 3,7                     | 0,0                     | -3,7                    | 45,4                   | 2264,4                   | 168,2                    | 0,0                      | -168,2                   |

|               |              |             |            |              |  |  |               |              |            |               |
|---------------|--------------|-------------|------------|--------------|--|--|---------------|--------------|------------|---------------|
| <b>Totaal</b> | <b>225,7</b> | <b>31,1</b> | <b>0,0</b> | <b>-31,1</b> |  |  | <b>6686,3</b> | <b>823,9</b> | <b>0,0</b> | <b>-823,9</b> |
|---------------|--------------|-------------|------------|--------------|--|--|---------------|--------------|------------|---------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving  | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|---------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk     | 0,70                                   | 0,0                     | 28,3                    | 28,1                    | 28,3                    | 4,3                    | 0,0                      | 120,8                    | 119,8                    | 120,8                    |
| Tussenstuk1   | 0,78                                   | 0,0                     | 29,7                    | 29,5                    | 29,7                    | 13,8                   | 0,0                      | 409,7                    | 406,5                    | 409,7                    |
| Tussenstuk2   | 0,95                                   | 0,0                     | 44,3                    | 43,9                    | 44,3                    | 25,9                   | 0,0                      | 1145,3                   | 1136,4                   | 1145,3                   |
| Bovenstuk1    | 1,05                                   | 0,0                     | 21,0                    | 20,9                    | 21,0                    | 36,6                   | 0,0                      | 769,2                    | 763,2                    | 769,2                    |
| Bovenstuk2    | 1,10                                   | 0,0                     | 15,1                    | 15,0                    | 15,1                    | 44,3                   | 0,0                      | 668,9                    | 663,6                    | 668,9                    |
| Topstuk       | 1,13                                   | 0,0                     | 1,5                     | 1,5                     | 1,5                     | 49,0                   | 0,0                      | 73,9                     | 73,3                     | 73,9                     |
| Ondertraverse | 1,02                                   | 0,0                     | 15,6                    | 14,8                    | 15,6                    | 34,0                   | 0,0                      | 530,5                    | 503,6                    | 530,5                    |
| Boventraverse | 1,11                                   | 0,0                     | 21,0                    | 20,0                    | 21,0                    | 45,4                   | 0,0                      | 954,1                    | 905,8                    | 954,1                    |

|               |            |              |              |              |  |  |            |               |               |               |
|---------------|------------|--------------|--------------|--------------|--|--|------------|---------------|---------------|---------------|
| <b>Totaal</b> | <b>0,0</b> | <b>176,5</b> | <b>173,6</b> | <b>176,5</b> |  |  | <b>0,0</b> | <b>4672,4</b> | <b>4572,3</b> | <b>4672,4</b> |
|---------------|------------|--------------|--------------|--------------|--|--|------------|---------------|---------------|---------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting     | 0                      | 0                      | 492                    | 0                       | 0                       | 0                       |
| Windrichting 0°          | 233                    | 0                      | 0                      | 0                       | 6906                    | 0                       |
| Windrichting 80°         | 32                     | 183                    | 0                      | 4889                    | 862                     | 0                       |
| Windrichting 90°         | 0                      | 181                    | 0                      | 4792                    | 0                       | 0                       |
| Windrichting 100°        | -32                    | 183                    | 0                      | 4889                    | -862                    | 0                       |

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### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $w_{z,G}$<br>[N/m] | IJsgebied | Formule | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $w_{z,G}$<br>[N/m] | IJsgebied | Formule | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 48,70             | 1,13                             | 1,2               | 0,14                |

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 Number: 18N

**Windbelasting back**

| Geleider | hoogte      |                                  | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $W_y$ | $W_{y,vak}$ | $D_{ijs,toeslag}$ | $W_{y,ijs}$ | $W_{y,ijs,vak}$ |
|----------|-------------|----------------------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] |                |               |       |               |       |             |                   |             |                 |
| 380ct1f1 | 40,9        | 1,08                             | 0,60           | 0,66          | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct1f2 | 40,9        | 1,08                             | 0,60           | 0,66          | 1,08  | 28,25         | 59,0  | 64,9        | 46,9              | 109,4       | 120,4           |
| 380ct1f3 | 52,2        | 1,15                             | 0,62           | 0,68          | 1,06  | 28,25         | 63,8  | 70,1        | 46,9              | 120,4       | 132,3           |
| bl1      | 56,4        | 1,17                             | 0,63           | 0,69          | 1,18  | 22,24         | 19,2  | 21,1        | 63,1              | 55,6        | 61,1            |

**Windbelasting ahead**

| Geleider | hoogte      |                                  | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $W_y$ | $W_{y,vak}$ | $D_{ijs,toeslag}$ | $W_{y,ijs}$ | $W_{y,ijs,vak}$ |
|----------|-------------|----------------------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] |                |               |       |               |       |             |                   |             |                 |
| 380ct1f1 | 24,9        | 0,94                             | 0,56           | 0,62          | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct1f2 | 24,9        | 0,94                             | 0,56           | 0,62          | 1,11  | 28,25         | 49,7  | 54,8        | 46,9              | 89,0        | 98,0            |
| 380ct1f3 | 36,2        | 1,04                             | 0,59           | 0,65          | 1,08  | 28,25         | 56,7  | 62,4        | 46,9              | 104,2       | 114,6           |
| bl1      | 40,4        | 1,07                             | 0,60           | 0,66          | 1,20  | 22,24         | 17,2  | 18,9        | 63,1              | 48,8        | 53,7            |

NB: belastingen  $w_v$  gelden voor bundel

Project: GT-RL380  
 Masttype: HA\_n (bouwfase)  
 Mast: 18N

Auteur: TBR  
 Versie: v12.0

**Geleiderbelastingen**

**Uitgangspunten**  
 Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 15 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |              |                     |  |          |          |                     |  |
|--|---------------------------|------------------------------|--------------|---------------------|--|----------|----------|---------------------|--|
| Belastingsgeval  | omschrijving              | Temp<br>°C                   | $\gamma_G$   |                     | $\gamma_Q$                               |          |          | $\gamma_a$<br>$A_k$ |  |
|  |                           |                              | $G_{k,mast}$ | $G_{k,geleider}$    | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ |                     |  |
| ULS 1a   | Wind                      | 10°                          | 1,20         | 1,20                | 0,00                                     | 1,25     | 0,00     | 0,0                 |  |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90         | 1,20                | 0,00                                     | 1,25     | 0,00     | 0,0                 |  |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90         | 0,90                | 0,00                                     | 1,25     | 0,00     | 0,0                 |  |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20         | 1,20                | 0,00                                     | 0,38     | 1,07     | 0,0                 |  |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20                | 0,00                                     | 0,38     | 1,07     | 0,0                 |  |
| ULS 4  | Koude+wind                | -20°                         | 1,20         | 1,20                | 0,00                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90         | 1,20                | 0,00                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00         | 1,00                | 1,00                                     | 0,00     | 0,00     | 1,0                 |  |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |  |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 1,50                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 0,00                                     | 0,25     | 0,00     | 0,0                 |  |
| ULS 7  | Permanent                 | 10°                          | 1,35         | 1,35                | 0,00                                     | 0,00     | 0,00     | 0,0                 |  |
| ULS 8  | Special                   | 10°                          | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |  |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              |              | $\gamma_G$<br>$G_k$ | $\gamma_Q$<br>$Q_{pk}$ $Q_{wk}$ $Q_{ik}$ |          |          | $A_k$               |  |
| SPLS 1a  | Wind                      | 10°                          | 1,20         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90         | 0,90                | 0,0                                      | 0,78     | 0,00     | 0,0                 |  |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |  |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |  |
| SPLS 4   | Koude+wind                | -20°                         | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |  |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |  |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 1,2                                      | 0,24     | 0,0      | 0,0                 |  |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,0      | 0,0                 |  |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              |              | $G_k$               | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |  |
| SLS 1a   | Wind                      | 10°                          | 1,00         | 1,00                | 0,0                                      | 0,87     | 0,0      | 0,0                 |  |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00         | 1,00                | 0,0                                      | 0,26     | 0,71     | 0,0                 |  |
| SLS 4  | Wind                      | -20°                         | 1,00         | 1,00                | 0,0                                      | 0,17     | 0,0      | 0,0                 |  |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00         | 1,00                | 0,0                                      | 0,17     | 0,0      | 0,0                 |  |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00         | 1,00                | 0,0                                      | 0,00     | 0,0      | 0,0                 |  |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 54  
 Aantal belastingcombinaties SPLS 210  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 2232

Project: GT-RLL380  
 Masttype: HA\_n (bouwfase)  
 Mast: 18N

### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -51,7         | 50,3          | 13,2          | 12,5          | 7,6           | 7,6           |
| 380ct1f1 | -143,3        | 138,9         | 42,1          | 37,6          | 27,3          | 27,3          |
| 380ct1f2 | -143,3        | 138,9         | 42,1          | 37,6          | 27,3          | 27,3          |
| 380ct1f3 | -145,9        | 142,1         | 44,4          | 40,9          | 27,3          | 27,3          |

#### Min. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 440,1  | 446,7 | 440,0 |
| 380ct1f1 | 440,0  | 445,3 | 440,0 |
| 380ct1f2 | 440,0  | 445,3 | 440,0 |
| 380ct1f3 | 440,0  | 445,5 | 440,0 |

#### Max. Weight span (m)

##### Weight sp: Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 479,0  | 437,2 |
| 380ct1f1 | 460,3  | 441,4 |
| 380ct1f2 | 460,3  | 441,4 |
| 380ct1f3 | 463,7  | 442,2 |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

| Voor alle geleiders | Wind / Weight span verhouding |
|---------------------|-------------------------------|
| Max. weight span    | 479,0 m<br>1,197 -            |
| Min. weight span    | 53,5 m<br>0,134 -             |

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| Geleider | Maximale waarden back+ahead span |            |            | Maximale waarden trekkracht geleider |               |
|----------|----------------------------------|------------|------------|--------------------------------------|---------------|
|          | Fx<br>[kN]                       | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN]                        | Ft_ah<br>[kN] |
| bl1      | 36,0                             | 25,4       | 7,6        | -52,2                                | 50,7          |
| 380ct1f1 | 118,9                            | 77,9       | 27,3       | -144,7                               | 140,3         |
| 380ct1f2 | 118,9                            | 77,9       | 27,3       | -144,7                               | 140,3         |
| 380ct1f3 | 122,0                            | 83,4       | 27,3       | -147,5                               | 143,5         |

| EDS-belastingen geleiders |            |            |            |               |               |
|---------------------------|------------|------------|------------|---------------|---------------|
| Geleider                  | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN] | Ft_ah<br>[kN] |
| bl1                       | 15,1       | 2,7        | 2,2        | -15,3         | 15,3          |
| 380ct1f1                  | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct1f2                  | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |
| 380ct1f3                  | 72,2       | 12,7       | 16,1       | -73,3         | 73,3          |

| Controle uplift SLS-wind |          |          |               |               |
|--------------------------|----------|----------|---------------|---------------|
| Combinati                |          | Geleider | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
| SLS 4                    | bl1      |          | 0,0           | 0,0           |
|                          | 380ct1f1 |          | 0,0           | 0,0           |
|                          | 380ct1f2 |          | 0,0           | 0,0           |
|                          | 380ct1f3 |          | 0,0           | 0,0           |



Project: GT-RLL380  
 Masttype: HA\_n (bouwfase)  
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**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -34           | 261           | 125           | 8246           | -1257          | 432            |
| ULS 1a_0,9_0      |             | 1             | 96            | 92            | 2438           | 20             | -7             |
| ULS 1a_0,9_0,9_90 |             | -38           | 251           | 51            | 8820           | -1391          | 479            |
| ULS 3_0           |             | 0             | 152           | 171           | 3556           | 11             | -4             |
| SLS 7             |             | 0             | 82            | 101           | 1784           | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

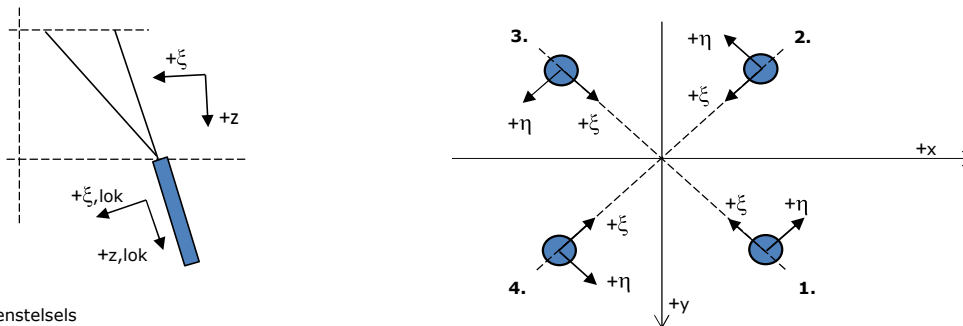
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -34           | 487           | 715           | 14250          | -1257          | 432            |
| ULS 1a_0,9_0,9_90 | -38           | 477           | 494           | 14824          | -1391          | 479            |
| SLS 7             | 0             | 82            | 593           | 1784           | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie                 | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|----------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_90              | -34           | 487           | 520           | <b>14858</b>   | -1257          | 432            |
| SPLS 1a_225 Ah All Cts     | -458          | -106          | 673           | -3774          | <b>-15883</b>  | 4076           |
| SPLS 3_270 Ah All Cts      | -396          | -15           | 680           | -953           | -14874         | <b>5050</b>    |
| SPLS 1a_0,9_100 Ah All Cts | -365          | 242           | 493           | <b>6901</b>    | <b>-13402</b>  | 4311           |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie             | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 1a_80 Ba All Cts  | 226           | 522           | <b>991</b>    | -209               | -528              | 31                    | 1138                |
| 2     | SPLS 1a_270 Ba All Cts | 356           | -312          | <b>896</b>    | -31                | -472              | 33                    | 1028                |
| 3     | SPLS 1a_225 Ah All Cts | -374          | -381          | <b>1017</b>   | -5                 | -534              | 39                    | 1168                |
| 4     | SPLS 1a_100 Ah All Cts | -231          | 541           | <b>1027</b>   | 219                | -546              | 34                    | 1179                |

**Maximale trekbelasting**

| Stijl | Combinatie                 | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|----------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 1a_0,9_225 Ah All Cts | -38           | -406          | <b>-708</b>   | 260                | 314               | -85                   | -813                |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -275          | 203           | <b>-753</b>   | 51                 | 338               | -86                   | -865                |
| 3     | SPLS 1a_0,9_80 Ba All Cts  | 250           | 189           | <b>-695</b>   | -43                | 310               | -82                   | -798                |
| 4     | SPLS 1a_0,9_270 Ba All Cts | 11            | -346          | <b>-595</b>   | -237               | 252               | -83                   | -683                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_80 Ah All Cts | 177           | -329          | -309          | <b>358</b>         | 108               | -66                   | -354                |
| 2     | ULS 1a_0,9_0,9_80        | -292          | 69            | -576          | <b>158</b>         | 255               | -70                   | -661                |
| 3     | ULS 1a_0                 | 27            | 126           | -286          | <b>70</b>          | 108               | -53                   | -329                |
| 4     | SPLS 1a_225 Ah All Cts   | -29           | 504           | 691           | <b>336</b>         | -377              | 13                    | 793                 |

**Maximale torsiebelasting (negatief)**

| Stijl | Combinatie                | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 3_270 Ba All Cts     | 56            | 507           | 741           | <b>-318</b>        | -398              | 20                    | 851                 |
| 2     | ULS 1a_225                | 115           | 55            | 8             | <b>-120</b>        | -42               | -38                   | 9                   |
| 3     | ULS 1a_0,9_0,9_100        | 251           | 28            | -455          | <b>-158</b>        | 197               | -60                   | -522                |
| 4     | SPLS 3_0,9_100 Ba All Cts | -167          | -307          | -298          | <b>-335</b>        | 99                | -69                   | -342                |

Project: GT-RLL380  
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#### Combinatie Ftrek+Fhor

| Stijl | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_0,9_225 Ah All Cts | -38                    | -406                   | <b>-708</b>            | <b>260</b>             | 314                    | -85                        | -813                       |
| 2     | ULS 1a_0,9_0,9_80          | -292                   | 69                     | <b>-576</b>            | <b>158</b>             | 255                    | -70                        | -661                       |
| 3     | ULS 1a_0,9_0,9_100         | 251                    | 28                     | <b>-455</b>            | <b>-158</b>            | 197                    | -60                        | -522                       |
| 4     | SPLS 3_0,9_270 Ba All Cts  | -57                    | -358                   | <b>-522</b>            | <b>-294</b>            | 213                    | -82                        | -600                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 117                    | 97                     | 225                    | 14                     | -151                   | -24                        | 259                        |
| 2     | SLS 7      | 37                     | -56                    | 71                     | 14                     | -66                    | -26                        | 82                         |
| 3     | SLS 7      | -37                    | -56                    | 71                     | -14                    | -66                    | -26                        | 82                         |
| 4     | SLS 7      | -117                   | 97                     | 225                    | -14                    | -151                   | -24                        | 259                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | SPLS 1a_100 Ah All Cts     | -231                   | 541                    | <b>1027</b>            | 219                    | -546                   | 34                         | 1179                       |
| Max. trek         | SPLS 1a_0,9_100 Ah All Cts | -275                   | 203                    | <b>-753</b>            | 51                     | 338                    | -86                        | -865                       |
| Max. pos. torsie  | SPLS 3_0,9_80 Ah All Cts   | 177                    | -329                   | -309                   | <b>358</b>             | 108                    | -66                        | -354                       |
| Max. neg. torsie  | SPLS 3_0,9_100 Ba All Cts  | -167                   | -307                   | -298                   | <b>-335</b>            | 99                     | -69                        | -342                       |
| Comb. trek+torsie | SPLS 1a_0,9_225 Ah All Cts | -38                    | -406                   | <b>-708</b>            | <b>260</b>             | 314                    | -85                        | -813                       |

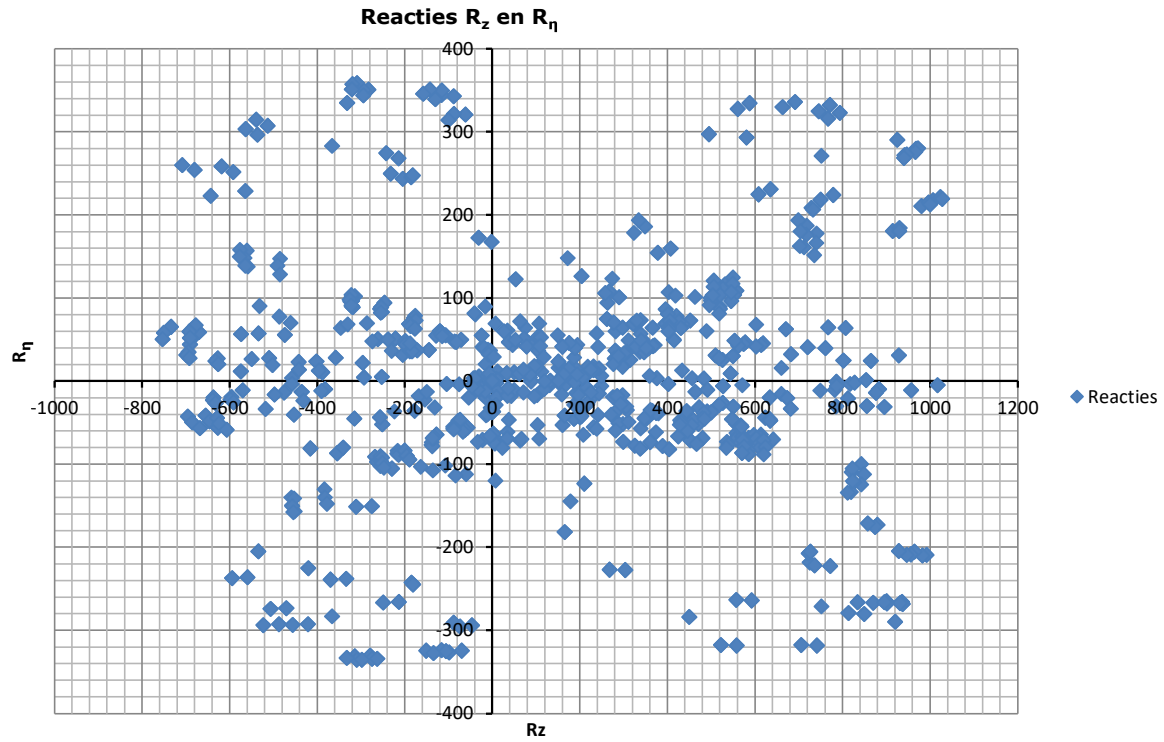
#### Maximale trekbelasting SLS

| Stijl | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_100 Ah All Cts  | 167                    | -329                   | <b>-321</b>            | 351                    | 115                    | -66                        | -368                       |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -275                   | 203                    | <b>-753</b>            | 51                     | 338                    | -86                        | -865                       |
| 3     | SPLS 1a_0,9_80 Ba Ct2      | 140                    | 11                     | <b>-268</b>            | -91                    | 107                    | -44                        | -308                       |
| 4     | SLS 1a_0                   | -67                    | -37                    | <b>-33</b>             | -73                    | -21                    | -40                        | -38                        |

#### Maximale drukbelasting SLS

| Stijl | Combinatie             | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_80 Ba Ct2      | 308                    | 154                    | <b>557</b>             | 109                    | -327                   | -13                        | 640                        |
| 2     | SLS 1a_0               | 87                     | -190                   | <b>330</b>             | 73                     | -196                   | -10                        | 379                        |
| 3     | SPLS 3_100 Ah All Cts  | -205                   | -272                   | <b>635</b>             | -48                    | -338                   | 20                         | 729                        |
| 4     | SPLS 1a_100 Ah All Cts | -231                   | 541                    | <b>1027</b>            | 219                    | -546                   | 34                         | 1179                       |

Project: GT-RL380  
Masttype: HA\_n (bouwfase)  
Mast: 18N



**Belastinggeval - afspannen**

Date: 2021-07-27  
Author: TBR  
Version: 1.1

RLL-TLB  
HA\_n

Invoergegevens
**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

| Circuits       | Aanduiding | Nummer   | Hoogteverschil |          | Richtingsverandering |          |
|----------------|------------|----------|----------------|----------|----------------------|----------|
|                |            |          | Dh_back        | Dh_ahead | Dy_back              | Dy_ahead |
| Circuit 1      | 10         | 380ct1f1 | -32,7          | 0,0 m    | 0,0                  | 0,0 m    |
| Circuit 1      | 11         | 380ct1f2 | -32,7          | 0,0 m    | 0,0                  | 0,0 m    |
| Circuit 1      | 12         | 380ct1f3 | -44,0          | 0,0 m    | 0,0                  | 0,0 m    |
| Bliksemdraad 1 | 1          | bl1      | -48,2          | 0,0 m    | 0,0                  | 0,0 m    |

**Lijn- en mastgegevens**

|                                       |          |  | Back  | Ahead   |
|---------------------------------------|----------|--|-------|---------|
| Ruling span $\sqrt{(SL3/SL)}$         |          |  | 66,0  | 400,0 m |
| Lijnhoek                              | $\beta$  |  | 180 ° |         |
| Rotatie mast t.o.v. bissectrice       | $\theta$ |  | 10 °  |         |
| Vaklengte                             |          |  | 66    | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld |          |  | 0,5 m |         |
| Beschouwde windrichtingen             | a1       |  | 0 °   |         |
| Windrichtingen volgens:               | a2       |  | 45 °  |         |
| <i>Geleiderbelastingen</i>            | a3       |  | 90 °  |         |
|                                       | a4       |  | 135 ° |         |
|                                       | a5       |  | 80 °  |         |
|                                       | a6       |  | 80 °  |         |

*Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.*

In onderstaande tabel zijn de optredende belastingen weergegeven, voor deze situatie geldt:

- belasting op geleider 1 en 10 t/m 12 zijn permanent aanwezig
- van de belasting op de overige geleiders is er telkens één aanwezig per belastingcombinatie

Uitvoer geleiderbelastingen

| Belastingcombi   | nummer | Fxtotaal     | Fytotaal     | Fztotaal    | Ftrekahead | Ftrekback |
|------------------|--------|--------------|--------------|-------------|------------|-----------|
| <b>ULS 6b_90</b> | 13     | <b>-83,5</b> | <b>15,8</b>  | <b>57,6</b> | 0,0        | -85,0     |
|                  | 10     | <b>88,8</b>  | <b>-12,4</b> | <b>19,3</b> | 89,6       | 0,0       |
|                  | 14     | <b>-83,5</b> | <b>15,8</b>  | <b>57,6</b> | 0,0        | -85,0     |
|                  | 11     | <b>88,8</b>  | <b>-12,4</b> | <b>19,3</b> | 89,6       | 0,0       |
|                  | 15     | <b>-83,6</b> | <b>15,8</b>  | <b>72,2</b> | 0,0        | -85,0     |
|                  | 12     | <b>89,5</b>  | <b>-12,2</b> | <b>19,3</b> | 90,2       | 0,0       |
|                  | 4      | <b>-17,4</b> | <b>3,3</b>   | <b>14,8</b> | 0,0        | -17,7     |
|                  | 1      | <b>19,2</b>  | <b>-2,4</b>  | <b>2,7</b>  | 19,4       | 0,0       |

## **APPENDIX B**

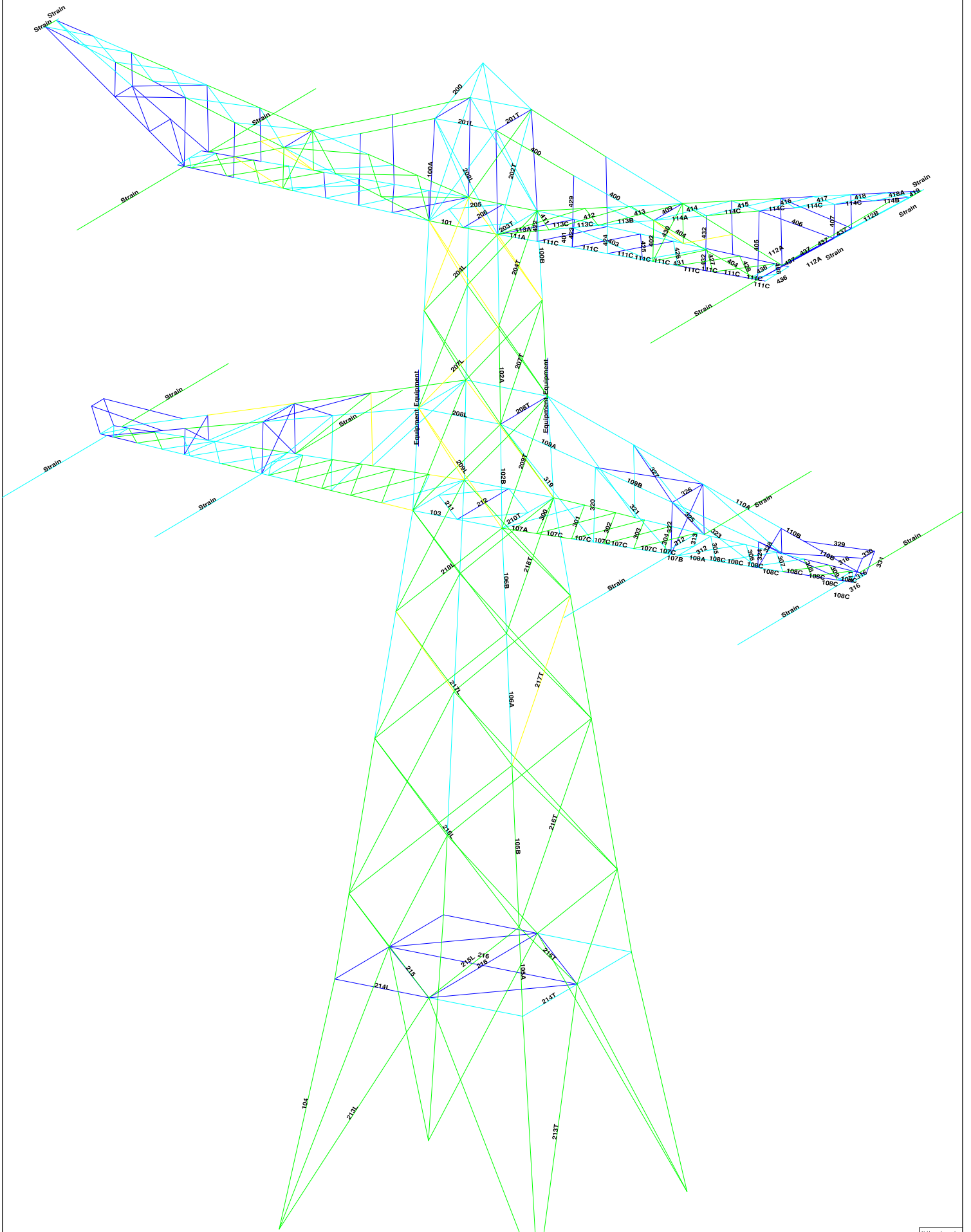
### **Resultaten PLS tower**

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Deze Appendix bevat de resultaten uit PLS Tower voor de verschillende masttypen. De samenstelling van de bovenstukken zijn voor alle masttypen gelijk. De resultaten van het bovenstuk zijn dan ook alleen opgenomen van het maatgevende masttype HA+5/n. De resultaten van het onderstuk zijn voor alle masten opgenomen.

Resultaten opgenomen voor:

- Masttype HA+0/n
- Masttype HA+5/n















Assessment of angle groups

Date 21-9-2021  
Author BIT  
Version 4.3

GT-RLL  
HA+3\_n

| Group Label | Element | Type | Code | Qun | U | U <sub>1</sub> | U <sub>2</sub> | U <sub>3</sub> | U <sub>4</sub> | U <sub>5</sub> | U <sub>6</sub> | U <sub>7</sub> | U <sub>8</sub> | U <sub>9</sub> | U <sub>10</sub> | U <sub>11</sub> | U <sub>12</sub> | U <sub>13</sub> | U <sub>14</sub> | U <sub>15</sub> | U <sub>16</sub> | U <sub>17</sub> | U <sub>18</sub> | U <sub>19</sub> | U <sub>20</sub> | U <sub>21</sub> | U <sub>22</sub> | U <sub>23</sub> | U <sub>24</sub> | U <sub>25</sub> | U <sub>26</sub> | U <sub>27</sub> | U <sub>28</sub> | U <sub>29</sub> | U <sub>30</sub> | U <sub>31</sub> | U <sub>32</sub> | U <sub>33</sub> | U <sub>34</sub> | U <sub>35</sub> | U <sub>36</sub> | U <sub>37</sub> | U <sub>38</sub> | U <sub>39</sub> | U <sub>40</sub> | U <sub>41</sub> | U <sub>42</sub> | U <sub>43</sub> | U <sub>44</sub> | U <sub>45</sub> | U <sub>46</sub> | U <sub>47</sub> | U <sub>48</sub> | U <sub>49</sub> | U <sub>50</sub> | U <sub>51</sub> | U <sub>52</sub> | U <sub>53</sub> | U <sub>54</sub> | U <sub>55</sub> | U <sub>56</sub> | U <sub>57</sub> | U <sub>58</sub> | U <sub>59</sub> | U <sub>60</sub> | U <sub>61</sub> | U <sub>62</sub> | U <sub>63</sub> | U <sub>64</sub> | U <sub>65</sub> | U <sub>66</sub> | U <sub>67</sub> | U <sub>68</sub> | U <sub>69</sub> | U <sub>70</sub> | U <sub>71</sub> | U <sub>72</sub> | U <sub>73</sub> | U <sub>74</sub> | U <sub>75</sub> | U <sub>76</sub> | U <sub>77</sub> | U <sub>78</sub> | U <sub>79</sub> | U <sub>80</sub> | U <sub>81</sub> | U <sub>82</sub> | U <sub>83</sub> | U <sub>84</sub> | U <sub>85</sub> | U <sub>86</sub> | U <sub>87</sub> | U <sub>88</sub> | U <sub>89</sub> | U <sub>90</sub> | U <sub>91</sub> | U <sub>92</sub> | U <sub>93</sub> | U <sub>94</sub> | U <sub>95</sub> | U <sub>96</sub> | U <sub>97</sub> | U <sub>98</sub> | U <sub>99</sub> | U <sub>100</sub> | U <sub>101</sub> | U <sub>102</sub> | U <sub>103</sub> | U <sub>104</sub> | U <sub>105</sub> | U <sub>106</sub> | U <sub>107</sub> | U <sub>108</sub> | U <sub>109</sub> | U <sub>110</sub> | U <sub>111</sub> | U <sub>112</sub> | U <sub>113</sub> | U <sub>114</sub> | U <sub>115</sub> | U <sub>116</sub> | U <sub>117</sub> | U <sub>118</sub> | U <sub>119</sub> | U <sub>120</sub> | U <sub>121</sub> | U <sub>122</sub> | U <sub>123</sub> | U <sub>124</sub> | U <sub>125</sub> | U <sub>126</sub> | U <sub>127</sub> | U <sub>128</sub> | U <sub>129</sub> | U <sub>130</sub> | U <sub>131</sub> | U <sub>132</sub> | U <sub>133</sub> | U <sub>134</sub> | U <sub>135</sub> | U <sub>136</sub> | U <sub>137</sub> | U <sub>138</sub> | U <sub>139</sub> | U <sub>140</sub> | U <sub>141</sub> | U <sub>142</sub> | U <sub>143</sub> | U <sub>144</sub> | U <sub>145</sub> | U <sub>146</sub> | U <sub>147</sub> | U <sub>148</sub> | U <sub>149</sub> | U <sub>150</sub> | U <sub>151</sub> | U <sub>152</sub> | U <sub>153</sub> | U <sub>154</sub> | U <sub>155</sub> | U <sub>156</sub> | U <sub>157</sub> | U <sub>158</sub> | U <sub>159</sub> | U <sub>160</sub> | U <sub>161</sub> | U <sub>162</sub> | U <sub>163</sub> | U <sub>164</sub> | U <sub>165</sub> | U <sub>166</sub> | U <sub>167</sub> | U <sub>168</sub> | U <sub>169</sub> | U <sub>170</sub> | U <sub>171</sub> | U <sub>172</sub> | U <sub>173</sub> | U <sub>174</sub> | U <sub>175</sub> | U <sub>176</sub> | U <sub>177</sub> | U <sub>178</sub> | U <sub>179</sub> | U <sub>180</sub> | U <sub>181</sub> | U <sub>182</sub> | U <sub>183</sub> | U <sub>184</sub> | U <sub>185</sub> | U <sub>186</sub> | U <sub>187</sub> | U <sub>188</sub> | U <sub>189</sub> | U <sub>190</sub> | U <sub>191</sub> | U <sub>192</sub> | U <sub>193</sub> | U <sub>194</sub> | U <sub>195</sub> | U <sub>196</sub> | U <sub>197</sub> | U <sub>198</sub> | U <sub>199</sub> | U <sub>200</sub> | U <sub>201</sub> | U <sub>202</sub> | U <sub>203</sub> | U <sub>204</sub> | U <sub>205</sub> | U <sub>206</sub> | U <sub>207</sub> | U <sub>208</sub> | U <sub>209</sub> | U <sub>210</sub> | U <sub>211</sub> | U <sub>212</sub> | U <sub>213</sub> | U <sub>214</sub> | U <sub>215</sub> | U <sub>216</sub> | U <sub>217</sub> | U <sub>218</sub> | U <sub>219</sub> | U <sub>220</sub> | U <sub>221</sub> | U <sub>222</sub> | U <sub>223</sub> | U <sub>224</sub> | U <sub>225</sub> | U <sub>226</sub> | U <sub>227</sub> | U <sub>228</sub> | U <sub>229</sub> | U <sub>230</sub> | U <sub>231</sub> | U <sub>232</sub> | U <sub>233</sub> | U <sub>234</sub> | U <sub>235</sub> | U <sub>236</sub> | U <sub>237</sub> | U <sub>238</sub> | U <sub>239</sub> | U <sub>240</sub> | U <sub>241</sub> | U <sub>242</sub> | U <sub>243</sub> | U <sub>244</sub> | U <sub>245</sub> | U <sub>246</sub> | U <sub>247</sub> | U <sub>248</sub> | U <sub>249</sub> | U <sub>250</sub> | U <sub>251</sub> | U <sub>252</sub> | U <sub>253</sub> | U <sub>254</sub> | U <sub>255</sub> | U <sub>256</sub> | U <sub>257</sub> | U <sub>258</sub> | U <sub>259</sub> | U <sub>260</sub> | U <sub>261</sub> | U <sub>262</sub> | U <sub>263</sub> | U <sub>264</sub> | U <sub>265</sub> | U <sub>266</sub> | U <sub>267</sub> | U <sub>268</sub> | U <sub>269</sub> | U <sub>270</sub> | U <sub>271</sub> | U <sub>272</sub> | U <sub>273</sub> | U <sub>274</sub> | U <sub>275</sub> | U <sub>276</sub> | U <sub>277</sub> | U <sub>278</sub> | U <sub>279</sub> | U <sub>280</sub> | U <sub>281</sub> | U <sub>282</sub> | U <sub>283</sub> | U <sub>284</sub> | U <sub>285</sub> | U <sub>286</sub> | U <sub>287</sub> | U <sub>288</sub> | U <sub>289</sub> | U <sub>290</sub> | U <sub>291</sub> | U <sub>292</sub> | U <sub>293</sub> | U <sub>294</sub> | U <sub>295</sub> | U <sub>296</sub> | U <sub>297</sub> | U <sub>298</sub> | U <sub>299</sub> | U <sub>300</sub> | U <sub>301</sub> | U <sub>302</sub> | U <sub>303</sub> | U <sub>304</sub> | U <sub>305</sub> | U <sub>306</sub> | U <sub>307</sub> | U <sub>308</sub> | U <sub>309</sub> | U <sub>310</sub> | U <sub>311</sub> | U <sub>312</sub> | U <sub>313</sub> | U <sub>314</sub> | U <sub>315</sub> | U <sub>316</sub> | U 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<sub>525</sub> | U <sub>526</sub> | U <sub>527</sub> | U <sub>528</sub> | U <sub>529</sub> | U <sub>530</sub> | U <sub>531</sub> | U <sub>532</sub> | U <sub>533</sub> | U <sub>534</sub> | U <sub>535</sub> | U <sub>536</sub> | U <sub>537</sub> | U <sub>538</sub> | U <sub>539</sub> | U <sub>540</sub> | U <sub>541</sub> | U <sub>542</sub> | U <sub>543</sub> | U <sub>544</sub> | U <sub>545</sub> | U <sub>546</sub> | U <sub>547</sub> | U <sub>548</sub> | U <sub>549</sub> | U <sub>550</sub> | U <sub>551</sub> | U <sub>552</sub> | U <sub>553</sub> | U <sub>554</sub> | U <sub>555</sub> | U <sub>556</sub> | U <sub>557</sub> | U <sub>558</sub> | U <sub>559</sub> | U <sub>560</sub> | U <sub>561</sub> | U <sub>562</sub> | U <sub>563</sub> | U <sub>564</sub> | U <sub>565</sub> | U <sub>566</sub> | U <sub>567</sub> | U <sub>568</sub> | U <sub>569</sub> | U <sub>570</sub> | U <sub>571</sub> | U <sub>572</sub> | U <sub>573</sub> | U <sub>574</sub> | U <sub>575</sub> | U <sub>576</sub> | U <sub>577</sub> | U <sub>578</sub> | U <sub>579</sub> | U <sub>580</sub> | U <sub>581</sub> | U <sub>582</sub> | U <sub>583</sub> | U <sub>584</sub> | U <sub>585</sub> | U <sub>586</sub> | U <sub>587</sub> | U <sub>588</sub> | U <sub>589</sub> | U <sub>590</sub> | U <sub>591</sub> | U <sub>592</sub> | U <sub>593</sub> | U <sub>594</sub> | U <sub>595</sub> | U <sub>596</sub> | U <sub>597</sub> | U <sub>598</sub> | U <sub>599</sub> | U <sub>600</sub> | U <sub>601</sub> | U <sub>602</sub> | U <sub>603</sub> | U <sub>604</sub> | U <sub>605</sub> | U <sub>606</sub> | U <sub>607</sub> | U <sub>608</sub> | U <sub>609</sub> | U <sub>610</sub> | U <sub>611</sub> | U <sub>612</sub> | U <sub>613</sub> | U <sub>614</sub> | U <sub>615</sub> | U <sub>616</sub> | U <sub>617</sub> | U <sub>618</sub> | U <sub>619</sub> | U <sub>620</sub> | U <sub>621</sub> | U <sub>622</sub> | U <sub>623</sub> | U <sub>624</sub> | U <sub>625</sub> | U <sub>626</sub> | U <sub>627</sub> | U <sub>628</sub> | U <sub>629</sub> | U <sub>630</sub> | U <sub>631</sub> | U <sub>632</sub> | U <sub>633</sub> | U <sub>634</sub> | U <sub>635</sub> | U <sub>636</sub> | U <sub>637</sub> | U <sub>638</sub> | U <sub>639</sub> | U <sub>640</sub> | U <sub>641</sub> | U <sub>642</sub> | U <sub>643</sub> | U <sub>644</sub> | U <sub>645</sub> | U <sub>646</sub> | U <sub>647</sub> | U <sub>648</sub> | U <sub>649</sub> | U <sub>650</sub> | U <sub>651</sub> | U <sub>652</sub> | U <sub>653</sub> | U <sub>654</sub> | U <sub>655</sub> | U <sub>656</sub> | U <sub>657</sub> | U <sub>658</sub> | U <sub>659</sub> | U <sub>660</sub> | U <sub>661</sub> | U <sub>662</sub> | U <sub>663</sub> | U <sub>664</sub> | U <sub>665</sub> | U <sub>666</sub> | U <sub>667</sub> | U <sub>668</sub> | U <sub>669</sub> | U <sub>670</sub> | U <sub>671</sub> | U <sub>672</sub> | U <sub>673</sub> | U <sub>674</sub> | U <sub>675</sub> | U <sub>676</sub> | U <sub>677</sub> | U <sub>678</sub> | U <sub>679</sub> | U <sub>680</sub> | U <sub>681</sub> | U <sub>682</sub> | U <sub>683</sub> | U <sub>684</sub> | U <sub>685</sub> | U <sub>686</sub> | U <sub>687</sub> | U <sub>688</sub> | U <sub>689</sub> | U <sub>690</sub> | U <sub>691</sub> | U <sub>692</sub> | U <sub>693</sub> | U <sub>694</sub> | U <sub>695</sub> | U <sub>696</sub> | U <sub>697</sub> | U <sub>698</sub> | U <sub>699</sub> | U <sub>700</sub> | U <sub>701</sub> | U <sub>702</sub> | U <sub>703</sub> | U <sub>704</sub> | U <sub>705</sub> | U <sub>706</sub> | U <sub>707</sub> | U <sub>708</sub> | U <sub>709</sub> | U <sub>710</sub> | U <sub>711</sub> | U <sub>712</sub> | U <sub>713</sub> | U <sub>714</sub> | U <sub>715</sub> | U <sub>716</sub> | U <sub>717</sub> | U <sub>718</sub> | U <sub>719</sub> | U <sub>720</sub> | U <sub>721</sub> | U <sub>722</sub> | U <sub>723</sub> | U <sub>724</sub> | U <sub>725</sub> | U <sub>726</sub> | U <sub>727</sub> | U <sub>728</sub> | U <sub>729</sub> | U <sub>730</sub> | U <sub>731</sub> | U <sub>732</sub> | U <sub>733</sub> | U <sub>734</sub> | U <sub>735</sub> | U <sub>736</sub> | U <sub>737</sub> | U <sub>738</sub> | U <sub>739</sub> | U <sub>740</sub> | U <sub>741</sub> | U <sub>742</sub> | U <sub>743</sub> | U <sub>744</sub> | U <sub>745</sub> | U <sub>746</sub> | U <sub>747</sub> | U <sub>748</sub> | U <sub>749</sub> | U <sub>750</sub> | U <sub>751</sub> | U <sub>752</sub> | U <sub>753</sub> | U <sub>754</sub> | U <sub>755</sub> | U <sub>756</sub> | U <sub>757</sub> | U <sub>758</sub> | U <sub>759</sub> | U <sub>760</sub> | U <sub>761</sub> | U <sub>762</sub> | U <sub>763</sub> | U <sub>764</sub> | U <sub>765</sub> | U <sub>766</sub> | U <sub>767</sub> | U <sub>768</sub> | U <sub>769</sub> | U <sub>770</sub> | U <sub>771</sub> | U <sub>772</sub> | U <sub>773</sub> | U <sub>774</sub> | U <sub>775</sub> | U <sub>776</sub> | U <sub>777</sub> | U <sub>778</sub> | U <sub>779</sub> | U <sub>780</sub> | U <sub>781</sub> | U <sub>782</sub> | U <sub>783</sub> | U <sub>784</sub> | U <sub>785</sub> | U <sub>786</sub> | U <sub>787</sub> | U <sub>788</sub> | U <sub>789</sub> | U <sub>790</sub> | U <sub>791</sub> | U <sub>792</sub> | U <sub>793</sub> | U <sub>794</sub> | U <sub>795</sub> | U <sub>796</sub> | U <sub>797</sub> | U <sub>798</sub> | U <sub>799</sub> | U <sub>800</sub> | U <sub>801</sub> | U <sub>802</sub> | U <sub>803</sub> | U <sub>804</sub> | U <sub>805</sub> | U <sub>806</sub> | U <sub>807</sub> | U <sub>808</sub> | U <sub>809</sub> | U <sub>810</sub> | U <sub>811</sub> | U <sub>812</sub> | U <sub>813</sub> | U <sub>814</sub> | U <sub>815</sub> | U <sub>8</sub> |
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## APPENDIX C

### Knikverkorters

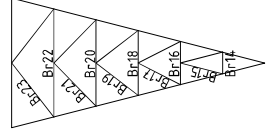
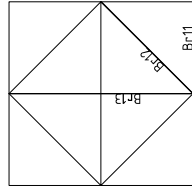
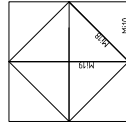
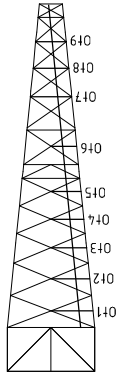
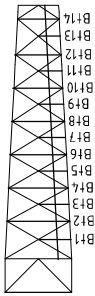
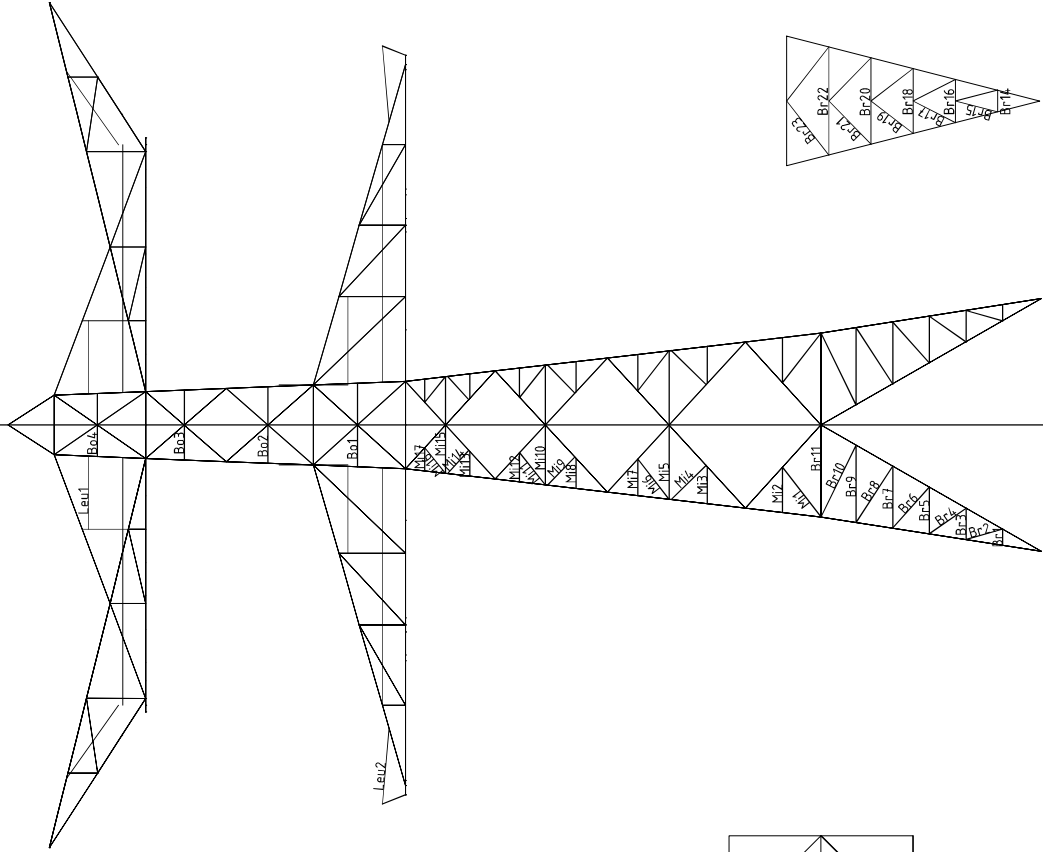
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Niet in PLS-TOWER gemodelleerde elementen in de constructie worden aanvullend getoetst. Hieronder vallen de knikverkorters van de randstijl en profielen onderdeel van stabiliteitsverbanden. De staven worden getoetst op:

- voldoende trek- of druksterkte als steungevend profiel voor randstijl, 1% van de knikcapaciteit van de randstijl;
- slankheid;
- klimbelasting

Voor de beloopbaarheid zijn staven in de traverse aanwezig. Deze zijn niet constructief (voorzien van slobgaten) en worden enkel getoetst op de klimbelasting van 1,0 kN. Zie hoofdstuk 4.2.5 en 5.7.2. van het uitgangspuntenrapport.

# Overzicht knikverkorters - HA+0\_n



# DNV-GL

Date: 2021-06-07  
 Author: BJT  
 Version: 1.8

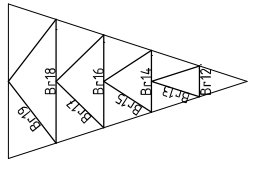
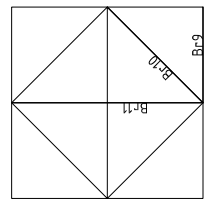
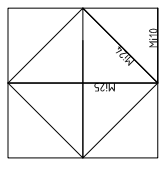
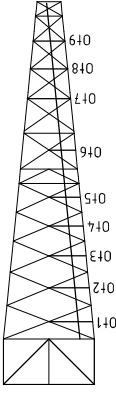
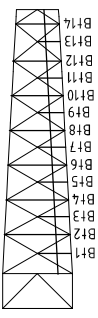
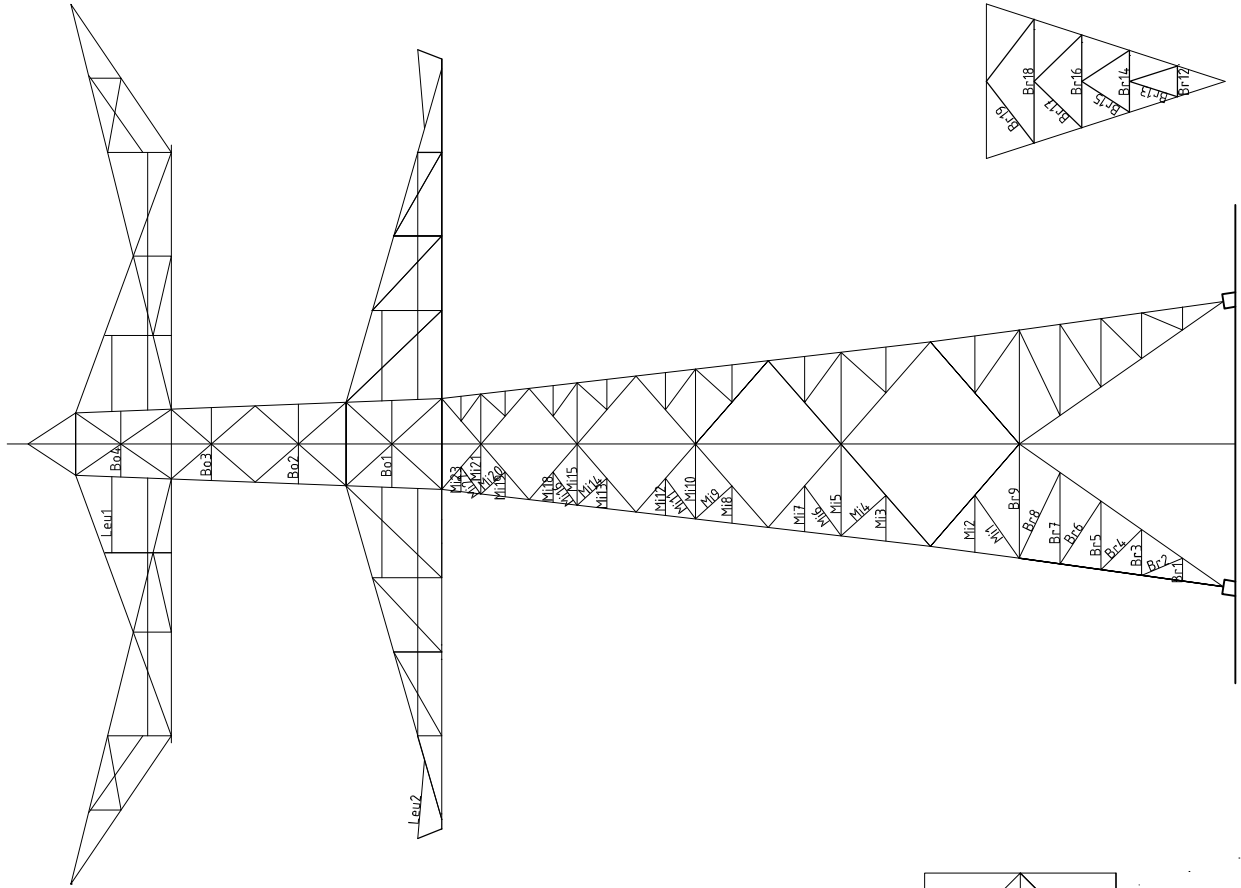
## Knikverkorters

ZWO  
 HA+0\_n

| Posnr. | Section           | Schematization             | Profile | Steel Quality | Bolt | Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|-------------------|----------------------------|---------|---------------|------|---------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
| B1     | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 0.704      | 0         | 72           | 26.1              | 0.26         | 80.3               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.63         |                 |       |
| B2     | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.660      | 74        | 171          | 26.1              | 0.00         | 30.9               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.84         |                 |       |
| B3     | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.370      | 0         | 141          | 26.1              | 0.51         | 40.3               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.65         |                 |       |
| B4     | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.950      | 55        | 167          | 26.1              | 0.00         | 45.9               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.57         |                 |       |
| B5     | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.030      | 0         | 174          | 26.1              | 0.76         | 43.3               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.60         |                 |       |
| B6     | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.400      | 42        | 205          | 26.1              | 0.00         | 33.8               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.77         |                 |       |
| B7     | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.700      | 0         | 231          | 26.1              | 1.01         | 28.1               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.93         |                 |       |
| B8     | Broekstuk         | Enkele staaf               | L70.7   | S355J0        | M16  | 8.8     | 2.920      | 33        | 214          | 26.1              | 0.00         | 43.1               | 60.3                 | 61.0              | 142.7                 | 2.23              | 0.61         |                 |       |
| B9     | Broekstuk         | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.360      | 0         | 214          | 26.1              | 1.26         | 43.0               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.61         |                 |       |
| B10    | Broekstuk         | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.470      | 26        | 221          | 26.1              | 1.17         | 40.9               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.64         |                 |       |
| B11    | Tussenschot +9,6r | Enkele staaf               | L100.8  | S355J0        | M16  | 8.8     | 4.000      | 0         | 203          | 0.0               | 0.00         | 77.0               | 60.3                 | 69.7              | 257.2                 | 5.49              | 0.29         |                 |       |
| B12    | Tussenschot +9,6r | Kniksteun op 0,5L          | L80.8   | S355J0        | M16  | 8.8     | 5.650      | 0         | 233          | 0.0               | 2.12         | 41.9               | 60.3                 | 69.7              | 194.4                 | 4.46              | 0.47         |                 |       |
| B13    | Tussenschot +9,6r | Kruisende staaf halverwege | L90.9   | S355J0        | M16  | 8.8     | 8.000      | 0         | 228          | 0.0               | 1.50         | 64.5               | 60.3                 | 78.4              | 254.0                 | 6.37              | 0.24         |                 |       |
| M1     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.730      | 37        | 234          | 0.0               | 0.00         | 27.6               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.00         |                 |       |
| M2     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.960      | 0         | 168          | 26.2              | 0.74         | 45.6               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.57         |                 |       |
| M3     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.600      | 0         | 137          | 26.2              | 0.60         | 60.2               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M4     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.120      | 45        | 181          | 26.2              | 0.00         | 40.7               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.64         |                 |       |
| M5     | Tussenstuk1       | Enkele staaf               | L70.7   | S355J0        | M16  | 8.8     | 3.320      | 0         | 243          | 26.2              | 1.25         | 35.2               | 60.3                 | 61.0              | 142.7                 | 2.23              | 0.74         |                 |       |
| M6     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.210      | 38        | 189          | 26.2              | 0.00         | 38.3               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.69         |                 |       |
| M7     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.590      | 0         | 136          | 26.2              | 0.60         | 60.7               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M8     | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.310      | 0         | 112          | 26.2              | 0.49         | 76.9               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M9     | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.710      | 45        | 146          | 26.2              | 0.00         | 55.1               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M10    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.600      | 0         | 222          | 26.2              | 0.98         | 29.8               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.88         |                 |       |
| M11    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.800      | 38        | 154          | 26.2              | 0.00         | 51.4               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.51         |                 |       |
| M12    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.280      | 0         | 110          | 26.2              | 0.48         | 78.9               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M13    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.060      | 0         | 91           | 26.2              | 0.40         | 95.9               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M14    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.360      | 42        | 116          | 26.2              | 0.70         | 41.3               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M15    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.100      | 0         | 180          | 26.2              | 0.00         | 69.3               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.64         |                 |       |
| M16    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.430      | 39        | 122          | 26.2              | 0.00         | 69.3               | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M17    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.010      | 0         | 86           | 26.2              | 0.38         | 100.2              | 60.3                 | 52.3              | 52.3                  | 1.40              | 0.50         |                 |       |
| M18    | Tussenstuk2       | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.680      | 0         | 234          | 0.0               | 1.38         | 37.3               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.54         |                 |       |
| M19    | Tussenschot 21,6  | Kruisende staaf halverwege | L80.6   | S355J0        | M16  | 8.8     | 5.210      | 0         | 166          | 0.0               | 0.98         | 62.8               | 60.3                 | 52.3              | 145.8                 | 3.40              | 0.29         |                 |       |
| B01    | Bovenstuk1        | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.810      | 0         | 186          | 12.2              | 0.68         | 27.2               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.87         |                 |       |
| B02    | Bovenstuk2        | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.660      | 0         | 171          | 12.2              | 0.62         | 30.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.79         |                 |       |
| B03    | Bovenstuk2        | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.520      | 0         | 156          | 6.4               | 0.57         | 35.0               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.73         |                 |       |
| O01    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.370      | 0         | 141          | 6.4               | 0.51         | 40.3               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.65         |                 |       |
| O04    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.836      | 0         | 189          | 0.0               | 0.69         | 26.7               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.88         |                 |       |
| O02    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.730      | 0         | 178          | 0.0               | 0.65         | 29.1               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.83         |                 |       |
| O03    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.610      | 0         | 165          | 0.0               | 0.60         | 32.3               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.77         |                 |       |
| O04    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.470      | 0         | 151          | 0.0               | 0.55         | 36.7               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.70         |                 |       |
| O05    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.330      | 0         | 137          | 0.0               | 0.50         | 41.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.64         |                 |       |



# Overzicht knikverkorters - HA+5





**Knikverkorters initial construction (afkeur)**

Date: 2021-06-07  
 Author: BJT  
 Version: 1.8

ZWO  
 HA+5\_n

| Posnr. | Section           | Schematization             | Profile | Steel Quality | Bolt | Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|-------------------|----------------------------|---------|---------------|------|---------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
| B1     | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 0.950      | 0         | 98           | 24.3              | 0.36         | 62.0               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.59         |                 |       |
| B2     | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.850      | 67        | 190          | 24.3              | 0.00         | 26.4               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.92         |                 |       |
| B3     | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.910      | 0         | 196          | 24.3              | 0.72         | 25.1               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.97         |                 |       |
| B4     | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.390      | 45        | 204          | 24.3              | 0.00         | 34.0               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.71         |                 |       |
| B5     | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.860      | 0         | 245          | 24.3              | 1.07         | 25.6               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.95         |                 |       |
| B6     | Broekstuk         | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.130      | 33        | 199          | 24.3              | 0.00         | 47.9               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.51         |                 |       |
| B7     | Broekstuk         | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.810      | 0         | 242          | 24.3              | 1.43         | 35.3               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.69         |                 |       |
| B8     | Broekstuk         | Enkele staaf               | L90.9   | S355J0        | M16  | 8.8     | 3.970      | 26        | 226          | 24.3              | 1.34         | 65.2               | 60.3                 | 78.4              | 254.0                 | 4.73              | 0.40         |                 |       |
| B9     | Broekstuk         | Enkele staaf               | L120.10 | S355J0        | M16  | 8.8     | 4.770      | 0         | 201          | 24.3              | 1.79         | 117.4              | 60.3                 | 87.1              | 399.8                 | 9.77              | 0.40         |                 |       |
| B10    | Tussenschot +9,6r | Kniksteun op 0,5L          | L100.8  | S355J0        | M16  | 8.8     | 6.740      | 0         | 219          | 0.0               | 2.53         | 57.8               | 60.3                 | 69.7              | 257.2                 | 7.19              | 0.35         |                 |       |
| B11    | Tussenschot +9,6r | Kruisende staaf halverwege | L100.8  | S355J0        | M16  | 8.8     | 9.540      | 0         | 242          | 0.0               | 1.79         | 58.5               | 60.3                 | 69.7              | 257.2                 | 7.19              | 0.25         |                 |       |
| B12    | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.300      | 0         | 134          | 8.5               | 0.49         | 43.1               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.62         |                 |       |
| B13    | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 2.100      | 72        | 216          | 8.5               | 0.00         | 21.7               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.39         |                 |       |
| B14    | Broekstuk         | Kniksteun op 0,5L          | L50.5   | S355J0        | M16  | 8.8     | 2.580      | 0         | 170          | 8.5               | 0.97         | 25.3               | 60.3                 | 41.3              | 43.1                  | 1.08              | 0.89         |                 |       |
| B15    | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 2.580      | 57        | 245          | 8.5               | 0.00         | 17.8               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.47         |                 |       |
| B16    | Broekstuk         | Kniksteun op 0,5L          | L60.6   | S355J0        | M16  | 8.8     | 3.870      | 0         | 213          | 8.5               | 1.45         | 26.8               | 60.3                 | 52.3              | 98.8                  | 1.88              | 0.77         |                 |       |
| B17    | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.780      | 46        | 238          | 8.5               | 0.00         | 26.8               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.32         |                 |       |
| B18    | Broekstuk         | Kniksteun op 0,5L          | L70.7   | S355J0        | M16  | 8.8     | 5.170      | 0         | 243          | 8.5               | 1.94         | 30.0               | 60.3                 | 61.0              | 142.7                 | 2.99              | 0.65         |                 |       |
| B19    | Broekstuk         | Enkele staaf               | L70.7   | S355J0        | M16  | 8.8     | 3.260      | 38        | 239          | 8.5               | 0.00         | 36.2               | 60.3                 | 61.0              | 142.7                 | 2.23              | 0.23         |                 |       |
| M1     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.200      | 35        | 236          | 23.3              | 0.00         | 37.0               | 60.3                 | 61.0              | 142.7                 | 2.23              | 0.63         |                 |       |
| M2     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.380      | 0         | 204          | 23.3              | 0.89         | 34.2               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.68         |                 |       |
| M3     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.900      | 0         | 163          | 23.3              | 0.71         | 47.6               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.53         |                 |       |
| M4     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.520      | 48        | 216          | 23.3              | 0.00         | 31.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.74         |                 |       |
| M5     | Tussenstuk1       | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.830      | 0         | 243          | 23.3              | 1.44         | 35.0               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.66         |                 |       |
| M6     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.580      | 36        | 221          | 23.3              | 0.00         | 30.2               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.77         |                 |       |
| M7     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.910      | 0         | 163          | 23.3              | 0.72         | 47.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.53         |                 |       |
| M8     | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.550      | 0         | 133          | 23.6              | 0.58         | 62.7               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M9     | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.060      | 48        | 176          | 23.6              | 0.00         | 42.4               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.56         |                 |       |
| M10    | Tussenstuk2       | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.130      | 0         | 199          | 23.6              | 1.17         | 47.9               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.49         |                 |       |
| M11    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.100      | 36        | 180          | 23.6              | 0.00         | 41.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.57         |                 |       |
| M12    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.590      | 0         | 133          | 23.6              | 0.58         | 62.7               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M13    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.260      | 0         | 108          | 23.6              | 0.47         | 80.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M14    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.670      | 48        | 143          | 23.6              | 0.00         | 56.9               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M15    | Tussenstuk2       | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 2.560      | 0         | 163          | 23.6              | 0.96         | 64.3               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.45         |                 |       |
| M16    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.710      | 36        | 146          | 23.6              | 0.00         | 55.1               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M17    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.270      | 0         | 109          | 23.6              | 0.48         | 79.6               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M18    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.030      | 0         | 88           | 23.6              | 0.39         | 98.5               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |
| M19    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.370      | 48        | 117          | 23.6              | 0.00         | 73.0               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |
| M20    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.100      | 0         | 180          | 23.6              | 0.79         | 41.3               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.58         |                 |       |
| M21    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.400      | 36        | 120          | 23.6              | 0.00         | 71.1               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |
| M22    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.030      | 0         | 88           | 23.6              | 0.39         | 98.5               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |

**Knikverkorters initial construction (afkeur)**

Date: 2021-06-07  
 Author: BJT  
 Version: 1.8

ZWO  
 HA+5\_n

| Posnr. | Section           | Schematization             | Profile | Steel Quality | Bolt | Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|-------------------|----------------------------|---------|---------------|------|---------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
| M124   | Tussenschot +21.1 | Enkele staaf               | L90.8   | S355J0        | M16  | 8.8     | 4,400      | 0         | 250          | 0.0               | 1.65         | 49.9               | 60.3                 | 69.7              | 225.8                 | 4.3               | 0.40         |                 |       |
| M125   | Tussenschot +21.1 | Kruisende staaf halverwege | L90.8   | S355J0        | M16  | 8.8     | 6,260      | 0         | 178          | 0.0               | 1.17         | 84.3               | 60.3                 | 69.7              | 225.8                 | 5.7               | 0.21         |                 |       |
| B01    | Bovenstuk1        | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,810      | 0         | 186          | 12.2              | 0.68         | 27.2               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.87         |                 |       |
| B02    | Bovenstuk2        | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,660      | 0         | 171          | 12.2              | 0.62         | 30.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.79         |                 |       |
| B03    | Bovenstuk2        | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,520      | 0         | 156          | 6.4               | 0.57         | 35.0               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.73         |                 |       |
| B04    | Bovenstuk2        | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,370      | 0         | 141          | 6.4               | 0.51         | 40.3               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.65         |                 |       |
| O11    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,830      | 0         | 188          | 0.0               | 0.69         | 26.8               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.87         |                 |       |
| O12    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,690      | 0         | 174          | 0.0               | 0.63         | 30.1               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.81         |                 |       |
| O13    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,550      | 0         | 159          | 0.0               | 0.58         | 34.1               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.74         |                 |       |
| O14    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,430      | 0         | 147          | 0.0               | 0.54         | 38.1               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.68         |                 |       |
| O15    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,320      | 0         | 136          | 0.0               | 0.50         | 42.3               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.63         |                 |       |
| O16    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,115      | 0         | 115          | 0.0               | 0.42         | 52.1               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.53         |                 |       |
| O17    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,790      | 0         | 184          | 0.0               | 0.67         | 27.7               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.86         |                 |       |
| O18    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,566      | 0         | 160          | 0.0               | 0.58         | 33.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.74         |                 |       |
| O19    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,530      | 0         | 157          | 0.0               | 0.58         | 41.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.64         |                 |       |
| B11    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,420      | 0         | 146          | 0.0               | 0.53         | 38.4               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.68         |                 |       |
| B12    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2,760      | 0         | 236          | 0.0               | 1.04         | 27.1               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.76         |                 |       |
| B13    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,340      | 0         | 138          | 0.0               | 0.50         | 41.5               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.64         |                 |       |
| B14    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2,610      | 0         | 223          | 0.0               | 0.98         | 29.6               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.72         |                 |       |
| B15    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,260      | 0         | 129          | 0.0               | 0.47         | 44.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.60         |                 |       |
| B16    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2,490      | 0         | 213          | 0.0               | 0.93         | 31.9               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.69         |                 |       |
| B17    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,210      | 0         | 124          | 0.0               | 0.45         | 47.2               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.58         |                 |       |
| B19    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2,350      | 0         | 201          | 0.0               | 0.88         | 34.9               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.65         |                 |       |
| B10    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,142      | 0         | 117          | 0.0               | 0.43         | 50.6               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.55         |                 |       |
| B11    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2,220      | 0         | 190          | 0.0               | 0.83         | 38.0               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.61         |                 |       |
| B12    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,070      | 0         | 110          | 0.0               | 0.40         | 54.6               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.51         |                 |       |
| B11    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 2,080      | 0         | 214          | 0.0               | 0.78         | 22.1               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.99         |                 |       |
| B13    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 0,950      | 0         | 98           | 0.0               | 0.36         | 62.0               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.45         |                 |       |
| B14    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1,822      | 0         | 187          | 0.0               | 0.68         | 27.0               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.87         |                 |       |
| Leu1   | Boventraverse     | Enkele staaf               | L70.7   | S355J0        | M16  | 8.8     | 3,180      | 0         | 233          | 0.0               | 1.19         | 37.7               | 60.3                 | 61.0              | 142.7                 | 2.2               | 0.55         |                 |       |
| Leu2   | Ondertraverse     | Enkele staaf               | L70.7   | S355J0        | M16  | 8.8     | 3,300      | 0         | 242          | 0.0               | 1.24         | 35.5               | 60.3                 | 61.0              | 142.7                 | 2.2               | 0.57         |                 |       |

## APPENDIX D

### Blokdeuvels

De belastingen op de fundatie uit Appendix A zijn uitgangspunt voor de berekening van de ingestorte rand met blokdeuvels. De belastingen in de richting van de randstijl zijn van toepassing. In de tabellen is dit opgenomen in de laatste kolom  $R_{z,lok}$ . De controles zijn uitgevoerd met een spreadsheet. Vanwege de helling van de drukdiagonaal wordt per krachtrichting bepaald hoeveel deuvels effectief zijn. Hierdoor kunnen het aantal deuvels in de berekening

Voor de berekening van de blokdeuvels zijn de masttypen als volgt samengevoegd:

- Masttype HA+0/n
- Masttype HA+5/n

De blokdeuvels worden getoetst op de maatgevende belasting per samenvoeging van masttypen (hoogste mast is maatgevend). De belastingen waaraan getoetst worden zijn onderstaand weergegeven.

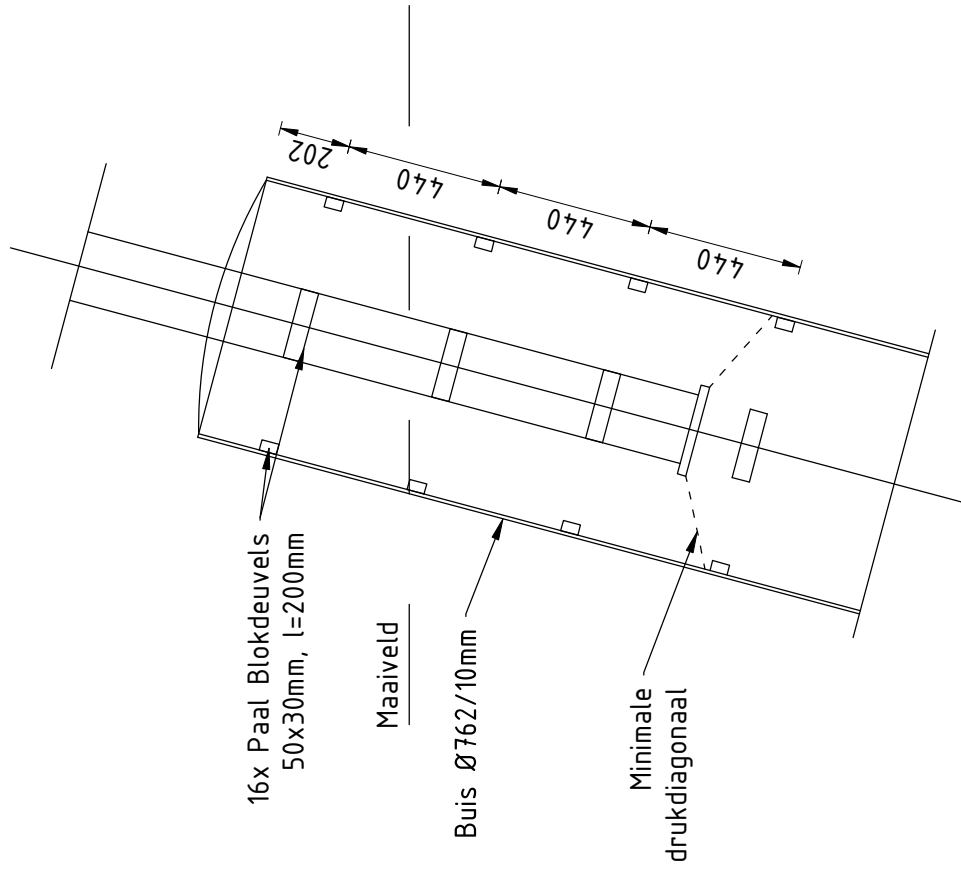
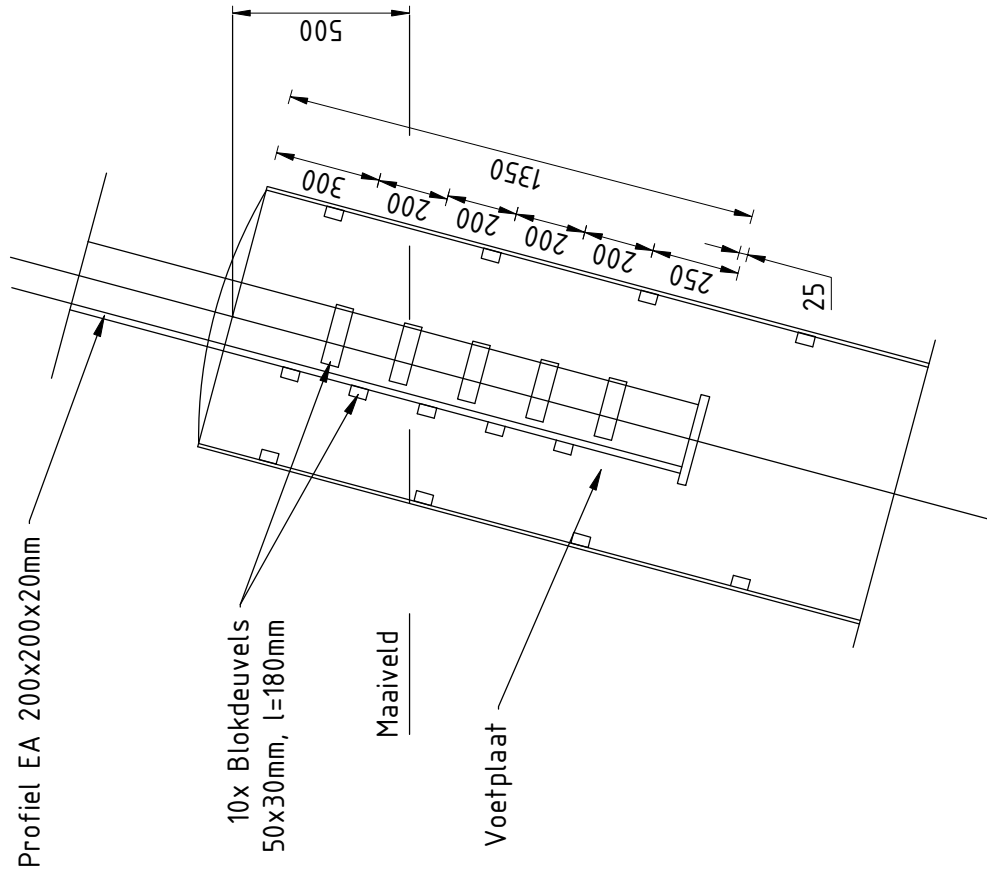
#### Masttype HA+0/n

| Omhullenden ongeacht stijl |                           | $R_x$ | $R_y$ | $R_z$        | $R_n$       | $R_E$ | $R_{E,lok}$ | $R_{z,lok}$ |
|----------------------------|---------------------------|-------|-------|--------------|-------------|-------|-------------|-------------|
| Belasting                  | Combinatie                | [kN]  | [kN]  | [kN]         | [kN]        | [kN]  | [kN]        | [kN]        |
| Max. druk                  | SPLS 3_80 Ah All Cts      | -294  | 328   | <b>1646</b>  | 24          | -440  | -76         | 1686        |
| Max. trek                  | SPLS 1a_0,9_90 Ah All Cts | -238  | 266   | <b>-1341</b> | -20         | 357   | 60          | -1373       |
| Max. pos. torsie           | SPLS 6a_90 Ah Ct1 Ba Ct1  | 125   | -128  | -29          | <b>179</b>  | 2     | -4          | -29         |
| Max. neg. torsie           | SPLS 3_80 Ba Ct1          | -157  | -100  | 139          | <b>-182</b> | -40   | -10         | 142         |
| Comb. trek+torsie          | SPLS 3_0,9_80 Ah All Cts  | -232  | 264   | <b>-1336</b> | <b>-23</b>  | 351   | 55          | -1368       |

#### Masttype HA+5/n

| Omhullenden ongeacht stijl |                           | $R_x$ | $R_y$ | $R_z$        | $R_n$       | $R_E$ | $R_{E,lok}$ | $R_{z,lok}$ |
|----------------------------|---------------------------|-------|-------|--------------|-------------|-------|-------------|-------------|
| Belasting                  | Combinatie                | [kN]  | [kN]  | [kN]         | [kN]        | [kN]  | [kN]        | [kN]        |
| Max. druk                  | SPLS 1a_90 Ah All Cts     | -296  | 317   | <b>1789</b>  | 15          | -434  | -92         | 1821        |
| Max. trek                  | SPLS 1a_0,9_90 Ah All Cts | -239  | 260   | <b>-1464</b> | -15         | 353   | 73          | -1491       |
| Max. pos. torsie           | SPLS 6a_90 Ah Ct1 Ba Ct1  | 108   | -112  | -26          | <b>156</b>  | 2     | -3          | -26         |
| Max. neg. torsie           | SPLS 3_80 Ba Ct1          | -139  | -86   | 148          | <b>-159</b> | -38   | -9          | 151         |
| Comb. trek+torsie          | SPLS 1a_0,9_90 Ah All Cts | -239  | 260   | <b>-1464</b> | <b>-15</b>  | 353   | 73          | -1491       |

# Principe blokdeuvels - HA+0+5/n 2ct



## Algemene opmerkingen

- Aarding niet aangegeven
- Spiraalwapening niet aangegeven

Project: GT-RLL  
Mast: HA+0\_n

### Shear blocks

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-07-26

Auteur: BJT

Versie: 1.4

| Load        |            |         | Results     |      |                |
|-------------|------------|---------|-------------|------|----------------|
| Compression | $F_{Ed,c}$ | 1646 kN | Compression | U.C. | 0.81 < 1,00 OK |
| Tension     | $F_{Ed,t}$ | 1341 kN | Tension     | U.C. | 0.73 < 1,00 OK |

#### Main leg

|                    |          |                      |
|--------------------|----------|----------------------|
| Profile            |          | <b>L200.20</b>       |
| Steel material     |          | S355                 |
| Cross section      |          | 7635 mm <sup>2</sup> |
| Axial capacity     | $N_{pl}$ | 2710 kN              |
| Width              | b        | 200 mm               |
| Thickness          | t        | 20 mm                |
| Length in concrete |          | 1350 mm              |

#### Capacity shear blocks main leg

|  |   |                        |
|--|---|------------------------|
| $A_{f1}$                                     | = | 5100 mm <sup>2</sup>   |
| $A_{f2}$                                     | = | 13800 mm <sup>2</sup>  |
| Slope  |   | 1: 5                   |
| $C_A = \sqrt{A_{f2}/A_{f1}}$                 | = | 1.64                   |
| $f_{jd} = C_A \times f_{cd}$                 | = | 26.3 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd}$ | = | 1074 kN                |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd}$ | = | 1074 kN                |

#### Shear blocks main leg

|                    |       |        |
|--------------------|-------|--------|
| Width              | b     | 50 mm  |
| Thickness          | h     | 30 mm  |
| Length             | L     | 170 mm |
| Welds              | a     | 5 mm   |
| c.t.c. separation  | s     | 200 mm |
| Number for compr.  | $n_c$ | 8 -    |
| Number for tension | $n_t$ | 8 -    |

#### Capacity foot plate

|                                       |   |                        |
|---------------------------------------|---|------------------------|
| $k_d$                                 | = | 1.73 -                 |
| $f_{jd} = C_A \times f_{cd}$          | = | 27.7 N/mm <sup>2</sup> |
| $c = t\sqrt{(f_{yd} / 3f_{jd})}$      | = | 53 mm                  |
| $m^* = \min(c, m)$                    | = | 30 mm                  |
| Type foot plate                       |   | Extending              |
| Effective for                         |   | Compr. and tension     |
| $A_{p,c}$                             | = | 35235 mm <sup>2</sup>  |
| $F_{Rd,c} = A_{p,druk} \times f_{jd}$ | = | 976 kN                 |
| $A_{p,t}$                             | = | 27600 mm <sup>2</sup>  |
| $F_{Rd,t} = A_{p,t} \times f_{jd}$    | = | 765 kN                 |

#### Foot plate

|             |   |       |
|-------------|---|-------|
| Thickness   | t | 25 mm |
| Ext. length | m | 30 mm |
| Welds       | a | 5 mm  |

#### Pile

|                   |  |                       |
|-------------------|--|-----------------------|
| Name              |  | Buispaal              |
| Diameter          |  | 762 mm                |
| Thickness         |  | 10 mm                 |
| Cross section     |  | 23625 mm <sup>2</sup> |
| Steel material    |  | S355                  |
| Capacity          |  | 8387 kN               |
| Concrete strength |  | C30/37                |

#### Capacities

|   |   |                |
|---|---|----------------|
| $F_{Rd,c,plate}$                                    | = | 956 kN         |
| $F_{Rd,blocks,c}$                                   | = | 1074 kN        |
| $F_{Rd,c} = F_{Rd,block} + F_{Rd,footplate}$        | = | <b>2029 kN</b> |
| U.C. compression                                    |   | 0.81 < 1,00 OK |
| Welds foot plate (see next page)                    |   | 956 kN         |
| $F_{Rd,t} = \min(\text{welds} / \text{foot plate})$ | = | 765 kN         |
| $F_{Rd,blocks,t}$                                   | = | 1074 kN        |
| $F_{Rd,t} = F_{Rd,block} + F_{Rd,footplate}$        | = | <b>1839 kN</b> |
| U.C. tension  |   | 0.73 < 1,00 OK |
| U.C. welds  |   | 0.48 < 1,00 OK |

#### Shear blocks pile

|                    |       |        |
|--------------------|-------|--------|
| Width              | b     | 50 mm  |
| Thickness          | h     | 30 mm  |
| Length             | L     | 200 mm |
| Welds              | a     | 5 mm   |
| c.t.c. separation  | s     | 520 mm |
| Number for compr.  | $n_c$ | 16 -   |
| Number for tension | $n_t$ | 16 -   |

#### Capacity shear blocks pile

|  |   |                        |
|--|---|------------------------|
| $A_{f1}$                                     | = | 6000 mm <sup>2</sup>   |
| $A_{f2}$                                     | = | 18000 mm <sup>2</sup>  |
| $C_A = \sqrt{A_{f2}/A_{f1}}$                 | = | 1.73 -                 |
| $f_{jd} = k_d \times f_{cd}$                 | = | 27.7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd}$ | = | <b>2660 kN</b>         |
| U.C. compression                             |   | 0.62 < 1,00 OK         |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd}$ | = | <b>2660 kN</b>         |
| U.C. tension                                 |   | 0.50 < 1,00 OK         |
| U.C. welds                                   |   | 0.42 < 1,00 OK         |

#### Design value concrete strength

|                  |            |                        |
|------------------|------------|------------------------|
| Material factor  | $\gamma_c$ | 1.5                    |
| Add. mat. factor | $\gamma_m$ | 1.25 -                 |
| $f_{cd} =$       |            | 16.0 N/mm <sup>2</sup> |

#### Steel tower stub

|                  |            |                       |
|------------------|------------|-----------------------|
| Yield strength   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Tensile strength | $f_{ud} =$ | 490 N/mm <sup>2</sup> |

#### "Splitting" of pile

|                       |            |                       |
|-----------------------|------------|-----------------------|
| Spread of forces      |            | 45 °                  |
| Length force flow     |            | 979 mm                |
| Splitting force       |            | 685 kN/m              |
| Yield strength wall   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Capacity tubular pile |            | 7100 kN/m             |
| U.C.                  |            | 0.10 < 1,00 OK        |

Project: GT-RLL  
Mast: HA+0\_n

### Welds of shear blocks of main leg

Out-of-plane loading

#### Plate

t = 50 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

#### Member forces

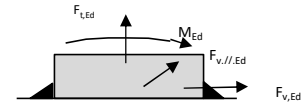
Factor 1.2  
F<sub>t,Ed</sub> = 0 kN  
F<sub>v,Ed</sub> = F<sub>Rd,c</sub> / n = 161 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 2.42 kNm

#### Check

σ<sub>w,Ed</sub> = 207 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 104 N/mm<sup>2</sup> ≤

#### Welds

a = 5 mm  
l = 170 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



#### Stress components

σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 4al = 0 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 4al = 67 N/mm<sup>2</sup>  
-----  
67 N/mm<sup>2</sup>  
b\* = b + 2/3av<sub>2</sub> = 54.7 mm  
σ<sub>1</sub> = τ<sub>1</sub> = 0,706M<sub>Ed</sub> / al b\* = 37 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>w,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 207 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.48 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.29 OK

### Welds of shear blocks of pile

Out-of-plane loading

#### Plate

t = 50 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

#### Member forces

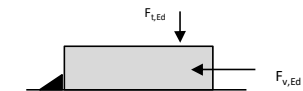
Factor 1.2  
F<sub>t,Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 60 kN  
F<sub>v,Ed</sub> = 200 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 0.00 kNm

#### Check

σ<sub>w,Ed</sub> = 183 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 92 N/mm<sup>2</sup> ≤

#### Welds

a = 5 mm  
l = 200 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



#### Stress components

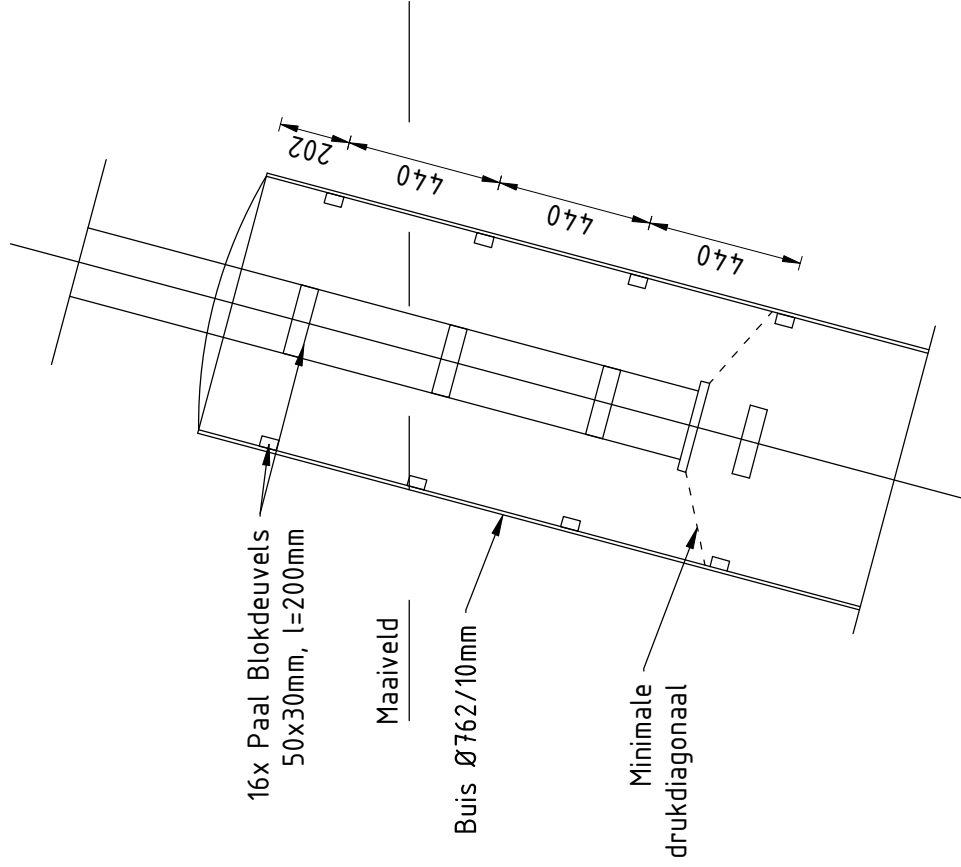
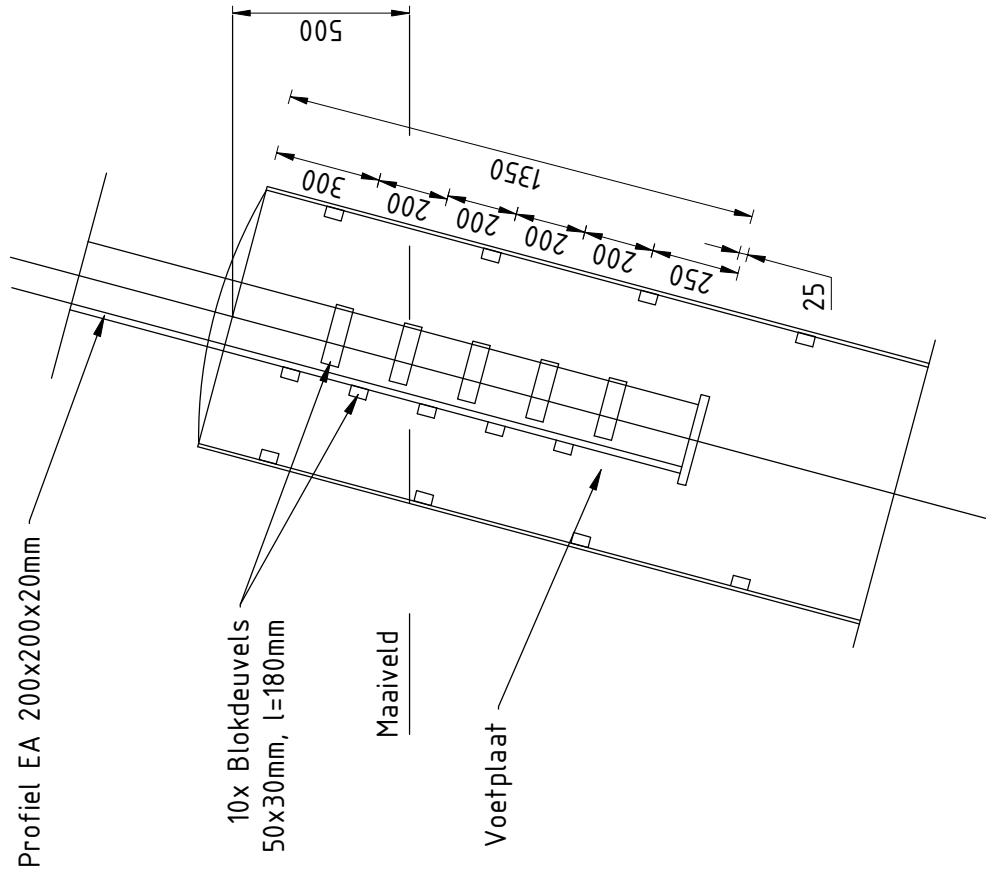
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 2al = 21 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 2al = 71 N/mm<sup>2</sup>  
-----  
92 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>w,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 183 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.42 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.26 OK

### Welds of foot plate

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup>  
Weld size a = 5 mm  
Length l = 2b + 2b - t = 760 mm  
Capacity F<sub>Rd</sub> = a x l x f<sub>w,d</sub> / √3 = 956 kN

# Principe blokdeuvels - HA+0+5/n 2ct



## Algemene opmerkingen

- Aarding niet aangegeven
- Spiraalwapening niet aangegeven

Project: GT-RLL  
Mast: HA+5\_n

### Shear blocks

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-07-26

Auteur: BJT

Versie: 1.4

| Load        |            |         | Results     |      |                |
|-------------|------------|---------|-------------|------|----------------|
| Compression | $F_{Ed,c}$ | 1789 kN | Compression | U.C. | 0.88 < 1,00 OK |
| Tension     | $F_{Ed,t}$ | 1464 kN | Tension     | U.C. | 0.80 < 1,00 OK |

#### Main leg

|                    |          |                      |
|--------------------|----------|----------------------|
| Profile            |          | <b>L200.20</b>       |
| Steel material     |          | S355                 |
| Cross section      |          | 7635 mm <sup>2</sup> |
| Axial capacity     | $N_{pl}$ | 2710 kN              |
| Width              | $b$      | 200 mm               |
| Thickness          | $t$      | 20 mm                |
| Length in concrete |          | 1350 mm              |

#### Capacity shear blocks main leg

|  |   |                        |
|--|---|------------------------|
| $A_{f1}$                                     | = | 5100 mm <sup>2</sup>   |
| $A_{f2}$                                     | = | 13800 mm <sup>2</sup>  |
| Slope  |   | 1 : 5                  |
| $C_A = \sqrt{A_{f2}/A_{f1}}$                 | = | 1.64                   |
| $f_{jd} = C_A \times f_{cd}$                 | = | 26.3 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd}$ | = | 1074 kN                |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd}$ | = | 1074 kN                |

#### Shear blocks main leg

|                    |       |        |
|--------------------|-------|--------|
| Width              | $b$   | 50 mm  |
| Thickness          | $h$   | 30 mm  |
| Length             | $L$   | 170 mm |
| Welds              | $a$   | 5 mm   |
| c.t.c. separation  | $s$   | 200 mm |
| Number for compr.  | $n_c$ | 8 -    |
| Number for tension | $n_t$ | 8 -    |

#### Capacity foot plate

|                                       |   |                        |
|---------------------------------------|---|------------------------|
| $k_d$                                 | = | 1.73 -                 |
| $f_{jd} = C_A \times f_{cd}$          | = | 27.7 N/mm <sup>2</sup> |
| $c = t\sqrt{(f_{yd} / 3f_{jd})}$      | = | 53 mm                  |
| $m^* = \min(c, m)$                    | = | 30 mm                  |
| Type foot plate                       |   | Extending              |
| Effective for                         |   | Compr. and tension     |
| $A_{p,c}$                             | = | 35235 mm <sup>2</sup>  |
| $F_{Rd,c} = A_{p,druk} \times f_{jd}$ | = | 976 kN                 |
| $A_{p,t}$                             | = | 27600 mm <sup>2</sup>  |
| $F_{Rd,t} = A_{p,t} \times f_{jd}$    | = | 765 kN                 |

#### Foot plate

|             |     |       |
|-------------|-----|-------|
| Thickness   | $t$ | 25 mm |
| Ext. length | $m$ | 30 mm |
| Welds       | $a$ | 5 mm  |

#### Pile

|                   |  |                       |
|-------------------|--|-----------------------|
| Name              |  | Buispaal              |
| Diameter          |  | 762 mm                |
| Thickness         |  | 10 mm                 |
| Cross section     |  | 23625 mm <sup>2</sup> |
| Steel material    |  | S355                  |
| Capacity          |  | 8387 kN               |
| Concrete strength |  | C30/37                |

#### Capacities

|   |   |                |
|---|---|----------------|
| $F_{Rd,c,plate}$                                      | = | 956 kN         |
| $F_{Rd,blocks,c}$                                     | = | 1074 kN        |
| $F_{Rd,c} = F_{Rd,block} + F_{Rd,footplate}$          | = | <b>2029 kN</b> |
| U.C. compression                                      |   | 0.88 < 1,00 OK |
| Welds foot plate (see next page)                      |   | 956 kN         |
| $F_{Rd,t} = \min. (\text{welds} / \text{foot plate})$ | = | 765 kN         |
| $F_{Rd,blocks,t}$                                     | = | 1074 kN        |
| $F_{Rd,t} = F_{Rd,block} + F_{Rd,footplate}$          | = | <b>1839 kN</b> |
| U.C. tension  |   | 0.80 < 1,00 OK |
| U.C. welds  |   | 0.48 < 1,00 OK |

#### Shear blocks pile

|                    |       |        |
|--------------------|-------|--------|
| Width              | $b$   | 50 mm  |
| Thickness          | $h$   | 30 mm  |
| Length             | $L$   | 200 mm |
| Welds              | $a$   | 5 mm   |
| c.t.c. separation  | $s$   | 520 mm |
| Number for compr.  | $n_c$ | 16 -   |
| Number for tension | $n_t$ | 16 -   |

#### Capacity shear blocks pile

|  |   |                        |
|--|---|------------------------|
| $A_{f1}$                                     | = | 6000 mm <sup>2</sup>   |
| $A_{f2}$                                     | = | 18000 mm <sup>2</sup>  |
| $C_A = \sqrt{A_{f2}/A_{f1}}$                 | = | 1.73 -                 |
| $f_{jd} = k_d \times f_{cd}$                 | = | 27.7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd}$ | = | <b>2660 kN</b>         |
| U.C. compression                             |   | 0.67 < 1,00 OK         |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd}$ | = | <b>2660 kN</b>         |
| U.C. tension                                 |   | 0.55 < 1,00 OK         |
| U.C. welds                                   |   | 0.42 < 1,00 OK         |

#### Design value concrete strength

|                  |            |                        |
|------------------|------------|------------------------|
| Material factor  | $\gamma_c$ | 1.5                    |
| Add. mat. factor | $\gamma_m$ | 1.25 -                 |
| $f_{cd} =$       |            | 16.0 N/mm <sup>2</sup> |

#### Steel tower stub

|                  |          |                       |
|------------------|----------|-----------------------|
| Yield strength   | $f_{yd}$ | 355 N/mm <sup>2</sup> |
| Tensile strength | $f_{ud}$ | 490 N/mm <sup>2</sup> |

#### "Splitting" of pile

|                       |            |                       |
|-----------------------|------------|-----------------------|
| Spread of forces      |            | 45 °                  |
| Length force flow     |            | 979 mm                |
| Splitting force       |            | 748 kN/m              |
| Yield strength wall   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Capacity tubular pile |            | 7100 kN/m             |
| U.C.                  |            | 0.11 < 1,00 OK        |



Project: GT-RLL  
Mast: HA+5\_n

### Welds of shear blocks of main leg

Out-of-plane loading

#### Plate

t = 50 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

#### Member forces

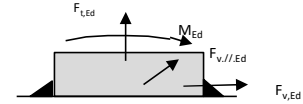
Factor 1.2  
F<sub>t,Ed</sub> = 0 kN  
F<sub>v,Ed</sub> = F<sub>rd,c</sub> / n = 161 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 2.42 kNm

#### Check

σ<sub>wv,Ed</sub> = 207 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 104 N/mm<sup>2</sup> ≤

#### Welds

a = 5 mm  
l = 170 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



#### Stress components

σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 4al = 0 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 4al = 67 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 4al = 67 N/mm<sup>2</sup>  
b\* = b + 2/3av<sup>2</sup> = 54.7 mm  
σ<sub>1</sub> = τ<sub>1</sub> = 0,706M<sub>Ed</sub> / al b\* = 37 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>wv,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 207 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.48 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.29 OK

### Welds of shear blocks of pile

Out-of-plane loading

#### Plate

t = 50 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

#### Member forces

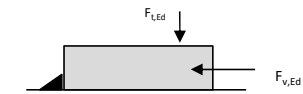
Factor 1.2  
F<sub>t,Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 60 kN  
F<sub>v,Ed</sub> = 200 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 0.00 kNm

#### Check

σ<sub>wv,Ed</sub> = 183 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 92 N/mm<sup>2</sup> ≤

#### Welds

a = 5 mm  
l = 200 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



#### Stress components

σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 2al = 21 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 2al = 71 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 2al = 71 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>wv,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 183 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.42 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.26 OK

### Welds of foot plate

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup>  
Weld size a = 5 mm  
Length l = 2b + 2b - t = 760 mm  
Capacity F<sub>Rd</sub> = a x l x f<sub>w,d</sub> / √3 = 956 kN



## **APPENDIX E**

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### **Liggers**

Niet van toepassing voor dit masttype.

## APPENDIX F

### Galloping

#### Uitgangspunten

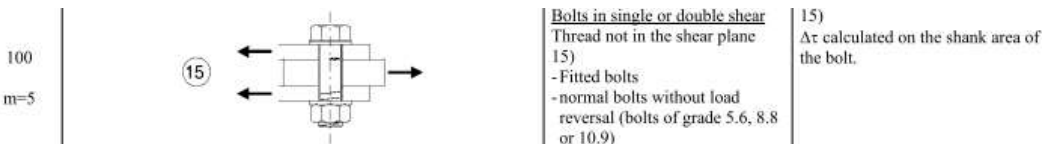
In het uitgangspuntendocument is beschreven dat wordt uitgegaan van een materiaalfactor voor vermoeiing  $\gamma_{mf} = 1,15$ . Dit komt overeen met de “Safe-life methode” met “Low consequence” van tabel 3.1 van NEN-EN 1993-1-9 of met “Damage tolerant” en “High consequence”.

| Assessment method | Consequence of failure |                  |
|-------------------|------------------------|------------------|
|                   | Low consequence        | High consequence |
| Damage tolerant   | 1,00                   | 1,15             |
| Safe life         | 1,15                   | 1,35             |

Voor staven met gatverzwakking met bouten in ruime gaten geldt volgens fig. 8.1 van NEN-EN 1993-1-9 categorie 50, met  $m=3$



Voor niet voorgespannen bouten belast op afschuiving geldt volgens fig. 8.1 van NEN-EN 1993-1-9 categorie 100, met  $m=5$ .



Het belastingspectrum is in de NNA (NEN-EN 50341-2-15) als volgt gedefinieerd.

**Table 4.11/NL.1 Load spectra line galloping for tension supports**

| Load spectra line galloping for tension supports |                   | Number of load cycles in 50 years |              |
|--|-------------------|-----------------------------------|--------------|
| Number   | Peak-to-peak load | Ice region A                      | Ice region B |
| 1  | 2·EDS             | 7.000                             | 3.000        |
| 2  | 1,5·EDS           | 36.000                            | 17.000       |
| 3  | 1,0·EDS           | 125.000                           | 65.000       |
| 4  | 0,5·EDS           | 482.000                           | 265.000      |

#### Aanpak

De vier belastingen van 0,5 tot 2,0EDS hebben een vaste onderlinge verhouding. Aangezien het aantal wisselingen zich in het  $m=3$  gebied van de vermoeiingskromme bevindt vanwege  $n < 2 \times 10^6$ , kan een relatie worden afgeleid tussen de grootte van de spanningswissel met bijvoorbeeld 1,0EDS en de spanningswisseling die bij  $2 \times 10^6$  wisselingen op basis van het spectrum nog net toelaatbaar is. Dit staat bekend als de equivalente spanningen methode. Via de factor lambda kan de spanningswisseling worden berekend.

$$\lambda = \left[ \frac{\sum \Delta\sigma_i^m \cdot n_i}{2 \cdot 10^6} \right]^{\frac{1}{m}}$$

Toepassen van de formule voor een spanning van 1 N/mm<sup>2</sup> bij 1,0EDS levert:

| Helling<br>Ijsgebied<br>Wisseling                       | m=3                     |                         | m=5                     |                         |
|---|-------------------------|-------------------------|-------------------------|-------------------------|
|   | A                       | B                       | A                       | B                       |
|   | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ |
| 2,0EDS  | 5,60E+04                | 2,40E+04                | 2,24E+05                | 9,60E+04                |
| 1,5EDS  | 1,22E+05                | 5,74E+04                | 2,73E+05                | 1,29E+05                |
| 1,0EDS  | 1,25E+05                | 6,50E+04                | 1,25E+05                | 6,50E+04                |
| 0,5EDS  | 6,03E+04                | 3,31E+04                | 1,51E+04                | 8,28E+03                |
| $\Sigma \sigma_i^m \times n_i$                          | 3,63E+05                | 1,80E+05                | 6,37E+05                | 2,98E+05                |
| $\lambda = (\Sigma \sigma_i n_i / 2 \times 10^6)^{1/m}$ | 0,57                    | 0,45                    | 0,80                    | 0,68                    |

Voor ijsgebied A is de toelaatbare spanningswisseling bij 1,0 EDS en 125.000 wisselingen dus 1/0,57 (175%) van de toelaatbare spanningswisseling bij een aantal wisselingen van  $2,0 \times 10^6$ . Er kan ook worden gesteld dat als de spanningswisselingen van 1,0 EDS 363.000 maal voorkomen, dezelfde schade wordt behaald als de vier niveaus afzonderlijk. Deze aanpak is gehanteerd.

- In de berekening van de mast wordt telkens één afspanpunt van de geleiders belast met een trekkracht in lijnrichting van 1,0 EDS.
- Het aantal wisselingen dat deze trekkracht voorkomt wordt vergroot om het hele spectrum te vervangen, dit is afhankelijk van ijsgebied en m-factor.
- Voor iedere staaf in de constructie wordt de schade berekend als gevolg van de trekkracht voor elke geleider.
- De schade wordt gesommeerd over alle geleiders.
- De toetsing is uitgedrukt als de verhouding tussen de optredende spanningswisseling bij  $n = 2 \times 10^6$  wisselingen en de toelaatbare spanningswisseling (43 MPa voor het staalprofiel en 87 MPa voor de bout).

## Resultaten

In de tabellen zijn de resultaten van mast HA+5/n gegeven. Vanwege de exponentiële invloed van het spanningsniveau heeft de verdeling van de U.C.'s een grote variatie. Het meest zwaar belast zijn de diagonalen in het ondervlak van de traverse in de nabijheid van de afspanpunten en de randen van de traverse. De conclusie is dat de staven en bouten voldoen.



**Check galloping**

Datum: 27-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RL  
 HA\_n

| Group | Omschrijving                    | Profiel    | Aantal<br>bouten | Bout | Controle netto oppervlak profiel |                 |                |               |               |                 |            |              |                       |                 | Controle boutdoorsnede |                 |            |  |  |  |
|-------|---------------------------------|------------|------------------|------|----------------------------------|-----------------|----------------|---------------|---------------|-----------------|------------|--------------|-----------------------|-----------------|------------------------|-----------------|------------|--|--|--|
|       |                                 |            |                  |      | DF;o<br>[kN]                     | Brutto<br>[mm2] | Netto<br>[mm2] | Δσ;i<br>[Mpa] | DC;o<br>[Mpa] | Δσ;c;o<br>[Mpa] | UC<br>opp. | DF;b<br>[kN] | Opp.<br>Bout<br>[mm2] | Δσ;i;b<br>[Mpa] | DC;b<br>[Mpa]          | Δσ;c;b<br>[Mpa] | UC<br>bout |  |  |  |
| 100A  | BVNSTK - Main member            | 120x120x12 | 0                | 0    | 11,0                             | 2750            | 2750           | 4,0           | 50            | 43              | 0,09       | 16,5         | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 100B  | BVNSTK - Main member            | 120x120x12 | 6                | M24  | 22,5                             | 2750            | 2438           | 9,2           | 50            | 43              | 0,21       | 32,7         | 452                   | 12,0            | 100                    | 87              | 0,14       |  |  |  |
| 101   | BVNSTK - Horizontal front       | 160x160x15 | 10               | M24  | 79,9                             | 4671            | 4281           | 18,7          | 50            | 43              | 0,43       | 116,5        | 452                   | 25,8            | 100                    | 87              | 0,30       |  |  |  |
| 102A  | Derde TSNSTK - Main member      | 160x160x15 | 6                | M24  | 44,7                             | 4671            | 4281           | 10,4          | 50            | 43              | 0,24       | 65,4         | 452                   | 24,1            | 100                    | 87              | 0,28       |  |  |  |
| 102B  | Derde TSNSTK - Main member      | 160x160x15 | 8                | M24  | 53,0                             | 4671            | 4281           | 12,4          | 50            | 43              | 0,28       | 75,2         | 452                   | 20,8            | 100                    | 87              | 0,24       |  |  |  |
| 103   | Derde TSNSTK - Horizontal front | 180x180x16 | 13               | M24  | 83,9                             | 5540            | 5124           | 16,4          | 50            | 43              | 0,38       | 122,0        | 452                   | 20,8            | 100                    | 87              | 0,24       |  |  |  |
| 104   | BRKSTK - Main member            | 200x200x20 | 12               | M24  | 109,1                            | 7640            | 7120           | 15,3          | 50            | 43              | 0,35       | 132,8        | 452                   | 24,5            | 100                    | 87              | 0,28       |  |  |  |
| 105A  | Eerste TSNSTK - Main member     | 200x200x20 | 12               | M24  | 108,9                            | 7640            | 7120           | 15,3          | 50            | 43              | 0,35       | 132,6        | 452                   | 24,5            | 100                    | 87              | 0,28       |  |  |  |
| 105B  | Eerste TSNSTK - Main member     | 200x200x20 | 12               | M24  | 108,8                            | 7640            | 7120           | 15,3          | 50            | 43              | 0,35       | 135,1        | 452                   | 24,9            | 100                    | 87              | 0,29       |  |  |  |
| 106A  | Tweede TSNSTK - Main member     | 200x200x18 | 10               | M24  | 92,9                             | 6910            | 6442           | 14,4          | 50            | 43              | 0,33       | 119,9        | 452                   | 26,5            | 100                    | 87              | 0,31       |  |  |  |
| 106B  | Tweede TSNSTK - Main member     | 200x200x18 | 10               | M24  | 91,0                             | 6910            | 6442           | 14,1          | 50            | 43              | 0,32       | 121,1        | 452                   | 26,8            | 100                    | 87              | 0,31       |  |  |  |
| 106C  | Tweede TSNSTK - Main member     | 200x200x18 | 10               | M24  | 75,3                             | 6910            | 6442           | 11,7          | 50            | 43              | 0,27       | 104,1        | 452                   | 23,0            | 100                    | 87              | 0,26       |  |  |  |
| 107A  | Eerste DWSRM - Main member bc   | 160x160x15 | 10               | M24  | 128,9                            | 4671            | 4281           | 30,1          | 50            | 43              | 0,69       | 189,9        | 452                   | 42,0            | 100                    | 87              | 0,48       |  |  |  |
| 107B  | Eerste DWSRM - Main member bc   | 180x180x16 | 8                | M24  | 99,5                             | 5540            | 5124           | 19,4          | 50            | 43              | 0,45       | 151,9        | 452                   | 42,0            | 100                    | 87              | 0,48       |  |  |  |
| 107C  | Eerste DWSRM - Main member bc   | 160x160x15 | 8                | M24  | 123,6                            | 4671            | 4671           | 26,5          | 50            | 43              | 0,61       | 183,8        | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 108A  | Eerste DWSRM - Main member bc   | 150x150x12 | 8                | M24  | 93,9                             | 3480            | 3168           | 29,7          | 50            | 43              | 0,68       | 143,4        | 452                   | 39,7            | 100                    | 87              | 0,46       |  |  |  |
| 108C  | Eerste DWSRM - Main member bc   | 150x150x12 | 0                | 0    | 89,6                             | 3480            | 3480           | 25,8          | 50            | 43              | 0,59       | 136,8        | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 109A  | Eerste DWSRM - Main member to   | 110x110x10 | 4                | M24  | 13,4                             | 2112            | 1852           | 7,3           | 50            | 43              | 0,17       | 20,0         | 452                   | 11,1            | 100                    | 87              | 0,13       |  |  |  |
| 109B  | Eerste DWSRM - Main member to   | 110x110x10 | 4                | M24  | 12,8                             | 2112            | 1852           | 6,9           | 50            | 43              | 0,16       | 19,2         | 452                   | 10,6            | 100                    | 87              | 0,12       |  |  |  |
| 110A  | Eerste DWSRM - Main member to   | 100x100x8  | 4                | M24  | 12,7                             | 1550            | 1342           | 9,4           | 50            | 43              | 0,22       | 19,2         | 452                   | 10,6            | 100                    | 87              | 0,12       |  |  |  |
| 110B  | Eerste DWSRM - Main member to   | 100x100x8  | 0                | 0    | 12,6                             | 1550            | 1550           | 8,1           | 50            | 43              | 0,19       | 19,1         | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 111A  | Tweede DWSRM - Main member t    | 150x150x12 | 8                | M24  | 90,9                             | 3480            | 3168           | 28,7          | 50            | 43              | 0,66       | 138,7        | 452                   | 38,4            | 100                    | 87              | 0,44       |  |  |  |
| 111C  | Tweede DWSRM - Main member t    | 150x150x12 | 0                | 0    | 85,9                             | 3480            | 3480           | 24,7          | 50            | 43              | 0,57       | 131,1        | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 112A  | Tweede DWSRM - Main member t    | 100x100x8  | 0                | 0    | 4,4                              | 1550            | 1550           | 2,8           | 50            | 43              | 0,07       | 6,5          | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 112B  | Tweede DWSRM - Main member t    | 100x100x8  | 2                | M24  | 3,5                              | 1550            | 1342           | 2,6           | 50            | 43              | 0,06       | 5,3          | 452                   | 5,9             | 100                    | 87              | 0,07       |  |  |  |
| 113A  | Tweede DWSRM - Main member t    | 120x120x10 | 4                | M24  | 47,8                             | 2320            | 2060           | 23,2          | 50            | 43              | 0,53       | 66,0         | 452                   | 36,5            | 100                    | 87              | 0,42       |  |  |  |
| 113B  | Tweede DWSRM - Main member t    | 120x120x10 | 4                | M24  | 41,1                             | 2320            | 2060           | 20,0          | 50            | 43              | 0,46       | 57,8         | 452                   | 31,9            | 100                    | 87              | 0,37       |  |  |  |
| 113C  | Tweede DWSRM - Main member t    | 120x120x10 | 0                | 0    | 45,1                             | 2320            | 2320           | 19,4          | 50            | 43              | 0,45       | 63,3         | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 114A  | Tweede DWSRM - Main member t    | 120x120x10 | 4                | M24  | 39,4                             | 2320            | 2060           | 19,1          | 50            | 43              | 0,44       | 55,4         | 452                   | 30,6            | 100                    | 87              | 0,35       |  |  |  |
| 114B  | Tweede DWSRM - Main member t    | 120x120x10 | 5                | M24  | 6,5                              | 2320            | 2060           | 3,2           | 50            | 43              | 0,07       | 9,2          | 452                   | 4,0             | 100                    | 87              | 0,05       |  |  |  |
| 114C  | Tweede DWSRM - Main member t    | 120x120x10 | 0                | 0    | 35,2                             | 2320            | 2320           | 15,2          | 50            | 43              | 0,35       | 49,5         | 0                     | 0,0             | 100                    | 87              | 0,00       |  |  |  |
| 200   | BVNSTK - Top cap                | 80x80x6    | 2                | M16  | 8,4                              | 940             | 832            | 10,1          | 50            | 43              | 0,23       | 11,7         | 201                   | 29,2            | 100                    | 87              | 0,34       |  |  |  |
| 201L  | BVNSTK - Horizontal front       | 100x100x10 | 3                | M24  | 13,7                             | 1920            | 1660           | 8,3           | 50            | 43              | 0,19       | 19,1         | 452                   | 14,1            | 100                    | 87              | 0,16       |  |  |  |
| 201T  | BVNSTK - Horizontal side        | 80x80x6    | 2                | M20  | 0,6                              | 940             | 808            | 0,8           | 50            | 43              | 0,02       | 0,9          | 314                   | 1,4             | 100                    | 87              | 0,02       |  |  |  |
| 202L  | BVNSTK - CD front               | 100x100x8  | 2                | M24  | 13,4                             | 1550            | 1342           | 10,0          | 50            | 43              | 0,23       | 19,2         | 452                   | 21,2            | 100                    | 87              | 0,24       |  |  |  |



**Check galloping**

Datum: 27-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RL  
 HA\_n

| Group | Omschrijving                           | Profiel    | Aantal<br>bouten | Bout | Controle netto oppervlak profiel |                 |                |               |               |                 |            |              |               |              | Controle boutdoorsnede |               |                 |            |  |
|-------|--|------------|------------------|------|----------------------------------|-----------------|----------------|---------------|---------------|-----------------|------------|--------------|---------------|--------------|------------------------|---------------|-----------------|------------|--|
|       |  |            |                  |      | ΔF;o<br>[kN]                     | Brutto<br>[mm2] | Netto<br>[mm2] | Δσ;o<br>[Mpa] | DC;o<br>[Mpa] | Δσ;c;o<br>[Mpa] | UC<br>opp. | ΔF;b<br>[kN] | Bout<br>[mm2] | Opp.<br>Bout | Δσ;i;b<br>[Mpa]        | DC;b<br>[Mpa] | Δσ;c;b<br>[Mpa] | UC<br>bout |  |
| 202T  | BVNSTK - CD side                       | 80x80x8    | 2                | M24  | 8,6                              | 1230            | 1022           | 8,4           | 50            | 43              | 0,19       | 12,2         | 452           | 13,5         | 100                    | 87            | 0,16            |            |  |
| 203T  | BVNSTK - Horizontal side               | 100x100x10 | 5                | M20  | 29,5                             | 1920            | 1700           | 17,4          | 50            | 43              | 0,40       | 40,2         | 314           | 25,6         | 100                    | 87            | 0,29            |            |  |
| 204L  | BVNSTK - CD front                      | 130x130x12 | 3                | M24  | 66,8                             | 3000            | 2688           | 24,8          | 50            | 43              | 0,57       | 92,1         | 452           | 68,0         | 100                    | 87            | 0,78            |            |  |
| 204T  | BVNSTK - CD side                       | 130x130x12 | 3                | M24  | 65,6                             | 3000            | 2688           | 24,4          | 50            | 43              | 0,56       | 94,2         | 452           | 69,5         | 100                    | 87            | 0,80            |            |  |
| 205   | BVNSTK - Diagonal for crossarm         | 120x120x12 | 4                | M24  | 39,5                             | 2750            | 2438           | 16,2          | 50            | 43              | 0,37       | 53,6         | 452           | 29,6         | 100                    | 87            | 0,34            |            |  |
| 206   | BVNSTK - CD for crossarm diaphragm     | 50x50x5    | 1                | M16  | 0,0                              | 480             | 390            | 0,0           | 50            | 43              | 0,00       | 0,0          | 201           | 0,1          | 100                    | 87            | 0,00            |            |  |
| 207L  | Derde TSNSTK - CD front                | 130x130x12 | 3                | M24  | 60,9                             | 3000            | 2688           | 22,6          | 50            | 43              | 0,52       | 83,9         | 452           | 61,9         | 100                    | 87            | 0,71            |            |  |
| 207T  | Derde TSNSTK - CD side                 | 130x130x12 | 3                | M24  | 59,8                             | 3000            | 2688           | 22,2          | 50            | 43              | 0,51       | 85,8         | 452           | 63,3         | 100                    | 87            | 0,73            |            |  |
| 208L  | Derde TSNSTK - Horizontal front        | 120x120x10 | 4                | M24  | 8,7                              | 2320            | 2060           | 4,2           | 50            | 43              | 0,10       | 10,6         | 452           | 5,9          | 100                    | 87            | 0,07            |            |  |
| 208T  | Derde TSNSTK - Horizontal side         | 120x120x10 | 4                | M24  | 2,1                              | 2320            | 2060           | 1,0           | 50            | 43              | 0,02       | 3,1          | 452           | 1,7          | 100                    | 87            | 0,02            |            |  |
| 209L  | Derde TSNSTK - CD front                | 130x130x12 | 3                | M24  | 51,4                             | 3000            | 2688           | 19,1          | 50            | 43              | 0,44       | 74,4         | 452           | 54,9         | 100                    | 87            | 0,63            |            |  |
| 209T  | Derde TSNSTK - CD side                 | 130x130x12 | 3                | M24  | 54,0                             | 3000            | 2688           | 20,1          | 50            | 43              | 0,46       | 78,1         | 452           | 57,6         | 100                    | 87            | 0,66            |            |  |
| 210T  | Derde TSNSTK - Horizontal side         | 120x120x10 | 6                | M20  | 32,3                             | 2320            | 2100           | 15,4          | 50            | 43              | 0,35       | 43,5         | 314           | 23,1         | 100                    | 87            | 0,27            |            |  |
| 211   | Derde TSNSTK - Diagonal for crossarm   | 130x130x12 | 4                | M24  | 44,2                             | 3000            | 2688           | 16,4          | 50            | 43              | 0,38       | 59,7         | 452           | 33,0         | 100                    | 87            | 0,38            |            |  |
| 212   | Derde TSNSTK - CD for crossarm         | 55x55x6    | 1                | M16  | 0,0                              | 600             | 492            | 0,1           | 50            | 43              | 0,00       | 0,1          | 201           | 0,3          | 100                    | 87            | 0,00            |            |  |
| 213L  | BRKSTK - Main diagonal                 | 150x150x14 | 4                | M24  | 37,4                             | 4014            | 3650           | 10,2          | 50            | 43              | 0,24       | 47,0         | 452           | 26,0         | 100                    | 87            | 0,30            |            |  |
| 213T  | BRKSTK - Main diagonal                 | 150x150x14 | 4                | M24  | 37,3                             | 4014            | 3650           | 10,2          | 50            | 43              | 0,23       | 46,4         | 452           | 25,7         | 100                    | 87            | 0,30            |            |  |
| 214L  | BRKSTK - Diaphragm horizontal          | 120x120x10 | 2                | M24  | 0,4                              | 2320            | 2060           | 0,2           | 50            | 43              | 0,00       | 0,5          | 452           | 0,6          | 100                    | 87            | 0,01            |            |  |
| 214T  | BRKSTK - Diaphragm horizontal          | 120x120x10 | 2                | M24  | 0,5                              | 2320            | 2060           | 0,3           | 50            | 43              | 0,01       | 0,7          | 452           | 0,7          | 100                    | 87            | 0,01            |            |  |
| 215   | BRKSTK - Diaphragm diagonal            | 100x100x8  | 1                | M20  | 0,2                              | 1550            | 1374           | 0,2           | 50            | 43              | 0,00       | 0,3          | 314           | 1,0          | 100                    | 87            | 0,01            |            |  |
| 215L  | Eerste TSNSTK - First diag from bottom | 150x150x12 | 3                | M24  | 29,3                             | 3480            | 3168           | 9,2           | 50            | 43              | 0,21       | 37,4         | 452           | 27,6         | 100                    | 87            | 0,32            |            |  |
| 215T  | Eerste TSNSTK - First diag from top    | 150x150x12 | 3                | M24  | 28,6                             | 3480            | 3168           | 9,0           | 50            | 43              | 0,21       | 35,7         | 452           | 26,4         | 100                    | 87            | 0,30            |            |  |
| 216   | BRKSTK - Diaphragm CD                  | 100x100x8  | 1                | M20  | 0,0                              | 1550            | 1374           | 0,0           | 50            | 43              | 0,00       | 0,0          | 314           | 0,0          | 100                    | 87            | 0,00            |            |  |
| 216L  | Eerste TSNSTK - First CD from bottom   | 150x150x12 | 4                | M24  | 35,5                             | 3480            | 3168           | 11,2          | 50            | 43              | 0,26       | 44,8         | 452           | 24,8         | 100                    | 87            | 0,29            |            |  |
| 216T  | Eerste TSNSTK - First CD from top      | 150x150x12 | 4                | M24  | 36,0                             | 3480            | 3168           | 11,4          | 50            | 43              | 0,26       | 45,3         | 452           | 25,0         | 100                    | 87            | 0,29            |            |  |
| 217L  | Tweede TSNSTK - First CD from bottom   | 140x140x13 | 4                | M24  | 43,4                             | 3521            | 3183           | 13,6          | 50            | 43              | 0,31       | 54,8         | 452           | 30,3         | 100                    | 87            | 0,35            |            |  |
| 217T  | Tweede TSNSTK - First CD from top      | 140x140x13 | 4                | M24  | 44,0                             | 3521            | 3183           | 13,8          | 50            | 43              | 0,32       | 55,4         | 452           | 30,6         | 100                    | 87            | 0,35            |            |  |
| 218L  | Tweede TSNSTK - Second CD from bottom  | 140x140x13 | 4                | M24  | 53,1                             | 3521            | 3183           | 16,7          | 50            | 43              | 0,38       | 67,0         | 452           | 37,1         | 100                    | 87            | 0,43            |            |  |
| 218T  | Tweede TSNSTK - Second CD from top     | 140x140x13 | 4                | M24  | 53,8                             | 3521            | 3183           | 16,9          | 50            | 43              | 0,39       | 67,6         | 452           | 37,4         | 100                    | 87            | 0,43            |            |  |
| 219L  | Tweede TSNSTK - Third CD from bottom   | 140x140x13 | 5                | M24  | 64,6                             | 3521            | 3183           | 20,3          | 50            | 43              | 0,47       | 81,6         | 452           | 36,1         | 100                    | 87            | 0,42            |            |  |
| 219T  | Tweede TSNSTK - Third CD from top      | 140x140x13 | 5                | M24  | 65,5                             | 3521            | 3183           | 20,6          | 50            | 43              | 0,47       | 82,4         | 452           | 36,5         | 100                    | 87            | 0,42            |            |  |
| 300   | Eerste DWSRM CD 1 under                | 80x80x6    | 2                | M20  | 14,1                             | 940             | 808            | 17,5          | 50            | 43              | 0,40       | 19,6         | 314           | 31,3         | 100                    | 87            | 0,36            |            |  |
| 301   | Eerste DWSRM CD 2 under                | 80x80x6    | 2                | M20  | 16,5                             | 940             | 808            | 20,5          | 50            | 43              | 0,47       | 23,0         | 314           | 36,6         | 100                    | 87            | 0,42            |            |  |
| 302   | Eerste DWSRM CD 3 under                | 80x80x6    | 2                | M20  | 17,8                             | 940             | 808            | 22,0          | 50            | 43              | 0,51       | 24,7         | 314           | 39,4         | 100                    | 87            | 0,45            |            |  |
| 303   | Eerste DWSRM CD 4 under                | 80x80x6    | 2                | M20  | 19,6                             | 940             | 808            | 24,2          | 50            | 43              | 0,56       | 27,2         | 314           | 43,4         | 100                    | 87            | 0,50            |            |  |



**Check galloping**

Datum: 27-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RL  
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| Group | Omschrijving                    | Profiel                  | Aantal bouten | Bout | Controle netto oppervlak profiel |              |             |                         |                         |                         |                       |                       |                       |                         | Controle boutdoorsnede  |                         |                       |                       |                       |                 |                   |
|-------|---------------------------------|--------------------------|---------------|------|----------------------------------|--------------|-------------|-------------------------|-------------------------|-------------------------|-----------------------|-----------------------|-----------------------|-------------------------|-------------------------|-------------------------|-----------------------|-----------------------|-----------------------|-----------------|-------------------|
|       |                                 |                          |               |      | $\Delta F_o$ [kN]                | Brutto [mm2] | Netto [mm2] | $\Delta \sigma_i$ [Mpa] | $\Delta \sigma_j$ [Mpa] | $\Delta \sigma_k$ [Mpa] | DC <sub>i</sub> [Mpa] | DC <sub>j</sub> [Mpa] | DC <sub>k</sub> [Mpa] | $\Delta \sigma_i$ [Mpa] | $\Delta \sigma_j$ [Mpa] | $\Delta \sigma_k$ [Mpa] | DC <sub>i</sub> [Mpa] | DC <sub>j</sub> [Mpa] | DC <sub>k</sub> [Mpa] | Opp. Bout [mm2] | $\Delta F_o$ [kN] |
| 304   | Eerste DWSRM CD 5 onder         | 80x80x6                  | 2             | M20  | 20,6                             | 940          | 808         | 25,5                    | 50                      | 43                      | 0,59                  | 28,6                  | 314                   | 45,6                    | 100                     | 87                      | 0,52                  | 87                    | 0,27                  | 87              | 0,27              |
| 305   | Eerste DWSRM CD 6 onder         | 70x70x6                  | 2             | M20  | 9,7                              | 810          | 678         | 14,2                    | 50                      | 43                      | 0,33                  | 14,7                  | 314                   | 23,5                    | 100                     | 87                      | 0,32                  | 87                    | 0,32                  | 87              | 0,32              |
| 306   | Eerste DWSRM CD 7 onder         | 70x70x6                  | 2             | M20  | 11,4                             | 810          | 678         | 16,9                    | 50                      | 43                      | 0,39                  | 17,4                  | 314                   | 27,8                    | 100                     | 87                      | 0,36                  | 87                    | 0,36                  | 87              | 0,36              |
| 307   | Eerste DWSRM CD 8 onder         | 70x70x6                  | 2             | M20  | 12,9                             | 810          | 678         | 19,1                    | 50                      | 43                      | 0,44                  | 19,7                  | 314                   | 31,4                    | 100                     | 87                      | 0,44                  | 87                    | 0,44                  | 87              | 0,44              |
| 308   | Eerste DWSRM CD 9 onder         | 70x70x6                  | 2             | M20  | 15,9                             | 810          | 678         | 23,5                    | 50                      | 43                      | 0,54                  | 24,3                  | 314                   | 38,7                    | 100                     | 87                      | 0,51                  | 87                    | 0,51                  | 87              | 0,51              |
| 309   | Eerste DWSRM CD 10 onder        | 70x70x6                  | 2             | M20  | 18,2                             | 810          | 678         | 26,9                    | 50                      | 43                      | 0,62                  | 27,8                  | 314                   | 44,3                    | 100                     | 87                      | 0,42                  | 87                    | 0,42                  | 87              | 0,42              |
| 311   | Eerste DWSRM CD 12 onder        | 70x70x6                  | 2             | M20  | 7,4                              | 810          | 678         | 11,0                    | 50                      | 43                      | 0,25                  | 11,4                  | 314                   | 36,2                    | 100                     | 87                      | 0,49                  | 87                    | 0,49                  | 87              | 0,49              |
| 312   | Eerste DWSRM 2&3 horiz onder    | 150x150x14 (not coupled) | 2             | M20  | 19,4                             | 8028         | 7720        | 2,5                     | 50                      | 43                      | 0,06                  | 27,0                  | 314                   | 43,0                    | 100                     | 87                      | 0,39                  | 87                    | 0,39                  | 87              | 0,39              |
| 313   | Eerste DWSRM Diag between hor   | 80x80x8                  | 1             | M24  | 11,6                             | 1230         | 1022        | 11,3                    | 50                      | 43                      | 0,26                  | 15,5                  | 452                   | 34,3                    | 100                     | 87                      | 0,24                  | 87                    | 0,24                  | 87              | 0,24              |
| 316   | Eerste DWSRM horiz 6&7          | 150x150x14 (not coupled) | 2             | M20  | 8,7                              | 8028         | 7720        | 1,1                     | 50                      | 43                      | 0,03                  | 13,3                  | 314                   | 21,2                    | 100                     | 87                      | 0,13                  | 87                    | 0,13                  | 87              | 0,13              |
| 319   | 1ste DWSRM front bracing 1      | 70x70x6                  | 2             | M20  | 5,1                              | 810          | 678         | 7,5                     | 50                      | 43                      | 0,17                  | 7,1                   | 314                   | 11,3                    | 100                     | 87                      | 0,19                  | 87                    | 0,19                  | 87              | 0,19              |
| 320   | 1ste DWSRM front bracing 2      | 70x70x6                  | 2             | M20  | 3,6                              | 810          | 678         | 5,3                     | 50                      | 43                      | 0,12                  | 5,1                   | 314                   | 16,1                    | 100                     | 87                      | 0,20                  | 87                    | 0,20                  | 87              | 0,20              |
| 321   | 1ste DWSRM front bracing 3      | 80x80x6                  | 2             | M20  | 7,6                              | 940          | 808         | 9,4                     | 50                      | 43                      | 0,22                  | 10,7                  | 314                   | 17,0                    | 100                     | 87                      | 0,03                  | 87                    | 0,03                  | 87              | 0,03              |
| 322   | 1ste DWSRM front bracing 4      | 70x70x6                  | 1             | M20  | 0,7                              | 810          | 678         | 1,0                     | 50                      | 43                      | 0,02                  | 0,9                   | 314                   | 2,9                     | 100                     | 87                      | 0,15                  | 87                    | 0,15                  | 87              | 0,15              |
| 323   | 1ste DWSRM front bracing 5      | 70x70x6                  | 1             | M16  | 1,7                              | 810          | 702         | 2,4                     | 50                      | 43                      | 0,06                  | 2,6                   | 201                   | 12,9                    | 100                     | 87                      | 0,08                  | 87                    | 0,08                  | 87              | 0,08              |
| 324   | 1ste DWSRM front bracing 6      | 50x50x5                  | 1             | M16  | 0,2                              | 480          | 390         | 0,4                     | 50                      | 43                      | 0,01                  | 0,3                   | 201                   | 1,3                     | 100                     | 87                      | 0,04                  | 87                    | 0,04                  | 87              | 0,04              |
| 325   | 1ste DWSRM section BB CD        | 50x50x5                  | 1             | M16  | 1,0                              | 480          | 390         | 2,4                     | 50                      | 43                      | 0,06                  | 1,3                   | 201                   | 6,6                     | 100                     | 87                      | 0,09                  | 87                    | 0,09                  | 87              | 0,09              |
| 326   | 1ste DWSRM section BB horiz     | 60x60x6                  | 1             | M16  | 0,5                              | 690          | 582         | 0,9                     | 50                      | 43                      | 0,02                  | 0,7                   | 201                   | 3,6                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 327   | 1ste DWSRM section horiz on top | 60x60x6                  | 1             | M16  | 1,2                              | 690          | 582         | 2,0                     | 50                      | 43                      | 0,05                  | 1,5                   | 201                   | 7,6                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 328   | 1ste DWSRM diag on top          | 50x50x5                  | 0             |      | 0,2                              | 480          | 480         | 0,3                     | 50                      | 43                      | 0,01                  | 0,2                   | 0                     | 0,0                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 329   | 1ste DWSRM preekstoel leuning   | 70x70x7                  | 0             |      | 0,3                              | 940          | 940         | 0,3                     | 50                      | 43                      | 0,01                  | 0,4                   | 0                     | 0,0                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 330   | 1ste DWSRM preekstoel ligger    | 100x50x6                 | 0             |      | 0,0                              | 870          | 870         | 0,0                     | 50                      | 43                      | 0,00                  | 0,0                   | 0                     | 0,0                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 331   | 1ste DWSRM preekstoel stijl     | 50x50x5                  | 0             |      | 0,2                              | 480          | 480         | 0,3                     | 50                      | 43                      | 0,01                  | 0,2                   | 0                     | 0,0                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 400   | Tweede DWSRM - Main diagonal 1  | 120x120x10               | 3             | M24  | 23,2                             | 2320         | 2060        | 11,3                    | 50                      | 43                      | 0,26                  | 35,5                  | 452                   | 26,2                    | 100                     | 87                      | 0,30                  | 87                    | 0,30                  | 87              | 0,30              |
| 401   | Tweede DWSRM - Vertical front   | 50x50x5                  | 1             | M16  | 0,7                              | 480          | 390         | 1,8                     | 50                      | 43                      | 0,04                  | 1,0                   | 201                   | 5,2                     | 100                     | 87                      | 0,06                  | 87                    | 0,06                  | 87              | 0,06              |
| 402   | Tweede DWSRM - Vertical front   | 50x50x5                  | 1             | M16  | 4,5                              | 480          | 390         | 11,5                    | 50                      | 43                      | 0,26                  | 6,8                   | 201                   | 33,9                    | 100                     | 87                      | 0,39                  | 87                    | 0,39                  | 87              | 0,39              |
| 403   | Tweede DWSRM - Vertical front   | 70x70x6                  | 1             | M16  | 3,5                              | 810          | 702         | 4,9                     | 50                      | 43                      | 0,11                  | 5,2                   | 201                   | 26,1                    | 100                     | 87                      | 0,30                  | 87                    | 0,30                  | 87              | 0,30              |
| 404   | Tweede DWSRM - Vertical front   | 90x90x9                  | 3             | M24  | 9,2                              | 1539         | 1305        | 7,0                     | 50                      | 43                      | 0,16                  | 12,8                  | 452                   | 9,5                     | 100                     | 87                      | 0,11                  | 87                    | 0,11                  | 87              | 0,11              |
| 405   | Tweede DWSRM - Diagonal front   | 60x60x6                  | 1             | M16  | 0,2                              | 690          | 582         | 0,3                     | 50                      | 43                      | 0,01                  | 0,3                   | 201                   | 1,3                     | 100                     | 87                      | 0,02                  | 87                    | 0,02                  | 87              | 0,02              |
| 406   | Tweede DWSRM - Diagonal front   | 60x60x6                  | 1             | M16  | 0,0                              | 690          | 582         | 0,1                     | 50                      | 43                      | 0,00                  | 0,1                   | 201                   | 0,3                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 407   | Tweede DWSRM - Diagonal front   | 50x50x5                  | 1             | M16  | 0,1                              | 480          | 390         | 0,1                     | 50                      | 43                      | 0,00                  | 0,1                   | 201                   | 0,4                     | 100                     | 87                      | 0,00                  | 87                    | 0,00                  | 87              | 0,00              |
| 408   | Tweede DWSRM - under diag       | 60x60x6                  | 2             | M16  | 8,5                              | 690          | 582         | 14,6                    | 50                      | 43                      | 0,34                  | 13,0                  | 201                   | 32,2                    | 100                     | 87                      | 0,37                  | 87                    | 0,37                  | 87              | 0,37              |
| 409   | Tweede DWSRM - horiz on top     | 60x60x6                  | 1             | M16  | 0,1                              | 690          | 582         | 0,2                     | 50                      | 43                      | 0,01                  | 0,2                   | 201                   | 1,1                     | 100                     | 87                      | 0,01                  | 87                    | 0,01                  | 87              | 0,01              |
| 411   | Tweede DWSRM - CD top           | 70x70x6                  | 1             | M20  | 7,3                              | 810          | 678         | 10,8                    | 50                      | 43                      | 0,25                  | 11,1                  | 314                   | 35,2                    | 100                     | 87                      | 0,40                  | 87                    | 0,40                  | 87              | 0,40              |
| 412   | Tweede DWSRM - CD top           | 70x70x6                  | 1             | M20  | 8,4                              | 810          | 678         | 12,4                    | 50                      | 43                      | 0,28                  | 12,7                  | 314                   | 40,4                    | 100                     | 87                      | 0,46                  | 87                    | 0,46                  | 87              | 0,46              |



**Check galloping**

Datum: 27-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RLl  
 HA\_n

| Group | Omschrijving                   | Profiel                  | Aantal bouten | Bout | Controle netto oppervlak profiel |                           |                          |                        |                       |                        |         |                     |                         |                          | Controle boutdoorsnede |                          |         |  |  |  |
|-------|--------------------------------|--------------------------|---------------|------|----------------------------------|---------------------------|--------------------------|------------------------|-----------------------|------------------------|---------|---------------------|-------------------------|--------------------------|------------------------|--------------------------|---------|--|--|--|
|       |                                |                          |               |      | $\Delta F_i$ [kN]                | Brutto [mm <sup>2</sup> ] | Netto [mm <sup>2</sup> ] | $\Delta\sigma_i$ [Mpa] | DC <sub>i</sub> [Mpa] | $\Delta\sigma_c$ [Mpa] | UC opp. | $\Delta F_i/b$ [kN] | Bout [mm <sup>2</sup> ] | $\Delta\sigma_i/b$ [Mpa] | DC <sub>i</sub> [Mpa]  | $\Delta\sigma_c/b$ [Mpa] | UC bout |  |  |  |
| 413   | Tweede DWSRM - CD top          | 70x70x6                  | 1             | M20  | 10,4                             | 810                       | 678                      | 15,3                   | 50                    | 43                     | 0,35    | 15,6                | 314                     | 49,8                     | 100                    | 87                       | 0,57    |  |  |  |
| 414   | Tweede DWSRM - CD top          | 50x50x5                  | 1             | M16  | 2,4                              | 480                       | 390                      | 6,2                    | 50                    | 43                     | 0,14    | 3,4                 | 201                     | 16,9                     | 100                    | 87                       | 0,19    |  |  |  |
| 415   | Tweede DWSRM - CD top          | 50x50x5                  | 1             | M16  | 3,1                              | 480                       | 390                      | 7,9                    | 50                    | 43                     | 0,18    | 4,3                 | 201                     | 21,5                     | 100                    | 87                       | 0,25    |  |  |  |
| 416   | Tweede DWSRM - CD top          | 50x50x5                  | 1             | M16  | 3,1                              | 480                       | 390                      | 7,9                    | 50                    | 43                     | 0,18    | 4,3                 | 201                     | 21,6                     | 100                    | 87                       | 0,25    |  |  |  |
| 417   | Tweede DWSRM - CD top          | 50x50x5                  | 1             | M16  | 4,1                              | 480                       | 390                      | 10,5                   | 50                    | 43                     | 0,24    | 5,7                 | 201                     | 28,6                     | 100                    | 87                       | 0,33    |  |  |  |
| 418   | Tweede DWSRM - CD top          | 60x60x6                  | 1             | M16  | 5,2                              | 690                       | 582                      | 9,0                    | 50                    | 43                     | 0,21    | 7,3                 | 201                     | 36,5                     | 100                    | 87                       | 0,42    |  |  |  |
| 418A  | Tweede DWSRM - CD top          | 60x60x6                  | 1             | M16  | 7,7                              | 690                       | 582                      | 13,3                   | 50                    | 43                     | 0,31    | 10,9                | 201                     | 27,0                     | 100                    | 87                       | 0,31    |  |  |  |
| 419   | Tweede DWSRM - CD UNP top      | UNP160                   | 1             | M20  | 4,2                              | 2400                      | 2235                     | 1,9                    | 50                    | 43                     | 0,04    | 5,9                 | 314                     | 18,7                     | 100                    | 87                       | 0,22    |  |  |  |
| 422   | Tweede DWSRM - CD under 1      | 70x70x6                  | 2             | M20  | 5,1                              | 810                       | 678                      | 7,5                    | 50                    | 43                     | 0,17    | 7,7                 | 314                     | 12,3                     | 100                    | 87                       | 0,14    |  |  |  |
| 423   | Tweede DWSRM - CD under 2      | 70x70x6                  | 2             | M20  | 5,8                              | 810                       | 678                      | 8,6                    | 50                    | 43                     | 0,20    | 8,9                 | 314                     | 14,1                     | 100                    | 87                       | 0,16    |  |  |  |
| 424   | Tweede DWSRM - CD under 3      | 70x70x6                  | 2             | M20  | 6,3                              | 810                       | 678                      | 9,3                    | 50                    | 43                     | 0,21    | 9,6                 | 314                     | 15,3                     | 100                    | 87                       | 0,18    |  |  |  |
| 425   | Tweede DWSRM - CD under 4      | 70x70x6                  | 2             | M20  | 6,1                              | 810                       | 678                      | 9,0                    | 50                    | 43                     | 0,21    | 9,3                 | 314                     | 14,7                     | 100                    | 87                       | 0,17    |  |  |  |
| 426   | Tweede DWSRM - CD under 5      | 70x70x6                  | 2             | M20  | 13,3                             | 810                       | 678                      | 19,7                   | 50                    | 43                     | 0,45    | 20,4                | 314                     | 32,4                     | 100                    | 87                       | 0,37    |  |  |  |
| 427   | Tweede DWSRM - CD under 6      | 70x70x6                  | 2             | M20  | 17,7                             | 810                       | 678                      | 26,0                   | 50                    | 43                     | 0,60    | 26,9                | 314                     | 42,9                     | 100                    | 87                       | 0,49    |  |  |  |
| 428   | Tweede DWSRM - CD under 7      | 70x70x6                  | 2             | M20  | 19,3                             | 810                       | 678                      | 28,5                   | 50                    | 43                     | 0,66    | 29,5                | 314                     | 46,9                     | 100                    | 87                       | 0,54    |  |  |  |
| 429   | Tweede DWSRM - CD under 8      | 70x70x7                  | 1             | M16  | 0,7                              | 940                       | 814                      | 0,8                    | 50                    | 43                     | 0,02    | 1,0                 | 201                     | 5,0                      | 100                    | 87                       | 0,06    |  |  |  |
| 430   | 2e DWSRM diag verband          | 60x60x6                  | 1             | M16  | 8,8                              | 690                       | 582                      | 15,2                   | 50                    | 43                     | 0,35    | 13,5                | 201                     | 67,0                     | 100                    | 87                       | 0,77    |  |  |  |
| 431   | 2e DWSRM kniksteun             | 50x50x5                  | 1             | M16  | 2,4                              | 480                       | 390                      | 6,1                    | 50                    | 43                     | 0,14    | 3,6                 | 201                     | 17,9                     | 100                    | 87                       | 0,21    |  |  |  |
| 432   | 2e DWSRM kniksteun             | 50x50x5                  | 1             | M16  | 1,3                              | 480                       | 390                      | 3,4                    | 50                    | 43                     | 0,08    | 2,0                 | 201                     | 10,0                     | 100                    | 87                       | 0,11    |  |  |  |
| 436   | Tweede DWSRM - Horizontaal und | 150x150x14 (not coupled) | 3             | M20  | 14,1                             | 8028                      | 7720                     | 1,8                    | 50                    | 43                     | 0,04    | 21,5                | 314                     | 22,8                     | 100                    | 87                       | 0,26    |  |  |  |
| 437   | Tweede DWSRM - diagonaal katt  | 55x55x6                  | 1             | M16  | 2,8                              | 600                       | 492                      | 5,7                    | 50                    | 43                     | 0,13    | 4,1                 | 201                     | 20,2                     | 100                    | 87                       | 0,23    |  |  |  |





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## B.10 Mastrapportage hoekmasten reconstructie



ZUID-WEST 380 KV OOST VERBINDINGEN

# Mastrapportage GT-RLI HB+5/n

TenneT TSO B.V.

Meridian doc.nr.: 002.678.00.0934571

Rapport nr.: 21-0887, Rev. 1

Datum: 23-08-2021

**DATUM:** 04-11-2021

**STATUS TENNET:** DEFINITIEF

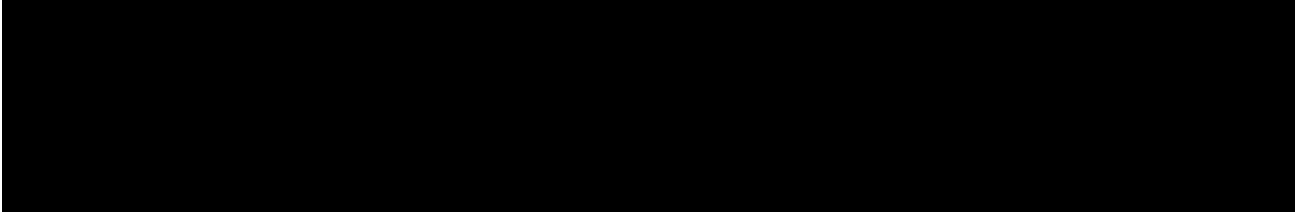
**REVISIE TENNET:** 1.0





Projectnaam: Zuid-West 380 kV Oost Verbindingen  
Rapport titel: Mastrapportage GT-RLL HB+5/n  
Klant: TenneT TSO B.V.  
Contactpersoon klant: XXXXXXXXXX  
Datum uitgave: 23-08-2021  
Project nr.: 10124719  
Organisatie unit: TDT  
Meridian doc.nr.: 002.678.00.0934571  
Rapport nr.: 21-0887, Rev. 1

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|------|------------|-------------------------|--|-------------|------------|
| 0    | 29-07-2021 | Eerste uitgave          | <span style="background-color: black; color: black;">XXXXXXXXXX</span> |             |            |
| 1    | 23-08-2021 | RFA-commentaar verwerkt | <span style="background-color: black; color: black;">XXXXXXXXXX</span> |             |            |

## Inhoudsopgave

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## 1 INLEIDING

In het basisontwerp van de vakwerkmasten voor de verbinding GT-RLL380 in het project Zuid-West 380 kV-Oost zijn voor het vaststellen van de haalbaarheid constructieve berekeningen uitgevoerd aan de masten en fundaties. In de Definitief Ontwerpfase, moeten berekeningen verder worden uitgewerkt om te kunnen dienen voor de benodigde vergunningsdocumentatie, voor de aanbesteding en als voorbereiding voor de uitvoeringsfase. Het DO omvat het ontwerp van de mastconstructies, de fundaties en de opstijpunten in de verbinding.

Deze rapportage bevat de resultaten van de toetsing van masttype HB+5/n ten behoeve van de reconstructie. Deze mast is gebaseerd op de bestaande HB+5 masten uit de verbinding GT-RLL380 met de aanpassingen om te voldoen aan de belasting uit de nieuwe situatie.

In deze rapportage is de toetsing van de mast van de hoekmast HB+5/n opgenomen. De toetsing bestaat uit controle van:

- de profielen en boutverbindingen onderdeel van de hoofddraagconstructie
- de knikverkorters
- de liggers voor de isolatorkettingen
- de verbinding met de fundatie via blokdeuvels
- de toetsing op galloping.

Buiten de scope van dit DO-rapport valt de controle van de schetsplaten en overige verbindingdetails in de constructie. Dit moet in de UO-fase worden uitgewerkt. Ook de voorzieningen voor de high-step rail en bordessen vallen onder uitwerking in UO-fase.

In hoofdstuk 2 zijn de uitgangspunten en randvoorwaarden vanuit de van toepassing zijnde normen en TenneT-specificaties opgenomen. Hoofdstuk 3 beschrijft de gevolgde aanpak van de berekening. In hoofdstuk 4 is de toetsing opgenomen.

## 2 UITGANGSPUNTEN EN RANDVOORWAARDEN

### 2.1 Normen

Er is gebruik gemaakt van de normen volgens Tabel 1.

**Tabel 1 Gebruikgemaakte normen, voorschriften en richtlijnen**

| Norm                                       | Titel  |
|--|--|
| NEN-EN 50341-1:2013                        | “Overhead electrical lines exceeding AC 1 kV - Part 1: General requirements – Common”                        |
| NEN-EN 50341-2-15:2019                     | “Overhead electrical lines exceeding AC 1 kV Part 2 National Normative Aspects (NNA) for THE NETHERLANDS”    |
| NEN-EN 1990+A1+A1/C2:2019/NB:2019nl        | “Grondslagen van het ontwerp”  |
| NEN-EN 1991-1-4+A1+C2:2011/NB:2019+C1:2020 | “Deel 1-4: Windbelasting op constructies”  |
| NEN-EN 1992-1-1+C2:2011/NB:2016+A1:2020    | “Eurocode 2: Ontwerp en berekening van betonconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-1-1+C2+A1:2016 nl              | “Eurocode 3: Ontwerp en berekening van staalconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-3-1:2007/NB:2011 nl            | “Deel 3-1: Torens, masten en schoorstenen - Torens en masten”  |
| NEN-EN 1993-1-8+C2:2011/NB:2011 nl         | “Ontwerp en berekening van staalconstructies, deel 1-8: ontwerp en berekening van verbindingen”              |

### 2.2 TenneT-specificaties

In Tabel 2 zijn de documenten opgenomen die relevant zijn voor de berekeningen en toetsingen die binnen dit project in de mastrapportage uitgevoerd zullen worden.

**Tabel 2 Relevante documenten t.b.v. mechanische rapportages**

| Nummer          | Onderwerp                           |
|-----------------|-------------------------------------|
| PVE.05.000 v3.2 | PvE Lijnen                          |
| sPVE.05.001     | sPvE Lijnen                         |
| SPE.05.346 v1.3 | Algemene specificatie stalen masten |

### 2.3 Eisenverificatie

Voor de eisenverificatie wordt verwezen naar het rapport “Verificatierapport eisen reconstructies”.

### 2.4 Ontwerprapporten

Voor de achtergrond van het ontwerp wordt verwezen naar het uitgangspuntenrapport “D1.3 Uitgangspunten reconstructies”, DNV GL rapport 21-0702, Meridiannummer 002.678.00 0927721.

### 2.5 Materialen

Voor het ontwerp van de mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 3.

**Tabel 3 Materialen aangepaste constructie**

|                |   |
|----------------|---|
| Staalsoort     | S355J0 (t≤16 mm)<br>S355J2 (16<t≤40 mm) |
| Boutkwaliteit  | 8.8 gerolde draad                       |
| Betonkwaliteit | C30/37                                  |
| Wapeningsstaal | B500                                    |



Voor de constructie geldt conform TenneT-specificatie:

- Toe te passen bouten: M16/M20/M24
- Voor hoekstaal is de minimale afmeting L50x5 mm
- Minimale plaatdikte 6 mm.

Mocht het noodzakelijk zijn M30 toe te passen, bij grote plaatdiktes is dit als afwijking door TenneT toegestaan.

## 2.6 Software

De gebruikte software wordt benoemd in Tabel 4.

**Tabel 4 Toegepaste software**

| Software              |           | Versie |
|-----------------------|-----------|--------|
| Mastontwerp           | PLS-CADD  | 16.65  |
| Mastberekeningen      | PLS-TOWER | 16.65  |
| Constructieve analyse | AxisVM    | X5 R4h |



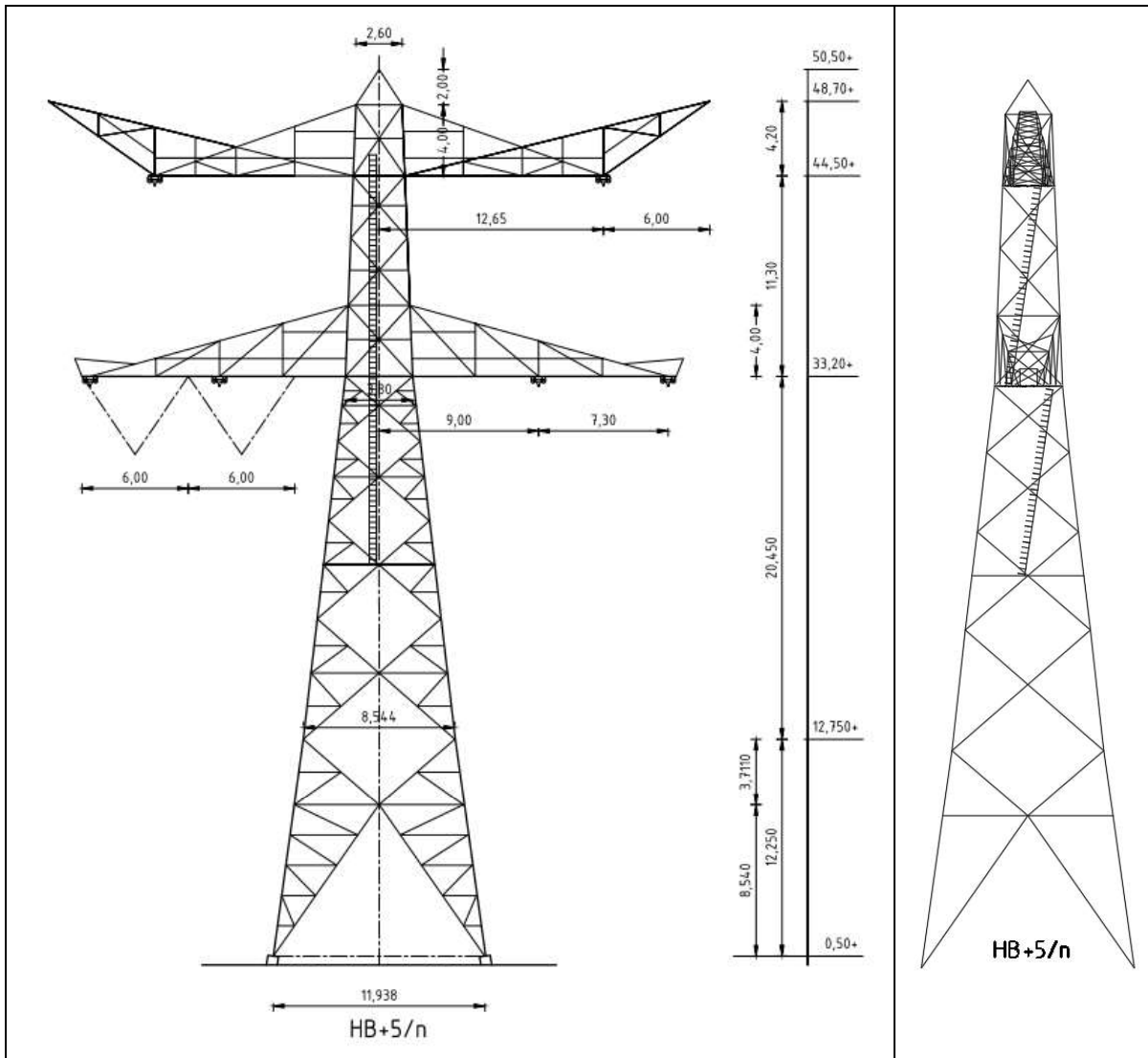
### 3 MASTONTWERP

#### 3.1 Mastbeelden

In dit hoofdstuk worden het mastbeeld weergegeven met de belangrijkste maatvoering, de figuren zijn ontleend aan de bij deze rapportage horende tekeningen van de masttypen. Het gaat om de volgende tekeningen:

- Overzichtstekening HB+5/n, Meridiannummer 002.678.00 0934588

Masttype reconstructie HB+5/n is een hoekmast voor twee circuits 380 kV.



Figuur 1 Mastbeeld masttype HB+5/n

## 3.2 Uitgangspunten berekening

De uitgangspunten volgens Tabel 5 zijn van toepassing.

**Tabel 5 Uitgangspunten**

|                             |                       |
|-----------------------------|-----------------------|
| Norm                        | NEN-EN50341-2-15:2019 |
| Gevolgklasse initieel       | CC2                   |
| Betrouwbaarheidsniveau      | Nieuwbouw             |
| Referentieperiode           | 50 jaar               |
| Windgebied                  | III                   |
| Windsnelheid (m/s)          | 24,5                  |
| Terreincategorie            | II                    |
| Reductiefactor $c_{dir}$    | 1,00                  |
| IJsg gebied fasegeleider    | B                     |
| IJsg gebied bliksemgeleider | A                     |

## 3.3 Mastenlijst

In Tabel 6 zijn alle masten in het tracé van het type HB+5/n opgenomen. De mast met grootste wind span is vetgedrukt aangegeven. Het masttype zal niet met deze wind en weight span worden berekend maar met generieke wind en weight span, zie uitgangspuntenrapport.

**Tabel 6 Mastenlijst HB+5/n**

| Mast-nummer | Masttype | Lijnhoek (°) | Wind span (m) | Weight span (m) | Hoogteverschil ba+ah (m) | Hoogteverschil back (m) | Hoogteverschil ahead (m) |
|-------------|----------|--------------|---------------|-----------------|--------------------------|-------------------------|--------------------------|
| <b>69N</b>  | HB+5/n   | 148,6        | 322,3         | 347,7           | 6,2                      | 0,6                     | 5,6                      |

## 3.4 Geleiderbelastingen

De berekening is uitgevoerd met het geleiderbelastingprogramma van DNV. De belastingen op de mastconstructie zijn bepaald op basis van de modellering in PLS-TOWER (staafoppervlaktes). Voor de toeslagen op eigen gewicht en windoppervlakte wordt verwezen naar het uitgangspuntenrapport. In Appendix A zijn de resultaten van de geleiderbelastingen samengevat.

## 3.5 Reacties op de fundering

De oplegreacties op de fundering worden ontleend aan de uitvoer van het geleiderbelastingprogramma. Zie Appendix A.

## 3.6 Modelling

Op basis van de ontwerptekeningen is de mast in PLS-TOWER ingevoerd. De toetsing wordt per staafgroep uitgevoerd. De hoofdelementen zijn gemodelleerd, niet-dragende profielen als knikverkorters zijn weggelaten, deze worden separaat getoetst. De profielen zijn in PLS-TOWER inclusief de boutverbindingen ingevoerd en getoetst, de controle van de schetsplaten en andere detailverbindingen valt buiten de scope.

De geleiderbelastingen vanuit het geleiderbelastingprogramma zijn als invoer voor de belastingen gebruikt.

De gewichts- en windbelasting op de mastconstructie wordt door PLS-TOWER automatisch bepaald. Via toeslagfactoren wordt de invloed van niet gemodelleerde elementen als knikverkorters, bordesconstructies en



Klimvoorzieningen meegenomen. Voor schetsplaten, zinklaag en bouten is een aanvullende toeslag op het gewicht van 20% toeslag gerekend.

Diagonalen in voor- en achtervlak respectievelijk de twee zijvlakken zijn samengenomen in een groep.

### **3.7 Overige controles**

In PLS-TOWER zijn niet alle elementen getoetst. Knikverkorteprofielen en overige profielen voor beloopbaarheid worden separaat getoetst. In Appendix C is dit opgenomen. De verbinding met de fundatie bestaat uit ingestorte profielen voorzien van blokdeuvels. Dit is in Appendix D opgenomen. De liggers van isolatorkettingen zijn gebaseerd op Moldaumasten en hebben geen aanvullende controle op buiging vanwege aanmerkelijk lagere belastingen. Appendix E is niet ingevuld bij dit masttype maar vanwege consistentie met andere rapporten hier opgenomen. Appendix F omvat de toetsing op galloping.

### **3.8 Mastgewicht**

Het totale mastgewicht is met de uitgangspunten van paragraaf 3.6 bepaald op:

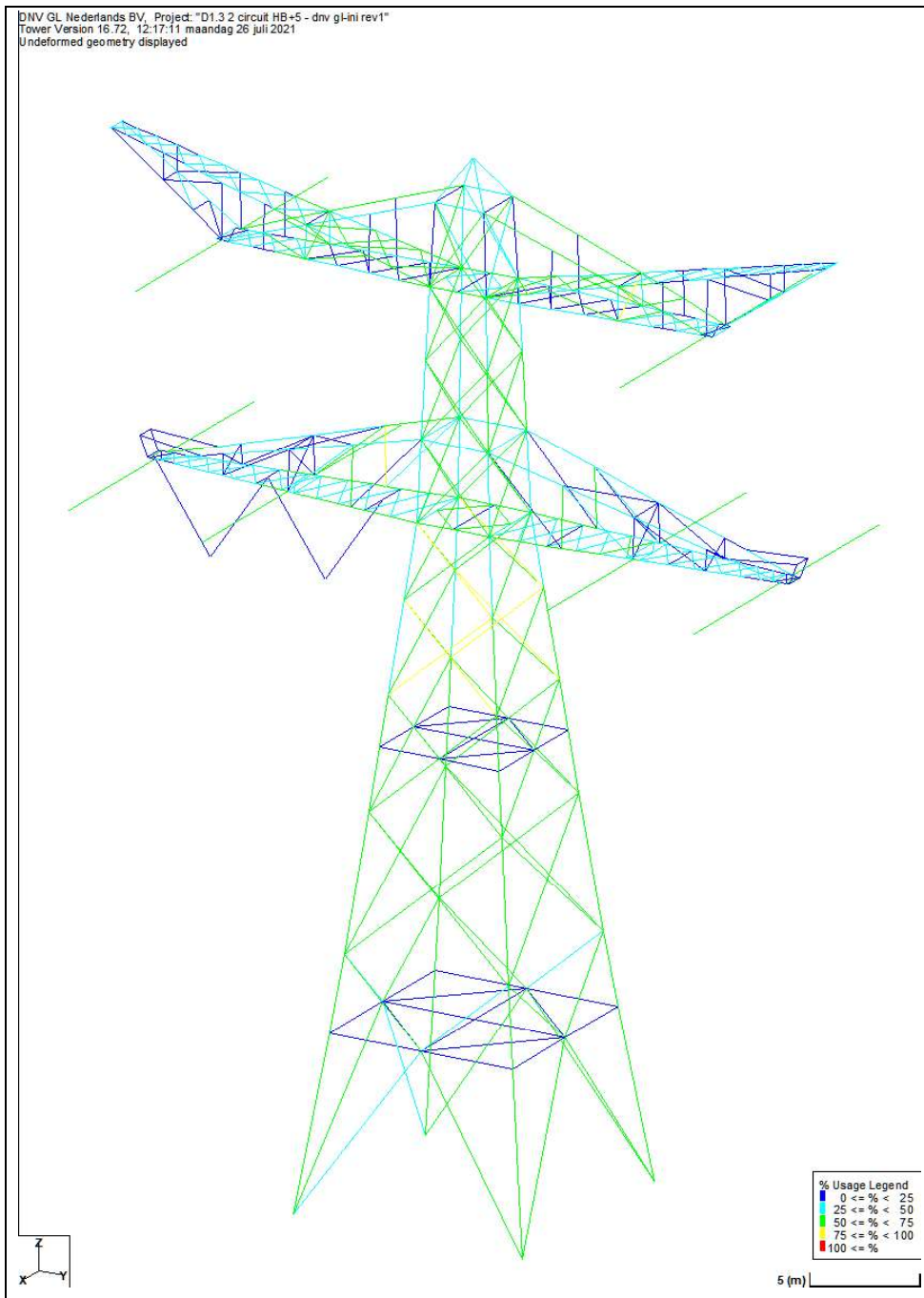
Het gewicht van masttype HB+5/n is bepaald op 52,5 ton.

## 4 TOETSING

### 4.1 Resultaat PLS-TOWER

Het resultaat van de toetsing met PLS-TOWER is per masttype weergegeven in Figuur 2.

De uitnutting van de constructie loopt op van blauw (0-25%) tot geel (75-100%). Uit de figuur wordt geconcludeerd dat alle profielen en boutverbindingen voldoen.



Figuur 2 Resultaat PLS-TOWER voor de hoekmast HB+5/n

## 4.2 Toetsing overige onderdelen

In Tabel 7 zijn de resultaten van de uitgevoerde toetsingen weergegeven.

**Tabel 7 Samenvatting uitgevoerde controles**

| Controle van          | Beoordeling | Referentie             |
|-----------------------|-------------|------------------------|
| Profielen             | Voldoen     | Figuur 2<br>Appendix B |
| Knikverkorters        | Voldoen     | Appendix C             |
| Blokdeuvels randstijl | Voldoen     | Appendix D             |
| Galloping             | Voldoet     | Appendix F             |



## APPENDIX A

### Geleiderbelastingen

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Geleiderbelastingen opgenomen:

- Masttype HB+5/n.



Project: GT-RLL380  
 Tower: HB+5\_n (140 gr)  
 Number: 69N

Auteur: TBR  
 Versie: v12.0

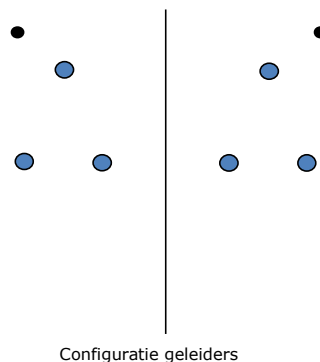
### Geleiderbelastingen

#### Algemeen

Benaming HB+5\_n (140 gr)  
 Masttype Hoekmast  
 Aantal circuits 2  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 2

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 50 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 50 jaar  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsgebied fasegeleider B  
 IJsgebied bliksemgeleider A



Configuratie geleiders

#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                     |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A         | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A         | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                      |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A         | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A         | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging     | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Circuit 2      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Bliksemdraad 1 | Afspanketting | 0,10         | 0,20       | 0,20                       |
| Bliksemdraad 2 | Afspanketting | 0,10         | 0,20       | 0,20                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 32,7 m       | 32,7 m       | -16,3 m                                |
| Circuit 1      | 11         | 380ct1f2 | 32,7 m       | 32,7 m       | -9,0 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 44,0 m       | 44,0 m       | -12,7 m                                |
| Circuit 2      | 20         | 380ct2f1 | 32,7 m       | 32,7 m       | 16,3 m                                 |
| Circuit 2      | 21         | 380ct2f2 | 32,7 m       | 32,7 m       | 9,0 m                                  |
| Circuit 2      | 22         | 380ct2f3 | 44,0 m       | 44,0 m       | 12,7 m                                 |
| Bliksemdraad 1 | 1          | bl1      | 48,2 m       | 48,2 m       | -18,7 m                                |
| Bliksemdraad 2 | 3          | bl2      | 48,2 m       | 48,2 m       | 18,7 m                                 |



Project: GT-RLL380  
 Tower: HB+5\_n (140 gr)  
 Number: 69N

**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead   |   |
|------------------------------------|---------------------------|---------|---|
| Verhoging voor windbelasting       | 5,0 m                     | 5,0 m   | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -10,0 m                   | -10,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |         |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

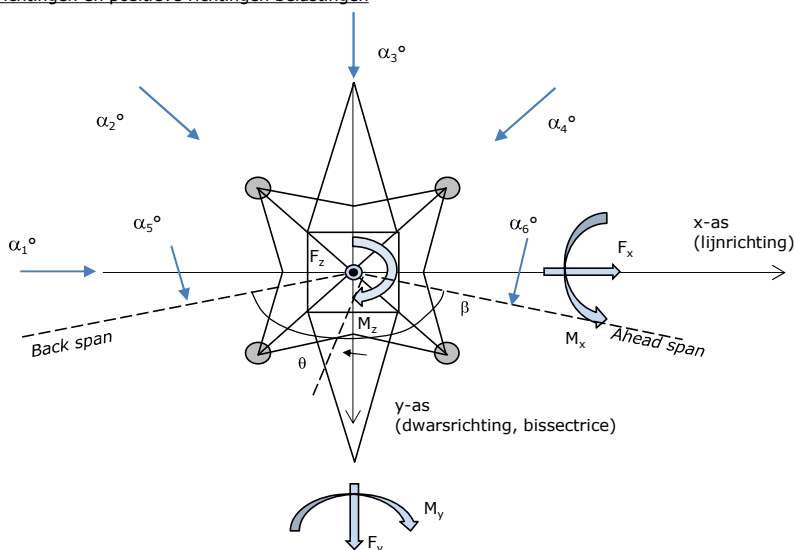
| Circuits       | Aanduiding | Nummer   | Hoogteverschil  |                  | Richtingsverandering |                  |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
|                |            |          | $\Delta h$ back | $\Delta h$ ahead | $\Delta y$ back      | $\Delta y$ ahead |
| Circuit 1      | 10         | 380ct1f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 11         | 380ct1f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 12         | 380ct1f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 20         | 380ct2f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 21         | 380ct2f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 22         | 380ct2f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 1 | 1          | bl1      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 2 | 3          | bl2      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek $\beta$                           | 140 °      |         |
| Rotatie mast t.o.v. bissectrice $\theta$   | 0 °        |         |
| Vaklengte                                  | 400        | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 45 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 135 °   |
|  | $\alpha_5$ | 70 °    |
|  | $\alpha_6$ | 110 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



**Beschouwd aantal windrichtingen**

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

Project: GT-RLL380  
 Tower: HB+5\_n (140 gr)  
 Number: 69N

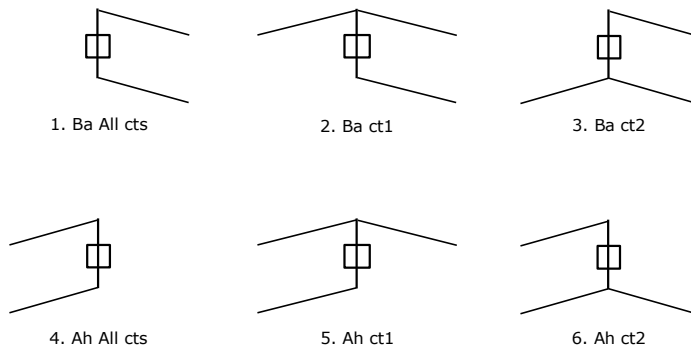
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | bl1      | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | bl2      | 0             | 1    | 1                        | 0    | 1                  | 0    |

### Belastingsituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

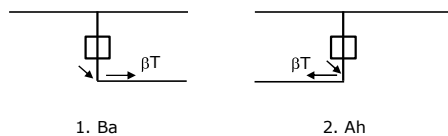
Principe belastingssituaties:



### Belastingsituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



Project: GT-RLL380  
 Tower: HB+5\_n (140 gr)  
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### Belastingsituaties 6. Bouw- en onderhoud

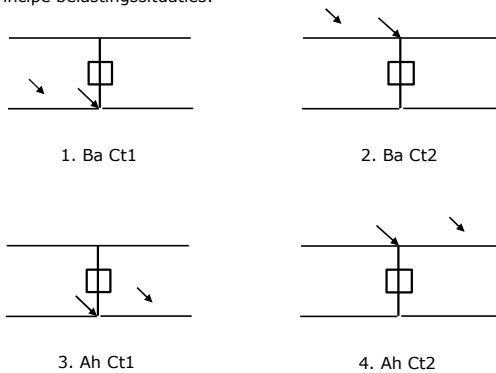
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



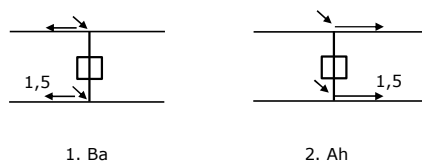
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingsspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

Project: GT-RLL380  
 Tower: HB+5\_n (140 gr)  
 Number: 69N

## Mastconstructie

### Eigenschappen

|   |                 |         |
|---|-----------------|---------|
| Masttype                                    | Hoekmast        |         |
| Mastbenaming                                | HB+5_n (140 gr) |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m           |         |
| Masthoogte t.o.v. voetplaat                 | 50,0 m          |         |
| Gewicht mast                                | 516,0 kN        |         |
| <i>Breedte en helling mast bij fundatie</i> |                 |         |
|   | x-ri.           | y-ri.   |
| Pootsprei                                   | 11,94           | 11,94 m |
| Helling van de randstijl                    | 0,139           | 0,139 - |
| Factor spatkracht                           | 1,3             | 1,3 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,00 (Masthoogte < 60 m)              |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 12,25    | 11,94                 | 8,54                  | 12,25     | 0,139                 | 125,45                              | 17,57                               | 0,14                                      | 3,21           |
| Eerste tussenstuk | 24,56    | 8,54                  | 5,69                  | 12,31     | 0,116                 | 87,60                               | 16,12                               | 0,18                                      | 3,00           |
| Tweede tussenstuk | 32,70    | 5,69                  | 3,80                  | 8,14      | 0,116                 | 38,62                               | 12,69                               | 0,33                                      | 2,44           |
| Bovenstuk 1       | 40,50    | 3,80                  | 3,19                  | 7,80      | 0,039                 | 27,26                               | 8,02                                | 0,29                                      | 2,56           |
| Bovenstuk 2       | 48,00    | 3,19                  | 2,60                  | 7,50      | 0,039                 | 21,71                               | 6,12                                | 0,28                                      | 2,60           |
| Topstuk           | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse     | 32,70    | 14,86                 |                       | 4,00      |                       | 29,72                               | 7,50                                | 0,25                                      | 2,71           |
| Boventraverse     | 44,00    | 17,19                 |                       | 4,00      |                       | 34,39                               | 8,70                                | 0,25                                      | 2,71           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 12,25    | 11,94                 | 8,54                  | 12,25     | 0,139                 | 125,45                              | 17,57                               | 0,14                                      | 3,21           |
| Eerste tussenstuk | 24,56    | 8,54                  | 5,69                  | 12,31     | 0,116                 | 87,60                               | 16,12                               | 0,18                                      | 3,00           |
| Tweede tussenstuk | 32,70    | 5,69                  | 3,80                  | 8,14      | 0,116                 | 38,62                               | 12,69                               | 0,33                                      | 2,44           |
| Bovenstuk 1       | 40,50    | 3,80                  | 3,19                  | 7,80      | 0,039                 | 27,26                               | 8,02                                | 0,29                                      | 2,56           |
| Bovenstuk 2       | 48,00    | 3,19                  | 2,60                  | 7,50      | 0,039                 | 21,71                               | 6,12                                | 0,28                                      | 2,60           |
| Topstuk           | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse     | 32,70    | 14,86                 |                       | 4,00      |                       | 29,72                               | 7,50                                | 0,25                                      | 2,71           |
| Boventraverse     | 44,00    | 17,19                 |                       | 4,00      |                       | 34,39                               | 8,70                                | 0,25                                      | 2,71           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

Project: GT-RLL380  
 Tower: HB+5\_n (140 gr)  
 Number: 69N

#### Windoppervlak feeders telecominstallaties

| Onderdeel         | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk         | 0,20                  | 0,71   | 12,3 | 1,7            |
| Eerste tussenstuk | 0,20                  | 0,71   | 12,3 | 1,7            |
| Tweede tussenstuk | 0,20                  | 0,71   | 8,1  | 1,2            |
| Bovenstuk 1       |                       |        |      |                |
| Bovenstuk 2       |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>i</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,0                 | 35    | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 39,5                    | 33,5                    | 0,0                     | -33,5                   | 6,1                    | 241,9                    | 205,3                    | 0,0                      | -205,3                   |
| Eerste tussenstuk | 0,86                                   | 41,4                    | 35,1                    | 0,0                     | -35,1                   | 18,4                   | 762,1                    | 646,6                    | 0,0                      | -646,6                   |
| Tweede tussenstuk | 0,98                                   | 30,1                    | 25,6                    | 0,0                     | -25,6                   | 28,6                   | 863,1                    | 732,4                    | 0,0                      | -732,4                   |
| Bovenstuk 1       | 1,05                                   | 21,5                    | 18,2                    | 0,0                     | -18,2                   | 36,6                   | 786,4                    | 667,2                    | 0,0                      | -667,2                   |
| Bovenstuk 2       | 1,10                                   | 17,5                    | 14,9                    | 0,0                     | -14,9                   | 44,3                   | 774,5                    | 657,2                    | 0,0                      | -657,2                   |
| Topstuk           | 1,13                                   | 1,4                     | 1,2                     | 0,0                     | -1,2                    | 49,0                   | 69,7                     | 59,1                     | 0,0                      | -59,1                    |
| Ondertraverse     | 1,02                                   | 41,7                    | 24,7                    | 0,0                     | -24,7                   | 34,0                   | 1418,0                   | 842,2                    | 0,0                      | -842,2                   |
| Boventraverse     | 1,11                                   | 52,2                    | 31,0                    | 0,0                     | -31,0                   | 45,3                   | 2365,5                   | 1405,1                   | 0,0                      | -1405,1                  |

|               |              |              |            |               |               |               |            |                |
|---------------|--------------|--------------|------------|---------------|---------------|---------------|------------|----------------|
| <b>Totaal</b> | <b>245,3</b> | <b>184,3</b> | <b>0,0</b> | <b>-184,3</b> | <b>7281,2</b> | <b>5215,2</b> | <b>0,0</b> | <b>-5215,2</b> |
|---------------|--------------|--------------|------------|---------------|---------------|---------------|------------|----------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 0,0                     | 33,5                    | 39,5                    | 33,5                    | 6,1                    | 0,0                      | 205,3                    | 241,9                    | 205,3                    |
| Eerste tussenstuk | 0,86                                   | 0,0                     | 35,1                    | 41,4                    | 35,1                    | 18,4                   | 0,0                      | 646,6                    | 762,1                    | 646,6                    |
| Tweede tussenstuk | 0,98                                   | 0,0                     | 25,6                    | 30,1                    | 25,6                    | 28,6                   | 0,0                      | 732,4                    | 863,1                    | 732,4                    |
| Bovenstuk 1       | 1,05                                   | 0,0                     | 18,2                    | 21,5                    | 18,2                    | 36,6                   | 0,0                      | 667,2                    | 786,4                    | 667,2                    |
| Bovenstuk 2       | 1,10                                   | 0,0                     | 14,9                    | 17,5                    | 14,9                    | 44,3                   | 0,0                      | 657,2                    | 774,5                    | 657,2                    |
| Topstuk           | 1,13                                   | 0,0                     | 1,2                     | 1,4                     | 1,2                     | 49,0                   | 0,0                      | 59,1                     | 69,7                     | 59,1                     |
| Ondertraverse     | 1,02                                   | 0,0                     | 24,7                    | 16,7                    | 24,7                    | 34,0                   | 0,0                      | 842,2                    | 567,2                    | 842,2                    |
| Boventraverse     | 1,11                                   | 0,0                     | 31,0                    | 20,9                    | 31,0                    | 45,3                   | 0,0                      | 1405,1                   | 946,2                    | 1405,1                   |

|               |            |              |              |              |            |               |               |               |
|---------------|------------|--------------|--------------|--------------|------------|---------------|---------------|---------------|
| <b>Totaal</b> | <b>0,0</b> | <b>184,3</b> | <b>189,0</b> | <b>184,3</b> | <b>0,0</b> | <b>5215,2</b> | <b>5011,1</b> | <b>5215,2</b> |
|---------------|------------|--------------|--------------|--------------|------------|---------------|---------------|---------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub> | F <sub>y</sub> | F <sub>z</sub> | M <sub>x</sub> | M <sub>y</sub> | M <sub>z</sub> |
|--------------------------|----------------|----------------|----------------|----------------|----------------|----------------|
|                          | [kN]           | [kN]           | [kN]           | [kNm]          | [kNm]          | [kNm]          |
| Permanente belasting     | 0              | 0              | 516            | 0              | 0              | 0              |
| Windrichting 0°          | 251            | 0              | 0              | 0              | 7498           | 0              |
| Windrichting 45°         | 189            | 189            | 0              | 5368           | 5368           | 0              |
| Windrichting 90°         | 0              | 195            | 0              | 5228           | 0              | 0              |
| Windrichting 135°        | -189           | 189            | 0              | 5368           | -5368          | 0              |

Project: GT-RL380  
 Tower: HB+5\_n (140 gr)  
 Number: 69N

### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| 380ct2f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct2f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct2f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,2                           | 48,70             | 1,13                             | 1,2               | 0,27                |
| bl2      | 0,10                   | 1      | 0,1                 | 0,2           | 0,2                           | 48,70             | 1,13                             | 1,2               | 0,27                |

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#### Windbelasting back

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| 380ct2f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| bl1      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,19  | 22,24         | 17,5  | 19,3        | 63,1              | 50,0        | 55,0            |
| bl2      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,20  | 22,13         | 17,5  | 19,2        | 63,0              | 49,9        | 54,9            |

#### Windbelasting ahead

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| 380ct2f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| bl1      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,19  | 22,24         | 17,5  | 19,3        | 63,1              | 50,0        | 55,0            |
| bl2      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,20  | 22,13         | 17,5  | 19,2        | 63,0              | 49,9        | 54,9            |

NB: belastingen  $w_v$  gelden voor bundel

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 Masttype: HB+5\_n (140 gr)  
 Mast: 69N

Auteur: TBR  
 Versie: v12.0

### Geleiderbelastingen

#### Uitgangspunten

Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 50 jaar

| ULS (bezwijksterkte)   |                           | NEN-EN50341-2-15:2019 |              |                     |  |          |          |                     |
|--|---------------------------|-----------------------|--------------|---------------------|--|----------|----------|---------------------|
| Belastingsgeval  | omschrijving              | Temp<br>°C            | $\gamma_G$   |                     | $\gamma_Q$                               |          |          | $\gamma_a$<br>$A_k$ |
|  |                           |                       | $G_{k,mast}$ | $G_{k,geleider}$    | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a   | Wind                      | 10°                   | 1,20         | 1,20                | 0,00                                     | 1,50     | 0,00     | 0,0                 |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                   | 0,90         | 1,20                | 0,00                                     | 1,50     | 0,00     | 0,0                 |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                   | 0,90         | 0,90                | 0,00                                     | 1,50     | 0,00     | 0,0                 |
| ULS 3  | Wind+ijs                  | -5°                   | 1,20         | 1,20                | 0,00                                     | 0,45     | 1,50     | 0,0                 |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                   | 0,90         | 1,20                | 0,00                                     | 0,45     | 1,50     | 0,0                 |
| ULS 4  | Koude+wind                | -20°                  | 1,20         | 1,20                | 0,00                                     | 0,30     | 0,00     | 0,0                 |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                  | 0,90         | 1,20                | 0,00                                     | 0,30     | 0,00     | 0,0                 |
| ULS 5a   | Torsiebelastingen         | 10°                   | 1,00         | 1,00                | 1,00                                     | 0,00     | 0,00     | 1,0                 |
| ULS 5b   | Longitudinale belastingen | 10°                   | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |
| ULS 6  | Bouw en onderhoud         | 5°                    | 1,20         | 1,20                | 1,50                                     | 0,30     | 0,00     | 0,0                 |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                    | 1,20         | 1,20                | 0,00                                     | 0,30     | 0,00     | 0,0                 |
| ULS 7  | Permanent                 | 10°                   | 1,35         | 1,35                | 0,00                                     | 0,00     | 0,00     | 0,0                 |
| ULS 8  | Special                   | 10°                   | 1,00         | 1,00                | 0,00                                     | 0,00     | 0,00     | 1,0                 |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                       |              | $\gamma_G$<br>$G_k$ | $\gamma_Q$<br>$Q_{pk}$ $Q_{wk}$ $Q_{ik}$ |          |          | $A_k$               |
| SPLS 1a  | Wind                      | 10°                   | 1,20         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                   | 0,90         | 1,20                | 0,0                                      | 0,78     | 0,00     | 0,0                 |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                   | 0,90         | 0,90                | 0,0                                      | 0,78     | 0,00     | 0,0                 |
| SPLS 3   | Wind+ijs                  | -5°                   | 1,20         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                   | 0,90         | 1,20                | 0,0                                      | 0,36     | 0,34     | 0,0                 |
| SPLS 4   | Koude+wind                | -20°                  | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                  | 0,90         | 1,20                | 0,0                                      | 0,24     | 0,00     | 0,0                 |
| SPLS 6   | Bouw en onderhoud         | 5°                    | 1,20         | 1,20                | 1,2                                      | 0,24     | 0,0      | 0,0                 |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                    | 1,20         | 1,20                | 0,0                                      | 0,24     | 0,0      | 0,0                 |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                       |              | $G_k$               | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SLS 1a   | Wind                      | 10°                   | 1,00         | 1,00                | 0,0                                      | 1,00     | 0,0      | 0,0                 |
| SLS 3  | Wind+ijs                  | -5°                   | 1,00         | 1,00                | 0,0                                      | 0,30     | 1,00     | 0,0                 |
| SLS 4  | Wind                      | -20°                  | 1,00         | 1,00                | 0,0                                      | 0,20     | 0,0      | 0,0                 |
| SLS 6  | Bouw en onderhoud         | 5°                    | 1,00         | 1,00                | 0,0                                      | 0,20     | 0,0      | 0,0                 |
| SLS 7  | PB (EDS, geen wind)       | 10°                   | 1,00         | 1,00                | 0,0                                      | 0,00     | 0,0      | 0,0                 |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 72  
 Aantal belastingcombinaties SPLS 222  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 5562



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### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -57,7         | 57,7          | 25,9          | 25,9          | 11,1          | 11,1          |
| bl2         | -56,9         | 56,9          | 25,6          | 25,6          | 11,0          | 11,0          |
| 380ct1f1    | -145,5        | 145,5         | 67,4          | 67,4          | 30,7          | 30,7          |
| 380ct1f2    | -145,5        | 145,5         | 67,4          | 67,4          | 30,7          | 30,7          |
| 380ct1f3    | -148,6        | 148,6         | 72,9          | 72,9          | 30,8          | 30,8          |
| 380ct2f1    | -145,5        | 145,5         | 67,4          | 67,4          | 30,7          | 30,7          |
| 380ct2f2    | -145,5        | 145,5         | 67,4          | 67,4          | 30,7          | 30,7          |
| 380ct2f3    | -148,6        | 148,6         | 72,9          | 72,9          | 30,8          | 30,8          |
| V-fixatie 1 | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           |
| V-fixatie 2 | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 481,9  | 493,6 | 480,0 |
| bl2         | 482,0  | 493,8 | 480,0 |
| 380ct1f1    | 480,7  | 490,5 | 480,0 |
| 380ct1f2    | 480,7  | 490,5 | 480,0 |
| 380ct1f3    | 480,9  | 491,0 | 480,0 |
| 380ct2f1    | 480,7  | 490,5 | 480,0 |
| 380ct2f2    | 480,7  | 490,5 | 480,0 |
| 380ct2f3    | 480,9  | 491,0 | 480,0 |
| V-fixatie 1 |        |       |       |
| V-fixatie 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 563,2  | 465,8 |
| bl2         | 565,6  | 465,5 |
| 380ct1f1    | 522,6  | 479,5 |
| 380ct1f2    | 522,6  | 479,5 |
| 380ct1f3    | 531,0  | 481,0 |
| 380ct2f1    | 522,6  | 479,5 |
| 380ct2f2    | 522,6  | 479,5 |
| 380ct2f3    | 531,0  | 481,0 |
| V-fixatie 1 |        |       |
| V-fixatie 2 |        |       |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

|                  |         | Wind / Weight span verhouding |
|------------------|---------|-------------------------------|
| Max. weight span | 565,6 m | 1,414 -                       |
| Min. weight span | 292,7 m | 0,732 -                       |

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**Maximale waarden back+ahead span      Maximale waarden trekkracht geleider**

| Geleider    | Fx    | Fy    | Fz   | Ft_ba  | Ft_ah |
|-------------|-------|-------|------|--------|-------|
|             | [kN]  | [kN]  | [kN] | [kN]   | [kN]  |
| bl1         | 32,2  | 50,1  | 11,1 | -63,1  | 63,1  |
| bl2         | 31,8  | 49,5  | 11,0 | -62,3  | 62,3  |
| 380ct1f1    | 112,0 | 123,9 | 30,7 | -158,3 | 158,3 |
| 380ct1f2    | 112,0 | 123,9 | 30,7 | -158,3 | 158,3 |
| 380ct1f3    | 112,2 | 133,5 | 30,8 | -162,0 | 162,0 |
| 380ct2f1    | 112,0 | 123,9 | 30,7 | -158,3 | 158,3 |
| 380ct2f2    | 112,0 | 123,9 | 30,7 | -158,3 | 158,3 |
| 380ct2f3    | 112,2 | 133,5 | 30,8 | -162,0 | 162,0 |
| V-fixatie 1 | 3,6   | 3,6   | 6,8  | 0,0    |       |
| V-fixatie 2 | 3,6   | 3,6   | 6,8  | 0,0    |       |

**EDS-belastingen geleiders**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 14,4 | 5,2  | 2,4  | -15,3 | 15,3  |
| bl2         | 14,0 | 5,1  | 2,3  | -14,9 | 14,9  |
| 380ct1f1    | 68,9 | 25,1 | 17,0 | -73,3 | 73,3  |
| 380ct1f2    | 68,9 | 25,1 | 17,0 | -73,3 | 73,3  |
| 380ct1f3    | 68,9 | 25,1 | 17,0 | -73,3 | 73,3  |
| 380ct2f1    | 68,9 | 25,1 | 17,0 | -73,3 | 73,3  |
| 380ct2f2    | 68,9 | 25,1 | 17,0 | -73,3 | 73,3  |
| 380ct2f3    | 68,9 | 25,1 | 17,0 | -73,3 | 73,3  |
| V-fixatie 1 | 0,0  | 0,0  | 5,0  | 0,0   |       |
| V-fixatie 2 | 0,0  | 0,0  | 5,0  | 0,0   |       |

**Controle uplift SLS-wind**

| Combinatie:Geleider | Fz_ba | Fz_ah |
|---------------------|-------|-------|
|                     | [kN]  | [kN]  |
| SLS 4               |       |       |
| bl1                 | 0,0   | 0,0   |
| bl2                 | 0,0   | 0,0   |
| 380ct1f1            | 0,0   | 0,0   |
| 380ct1f2            | 0,0   | 0,0   |
| 380ct1f3            | 0,0   | 0,0   |
| 380ct2f1            | 0,0   | 0,0   |
| 380ct2f2            | 0,0   | 0,0   |
| 380ct2f3            | 0,0   | 0,0   |
| V-fixatie 1         | 0,0   |       |
| V-fixatie 2         | 0,0   |       |

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**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | 0             | 840           | 285           | 31401          | 0              | 0              |
| ULS 1a_0,9_0      |             | 18            | 384           | 223           | 14176          | 630            | -92            |
| ULS 1a_0,9_0,9_90 |             | 0             | 802           | 159           | 30069          | 0              | 0              |
| ULS 3_0           |             | 8             | 678           | 421           | 25505          | 282            | -28            |
| SLS 7             |             | 0             | 322           | 223           | 11844          | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

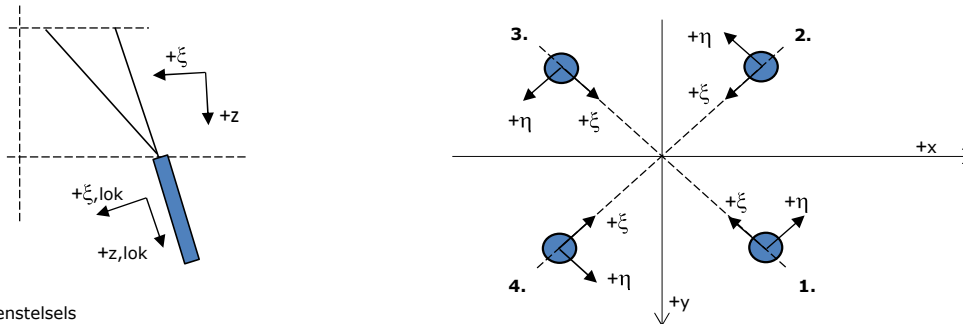
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | 0             | 1132          | 904           | 39243          | 0              | 0              |
| ULS 1a_0,9_0,9_90 | 0             | 1095          | 623           | 37911          | 0              | 0              |
| SLS 7             | 0             | 322           | 739           | 11844          | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie               | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|--------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_90            | 0             | 1132          | 679           | <b>39281</b>   | 0              | 0              |
| SPLS 3_90 Ba All Cts     | 698           | 360           | 820           | 12599          | <b>26214</b>   | -8             |
| SPLS 6a_90 Ba Ct1 Ah Ct1 | 367           | 406           | 884           | 14814          | 13759          | <b>-4832</b>   |
| ULS 1a_0,9_70            | -86           | 1092          | 680           | <b>37705</b>   | <b>-4479</b>   | -30            |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie           | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|----------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_110           | 347           | 347           | <b>1991</b>   | 0                | -490            | -100                  | 2028                |
| 2     | SPLS 1a_0 Ba All Cts | 168           | -181          | <b>988</b>    | 9                | -247            | -53                   | 1006                |
| 3     | ULS 8 Ba             | -131          | -158          | <b>839</b>    | -19              | -205            | -40                   | 855                 |
| 4     | ULS 1a_70            | -347          | 347           | <b>1991</b>   | 0                | -490            | -100                  | 2028                |

**Maximale trekbelasting**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 8 Ba                 | -65           | -93           | <b>-475</b>   | 20               | 112             | 19                    | -484                |
| 2     | ULS 1a_0,9_70            | -275          | 277           | <b>-1597</b>  | -2               | 390             | 77                    | -1627               |
| 3     | ULS 1a_0,9_110           | 275           | 277           | <b>-1597</b>  | 2                | 390             | 77                    | -1627               |
| 4     | SPLS 1a_0,9_0 Ba All Cts | 101           | -119          | <b>-629</b>   | -13              | 156             | 32                    | -641                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ba Ct1 | 161           | -64           | 265           | <b>159</b>       | -69             | -17                   | 270                 |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -77           | -143          | 200           | <b>155</b>       | -47             | -7                    | 204                 |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | 58            | 266           | -951          | <b>147</b>       | 230             | 43                    | -969                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -142          | 346           | 1418          | <b>144</b>       | -345            | -68                   | 1445                |

**Maximale torsiebelasting (negatief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 142           | 346           | 1418          | <b>-144</b>      | -345            | -68                   | 1445                |
| 2     | SPLS 6a_90 Ah Ct2 Ba Ct2 | -58           | 266           | -951          | <b>-147</b>      | 230             | 43                    | -969                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 77            | -143          | 200           | <b>-155</b>      | -47             | -7                    | 204                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -161          | -64           | 265           | <b>-159</b>      | -69             | -17                   | 270                 |

Project: GT-RLL380  
 Masttype: HB+5\_n (140 gr)  
 Mast: 69N

#### Combinatie Ftrek+Fhor

| Stijl | Combinatie               | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|--------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | ULS 8 Ba                 | -65                    | -93                    | <b>-475</b>            | <b>20</b>              | 112                    | 19                         | -484                       |
| 2     | ULS 1a_0,9_70            | -275                   | 277                    | <b>-1597</b>           | <b>-2</b>              | 390                    | 77                         | -1627                      |
| 3     | ULS 1a_0,9_110           | 275                    | 277                    | <b>-1597</b>           | <b>2</b>               | 390                    | 77                         | -1627                      |
| 4     | SPLS 1a_0,9_0 Ba All Cts | 101                    | -119                   | <b>-629</b>            | <b>-13</b>             | 156                    | 32                         | -641                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 123                    | 114                    | 681                    | 6                      | -167                   | -34                        | 694                        |
| 2     | SLS 7      | -56                    | 47                     | -311                   | 6                      | 73                     | 12                         | -317                       |
| 3     | SLS 7      | 56                     | 47                     | -311                   | -6                     | 73                     | 12                         | -317                       |
| 4     | SLS 7      | -123                   | 114                    | 681                    | -6                     | -167                   | -34                        | 694                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie               | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|--------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | ULS 1a_70                | -347                   | 347                    | <b>1991</b>            | 0                      | -490                   | -100                       | 2028                       |
| Max. trek         | ULS 1a_0,9_70            | -275                   | 277                    | <b>-1597</b>           | -2                     | 390                    | 77                         | -1627                      |
| Max. pos. torsie  | SPLS 6a_90 Ah Ct1 Ba Ct1 | 161                    | -64                    | 265                    | <b>159</b>             | -69                    | -17                        | 270                        |
| Max. neg. torsie  | SPLS 6a_90 Ba Ct1 Ah Ct1 | -161                   | -64                    | 265                    | <b>-159</b>            | -69                    | -17                        | 270                        |
| Comb. trek+torsie | ULS 1a_0,9_70            | -275                   | 277                    | <b>-1597</b>           | <b>-2</b>              | 390                    | 77                         | -1627                      |

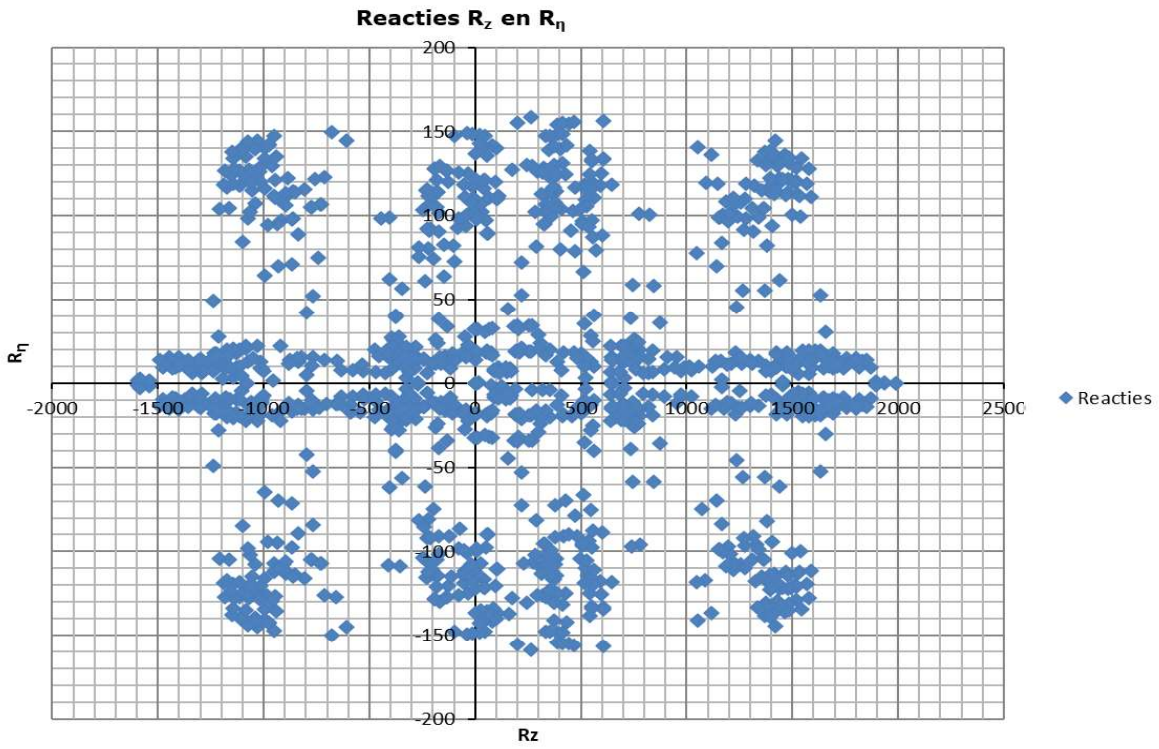
#### Maximale trekbelasting SLS

| Stijl | Combinatie                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_110 Ah All Cts | -53                    | -78                    | <b>-408</b>            | 18                     | 93                     | 13                         | -416                       |
| 2     | ULS 1a_0,9_70             | -275                   | 277                    | <b>-1597</b>           | -2                     | 390                    | 77                         | -1627                      |
| 3     | ULS 1a_0,9_110            | 275                    | 277                    | <b>-1597</b>           | 2                      | 390                    | 77                         | -1627                      |
| 4     | SPLS 3_0,9_70 Ba All Cts  | 53                     | -78                    | <b>-408</b>            | -18                    | 93                     | 13                         | -416                       |

#### Maximale drukbelasting SLS

| Stijl | Combinatie            | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | ULS 1a_110            | 347                    | 347                    | <b>1991</b>            | 0                      | -490                   | -100                       | 2028                       |
| 2     | SPLS 3_70 Ba All Cts  | 120                    | -143                   | <b>773</b>             | 17                     | -186                   | -34                        | 788                        |
| 3     | SPLS 3_110 Ah All Cts | -120                   | -143                   | <b>773</b>             | -17                    | -186                   | -34                        | 788                        |
| 4     | ULS 1a_70             | -347                   | 347                    | <b>1991</b>            | 0                      | -490                   | -100                       | 2028                       |

Project: GT-RLL380  
Masttype: HB+5\_n (140 gr)  
Mast: 69N





Project: GT-RLL380  
 Tower: HB+5\_n (160 gr)  
 Number: 69N

Auteur: TBR  
 Versie: v12.0

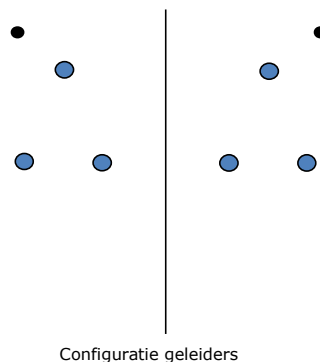
### Geleiderbelastingen

#### Algemeen

Benaming HB+5\_n (160 gr)  
 Masttype Hoekmast  
 Aantal circuits 2  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 2

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 50 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 50 jaar  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsgebied fasegeleider B  
 IJsgebied bliksemgeleider A



#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                     |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A         | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A         | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                      |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A         | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A         | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging     | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Circuit 2      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Bliksemdraad 1 | Afspanketting | 0,10         | 0,20       | 0,20                       |
| Bliksemdraad 2 | Afspanketting | 0,10         | 0,20       | 0,20                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 32,7 m       | 32,7 m       | -16,3 m                                |
| Circuit 1      | 11         | 380ct1f2 | 32,7 m       | 32,7 m       | -9,0 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 44,0 m       | 44,0 m       | -12,7 m                                |
| Circuit 2      | 20         | 380ct2f1 | 32,7 m       | 32,7 m       | 16,3 m                                 |
| Circuit 2      | 21         | 380ct2f2 | 32,7 m       | 32,7 m       | 9,0 m                                  |
| Circuit 2      | 22         | 380ct2f3 | 44,0 m       | 44,0 m       | 12,7 m                                 |
| Bliksemdraad 1 | 1          | bl1      | 48,2 m       | 48,2 m       | -18,7 m                                |
| Bliksemdraad 2 | 3          | bl2      | 48,2 m       | 48,2 m       | 18,7 m                                 |

Project: GT-RLL380  
 Tower: HB+5\_n (160 gr)  
 Number: 69N

**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead   |   |
|------------------------------------|---------------------------|---------|---|
| Verhoging voor windbelasting       | 5,0 m                     | 5,0 m   | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -10,0 m                   | -10,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |         |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

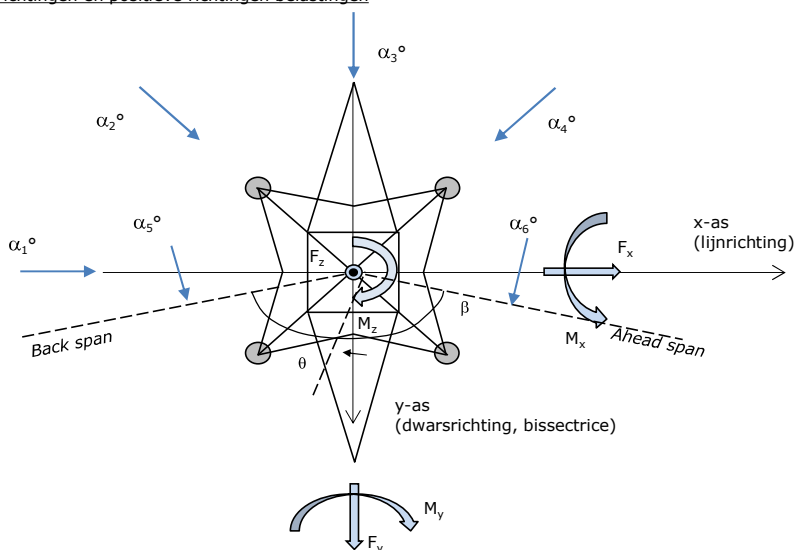
| Circuits       | Aanduiding | Nummer   | Hoogteverschil  |                  | Richtingsverandering |                  |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
|                |            |          | $\Delta h$ back | $\Delta h$ ahead | $\Delta y$ back      | $\Delta y$ ahead |
| Circuit 1      | 10         | 380ct1f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 11         | 380ct1f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 12         | 380ct1f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 20         | 380ct2f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 21         | 380ct2f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 22         | 380ct2f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 1 | 1          | bl1      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 2 | 3          | bl2      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek $\beta$                           | 160 °      |         |
| Rotatie mast t.o.v. bissectrice $\theta$   | 0 °        |         |
| Vaklengte                                  | 400        | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 45 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 135 °   |
|  | $\alpha_5$ | 80 °    |
|  | $\alpha_6$ | 100 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



**Beschouwd aantal windrichtingen**

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |



Project: GT-RLL380  
 Tower: HB+5\_n (160 gr)  
 Number: 69N

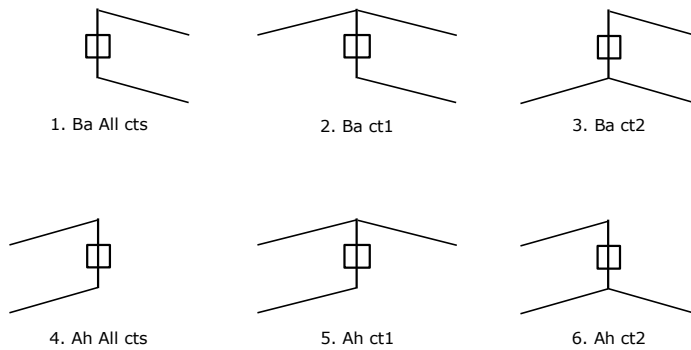
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | bl1      | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | bl2      | 0             | 1    | 1                        | 0    | 1                  | 0    |

### Belastingsituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

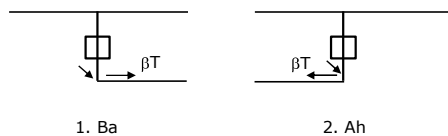
Principe belastingssituaties:



### Belastingsituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



Project: GT-RLL380  
 Tower: HB+5\_n (160 gr)  
 Number: 69N

### Belastingsituaties 6. Bouw- en onderhoud

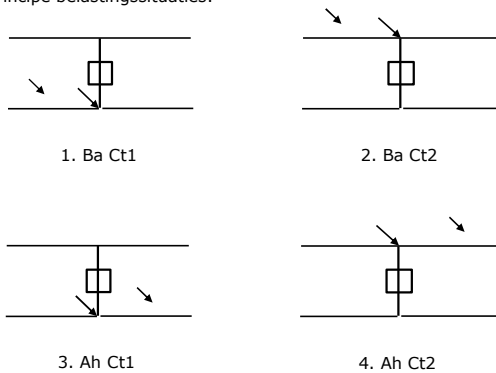
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



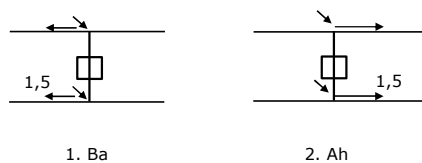
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten

Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast

Door gebruiker via het belastingspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

Project: GT-RLL380  
 Tower: HB+5\_n (160 gr)  
 Number: 69N

## Mastconstructie

### Eigenschappen

|   |                 |         |
|---|-----------------|---------|
| Masttype                                    | Hoekmast        |         |
| Mastbenaming                                | HB+5_n (160 gr) |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m           |         |
| Masthoogte t.o.v. voetplaat                 | 50,0 m          |         |
| Gewicht mast                                | 516,0 kN        |         |
| <i>Breedte en helling mast bij fundatie</i> |                 |         |
|   | x-ri.           | y-ri.   |
| Pootsprei                                   | 11,94           | 11,94 m |
| Helling van de randstijl                    | 0,139           | 0,139 - |
| Factor spatkracht                           | 1,3             | 1,3 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,00 (Masthoogte < 60 m)              |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 12,25    | 11,94                 | 8,54                  | 12,25     | 0,139                 | 125,45                              | 17,57                               | 0,14                                      | 3,21           |
| Eerste tussenstuk | 24,56    | 8,54                  | 5,69                  | 12,31     | 0,116                 | 87,60                               | 16,12                               | 0,18                                      | 3,00           |
| Tweede tussenstuk | 32,70    | 5,69                  | 3,80                  | 8,14      | 0,116                 | 38,62                               | 12,69                               | 0,33                                      | 2,44           |
| Bovenstuk 1       | 40,50    | 3,80                  | 3,19                  | 7,80      | 0,039                 | 27,26                               | 8,02                                | 0,29                                      | 2,56           |
| Bovenstuk 2       | 48,00    | 3,19                  | 2,60                  | 7,50      | 0,039                 | 21,71                               | 6,12                                | 0,28                                      | 2,60           |
| Topstuk           | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse     | 32,70    | 14,86                 |                       | 4,00      |                       | 29,72                               | 7,50                                | 0,25                                      | 2,71           |
| Boventraverse     | 44,00    | 17,19                 |                       | 4,00      |                       | 34,39                               | 8,70                                | 0,25                                      | 2,71           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 12,25    | 11,94                 | 8,54                  | 12,25     | 0,139                 | 125,45                              | 17,57                               | 0,14                                      | 3,21           |
| Eerste tussenstuk | 24,56    | 8,54                  | 5,69                  | 12,31     | 0,116                 | 87,60                               | 16,12                               | 0,18                                      | 3,00           |
| Tweede tussenstuk | 32,70    | 5,69                  | 3,80                  | 8,14      | 0,116                 | 38,62                               | 12,69                               | 0,33                                      | 2,44           |
| Bovenstuk 1       | 40,50    | 3,80                  | 3,19                  | 7,80      | 0,039                 | 27,26                               | 8,02                                | 0,29                                      | 2,56           |
| Bovenstuk 2       | 48,00    | 3,19                  | 2,60                  | 7,50      | 0,039                 | 21,71                               | 6,12                                | 0,28                                      | 2,60           |
| Topstuk           | 50,00    | 2,60                  |                       | 2,00      |                       | 2,60                                | 0,40                                | 0,15                                      | 3,14           |
| Ondertraverse     | 32,70    | 14,86                 |                       | 4,00      |                       | 29,72                               | 7,50                                | 0,25                                      | 2,71           |
| Boventraverse     | 44,00    | 17,19                 |                       | 4,00      |                       | 34,39                               | 8,70                                | 0,25                                      | 2,71           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

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#### Windoppervlak feeders telecominstallaties

| Onderdeel         | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk         | 0,20                  | 0,71   | 12,3 | 1,7            |
| Eerste tussenstuk | 0,20                  | 0,71   | 12,3 | 1,7            |
| Tweede tussenstuk | 0,20                  | 0,71   | 8,1  | 1,2            |
| Bovenstuk 1       |                       |        |      |                |
| Bovenstuk 2       |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>i</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,0                 | 35    | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 39,5                    | 33,5                    | 0,0                     | -33,5                   | 6,1                    | 241,9                    | 205,3                    | 0,0                      | -205,3                   |
| Eerste tussenstuk | 0,86                                   | 41,4                    | 35,1                    | 0,0                     | -35,1                   | 18,4                   | 762,1                    | 646,6                    | 0,0                      | -646,6                   |
| Tweede tussenstuk | 0,98                                   | 30,1                    | 25,6                    | 0,0                     | -25,6                   | 28,6                   | 863,1                    | 732,4                    | 0,0                      | -732,4                   |
| Bovenstuk 1       | 1,05                                   | 21,5                    | 18,2                    | 0,0                     | -18,2                   | 36,6                   | 786,4                    | 667,2                    | 0,0                      | -667,2                   |
| Bovenstuk 2       | 1,10                                   | 17,5                    | 14,9                    | 0,0                     | -14,9                   | 44,3                   | 774,5                    | 657,2                    | 0,0                      | -657,2                   |
| Topstuk           | 1,13                                   | 1,4                     | 1,2                     | 0,0                     | -1,2                    | 49,0                   | 69,7                     | 59,1                     | 0,0                      | -59,1                    |
| Ondertraverse     | 1,02                                   | 41,7                    | 24,7                    | 0,0                     | -24,7                   | 34,0                   | 1418,0                   | 842,2                    | 0,0                      | -842,2                   |
| Boventraverse     | 1,11                                   | 52,2                    | 31,0                    | 0,0                     | -31,0                   | 45,3                   | 2365,5                   | 1405,1                   | 0,0                      | -1405,1                  |

|               |              |              |            |               |               |               |            |                |
|---------------|--------------|--------------|------------|---------------|---------------|---------------|------------|----------------|
| <b>Totaal</b> | <b>245,3</b> | <b>184,3</b> | <b>0,0</b> | <b>-184,3</b> | <b>7281,2</b> | <b>5215,2</b> | <b>0,0</b> | <b>-5215,2</b> |
|---------------|--------------|--------------|------------|---------------|---------------|---------------|------------|----------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 0,0                     | 33,5                    | 39,5                    | 33,5                    | 6,1                    | 0,0                      | 205,3                    | 241,9                    | 205,3                    |
| Eerste tussenstuk | 0,86                                   | 0,0                     | 35,1                    | 41,4                    | 35,1                    | 18,4                   | 0,0                      | 646,6                    | 762,1                    | 646,6                    |
| Tweede tussenstuk | 0,98                                   | 0,0                     | 25,6                    | 30,1                    | 25,6                    | 28,6                   | 0,0                      | 732,4                    | 863,1                    | 732,4                    |
| Bovenstuk 1       | 1,05                                   | 0,0                     | 18,2                    | 21,5                    | 18,2                    | 36,6                   | 0,0                      | 667,2                    | 786,4                    | 667,2                    |
| Bovenstuk 2       | 1,10                                   | 0,0                     | 14,9                    | 17,5                    | 14,9                    | 44,3                   | 0,0                      | 657,2                    | 774,5                    | 657,2                    |
| Topstuk           | 1,13                                   | 0,0                     | 1,2                     | 1,4                     | 1,2                     | 49,0                   | 0,0                      | 59,1                     | 69,7                     | 59,1                     |
| Ondertraverse     | 1,02                                   | 0,0                     | 24,7                    | 16,7                    | 24,7                    | 34,0                   | 0,0                      | 842,2                    | 567,2                    | 842,2                    |
| Boventraverse     | 1,11                                   | 0,0                     | 31,0                    | 20,9                    | 31,0                    | 45,3                   | 0,0                      | 1405,1                   | 946,2                    | 1405,1                   |

|               |            |              |              |              |            |               |               |               |
|---------------|------------|--------------|--------------|--------------|------------|---------------|---------------|---------------|
| <b>Totaal</b> | <b>0,0</b> | <b>184,3</b> | <b>189,0</b> | <b>184,3</b> | <b>0,0</b> | <b>5215,2</b> | <b>5011,1</b> | <b>5215,2</b> |
|---------------|------------|--------------|--------------|--------------|------------|---------------|---------------|---------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub> | F <sub>y</sub> | F <sub>z</sub> | M <sub>x</sub> | M <sub>y</sub> | M <sub>z</sub> |
|--------------------------|----------------|----------------|----------------|----------------|----------------|----------------|
|                          | [kN]           | [kN]           | [kN]           | [kNm]          | [kNm]          | [kNm]          |
| Permanente belasting     | 0              | 0              | 516            | 0              | 0              | 0              |
| Windrichting 0°          | 251            | 0              | 0              | 0              | 7498           | 0              |
| Windrichting 45°         | 189            | 189            | 0              | 5368           | 5368           | 0              |
| Windrichting 90°         | 0              | 195            | 0              | 5228           | 0              | 0              |
| Windrichting 135°        | -189           | 189            | 0              | 5368           | -5368          | 0              |

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### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| 380ct2f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct2f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct2f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,2                           | 48,70             | 1,13                             | 1,2               | 0,27                |
| bl2      | 0,10                   | 1      | 0,1                 | 0,2           | 0,2                           | 48,70             | 1,13                             | 1,2               | 0,27                |

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#### Windbelasting back

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| 380ct2f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| bl1      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,19  | 22,24         | 17,5  | 19,3        | 63,1              | 50,0        | 55,0            |
| bl2      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,20  | 22,13         | 17,5  | 19,2        | 63,0              | 49,9        | 54,9            |

#### Windbelasting ahead

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| 380ct2f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct2f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| bl1      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,19  | 22,24         | 17,5  | 19,3        | 63,1              | 50,0        | 55,0            |
| bl2      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,20  | 22,13         | 17,5  | 19,2        | 63,0              | 49,9        | 54,9            |

NB: belastingen  $w_v$  gelden voor bundel

Project: GT-RL380  
 Masttype: HB+5\_n (160 gr)  
 Mast: 69N

Auteur: TBR  
 Versie: v12.0

**Geleiderbelastingen**
**Uitgangspunten**

Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 50 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |                            |                                | $\gamma_Q$                               |          |          | $\gamma_a$ |
|--|---------------------------|------------------------------|----------------------------|--------------------------------|--|----------|----------|------------|
| Belastingsgeval  | omschrijving              | Temp °C                      | $\gamma_G$<br>$G_{k,mast}$ | $\gamma_G$<br>$G_{k,geleider}$ | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ | $A_k$      |
| ULS 1a   | Wind                      | 10°                          | 1,20                       | 1,20                           | 0,00                                     | 1,50     | 0,00     | 0,0        |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90                       | 1,20                           | 0,00                                     | 1,50     | 0,00     | 0,0        |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90                       | 0,90                           | 0,00                                     | 1,50     | 0,00     | 0,0        |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20                       | 1,20                           | 0,00                                     | 0,45     | 1,50     | 0,0        |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90                       | 1,20                           | 0,00                                     | 0,45     | 1,50     | 0,0        |
| ULS 4  | Koude+wind                | -20°                         | 1,20                       | 1,20                           | 0,00                                     | 0,30     | 0,00     | 0,0        |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90                       | 1,20                           | 0,00                                     | 0,30     | 0,00     | 0,0        |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00                       | 1,00                           | 1,00                                     | 0,00     | 0,00     | 1,0        |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00                       | 1,00                           | 0,00                                     | 0,00     | 0,00     | 1,0        |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 1,50                                     | 0,30     | 0,00     | 0,0        |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 0,00                                     | 0,30     | 0,00     | 0,0        |
| ULS 7  | Permanent                 | 10°                          | 1,35                       | 1,35                           | 0,00                                     | 0,00     | 0,00     | 0,0        |
| ULS 8  | Special                   | 10°                          | 1,00                       | 1,00                           | 0,00                                     | 0,00     | 0,00     | 1,0        |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              | $\gamma_G$<br>$G_k$        |                                | $\gamma_Q$<br>$Q_{pk}$ $Q_{wk}$ $Q_{ik}$ |          |          | $A_k$      |
| SPLS 1a  | Wind                      | 10°                          | 1,20                       | 1,20                           | 0,0                                      | 0,78     | 0,00     | 0,0        |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90                       | 1,20                           | 0,0                                      | 0,78     | 0,00     | 0,0        |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90                       | 0,90                           | 0,0                                      | 0,78     | 0,00     | 0,0        |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20                       | 1,20                           | 0,0                                      | 0,36     | 0,34     | 0,0        |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90                       | 1,20                           | 0,0                                      | 0,36     | 0,34     | 0,0        |
| SPLS 4   | Koude+wind                | -20°                         | 1,20                       | 1,20                           | 0,0                                      | 0,24     | 0,00     | 0,0        |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90                       | 1,20                           | 0,0                                      | 0,24     | 0,00     | 0,0        |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 1,2                                      | 0,24     | 0,0      | 0,0        |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 0,0                                      | 0,24     | 0,0      | 0,0        |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              | $G_k$                      |                                | $Q_{pk}$ $Q_{wk}$ $Q_{ik}$               |          |          | $A_k$      |
| SLS 1a   | Wind                      | 10°                          | 1,00                       | 1,00                           | 0,0                                      | 1,00     | 0,0      | 0,0        |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00                       | 1,00                           | 0,0                                      | 0,30     | 1,00     | 0,0        |
| SLS 4  | Wind                      | -20°                         | 1,00                       | 1,00                           | 0,0                                      | 0,20     | 0,0      | 0,0        |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00                       | 1,00                           | 0,0                                      | 0,20     | 0,0      | 0,0        |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00                       | 1,00                           | 0,0                                      | 0,00     | 0,0      | 0,0        |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 72  
 Aantal belastingcombinaties SPLS 222  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 5562

Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr)  
 Mast: 69N

### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -61,3         | 61,3          | 15,5          | 15,5          | 11,1          | 11,1          |
| bl2         | -60,5         | 60,5          | 15,4          | 15,4          | 11,0          | 11,0          |
| 380ct1f1    | -154,3        | 154,3         | 43,9          | 43,9          | 30,7          | 30,7          |
| 380ct1f2    | -154,3        | 154,3         | 43,9          | 43,9          | 30,7          | 30,7          |
| 380ct1f3    | -157,7        | 157,7         | 47,7          | 47,7          | 30,8          | 30,8          |
| 380ct2f1    | -154,3        | 154,3         | 43,9          | 43,9          | 30,7          | 30,7          |
| 380ct2f2    | -154,3        | 154,3         | 43,9          | 43,9          | 30,7          | 30,7          |
| 380ct2f3    | -157,7        | 157,7         | 47,7          | 47,7          | 30,8          | 30,8          |
| V-fixatie 1 | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           |
| V-fixatie 2 | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 480,1  | 494,5 | 480,0 |
| bl2         | 480,1  | 494,7 | 480,0 |
| 380ct1f1    | 480,0  | 490,9 | 480,0 |
| 380ct1f2    | 480,0  | 490,9 | 480,0 |
| 380ct1f3    | 480,1  | 491,5 | 480,0 |
| 380ct2f1    | 480,0  | 490,9 | 480,0 |
| 380ct2f2    | 480,0  | 490,9 | 480,0 |
| 380ct2f3    | 480,1  | 491,5 | 480,0 |
| V-fixatie 1 |        |       |       |
| V-fixatie 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 573,8  | 466,7 |
| bl2         | 576,4  | 466,4 |
| 380ct1f1    | 529,2  | 480,5 |
| 380ct1f2    | 529,2  | 480,5 |
| 380ct1f3    | 538,5  | 482,3 |
| 380ct2f1    | 529,2  | 480,5 |
| 380ct2f2    | 529,2  | 480,5 |
| 380ct2f3    | 538,5  | 482,3 |
| V-fixatie 1 |        |       |
| V-fixatie 2 |        |       |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

|                  | Wind / Weight span verhouding |
|------------------|-------------------------------|
| Max. weight span | 576,4 m<br>1,441 -            |
| Min. weight span | 285,2 m<br>0,713 -            |



Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr)  
 Mast: 69N

**Maximale waarden back+ahead span      Maximale waarden trekkracht geleider**

| Geleider    | Fx    | Fy   | Fz   | Ft_ba  | Ft_ah |
|-------------|-------|------|------|--------|-------|
|             | [kN]  | [kN] | [kN] | [kN]   | [kN]  |
| bl1         | 34,0  | 30,6 | 11,1 | -63,1  | 63,1  |
| bl2         | 33,5  | 30,3 | 11,0 | -62,3  | 62,3  |
| 380ct1f1    | 118,1 | 85,8 | 30,7 | -158,3 | 158,3 |
| 380ct1f2    | 118,1 | 85,8 | 30,7 | -158,3 | 158,3 |
| 380ct1f3    | 118,4 | 93,1 | 30,8 | -162,0 | 162,0 |
| 380ct2f1    | 118,1 | 85,8 | 30,7 | -158,3 | 158,3 |
| 380ct2f2    | 118,1 | 85,8 | 30,7 | -158,3 | 158,3 |
| 380ct2f3    | 118,4 | 93,1 | 30,8 | -162,0 | 162,0 |
| V-fixatie 1 | 3,6   | 3,6  | 6,8  | 0,0    |       |
| V-fixatie 2 | 3,6   | 3,6  | 6,8  | 0,0    |       |

**EDS-belastingen geleiders**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 15,1 | 2,7  | 2,4  | -15,3 | 15,3  |
| bl2         | 14,7 | 2,6  | 2,3  | -14,9 | 14,9  |
| 380ct1f1    | 72,2 | 12,7 | 17,0 | -73,3 | 73,3  |
| 380ct1f2    | 72,2 | 12,7 | 17,0 | -73,3 | 73,3  |
| 380ct1f3    | 72,2 | 12,7 | 17,0 | -73,3 | 73,3  |
| 380ct2f1    | 72,2 | 12,7 | 17,0 | -73,3 | 73,3  |
| 380ct2f2    | 72,2 | 12,7 | 17,0 | -73,3 | 73,3  |
| 380ct2f3    | 72,2 | 12,7 | 17,0 | -73,3 | 73,3  |
| V-fixatie 1 | 0,0  | 0,0  | 5,0  | 0,0   |       |
| V-fixatie 2 | 0,0  | 0,0  | 5,0  | 0,0   |       |

**Controle uplift SLS-wind**

| Combinatie:Geleider | Fz_ba | Fz_ah |
|---------------------|-------|-------|
|                     | [kN]  | [kN]  |
| SLS 4 bl1           | 0,0   | 0,0   |
| bl2                 | 0,0   | 0,0   |
| 380ct1f1            | 0,0   | 0,0   |
| 380ct1f2            | 0,0   | 0,0   |
| 380ct1f3            | 0,0   | 0,0   |
| 380ct2f1            | 0,0   | 0,0   |
| 380ct2f2            | 0,0   | 0,0   |
| 380ct2f3            | 0,0   | 0,0   |
| V-fixatie 1         | 0,0   |       |
| V-fixatie 2         | 0,0   |       |

Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr)  
 Mast: 69N

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | 0             | 586           | 288           | 21876          | 0              | 0              |
| ULS 1a_0,9_0      |             | 9             | 192           | 223           | 7025           | 290            | -92            |
| ULS 1a_0,9_0,9_90 |             | 0             | 569           | 157           | 21278          | 0              | 0              |
| ULS 3_0           |             | 3             | 344           | 421           | 12856          | 99             | -28            |
| SLS 7             |             | 0             | 163           | 223           | 5950           | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

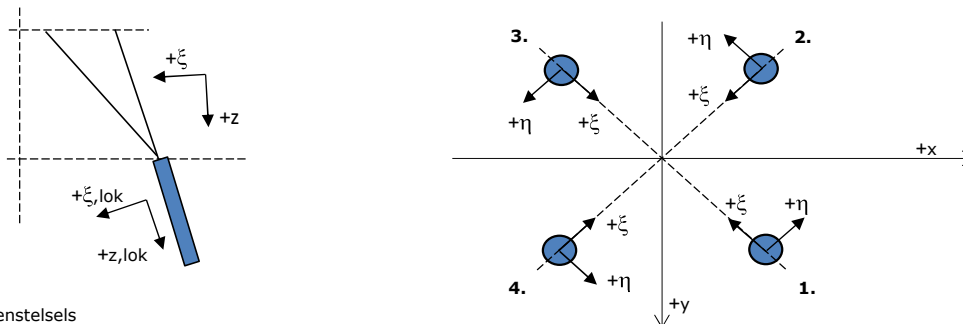
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | 0             | 879           | 907           | 29718          | 0              | 0              |
| ULS 1a_0,9_0,9_90 | 0             | 861           | 622           | 29120          | 0              | 0              |
| SLS 7             | 0             | 163           | 739           | 5950           | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie                | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_90             | 0             | 879           | 678           | <b>29757</b>   | 0              | 0              |
| SPLS 3_90 Ba All Cts      | 752           | 241           | 821           | 8119           | <b>28259</b>   | -8             |
| SPLS 6a_90 Ba Ct1 Ah Ct1  | 387           | 248           | 884           | 8913           | 14509          | <b>-5095</b>   |
| SPLS 1a_0,9_90 Ba All Cts | 674           | 353           | 622           | <b>11463</b>   | <b>25247</b>   | -7             |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie            | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|-----------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 1a_90 Ba All Cts | 291           | 315           | <b>1737</b>   | -17                | -428              | -88                   | 1770                |
| 2     | SPLS 3_0 Ba All Cts   | 193           | -212          | <b>1170</b>   | 14                 | -287              | -58                   | 1192                |
| 3     | ULS 8 Ba              | -172          | -197          | <b>1074</b>   | -17                | -261              | -51                   | 1094                |
| 4     | SPLS 1a_90 Ah All Cts | -291          | 315           | <b>1737</b>   | 17                 | -428              | -88                   | 1770                |

**Maximale trekbelasting**

| Stijl | Combinatie                | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | ULS 8 Ba                  | -106          | -132          | <b>-710</b>   | 18                 | 168               | 29                    | -724                |
| 2     | SPLS 1a_0,9_90 Ah All Cts | -227          | 250           | <b>-1382</b>  | -16                | 338               | 67                    | -1408               |
| 3     | SPLS 1a_0,9_90 Ba All Cts | 227           | 250           | <b>-1382</b>  | 16                 | 338               | 67                    | -1408               |
| 4     | SPLS 3_0,9_0 Ba All Cts   | 126           | -148          | <b>-805</b>   | -16                | 194               | 36                    | -820                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ba Ct1 | 117           | -114          | -13           | <b>163</b>         | -2                | -4                    | -14                 |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -33           | -193          | 479           | <b>160</b>         | -114              | -20                   | 488                 |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | 13            | 238           | -735          | <b>159</b>         | 178               | 34                    | -749                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -97           | 318           | 1202          | <b>156</b>         | -294              | -58                   | 1225                |

**Maximale torsiebelasting (negatief)**

| Stijl | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 97            | 318           | 1202          | <b>-156</b>        | -294              | -58                   | 1225                |
| 2     | SPLS 6a_90 Ah Ct2 Ba Ct2 | -13           | 238           | -735          | <b>-159</b>        | 178               | 34                    | -749                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 33            | -193          | 479           | <b>-160</b>        | -114              | -20                   | 488                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -117          | -114          | -13           | <b>-163</b>        | -2                | -4                    | -14                 |

Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr)  
 Mast: 69N

#### Combinatie Ftrek+Fhor

| Stijl | Combinatie                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | ULS 8 Ba                  | -106                   | -132                   | <b>-710</b>            | <b>18</b>              | 168                    | 29                         | -724                       |
| 2     | SPLS 1a_0,9_90 Ah All Cts | -227                   | 250                    | <b>-1382</b>           | <b>-16</b>             | 338                    | 67                         | -1408                      |
| 3     | SPLS 1a_0,9_90 Ba All Cts | 227                    | 250                    | <b>-1382</b>           | <b>16</b>              | 338                    | 67                         | -1408                      |
| 4     | SPLS 3_0,9_0 Ba All Cts   | 126                    | -148                   | <b>-805</b>            | <b>-16</b>             | 194                    | 36                         | -820                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 78                     | 74                     | 434                    | 3                      | -108                   | -23                        | 442                        |
| 2     | SLS 7      | -12                    | 8                      | -64                    | 3                      | 14                     | 1                          | -66                        |
| 3     | SLS 7      | 12                     | 8                      | -64                    | -3                     | 14                     | 1                          | -66                        |
| 4     | SLS 7      | -78                    | 74                     | 434                    | -3                     | -108                   | -23                        | 442                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|---------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | SPLS 1a_90 Ba All Cts     | 291                    | 315                    | <b>1737</b>            | -17                    | -428                   | -88                        | 1770                       |
| Max. trek         | SPLS 1a_0,9_90 Ba All Cts | 227                    | 250                    | <b>-1382</b>           | 16                     | 338                    | 67                         | -1408                      |
| Max. pos. torsie  | SPLS 6a_90 Ah Ct1 Ba Ct1  | 117                    | -114                   | -13                    | <b>163</b>             | -2                     | -4                         | -14                        |
| Max. neg. torsie  | SPLS 6a_90 Ba Ct1 Ah Ct1  | -117                   | -114                   | -13                    | <b>-163</b>            | -2                     | -4                         | -14                        |
| Comb. trek+torsie | SPLS 1a_0,9_90 Ba All Cts | 227                    | 250                    | <b>-1382</b>           | <b>16</b>              | 338                    | 67                         | -1408                      |

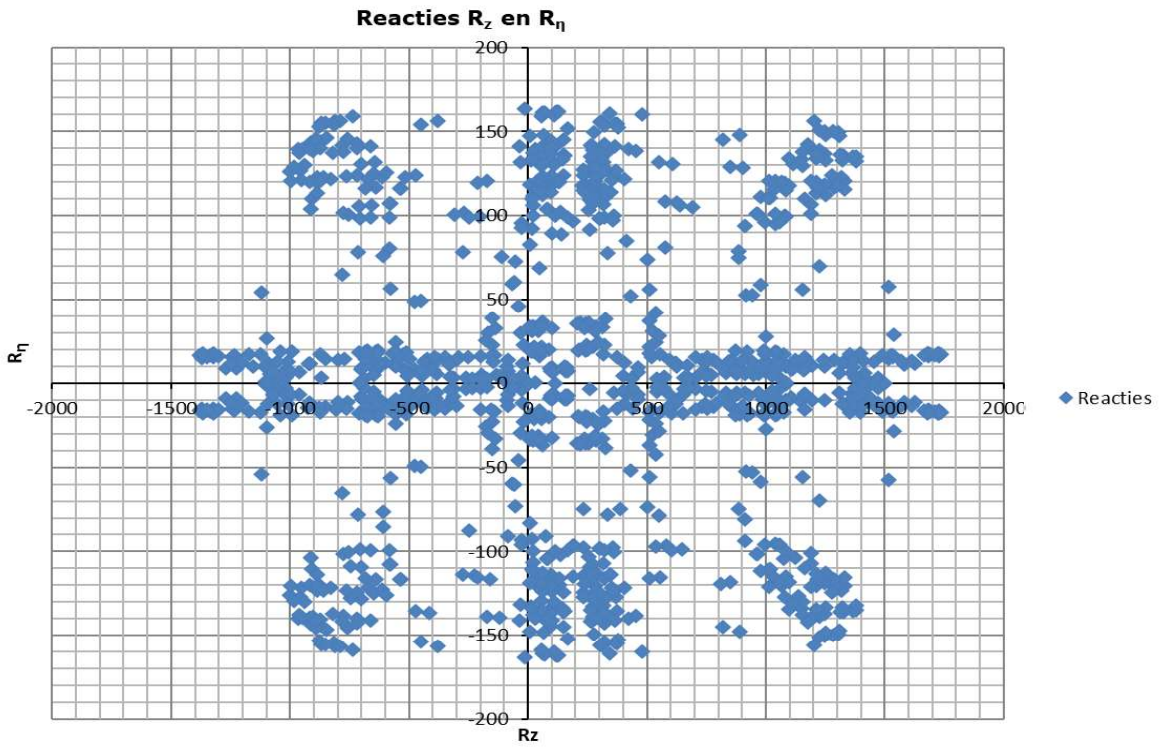
#### Maximale trekbelasting SLS

| Stijl | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_100 Ah All Cts  | -98                    | -124                   | <b>-680</b>            | 18                     | 157                    | 24                         | -693                       |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -227                   | 248                    | <b>-1370</b>           | -15                    | 336                    | 68                         | -1396                      |
| 3     | SPLS 1a_0,9_100 Ba Ct2     | 70                     | 265                    | <b>-962</b>            | 137                    | 237                    | 49                         | -980                       |
| 4     | SPLS 3_0,9_100 Ba Ct2      | 85                     | 104                    | <b>16</b>              | 134                    | -13                    | -10                        | 16                         |

#### Maximale drukbelasting SLS

| Stijl | Combinatie            | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_100 Ba Ct2    | 316                    | 153                    | <b>1329</b>            | 115                    | -332                   | -71                        | 1354                       |
| 2     | SPLS 3_100 Ba Ct2     | -47                    | -169                   | <b>379</b>             | 152                    | -86                    | -12                        | 387                        |
| 3     | SPLS 3_100 Ah All Cts | -165                   | -189                   | <b>1045</b>            | -17                    | -250                   | -45                        | 1065                       |
| 4     | SPLS 3_80 Ah All Cts  | -285                   | 310                    | <b>1727</b>            | 18                     | -421                   | -82                        | 1760                       |

Project: GT-RLL380  
Masttype: HB+5\_n (160 gr)  
Mast: 69N





Project: GT-RLL380  
 Tower: HB+5\_n (160 gr bouwfase)  
 Number: 69N

Auteur: TBR  
 Versie: v12.0

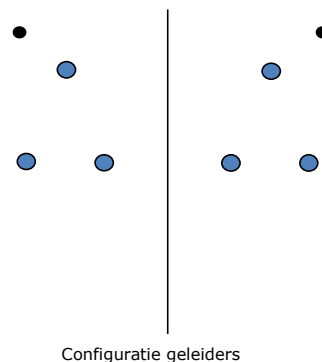
### Geleiderbelastingen

#### Algemeen

Benaming HB+5\_n (160 gr bouwfase)  
 Masttype Hoekmast  
 Aantal circuits 1  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 1

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 15 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsg gebied fasegeleider B  
 IJsg gebied bliksemgeleider A



#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging     | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------|--------------|------------|----------------------------|
| Circuit 1      | Afspanketting | 6,00         | 7,90       | 2,00                       |
| Bliksemdraad 1 | Afspanketting | 0,10         | 0,20       | 0,20                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 32,7 m       | 32,7 m       | -16,3 m                                |
| Circuit 1      | 11         | 380ct1f2 | 32,7 m       | 32,7 m       | -9,0 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 44,0 m       | 44,0 m       | -12,7 m                                |
| Bliksemdraad 1 | 1          | bl1      | 48,2 m       | 48,2 m       | -18,7 m                                |

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**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead   |   |
|------------------------------------|---------------------------|---------|---|
| Verhoging voor windbelasting       | 5,0 m                     | 5,0 m   | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -10,0 m                   | -10,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |         |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

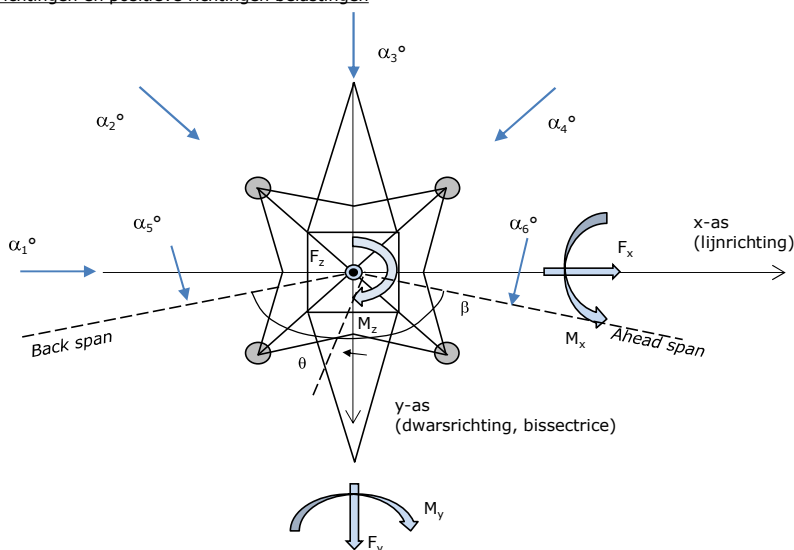
| Circuits       | Aanduiding | Nummer   | Hoogteverschil  |                  | Richtingsverandering |                  |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
|                |            |          | $\Delta h$ back | $\Delta h$ ahead | $\Delta y$ back      | $\Delta y$ ahead |
| Circuit 1      | 10         | 380ct1f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 11         | 380ct1f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 12         | 380ct1f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 1 | 1          | bl1      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek $\beta$                           | 160 °      |         |
| Rotatie mast t.o.v. bissectrice $\theta$   | 0 °        |         |
| Vaklengte                                  | 400        | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 80 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 100 °   |
|  | $\alpha_5$ | 225 °   |
|  | $\alpha_6$ | 270 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



**Beschouwd aantal windrichtingen**

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

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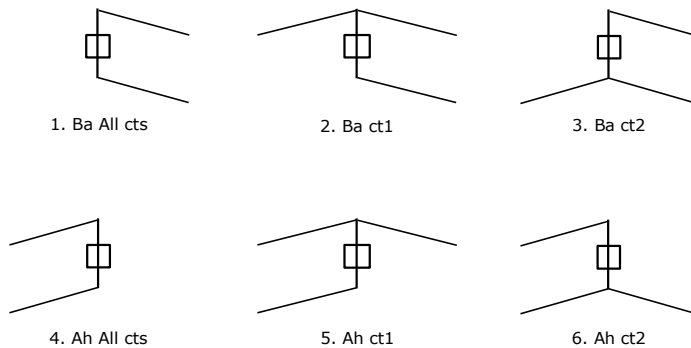
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |

### Belastingssituaties SPLS

Beschouwde situaties SPLS: 1 t/m 6, alle mogelijke situaties.

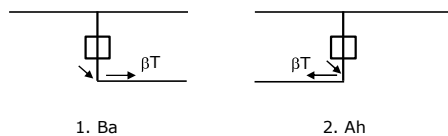
Principe belastingssituaties:



### Belastingssituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:





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**Belastingsituaties 6. Bouw- en onderhoud**

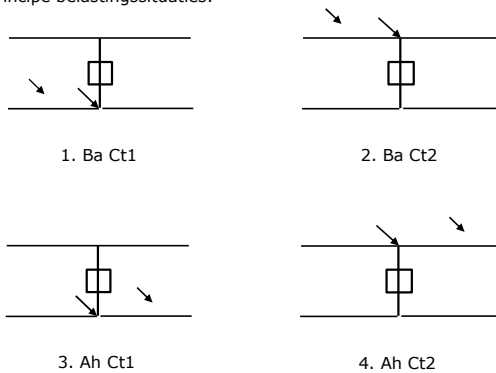
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



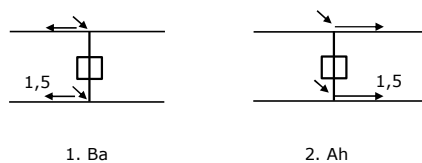
**Belastingsituaties 8. Lijndansen als statische belasting**

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



**Belastingcombinatie 8. Lijndansen als dynamische belasting**

Alleen van toepassing op hoek- en eindmasten  
 Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast  
 Door gebruiker via het belastingspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

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## Mastconstructie

### Eigenschappen

| Masttype                                    | Hoekmast                 |         |
|---|--------------------------|---------|
| Mastbenaming                                | HB+5_n (160 gr bouwfase) |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m                    |         |
| Masthoogte t.o.v. voetplaat                 | 50,0 m                   |         |
| Gewicht mast                                | 516,0 kN                 |         |
| <i>Breedte en helling mast bij fundatie</i> |                          |         |
|   | x-ri.                    | y-ri.   |
| Pootsprei                                   | 11,94                    | 11,94 m |
| Helling van de randstijl                    | 0,139                    | 0,139 - |
| Factor spatkracht                           | 1,3                      | 1,3 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,00 (Masthoogte < 60 m)              |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving      | h<br>[m] | $b_1$<br>[m] | $b_2$<br>[m] | $\Delta h$<br>[m] | $\Delta_x$<br>[m] | $A_0$<br>[m <sup>2</sup> ] | $A_1$<br>[m <sup>2</sup> ] | $\chi = A_1/A_0$<br>[-] | $C_c$ |
|-------------------|----------|--------------|--------------|-------------------|-------------------|----------------------------|----------------------------|-------------------------|-------|
| Broekstuk         | 12,25    | 11,94        | 8,54         | 12,25             | 0,139             | 125,45                     | 17,57                      | 0,14                    | 3,21  |
| Eerste tussenstuk | 24,56    | 8,54         | 5,69         | 12,31             | 0,116             | 87,60                      | 16,12                      | 0,18                    | 3,00  |
| Tweede tussenstuk | 32,70    | 5,69         | 3,80         | 8,14              | 0,116             | 38,62                      | 12,69                      | 0,33                    | 2,44  |
| Bovenstuk 1       | 40,50    | 3,80         | 3,19         | 7,80              | 0,039             | 27,26                      | 8,02                       | 0,29                    | 2,56  |
| Bovenstuk 2       | 48,00    | 3,19         | 2,60         | 7,50              | 0,039             | 21,71                      | 6,12                       | 0,28                    | 2,60  |
| Topstuk           | 45,00    | 2,60         |              | -3,00             |                   | -3,90                      | 0,40                       | -0,10                   | 4,61  |
| Ondertraverse     | 32,70    | 14,86        |              | 4,00              |                   | 29,72                      | 7,50                       | 0,25                    | 2,71  |
| Boventraverse     | 44,00    | 17,19        |              | 4,00              |                   | 34,39                      | 8,70                       | 0,25                    | 2,71  |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving      | h<br>[m] | $b_1$<br>[m] | $b_2$<br>[m] | $\Delta h$<br>[m] | $\Delta_x$<br>[m] | $A_0$<br>[m <sup>2</sup> ] | $A_1$<br>[m <sup>2</sup> ] | $\chi = A_1/A_0$<br>[-] | $C_c$ |
|-------------------|----------|--------------|--------------|-------------------|-------------------|----------------------------|----------------------------|-------------------------|-------|
| Broekstuk         | 12,25    | 11,94        | 8,54         | 12,25             | 0,139             | 125,45                     | 17,57                      | 0,14                    | 3,21  |
| Eerste tussenstuk | 24,56    | 8,54         | 5,69         | 12,31             | 0,116             | 87,60                      | 16,12                      | 0,18                    | 3,00  |
| Tweede tussenstuk | 32,70    | 5,69         | 3,80         | 8,14              | 0,116             | 38,62                      | 12,69                      | 0,33                    | 2,44  |
| Bovenstuk 1       | 40,50    | 3,80         | 3,19         | 7,80              | 0,039             | 27,26                      | 8,02                       | 0,29                    | 2,56  |
| Bovenstuk 2       | 48,00    | 3,19         | 2,60         | 7,50              | 0,039             | 21,71                      | 6,12                       | 0,28                    | 2,60  |
| Topstuk           | 45,00    | 2,60         |              | -3,00             |                   | -3,90                      | 0,40                       | -0,10                   | 4,61  |
| Ondertraverse     | 32,70    | 14,86        |              | 4,00              |                   | 29,72                      | 7,50                       | 0,25                    | 2,71  |
| Boventraverse     | 44,00    | 17,19        |              | 4,00              |                   | 34,39                      | 8,70                       | 0,25                    | 2,71  |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.

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#### Windoppervlak feeders telecominstallaties

| Onderdeel         | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk         | 0,20                  | 0,71   | 12,3 | 1,7            |
| Eerste tussenstuk | 0,20                  | 0,71   | 12,3 | 1,7            |
| Tweede tussenstuk | 0,20                  | 0,71   | 8,1  | 1,2            |
| Bovenstuk 1       |                       |        |      |                |
| Bovenstuk 2       |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>i</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,0                 | 35    | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 39,5                    | 7,0                     | 0,0                     | -7,0                    | 6,1                    | 241,9                    | 43,0                     | 0,0                      | -43,0                    |
| Eerste tussenstuk | 0,86                                   | 41,4                    | 7,4                     | 0,0                     | -7,4                    | 18,4                   | 762,1                    | 135,4                    | 0,0                      | -135,4                   |
| Tweede tussenstuk | 0,98                                   | 30,1                    | 5,4                     | 0,0                     | -5,4                    | 28,6                   | 863,1                    | 153,4                    | 0,0                      | -153,4                   |
| Bovenstuk 1       | 1,05                                   | 21,5                    | 3,8                     | 0,0                     | -3,8                    | 36,6                   | 786,4                    | 139,7                    | 0,0                      | -139,7                   |
| Bovenstuk 2       | 1,10                                   | 17,5                    | 3,1                     | 0,0                     | -3,1                    | 44,3                   | 774,5                    | 137,6                    | 0,0                      | -137,6                   |
| Topstuk           | 1,11                                   | 2,1                     | 0,4                     | 0,0                     | -0,4                    | 46,5                   | 95,9                     | 17,0                     | 0,0                      | -17,0                    |
| Ondertraverse     | 1,02                                   | 41,7                    | 3,1                     | 0,0                     | -3,1                    | 34,0                   | 1418,0                   | 105,4                    | 0,0                      | -105,4                   |
| Boventraverse     | 1,11                                   | 52,2                    | 3,9                     | 0,0                     | -3,9                    | 45,3                   | 2365,5                   | 175,8                    | 0,0                      | -175,8                   |
| <b>Totaal</b>     |  | <b>245,9</b>            | <b>34,0</b>             | <b>0,0</b>              | <b>-34,0</b>            |                        | <b>7307,4</b>            | <b>907,3</b>             | <b>0,0</b>               | <b>-907,3</b>            |

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 0,0                     | 39,8                    | 39,5                    | 39,8                    | 6,1                    | 0,0                      | 243,8                    | 241,9                    | 243,8                    |
| Eerste tussenstuk | 0,86                                   | 0,0                     | 41,7                    | 41,4                    | 41,7                    | 18,4                   | 0,0                      | 768,0                    | 762,1                    | 768,0                    |
| Tweede tussenstuk | 0,98                                   | 0,0                     | 30,4                    | 30,1                    | 30,4                    | 28,6                   | 0,0                      | 869,9                    | 863,1                    | 869,9                    |
| Bovenstuk 1       | 1,05                                   | 0,0                     | 21,7                    | 21,5                    | 21,7                    | 36,6                   | 0,0                      | 792,5                    | 786,4                    | 792,5                    |
| Bovenstuk 2       | 1,10                                   | 0,0                     | 17,6                    | 17,5                    | 17,6                    | 44,3                   | 0,0                      | 780,6                    | 774,5                    | 780,6                    |
| Topstuk           | 1,11                                   | 0,0                     | 2,1                     | 2,1                     | 2,1                     | 46,5                   | 0,0                      | 96,6                     | 95,9                     | 96,6                     |
| Ondertraverse     | 1,02                                   | 0,0                     | 17,6                    | 16,7                    | 17,6                    | 34,0                   | 0,0                      | 597,5                    | 567,2                    | 597,5                    |
| Boventraverse     | 1,11                                   | 0,0                     | 22,0                    | 20,9                    | 22,0                    | 45,3                   | 0,0                      | 996,8                    | 946,2                    | 996,8                    |
| <b>Totaal</b>     |  | <b>0,0</b>              | <b>192,8</b>            | <b>189,6</b>            | <b>192,8</b>            |                        | <b>0,0</b>               | <b>5145,8</b>            | <b>5037,3</b>            | <b>5145,8</b>            |

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting     | 0                      | 0                      | 516                    | 0                       | 0                       | 0                       |
| Windrichting 0°          | 252                    | 0                      | 0                      | 0                       | 7524                    | 0                       |
| Windrichting 80°         | 35                     | 199                    | 0                      | 5359                    | 945                     | 0                       |
| Windrichting 90°         | 0                      | 196                    | 0                      | 5254                    | 0                       | 0                       |
| Windrichting 100°        | -35                    | 199                    | 0                      | 5359                    | -945                    | 0                       |

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### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f2 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 33,20             | 1,02                             | 1,2               | 2,44                |
| 380ct1f3 | 6,00                   | 1      | 6                   | 7,9           | 2,0                           | 44,50             | 1,10                             | 1,2               | 2,64                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,2                           | 48,70             | 1,13                             | 1,2               | 0,27                |

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**Windbelasting back**

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| bl1      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,19  | 22,24         | 17,5  | 19,3        | 63,1              | 50,0        | 55,0            |

**Windbelasting ahead**

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f2 | 27,4   | 0,96                 | 0,57           | 0,63          | 1,11  | 28,25         | 51,5  | 56,7        | 46,9              | 92,7        | 102,1           |
| 380ct1f3 | 38,7   | 1,06                 | 0,60           | 0,66          | 1,08  | 28,25         | 58,0  | 63,8        | 46,9              | 107,0       | 117,7           |
| bl1      | 42,9   | 1,09                 | 0,61           | 0,67          | 1,19  | 22,24         | 17,5  | 19,3        | 63,1              | 50,0        | 55,0            |

NB: belastingen  $w_v$  gelden voor bundel

Project: GT-RL380  
 Masttype: HB+5\_n (160 gr bouwphase)  
 Mast: 69N

**Geleiderbelastingen** Auteur: TBR  
Versie: v12.0

**Uitgangspunten**  
 Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 15 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |              |                  |            |          |          |                     |
|--|---------------------------|------------------------------|--------------|------------------|------------|----------|----------|---------------------|
| Belastingsgeval  | omschrijving              | Temp<br>°C                   | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|  |                           |                              | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a   | Wind                      | 10°                          | 1,20         | 1,20             | 0,00       | 1,25     | 0,00     | 0,0                 |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90         | 1,20             | 0,00       | 1,25     | 0,00     | 0,0                 |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90         | 0,90             | 0,00       | 1,25     | 0,00     | 0,0                 |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20         | 1,20             | 0,00       | 0,38     | 1,07     | 0,0                 |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20             | 0,00       | 0,38     | 1,07     | 0,0                 |
| ULS 4  | Koude+wind                | -20°                         | 1,20         | 1,20             | 0,00       | 0,25     | 0,00     | 0,0                 |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90         | 1,20             | 0,00       | 0,25     | 0,00     | 0,0                 |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00         | 1,00             | 1,00       | 0,00     | 0,00     | 1,0                 |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00         | 1,00             | 0,00       | 0,00     | 0,00     | 1,0                 |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 1,50       | 0,25     | 0,00     | 0,0                 |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 0,00       | 0,25     | 0,00     | 0,0                 |
| ULS 7  | Permanent                 | 10°                          | 1,35         | 1,35             | 0,00       | 0,00     | 0,00     | 0,0                 |
| ULS 8  | Special                   | 10°                          | 1,00         | 1,00             | 0,00       | 0,00     | 0,00     | 1,0                 |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
|  |                           |                              | $G_k$        |                  | $Q_k$      |          |          | $A_k$               |
| SPLS 1a  | Wind                      | 10°                          | 1,20         | 1,20             | 0,0        | 0,78     | 0,00     | 0,0                 |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90         | 1,20             | 0,0        | 0,78     | 0,00     | 0,0                 |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90         | 0,90             | 0,0        | 0,78     | 0,00     | 0,0                 |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20         | 1,20             | 0,0        | 0,36     | 0,34     | 0,0                 |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20             | 0,0        | 0,36     | 0,34     | 0,0                 |
| SPLS 4   | Koude+wind                | -20°                         | 1,20         | 1,20             | 0,0        | 0,24     | 0,00     | 0,0                 |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90         | 1,20             | 0,0        | 0,24     | 0,00     | 0,0                 |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 1,2        | 0,24     | 0,0      | 0,0                 |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 0,0        | 0,24     | 0,0      | 0,0                 |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              | $G_k$        |                  | $Q_k$      |          |          | $A_k$               |
| SLS 1a   | Wind                      | 10°                          | 1,00         | 1,00             | 0,0        | 0,87     | 0,0      | 0,0                 |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00         | 1,00             | 0,0        | 0,26     | 0,71     | 0,0                 |
| SLS 4  | Wind                      | -20°                         | 1,00         | 1,00             | 0,0        | 0,17     | 0,0      | 0,0                 |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00         | 1,00             | 0,0        | 0,17     | 0,0      | 0,0                 |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00         | 1,00             | 0,0        | 0,00     | 0,0      | 0,0                 |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 54  
 Aantal belastingcombinaties SPLS 210  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 2790

Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr bouwfase)  
 Mast: 69N

### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -50,6         | 50,6          | 12,7          | 12,7          | 8,3           | 8,3           |
| 380ct1f1    | -139,7        | 139,7         | 38,4          | 38,4          | 28,9          | 28,9          |
| 380ct1f2    | -139,7        | 139,7         | 38,4          | 38,4          | 28,9          | 28,9          |
| 380ct1f3    | -142,8        | 142,8         | 41,6          | 41,6          | 28,9          | 28,9          |
| V-fixatie 1 | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           |
| V-fixatie 2 | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           | 0,0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 480,1  | 493,2 | 480,0 |
| 380ct1f1    | 480,0  | 490,4 | 480,0 |
| 380ct1f2    | 480,0  | 490,4 | 480,0 |
| 380ct1f3    | 480,0  | 490,8 | 480,0 |
| V-fixatie 1 |        |       |       |
| V-fixatie 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 554,2  | 473,8 |
| 380ct1f1    | 517,1  | 482,0 |
| 380ct1f2    | 517,1  | 482,0 |
| 380ct1f3    | 524,7  | 483,7 |
| V-fixatie 1 |        |       |
| V-fixatie 2 |        |       |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

| Voor alle geleiders | Wind / Weight span verhouding |
|---------------------|-------------------------------|
| Max. weight span    | 554,2 m<br>1,386 -            |
| Min. weight span    | 300,8 m<br>0,752 -            |

Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr bouwfase)  
 Mast: 69N

| Geleider    | Maximale waarden back+ahead span |            |            | Maximale waarden trekkracht geleider |               |
|-------------|----------------------------------|------------|------------|--------------------------------------|---------------|
|             | Fx<br>[kN]                       | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN]                        | Ft_ah<br>[kN] |
| bl1         | 34,0                             | 25,0       | 8,3        | -51,0                                | 51,0          |
| 380ct1f1    | 118,1                            | 75,2       | 28,9       | -141,0                               | 141,0         |
| 380ct1f2    | 118,1                            | 75,2       | 28,9       | -141,0                               | 141,0         |
| 380ct1f3    | 118,4                            | 81,2       | 28,9       | -144,2                               | 144,2         |
| V-fixatie 1 | 3,0                              | 3,0        | 6,8        | 0,0                                  |               |
| V-fixatie 2 | 3,0                              | 3,0        | 6,8        | 0,0                                  |               |

| EDS-belastingen geleiders |            |            |            |               |               |
|---------------------------|------------|------------|------------|---------------|---------------|
| Geleider                  | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN] | Ft_ah<br>[kN] |
| bl1                       | 15,1       | 2,7        | 2,4        | -15,3         | 15,3          |
| 380ct1f1                  | 72,2       | 12,7       | 17,0       | -73,3         | 73,3          |
| 380ct1f2                  | 72,2       | 12,7       | 17,0       | -73,3         | 73,3          |
| 380ct1f3                  | 72,2       | 12,7       | 17,0       | -73,3         | 73,3          |
| V-fixatie 1               | 0,0        | 0,0        | 5,0        | 0,0           |               |
| V-fixatie 2               | 0,0        | 0,0        | 5,0        | 0,0           |               |

| Controle uplift SLS-wind |             |               |               |
|--------------------------|-------------|---------------|---------------|
| Combinatie:Geleider      |             | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
| SLS 4                    | bl1         | 0,0           | 0,0           |
|                          | 380ct1f1    | 0,0           | 0,0           |
|                          | 380ct1f2    | 0,0           | 0,0           |
|                          | 380ct1f3    | 0,0           | 0,0           |
|                          | V-fixatie 1 | 0,0           | 0,0           |
|                          | V-fixatie 2 | 0,0           | 0,0           |



Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr bouwfase)  
 Mast: 69N

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | 0             | 259           | 148           | 7816           | 0              | 0              |
| ULS 1a_0,9_0      |             | 7             | 96            | 116           | 2078           | 221            | -85            |
| ULS 1a_0,9_0,9_90 |             | 0             | 249           | 85            | 8260           | 0              | 0              |
| ULS 3_0           |             | 2             | 152           | 194           | 3180           | 71             | -27            |
| SLS 7             |             | 0             | 82            | 117           | 1536           | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

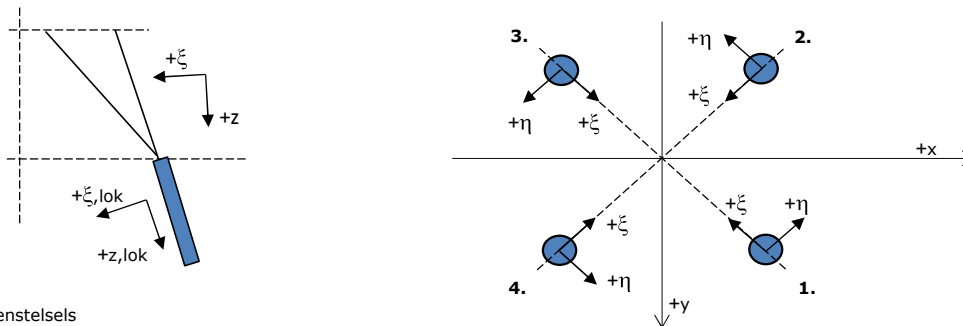
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | 0             | 505           | 767           | 14399          | 0              | 0              |
| ULS 1a_0,9_0,9_90 | 0             | 494           | 549           | 14844          | 0              | 0              |
| SLS 7             | 0             | 82            | 633           | 1536           | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie                   | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|------------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_90                | 0             | 505           | 577           | <b>14862</b>   | 0              | 0              |
| SPLS 1a_0 Ba All Cts         | 473           | 47            | 717           | 501            | <b>16126</b>   | -3597          |
| SPLS 6a_90 Ba All Cts Ah Ct1 | 387           | 128           | 746           | 2652           | 14509          | <b>-5095</b>   |
| SPLS 1a_225 Ah All Cts       | -463          | -120          | 718           | <b>-4434</b>   | <b>-15989</b>  | 4129           |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie             | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 1a_80 Ba All Cts  | 81            | 284           | <b>998</b>    | -144             | -257            | -62                   | 1017                |
| 2     | SPLS 1a_270 Ba All Cts | 250           | -69           | <b>922</b>    | -129             | -226            | -45                   | 939                 |
| 3     | SPLS 1a_225 Ah All Cts | -268          | -96           | <b>1035</b>   | 121              | -258            | -55                   | 1055                |
| 4     | SPLS 1a_100 Ah All Cts | -81           | 284           | <b>998</b>    | 144              | -257            | -62                   | 1017                |

**Maximale trekbelasting**

| Stijl | Combinatie                 | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|----------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 1a_0,9_225 Ah All Cts | -37           | -212          | <b>-710</b>   | 124              | 176             | 37                    | -724                |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -205          | 47            | <b>-690</b>   | 112              | 178             | 43                    | -704                |
| 3     | SPLS 1a_0,9_80 Ba All Cts  | 205           | 47            | <b>-690</b>   | -112             | 178             | 43                    | -704                |
| 4     | SPLS 1a_0,9_270 Ba All Cts | 0             | -203          | <b>-596</b>   | -143             | 144             | 27                    | -608                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie                   | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_270 Ah All Cts    | 26            | -194          | -514          | <b>155</b>       | 119             | 19                    | -524                |
| 2     | SPLS 3_0,9_270 Ah All Cts    | -166          | -28           | -410          | <b>137</b>       | 98              | 18                    | -418                |
| 3     | SPLS 6a_90 Ah All Cts Ba Ct1 | -217          | -4            | 683           | <b>151</b>       | -157            | -23                   | 696                 |
| 4     | SPLS 6a_90 Ah All Cts Ba Ct1 | -44           | 282           | 905           | <b>168</b>       | -230            | -53                   | 923                 |

**Maximale torsiebelasting (negatief)**

| Stijl | Combinatie                   | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba All Cts Ah Ct1 | 44            | 282           | 905           | <b>-168</b>      | -230            | -53                   | 923                 |
| 2     | SPLS 6a_90 Ba All Cts Ah Ct1 | 217           | -4            | 683           | <b>-151</b>      | -157            | -23                   | 696                 |
| 3     | SPLS 3_0,9_270 Ba All Cts    | 166           | -28           | -410          | <b>-137</b>      | 98              | 18                    | -418                |
| 4     | SPLS 3_0,9_270 Ba All Cts    | -26           | -194          | -514          | <b>-155</b>      | 119             | 19                    | -524                |

Project: GT-RLL380  
 Masttype: HB+5\_n (160 gr bouwfase)  
 Mast: 69N

#### Combinatie Ftrek+Fhor

| Stijl | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 1a_0,9_225 Ah All Cts | -37                    | -212                   | <b>-710</b>            | <b>124</b>             | 176                    | 37                         | -724                       |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -205                   | 47                     | <b>-690</b>            | <b>112</b>             | 178                    | 43                         | -704                       |
| 3     | SPLS 1a_0,9_80 Ba All Cts  | 205                    | 47                     | <b>-690</b>            | <b>-112</b>            | 178                    | 43                         | -704                       |
| 4     | SPLS 1a_0,9_270 Ba All Cts | 0                      | -203                   | <b>-596</b>            | <b>-143</b>            | 144                    | 27                         | -608                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 40                     | 49                     | 223                    | -6                     | -63                    | -19                        | 227                        |
| 2     | SLS 7      | 17                     | -8                     | 94                     | -6                     | -18                    | 1                          | 96                         |
| 3     | SLS 7      | -17                    | -8                     | 94                     | 6                      | -18                    | 1                          | 96                         |
| 4     | SLS 7      | -40                    | 49                     | 223                    | 6                      | -63                    | -19                        | 227                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie                   | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | SPLS 1a_225 Ah All Cts       | -268                   | -96                    | <b>1035</b>            | 121                    | -258                   | -55                        | 1055                       |
| Max. trek         | SPLS 1a_0,9_225 Ah All Cts   | -37                    | -212                   | <b>-710</b>            | 124                    | 176                    | 37                         | -724                       |
| Max. pos. torsie  | SPLS 6a_90 Ah All Cts Ba Ct1 | -44                    | 282                    | 905                    | <b>168</b>             | -230                   | -53                        | 923                        |
| Max. neg. torsie  | SPLS 6a_90 Ba All Cts Ah Ct1 | 44                     | 282                    | 905                    | <b>-168</b>            | -230                   | -53                        | 923                        |
| Comb. trek+torsie | SPLS 1a_0,9_225 Ah All Cts   | -37                    | -212                   | <b>-710</b>            | <b>124</b>             | 176                    | 37                         | -724                       |

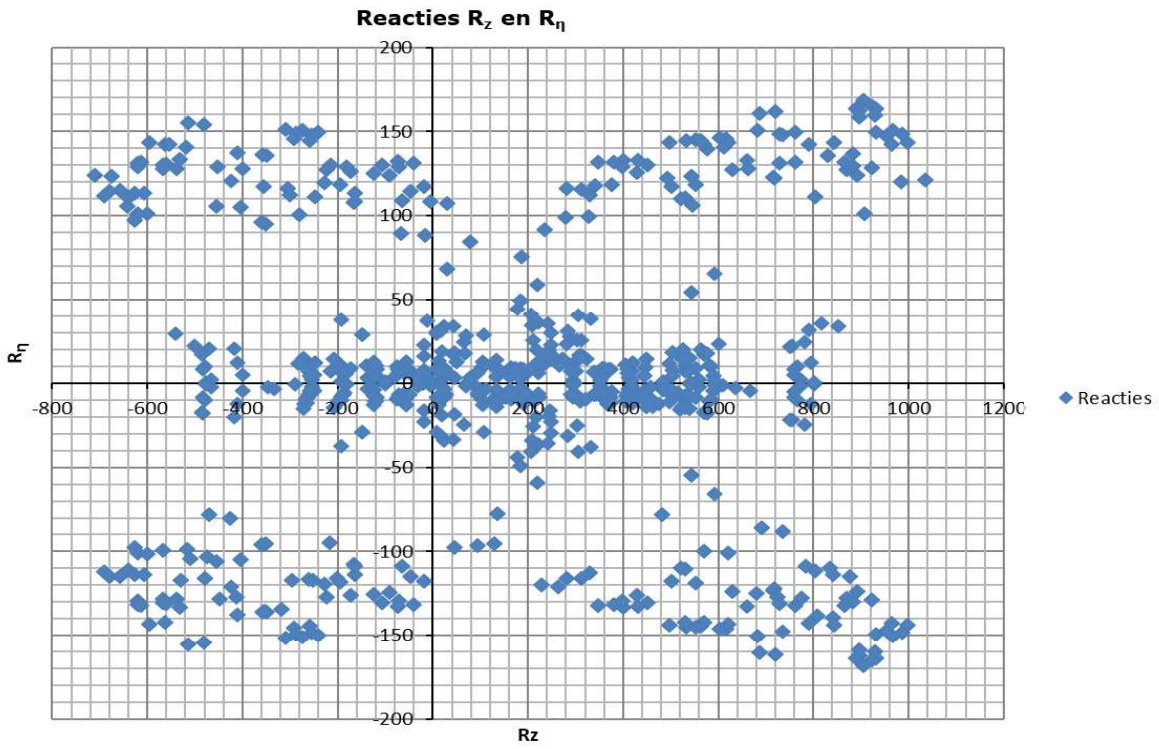
#### Maximale trekbelasting SLS

| Stijl | Combinatie                 | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 3_0,9_100 Ah All Cts  | 61                     | -145                   | <b>-292</b>            | 146                    | 60                     | 2                          | -298                       |
| 2     | SPLS 1a_0,9_100 Ah All Cts | -205                   | 47                     | <b>-690</b>            | 112                    | 178                    | 43                         | -704                       |
| 3     | SLS 1a_80                  | 46                     | 68                     | <b>-272</b>            | 15                     | 81                     | 27                         | -277                       |
| 4     | SLS 1a_0                   | 14                     | -3                     | <b>-57</b>             | 8                      | 12                     | 1                          | -58                        |

#### Maximale drukbelasting SLS

| Stijl | Combinatie             | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_80              | 113                    | 115                    | <b>591</b>             | -1                     | -162                   | -46                        | 602                        |
| 2     | SLS 1a_0               | 74                     | -57                    | <b>373</b>             | -12                    | -93                    | -20                        | 380                        |
| 3     | SPLS 3_100 Ah All Cts  | -202                   | 1                      | <b>622</b>             | 143                    | -142                   | -21                        | 633                        |
| 4     | SPLS 1a_100 Ah All Cts | -81                    | 284                    | <b>998</b>             | 144                    | -257                   | -62                        | 1017                       |

Project: GT-RLL380  
Masttype: HB+5\_n (160 gr bouwfase)  
Mast: 69N



**Belastinggeval - afspannen**

Date: 2021-07-27  
Author: TBR  
Version: 1.1

RLL-TLB  
HB+5/n

Invoergegevens
**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

| Circuits       | Aanduiding | Nummer   | Hoogteverschil |          | Richtingsverandering |          |
|----------------|------------|----------|----------------|----------|----------------------|----------|
|                |            |          | Dh_back        | Dh_ahead | Dy_back              | Dy_ahead |
| Circuit 1      | 10         | 380ct1f1 | -32,7          | 0,0 m    | 0,0                  | 0,0 m    |
| Circuit 1      | 11         | 380ct1f2 | -32,7          | 0,0 m    | 0,0                  | 0,0 m    |
| Circuit 1      | 12         | 380ct1f3 | -44,0          | 0,0 m    | 0,0                  | 0,0 m    |
| Bliksemdraad 1 | 1          | bl1      | -48,2          | 0,0 m    | 0,0                  | 0,0 m    |

**Lijn- en mastgegevens**

|                                       |          |  | Back  | Ahead   |
|---------------------------------------|----------|--|-------|---------|
| Ruling span $\sqrt{(SL3/SL)}$         |          |  | 66,0  | 400,0 m |
| Lijnhoek                              | $\beta$  |  | 180 ° |         |
| Rotatie mast t.o.v. bissectrice       | $\theta$ |  | 10 °  |         |
| Vaklengte                             |          |  | 66    | 400 m   |
| Hoogte onderkant mast t.o.v. maaiveld |          |  | 0,5 m |         |
| Beschouwde windrichtingen             | a1       |  | 0 °   |         |
| Windrichtingen volgens:               | a2       |  | 45 °  |         |
| <i>Geleiderbelastingen</i>            | a3       |  | 90 °  |         |
|                                       | a4       |  | 135 ° |         |
|                                       | a5       |  | 80 °  |         |
|                                       | a6       |  | 80 °  |         |

*Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.*

In onderstaande tabel zijn de optredende belastingen weergegeven, voor deze situatie geldt:

- belasting op geleider 1 en 10 t/m 12 zijn permanent aanwezig
- van de belasting op de overige geleiders is er telkens één aanwezig per belastingcombinatie

Uitvoer geleiderbelastingen

| Belastingcombi   | nummer | Fxtotaal     | Fytotaal     | Fztotaal    | Ftrekahead | Ftrekback |
|------------------|--------|--------------|--------------|-------------|------------|-----------|
| <b>ULS 6b_90</b> | 13     | <b>-83,5</b> | <b>15,8</b>  | <b>57,6</b> | 0,0        | -85,0     |
|                  | 10     | <b>88,8</b>  | <b>-12,4</b> | <b>19,3</b> | 89,6       | 0,0       |
|                  | 14     | <b>-83,5</b> | <b>15,8</b>  | <b>57,6</b> | 0,0        | -85,0     |
|                  | 11     | <b>88,8</b>  | <b>-12,4</b> | <b>19,3</b> | 89,6       | 0,0       |
|                  | 15     | <b>-83,6</b> | <b>15,8</b>  | <b>72,2</b> | 0,0        | -85,0     |
|                  | 12     | <b>89,5</b>  | <b>-12,2</b> | <b>19,3</b> | 90,2       | 0,0       |
|                  | 4      | <b>-17,4</b> | <b>3,3</b>   | <b>14,8</b> | 0,0        | -17,7     |
|                  | 1      | <b>19,2</b>  | <b>-2,4</b>  | <b>2,7</b>  | 19,4       | 0,0       |



## **APPENDIX B**

### **Resultaten PLS-TOWER**

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Deze Appendix bevat de resultaten voor de toetsing van profielen en bouten uit PLS-TOWER voor masttype HB+5/n.





Assessment of angle groups



Date 26-7-2021  
Author BIT  
Version 1.0

GT-RLL  
HB+5\_N

| Group Label | Description                      | Type | Profile             | Steel Qual/Bois | #shp.1 c1  | c2 | p1 | RLX | RLY | RLZ  | Slenderness | Compression | Lead Cries | Compressor Buckling | Shear (Comp) [atng (Comp) | U.C. (Comp) [eafance (Comp) | U.C. (Comp) [eafance (Comp) | Tension | Lead Cries                  | [Tension] | Net Section ear (Tens) [atng (Tens) | U.C. (Tens) [eafance (Tens) |      |
|-------------|----------------------------------|------|---------------------|-----------------|------------|----|----|-----|-----|------|-------------|-------------|------------|---------------------|---------------------------|-----------------------------|-----------------------------|---------|-----------------------------|-----------|-------------------------------------|-----------------------------|------|
| 422         | Twisted DWSRM - CD under         | EA   | 70x70x6             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 127        | 103.4               | 188.2                     | 176.4                       | 0.14                        | 15.8    | U.S 8 Bs (bow)              | 128.4     | 188.2                               | 189.6                       | 0.14 |
| 423         | Twisted DWSRM - CD under         | EA   | 70x70x6             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 121        | 103.4               | 188.2                     | 176.4                       | 0.19                        | 15.8    | U.S 8 Bs (bow)              | 128.4     | 188.2                               | 189.6                       | 0.14 |
| 424         | Twisted DWSRM - CD under         | EA   | 70x70x6             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 110        | 103.4               | 188.2                     | 176.4                       | 0.36                        | 20.5    | U.S 8 Bs (bow)              | 128.4     | 188.2                               | 189.6                       | 0.16 |
| 425         | Twisted DWSRM - CD under         | EA   | 70x70x6             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 104        | 103.4               | 188.2                     | 176.4                       | 0.43                        | 20.5    | U.S 8 Bs (bow)              | 128.4     | 188.2                               | 189.6                       | 0.16 |
| 426         | Twisted DWSRM - CD under         | EA   | 70x70x7             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 104        | 142.4               | 188.2                     | 205.8                       | 0.48                        | 59.1    | SPLS 3_0_0_100 Bs C12_1     | 148.5     | 188.2                               | 197.9                       | 0.40 |
| 427         | Twisted DWSRM - CD under         | EA   | 70x70x7             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 91         | 163.2               | 188.2                     | 205.8                       | 0.38                        | 64.2    | SPLS 6x_90 Bs All C12_Ah Ct | 148.5     | 188.2                               | 197.9                       | 0.43 |
| 428         | Twisted DWSRM - CD under         | EA   | 70x70x7             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 70         | 173.5               | 188.2                     | 176.4                       | 0.13                        | 24.9    | SPLS 3_0_0_100 Bs C12_1     | 128.4     | 188.2                               | 189.6                       | 0.19 |
| 429         | Twisted DWSRM - CD under         | EA   | 70x70x6             | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 0.53 | 0.53        | 0.53        | 70         | 173.5               | 188.2                     | 176.4                       | 0.13                        | 24.9    | SPLS 3_0_0_100 Bs C12_1     | 128.4     | 188.2                               | 189.6                       | 0.19 |
| 436         | Twisted DWSRM - Horizontal under | DFA  | 150x150x14 (not co) | S355            | 2820x48-R1 | 1  | 45 | 35  | 70  | 1.00 | 1.00        | 1.00        | 56         | 194.8               | 188.2                     | 82.2                        | 0.00                        | 0.0     | U.S 3_20_140 deg            | 220.0     | 188.2                               | 79.7                        | 0.48 |
| 437         | Twisted DWSRM - Vertical front   | EA   | 70x70x6             | S355            | 1816x48-R1 | 1  | 45 | 35  | 70  | 1.00 | 1.00        | 1.00        | 119        | 82.2                | 60.3                      | 70.6                        | 0.00                        | 0.0     | U.S 8 Bs (bow)              | 75.3      | 60.3                                | 0.0                         | 0.01 |
| 402         | Twisted DWSRM - Vertical front   | EA   | 70x70x6             | S355            | 1816x48-R1 | 1  | 45 | 35  | 70  | 1.00 | 1.00        | 1.00        | 119        | 82.2                | 60.3                      | 70.6                        | 0.00                        | 0.0     | U.S 8 Bs (bow)              | 75.3      | 60.3                                | 0.0                         | 0.01 |
| 403         | Twisted DWSRM - Vertical front   | EA   | 60x60x6             | S355            | 1816x48-R1 | 1  | 35 | 25  | 55  | 1.00 | 1.00        | 1.00        | 234        | 27.6                | 60.3                      | 70.6                        | 0.15                        | 0.9     | U.S 8 Bs (bow)              | 62.7      | 60.3                                | 0.0                         | 0.00 |
| 404         | Twisted DWSRM - Vertical front   | EA   | 50x50x5             | S355            | 1816x48-R1 | 1  | 35 | 25  | 55  | 1.00 | 1.00        | 1.00        | 235        | 45.7                | 60.3                      | 70.6                        | 0.07                        | 0.0     | U.S 8 Bs (bow)              | 62.7      | 60.3                                | 0.0                         | 0.00 |
| 405         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 406         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 407         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 408         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 409         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 410         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 411         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 412         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 413         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 414         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 415         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 416         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 417         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 418         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 419         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 420         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 421         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 422         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 423         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 424         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 425         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 426         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 427         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 428         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 429         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 430         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 431         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 432         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 433         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 434         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 435         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 436         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        | 230.9   | U.S 61_90 (Espalmen)        | 355.4     | 406.7                               | 493.6                       | 0.68 |
| 437         | Twisted DWSRM - Diagonal front   | EA   | 100x100x10          | S355            | 3824x48-R1 | 1  | 55 | 40  | 80  | 2.00 | 1.00        | 1.00        | 157        | 165.0               | 406.7                     | 529.2                       | 0.03                        |         |                             |           |                                     |                             |      |



## APPENDIX C

### Knikverkorters

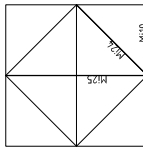
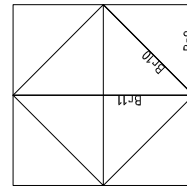
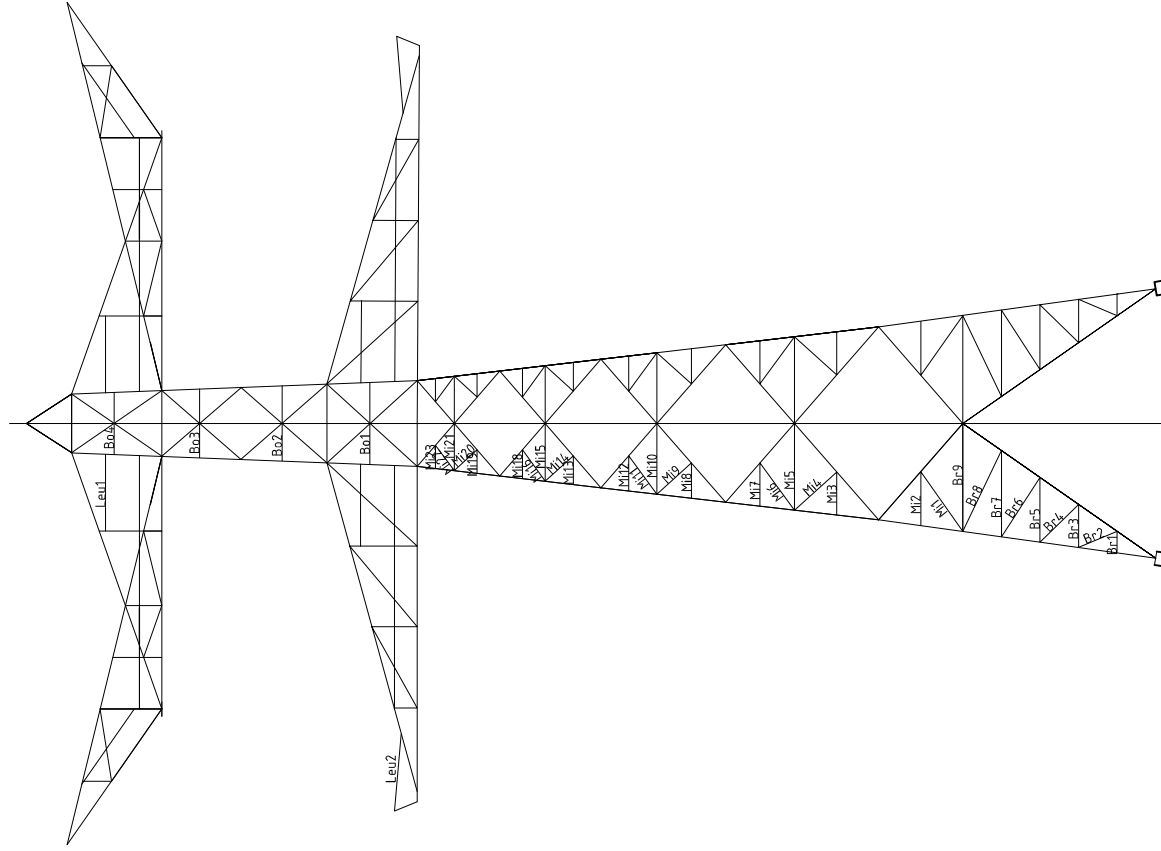
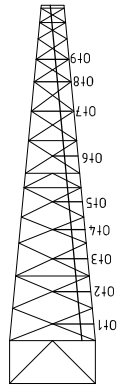
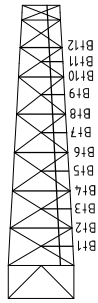
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Niet in PLS-TOWER gemodelleerde elementen in de constructie worden aanvullend getoetst. Hieronder vallen de knikverkorters van de randstijl en profielen onderdeel van stabiliteitsverbanden. De staven worden getoetst op:

- voldoende trek- of druksterkte als steungevend profiel voor randstijl, 1% van de knikcapaciteit van de randstijl;
- slankheid;
- klimbelasting

Voor de beloopbaarheid zijn staven in de traverse aanwezig. Deze zijn niet constructief (voorzien van slobgaten) en worden enkel getoetst op de klimbelasting van 1,0 kN. Zie hoofdstuk 4.2.5 en 5.7.2. van het uitgangspuntenrapport.

# Overzicht knikverkorters – HB+5



# DNV-GL

## Knikverkorters

Date: 2021-07-12  
 Author: BJT  
 Version: 1.8

GT-RLL  
 HB+5\_n

| Posnr. | Section           | Schematization             | Profile | Steel Quality | Bolt | Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|-------------------|----------------------------|---------|---------------|------|---------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
| Br1    | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 0.950      | 0         | 98           | 24.3              | 0.36         | 62.0               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.59         |                 |       |
| Br2    | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.850      | 67        | 190          | 24.3              | 0.00         | 26.4               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.92         |                 |       |
| Br3    | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.910      | 0         | 196          | 24.3              | 0.72         | 25.1               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.97         |                 |       |
| Br4    | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.390      | 45        | 204          | 24.3              | 0.00         | 34.0               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.71         |                 |       |
| Br5    | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.860      | 0         | 245          | 24.3              | 1.07         | 25.6               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.95         |                 |       |
| Br6    | Broekstuk         | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.130      | 33        | 199          | 24.3              | 0.00         | 47.9               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.51         |                 |       |
| Br7    | Broekstuk         | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.810      | 0         | 242          | 24.3              | 1.43         | 35.3               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.69         |                 |       |
| Br8    | Broekstuk         | Enkele staaf               | L90.9   | S355J0        | M16  | 8.8     | 3.970      | 26        | 226          | 24.3              | 1.34         | 65.2               | 60.3                 | 78.4              | 254.0                 | 4.73              | 0.40         |                 |       |
| Br9    | Broekstuk         | Enkele staaf               | L120.10 | S355J0        | M16  | 8.8     | 4.770      | 0         | 201          | 24.3              | 1.79         | 117.4              | 60.3                 | 87.1              | 399.8                 | 9.77              | 0.40         |                 |       |
| Br10   | Tussenschot +9,6r | Kniksteun op 0,5L          | L100.8  | S355J0        | M16  | 8.8     | 6.740      | 0         | 219          | 0.0               | 2.53         | 58.5               | 60.3                 | 69.7              | 257.2                 | 7.19              | 0.35         |                 |       |
| Br11   | Tussenschot +9,6r | Kruisende staaf halverwege | L100.8  | S355J0        | M16  | 8.8     | 9.540      | 0         | 242          | 0.0               | 1.79         | 58.5               | 60.3                 | 69.7              | 257.2                 | 7.19              | 0.25         |                 |       |
| Br12   | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 1.300      | 0         | 134          | 8.5               | 0.49         | 43.1               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.62         |                 |       |
| Br13   | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 2.100      | 72        | 216          | 8.5               | 0.00         | 21.7               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.39         |                 |       |
| Br14   | Broekstuk         | Kniksteun op 0,5L          | L50.5   | S355J0        | M16  | 8.8     | 2.580      | 0         | 170          | 8.5               | 0.97         | 25.3               | 60.3                 | 41.3              | 43.1                  | 1.08              | 0.89         |                 |       |
| Br15   | Broekstuk         | Enkele staaf               | L50.5   | S355J0        | M16  | 8.8     | 2.380      | 57        | 245          | 8.5               | 0.00         | 17.8               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.47         |                 |       |
| Br16   | Broekstuk         | Kniksteun op 0,5L          | L60.6   | S355J0        | M16  | 8.8     | 3.870      | 0         | 213          | 8.5               | 1.45         | 26.8               | 60.3                 | 52.3              | 98.8                  | 1.88              | 0.77         |                 |       |
| Br17   | Broekstuk         | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.780      | 46        | 238          | 8.5               | 0.00         | 26.8               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.32         |                 |       |
| Br18   | Broekstuk         | Kniksteun op 0,5L          | L70.7   | S355J0        | M16  | 8.8     | 5.170      | 0         | 243          | 8.5               | 1.94         | 30.0               | 60.3                 | 61.0              | 142.7                 | 2.99              | 0.65         |                 |       |
| Br19   | Broekstuk         | Enkele staaf               | L70.7   | S355J0        | M16  | 8.8     | 3.260      | 38        | 239          | 8.5               | 0.00         | 36.2               | 60.3                 | 61.0              | 142.7                 | 2.23              | 0.23         |                 |       |
| M1     | Tussenstuk1       | Enkele staaf               | L70.7   | S355J0        | M16  | 8.8     | 3.220      | 35        | 236          | 23.3              | 0.00         | 37.0               | 60.3                 | 61.0              | 142.7                 | 2.23              | 0.63         |                 |       |
| M2     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.380      | 0         | 204          | 23.3              | 0.89         | 34.2               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.68         |                 |       |
| M3     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.900      | 0         | 163          | 23.3              | 0.71         | 47.6               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.53         |                 |       |
| M4     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.520      | 48        | 216          | 23.3              | 0.00         | 31.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.74         |                 |       |
| M5     | Tussenstuk1       | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.830      | 0         | 243          | 23.3              | 1.44         | 35.0               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.66         |                 |       |
| M6     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.580      | 36        | 221          | 23.3              | 0.00         | 30.2               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.77         |                 |       |
| M7     | Tussenstuk1       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.910      | 0         | 163          | 23.3              | 0.72         | 47.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.53         |                 |       |
| M8     | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.550      | 0         | 133          | 23.6              | 0.58         | 62.7               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M9     | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.060      | 48        | 176          | 23.6              | 0.00         | 42.4               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.56         |                 |       |
| M10    | Tussenstuk2       | Enkele staaf               | L80.6   | S355J0        | M16  | 8.8     | 3.130      | 0         | 199          | 23.6              | 1.17         | 47.9               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.49         |                 |       |
| M11    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.100      | 36        | 180          | 23.6              | 0.00         | 41.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.57         |                 |       |
| M12    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.590      | 0         | 133          | 23.6              | 0.58         | 62.7               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M13    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.260      | 0         | 108          | 23.6              | 0.47         | 80.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M14    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.670      | 48        | 143          | 23.6              | 0.00         | 56.9               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M15    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.560      | 0         | 163          | 23.6              | 0.96         | 64.3               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.45         |                 |       |
| M16    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.710      | 36        | 146          | 23.6              | 0.00         | 55.1               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M17    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.270      | 0         | 109          | 23.6              | 0.48         | 79.6               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.45         |                 |       |
| M18    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.030      | 0         | 88           | 23.6              | 0.39         | 98.5               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |
| M19    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.370      | 48        | 117          | 23.6              | 0.00         | 73.0               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |
| M20    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 2.100      | 0         | 180          | 23.6              | 0.79         | 41.3               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.58         |                 |       |
| M21    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.400      | 36        | 120          | 23.6              | 0.00         | 71.1               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |
| M22    | Tussenstuk2       | Enkele staaf               | L60.6   | S355J0        | M16  | 8.8     | 1.030      | 0         | 88           | 23.6              | 0.39         | 98.5               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.45         |                 |       |

# DNV-GL

## Knikverkorters

GT-RLL  
HB+5\_n

Date: 2021-07-12  
Author: BJT  
Version: 1.8

| Posnr. | Section           | Schematization             | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |  |
|--------|-------------------|----------------------------|---------|---------------|--------------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|--|
| M24    | Tussenschot +21.1 | Enkele staaf               | L90.8   | S355J0        | M16          | 8.8        | 4,400     | 0            | 250               | 0.0          | 1.65               | 60.3                 | 69.7              | 225.8                 | 4.3               | 0.40         |                 |       |  |
| M25    | Tussenschot +21.1 | Kruisende staaf halverwege | L90.8   | S355J0        | M16          | 8.8        | 6,260     | 0            | 178               | 0.0          | 1.17               | 84.3                 | 60.3              | 69.7                  | 225.8             | 5.7          | 0.21            |       |  |
| B01    | Bovenstuk1        | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,810     | 0            | 186               | 12.2         | 0.68               | 27.2                 | 60.3              | 43.1                  | 43.1              | 0.8          | 0.87            |       |  |
| B02    | Bovenstuk1        | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,660     | 0            | 171               | 12.2         | 0.62               | 30.9                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.79            |       |  |
| B03    | Bovenstuk2        | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,520     | 0            | 156               | 6.4          | 0.57               | 35.0                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.73            |       |  |
| B04    | Bovenstuk2        | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,370     | 0            | 141               | 6.4          | 0.51               | 40.3                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.65            |       |  |
| O01    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,830     | 0            | 188               | 0.0          | 0.69               | 26.8                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.87            |       |  |
| O02    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,690     | 0            | 174               | 0.0          | 0.63               | 30.1                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.81            |       |  |
| O03    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,550     | 0            | 159               | 0.0          | 0.58               | 34.1                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.74            |       |  |
| O04    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,430     | 0            | 147               | 0.0          | 0.54               | 38.1                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.68            |       |  |
| O05    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,310     | 0            | 135               | 0.0          | 0.49               | 42.7                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.63            |       |  |
| O06    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,115     | 0            | 115               | 0.0          | 0.42               | 52.1                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.53            |       |  |
| O07    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,790     | 0            | 184               | 0.0          | 0.67               | 27.7                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.86            |       |  |
| O08    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,640     | 0            | 169               | 0.0          | 0.62               | 31.4                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.78            |       |  |
| O09    | Ondertraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,450     | 0            | 149               | 0.0          | 0.54               | 37.3                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.69            |       |  |
| B11    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,410     | 0            | 145               | 0.0          | 0.53               | 38.8                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.67            |       |  |
| B12    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16          | 8.8        | 2,730     | 0            | 234               | 0.0          | 1.02               | 27.6                 | 60.3              | 52.3                  | 98.8              | 1.4          | 0.75            |       |  |
| B13    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,330     | 0            | 137               | 0.0          | 0.50               | 41.9                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.64            |       |  |
| B14    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16          | 8.8        | 2,550     | 0            | 218               | 0.0          | 0.96               | 30.7                 | 60.3              | 52.3                  | 98.8              | 1.4          | 0.71            |       |  |
| B15    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,230     | 0            | 126               | 0.0          | 0.46               | 46.3                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.59            |       |  |
| B16    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16          | 8.8        | 2,360     | 0            | 202               | 0.0          | 0.89               | 34.6                 | 60.3              | 52.3                  | 98.8              | 1.4          | 0.65            |       |  |
| B17    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,130     | 0            | 116               | 0.0          | 0.42               | 51.3                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.54            |       |  |
| B18    | Boventraverse     | Enkele staaf               | L60.6   | S355J0        | M16          | 8.8        | 2,180     | 0            | 187               | 0.0          | 0.82               | 39.0                 | 60.3              | 52.3                  | 98.8              | 1.4          | 0.60            |       |  |
| B19    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,040     | 0            | 107               | 0.0          | 0.39               | 56.3                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.50            |       |  |
| B10    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 2,000     | 0            | 205               | 0.0          | 0.75               | 23.4                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.96            |       |  |
| B11    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 0,960     | 0            | 99                | 0.0          | 0.36               | 61.3                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.46            |       |  |
| B12    | Boventraverse     | Enkele staaf               | L50.5   | S355J0        | M16          | 8.8        | 1,850     | 0            | 190               | 0.0          | 0.69               | 26.4                 | 60.3              | 41.3                  | 43.1              | 0.8          | 0.88            |       |  |
| Leu1   | Boventraverse     | Enkele staaf               | L70.7   | S355J0        | M16          | 8.8        | 3,180     | 0            | 233               | 0.0          | 1.19               | 37.7                 | 60.3              | 61.0                  | 142.7             | 2.2          | 0.55            |       |  |
| Leu2   | Boventraverse     | Enkele staaf               | L70.7   | S355J0        | M16          | 8.8        | 3,300     | 0            | 242               | 0.0          | 1.24               | 35.5                 | 60.3              | 61.0                  | 142.7             | 2.2          | 0.57            |       |  |

## APPENDIX D

### Blokdeuvels

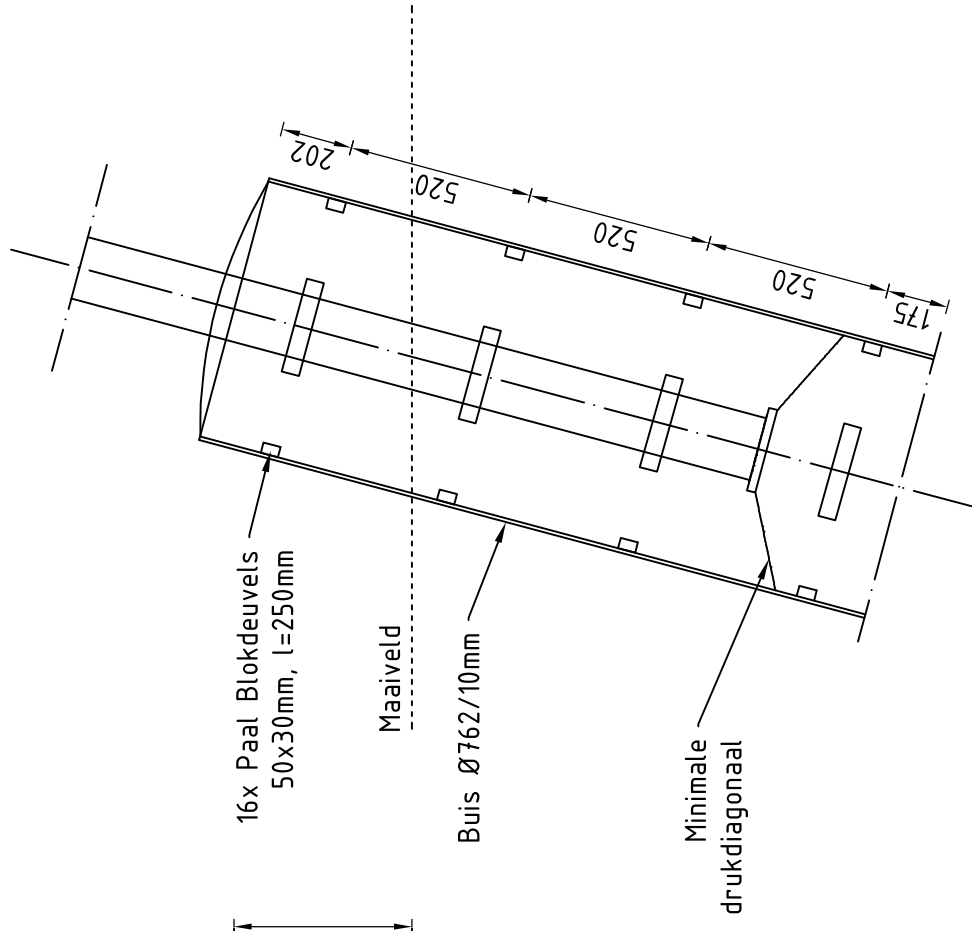
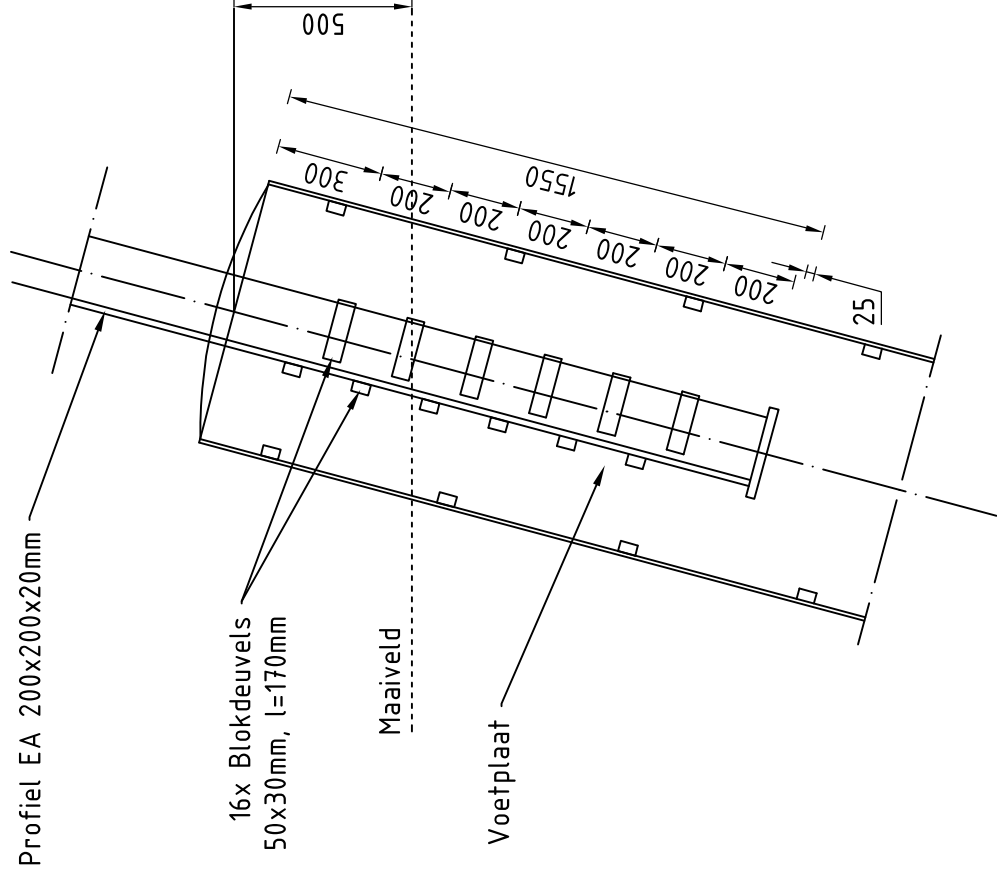
De belastingen op de fundatie uit Appendix A zijn uitgangspunt voor de berekening van de ingestorte rand met blokdeuvels. De belastingen in de richting van de randstijl zijn van toepassing. In de tabellen is dit opgenomen in de laatste kolom  $R_{z,lok}$ . De controles zijn uitgevoerd met een spreadsheet. Vanwege de helling van de drukdiagonaal wordt per krachtrichting bepaald hoeveel deuvels effectief zijn. Om deze reden kan het aantal 'Shear blocks main leg' in de berekening lager zijn dan het aantal op tekening staat aangegeven.

De belastingen waaraan getoetst worden zijn onderstaand weergegeven.

#### Masttype HB+5

| Omhullenden ongeacht stijl |                          |               |               |               |                      |                   |                       |                     |
|----------------------------|--------------------------|---------------|---------------|---------------|----------------------|-------------------|-----------------------|---------------------|
| Belasting                  | Combinatie               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\theta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
| Max. druk                  | ULS 1a_70                | -344          | 344           | <b>1974</b>   | 0                    | -487              | -99                   | 2012                |
| Max. trek                  | ULS 1a_0,9_70            | -277          | 279           | <b>-1609</b>  | -1                   | 393               | 78                    | -1639               |
| Max. pos. torsie           | SPLS 6a_90 Ah Ct1 Ba Ct1 | 158           | -67           | 249           | <b>159</b>           | -65               | -16                   | 254                 |
| Max. neg. torsie           | SPLS 6a_90 Ba Ct1 Ah Ct1 | -158          | -67           | 249           | <b>-159</b>          | -65               | -16                   | 254                 |
| Comb. trek+torsie          | ULS 1a_0,9_70            | -277          | 279           | <b>-1609</b>  | <b>-1</b>            | 393               | 78                    | -1639               |

# Principe blokdeuvels - HB+5/n



## Algemene opmerkingen

- Aarding niet aangegeven
- Spiraalwapening niet aangegeven

Project: GT-RLL  
Mast: HB+5\_n

**Shear blocks**

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-07-29  
Auteur: BJT  
Versie: 1.4

| Load        |            |         | Results     |      |                |
|-------------|------------|---------|-------------|------|----------------|
| Compression | $F_{Ed,c}$ | 2012 kN | Compression | U.C. | 0,88 < 1,00 OK |
| Tension     | $F_{Ed,t}$ | 1639 kN | Tension     | U.C. | 0,78 < 1,00 OK |

**Main leg**

|                    |          |                      |
|--------------------|----------|----------------------|
| Profile            |          | <b>L200.20</b>       |
| Steel material     |          | S355                 |
| Cross section      |          | 7635 mm <sup>2</sup> |
| Axial capacity     | $N_{pl}$ | 2710 kN              |
| Width              | b        | 200 mm               |
| Thickness          | t        | 20 mm                |
| Length in concrete |          | 1550 mm              |

**Capacity shear blocks main leg**

|  |   |                        |
|--|---|------------------------|
| $A_{f1}$                                     | = | 5100 mm <sup>2</sup>   |
| $A_{f2}$                                     | = | 13800 mm <sup>2</sup>  |
| Slope  |   | 1 : 5                  |
| $C_A = \sqrt{A_{f2}/A_{f1}}$                 | = | 1,64                   |
| $f_{jd} = C_A \times f_{cd}$                 | = | 26,3 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd}$ | = | 1342 kN                |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd}$ | = | 1342 kN                |

**Shear blocks main leg**

|                    |       |        |
|--------------------|-------|--------|
| Width              | b     | 50 mm  |
| Thickness          | h     | 30 mm  |
| Length             | L     | 170 mm |
| Welds              | a     | 5 mm   |
| c.t.c. separation  | s     | 200 mm |
| Number for compr.  | $n_c$ | 10 -   |
| Number for tension | $n_t$ | 10 -   |

**Capacity foot plate**

|                                       |   |                        |
|---------------------------------------|---|------------------------|
| $k_d$                                 | = | 1,73 -                 |
| $f_{jd} = C_A \times f_{cd}$          | = | 27,7 N/mm <sup>2</sup> |
| $c = t\sqrt{(f_{yd} / 3f_{jd})}$      | = | 53 mm                  |
| $m^* = \min(c,m)$                     | = | 30 mm                  |
| Type foot plate                       |   | Extending              |
| Effective for                         |   | Compr. and tension     |
| $A_{p,c}$                             | = | 35235 mm <sup>2</sup>  |
| $F_{Rd,c} = A_{p,druk} \times f_{jd}$ | = | 976 kN                 |
| $A_{p,t}$                             | = | 27600 mm <sup>2</sup>  |
| $F_{Rd,t} = A_{p,t} \times f_{jd}$    | = | 765 kN                 |

**Foot plate**

|             |   |       |
|-------------|---|-------|
| Thickness   | t | 25 mm |
| Ext. length | m | 30 mm |
| Welds       | a | 5 mm  |

**Pile**

|                   |  |                       |
|-------------------|--|-----------------------|
| Name              |  | Buispaal              |
| Diameter          |  | 762 mm                |
| Thickness         |  | 10 mm                 |
| Cross section     |  | 23625 mm <sup>2</sup> |
| Steel material    |  | S355                  |
| Capacity          |  | 8387 kN               |
| Concrete strength |  | C30/37                |

**Capacities**

|  |   |                |
|--|---|----------------|
| $F_{Rd,c,plate}$                             | = | 956 kN         |
| $F_{Rd,blocks,c}$                            | = | 1342 kN        |
| $F_{Rd,c} = F_{Rd,block} + F_{Rd,footplate}$ | = | <b>2298 kN</b> |
| U.C. compression                             |   | 0,88 < 1,00 OK |
| Welds foot plate (see next page)             |   | 956 kN         |
| $F_{Rd,t} = \min. (welds / foot plate) =$    |   | 765 kN         |
| $F_{Rd,blocks,t}$                            | = | 1342 kN        |
| $F_{Rd,t} = F_{Rd,block} + F_{Rd,footplate}$ | = | <b>2107 kN</b> |
| U.C. tension                                 |   | 0,78 < 1,00 OK |
| U.C. welds                                   |   | 0,48 < 1,00 OK |

**Shear blocks pile**

|                    |       |        |
|--------------------|-------|--------|
| Width              | b     | 50 mm  |
| Thickness          | h     | 30 mm  |
| Length             | L     | 250 mm |
| Welds              | a     | 5 mm   |
| c.t.c. separation  | s     | 520 mm |
| Number for compr.  | $n_c$ | 12 -   |
| Number for tension | $n_t$ | 12 -   |

**Capacity shear blocks pile**

|  |   |                        |
|--|---|------------------------|
| $A_{f1}$                                     | = | 7500 mm <sup>2</sup>   |
| $A_{f2}$                                     | = | 22500 mm <sup>2</sup>  |
| $C_A = \sqrt{A_{f2}/A_{f1}}$                 | = | 1,73 -                 |
| $f_{jd} = k_d \times f_{cd}$                 | = | 27,7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd}$ | = | <b>2494 kN</b>         |
| U.C. compression                             |   | 0,81 < 1,00 OK         |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd}$ | = | <b>2494 kN</b>         |
| U.C. tension                                 |   | 0,66 < 1,00 OK         |
| U.C. welds                                   |   | 0,42 < 1,00 OK         |

**Design value concrete strength**

|                  |            |                        |
|------------------|------------|------------------------|
| Material factor  | $\gamma_c$ | 1,5                    |
| Add. mat. factor | $\gamma_m$ | 1,25 -                 |
| $f_{cd} =$       |            | 16,0 N/mm <sup>2</sup> |

**Steel tower stub**

|                  |            |                       |
|------------------|------------|-----------------------|
| Yield strength   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Tensile strength | $f_{ud} =$ | 490 N/mm <sup>2</sup> |

**"Splitting" of pile**

|                       |            |                       |
|-----------------------|------------|-----------------------|
| Spread of forces      |            | 45 °                  |
| Length force flow     |            | 1179 mm               |
| Splitting force       |            | 695 kN/m              |
| Yield strength wall   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Capacity tubular pile |            | 7100 kN/m             |
| U.C.                  |            | 0,10 < 1,00 OK        |

Project: GT-RLL  
 Mast: HB+5\_n

**Welds of shear blocks of main leg**

*Out-of-plane loading*

**Plate**

t = 50 mm  
 Grade S355  
 $f_{yd} = 355 \text{ N/mm}^2$   
 $f_u = 490 \text{ N/mm}^2$

**Member forces**

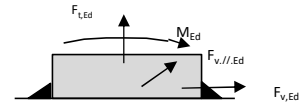
Factor 1,2  
 $F_{t,Ed} = 0 \text{ kN}$   
 $F_{v,Ed} = F_{rd,c} / n = 161 \text{ kN}$   
 $F_{v//,Ed} = 0 \text{ kN}$   
 $M_{Ed} = 1/2 b / h \times F_{v,Ed} = 2,42 \text{ kNm}$

**Check**

$\sigma_{vw,Ed} = 207 \text{ N/mm}^2 \leq$   
 $\sigma_1 = 104 \text{ N/mm}^2 \leq$

**Welds**

a = 5 mm  
 l = 170 mm  
 $\beta_w = 0,9$   
 $\gamma_{M2} = 1,25$



**Stress components**

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 4al = 0 \text{ N/mm}^2$   
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 4al = 67 \text{ N/mm}^2$   


---

 $b^* = b + 2/3av\sqrt{2} = 54,7 \text{ mm}$   
 $\sigma_1 = \tau_1 = 0,706M_{Ed} / al b^* = 37 \text{ N/mm}^2$   
 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$   
 $\sigma_{vw,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 207 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$  U.C. = **0,48 OK**  
 $0,9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$  U.C. = **0,29 OK**

**Welds of shear blocks of pile**

*Out-of-plane loading*

**Plate**

t = 50 mm  
 Grade S355  
 $f_{yd} = 355 \text{ N/mm}^2$   
 $f_u = 490 \text{ N/mm}^2$

**Member forces**

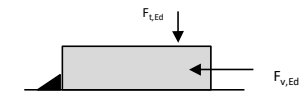
Factor 1,2  
 $F_{t,Ed} = 1/2 b / h \times F_{v,Ed} = 75 \text{ kN}$   
 $F_{v,Ed} = 249 \text{ kN}$   
 $F_{v//,Ed} = 0 \text{ kN}$   
 $M_{Ed} = 0,00 \text{ kNm}$

**Check**

$\sigma_{vw,Ed} = 183 \text{ N/mm}^2 \leq$   
 $\sigma_1 = 92 \text{ N/mm}^2 \leq$

**Welds**

a = 5 mm  
 l = 250 mm  
 $\beta_w = 0,9$   
 $\gamma_{M2} = 1,25$



**Stress components**

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 2al = 21 \text{ N/mm}^2$   
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 2al = 71 \text{ N/mm}^2$   


---

 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$   
 $\sigma_{vw,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 183 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$  U.C. = **0,42 OK**  
 $0,9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$  U.C. = **0,26 OK**

**Welds of foot plate**

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$   
 Weld size a = 5 mm  
 Length l = 2b + 2b - t = 760 mm  
 Capacity  $F_{Rd} = a \times l \times f_{w,d} / \sqrt{3} = 956 \text{ kN}$





## APPENDIX E

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### Liggers

Niet van toepassing voor dit masttype.

## APPENDIX F

### Galloping

#### Uitgangspunten

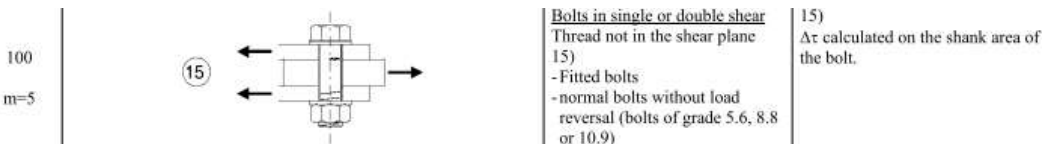
In het uitgangspuntendocument is beschreven dat wordt uitgegaan van een materiaalfactor voor vermoeiing  $\gamma_{mf} = 1,15$ . Dit komt overeen met de “Safe-life methode” met “Low consequence” van tabel 3.1 van NEN-EN 1993-1-9 of met “Damage tolerant” en “High consequence”.

| Assessment method | Consequence of failure |                  |
|-------------------|------------------------|------------------|
|                   | Low consequence        | High consequence |
| Damage tolerant   | 1,00                   | 1,15             |
| Safe life         | 1,15                   | 1,35             |

Voor staven met gatverzwakking met bouten in ruime gaten geldt volgens fig. 8.1 van NEN-EN 1993-1-9 categorie 50, met  $m=3$



Voor niet voorgespannen bouten belast op afschuiving geldt volgens fig. 8.1 van NEN-EN 1993-1-9 categorie 100, met  $m=5$ .



Het belastingspectrum is in de NNA (NEN-EN 50341-2-15) als volgt gedefinieerd.

**Table 4.11/NL.1 Load spectra line galloping for tension supports**

| Load spectra line galloping for tension supports |                   | Number of load cycles in 50 years |              |
|--|-------------------|-----------------------------------|--------------|
| Number   | Peak-to-peak load | Ice region A                      | Ice region B |
| 1  | 2·EDS             | 7.000                             | 3.000        |
| 2  | 1,5·EDS           | 36.000                            | 17.000       |
| 3  | 1,0·EDS           | 125.000                           | 65.000       |
| 4  | 0,5·EDS           | 482.000                           | 265.000      |

#### Aanpak

De vier belastingen van 0,5 tot 2,0EDS hebben een vaste onderlinge verhouding. Aangezien het aantal wisselingen zich in het  $m=3$  gebied van de vermoeiingskromme bevindt vanwege  $n < 2 \times 10^6$ , kan een relatie worden afgeleid tussen de grootte van de spanningswissel met bijvoorbeeld 1,0EDS en de spanningswisseling die bij  $2 \times 10^6$  wisselingen op basis van het spectrum nog net toelaatbaar is. Dit staat bekend als de equivalente spanningen methode. Via de factor lambda kan de spanningswisseling worden berekend.

$$\lambda = \left[ \frac{\sum \Delta\sigma_i^m \cdot n_i}{2 \cdot 10^6} \right]^{\frac{1}{m}}$$

Toepassen van de formule voor een spanning van 1 N/mm<sup>2</sup> bij 1,0EDS levert:

| Helling<br>IJsgebied<br>Wisseling                       | m=3                     |                         | m=5                     |                         |
|---|-------------------------|-------------------------|-------------------------|-------------------------|
|   | A                       | B                       | A                       | B                       |
|   | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ | $\sigma_i^m \times n_i$ |
| 2,0EDS  | 5,60E+04                | 2,40E+04                | 2,24E+05                | 9,60E+04                |
| 1,5EDS  | 1,22E+05                | 5,74E+04                | 2,73E+05                | 1,29E+05                |
| 1,0EDS  | 1,25E+05                | 6,50E+04                | 1,25E+05                | 6,50E+04                |
| 0,5EDS  | 6,03E+04                | 3,31E+04                | 1,51E+04                | 8,28E+03                |
| $\Sigma \sigma_i^m \times n_i$                          | 3,63E+05                | 1,80E+05                | 6,37E+05                | 2,98E+05                |
| $\lambda = (\Sigma \sigma_i n_i / 2 \times 10^6)^{1/m}$ | 0,57                    | 0,45                    | 0,80                    | 0,68                    |

Voor ijsgebied A is de toelaatbare spanningswisseling bij 1,0 EDS en 125.000 wisselingen dus 1/0,57 (175%) van de toelaatbare spanningswisseling bij een aantal wisselingen van  $2,0 \times 10^6$ . Er kan ook worden gesteld dat als de spanningswisselingen van 1,0 EDS 363.000 maal voorkomen, dezelfde schade wordt behaald als de vier niveaus afzonderlijk. Deze aanpak is gehanteerd.

- In de berekening van de mast wordt telkens één afspanpunt van de geleiders belast met een trekkracht in lijnrichting van 1,0 EDS.
- Het aantal wisselingen dat deze trekkracht voorkomt wordt vergroot om het hele spectrum te vervangen, dit is afhankelijk van ijsgebied en m-factor.
- Voor iedere staaf in de constructie wordt de schade berekend als gevolg van de trekkracht voor elke geleider.
- De schade wordt gesommeerd over alle geleiders.
- De toetsing is uitgedrukt als de verhouding tussen de optredende spanningswisseling bij  $n = 2 \times 10^6$  wisselingen en de toelaatbare spanningswisseling (43 MPa voor het staalprofiel en 87 MPa voor de bout).

## Resultaten

In de tabel zijn de resultaten van mast HB+5/n gegeven. Vanwege de exponentiële invloed van het spanningsniveau heeft de verdeling van de U.C.'s een grote variatie. Het meest zwaar belast zijn de onderranden van de traverse ter plaatse van de aansluiting aan het mastlichaam. De conclusie is dat de staven en bouten voldoen.



**Check galloping**

Datum: 26-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RL  
 HB+5/n

| Group | Omschrijving                    | Profiel    | Aantal bouten | Bout | Controle netto oppervlak profiel |              |             |              |              |              |         |           |            |              | Controle boutdoorsnede |              |         |      |  |  |
|-------|---------------------------------|------------|---------------|------|----------------------------------|--------------|-------------|--------------|--------------|--------------|---------|-----------|------------|--------------|------------------------|--------------|---------|------|--|--|
|       |                                 |            |               |      | ΔF;o [kN]                        | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;i;o [Mpa] | Δσ;c;o [Mpa] | UC opp. | ΔF;b [kN] | Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa]             | Δσ;c;b [Mpa] | UC bout |      |  |  |
| 100A  | BVNSTK - Main member            | 120x120x10 | 0             | 0    | 12,3                             | 2320         | 2320        | 2320         | 5,3          | 50           | 43      | 0,12      | 18,4       | 0            | 0,0                    | 100          | 87      | 0,00 |  |  |
| 100B  | BVNSTK - Main member            | 120x120x10 | 6             | M24  | 23,2                             | 2320         | 2060        | 11,3         | 50           | 43           | 0,26    | 34,0      | 452        | 12,5         | 100                    | 87           | 0,14    |      |  |  |
| 101   | BVNSTK - Horizontal front       | 160x160x15 | 8             | M24  | 81,5                             | 4671         | 4281        | 19,0         | 50           | 43           | 0,44    | 118,9     | 452        | 32,9         | 100                    | 87           | 0,38    |      |  |  |
| 102A  | Derde TSNSTK - Main member      | 160x160x15 | 8             | M24  | 46,4                             | 4671         | 4281        | 10,8         | 50           | 43           | 0,25    | 68,5      | 452        | 25,2         | 100                    | 87           | 0,29    |      |  |  |
| 102B  | Derde TSNSTK - Main member      | 160x160x15 | 8             | M24  | 52,2                             | 4671         | 4281        | 12,2         | 50           | 43           | 0,28    | 74,8      | 452        | 20,7         | 100                    | 87           | 0,24    |      |  |  |
| 103   | Derde TSNSTK - Horizontal front | 160x160x15 | 10            | M24  | 84,5                             | 4671         | 4281        | 19,7         | 50           | 43           | 0,45    | 122,7     | 452        | 27,2         | 100                    | 87           | 0,31    |      |  |  |
| 105A  | Eerste TSNSTK - Main member     | 200x200x18 | 10            | M24  | 92,7                             | 6910         | 6442        | 14,4         | 50           | 43           | 0,33    | 120,0     | 452        | 26,6         | 100                    | 87           | 0,31    |      |  |  |
| 105B  | Eerste TSNSTK - Main member     | 200x200x20 | 12            | M24  | 109,0                            | 7640         | 7120        | 15,3         | 50           | 43           | 0,35    | 135,3     | 452        | 25,0         | 100                    | 87           | 0,29    |      |  |  |
| 106A  | BRKSTK - Main member            | 200x200x20 | 12            | M24  | 109,3                            | 7640         | 7120        | 15,4         | 50           | 43           | 0,35    | 133,1     | 452        | 24,5         | 100                    | 87           | 0,28    |      |  |  |
| 106B  | BRKSTK - Main member            | 200x200x20 | 12            | M24  | 109,4                            | 7640         | 7120        | 15,4         | 50           | 43           | 0,35    | 133,2     | 452        | 24,6         | 100                    | 87           | 0,28    |      |  |  |
| 107A  | Eerste DWSRM - Main member bc   | 160x160x15 | 10            | M24  | 133,4                            | 4671         | 4281        | 31,2         | 50           | 43           | 0,72    | 196,6     | 452        | 43,5         | 100                    | 87           | 0,50    |      |  |  |
| 107B  | Eerste DWSRM - Main member bc   | 160x160x15 | 6             | M24  | 102,4                            | 4671         | 4281        | 23,9         | 50           | 43           | 0,55    | 156,3     | 452        | 57,6         | 100                    | 87           | 0,66    |      |  |  |
| 107C  | Eerste DWSRM - Main member bc   | 160x160x15 | 0             |      | 128,0                            | 4671         | 4671        | 27,4         | 50           | 43           | 0,63    | 190,2     | 0          | 0,0          | 100                    | 87           | 0,00    |      |  |  |
| 108A  | Eerste DWSRM - Main member bc   | 150x150x14 | 6             | M24  | 97,1                             | 4014         | 3650        | 26,6         | 50           | 43           | 0,61    | 148,3     | 452        | 54,7         | 100                    | 87           | 0,63    |      |  |  |
| 108C  | Eerste DWSRM - Main member bc   | 150x150x14 | 0             |      | 86,9                             | 4014         | 4014        | 21,7         | 50           | 43           | 0,50    | 132,7     | 0          | 0,0          | 100                    | 87           | 0,00    |      |  |  |
| 109A  | Eerste DWSRM - Main member to   | 120x120x10 | 4             | M24  | 16,7                             | 2320         | 2060        | 8,1          | 50           | 43           | 0,19    | 25,0      | 452        | 13,8         | 100                    | 87           | 0,16    |      |  |  |
| 109B  | Eerste DWSRM - Main member to   | 120x120x10 | 4             | M24  | 15,8                             | 2320         | 2060        | 7,7          | 50           | 43           | 0,18    | 23,8      | 452        | 13,2         | 100                    | 87           | 0,15    |      |  |  |
| 110A  | Eerste DWSRM - Main member to   | 110x110x10 | 0             |      | 15,3                             | 2112         | 1852        | 8,2          | 50           | 43           | 0,19    | 23,2      | 452        | 12,8         | 100                    | 87           | 0,15    |      |  |  |
| 110B  | Eerste DWSRM - Main member to   | 110x110x10 | 0             |      | 15,2                             | 2112         | 2112        | 7,2          | 50           | 43           | 0,17    | 23,1      | 0          | 0,0          | 100                    | 87           | 0,00    |      |  |  |
| 111A  | Tweede DWSRM - Main member l    | 150x150x12 | 8             | M24  | 92,6                             | 3480         | 3168        | 29,2         | 50           | 43           | 0,67    | 141,4     | 452        | 39,1         | 100                    | 87           | 0,45    |      |  |  |
| 111C  | Tweede DWSRM - Main member l    | 150x150x12 | 0             |      | 87,8                             | 3480         | 3480        | 25,2         | 50           | 43           | 0,58    | 134,0     | 0          | 0,0          | 100                    | 87           | 0,00    |      |  |  |
| 112A  | Tweede DWSRM - Main member l    | 100x100x8  | 2             | M24  | 4,6                              | 1550         | 1342        | 3,5          | 50           | 43           | 0,08    | 6,7       | 452        | 7,5          | 100                    | 87           | 0,09    |      |  |  |
| 112B  | Tweede DWSRM - Main member l    | 100x100x8  | 2             | M24  | 3,5                              | 1550         | 1342        | 2,6          | 50           | 43           | 0,06    | 5,3       | 452        | 5,9          | 100                    | 87           | 0,07    |      |  |  |
| 113A  | Tweede DWSRM - Main member t    | 120x120x12 | 4             | M24  | 49,2                             | 2750         | 2438        | 20,2         | 50           | 43           | 0,46    | 67,8      | 452        | 37,5         | 100                    | 87           | 0,43    |      |  |  |
| 113B  | Tweede DWSRM - Main member t    | 120x120x10 | 4             | M24  | 40,1                             | 2320         | 2060        | 19,4         | 50           | 43           | 0,45    | 56,2      | 452        | 31,1         | 100                    | 87           | 0,36    |      |  |  |
| 113C  | Tweede DWSRM - Main member t    | 120x120x12 | 0             |      | 45,2                             | 2750         | 2750        | 16,4         | 50           | 43           | 0,38    | 63,4      | 0          | 0,0          | 100                    | 87           | 0,00    |      |  |  |
| 114A  | Tweede DWSRM - Main member t    | 120x120x10 | 4             | M24  | 38,9                             | 2320         | 2060        | 18,9         | 50           | 43           | 0,43    | 54,7      | 452        | 30,2         | 100                    | 87           | 0,35    |      |  |  |
| 114B  | Tweede DWSRM - Main member t    | 120x120x12 | 2             | M24  | 3,5                              | 2750         | 2438        | 1,4          | 50           | 43           | 0,03    | 4,9       | 452        | 5,4          | 100                    | 87           | 0,06    |      |  |  |
| 114C  | Tweede DWSRM - Main member t    | 120x120x10 | 0             |      | 35,3                             | 2320         | 2320        | 15,2         | 50           | 43           | 0,35    | 49,6      | 0          | 0,0          | 100                    | 87           | 0,00    |      |  |  |
| 200   | BVNSTK - Top cap                | 80x80x8    | 2             | M20  | 10,1                             | 1230         | 1054        | 9,6          | 50           | 43           | 0,22    | 14,1      | 314        | 22,4         | 100                    | 87           | 0,26    |      |  |  |
| 201L  | BVNSTK - Horizontal front       | 120x120x10 | 4             | M24  | 16,3                             | 2320         | 2060        | 7,9          | 50           | 43           | 0,18    | 22,7      | 452        | 12,6         | 100                    | 87           | 0,14    |      |  |  |
| 201T  | BVNSTK - Horizontal side        | 80x80x6    | 2             | M20  | 0,9                              | 940          | 808         | 1,1          | 50           | 43           | 0,03    | 1,3       | 314        | 2,0          | 100                    | 87           | 0,02    |      |  |  |
| 202L  | BVNSTK - CD front               | 100x100x8  | 2             | M24  | 15,3                             | 1550         | 1342        | 11,4         | 50           | 43           | 0,26    | 21,6      | 452        | 23,8         | 100                    | 87           | 0,27    |      |  |  |
| 202T  | BVNSTK - CD side                | 90x90x8    | 2             | M24  | 10,4                             | 1390         | 1182        | 8,8          | 50           | 43           | 0,20    | 14,7      | 452        | 16,2         | 100                    | 87           | 0,19    |      |  |  |
| 203T  | BVNSTK - Horizontal side        | 90x90x8    | 4             | M24  | 30,7                             | 1390         | 1182        | 26,0         | 50           | 43           | 0,60    | 41,8      | 452        | 23,1         | 100                    | 87           | 0,27    |      |  |  |



**Check galloping**

Datum: 26-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RL  
 HB+5/n

| Group | Omschrijving                      | Profiel    | Aantal<br>bouten | Bout | Controle netto oppervlak profiel |                 |                |               |               |                 |            |              |                       |                 | Controle boutdoorsnede |                 |            |  |  |
|-------|-----------------------------------|------------|------------------|------|----------------------------------|-----------------|----------------|---------------|---------------|-----------------|------------|--------------|-----------------------|-----------------|------------------------|-----------------|------------|--|--|
|       |                                   |            |                  |      | ΔF;o<br>[kN]                     | Brutto<br>[mm2] | Netto<br>[mm2] | Δσ;o<br>[Mpa] | DC;o<br>[Mpa] | Δσ;c;o<br>[Mpa] | UC<br>opp. | ΔF;b<br>[kN] | Opp.<br>Bout<br>[mm2] | Δσ;i;b<br>[Mpa] | DC;b<br>[Mpa]          | Δσ;c;b<br>[Mpa] | UC<br>bout |  |  |
| 204L  | BVNSTK - CD front                 | 140x140x13 | 4                | M24  | 69,8                             | 3521            | 3183           | 21,9          | 50            | 43              | 0,50       | 96,4         | 452                   | 53,3            | 100                    | 87              | 0,61       |  |  |
| 204T  | BVNSTK - CD side                  | 140x140x13 | 4                | M24  | 68,0                             | 3521            | 3183           | 21,4          | 50            | 43              | 0,49       | 97,5         | 452                   | 53,9            | 100                    | 87              | 0,62       |  |  |
| 205   | BVNSTK - Diagonal for crossarm    | 120x120x12 | 3                | M24  | 40,2                             | 2750            | 2438           | 16,5          | 50            | 43              | 0,38       | 54,7         | 452                   | 40,3            | 100                    | 87              | 0,46       |  |  |
| 206   | BVNSTK - CD for crossarm diaphr   | 50x50x5    | 1                | M16  | 0,0                              | 480             | 390            | 0,1           | 50            | 43              | 0,00       | 0,0          | 201                   | 0,2             | 100                    | 87              | 0,00       |  |  |
| 207L  | Derde TSNSTK - CD front           | 140x140x13 | 4                | M24  | 63,5                             | 3521            | 3183           | 20,0          | 50            | 43              | 0,46       | 87,8         | 452                   | 48,6            | 100                    | 87              | 0,56       |  |  |
| 207T  | Derde TSNSTK - CD side            | 140x140x13 | 4                | M24  | 61,9                             | 3521            | 3183           | 19,5          | 50            | 43              | 0,45       | 88,7         | 452                   | 49,1            | 100                    | 87              | 0,56       |  |  |
| 208L  | Derde TSNSTK - Horizontal front   | 120x120x12 | 2                | M24  | 9,7                              | 2750            | 2438           | 4,0           | 50            | 43              | 0,09       | 11,7         | 452                   | 6,5             | 100                    | 87              | 0,07       |  |  |
| 208T  | Derde TSNSTK - Horizontal side    | 120x120x10 | 2                | M24  | 2,2                              | 2320            | 2060           | 1,1           | 50            | 43              | 0,02       | 3,3          | 452                   | 3,6             | 100                    | 87              | 0,04       |  |  |
| 209L  | Derde TSNSTK - CD front           | 140x140x13 | 4                | M24  | 53,6                             | 3521            | 3183           | 16,8          | 50            | 43              | 0,39       | 77,9         | 452                   | 43,1            | 100                    | 87              | 0,50       |  |  |
| 209T  | Derde TSNSTK - CD side            | 140x140x13 | 4                | M24  | 56,1                             | 3521            | 3183           | 17,6          | 50            | 43              | 0,41       | 81,1         | 452                   | 44,9            | 100                    | 87              | 0,52       |  |  |
| 210T  | Derde TSNSTK - Horizontal side    | 120x120x10 | 3                | M24  | 32,5                             | 2320            | 2060           | 15,8          | 50            | 43              | 0,36       | 43,9         | 452                   | 32,3            | 100                    | 87              | 0,37       |  |  |
| 211   | Derde TSNSTK - Diagonal for cross | 120x120x10 | 4                | M24  | 44,3                             | 2320            | 2060           | 21,5          | 50            | 43              | 0,50       | 59,9         | 452                   | 33,1            | 100                    | 87              | 0,38       |  |  |
| 212   | Derde TSNSTK - CD for crossarm    | 55x55x6    | 1                | M16  | 0,0                              | 600             | 492            | 0,1           | 50            | 43              | 0,00       | 0,0          | 201                   | 0,2             | 100                    | 87              | 0,00       |  |  |
| 213L  | Tweede TSNSTK - CD front          | 140x140x13 | 5                | M24  | 68,6                             | 3521            | 3183           | 21,5          | 50            | 43              | 0,50       | 87,0         | 452                   | 38,5            | 100                    | 87              | 0,44       |  |  |
| 213T  | Tweede TSNSTK - CD side           | 140x140x13 | 5                | M24  | 66,3                             | 3521            | 3183           | 20,8          | 50            | 43              | 0,48       | 83,2         | 452                   | 36,8            | 100                    | 87              | 0,42       |  |  |
| 214L  | Tweede TSNSTK - CD front          | 140x140x13 | 4                | M24  | 56,3                             | 3521            | 3183           | 17,7          | 50            | 43              | 0,41       | 71,4         | 452                   | 39,5            | 100                    | 87              | 0,45       |  |  |
| 214T  | Tweede TSNSTK - CD side           | 140x140x13 | 4                | M24  | 54,5                             | 3521            | 3183           | 17,1          | 50            | 43              | 0,39       | 68,3         | 452                   | 37,8            | 100                    | 87              | 0,43       |  |  |
| 215L  | Eerste TSNSTK - Diagonal front    | 140x140x13 | 4                | M24  | 46,1                             | 3521            | 3183           | 14,5          | 50            | 43              | 0,33       | 58,4         | 452                   | 32,3            | 100                    | 87              | 0,37       |  |  |
| 215T  | Eerste TSNSTK - Diagonal side     | 140x140x13 | 4                | M24  | 47,1                             | 3521            | 3183           | 14,8          | 50            | 43              | 0,34       | 59,4         | 452                   | 32,8            | 100                    | 87              | 0,38       |  |  |
| 216L  | Eerste TSNSTK - CD front          | 150x150x12 | 4                | M24  | 35,6                             | 3480            | 3168           | 11,2          | 50            | 43              | 0,26       | 44,9         | 452                   | 24,8            | 100                    | 87              | 0,29       |  |  |
| 216T  | Eerste TSNSTK - CD side           | 150x150x12 | 4                | M24  | 38,4                             | 3480            | 3168           | 12,1          | 50            | 43              | 0,28       | 48,5         | 452                   | 26,8            | 100                    | 87              | 0,31       |  |  |
| 217L  | BRKSTK - Diagonal front           | 150x150x12 | 4                | M24  | 39,0                             | 3480            | 3168           | 12,3          | 50            | 43              | 0,28       | 48,7         | 452                   | 26,7            | 100                    | 87              | 0,31       |  |  |
| 217T  | BRKSTK - Diagonal side            | 150x150x12 | 4                | M24  | 39,0                             | 3480            | 3168           | 12,3          | 50            | 43              | 0,28       | 48,7         | 452                   | 26,9            | 100                    | 87              | 0,31       |  |  |
| 218L  | BRKSTK - Horizontal front         | 100x100x8  | 2                | M24  | 0,3                              | 1550            | 1342           | 0,2           | 50            | 43              | 0,00       | 0,3          | 452                   | 0,4             | 100                    | 87              | 0,00       |  |  |
| 218T  | BRKSTK - Horizontal side          | 100x100x8  | 2                | M24  | 0,4                              | 1550            | 1342           | 0,3           | 50            | 43              | 0,01       | 0,5          | 452                   | 0,5             | 100                    | 87              | 0,01       |  |  |
| 300   | Eerste DWSRM - Diagonal front     | 100x100x8  | 2                | M20  | 5,3                              | 1550            | 1374           | 3,9           | 50            | 43              | 0,09       | 7,5          | 314                   | 11,9            | 100                    | 87              | 0,14       |  |  |
| 301   | Eerste DWSRM - Diagonal front     | 90x90x8    | 2                | M20  | 8,7                              | 1390            | 1214           | 7,2           | 50            | 43              | 0,17       | 12,3         | 314                   | 19,6            | 100                    | 87              | 0,22       |  |  |
| 302   | Eerste DWSRM - Diagonal front     | 70x70x6    | 1                | M20  | 1,5                              | 810             | 678            | 2,2           | 50            | 43              | 0,05       | 2,3          | 314                   | 7,3             | 100                    | 87              | 0,08       |  |  |
| 303   | Eerste DWSRM - Vertical front     | 80x80x6    | 1                | M20  | 3,8                              | 940             | 808            | 4,8           | 50            | 43              | 0,11       | 5,4          | 314                   | 17,2            | 100                    | 87              | 0,20       |  |  |
| 304   | Eerste DWSRM - Vertical front     | 70x70x6    | 1                | M20  | 0,8                              | 810             | 678            | 1,2           | 50            | 43              | 0,03       | 1,1          | 314                   | 3,6             | 100                    | 87              | 0,04       |  |  |
| 305   | Eerste DWSRM - Vertical front     | 50x50x5    | 1                | M16  | 0,2                              | 480             | 390            | 0,5           | 50            | 43              | 0,01       | 0,3          | 201                   | 1,3             | 100                    | 87              | 0,02       |  |  |
| 306   | Eerste DWSRM - CD under           | 80x80x8    | 2                | M20  | 14,5                             | 1230            | 1054           | 13,8          | 50            | 43              | 0,32       | 20,2         | 314                   | 32,2            | 100                    | 87              | 0,37       |  |  |
| 307   | Eerste DWSRM - CD under           | 80x80x8    | 2                | M20  | 16,2                             | 1230            | 1054           | 15,4          | 50            | 43              | 0,35       | 22,5         | 314                   | 35,8            | 100                    | 87              | 0,41       |  |  |
| 308   | Eerste DWSRM - CD under           | 80x80x8    | 2                | M20  | 18,0                             | 1230            | 1054           | 17,1          | 50            | 43              | 0,39       | 25,0         | 314                   | 39,9            | 100                    | 87              | 0,46       |  |  |
| 309   | Eerste DWSRM - CD under           | 80x80x8    | 2                | M20  | 19,4                             | 1230            | 1054           | 18,4          | 50            | 43              | 0,42       | 27,0         | 314                   | 42,9            | 100                    | 87              | 0,49       |  |  |



**Check galloping**

Datum: 26-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RL  
 HB+5/n

| Group | Omschrijving                     | Profiel                  | Aantal bouten | Bout | Controle netto oppervlak profiel |              |             |              |            |              |         |           |            |              | Controle boutdoorsnede |              |         |  |  |  |
|-------|----------------------------------|--------------------------|---------------|------|----------------------------------|--------------|-------------|--------------|------------|--------------|---------|-----------|------------|--------------|------------------------|--------------|---------|--|--|--|
|       |                                  |                          |               |      | ΔF;o [kN]                        | Brutto [mm2] | Netto [mm2] | Δσ;i;o [Mpa] | DC;o [Mpa] | Δσ;c;o [Mpa] | UC opp. | ΔF;b [kN] | Bout [mm2] | Δσ;i;b [Mpa] | DC;b [Mpa]             | Δσ;c;b [Mpa] | UC bout |  |  |  |
| 311   | Eerste DWSRM - CD onder          | 70x70x6                  | 2             | M20  | 9,0                              | 810          | 678         | 13,3         | 50         | 43           | 0,31    | 13,8      | 314        | 22,0         | 100                    | 87           | 0,25    |  |  |  |
| 312   | Eerste DWSRM - CD onder          | 70x70x6                  | 2             | M20  | 10,2                             | 810          | 678         | 15,1         | 50         | 43           | 0,35    | 15,6      | 314        | 24,9         | 100                    | 87           | 0,29    |  |  |  |
| 313   | Eerste DWSRM - CD onder          | 70x70x6                  | 2             | M20  | 12,7                             | 810          | 678         | 18,7         | 50         | 43           | 0,43    | 19,3      | 314        | 30,8         | 100                    | 87           | 0,35    |  |  |  |
| 314   | Eerste DWSRM - CD onder          | 70x70x7                  | 2             | M20  | 14,0                             | 940          | 786         | 17,8         | 50         | 43           | 0,41    | 21,4      | 314        | 34,0         | 100                    | 87           | 0,39    |  |  |  |
| 316   | Eerste DWSRM - CD onder          | 70x70x7                  | 2             | M20  | 16,3                             | 940          | 786         | 20,8         | 50         | 43           | 0,48    | 24,9      | 314        | 39,7         | 100                    | 87           | 0,46    |  |  |  |
| 319   | Eerste DWSRM - Horizontaal onder | 150x150x14 (not coupled) | 2             | M20  | 18,8                             | 8028         | 7720        | 2,4          | 50         | 43           | 0,06    | 26,1      | 314        | 41,5         | 100                    | 87           | 0,48    |  |  |  |
| 320   | Eerste DWSRM - Horizontaal onder | HEA160                   | 2             | M20  | 0,8                              | 3900         | 3680        | 0,2          | 50         | 43           | 0,00    | 1,1       | 314        | 1,7          | 100                    | 87           | 0,02    |  |  |  |
| 321   | Eerste DWSRM - Horizontaal onder | 150x150x14 (not coupled) | 2             | M20  | 10,8                             | 8028         | 7720        | 1,4          | 50         | 43           | 0,03    | 16,6      | 314        | 26,4         | 100                    | 87           | 0,30    |  |  |  |
| 322   | Eerste DWSRM - Horizontaal onder | 150x150x14 (not coupled) | 2             | M20  | 2,8                              | 8028         | 7720        | 0,4          | 50         | 43           | 0,01    | 4,3       | 314        | 6,8          | 100                    | 87           | 0,08    |  |  |  |
| 329   | Eerste DWSRM - Diagonaal onder   | 70x70x7                  | 2             | M20  | 11,2                             | 940          | 786         | 14,3         | 50         | 43           | 0,33    | 15,0      | 314        | 23,8         | 100                    | 87           | 0,27    |  |  |  |
| 330   | Eerste DWSRM - CD doorsnede A    | 50x50x5                  | 1             | M16  | 1,1                              | 480          | 390         | 2,9          | 50         | 43           | 0,07    | 1,6       | 201        | 7,9          | 100                    | 87           | 0,09    |  |  |  |
| 331   | Eerste DWSRM - Horizontaal on to | 60x60x6                  | 1             | M16  | 0,6                              | 690          | 582         | 1,1          | 50         | 43           | 0,02    | 0,9       | 201        | 4,4          | 100                    | 87           | 0,05    |  |  |  |
| 400   | Tweede DWSRM - Main diagonal     | 120x120x10               | 4             | M24  | 26,7                             | 2320         | 2060        | 13,0         | 50         | 43           | 0,30    | 40,7      | 452        | 22,5         | 100                    | 87           | 0,26    |  |  |  |
| 401   | Tweede DWSRM - Vertical front    | 50x50x5                  | 1             | M16  | 0,7                              | 480          | 390         | 1,8          | 50         | 43           | 0,04    | 1,1       | 201        | 5,4          | 100                    | 87           | 0,06    |  |  |  |
| 402   | Tweede DWSRM - Vertical front    | 70x70x6                  | 1             | M20  | 4,8                              | 810          | 678         | 7,1          | 50         | 43           | 0,16    | 7,4       | 314        | 23,5         | 100                    | 87           | 0,27    |  |  |  |
| 403   | Tweede DWSRM - Vertical front    | 60x60x6                  | 1             | M16  | 0,2                              | 690          | 582         | 0,3          | 50         | 43           | 0,01    | 0,3       | 201        | 1,3          | 100                    | 87           | 0,01    |  |  |  |
| 404   | Tweede DWSRM - Vertical front    | 50x50x5                  | 1             | M16  | 0,1                              | 480          | 390         | 0,1          | 50         | 43           | 0,00    | 0,1       | 201        | 0,4          | 100                    | 87           | 0,00    |  |  |  |
| 405   | Tweede DWSRM - Diagonaal front   | 70x70x6                  | 1             | M20  | 2,7                              | 810          | 678         | 3,9          | 50         | 43           | 0,09    | 4,0       | 314        | 12,8         | 100                    | 87           | 0,15    |  |  |  |
| 406   | Tweede DWSRM - Diagonaal front   | 100x100x10               | 3             | M24  | 9,3                              | 1920         | 1660        | 5,6          | 50         | 43           | 0,13    | 14,2      | 452        | 10,4         | 100                    | 87           | 0,12    |  |  |  |
| 407   | Tweede DWSRM - Diagonaal front   | 70x70x6                  | 1             | M16  | 0,1                              | 810          | 702         | 0,1          | 50         | 43           | 0,00    | 0,1       | 201        | 0,4          | 100                    | 87           | 0,00    |  |  |  |
| 408   | Tweede DWSRM - UNP member        | UNP160                   | 2             | M20  | 4,1                              | 2400         | 2235        | 1,8          | 50         | 43           | 0,04    | 5,8       | 314        | 9,2          | 100                    | 87           | 0,11    |  |  |  |
| 409   | Tweede DWSRM - Doorsnede A-A     | 70x70x6                  | 1             | M16  | 9,1                              | 810          | 702         | 12,9         | 50         | 43           | 0,30    | 13,8      | 201        | 68,7         | 100                    | 87           | 0,79    |  |  |  |
| 411   | Tweede DWSRM - CD top            | 70x70x6                  | 1             | M20  | 7,7                              | 810          | 678         | 11,4         | 50         | 43           | 0,26    | 11,6      | 314        | 37,0         | 100                    | 87           | 0,43    |  |  |  |
| 412   | Tweede DWSRM - CD top            | 70x70x6                  | 1             | M20  | 9,2                              | 810          | 678         | 13,6         | 50         | 43           | 0,31    | 13,8      | 314        | 44,0         | 100                    | 87           | 0,51    |  |  |  |
| 413   | Tweede DWSRM - CD top            | 70x70x6                  | 1             | M20  | 10,9                             | 810          | 678         | 16,0         | 50         | 43           | 0,37    | 16,3      | 314        | 51,9         | 100                    | 87           | 0,60    |  |  |  |
| 414   | Tweede DWSRM - CD top            | 50x50x5                  | 1             | M16  | 2,4                              | 480          | 390         | 6,2          | 50         | 43           | 0,14    | 3,4       | 201        | 16,9         | 100                    | 87           | 0,19    |  |  |  |
| 415   | Tweede DWSRM - CD top            | 50x50x5                  | 1             | M16  | 2,9                              | 480          | 390         | 7,4          | 50         | 43           | 0,17    | 4,1       | 201        | 20,3         | 100                    | 87           | 0,23    |  |  |  |
| 416   | Tweede DWSRM - CD top            | 50x50x5                  | 1             | M16  | 3,4                              | 480          | 390         | 8,6          | 50         | 43           | 0,20    | 4,7       | 201        | 23,5         | 100                    | 87           | 0,27    |  |  |  |
| 417   | Tweede DWSRM - CD top            | 50x50x5                  | 1             | M16  | 3,4                              | 480          | 390         | 8,6          | 50         | 43           | 0,20    | 4,7       | 201        | 23,6         | 100                    | 87           | 0,27    |  |  |  |
| 418   | Tweede DWSRM - CD top            | 50x50x5                  | 1             | M16  | 3,7                              | 480          | 390         | 9,6          | 50         | 43           | 0,22    | 5,3       | 201        | 26,2         | 100                    | 87           | 0,30    |  |  |  |
| 419   | Tweede DWSRM - CD top            | 50x50x5                  | 1             | M16  | 4,2                              | 480          | 390         | 10,7         | 50         | 43           | 0,25    | 5,9       | 201        | 29,3         | 100                    | 87           | 0,34    |  |  |  |
| 422   | Tweede DWSRM - CD onder          | 70x70x6                  | 2             | M20  | 4,5                              | 810          | 678         | 6,6          | 50         | 43           | 0,15    | 6,8       | 314        | 10,9         | 100                    | 87           | 0,12    |  |  |  |
| 423   | Tweede DWSRM - CD onder          | 70x70x6                  | 2             | M20  | 5,4                              | 810          | 678         | 8,0          | 50         | 43           | 0,18    | 8,3       | 314        | 13,1         | 100                    | 87           | 0,15    |  |  |  |
| 424   | Tweede DWSRM - CD onder          | 70x70x6                  | 2             | M20  | 5,8                              | 810          | 678         | 8,6          | 50         | 43           | 0,20    | 8,8       | 314        | 14,0         | 100                    | 87           | 0,16    |  |  |  |
| 425   | Tweede DWSRM - CD onder          | 70x70x6                  | 2             | M20  | 6,7                              | 810          | 678         | 9,8          | 50         | 43           | 0,23    | 10,1      | 314        | 16,1         | 100                    | 87           | 0,19    |  |  |  |



**Check galloping**

Datum: 26-7-2021  
 Auteur: TBR  
 Versie: 1.0

GT-RL  
 HB+5/n

| Group | Omschrijving                  | Profiel                  | Aantal bouten | Bout | Controle netto oppervlak profiel |              |             |                          |                          |                    |                          |         |                     |                 | Controle boutdoorsnede   |            |                          |         |  |
|-------|-------------------------------|--------------------------|---------------|------|----------------------------------|--------------|-------------|--------------------------|--------------------------|--------------------|--------------------------|---------|---------------------|-----------------|--------------------------|------------|--------------------------|---------|--|
|       |                               |                          |               |      | $\Delta F;o$ [kN]                | Brutto [mm2] | Netto [mm2] | $\Delta\sigma;i;o$ [Mpa] | $\Delta\sigma;j;o$ [Mpa] | $\Delta C;o$ [Mpa] | $\Delta\sigma;c;o$ [Mpa] | UC opp. | $\Delta F;i;b$ [kN] | Opp. Bout [mm2] | $\Delta\sigma;i;b$ [Mpa] | DC;b [Mpa] | $\Delta\sigma;c;b$ [Mpa] | UC bout |  |
| 426   | Tweede DWSRM - CD under       | 70x70x7                  | 2             | M20  | 16,4                             | 940          | 786         | 20,9                     | 50                       | 43                 | 0,48                     | 25,1    | 314                 | 40,0            | 100                      | 87         | 0,46                     |         |  |
| 427   | Tweede DWSRM - CD under       | 70x70x7                  | 2             | M20  | 17,1                             | 940          | 786         | 21,7                     | 50                       | 43                 | 0,50                     | 26,1    | 314                 | 41,5            | 100                      | 87         | 0,48                     |         |  |
| 428   | Tweede DWSRM - CD under       | 70x70x7                  | 2             | M20  | 18,3                             | 940          | 786         | 23,3                     | 50                       | 43                 | 0,54                     | 28,0    | 314                 | 44,5            | 100                      | 87         | 0,51                     |         |  |
| 429   | Tweede DWSRM - CD under       | 70x70x6                  | 2             | M20  | 6,8                              | 810          | 678         | 10,1                     | 50                       | 43                 | 0,23                     | 10,4    | 314                 | 16,6            | 100                      | 87         | 0,19                     |         |  |
| 436   | Tweede DWSRM - Horizontal und | 150x150x14 (not coupled) | 2             | M20  | 8,7                              | 8028         | 7720        | 1,1                      | 50                       | 43                 | 0,03                     | 13,3    | 314                 | 21,3            | 100                      | 87         | 0,24                     |         |  |
| 437   | Tweede DWSRM - diagonaal katt | 55x55x6                  | 1             | M16  | 3,6                              | 600          | 492         | 7,3                      | 50                       | 43                 | 0,17                     | 5,3     | 201                 | 26,3            | 100                      | 87         | 0,30                     |         |  |



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## B.11 Mastrapportage bestaande reconstructiemasten

ZUID-WEST 380 KV OOST VERBINDINGEN

# **Mastrapport bestaande reconstructiemasten HB+0, HS+0 en HC+0 in GT-RLL380**

TenneT TSO B.V.

**Meridian doc.nr.:** 002.678.00 0934573

**Rapport nr.:** 21-0888, Rev. 1

**Datum:** 2021-08-11

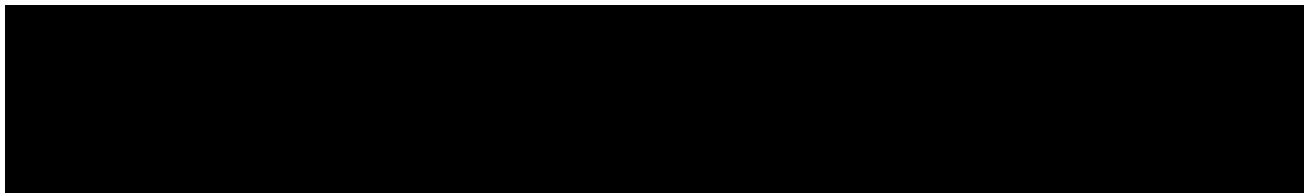




Projectnaam: Zuid-West 380 kV Oost Verbindingen  
Rapport titel: Mastrapport bestaande reconstructiemasten HB+0, HS+0 en HC+0 in GT-RLL380  
Klant: TenneT TSO B.V.,  
Contactpersoon klant: XXXXXXXXXX  
Datum uitgave: 2021-08-11  
Project nr.: 10124719  
Organisatie unit: TDT  
Meridian doc.nr.: 002.678.00 0934573  
Rapport nr.: 21-0888, Rev. 1

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|------|------------|-------------------|--|--|--|
| 0    | 2021-06-04 | Eerste uitgave    | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> |
| 1    | 2021-08-11 | Na RFA            | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> |

## Inhoudsopgave

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## 1 INLEIDING

In het basisontwerp van de vakwerkmasten voor de verbinding GT-RLL380 in het project Zuid-West 380 kV-Oost zijn voor het vaststellen van de haalbaarheid constructieve berekeningen uitgevoerd aan de masten en fundaties. In de Definitief Ontwerpfase, moeten berekeningen verder worden uitgewerkt om te kunnen dienen voor de benodigde vergunningsdocumentatie, voor de aanbesteding en als voorbereiding voor de uitvoeringsfase. Het DO omvat het ontwerp van de mastconstructies, de fundaties en de opstijpunten in de verbinding.

Deze rapportage bevat de resultaten van de toetsing van de volgende bestaande masten t.b.v. de reconstructie.

**Tabel 1 - Overzicht bestaande reconstructiemasten**

| Verbinding | Mast Nr. | Masttype |
|------------|----------|----------|
| GT-RLL     | 78       | HB+0     |
|            | 68       | HB+0     |
|            | 26       | HS+0     |
|            | 16       | HC+0     |

Deze masten zijn locatiespecifiek doorgerekend en moeten voldoen aan de belastingen uit de nieuwe situatie.

In deze rapportage zijn de toetsingen van de bovenstaande masten opgenomen. De toetsing bestaat uit controle van:

- de profielen en boutverbindingen onderdeel van de hoofd draagconstructie
- de knikverkorters
- de verbinding met de fundatie via blokdeuvels.

Buiten de scope van dit DO-rapport valt eventueel benodigde controle van de schetsplaten en overige verbindingdetails in de constructie. Dit moet in de UO-fase worden uitgewerkt.

In hoofdstuk 2 zijn de uitgangspunten en randvoorwaarden vanuit de van toepassing zijnde normen en TenneT-specificaties opgenomen. Hoofdstuk 3 beschrijft de gevolgde aanpak van de berekening. In hoofdstuk 4 is de toetsing opgenomen. Hoofdstuk 5 bevat de eventuele aanpassingen in de mast.

## 2 UITGANGSPUNTEN EN RANDVOORWAARDEN

### 2.1 Normen

Er is gebruik gemaakt van de normen volgens Tabel 2.

**Tabel 2 Gebruikgemaakte normen, voorschriften en richtlijnen**

| Norm                                       | Titel  |
|--|--|
| NEN-EN 50341-1:2013                        | “Overhead electrical lines exceeding AC 1 kV - Part 1: General requirements – Common”                        |
| NEN-EN 50341-2-15:2019                     | “Overhead electrical lines exceeding AC 1 kV Part 2 National Normative Aspects (NNA) for THE NETHERLANDS”    |
| NEN-EN 1990+A1+A1/C2:2019/NB:2019nl        | “Grondslagen van het ontwerp”  |
| NEN-EN 1991-1-4+A1+C2:2011/NB:2019+C1:2020 | “Deel 1-4: Windbelasting op constructies”  |
| NEN-EN 1992-1-1+C2:2011/NB:2016+A1:2020    | “Eurocode 2: Ontwerp en berekening van betonconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-1-1+C2+A1:2016 nl              | “Eurocode 3: Ontwerp en berekening van staalconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-3-1:2007/NB:2011 nl            | “Deel 3-1: Torens, masten en schoorstenen - Torens en masten”  |
| NEN-EN 1993-1-8+C2:2011/NB:2011 nl         | “Ontwerp en berekening van staalconstructies, deel 1-8: ontwerp en berekening van verbindingen”              |

### 2.2 TenneT-specificaties

In Tabel 3 zijn de documenten opgenomen die relevant zijn voor de berekeningen en toetsingen die binnen dit project in de mastrapportage uitgevoerd zullen worden.

**Tabel 3 Relevante documenten t.b.v. mechanische rapportages**

| Nummer          | Onderwerp                           |
|-----------------|-------------------------------------|
| PVE.05.000 v3.2 | PvE Lijnen                          |
| sPVE.05.001     | sPvE Lijnen                         |
| SPE.05.346 v1.3 | Algemene specificatie stalen masten |

### 2.3 Ontwerprapporten

Voor de achtergrond van het ontwerp wordt verwezen naar het uitgangspuntenrapport “D1.3 Uitgangspunten reconstructies”, DNV GL rapport 21-0702, Meridiannummer 002.678.00 0927721.

### 2.4 Eisenverificatie

Voor de eisenverificatie wordt verwezen naar het rapport “Verificatierapport eisen reconstructies”.

### 2.5 Materialen

Voor het ontwerp van de mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 4.

**Tabel 4 Materialen aangepaste constructie**

|                |   |
|----------------|---|
| Staalsoort     | S355J0 (t≤16 mm)<br>S355J2 (16<t≤40 mm) |
| Boutkwaliteit  | 8.8 gerolde draad                       |
| Betonkwaliteit | C30/37                                  |
| Wapeningsstaal | B500                                    |

Voor de constructie geldt conform TenneT-specificatie:

- Toe te passen bouten: M16/M20/M24;
- Voor hoekstaal is de minimale afmeting L50x5 mm;
- Minimale plaatdikte 6 mm.

Indien bestaande bouten afwijkend zijn (M12) dan is het toegestaan deze door nieuwe bouten met eenzelfde diameter te vervangen.

## 2.6 Software

De gebruikte software wordt benoemd in Tabel 5.

**Tabel 5 Toegepaste software**

| Software              |           | Versie |
|-----------------------|-----------|--------|
| Mastontwerp           | PLS-CADD  | 16.65  |
| Mastberekeningen      | PLS-TOWER | 16.65  |
| Constructieve analyse | AxisVM    | X5 R4h |

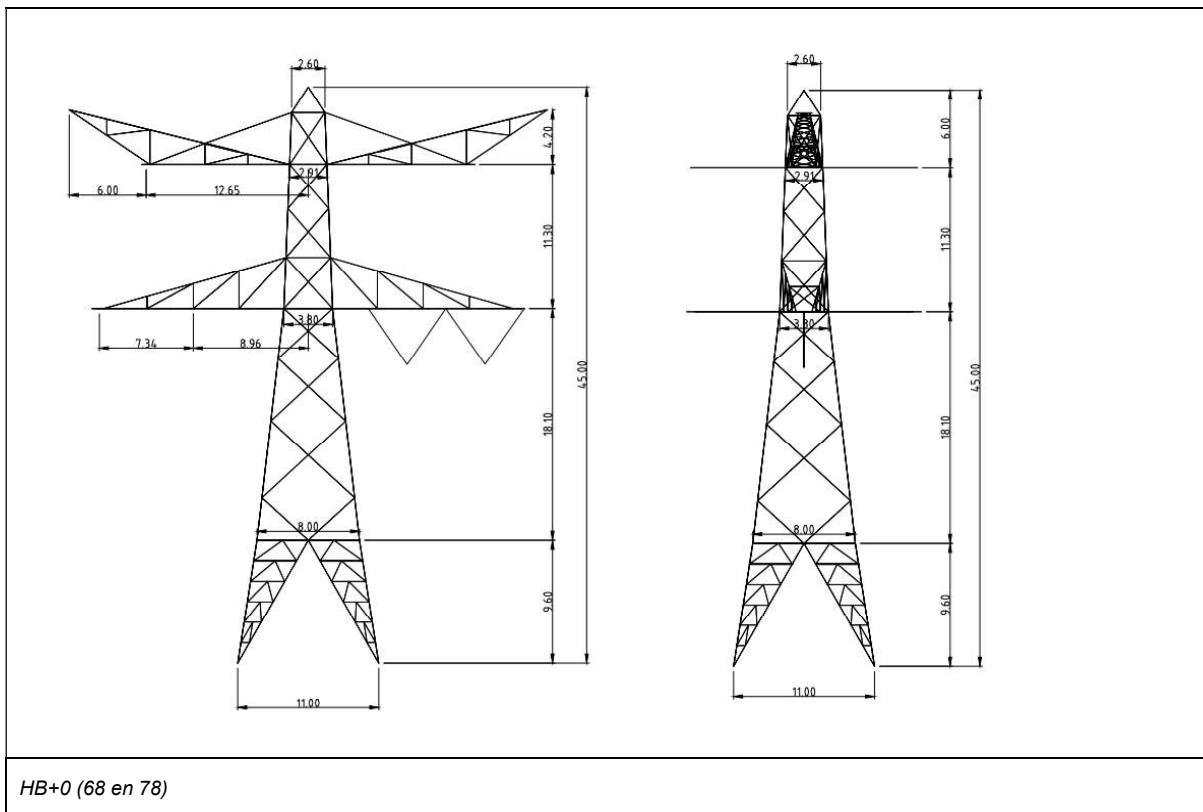
### 3 MASTONTWERP

#### 3.1 Mastbeeld

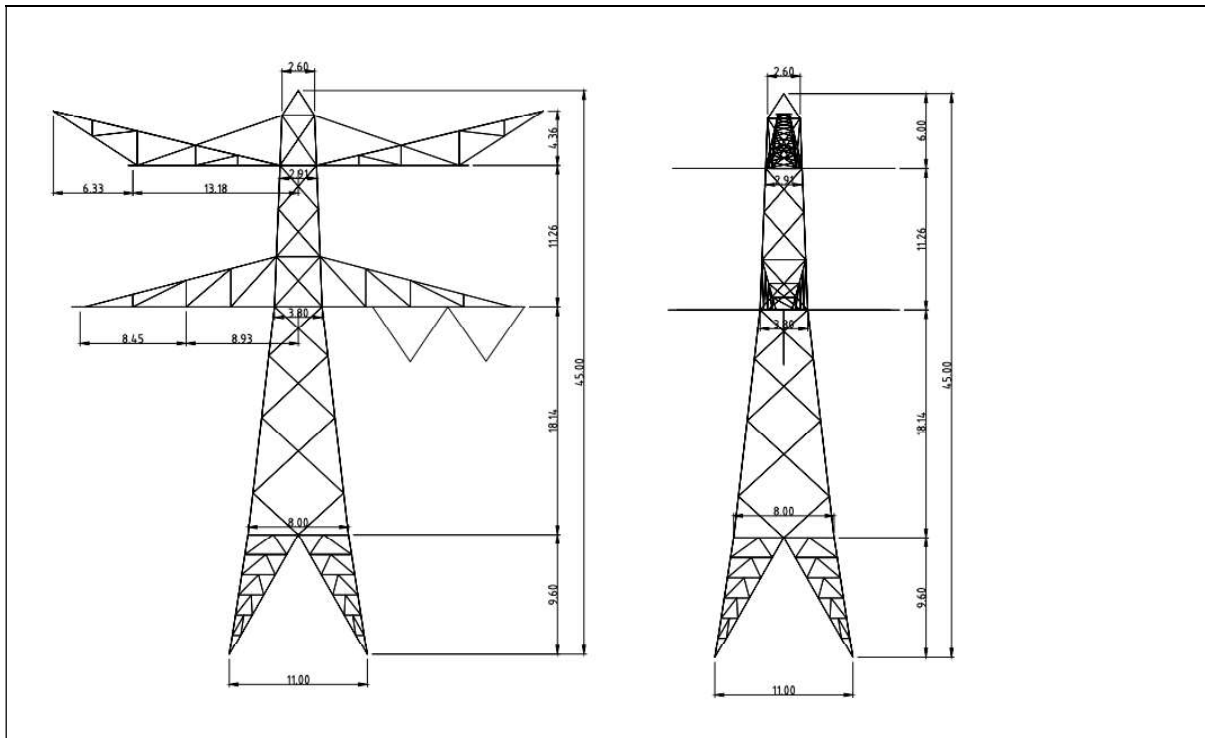
In dit hoofdstuk worden de mastbeelden weergegeven met de belangrijkste maatvoering, de figuren zijn ontleend aan de bij deze rapportage horende tekeningen van de masttypen. Het gaat om de volgende tekeningen:

- Overzichtstekening HB+0, Meridiannummer 002.678.00 0934587
- Overzichtstekening HC+0, Meridiannummer 002.678.00 0934589
- Overzichtstekening HS+0, Meridiannummer 002.678.00 0934590

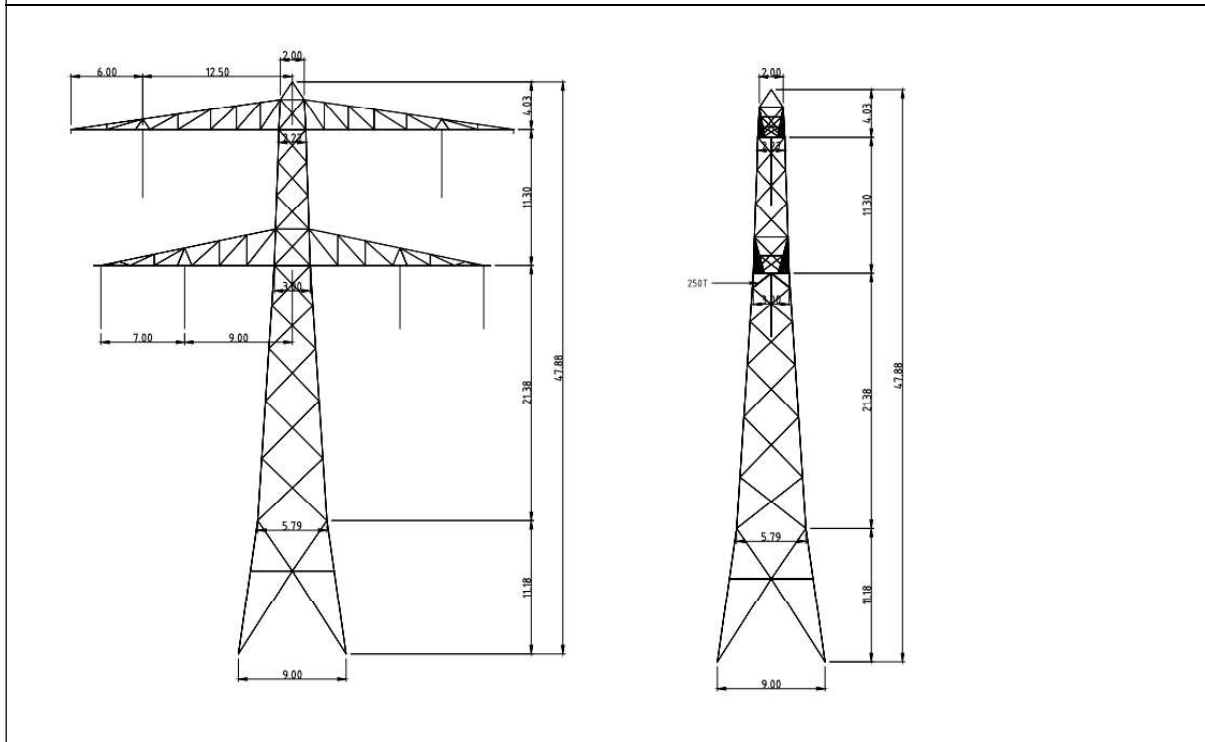
Zie in Tabel 1 de figuren van de bestaande reconstructiemasten.







HC+0 (16)



HS+0 (26)

**Figuur 1 Mastbeeld masttype HB+0, HC+0 en HS+0**

### 3.2 Uitgangspunten berekening

De uitgangspunten volgens Tabel 6 zijn van toepassing.

**Tabel 6 Uitgangspunten**

| Norm                        |  | NEN-EN50341-2-15:2019 |
|-----------------------------|--|-----------------------|
| Gevolgklasse initieel       |  | CC2-0                 |
| Betrouwbaarheidsniveau      |  | Afkeur                |
| Referentieperiode           |  | 30 jaar               |
| Gevolgklasse initieel       |  | CC2                   |
| Betrouwbaarheidsniveau      |  | Verbouw               |
| Referentieperiode           |  | 50 jaar               |
| Windgebied                  |  | III                   |
| Windsnelheid (m/s)          |  | 24,5                  |
| Terreincategorie            |  | II                    |
| Reductiefactor $c_{dir}$    |  | 1,00                  |
| IJsg gebied fasegeleider    |  | B                     |
| IJsg gebied bliksemgeleider |  | A                     |

### 3.3 Mastenlijst

In Tabel 7 zijn alle bestaande reconstructiemasten in het tracé GT-RLL opgenomen. De masten zijn locatie specifiek doorgerekend.

**Tabel 7 Mastenlijst bestaande reconstructie masten in GT-RLL380**

| Mast-nummer   | Masttype  | Lijnhoek (°) | Windspan (m) | Weightspan (m) | Hoogteverschil ba+ah (m) | Hoogteverschil back (m) | Hoogteverschil ahead (m) |
|---------------|-----------|--------------|--------------|----------------|--------------------------|-------------------------|--------------------------|
| <b>78</b>     | HB+0 (78) | 174,8        | 356,7        | 378,1          | -0,3                     | -4,8                    | 4,5                      |
| <b>68</b>     | HB+0 (68) | 180,0        | 374,3        | 335,2          | -10,4                    | -5,6                    | -4,8                     |
| <b>26(HS)</b> | HS+0 (26) | 177,3        | 343,8        | 364,3          | 5,0                      | -0,4                    | 5,4                      |
| <b>16</b>     | HC+0 (16) | 129,2        | 331,7        | 322,7          | -3,2                     | 1,6                     | -4,8                     |

*Noot: bij de hoekmastposities is de mast geroteerd ten opzichte van de bissectrice. Zie hiervoor Appendix A.*

### 3.4 Proces stappen

Het proces van het bepalen van eventueel benodigde verstevigingen bestaat uit de volgende stappen:

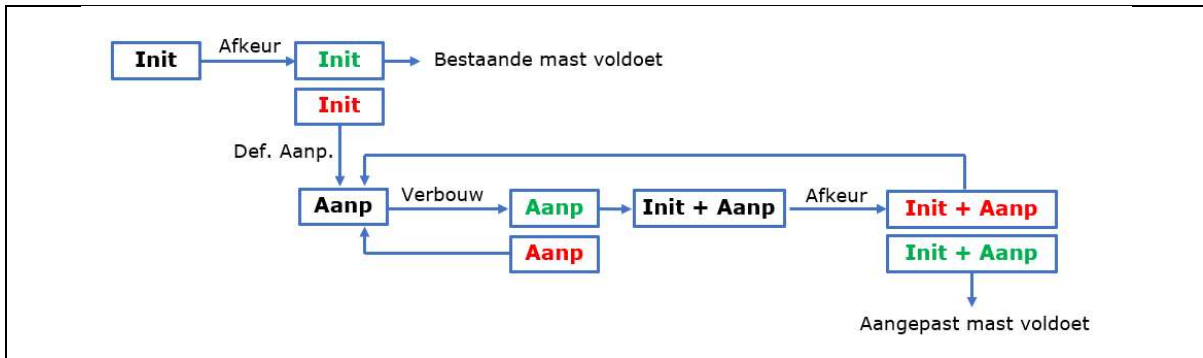
Stap 1: Toets bestaande (Init) mast op Afkeur

Stap 2: Definiëren benodigde aanpassingen indien initiële mast niet voldoet aan toets op Afkeur (Def. Aanp.)

Stap 3: Het toetsen van (alleen) de uitgewerkte aanpassingen (Aanp) op Verbouw

Stap 4: Het opnieuw toetsen van de complete mast inclusief aanpassingen (Initi + Aanp) op Afkeur

Het hierboven omschreven proces is in Figuur 1 weergegeven.



**Figuur 1** Process diagram

### 3.5 Geleiderbelastingen

De berekening is uitgevoerd met het geleiderbelastingprogramma van DNV GL. Belastingen zijn locatiespecifiek. De belastingen op de mastconstructie zijn bepaald op basis van de modellering in PLS-TOWER (staafoppervlaktes). Voor de toeslagen op eigen gewicht en windoppervlakte wordt verwezen naar het uitgangspuntenrapport. In Appendix A zijn de resultaten van de geleiderbelastingen samengevat.

### 3.6 Reacties op de fundering

De oplegreacties op de fundering worden ontleend aan de uitvoer van het geleiderbelastingenprogramma. Zie Appendix A.

### 3.7 Modelling

Op basis van de ontwerptekeningen is de mast in PLS-TOWER ingevoerd. De toetsing wordt per staafgroep uitgevoerd. De hoofdelementen zijn gemodelleerd, niet-dragende profielen als knikverkorters zijn weggelaten, deze worden separaat getoetst. De profielen zijn in PLS-TOWER inclusief de boutverbindingen ingevoerd en getoetst, de controle van de schetsplaten en andere detailverbindingen valt buiten de scope.

De geleiderbelastingen vanuit het geleiderbelastingenprogramma zijn als invoer voor de belastingen gebruikt.

De gewichts- en windbelasting op de mastconstructie wordt door PLS-TOWER automatisch bepaald. Via toeslagfactoren wordt de invloed van niet gemodelleerde elementen als knikverkorters, bordesconstructies en klimvoorzieningen meegenomen. Voor schetsplaten, zinklaag en bouten is een aanvullende toeslag op het gewicht van 20% toeslag gerekend.

Diagonalen in voor- en achtervlak respectievelijk de twee zijvlakken zijn samengenomen in een groep.

### 3.8 Overige controles

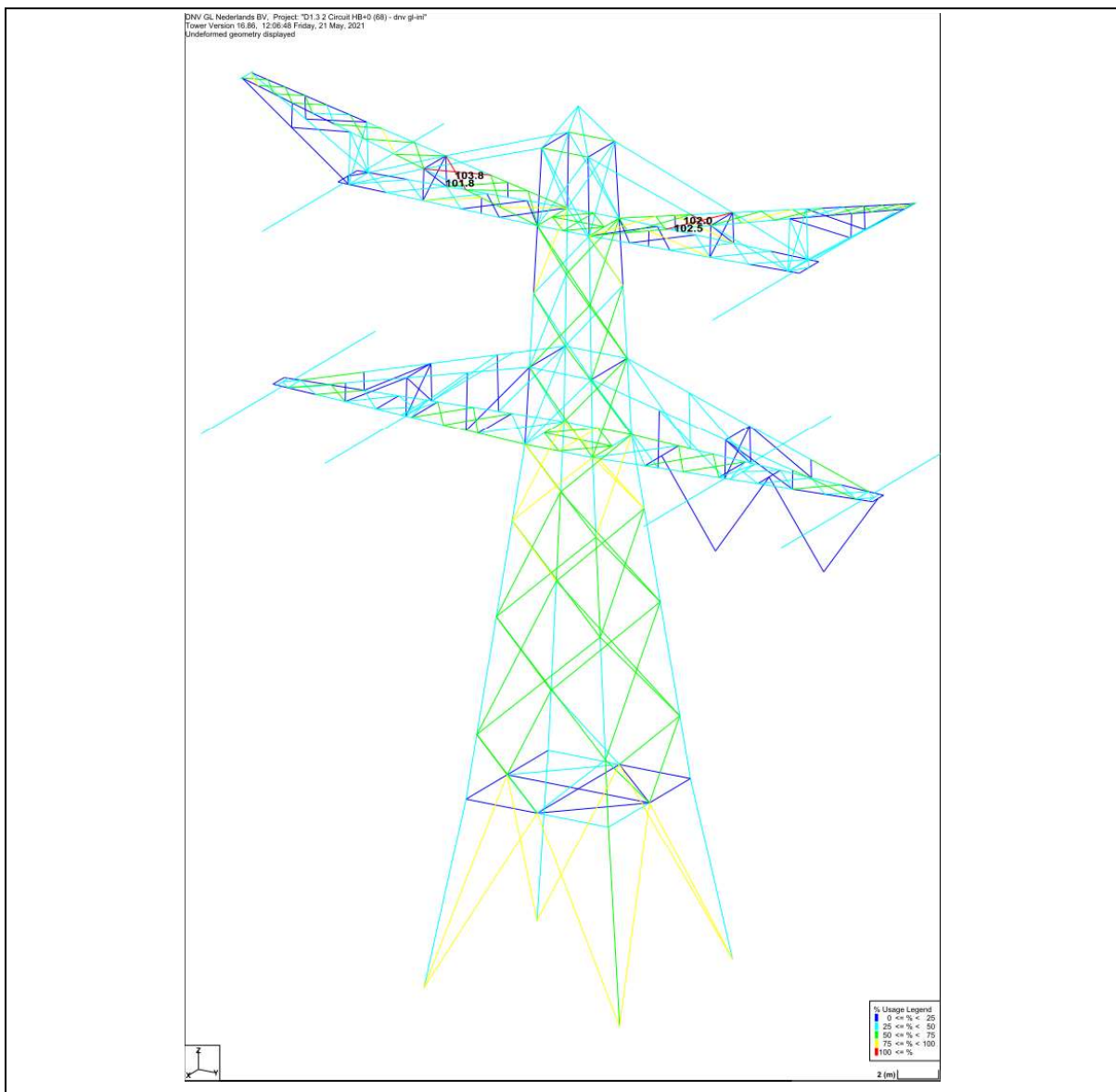
In PLS-TOWER zijn niet alle elementen getoetst. Knikverkortersprofielen en overige profielen voor beloopbaarheid worden separaat getoetst. In Appendix C is dit opgenomen. De verbinding met de fundatie bestaat uit ingestorte profielen voorzien van blokdeuvels. Dit is in Appendix D opgenomen.

## 4 TOETSING

### 4.1 Resultaat PLS-TOWER

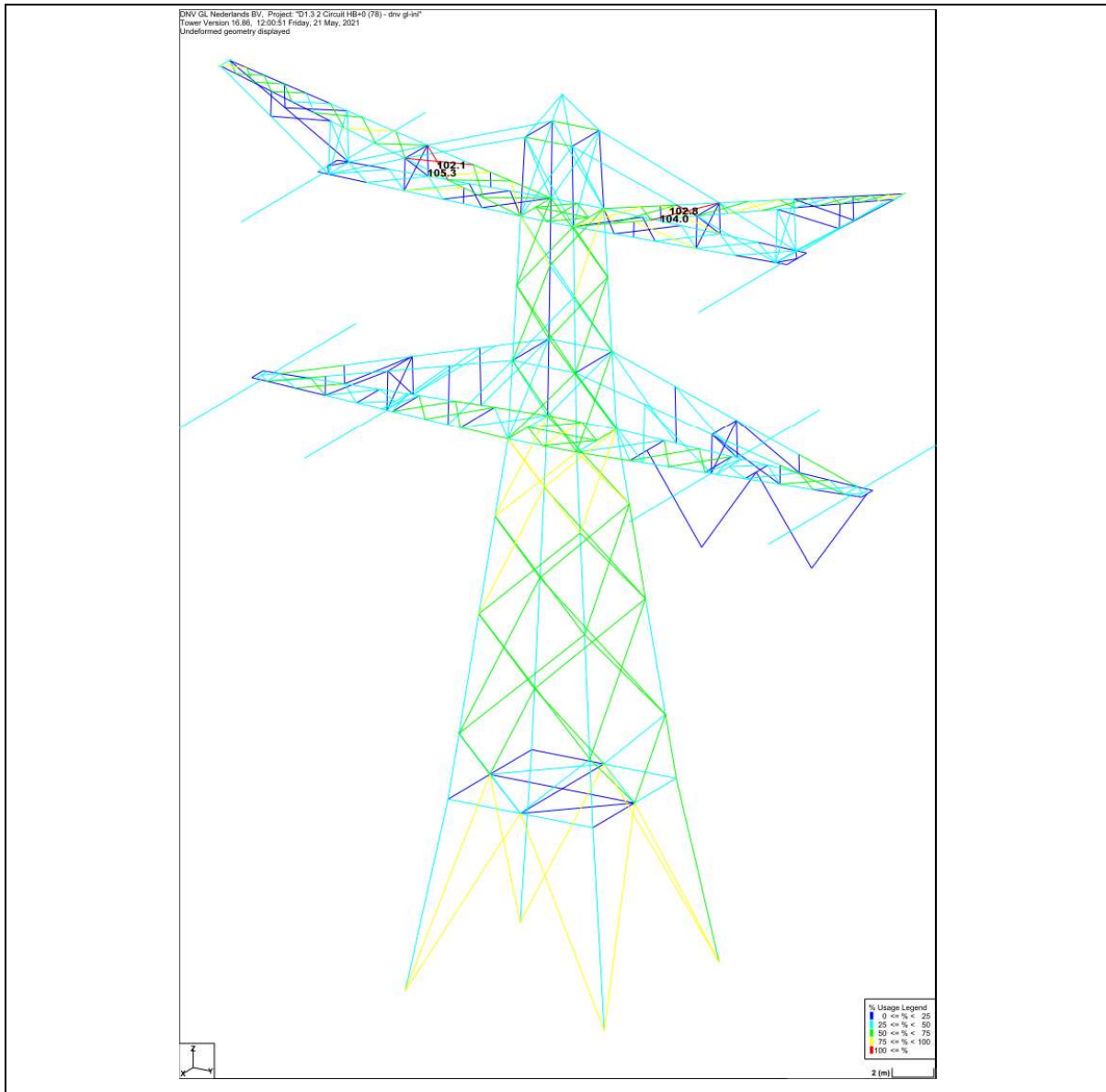
Het resultaat van de toetsing met PLS-TOWER is per masttype weergegeven in Figuur 2 tot en met Figuur 5. Voor elk masttype zijn de belastingen apart bepaald. De bestaande masten dienen in het nieuwe tracé te voldoen aan het afkeurniveau van NEN 8700 met 30 jaar referentieperiode. In dit DO is een mechanische toetsing uitgevoerd op de masten die in de toekomstige situatie de overgang zullen vormen van het bestaande tracé naar het nieuwe tracé.

De uitnutting van de constructie loopt op van blauw (0-25%) tot geel (75-100%). In het verband van de boventransverse treden overschrijdingen op. Dit wordt veroorzaakt door het uitgangspunt van ijsgebied A voor bliksemgeleiders. Door uitwisseling met nieuwe profielen kunnen overschrijdingen worden opgelost.



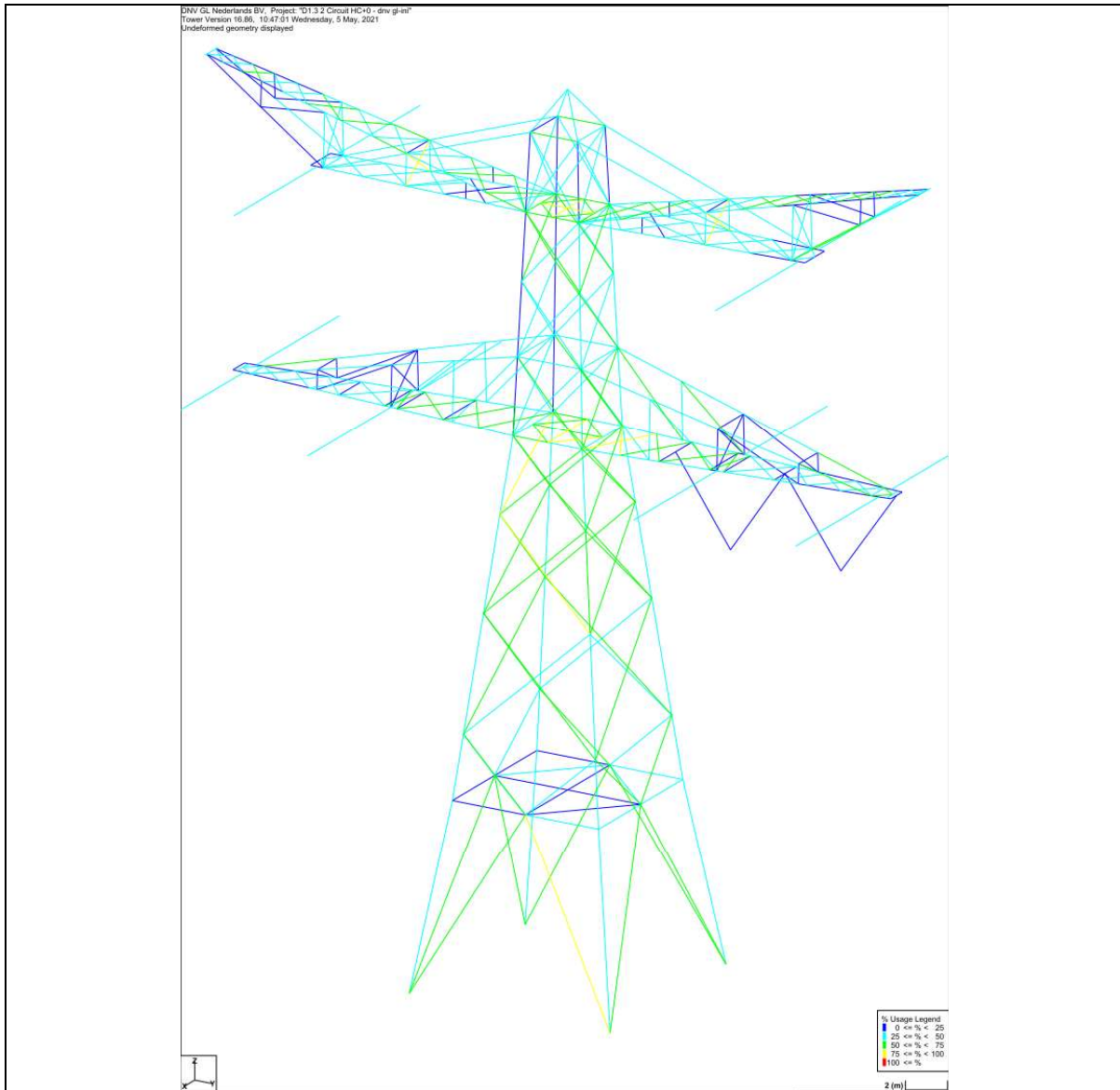
**Figuur 2 Resultaat PLS-TOWER voor masttype HB+0 (68)**

Bij mast 78 is eenzelfde overschrijding als in mast 68 aanwezig.



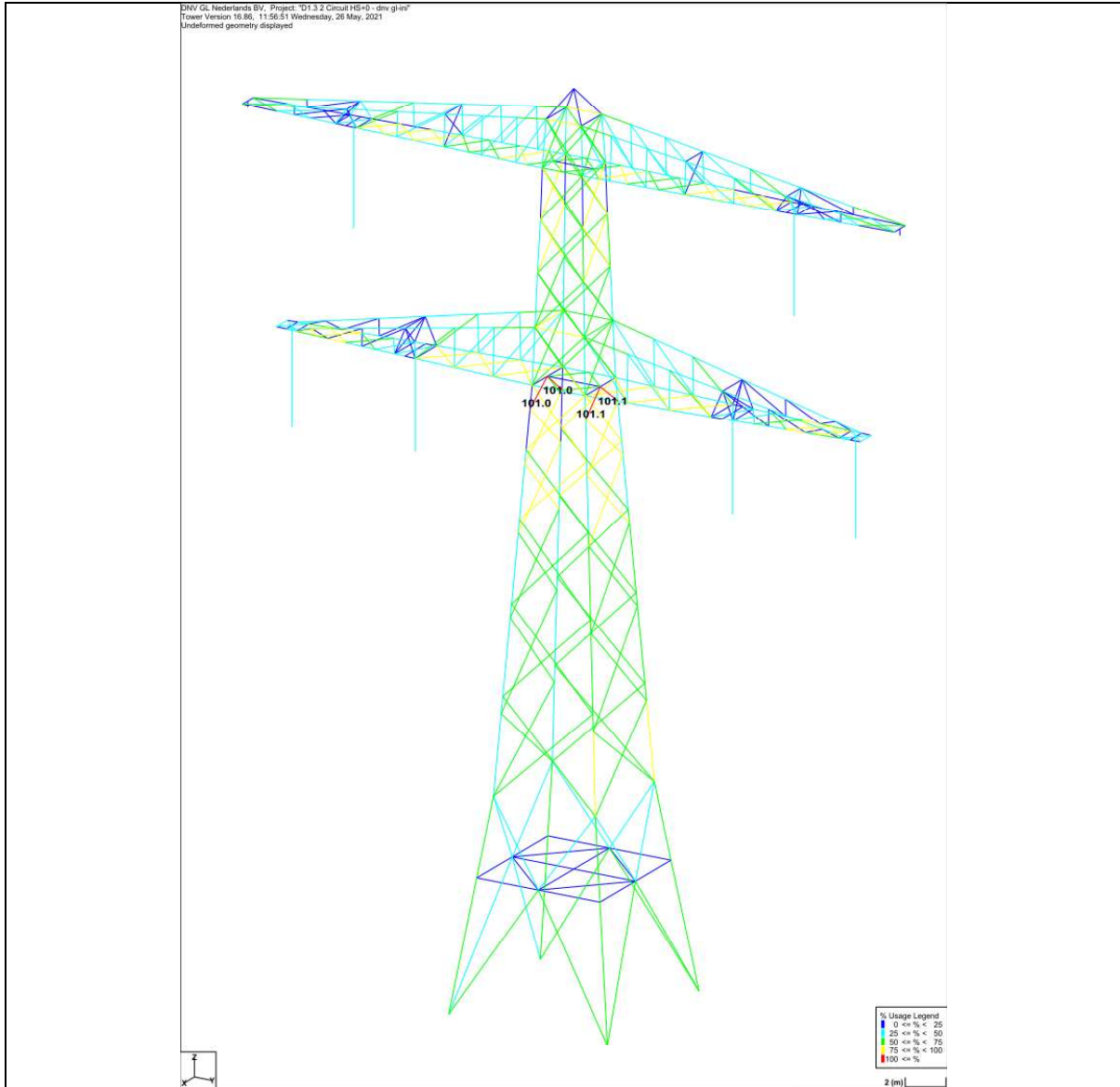
Figuur 3 Resultaat PLS-TOWER voor masttype HB+0 (78)

Bij mast 16 treden geen overschrijdingen op.



Figuur 4 Resultaat PLS-TOWER voor masttype HC+0

Bij mast 26 is een overschrijding op de sterkte van een diagonaalgroep aanwezig. Door uitwisseling met nieuwe profielen kunnen overschrijdingen worden opgelost.



**Figuur 5 Resultaat PLS-TOWER voor masttype HS+0**

## 4.2 Toetsing overige onderdelen

In Tabel 8 zijn de resultaten van de uitgevoerde toetsingen weergegeven.

**Tabel 8 Samenvatting uitgevoerde controles**

| Controle van          | Beoordeling                                  | Referentie |
|-----------------------|--|------------|
| Profielen en bouten   | Aanpassingen benodigd bij mast 68, 78 en 26. | Figuur 2   |
|                       |  | Figuur 3   |
|                       |  | Figuur 4   |
|                       |  | Figuur 5   |
|                       |  | Appendix B |
| Knikverkorters        | Aanpassingen benodigd bij mast 68, 78 en 16. | Appendix C |
| Blokdeuvels randstijl | Voldoen                                      | Appendix D |

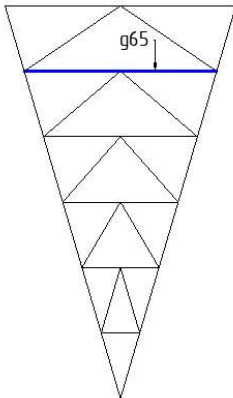
## 5 AANPASSINGEN

### 5.1 Inleiding

Een versterkingsvoorstel om de mast aan afkeurniveau te laten voldoen en nieuwe onderdelen aan verbouwniveau is uitgewerkt. Dit voorstel bevat de volgende maatregelen:

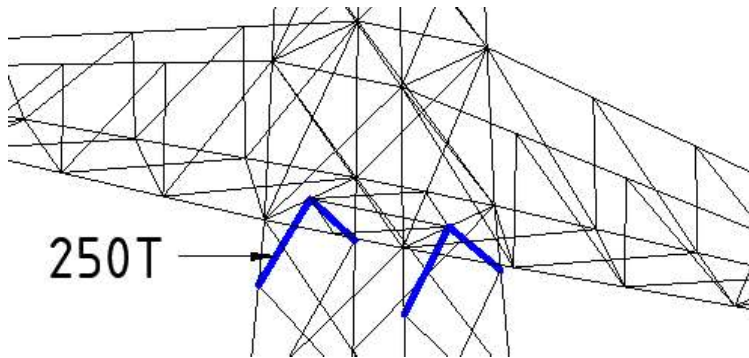
- Knikverkorters in pootverband vervangen (HC+0 en HB+0)
- Diagonalen in mastlichaam ter hoogte van onder traverse vervangen (HS+0)
- Horizontale diagonalen in boven traverse vervangen (HB+0)

### 5.2 Aanpassingen

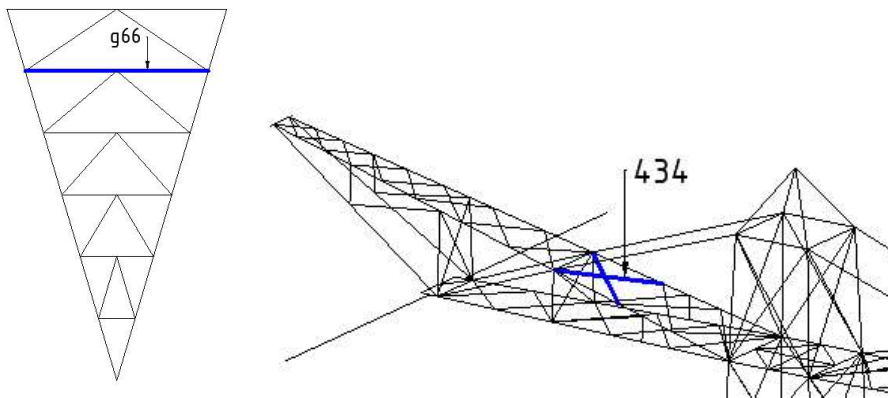


**Figuur 2 Knikverkorters in pootverband uitwisselen HC+0 (16)**





**Figuur 3** Diagonalen uitwisselen HS+0 (26)



**Figuur 4** Knikverkorter in pootverband en diagonalen in boven traverse uitwisselen HB+0 (68&78)

In Tabel 1 tot en met Tabel 3 zijn de gegevens van de toegevoegde- en uitgewisselde profielen weergegeven. De tekeningen zijn terug te vinden in Appendix E. De gewichten van de additionele bouten en platen van de versterkte verbinding zijn niet meegenomen.

**Tabel 1 Gewichten HC+0 (16) van uitgewisselde profielen**

| Staafgroep | Profiel | Materiaal | Bouten    | Profiel nw. | Materiaal nw. | Bouten nw. | Maatregel            | Aantal | Lengte (m) | Gewicht (kg) |
|------------|---------|-----------|-----------|-------------|---------------|------------|----------------------|--------|------------|--------------|
| G65        | L50x5   | S235      | 1M16-8.8t | L70x7       | S355          | 1M16-8.8t  | Profiel uitgewisseld | 4      | 4.63       | 139.21       |
|            |         |           |           |             |               |            |                      |        | 18.51      | 139.21       |

**Tabel 2 Gewichten HS+0 (26) van uitgewisselde profielen**

| Staafgroep | Profiel  | Materiaal | Bouten    | Profiel nw. | Materiaal nw. | Bouten nw. | Maatregel            | Aantal | Lengte (m) | Gewicht (kg) |
|------------|----------|-----------|-----------|-------------|---------------|------------|----------------------|--------|------------|--------------|
| 250T       | L80x65x6 | S235      | 3M20-8.8t | L70x7       | S355          | 3M20-8.8t  | Profiel uitgewisseld | 4      | 2.00       | 60.19        |
|            |          |           |           |             |               |            |                      |        | 8.00       | 60.19        |

**Tabel 3 Gewichten HB+0 (68&78) van uitgewisselde profielen**

| Staafgroep | Profiel | Materiaal | Bouten    | Profiel nw. | Materiaal nw. | Bouten nw. | Maatregel            | Aantal | Lengte (m) | Gewicht (kg) |
|------------|---------|-----------|-----------|-------------|---------------|------------|----------------------|--------|------------|--------------|
| G66        | L50x5   | S235      | 1M16-8.8t | L70x7       | S355          | 1M16-8.8t  | Profiel uitgewisseld | 4      | 4.63       | 139.21       |
| 434        | L55x6   | S235      | 1M16-8.8t | L55x6       | S355          | 1M16-8.8t  | Profiel uitgewisseld | 4      | 3.40       | 68.73        |
|            |         |           |           |             |               |            |                      |        | 32.13      | 207.94       |



## APPENDIX A

### Geleiderbelastingen

---

Hierin zijn de geleiderbelastingen opgenomen van de volgende masten:

- Masttype HB+0 (68)
- Masttype HB+0 (78)
- Masttype HC+0 (16)
- Masttype HS+0 (26)



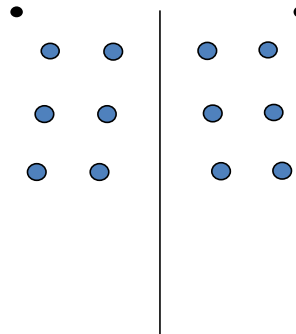
Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

Auteur: TBR  
 Versie: v11.8

### Conductor loads

#### General

Description HB+0  
 Tower type Hoekmast  
 Number of circuits 2  
 Configuration 2-circuit-donau  
 Number of earth wires 2



Configuratie geleiders

#### Starting points

Norm NEN-EN50341-2-15:2019  
 Consequence class CC2-0  
 Reliability level initial Afkeur CC2-0  
 Reference period initial 30 jaar  
 Consequence class modified CC2  
 Reliability level modified Verbouw  
 Reference period modified 50 jaar  
 Wind zone III  
 Wind speed (m/s) 24.5 m/s  
 Terrain category II  
 Reduction factor  $c_{dir}$  1.00  
 Ice region phase conductor B  
 Ice region earth conductor A

#### Conductors back

| Description    | Voltage | Conductor Back        | Bundle Ba | Ice region | Additional weight | Additional diameter | Catenary $P_{back}$ |
|----------------|---------|-----------------------|-----------|------------|-------------------|---------------------|---------------------|
| Circuit 1      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                |
| Circuit 2      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 1 |         | ACSR-26/7-242/39-HAWK | 1         | A          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 2 |         | OPGW 226              | 1         | A          | 2 %               | 2 %                 | 1375                |

#### Conductors ahead

| Description    | Voltage | Conductor Ahead        | Bundle Ah | Ice region | Additional weight | Additional diameter | Catenary $P_{ahead}$ |
|----------------|---------|------------------------|-----------|------------|-------------------|---------------------|----------------------|
| Circuit 1      | 380 kV  | ACCC-Warsaw            | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Circuit 2      | 380 kV  | ACCC-Warsaw            | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 1 |         | AACSR 241-AL3-39-A20SA | 1         | A          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 2 |         | OPGW AFL-226/38        | 1         | A          | 2 %               | 2 %                 | 1375                 |

#### Insulators (1)

| Description    | Suspension    | Weight [kN] | Length [m] | Wind area [m <sup>2</sup> ] |
|----------------|---------------|-------------|------------|-----------------------------|
| Circuit 1      | Afspanketting | 6.00        | 7.90       | 2.00                        |
| Circuit 2      | Afspanketting | 6.00        | 7.90       | 2.00                        |
| Bliksemdraad 1 | Afspanketting | 0.10        | 0.20       | 0.10                        |
| Bliksemdraad 2 | Afspanketting | 0.10        | 0.20       | 0.10                        |

1. Properties apply to the entire isolator set

#### Suspension height and position in mast

| Circuits       | Designation | Number   | Suspension height | Attach point | Position in tower Horizontal distance |
|----------------|-------------|----------|-------------------|--------------|---------------------------------------|
| Circuit 1      | 10          | 380ct1f1 | 27.7 m            | 27.7 m       | -16.3 m                               |
| Circuit 1      | 11          | 380ct1f2 | 27.7 m            | 27.7 m       | -9.0 m                                |
| Circuit 1      | 12          | 380ct1f3 | 39.0 m            | 39.0 m       | -12.7 m                               |
| Circuit 2      | 20          | 380ct2f1 | 27.7 m            | 27.7 m       | 9.0 m                                 |
| Circuit 2      | 21          | 380ct2f2 | 27.7 m            | 27.7 m       | 16.3 m                                |
| Circuit 2      | 22          | 380ct2f3 | 39.0 m            | 39.0 m       | 12.7 m                                |
| Bliksemdraad 1 | 1           | bl1      | 43.2 m            | 43.2 m       | -18.7 m                               |
| Bliksemdraad 2 | 3           | bl2      | 43.2 m            | 43.2 m       | 18.7 m                                |

Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

**Height adjustment adjacent masts** (wind and weight span adjustment)

|                                     | Back  | Ahead |  |
|-------------------------------------|-------|-------|--|
| Height increase for wind pressure   | 0.0 m | 0.0 m | (positive: higher)                     |
| Height decrease for vertical load   | 0.0 m | 0.0 m | (negative: decrease, more weight span) |
| Decrease: Niet in 0,9EG-combinaties |       |       |  |

**Height difference adjacent tower and change of direction with respect to Line direction**

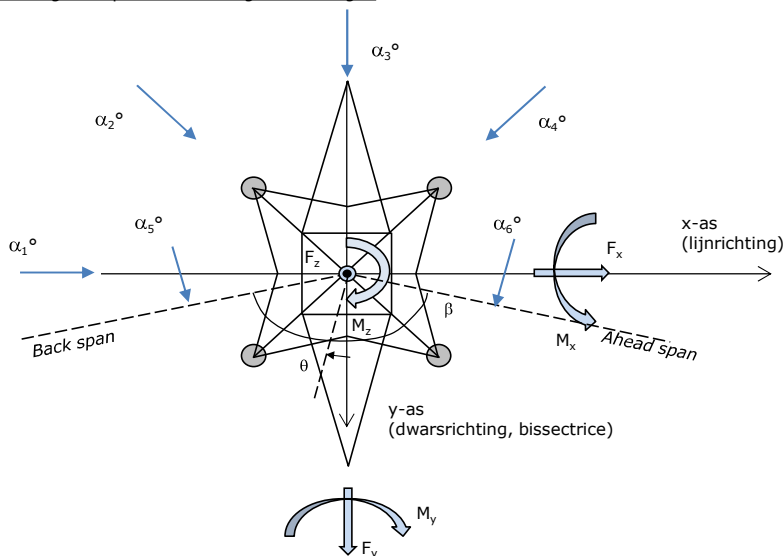
| Circuits       | Aanduiding | Nummer   | Hoogteverschil    |                    | Richtingsverandering |                    |
|----------------|------------|----------|-------------------|--------------------|----------------------|--------------------|
|                |            |          | $\Delta h_{back}$ | $\Delta h_{ahead}$ | $\Delta y_{back}$    | $\Delta y_{ahead}$ |
| Circuit 1      | 10         | 380ct1f1 | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 11         | 380ct1f2 | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 12         | 380ct1f3 | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 20         | 380ct2f1 | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 21         | 380ct2f2 | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 22         | 380ct2f3 | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 1 | 1          | bl1      | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 2 | 3          | bl2      | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |

**Line and tower data**

|  | Back           | Ahead           |
|--|----------------|-----------------|
| Ruling span $\sqrt{(\Sigma L^3 / \Sigma L)}$ | 396.5          | 348.8 m         |
| Line angle                                   | 385.2          | 348.8 m         |
| Tower orientation with respect to bis0       | $179.95^\circ$ |                 |
| Section length                               | 2305           | 349 m           |
| Height bottom of tower to ground level       | 0.5 m          |                 |
| Wind directions considered                   | $\alpha_1$     | $0^\circ$       |
| Wind directions according to:                | $\alpha_2$     | $45^\circ$      |
| <i>Geleiderbelastingen</i>                   | $\alpha_3$     | $90^\circ$      |
|  | $\alpha_4$     | $135^\circ$     |
|  | $\alpha_5$     | $105.975^\circ$ |
|  | $\alpha_6$     | $106.025^\circ$ |

Wind directions apply to the main direction of mast construction, not to the bisector.

Windrichtingen en positieve richtingen belastingen



Considered number of wind directions

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

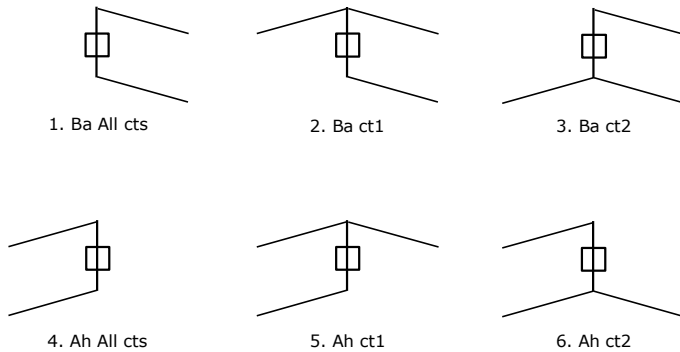
**Absence of conductors**

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | b2       | 0             | 1    | 1                        | 0    | 1                  | 0    |

**Load situations SPLS**

Considered situations SPLS: 1 up to 6, All possible situations

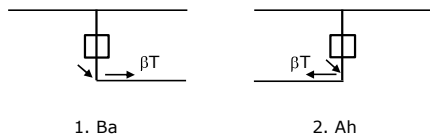
Principle of load situations:



**Load situation 5a. Conductor failure**

Considered situations conductor failure 5a: 1 and 2, all possible situations

Principle of load situations:



Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

**Load situations LC6. Construction and maintenance**

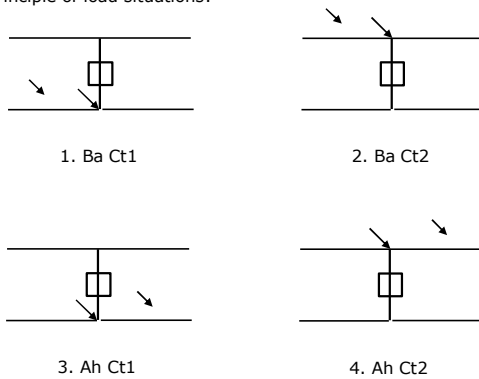
Under 6a, the load due to the presence of a line vehicle or line bicycle in combination with point load on the traverse is assessed. Combination 6b does not contain any loads in conductor or on traverse. This combination has been added to be able to combine with separate control platforms, etc. The situations are applied in ULS and in every SPLS situation (in case of angle tower).

|                             | Phase  | Earth  |
|-----------------------------|--------|--------|
| Line vehicle                | 4.0 kN | 2.0 kN |
| Concentrated load cross arm | 1.0 kN | 1.0 kN |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Presence line vehicle: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principle of load situations:



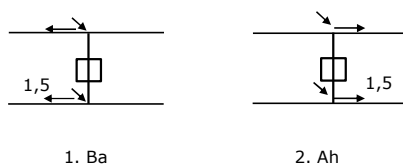
**Load situations 8. Galloping as a static load**

| Conductor                    |         |       |
|------------------------------|---------|-------|
| Suspension tower phase       | 0.866 W | 1.5 W |
| Suspension tower earth       | 1.5 EDS | 1.5 W |
| Strain tower phase and earth | 1.5 EDS | 1.5 W |

Considered situations galloping 8: None (existing structure)

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principle of load situations:



**Load combination 8. Galloping as a dynamic load**

Only applies to tension towers  
 Load consists of EDS tensile load in one of the conductors on one side of the tower  
 Can be converted by user to fatigue spectrum via the load spectrum of table 4.11 / NL.1

Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

### Tower structure

#### Properties

|                                      |             |               |
|--------------------------------------|-------------|---------------|
| Tower type                           | Hoekmast    |               |
| Tower designation                    | HB+0        |               |
| Base plate w.r.t. ground level       | 0.5 m       |               |
| Tower height w.r.t. base plate       | 48.5 m      |               |
| Tower self weight                    | 450.0 kN    |               |
| <i>Width and slope at foundation</i> |             |               |
| Leg spread                           | x-ri. 11.00 | y-ri. 11.00 m |
| Inclination of main leg              | 0.156       | 0.156 -       |
| Horizontal force factor              | 1.3         | 1.3 -         |

#### Calculation Wind load

|  |                                       |
|--|---------------------------------------|
| Dynamic factor $G_T$   | 1.00 ( <i>Masthoogte &lt; 60 m</i> )  |
| Wind load diagonally to tower body proportional to:            | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Wind load diagonally on traverse proportional to:              | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Magnification factor diagonal wind to tower body               | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor diagonal wind to cross arm                | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor wind parallel to perpendicular to cross a | 0.4                                   |

#### Properties mast sections longitudinal direction (front view, yz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 9.60     | 11.00                 | 8.00                  | 9.60      | 0.156                 | 91.20                               | 7.50                                | 0.08                                      | 3.50           |
| Eerste tussenstuk | 18.90    | 8.00                  | 5.84                  | 9.30      | 0.116                 | 64.36                               | 7.88                                | 0.12                                      | 3.29           |
| Tweede tussenstuk | 27.70    | 5.84                  | 3.78                  | 8.80      | 0.117                 | 42.33                               | 8.02                                | 0.19                                      | 2.98           |
| Bovenstuk 1       | 35.50    | 3.78                  | 3.18                  | 7.80      | 0.038                 | 27.14                               | 5.89                                | 0.22                                      | 2.86           |
| Bovenstuk 2       | 43.00    | 3.18                  | 2.60                  | 7.50      | 0.039                 | 21.68                               | 5.48                                | 0.25                                      | 2.71           |
| Topstuk           | 45.00    | 2.60                  |                       | 2.00      |                       | 2.60                                | 0.50                                | 0.19                                      | 2.96           |
| Ondertraverse     | 27.70    | 14.46                 |                       | 4.00      |                       | 28.92                               | 5.94                                | 0.21                                      | 2.91           |
| Boventraverse     | 39.00    | 17.19                 |                       | 4.20      |                       | 36.10                               | 7.84                                | 0.22                                      | 2.86           |

#### Properties tower sections transversal direction (side view, xz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 9.60     | 11.00                 | 8.00                  | 9.60      | 0.156                 | 91.20                               | 7.50                                | 0.08                                      | 3.50           |
| Eerste tussenstuk | 18.90    | 8.00                  | 5.84                  | 9.30      | 0.116                 | 64.36                               | 7.88                                | 0.12                                      | 3.29           |
| Tweede tussenstuk | 27.70    | 5.84                  | 3.78                  | 8.80      | 0.117                 | 42.33                               | 8.02                                | 0.19                                      | 2.98           |
| Bovenstuk 1       | 35.50    | 3.78                  | 3.18                  | 7.80      | 0.038                 | 27.14                               | 5.89                                | 0.22                                      | 2.86           |
| Bovenstuk 2       | 43.00    | 3.18                  | 2.60                  | 7.50      | 0.039                 | 21.68                               | 5.48                                | 0.25                                      | 2.71           |
| Topstuk           | 45.00    | 2.60                  |                       | 2.00      |                       | 2.60                                | 0.50                                | 0.19                                      | 2.96           |
| Ondertraverse     | 27.70    | 14.46                 |                       | 4.00      |                       | 28.92                               | 5.94                                | 0.21                                      | 2.91           |
| Boventraverse     | 39.00    | 17.19                 |                       | 4.20      |                       | 36.10                               | 7.84                                | 0.22                                      | 2.86           |

Note: Surface transverse direction is reduced in calculation.



Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

#### Wind surface feeders telecom installations

| Part              | A (m <sup>2</sup> /m) | Factor | Δh | A <sub>1</sub> |
|-------------------|-----------------------|--------|----|----------------|
| Broekstuk         |                       |        |    |                |
| Eerste tussenstuk |                       |        |    |                |
| Tweede tussenstuk |                       |        |    |                |
| Bovenstuk 1       |                       |        |    |                |
| Bovenstuk 2       |                       |        |    |                |

#### Input antennas

| Description  | A (m <sup>2</sup> ) | h (m) | C <sub>r</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. |                     |       |                    |

#### Tower section loads longitudinal (x-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 18.4                    | 15.6                    | 0.0                     | -15.6                   | 4.8                    | 88.3                     | 74.9                     | 0.0                      | -74.9                    |
| Eerste tussenstuk | 0.79                                   | 20.5                    | 17.4                    | 0.0                     | -17.4                   | 14.3                   | 291.8                    | 247.6                    | 0.0                      | -247.6                   |
| Tweede tussenstuk | 0.92                                   | 21.9                    | 18.6                    | 0.0                     | -18.6                   | 23.3                   | 511.3                    | 433.8                    | 0.0                      | -433.8                   |
| Bovenstuk 1       | 1.01                                   | 17.0                    | 14.4                    | 0.0                     | -14.4                   | 31.6                   | 535.8                    | 454.6                    | 0.0                      | -454.6                   |
| Bovenstuk 2       | 1.06                                   | 15.8                    | 13.4                    | 0.0                     | -13.4                   | 39.3                   | 620.8                    | 526.7                    | 0.0                      | -526.7                   |
| Topstuk           | 1.10                                   | 1.6                     | 1.4                     | 0.0                     | -1.4                    | 44.0                   | 71.6                     | 60.8                     | 0.0                      | -60.8                    |
| Ondertraverse     | 0.98                                   | 33.8                    | 20.1                    | 0.0                     | -20.1                   | 29.0                   | 982.3                    | 583.4                    | 0.0                      | -583.4                   |
| Boventraverse     | 1.07                                   | 48.1                    | 28.6                    | 0.0                     | -28.6                   | 40.4                   | 1942.6                   | 1153.8                   | 0.0                      | -1153.8                  |
| <b>Totaal</b>     |  | <b>177.1</b>            | <b>129.5</b>            | <b>0.0</b>              | <b>-129.5</b>           |                        | <b>5044.3</b>            | <b>3535.7</b>            | <b>0.0</b>               | <b>-3535.7</b>           |

#### Tower section loads transversal (y-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 0.0                     | 15.6                    | 18.4                    | 15.6                    | 4.8                    | 0.0                      | 74.9                     | 88.3                     | 74.9                     |
| Eerste tussenstuk | 0.79                                   | 0.0                     | 17.4                    | 20.5                    | 17.4                    | 14.3                   | 0.0                      | 247.6                    | 291.8                    | 247.6                    |
| Tweede tussenstuk | 0.92                                   | 0.0                     | 18.6                    | 21.9                    | 18.6                    | 23.3                   | 0.0                      | 433.8                    | 511.3                    | 433.8                    |
| Bovenstuk 1       | 1.01                                   | 0.0                     | 14.4                    | 17.0                    | 14.4                    | 31.6                   | 0.0                      | 454.6                    | 535.8                    | 454.6                    |
| Bovenstuk 2       | 1.06                                   | 0.0                     | 13.4                    | 15.8                    | 13.4                    | 39.3                   | 0.0                      | 526.7                    | 620.8                    | 526.7                    |
| Topstuk           | 1.10                                   | 0.0                     | 1.4                     | 1.6                     | 1.4                     | 44.0                   | 0.0                      | 60.8                     | 71.6                     | 60.8                     |
| Ondertraverse     | 0.98                                   | 0.0                     | 20.1                    | 13.5                    | 20.1                    | 29.0                   | 0.0                      | 583.4                    | 392.9                    | 583.4                    |
| Boventraverse     | 1.07                                   | 0.0                     | 28.6                    | 19.2                    | 28.6                    | 40.4                   | 0.0                      | 1153.8                   | 777.0                    | 1153.8                   |
| <b>Total</b>      |  | <b>0.0</b>              | <b>129.5</b>            | <b>128.0</b>            | <b>129.5</b>            |                        | <b>0.0</b>               | <b>3535.7</b>            | <b>3289.5</b>            | <b>3535.7</b>            |

#### Resulting loads from mast construction incl. Antenna without conductors level foundation (char. Value)

| Load / wind direction | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|-----------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting  | 0                      | 0                      | 450                    | 0                       | 0                       | 0                       |
| Windrichting 0°       | 177                    | 0                      | 0                      | 0                       | 5044                    | 0                       |
| Windrichting 45°      | 129                    | 129                    | 0                      | 3536                    | 3536                    | 0                       |
| Windrichting 90°      | 0                      | 128                    | 0                      | 3289                    | 0                       | 0                       |
| Windrichting 135°     | -129                   | 129                    | 0                      | 3536                    | -3536                   | 0                       |

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### Intermediate results for conductor loads

#### Conductors back

| Circuit        | Geleider              | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|-----------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Circuit 2      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Bliksemdraad 1 | ACSR-26/7-242/39-HAWK | 21.8             | 281.1                   | 9.81       | 75000                     | 1.89E-05          |
| Bliksemdraad 2 | OPGW 226              | 21.7             | 264.0                   | 9.80       | 81000                     | 2.30E-05          |

#### Conductors ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27.7             | 571.0                   | 14.98      | 62700                     | 1.88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27.7             | 571.0                   | 14.98      | 62700                     | 1.88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21.8             | 281.0                   | 9.38       | 70165                     | 1.97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21.7             | 264.0                   | 9.13       | 72000                     | 1.98E-05          |

#### Vertical load back

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Circuit 2      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Bliksemdraad 1 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Vertical load ahead

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.8               |            | B 4+0,2d  | 9.5                  | 28.6                        |
| Circuit 2      | 3             | 2                 | 45.8               |            | B 4+0,2d  | 9.5                  | 28.6                        |
| Bliksemdraad 1 | 1             | 2                 | 9.6                |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 9.3                |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Insulators

| Conductor | $G_{isolator}$<br>[kN] | Number | $F_{v,iso}$<br>[kN] | Length<br>[m] | Wind surf.<br>[m <sup>2</sup> ] | Wind heigth<br>[m] | Pressure<br>[kN/m <sup>2</sup> ] | Drag factor<br>[-] | $F_{h,iso}$<br>[kN] |
|-----------|------------------------|--------|---------------------|---------------|---------------------------------|--------------------|----------------------------------|--------------------|---------------------|
| 380ct1f1  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct1f2  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct1f3  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 39.50              | 1.07                             | 1.2                | 2.56                |
| 380ct2f1  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct2f2  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct2f3  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 39.50              | 1.07                             | 1.2                | 2.56                |
| bl1       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 43.70              | 1.10                             | 1.2                | 0.13                |
| bl2       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 43.70              | 1.10                             | 1.2                | 0.13                |

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#### Wind load back

| Conductor | Height |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{additional}$ | $w_y$ | $w_{y,section}$ | $D_{ijs,additional}$ | $w_{y,ijs}$ | $w_{y,ijs,section}$ |
|-----------|--------|----------------------|----------------|---------------|-------|------------------|-------|-----------------|----------------------|-------------|---------------------|
|           | wind   | Pressure             |                |               |       |                  |       |                 |                      |             |                     |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]             | [N/m] | [N/m]           | [mm]                 | [N/m]       | [N/m]               |
| 380ct1f1  | 18.7   | 0.86                 | 0.54           | 0.48          | 1.13  | 28.50            | 45.3  | 40.0            | 47.2                 | 79.5        | 70.2                |
| 380ct1f2  | 18.7   | 0.86                 | 0.54           | 0.48          | 1.13  | 28.50            | 45.3  | 40.0            | 47.2                 | 79.5        | 70.2                |
| 380ct1f3  | 30.0   | 0.99                 | 0.58           | 0.51          | 1.09  | 28.50            | 53.9  | 47.5            | 47.2                 | 97.7        | 86.2                |
| 380ct2f1  | 18.7   | 0.86                 | 0.54           | 0.48          | 1.13  | 28.50            | 45.3  | 40.0            | 47.2                 | 79.5        | 70.2                |
| 380ct2f2  | 18.7   | 0.86                 | 0.54           | 0.48          | 1.13  | 28.50            | 45.3  | 40.0            | 47.2                 | 79.5        | 70.2                |
| 380ct2f3  | 30.0   | 0.99                 | 0.58           | 0.51          | 1.09  | 28.50            | 53.9  | 47.5            | 47.2                 | 97.7        | 86.2                |
| bl1       | 34.2   | 1.03                 | 0.59           | 0.52          | 1.20  | 22.24            | 16.2  | 14.3            | 63.1                 | 46.1        | 40.6                |
| bl2       | 34.2   | 1.03                 | 0.59           | 0.52          | 1.20  | 22.13            | 16.1  | 14.2            | 63.0                 | 46.0        | 40.6                |

#### Wind load ahead

| Conductor | Height |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{additional}$ | $w_y$ | $w_{y,section}$ | $D_{ijs,additional}$ | $w_{y,ijs}$ | $w_{y,ijs,section}$ |
|-----------|--------|----------------------|----------------|---------------|-------|------------------|-------|-----------------|----------------------|-------------|---------------------|
|           | wind   | Pressure             |                |               |       |                  |       |                 |                      |             |                     |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]             | [N/m] | [N/m]           | [mm]                 | [N/m]       | [N/m]               |
| 380ct1f1  | 23.3   | 0.92                 | 0.56           | 0.63          | 1.12  | 28.25            | 49.0  | 54.6            | 46.9                 | 87.4        | 97.3                |
| 380ct1f2  | 23.3   | 0.92                 | 0.56           | 0.63          | 1.12  | 28.25            | 49.0  | 54.6            | 46.9                 | 87.4        | 97.3                |
| 380ct1f3  | 34.6   | 1.03                 | 0.59           | 0.66          | 1.09  | 28.25            | 56.4  | 62.7            | 46.9                 | 103.3       | 114.9               |
| 380ct2f1  | 23.3   | 0.92                 | 0.56           | 0.63          | 1.12  | 28.25            | 49.0  | 54.6            | 46.9                 | 87.4        | 97.3                |
| 380ct2f2  | 23.3   | 0.92                 | 0.56           | 0.63          | 1.12  | 28.25            | 49.0  | 54.6            | 46.9                 | 87.4        | 97.3                |
| 380ct2f3  | 34.6   | 1.03                 | 0.59           | 0.66          | 1.09  | 28.25            | 56.4  | 62.7            | 46.9                 | 103.3       | 114.9               |
| bl1       | 38.8   | 1.06                 | 0.60           | 0.67          | 1.20  | 22.24            | 17.1  | 19.0            | 63.1                 | 48.5        | 54.0                |
| bl2       | 38.8   | 1.06                 | 0.60           | 0.67          | 1.20  | 22.13            | 17.0  | 18.9            | 63.0                 | 48.4        | 53.9                |

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**Conductor loads** Auteur: TBR  
Versie: v11.8

**Starting points**  
 Consequence class Afkeur CC2-0  
 Reference period 30 jaar

| ULS (strength)  |                            | NEN-EN50341-2-15:2019 |              |                  |            |          |          |                     |
|---|----------------------------|-----------------------|--------------|------------------|------------|----------|----------|---------------------|
| Load case   | description                | Temp °C               | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|   |                            |                       | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a  | Wind                       | 10°                   | 1.05         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9  | Wind 0,9Gk only tower      | 10°                   | 0.90         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9_0,9  | Wind 0,9Gk conductors too  | 10°                   | 0.90         | 0.90             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 3   | Wind+ice                   | -5°                   | 1.05         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 3_0,9   | Wind+ice 0,9Gk             | -5°                   | 0.90         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 4   | Cold+wind                  | -20°                  | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 4_0,9   | Cold+wind 0,9Gk            | -20°                  | 0.90         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 5a  | Torsional loads            | 10°                   | 1.00         | 1.00             | 1.00       | 0.00     | 0.00     | 1.0                 |
| ULS 5b  | Longitudinal loads         | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| ULS 6   | Construction + maintenance | 5°                    | 1.05         | 1.05             | 1.20       | 0.22     | 0.00     | 0.0                 |
| ULS 6_0,9   | Construction + maintenance | 5°                    | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 7   | Permanent                  | 10°                   | 1.15         | 1.15             | 0.00       | 0.00     | 0.00     | 0.0                 |
| ULS 8   | Special                    | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| <b>SPLS (strength, for angle towers: absence of conductors)</b> |                            |                       | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
|   |                            |                       | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SPLS 1a   | Wind                       | 10°                   | 1.05         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9   | Wind 0,9                   | 10°                   | 0.90         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9_0,9   | Wind 0,9                   | 10°                   | 0.90         | 0.90             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 3  | Wind+ice                   | -5°                   | 1.05         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 3_0,9  | Wind+ice 0,9               | -5°                   | 0.90         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 4  | Cold+wind                  | -20°                  | 1.05         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 4_0,9  | Cold+wind 0,9              | -20°                  | 0.90         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 6  | Maintenance                | 5°                    | 1.05         | 1.05             | 1.2        | 0.24     | 0.0      | 0.0                 |
| SPLS 6_0,9  | Maintenance                | 5°                    | 1.05         | 1.05             | 0.0        | 0.24     | 0.0      | 0.0                 |
| <b>SLS (deformations, fatigue, EDS)</b>                         |                            |                       | $G_k$        |                  | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SLS 1a  | Wind                       | 10°                   | 1.00         | 1.00             | 0.0        | 0.94     | 0.0      | 0.0                 |
| SLS 3   | Wind+ice                   | -5°                   | 1.00         | 1.00             | 0.0        | 0.28     | 0.88     | 0.0                 |
| SLS 4   | Wind                       | -20°                  | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 6   | Maintenance                | 5°                    | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 7   | EDS, no wind               | 10°                   | 1.00         | 1.00             | 0.0        | 0.00     | 0.0      | 0.0                 |

Number of wind directions 6  
 Number of load combinations for ULS 54  
 Number of load combinations for SPLS 222  
 Number of load combinations for SLS 15  
 Number of concentrated loads 5238

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### Summary table - Conductor loads

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

#### Maximum values for back and ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -41.4         | 39.8          | 0.1           | 14.4          | 6.6           | 5.2           |
| 380ct1f1    | -103.7        | 104.3         | 1.7           | 39.4          | 21.9          | 19.3          |
| 380ct1f2    | -103.7        | 104.3         | 1.7           | 39.4          | 21.9          | 19.3          |
| 380ct1f3    | -105.9        | 106.8         | 1.7           | 43.0          | 21.9          | 19.2          |
| 380ct2f1    | -103.7        | 104.3         | 1.7           | 39.4          | 21.9          | 19.3          |
| 380ct2f2    | -103.7        | 104.3         | 1.7           | 39.4          | 21.9          | 19.3          |
| 380ct2f3    | -105.9        | 106.8         | 1.7           | 43.0          | 21.9          | 19.2          |
| bl2         | -41.7         | 39.3          | 0.1           | 14.3          | 6.6           | 5.1           |
| V-ketting 1 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |
| V-ketting 2 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 334.9  | 349.6 | 352.9 |
| 380ct1f1    | 344.3  | 350.4 | 352.9 |
| 380ct1f2    | 344.3  | 350.4 | 352.9 |
| 380ct1f3    | 342.2  | 350.3 | 352.9 |
| 380ct2f1    | 344.3  | 350.4 | 352.9 |
| 380ct2f2    | 344.3  | 350.4 | 352.9 |
| 380ct2f3    | 342.2  | 350.3 | 352.9 |
| bl2         | 334.3  | 349.6 | 352.9 |
| V-ketting 1 |        |       |       |
| V-ketting 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 352.8  | 355.7 |
| 380ct1f1    | 353.0  | 353.2 |
| 380ct1f2    | 353.0  | 353.2 |
| 380ct1f3    | 352.9  | 353.2 |
| 380ct2f1    | 353.0  | 353.2 |
| 380ct2f2    | 353.0  | 353.2 |
| 380ct2f3    | 352.9  | 353.2 |
| bl2         | 352.8  | 355.8 |
| V-ketting 1 |        |       |
| V-ketting 2 |        |       |

#### Envelop of weight span over all combinations (incl. 0,9 combinations)

| For all conductors | Wind / Weight span ratio |
|--------------------|--------------------------|
| Max. weight span   | 355.8 m<br>0.955 -       |
| Min. weight span   | 325.6 m<br>0.874 -       |

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**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba  | Ft_ah |
|-------------|------|------|------|--------|-------|
|             | [kN] | [kN] | [kN] | [kN]   | [kN]  |
| bl1         | 28.2 | 9.2  | 6.6  | -42.2  | 42.3  |
| 380ct1f1    | 96.1 | 33.4 | 21.9 | -106.1 | 110.3 |
| 380ct1f2    | 96.1 | 33.4 | 21.9 | -106.1 | 110.3 |
| 380ct1f3    | 96.3 | 35.8 | 21.9 | -108.1 | 113.1 |
| 380ct2f1    | 96.1 | 33.4 | 21.9 | -106.1 | 110.3 |
| 380ct2f2    | 96.1 | 33.4 | 21.9 | -106.1 | 110.3 |
| 380ct2f3    | 96.3 | 35.8 | 21.9 | -108.1 | 113.1 |
| bl2         | 28.3 | 9.1  | 6.6  | -42.5  | 41.7  |
| V-ketting 1 | 1.9  | 1.9  | 3.5  | 0.0    |       |
| V-ketting 2 | 1.9  | 1.9  | 3.5  | 0.0    |       |

**EDS-loads conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 12.6 | 3.6  | 2.1  | -13.8 | 13.1  |
| 380ct1f1    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct1f2    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct1f3    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct2f1    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct2f2    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct2f3    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| bl2         | 12.3 | 3.5  | 2.1  | -13.7 | 12.8  |
| V-ketting 1 | 0.0  | 0.0  | 3.0  | 0.0   |       |
| V-ketting 2 | 0.0  | 0.0  | 3.0  | 0.0   |       |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4 bl1            | 0.0   | 0.0   |
| 380ct1f1             | 0.0   | 0.0   |
| 380ct1f2             | 0.0   | 0.0   |
| 380ct1f3             | 0.0   | 0.0   |
| 380ct2f1             | 0.0   | 0.0   |
| 380ct2f2             | 0.0   | 0.0   |
| 380ct2f3             | 0.0   | 0.0   |
| bl2                  | 0.0   | 0.0   |
| V-ketting 1          | 0.0   |       |
| V-ketting 2          | 0.0   |       |

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**ULS foundation loads for LC 1 and 3, wind perpendicular to the line or bisector and EDS, from conductors**

| Combination       | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | 38            | 178           | 188           | 5889           | 1225           | -5             |
| ULS 1a_0,9_0      |             | 9             | -12           | 190           | -330           | 246            | 36             |
| ULS 1a_0,9_0,9_90 |             | 44            | 180           | 160           | 5939           | 1436           | -4             |
| ULS 3_0           |             | 3             | -6            | 266           | -144           | 36             | -2             |
| SLS 7             |             | 0             | 0             | 182           | 74             | -7             | -6             |

**ULS foundation loads, LC 1 and 3, wind perpendicular to the line or bisector and EDS, total conductors and tower**

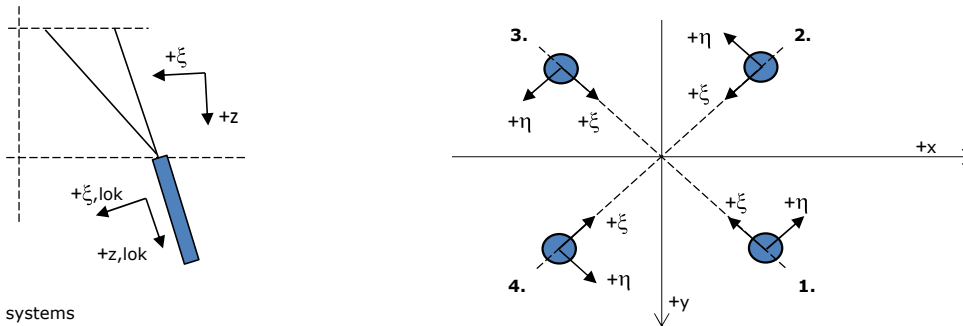
| Combination       | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | 38            | 321           | 660           | 9562           | 1225           | -5             |
| ULS 1a_0,9_0,9_90 | 44            | 323           | 565           | 9612           | 1436           | -4             |
| SLS 7             | 0             | 0             | 632           | 74             | -7             | -6             |

**Foundation loads, selection of load combinations based on greatest value**

| Combination               | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_0,9_106.025    | 6             | 344           | 565           | <b>10305</b>   | 463            | -16            |
| SPLS 3_105.975 Ba All Cts | 578           | 252           | 611           | 7973           | <b>18984</b>   | -10            |
| SPLS 6a_90 Ba Ct1 Ah Ct1  | 315           | 150           | 667           | 4923           | 10243          | <b>-4195</b>   |
| SPLS 3_105.975 Ba All Cts | 578           | 252           | 611           | <b>7973</b>    | <b>18984</b>   | -10            |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



**Maximum compression load**

| Index | Combination               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_105.975 Ba All Cts | 249           | 270           | <b>1378</b>   | -15              | -367            | -62                   | 1411                |
| 2     | SPLS 1a_0 Ba All Cts      | 133           | -162          | <b>764</b>    | 20               | -209            | -40                   | 782                 |
| 3     | SPLS 3_135 Ah All Cts     | -205          | -227          | <b>1143</b>   | -16              | -305            | -52                   | 1171                |
| 4     | SPLS 1a_135 Ah All Cts    | -178          | 204           | <b>991</b>    | 18               | -270            | -51                   | 1015                |

**Maximum tension load**

| Index | Combination                   | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|-------------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_135 Ah All Cts     | -145          | -166          | <b>-846</b>   | 15               | 220             | 33                    | -867                |
| 2     | SPLS 1a_0,9_135 Ah All Cts    | -118          | 146           | <b>-700</b>   | -19              | 187             | 32                    | -717                |
| 3     | SPLS 3_0,9_105.975 Ba All Cts | 191           | 211           | <b>-1089</b>  | 14               | 284             | 43                    | -1116               |
| 4     | SPLS 1a_0,9_0 Ba All Cts      | 77            | -103          | <b>-480</b>   | -18              | 127             | 21                    | -492                |

**Maximum torsional load (positive)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ah Ct2 | 114           | -85           | 74            | <b>141</b>       | -21             | -5                    | 76                  |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -24           | -186          | 426           | <b>149</b>       | -114            | -20                   | 436                 |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -8            | 193           | -505          | <b>142</b>       | 131             | 19                    | -517                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -10           | 213           | 583           | <b>143</b>       | -158            | -29                   | 597                 |

**Maximum torsional load (negative)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 63            | 261           | 856           | <b>-140</b>      | -229            | -40                   | 877                 |
| 2     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 60            | 144           | -238          | <b>-145</b>      | 60              | 7                     | -244                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | -30           | -228          | 682           | <b>-140</b>      | -182            | -32                   | 699                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -96           | -119          | -75           | <b>-152</b>      | 16              | -1                    | -77                 |

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#### Combination Ftensile+Fhor

| Index | Combination                   | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 6a_90 Ah All Cts Ba Ct1  | -100                   | -177                   | <b>-766</b>            | <b>55</b>              | 196                    | 27                         | -785                       |
| 2     | SPLS 1a_0,9_135 Ah Ct2        | -9                     | 166                    | <b>-455</b>            | <b>-111</b>            | 124                    | 23                         | -466                       |
| 3     | SPLS 3_0,9_105.975 Ba All Cts | 191                    | 211                    | <b>-1089</b>           | <b>14</b>              | 284                    | 43                         | -1116                      |
| 4     | SPLS 3_0,9_0 Ba All Cts       | 72                     | -104                   | <b>-475</b>            | <b>-23</b>             | 124                    | 19                         | -487                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 33                     | 32                     | 161                    | 0                      | -46                    | -10                        | 165                        |
| 2     | SLS 7       | 32                     | -32                    | 154                    | 0                      | -45                    | -11                        | 158                        |
| 3     | SLS 7       | -31                    | -32                    | 155                    | -1                     | -45                    | -11                        | 159                        |
| 4     | SLS 7       | -33                    | 32                     | 162                    | 0                      | -46                    | -10                        | 166                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination                   | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|-------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | SPLS 3_105.975 Ba All Cts     | 249                    | 270                    | <b>1378</b>            | -15                    | -367                   | -62                        | 1411                       |
| Max. tension         | SPLS 3_0,9_105.975 Ba All Cts | 191                    | 211                    | <b>-1089</b>           | 14                     | 284                    | 43                         | -1116                      |
| Max. pos. torsie     | SPLS 6a_90 Ba Ct2 Ah Ct2      | -24                    | -186                   | 426                    | <b>149</b>             | -114                   | -20                        | 436                        |
| Max. neg. torsie     | SPLS 6a_90 Ba Ct1 Ah Ct1      | -96                    | -119                   | -75                    | <b>-152</b>            | 16                     | -1                         | -77                        |
| Comb. tension+torsie | SPLS 3_0,9_105.975 Ba All Cts | 191                    | 211                    | <b>-1089</b>           | <b>14</b>              | 284                    | 43                         | -1116                      |

#### Maximum tension load - SLS

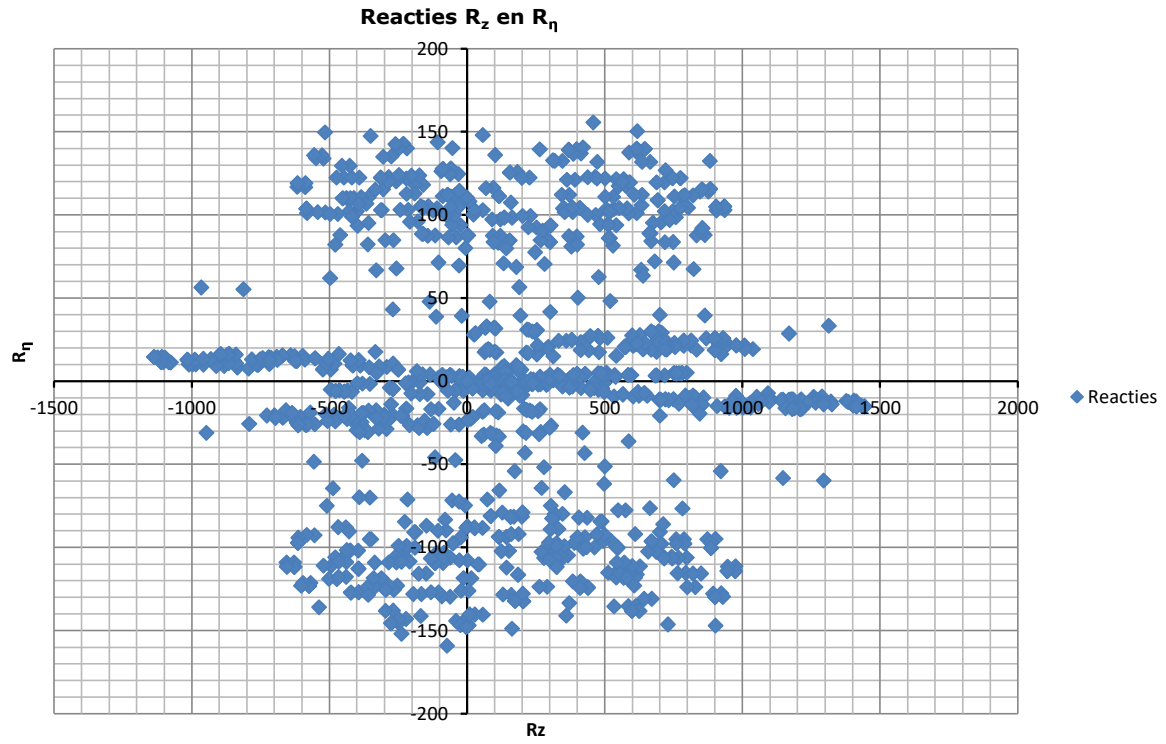
| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 33                     | 32                     | <b>161</b>             | 0                      | -46                    | -10                        | 165                        |
| 2     | SLS 1a_135  | -62                    | 55                     | <b>-303</b>            | 5                      | 83                     | 16                         | -311                       |
| 3     | SLS 1a_90   | 50                     | 45                     | <b>-253</b>            | -4                     | 67                     | 11                         | -260                       |
| 4     | SLS 1a_0    | 15                     | -16                    | <b>-80</b>             | -1                     | 21                     | 4                          | -81                        |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_90   | 114                    | 109                    | <b>568</b>             | 4                      | -157                   | -32                        | 582                        |
| 2     | SLS 1a_0    | 77                     | -81                    | <b>396</b>             | 3                      | -112                   | -25                        | 405                        |
| 3     | SLS 7       | -31                    | -32                    | <b>155</b>             | -1                     | -45                    | -11                        | 159                        |
| 4     | SLS 1a_135  | -127                   | 118                    | <b>618</b>             | -7                     | -173                   | -36                        | 633                        |



Project: GT-RL380  
Tower: HB+0  
Number: 68



Project: GT-RL380  
 Tower: HB+0  
 Number: 68

**Conductor loads** Auteur: TBR  
Versie: v11.8

**Starting points**  
 Consequence class Verbouw CC2  
 Reference period 50 jaar

| <b>ULS</b> (strength)   |                            | <b>NEN-EN50341-2-15:2019</b> |                            |                                | $\gamma_Q$                               |          |          | $\gamma_a$ |
|---|----------------------------|------------------------------|----------------------------|--------------------------------|--|----------|----------|------------|
| Load case   | description                | Temp °C                      | $\gamma_G$<br>$G_{k,mast}$ | $\gamma_G$<br>$G_{k,geleider}$ | $Q_{pk}$                                 | $Q_{wk}$ | $Q_{ik}$ | $A_k$      |
| ULS 1a  | Wind                       | 10°                          | 1.15                       | 1.15                           | 0.00                                     | 1.40     | 0.00     | 0.0        |
| ULS 1a_0,9  | Wind 0,9Gk only tower      | 10°                          | 0.90                       | 1.15                           | 0.00                                     | 1.40     | 0.00     | 0.0        |
| ULS 1a_0,9_0,9  | Wind 0,9Gk conductors too  | 10°                          | 0.90                       | 0.90                           | 0.00                                     | 1.40     | 0.00     | 0.0        |
| ULS 3   | Wind+ice                   | -5°                          | 1.15                       | 1.15                           | 0.00                                     | 0.42     | 1.30     | 0.0        |
| ULS 3_0,9   | Wind+ice 0,9Gk             | -5°                          | 0.90                       | 1.15                           | 0.00                                     | 0.42     | 1.30     | 0.0        |
| ULS 4   | Cold+wind                  | -20°                         | 1.15                       | 1.15                           | 0.00                                     | 0.28     | 0.00     | 0.0        |
| ULS 4_0,9   | Cold+wind 0,9Gk            | -20°                         | 0.90                       | 1.15                           | 0.00                                     | 0.28     | 0.00     | 0.0        |
| ULS 5a  | Torsional loads            | 10°                          | 1.00                       | 1.00                           | 1.00                                     | 0.00     | 0.00     | 1.0        |
| ULS 5b  | Longitudinal loads         | 10°                          | 1.00                       | 1.00                           | 0.00                                     | 0.00     | 0.00     | 1.0        |
| ULS 6   | Construction + maintenance | 5°                           | 1.15                       | 1.15                           | 1.30                                     | 0.28     | 0.00     | 0.0        |
| ULS 6_0,9   | Construction + maintenance | 5°                           | 1.15                       | 1.15                           | 0.00                                     | 0.28     | 0.00     | 0.0        |
| ULS 7   | Permanent                  | 10°                          | 1.30                       | 1.30                           | 0.00                                     | 0.00     | 0.00     | 0.0        |
| ULS 8   | Special                    | 10°                          | 1.00                       | 1.00                           | 0.00                                     | 0.00     | 0.00     | 1.0        |
| <b>SPLS</b> (strength, for angle towers: absence of conductors) |                            |                              | $\gamma_G$<br>$G_k$        |                                | $\gamma_Q$<br>$Q_{pk}$ $Q_{wk}$ $Q_{ik}$ |          |          | $A_k$      |
| SPLS 1a   | Wind                       | 10°                          | 1.15                       | 1.15                           | 0.0                                      | 0.78     | 0.00     | 0.0        |
| SPLS 1a_0,9   | Wind 0,9                   | 10°                          | 0.90                       | 1.15                           | 0.0                                      | 0.78     | 0.00     | 0.0        |
| SPLS 1a_0,9_0,9   | Wind 0,9                   | 10°                          | 0.90                       | 0.90                           | 0.0                                      | 0.78     | 0.00     | 0.0        |
| SPLS 3  | Wind+ice                   | -5°                          | 1.15                       | 1.15                           | 0.0                                      | 0.36     | 0.34     | 0.0        |
| SPLS 3_0,9  | Wind+ice 0,9               | -5°                          | 0.90                       | 1.15                           | 0.0                                      | 0.36     | 0.34     | 0.0        |
| SPLS 4  | Cold+wind                  | -20°                         | 1.15                       | 1.15                           | 0.0                                      | 0.24     | 0.00     | 0.0        |
| SPLS 4_0,9  | Cold+wind 0,9              | -20°                         | 0.90                       | 1.15                           | 0.0                                      | 0.24     | 0.00     | 0.0        |
| SPLS 6  | Maintenance                | 5°                           | 1.15                       | 1.15                           | 1.2                                      | 0.24     | 0.0      | 0.0        |
| SPLS 6_0,9  | Maintenance                | 5°                           | 1.15                       | 1.15                           | 0.0                                      | 0.24     | 0.0      | 0.0        |
| <b>SLS</b> (deformations, fatigue, EDS)                         |                            |                              | $G_k$                      |                                | $Q_{pk}$ $Q_{wk}$ $Q_{ik}$               |          |          | $A_k$      |
| SLS 1a  | Wind                       | 10°                          | 1.00                       | 1.00                           | 0.0                                      | 1.00     | 0.0      | 0.0        |
| SLS 3   | Wind+ice                   | -5°                          | 1.00                       | 1.00                           | 0.0                                      | 0.30     | 1.00     | 0.0        |
| SLS 4   | Wind                       | -20°                         | 1.00                       | 1.00                           | 0.0                                      | 0.20     | 0.0      | 0.0        |
| SLS 6   | Maintenance                | 5°                           | 1.00                       | 1.00                           | 0.0                                      | 0.20     | 0.0      | 0.0        |
| SLS 7   | EDS, no wind               | 10°                          | 1.00                       | 1.00                           | 0.0                                      | 0.00     | 0.0      | 0.0        |

Number of wind directions 6  
 Number of load combinations for ULS 54  
 Number of load combinations for SPLS 222  
 Number of load combinations for SLS 15  
 Number of concentrated loads 5238

Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

### Summary table - Conductor loads

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

#### Maximum values for back and ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -50.9         | 48.5          | 0.1           | 17.7          | 8.5           | 6.7           |
| 380ct1f1    | -120.5        | 121.2         | 1.7           | 47.0          | 24.7          | 21.0          |
| 380ct1f2    | -120.5        | 121.2         | 1.7           | 47.0          | 24.7          | 21.0          |
| 380ct1f3    | -123.4        | 124.3         | 1.7           | 51.5          | 24.7          | 21.0          |
| 380ct2f1    | -120.5        | 121.2         | 1.7           | 47.0          | 24.7          | 21.0          |
| 380ct2f2    | -120.5        | 121.2         | 1.7           | 47.0          | 24.7          | 21.0          |
| 380ct2f3    | -123.4        | 124.3         | 1.7           | 51.5          | 24.7          | 21.0          |
| bl2         | -51.2         | 47.8          | 0.1           | 17.5          | 8.5           | 6.7           |
| V-ketting 1 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |
| V-ketting 2 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 333.4  | 349.5 | 352.9 |
| 380ct1f1    | 343.5  | 350.3 | 352.9 |
| 380ct1f2    | 343.5  | 350.3 | 352.9 |
| 380ct1f3    | 341.2  | 350.2 | 352.9 |
| 380ct2f1    | 343.5  | 350.3 | 352.9 |
| 380ct2f2    | 343.5  | 350.3 | 352.9 |
| 380ct2f3    | 341.2  | 350.2 | 352.9 |
| bl2         | 332.8  | 349.4 | 352.9 |
| V-ketting 1 |        |       |       |
| V-ketting 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 353.0  | 356.7 |
| 380ct1f1    | 353.1  | 353.7 |
| 380ct1f2    | 353.1  | 353.7 |
| 380ct1f3    | 353.1  | 353.7 |
| 380ct2f1    | 353.1  | 353.7 |
| 380ct2f2    | 353.1  | 353.7 |
| 380ct2f3    | 353.1  | 353.7 |
| bl2         | 353.0  | 356.8 |
| V-ketting 1 |        |       |
| V-ketting 2 |        |       |

#### Envelop of weight span over all combinations (incl. 0,9 combinations)

| For all conductors | Wind / Weight span ratio |
|--------------------|--------------------------|
| Max. weight span   | 356.8 m<br>0.957 -       |
| Min. weight span   | 317.1 m<br>0.851 -       |

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**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider    | Maximum values back + ahead span |            |            | Maximum tension in conductor |               |
|-------------|----------------------------------|------------|------------|------------------------------|---------------|
|             | Fx<br>[kN]                       | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN]                | Ft_ah<br>[kN] |
| bl1         | 29.3                             | 10.2       | 8.5        | -51.8                        | 51.5          |
| 380ct1f1    | 101.0                            | 35.3       | 24.7       | -123.2                       | 128.3         |
| 380ct1f2    | 101.0                            | 35.3       | 24.7       | -123.2                       | 128.3         |
| 380ct1f3    | 101.2                            | 39.6       | 24.7       | -125.7                       | 131.8         |
| 380ct2f1    | 101.0                            | 35.3       | 24.7       | -123.2                       | 128.3         |
| 380ct2f2    | 101.0                            | 35.3       | 24.7       | -123.2                       | 128.3         |
| 380ct2f3    | 101.2                            | 39.6       | 24.7       | -125.7                       | 131.8         |
| bl2         | 29.3                             | 10.0       | 8.5        | -52.2                        | 50.8          |
| V-ketting 1 | 2.4                              | 2.4        | 3.9        | 0.0                          |               |
| V-ketting 2 | 2.4                              | 2.4        | 3.9        | 0.0                          |               |

**EDS-loads conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 12.6 | 3.6  | 2.1  | -13.8 | 13.1  |
| 380ct1f1    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct1f2    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct1f3    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct2f1    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct2f2    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| 380ct2f3    | 60.6 | 17.4 | 15.0 | -62.7 | 63.0  |
| bl2         | 12.3 | 3.5  | 2.1  | -13.7 | 12.8  |
| V-ketting 1 | 0.0  | 0.0  | 3.0  | 0.0   |       |
| V-ketting 2 | 0.0  | 0.0  | 3.0  | 0.0   |       |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4 bl1            | 0.0   | 0.0   |
| 380ct1f1             | 0.0   | 0.0   |
| 380ct1f2             | 0.0   | 0.0   |
| 380ct1f3             | 0.0   | 0.0   |
| 380ct2f1             | 0.0   | 0.0   |
| 380ct2f2             | 0.0   | 0.0   |
| 380ct2f3             | 0.0   | 0.0   |
| bl2                  | 0.0   | 0.0   |
| V-ketting 1          | 0.0   |       |
| V-ketting 2          | 0.0   |       |

Project: GT-RLL380  
 Tower: HB+0  
 Number: 68

**ULS foundation loads for LC 1 and 3, wind perpendicular to the line or bisector and EDS, from conductors**

| Combination       | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | 49            | 224           | 205           | 7383           | 1578           | -6             |
| ULS 1a_0,9_0      |             | 11            | -15           | 208           | -430           | 310            | 46             |
| ULS 1a_0,9_0,9_90 |             | 60            | 227           | 159           | 7465           | 1928           | -5             |
| ULS 3_0           |             | 2             | -8            | 311           | -207           | -3             | -1             |
| SLS 7             |             | 0             | 0             | 182           | 74             | -7             | -6             |

**ULS foundation loads, LC 1 and 3, wind perpendicular to the line or bisector and EDS, total conductors and tower**

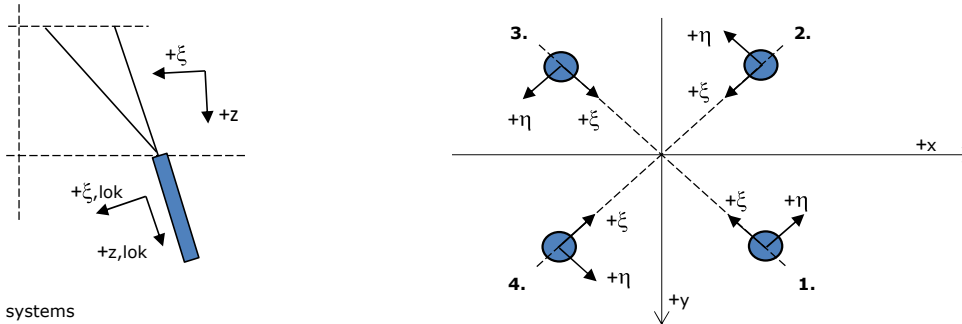
| Combination       | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | 49            | 403           | 723           | 11988          | 1578           | -6             |
| ULS 1a_0,9_0,9_90 | 60            | 406           | 564           | 12071          | 1928           | -5             |
| SLS 7             | 0             | 0             | 632           | 74             | -7             | -6             |

**Foundation loads, selection of load combinations based on greatest value**

| Combination               | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_0,9_106.025    | 10            | 433           | 563           | <b>12932</b>   | 682            | -20            |
| SPLS 3_135 Ah All Cts     | -620          | -90           | 687           | -3098          | <b>-19884</b>  | -13            |
| SPLS 6a_90 Ba Ct1 Ah Ct1  | 331           | 154           | 728           | 5108           | 10731          | <b>-4403</b>   |
| SPLS 3_105.975 Ba All Cts | 606           | 260           | 668           | <b>8229</b>    | <b>19854</b>   | -10            |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



**Maximum compression load**

| Index | Combination               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_105.975 Ba All Cts | 261           | 283           | <b>1444</b>   | -15              | -384            | -65                   | 1478                |
| 2     | SPLS 1a_0 Ba All Cts      | 142           | -172          | <b>814</b>    | 21               | -222            | -42                   | 833                 |
| 3     | SPLS 3_135 Ah All Cts     | -218          | -241          | <b>1216</b>   | -16              | -325            | -56                   | 1246                |
| 4     | SPLS 1a_135 Ah All Cts    | -186          | 213           | <b>1037</b>   | 19               | -283            | -53                   | 1062                |

**Maximum tension load**

| Index | Combination                   | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|-------------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_135 Ah All Cts     | -155          | -177          | <b>-902</b>   | 15               | 234             | 35                    | -924                |
| 2     | SPLS 1a_0,9_135 Ah All Cts    | -122          | 152           | <b>-728</b>   | -21              | 194             | 33                    | -745                |
| 3     | SPLS 3_0,9_105.975 Ba All Cts | 199           | 220           | <b>-1137</b>  | 15               | 296             | 45                    | -1165               |
| 4     | SPLS 1a_0,9_0 Ba All Cts      | 82            | -110          | <b>-513</b>   | -20              | 136             | 22                    | -525                |

**Maximum torsional load (positive)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ah Ct2 | 116           | -93           | 56            | <b>148</b>       | -16             | -4                    | 58                  |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -23           | -197          | 458           | <b>156</b>       | -123            | -22                   | 469                 |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -11           | 200           | -517          | <b>150</b>       | 134             | 20                    | -529                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -12           | 224           | 617           | <b>150</b>       | -167            | -31                   | 632                 |

**Maximum torsional load (negative)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 67            | 275           | 902           | <b>-147</b>      | -241            | -42                   | 924                 |
| 2     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 65            | 150           | -239          | <b>-152</b>      | 60              | 7                     | -244                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | -34           | -241          | 729           | <b>-146</b>      | -195            | -34                   | 747                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -102          | -124          | -74           | <b>-159</b>      | 16              | -1                    | -75                 |

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 Tower: HB+0  
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#### Combination Ftensile+Fhor

| Index | Combination                   | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 6a_90 Ah All Cts Ba Ct1  | -108                   | -186                   | <b>-813</b>            | <b>55</b>              | 208                    | 28                         | -833                       |
| 2     | SPLS 1a_0,9_135 Ah Ct2        | -6                     | 173                    | <b>-467</b>            | <b>-118</b>            | 127                    | 24                         | -478                       |
| 3     | SPLS 3_0,9_105.975 Ba All Cts | 199                    | 220                    | <b>-1137</b>           | <b>15</b>              | 296                    | 45                         | -1165                      |
| 4     | SPLS 3_0,9_0 Ba All Cts       | 77                     | -111                   | <b>-508</b>            | <b>-24</b>             | 133                    | 20                         | -520                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 33                     | 32                     | 161                    | 0                      | -46                    | -10                        | 165                        |
| 2     | SLS 7       | 32                     | -32                    | 154                    | 0                      | -45                    | -11                        | 158                        |
| 3     | SLS 7       | -31                    | -32                    | 155                    | -1                     | -45                    | -11                        | 159                        |
| 4     | SLS 7       | -33                    | 32                     | 162                    | 0                      | -46                    | -10                        | 166                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination                   | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|-------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | SPLS 3_105.975 Ba All Cts     | 261                    | 283                    | <b>1444</b>            | -15                    | -384                   | -65                        | 1478                       |
| Max. tension         | SPLS 3_0,9_105.975 Ba All Cts | 199                    | 220                    | <b>-1137</b>           | 15                     | 296                    | 45                         | -1165                      |
| Max. pos. torsie     | SPLS 6a_90 Ba Ct2 Ah Ct2      | -23                    | -197                   | 458                    | <b>156</b>             | -123                   | -22                        | 469                        |
| Max. neg. torsie     | SPLS 6a_90 Ba Ct1 Ah Ct1      | -102                   | -124                   | -74                    | <b>-159</b>            | 16                     | -1                         | -75                        |
| Comb. tension+torsie | SPLS 3_0,9_105.975 Ba All Cts | 199                    | 220                    | <b>-1137</b>           | <b>15</b>              | 296                    | 45                         | -1165                      |

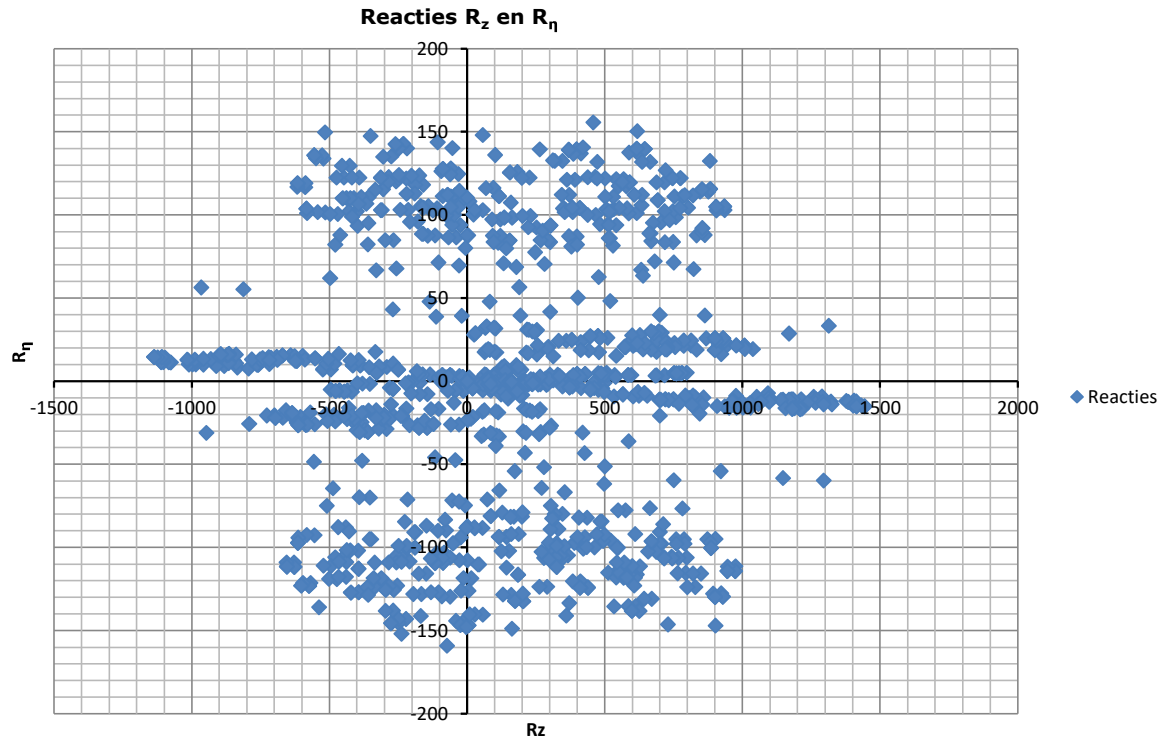
#### Maximum tension load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 33                     | 32                     | <b>161</b>             | 0                      | -46                    | -10                        | 165                        |
| 2     | SLS 1a_135  | -67                    | 60                     | <b>-329</b>            | 5                      | 90                     | 17                         | -337                       |
| 3     | SLS 1a_90   | 55                     | 50                     | <b>-281</b>            | -4                     | 74                     | 12                         | -288                       |
| 4     | SLS 1a_0    | 17                     | -18                    | <b>-94</b>             | -1                     | 25                     | 5                          | -96                        |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_90   | 119                    | 114                    | <b>595</b>             | 4                      | -165                   | -33                        | 610                        |
| 2     | SLS 1a_0    | 80                     | -84                    | <b>410</b>             | 3                      | -116                   | -26                        | 420                        |
| 3     | SLS 7       | -31                    | -32                    | <b>155</b>             | -1                     | -45                    | -11                        | 159                        |
| 4     | SLS 1a_135  | -132                   | 123                    | <b>644</b>             | -7                     | -180                   | -38                        | 660                        |

Project: GT-RL380  
Tower: HB+0  
Number: 68







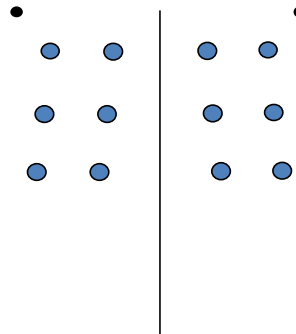
Project: GT-RLL380  
 Tower: HB+0  
 Number: 78

Auteur: TBR  
 Versie: v11.8

### Conductor loads

#### General

Description HB+0  
 Tower type Hoekmast  
 Number of circuits 2  
 Configuration 2-circuit-donau  
 Number of earth wires 2



Configuratie geleiders

#### Starting points

Norm NEN-EN50341-2-15:2019  
 Consequence class CC2-0  
 Reliability level initial Afkeur CC2-0  
 Reference period initial 30 jaar  
 Consequence class modified CC2  
 Reliability level modified Verbouw  
 Reference period modified 50 jaar  
 Wind zone III  
 Wind speed (m/s) 24.5 m/s  
 Terrain category II  
 Reduction factor  $c_{dir}$  1.00  
 Ice region phase conductor B  
 Ice region earth conductor A

#### Conductors back

| Description    | Voltage | Conductor Back         | Bundle Ba | Ice region | Additional weight | Additional diameter | Catenary $P_{back}$ |
|----------------|---------|------------------------|-----------|------------|-------------------|---------------------|---------------------|
| Circuit 1      | 380 kV  | ACCC-Warsaw            | 3         | B          | 2 %               | 2 %                 | 1375                |
| Circuit 2      | 380 kV  | ACCC-Warsaw            | 3         | B          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 1 |         | AACSR 241-AL3-39-A20SA | 1         | A          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 2 |         | OPGW AFL-226/38        | 1         | A          | 2 %               | 2 %                 | 1375                |

#### Conductors ahead

| Description    | Voltage | Conductor Ahead       | Bundle Ah | Ice region | Additional weight | Additional diameter | Catenary $P_{ahead}$ |
|----------------|---------|-----------------------|-----------|------------|-------------------|---------------------|----------------------|
| Circuit 1      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Circuit 2      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 1 |         | ACSR-26/7-242/39-HAWK | 1         | A          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 2 |         | OPGW 226              | 1         | A          | 2 %               | 2 %                 | 1375                 |

#### Insulators (1)

| Description    | Suspension    | Weight [kN] | Length [m] | Wind area [m <sup>2</sup> ] |
|----------------|---------------|-------------|------------|-----------------------------|
| Circuit 1      | Afspanketting | 6.00        | 7.90       | 2.00                        |
| Circuit 2      | Afspanketting | 6.00        | 7.90       | 2.00                        |
| Bliksemdraad 1 | Afspanketting | 0.10        | 0.20       | 0.10                        |
| Bliksemdraad 2 | Afspanketting | 0.10        | 0.20       | 0.10                        |

1. Properties apply to the entire isolator set

#### Suspension height and position in mast

| Circuits       | Designation | Number   | Suspension height | Attach point | Position in tower Horizontal distance |
|----------------|-------------|----------|-------------------|--------------|---------------------------------------|
| Circuit 1      | 10          | 380ct1f1 | 27.7 m            | 27.7 m       | -16.3 m                               |
| Circuit 1      | 11          | 380ct1f2 | 27.7 m            | 27.7 m       | -9.0 m                                |
| Circuit 1      | 12          | 380ct1f3 | 39.0 m            | 39.0 m       | -12.7 m                               |
| Circuit 2      | 20          | 380ct2f1 | 27.7 m            | 27.7 m       | 9.0 m                                 |
| Circuit 2      | 21          | 380ct2f2 | 27.7 m            | 27.7 m       | 16.3 m                                |
| Circuit 2      | 22          | 380ct2f3 | 39.0 m            | 39.0 m       | 12.7 m                                |
| Bliksemdraad 1 | 1           | bl1      | 43.2 m            | 43.2 m       | -18.7 m                               |
| Bliksemdraad 2 | 3           | bl2      | 43.2 m            | 43.2 m       | 18.7 m                                |

Project: GT-RLL380  
 Tower: HB+0  
 Number: 78

**Height adjustment adjacent masts** (wind and weight span adjustment)

|                                     | Back  | Ahead |  |
|-------------------------------------|-------|-------|--|
| Height increase for wind pressure   | 0.0 m | 0.0 m | (positive: higher)                     |
| Height decrease for vertical load   | 0.0 m | 0.0 m | (negative: decrease, more weight span) |
| Decrease: Niet in 0,9EG-combinaties |       |       |  |

**Height difference adjacent tower and change of direction with respect to Line direction**

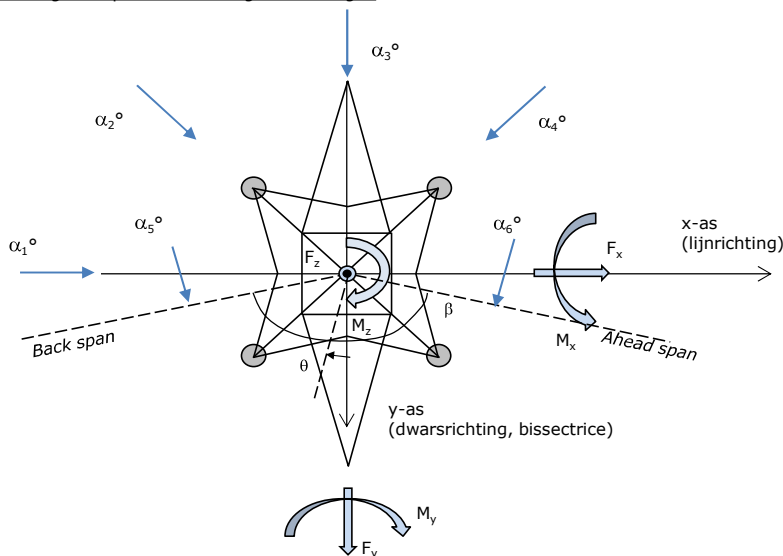
| Circuits       | Aanduiding | Nummer   | Hoogteverschil    |                    | Richtingsverandering |                    |
|----------------|------------|----------|-------------------|--------------------|----------------------|--------------------|
|                |            |          | $\Delta h_{back}$ | $\Delta h_{ahead}$ | $\Delta y_{back}$    | $\Delta y_{ahead}$ |
| Circuit 1      | 10         | 380ct1f1 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 11         | 380ct1f2 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 12         | 380ct1f3 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 20         | 380ct2f1 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 21         | 380ct2f2 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 22         | 380ct2f3 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 1 | 1          | bl1      | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 2 | 3          | bl2      | 0.0               | 5.0 m              | 0.0                  | 0.0 m              |

**Line and tower data**

|  | Back          | Ahead        |
|--|---------------|--------------|
| Ruling span $\sqrt{(\Sigma L^3 / \Sigma L)}$ | 356.7         | 398.0 m      |
| Line angle                                   | 356.7         | 387.7 m      |
| Tower orientation with respect to bis0       | $174.8^\circ$ |              |
| Section length                               | 357           | 1932 m       |
| Height bottom of tower to ground level       | 0.5 m         |              |
| Wind directions considered                   | $\alpha_1$    | $0^\circ$    |
| Wind directions according to:                | $\alpha_2$    | $45^\circ$   |
| <i>Geleiderbelastingen</i>                   | $\alpha_3$    | $90^\circ$   |
|  | $\alpha_4$    | $135^\circ$  |
|  | $\alpha_5$    | $74.4^\circ$ |
|  | $\alpha_6$    | $79.6^\circ$ |

Wind directions apply to the main direction of mast construction, not to the bisector.

Windrichtingen en positieve richtingen belastingen



**Considered number of wind directions**

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

Project: GT-RLL380  
 Tower: HB+0  
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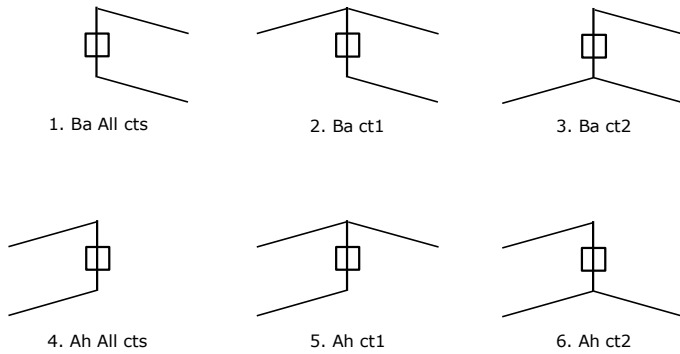
**Absence of conductors**

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | b2       | 0             | 1    | 1                        | 0    | 1                  | 0    |

**Load situations SPLS**

Considered situations SPLS: 1 up to 6, All possible situations

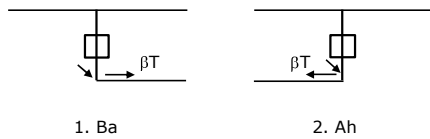
Principle of load situations:



**Load situation 5a. Conductor failure**

Considered situations conductor failure 5a: 1 and 2, all possible situations

Principle of load situations:



Project: GT-RLL380  
 Tower: HB+0  
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**Load situations LC6. Construction and maintenance**

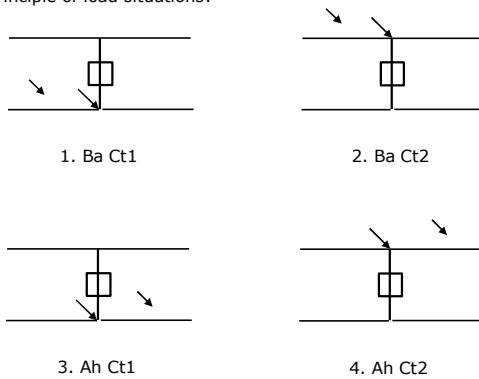
Under 6a, the load due to the presence of a line vehicle or line bicycle in combination with point load on the traverse is assessed. Combination 6b does not contain any loads in conductor or on traverse. This combination has been added to be able to combine with separate control platforms, etc. The situations are applied in ULS and in every SPLS situation (in case of angle tower).

|                             | Phase  | Earth  |
|-----------------------------|--------|--------|
| Line vehicle                | 4.0 kN | 2.0 kN |
| Concentrated load cross arm | 1.0 kN | 1.0 kN |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Presence line vehicle: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principle of load situations:



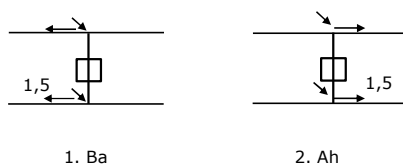
**Load situations 8. Galloping as a static load**

| Conductor                    |         |       |
|------------------------------|---------|-------|
| Suspension tower phase       | 0.866 W | 1.5 W |
| Suspension tower earth       | 1.5 EDS | 1.5 W |
| Strain tower phase and earth | 1.5 EDS | 1.5 W |

Considered situations galloping 8: None (existing structure)

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principle of load situations:



**Load combination 8. Galloping as a dynamic load**

Only applies to tension towers  
 Load consists of EDS tensile load in one of the conductors on one side of the tower  
 Can be converted by user to fatigue spectrum via the load spectrum of table 4.11 / NL.1

Project: GT-RLL380  
 Tower: HB+0  
 Number: 78

### Tower structure

#### Properties

|                                      |             |               |
|--------------------------------------|-------------|---------------|
| Tower type                           | Hoekmast    |               |
| Tower designation                    | HB+0        |               |
| Base plate w.r.t. ground level       | 0.5 m       |               |
| Tower height w.r.t. base plate       | 48.5 m      |               |
| Tower self weight                    | 450.0 kN    |               |
| <i>Width and slope at foundation</i> |             |               |
| Leg spread                           | x-ri. 11.00 | y-ri. 11.00 m |
| Inclination of main leg              | 0.156       | 0.156 -       |
| Horizontal force factor              | 1.3         | 1.3 -         |

#### Calculation Wind load

|  |                                       |
|--|---------------------------------------|
| Dynamic factor $G_T$   | 1.00 ( <i>Masthoogte &lt; 60 m</i> )  |
| Wind load diagonally to tower body proportional to:            | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Wind load diagonally on traverse proportional to:              | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Magnification factor diagonal wind to tower body               | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor diagonal wind to cross arm                | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor wind parallel to perpendicular to cross a | 0.4                                   |

#### Properties mast sections longitudinal direction (front view, yz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 9.60     | 11.00                 | 8.00                  | 9.60      | 0.156                 | 91.20                               | 7.50                                | 0.08                                      | 3.50           |
| Eerste tussenstuk | 18.90    | 8.00                  | 5.84                  | 9.30      | 0.116                 | 64.36                               | 7.88                                | 0.12                                      | 3.29           |
| Tweede tussenstuk | 27.70    | 5.84                  | 3.78                  | 8.80      | 0.117                 | 42.33                               | 8.02                                | 0.19                                      | 2.98           |
| Bovenstuk 1       | 35.50    | 3.78                  | 3.18                  | 7.80      | 0.038                 | 27.14                               | 5.89                                | 0.22                                      | 2.86           |
| Bovenstuk 2       | 43.00    | 3.18                  | 2.60                  | 7.50      | 0.039                 | 21.68                               | 5.48                                | 0.25                                      | 2.71           |
| Topstuk           | 45.00    | 2.60                  |                       | 2.00      |                       | 2.60                                | 0.50                                | 0.19                                      | 2.96           |
| Ondertraverse     | 27.70    | 14.46                 |                       | 4.00      |                       | 28.92                               | 5.94                                | 0.21                                      | 2.91           |
| Boventraverse     | 39.00    | 17.19                 |                       | 4.20      |                       | 36.10                               | 7.84                                | 0.22                                      | 2.86           |

#### Properties tower sections transversal direction (side view, xz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 9.60     | 11.00                 | 8.00                  | 9.60      | 0.156                 | 91.20                               | 7.50                                | 0.08                                      | 3.50           |
| Eerste tussenstuk | 18.90    | 8.00                  | 5.84                  | 9.30      | 0.116                 | 64.36                               | 7.88                                | 0.12                                      | 3.29           |
| Tweede tussenstuk | 27.70    | 5.84                  | 3.78                  | 8.80      | 0.117                 | 42.33                               | 8.02                                | 0.19                                      | 2.98           |
| Bovenstuk 1       | 35.50    | 3.78                  | 3.18                  | 7.80      | 0.038                 | 27.14                               | 5.89                                | 0.22                                      | 2.86           |
| Bovenstuk 2       | 43.00    | 3.18                  | 2.60                  | 7.50      | 0.039                 | 21.68                               | 5.48                                | 0.25                                      | 2.71           |
| Topstuk           | 45.00    | 2.60                  |                       | 2.00      |                       | 2.60                                | 0.50                                | 0.19                                      | 2.96           |
| Ondertraverse     | 27.70    | 14.46                 |                       | 4.00      |                       | 28.92                               | 5.94                                | 0.21                                      | 2.91           |
| Boventraverse     | 39.00    | 17.19                 |                       | 4.20      |                       | 36.10                               | 7.84                                | 0.22                                      | 2.86           |

Note: Surface transverse direction is reduced in calculation.

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#### Wind surface feeders telecom installations

| Part              | A (m <sup>2</sup> /m) | Factor | Δh | A <sub>1</sub> |
|-------------------|-----------------------|--------|----|----------------|
| Broekstuk         |                       |        |    |                |
| Eerste tussenstuk |                       |        |    |                |
| Tweede tussenstuk |                       |        |    |                |
| Bovenstuk 1       |                       |        |    |                |
| Bovenstuk 2       |                       |        |    |                |

#### Input antennas

| Description  | A (m <sup>2</sup> ) | h (m) | C <sub>r</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. |                     |       |                    |

#### Tower section loads longitudinal (x-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 18.4                    | 15.6                    | 0.0                     | -15.6                   | 4.8                    | 88.3                     | 74.9                     | 0.0                      | -74.9                    |
| Eerste tussenstuk | 0.79                                   | 20.5                    | 17.4                    | 0.0                     | -17.4                   | 14.3                   | 291.8                    | 247.6                    | 0.0                      | -247.6                   |
| Tweede tussenstuk | 0.92                                   | 21.9                    | 18.6                    | 0.0                     | -18.6                   | 23.3                   | 511.3                    | 433.8                    | 0.0                      | -433.8                   |
| Bovenstuk 1       | 1.01                                   | 17.0                    | 14.4                    | 0.0                     | -14.4                   | 31.6                   | 535.8                    | 454.6                    | 0.0                      | -454.6                   |
| Bovenstuk 2       | 1.06                                   | 15.8                    | 13.4                    | 0.0                     | -13.4                   | 39.3                   | 620.8                    | 526.7                    | 0.0                      | -526.7                   |
| Topstuk           | 1.10                                   | 1.6                     | 1.4                     | 0.0                     | -1.4                    | 44.0                   | 71.6                     | 60.8                     | 0.0                      | -60.8                    |
| Ondertraverse     | 0.98                                   | 33.8                    | 20.1                    | 0.0                     | -20.1                   | 29.0                   | 982.3                    | 583.4                    | 0.0                      | -583.4                   |
| Boventraverse     | 1.07                                   | 48.1                    | 28.6                    | 0.0                     | -28.6                   | 40.4                   | 1942.6                   | 1153.8                   | 0.0                      | -1153.8                  |
| <b>Totaal</b>     |  | <b>177.1</b>            | <b>129.5</b>            | <b>0.0</b>              | <b>-129.5</b>           |                        | <b>5044.3</b>            | <b>3535.7</b>            | <b>0.0</b>               | <b>-3535.7</b>           |

#### Tower section loads transversal (y-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 0.0                     | 15.6                    | 18.4                    | 15.6                    | 4.8                    | 0.0                      | 74.9                     | 88.3                     | 74.9                     |
| Eerste tussenstuk | 0.79                                   | 0.0                     | 17.4                    | 20.5                    | 17.4                    | 14.3                   | 0.0                      | 247.6                    | 291.8                    | 247.6                    |
| Tweede tussenstuk | 0.92                                   | 0.0                     | 18.6                    | 21.9                    | 18.6                    | 23.3                   | 0.0                      | 433.8                    | 511.3                    | 433.8                    |
| Bovenstuk 1       | 1.01                                   | 0.0                     | 14.4                    | 17.0                    | 14.4                    | 31.6                   | 0.0                      | 454.6                    | 535.8                    | 454.6                    |
| Bovenstuk 2       | 1.06                                   | 0.0                     | 13.4                    | 15.8                    | 13.4                    | 39.3                   | 0.0                      | 526.7                    | 620.8                    | 526.7                    |
| Topstuk           | 1.10                                   | 0.0                     | 1.4                     | 1.6                     | 1.4                     | 44.0                   | 0.0                      | 60.8                     | 71.6                     | 60.8                     |
| Ondertraverse     | 0.98                                   | 0.0                     | 20.1                    | 13.5                    | 20.1                    | 29.0                   | 0.0                      | 583.4                    | 392.9                    | 583.4                    |
| Boventraverse     | 1.07                                   | 0.0                     | 28.6                    | 19.2                    | 28.6                    | 40.4                   | 0.0                      | 1153.8                   | 777.0                    | 1153.8                   |
| <b>Total</b>      |  | <b>0.0</b>              | <b>129.5</b>            | <b>128.0</b>            | <b>129.5</b>            |                        | <b>0.0</b>               | <b>3535.7</b>            | <b>3289.5</b>            | <b>3535.7</b>            |

#### Resulting loads from mast construction incl. Antenna without conductors level foundation (char. Value)

| Load / wind direction | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|-----------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting  | 0                      | 0                      | 450                    | 0                       | 0                       | 0                       |
| Windrichting 0°       | 177                    | 0                      | 0                      | 0                       | 5044                    | 0                       |
| Windrichting 45°      | 129                    | 129                    | 0                      | 3536                    | 3536                    | 0                       |
| Windrichting 90°      | 0                      | 128                    | 0                      | 3289                    | 0                       | 0                       |
| Windrichting 135°     | -129                   | 129                    | 0                      | 3536                    | -3536                   | 0                       |

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### Intermediate results for conductor loads

#### Conductors back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27.7             | 571.0                   | 14.98      | 62700                     | 1.88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27.7             | 571.0                   | 14.98      | 62700                     | 1.88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21.8             | 281.0                   | 9.38       | 70165                     | 1.97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21.7             | 264.0                   | 9.13       | 72000                     | 1.98E-05          |

#### Conductors ahead

| Circuit        | Geleider              | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|-----------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Circuit 2      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Bliksemdraad 1 | ACSR-26/7-242/39-HAWK | 21.8             | 281.1                   | 9.81       | 75000                     | 1.89E-05          |
| Bliksemdraad 2 | OPGW 226              | 21.7             | 264.0                   | 9.80       | 81000                     | 2.30E-05          |

#### Vertical load back

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.8               |            | B 4+0,2d  | 9.5                  | 28.6                        |
| Circuit 2      | 3             | 2                 | 45.8               |            | B 4+0,2d  | 9.5                  | 28.6                        |
| Bliksemdraad 1 | 1             | 2                 | 9.6                |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 9.3                |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Vertical load ahead

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Circuit 2      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Bliksemdraad 1 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Insulators

| Conductor | $G_{isolator}$<br>[kN] | Number | $F_{v,iso}$<br>[kN] | Length<br>[m] | Wind surf.<br>[m <sup>2</sup> ] | Wind heigth<br>[m] | Pressure<br>[kN/m <sup>2</sup> ] | Drag factor<br>[-] | $F_{h,iso}$<br>[kN] |
|-----------|------------------------|--------|---------------------|---------------|---------------------------------|--------------------|----------------------------------|--------------------|---------------------|
| 380ct1f1  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct1f2  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct1f3  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 39.50              | 1.07                             | 1.2                | 2.56                |
| 380ct2f1  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct2f2  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 28.20              | 0.97                             | 1.2                | 2.33                |
| 380ct2f3  | 6.00                   | 1      | 6                   | 7.9           | 2.0                             | 39.50              | 1.07                             | 1.2                | 2.56                |
| bl1       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 43.70              | 1.10                             | 1.2                | 0.13                |
| bl2       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 43.70              | 1.10                             | 1.2                | 0.13                |

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**Wind load back**

| Conductor | Height |                      | G <sub>c_dwars</sub> | G <sub>c_trek</sub> | C <sub>c</sub> | d <sub>additional</sub> | w <sub>y</sub> | w <sub>y,section</sub> | D <sub>ijs,additional</sub> | w <sub>y,ijs</sub> | w <sub>y,ijs,section</sub> |
|-----------|--------|----------------------|----------------------|---------------------|----------------|-------------------------|----------------|------------------------|-----------------------------|--------------------|----------------------------|
|           | wind   | Pressure             |                      |                     |                |                         |                |                        |                             |                    |                            |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]                  | [-]                 | [-]            | [mm]                    | [N/m]          | [N/m]                  | [mm]                        | [N/m]              | [N/m]                      |
| 380ct1f1  | 20.5   | 0.88                 | 0.55                 | 0.61                | 1.13           | 28.25                   | 46.6           | 51.9                   | 46.9                        | 82.3               | 91.6                       |
| 380ct1f2  | 20.5   | 0.88                 | 0.55                 | 0.61                | 1.13           | 28.25                   | 46.6           | 51.9                   | 46.9                        | 82.3               | 91.6                       |
| 380ct1f3  | 31.8   | 1.00                 | 0.59                 | 0.65                | 1.09           | 28.25                   | 54.7           | 60.7                   | 46.9                        | 99.5               | 110.6                      |
| 380ct2f1  | 20.5   | 0.88                 | 0.55                 | 0.61                | 1.13           | 28.25                   | 46.6           | 51.9                   | 46.9                        | 82.3               | 91.6                       |
| 380ct2f2  | 20.5   | 0.88                 | 0.55                 | 0.61                | 1.13           | 28.25                   | 46.6           | 51.9                   | 46.9                        | 82.3               | 91.6                       |
| 380ct2f3  | 31.8   | 1.00                 | 0.59                 | 0.65                | 1.09           | 28.25                   | 54.7           | 60.7                   | 46.9                        | 99.5               | 110.6                      |
| bl1       | 36.0   | 1.04                 | 0.60                 | 0.66                | 1.20           | 22.24                   | 16.5           | 18.4                   | 63.1                        | 47.0               | 52.2                       |
| bl2       | 36.0   | 1.04                 | 0.60                 | 0.66                | 1.20           | 22.13                   | 16.5           | 18.3                   | 63.0                        | 46.9               | 52.1                       |

**Wind load ahead**

| Conductor | Height |                      | G <sub>c_dwars</sub> | G <sub>c_trek</sub> | C <sub>c</sub> | d <sub>additional</sub> | w <sub>y</sub> | w <sub>y,section</sub> | D <sub>ijs,additional</sub> | w <sub>y,ijs</sub> | w <sub>y,ijs,section</sub> |
|-----------|--------|----------------------|----------------------|---------------------|----------------|-------------------------|----------------|------------------------|-----------------------------|--------------------|----------------------------|
|           | wind   | Pressure             |                      |                     |                |                         |                |                        |                             |                    |                            |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]                  | [-]                 | [-]            | [mm]                    | [N/m]          | [N/m]                  | [mm]                        | [N/m]              | [N/m]                      |
| 380ct1f1  | 18.6   | 0.86                 | 0.54                 | 0.49                | 1.13           | 28.50                   | 45.2           | 40.6                   | 47.2                        | 79.2               | 71.2                       |
| 380ct1f2  | 18.6   | 0.86                 | 0.54                 | 0.49                | 1.13           | 28.50                   | 45.2           | 40.6                   | 47.2                        | 79.2               | 71.2                       |
| 380ct1f3  | 29.9   | 0.99                 | 0.58                 | 0.52                | 1.09           | 28.50                   | 53.7           | 48.3                   | 47.2                        | 97.5               | 87.6                       |
| 380ct2f1  | 18.6   | 0.86                 | 0.54                 | 0.49                | 1.13           | 28.50                   | 45.2           | 40.6                   | 47.2                        | 79.2               | 71.2                       |
| 380ct2f2  | 18.6   | 0.86                 | 0.54                 | 0.49                | 1.13           | 28.50                   | 45.2           | 40.6                   | 47.2                        | 79.2               | 71.2                       |
| 380ct2f3  | 29.9   | 0.99                 | 0.58                 | 0.52                | 1.09           | 28.50                   | 53.7           | 48.3                   | 47.2                        | 97.5               | 87.6                       |
| bl1       | 36.6   | 1.04                 | 0.60                 | 0.54                | 1.20           | 22.24                   | 16.7           | 15.0                   | 63.1                        | 47.3               | 42.5                       |
| bl2       | 36.6   | 1.04                 | 0.60                 | 0.54                | 1.20           | 22.13                   | 16.6           | 14.9                   | 63.0                        | 47.2               | 42.4                       |



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 Tower: HB+0  
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**Conductor loads** Auteur: TBR  
Versie: v11.8

**Starting points**  
 Consequence class Afkeur CC2-0  
 Reference period 30 jaar

| <b>ULS</b> (strength)   |                            | <b>NEN-EN50341-2-15:2019</b> |              |                  |            |          |          |                     |
|---|----------------------------|------------------------------|--------------|------------------|------------|----------|----------|---------------------|
| Load case   | description                | Temp °C                      | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|   |                            |                              | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a  | Wind                       | 10°                          | 1.05         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9  | Wind 0,9Gk only tower      | 10°                          | 0.90         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9_0,9  | Wind 0,9Gk conductors too  | 10°                          | 0.90         | 0.90             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 3   | Wind+ice                   | -5°                          | 1.05         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 3_0,9   | Wind+ice 0,9Gk             | -5°                          | 0.90         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 4   | Cold+wind                  | -20°                         | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 4_0,9   | Cold+wind 0,9Gk            | -20°                         | 0.90         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 5a  | Torsional loads            | 10°                          | 1.00         | 1.00             | 1.00       | 0.00     | 0.00     | 1.0                 |
| ULS 5b  | Longitudinal loads         | 10°                          | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| ULS 6   | Construction + maintenance | 5°                           | 1.05         | 1.05             | 1.20       | 0.22     | 0.00     | 0.0                 |
| ULS 6_0,9   | Construction + maintenance | 5°                           | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 7   | Permanent                  | 10°                          | 1.15         | 1.15             | 0.00       | 0.00     | 0.00     | 0.0                 |
| ULS 8   | Special                    | 10°                          | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| <b>SPLS</b> (strength, for angle towers: absence of conductors) |                            |                              | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
|   |                            |                              | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SPLS 1a   | Wind                       | 10°                          | 1.05         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9   | Wind 0,9                   | 10°                          | 0.90         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9_0,9   | Wind 0,9                   | 10°                          | 0.90         | 0.90             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 3  | Wind+ice                   | -5°                          | 1.05         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 3_0,9  | Wind+ice 0,9               | -5°                          | 0.90         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 4  | Cold+wind                  | -20°                         | 1.05         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 4_0,9  | Cold+wind 0,9              | -20°                         | 0.90         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 6  | Maintenance                | 5°                           | 1.05         | 1.05             | 1.2        | 0.24     | 0.0      | 0.0                 |
| SPLS 6_0,9  | Maintenance                | 5°                           | 1.05         | 1.05             | 0.0        | 0.24     | 0.0      | 0.0                 |
| <b>SLS</b> (deformations, fatigue, EDS)                         |                            |                              | $G_k$        |                  | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SLS 1a  | Wind                       | 10°                          | 1.00         | 1.00             | 0.0        | 0.94     | 0.0      | 0.0                 |
| SLS 3   | Wind+ice                   | -5°                          | 1.00         | 1.00             | 0.0        | 0.28     | 0.88     | 0.0                 |
| SLS 4   | Wind                       | -20°                         | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 6   | Maintenance                | 5°                           | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 7   | EDS, no wind               | 10°                          | 1.00         | 1.00             | 0.0        | 0.00     | 0.0      | 0.0                 |

Number of wind directions 6  
 Number of load combinations for ULS 54  
 Number of load combinations for SPLS 222  
 Number of load combinations for SLS 15  
 Number of concentrated loads 5238

Project: GT-RLL380  
 Tower: HB+0  
 Number: 78

### Summary table - Conductor loads

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

#### Maximum values for back and ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -39.9         | 42.4          | 14.1          | 0.1           | 5.8           | 6.1           |
| 380ct1f1    | -104.0        | 105.6         | 37.8          | 1.8           | 20.9          | 22.0          |
| 380ct1f2    | -104.0        | 105.6         | 37.8          | 1.8           | 20.9          | 22.0          |
| 380ct1f3    | -106.5        | 107.8         | 41.7          | 1.8           | 20.9          | 22.0          |
| 380ct2f1    | -104.0        | 105.6         | 37.8          | 1.8           | 20.9          | 22.0          |
| 380ct2f2    | -104.0        | 105.6         | 37.8          | 1.8           | 20.9          | 22.0          |
| 380ct2f3    | -106.5        | 107.8         | 41.7          | 1.8           | 20.9          | 22.0          |
| bl2         | -39.4         | 42.7          | 14.0          | 0.1           | 5.8           | 6.1           |
| V-ketting 1 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |
| V-ketting 2 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 349.2  | 358.0 | 360.1 |
| 380ct1f1    | 377.4  | 377.4 | 377.4 |
| 380ct1f2    | 377.4  | 377.4 | 377.4 |
| 380ct1f3    | 377.4  | 377.4 | 377.4 |
| 380ct2f1    | 377.4  | 377.4 | 377.4 |
| 380ct2f2    | 377.4  | 377.4 | 377.4 |
| 380ct2f3    | 377.4  | 377.4 | 377.4 |
| bl2         | 349.2  | 357.6 | 360.1 |
| V-ketting 1 |        |       |       |
| V-ketting 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 360.1  | 362.1 |
| 380ct1f1    | 377.4  | 377.4 |
| 380ct1f2    | 377.4  | 377.4 |
| 380ct1f3    | 377.4  | 377.4 |
| 380ct2f1    | 377.4  | 377.4 |
| 380ct2f2    | 377.4  | 377.4 |
| 380ct2f3    | 377.4  | 377.4 |
| bl2         | 360.1  | 362.0 |
| V-ketting 1 |        |       |
| V-ketting 2 |        |       |

Envelop of weight span over all combinations (incl. 0,9 combinations)

For all conductors

|                  |         | Wind / Weight span ratio |
|------------------|---------|--------------------------|
| Max. weight span | 377.4 m | 1.000 -                  |
| Min. weight span | 343.4 m | 0.910 -                  |

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**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba  | Ft_ah |
|-------------|------|------|------|--------|-------|
|             | [kN] | [kN] | [kN] | [kN]   | [kN]  |
| bl1         | 28.8 | 10.1 | 6.1  | -42.2  | 42.5  |
| 380ct1f1    | 95.7 | 34.5 | 22.0 | -109.5 | 106.2 |
| 380ct1f2    | 95.7 | 34.5 | 22.0 | -109.5 | 106.2 |
| 380ct1f3    | 96.0 | 39.0 | 22.0 | -112.5 | 108.3 |
| 380ct2f1    | 95.7 | 34.5 | 22.0 | -109.5 | 106.2 |
| 380ct2f2    | 95.7 | 34.5 | 22.0 | -109.5 | 106.2 |
| 380ct2f3    | 96.0 | 39.0 | 22.0 | -112.5 | 108.3 |
| bl2         | 28.9 | 9.9  | 6.1  | -41.7  | 42.8  |
| V-ketting 1 | 1.9  | 1.9  | 3.5  | 0.0    |       |
| V-ketting 2 | 1.9  | 1.9  | 3.5  | 0.0    |       |

**EDS-loads conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 13.5 | 3.5  | 1.9  | -13.1 | 13.8  |
| 380ct1f1    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct1f2    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct1f3    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct2f1    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct2f2    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct2f3    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| bl2         | 13.5 | 3.4  | 1.9  | -12.8 | 13.7  |
| V-ketting 1 | 0.0  | 0.0  | 3.0  | 0.0   |       |
| V-ketting 2 | 0.0  | 0.0  | 3.0  | 0.0   |       |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4      bl1       | 0.0   | 0.0   |
| 380ct1f1             | 0.0   | 0.0   |
| 380ct1f2             | 0.0   | 0.0   |
| 380ct1f3             | 0.0   | 0.0   |
| 380ct2f1             | 0.0   | 0.0   |
| 380ct2f2             | 0.0   | 0.0   |
| 380ct2f3             | 0.0   | 0.0   |
| bl2                  | 0.0   | 0.0   |
| V-ketting 1          | 0.0   |       |
| V-ketting 2          | 0.0   |       |

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**ULS foundation loads for LC 1 and 3, wind perpendicular to the line or bisector and EDS, from conductors**

| Combination       | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -7            | 226           | 198           | 7449           | -221           | 5              |
| ULS 1a_0,9_0      |             | 13            | 46            | 197           | 1552           | 408            | 48             |
| ULS 1a_0,9_0,9_90 |             | -12           | 224           | 170           | 7380           | -379           | 4              |
| ULS 3_0           |             | 16            | 66            | 277           | 2210           | 563            | 27             |
| SLS 7             |             | 8             | 36            | 189           | 1214           | 269            | 6              |

**ULS foundation loads, LC 1 and 3, wind perpendicular to the line or bisector and EDS, total conductors and tower**

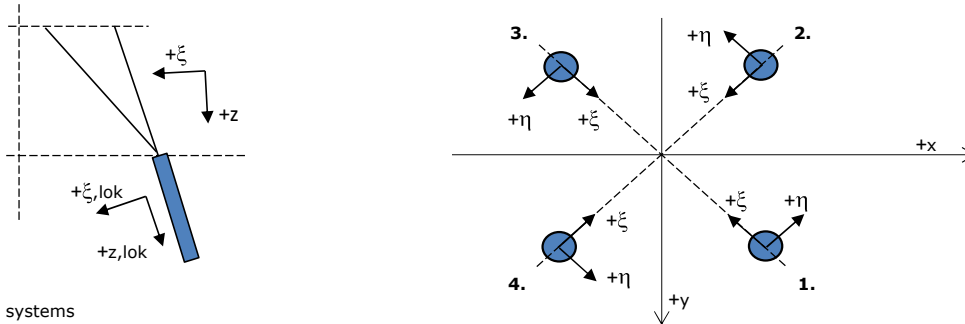
| Combination       | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -7            | 369           | 671           | 11123          | -221           | 5              |
| ULS 1a_0,9_0,9_90 | -12           | 367           | 575           | 11053          | -379           | 4              |
| SLS 7             | 8             | 36            | 639           | 1214           | 269            | 6              |

**Foundation loads, selection of load combinations based on greatest value**

| Combination              | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|--------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_74.4              | 19            | 389           | 671           | <b>11764</b>   | 336            | 16             |
| SPLS 3_74.4 Ba All Cts   | 590           | -23           | 628           | -1015          | <b>19167</b>   | 7              |
| SPLS 6a_90 Ah Ct1 Ba Ct1 | -309          | 166           | 676           | 5432           | -10053         | <b>4240</b>    |
| SPLS 3_79.6 Ah All Cts   | -576          | 244           | 621           | <b>7696</b>    | <b>-18881</b>  | 9              |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



**Maximum compression load**

| Index | Combination            | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 1a_45 Ba All Cts  | 190           | 213           | <b>1048</b>   | -16                | -285              | -54                   | 1073                |
| 2     | SPLS 3_0 Ba All Cts    | 203           | -225          | <b>1125</b>   | 16                 | -302              | -54                   | 1152                |
| 3     | SPLS 3_135 Ah All Cts  | -113          | -146          | <b>677</b>    | -23                | -183              | -33                   | 693                 |
| 4     | SPLS 3_79.6 Ah All Cts | -246          | 267           | <b>1363</b>   | 15                 | -363              | -62                   | 1396                |

**Maximum tension load**

| Index | Combination                | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|----------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_135 Ah All Cts  | -53           | -86           | <b>-384</b>   | 23                 | 98                | 14                    | -393                |
| 2     | SPLS 3_0,9_79.6 Ah All Cts | -187          | 207           | <b>-1069</b>  | -14                | 279               | 42                    | -1095               |
| 3     | SPLS 1a_0,9_45 Ba All Cts  | 130           | 155           | <b>-757</b>   | 18                 | 202               | 34                    | -775                |
| 4     | SPLS 3_0,9_0 Ba All Cts    | 143           | -164          | <b>-828</b>   | -15                | 217               | 34                    | -848                |

**Maximum torsional load (positive)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ba Ct1 | 104           | -113          | -41           | <b>153</b>         | 7                 | -2                    | -42                 |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | 18            | -219          | 627           | <b>142</b>         | -168              | -29                   | 643                 |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -43           | 161           | -325          | <b>144</b>         | 83                | 11                    | -333                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -65           | 265           | 873           | <b>141</b>         | -234              | -41                   | 894                 |

**Maximum torsional load (negative)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 28            | 229           | 677           | <b>-142</b>        | -182              | -33                   | 693                 |
| 2     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 6             | 196           | -519          | <b>-143</b>        | 134               | 20                    | -532                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 31            | -182          | 395           | <b>-151</b>        | -106              | -19                   | 404                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -53           | -150          | -277          | <b>-144</b>        | 69                | 7                     | -283                |

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#### Combination Ftensile+Fhor

| Index | Combination                  | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 6a_90 Ah All Cts Ba Ct1 | -11                    | -107                   | <b>-338</b>            | <b>68</b>              | 83                     | 9                          | -346                       |
| 2     | SPLS 3_0_9_79.6 Ah All Cts   | -187                   | 207                    | <b>-1069</b>           | <b>-14</b>             | 279                    | 42                         | -1095                      |
| 3     | SPLS 1a_0_9_74.4 Ba Ct2      | 9                      | 177                    | <b>-489</b>            | <b>119</b>             | 132                    | 24                         | -501                       |
| 4     | SPLS 6a_90 Ba All Cts Ah Ct1 | 86                     | -168                   | <b>-705</b>            | <b>-58</b>             | 180                    | 24                         | -722                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 46                     | 44                     | 227                    | 1                      | -63                    | -13                        | 233                        |
| 2     | SLS 7       | 23                     | -26                    | 117                    | 2                      | -35                    | -9                         | 120                        |
| 3     | SLS 7       | -19                    | -21                    | 92                     | -1                     | -28                    | -8                         | 95                         |
| 4     | SLS 7       | -42                    | 39                     | 203                    | -2                     | -57                    | -12                        | 208                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | SPLS 3_79.6 Ah All Cts     | -246                   | 267                    | <b>1363</b>            | 15                     | -363                   | -62                        | 1396                       |
| Max. tension         | SPLS 3_0_9_79.6 Ah All Cts | -187                   | 207                    | <b>-1069</b>           | -14                    | 279                    | 42                         | -1095                      |
| Max. pos. torsie     | SPLS 6a_90 Ah Ct1 Ba Ct1   | 104                    | -113                   | -41                    | <b>153</b>             | 7                      | -2                         | -42                        |
| Max. neg. torsie     | SPLS 6a_90 Ah Ct2 Ba Ct2   | 31                     | -182                   | 395                    | <b>-151</b>            | -106                   | -19                        | 404                        |
| Comb. tension+torsie | SPLS 3_0_9_79.6 Ah All Cts | -187                   | 207                    | <b>-1069</b>           | <b>-14</b>             | 279                    | 42                         | -1095                      |

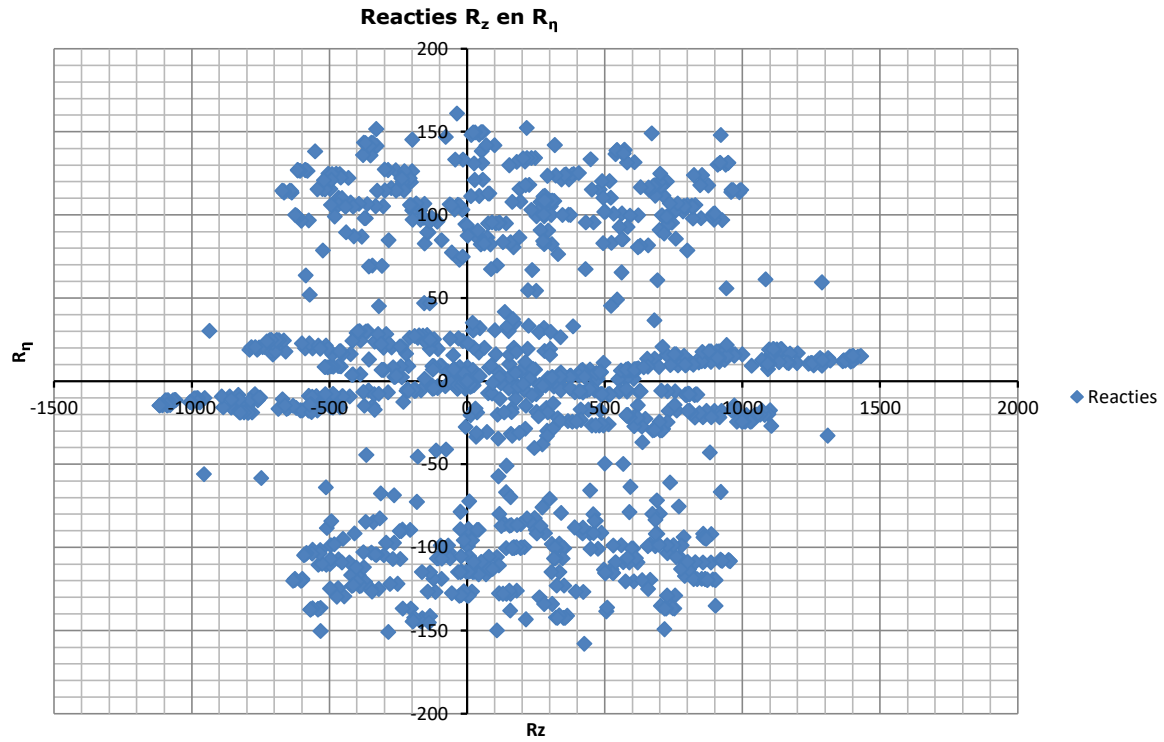
#### Maximum tension load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 46                     | 44                     | <b>227</b>             | 1                      | -63                    | -13                        | 233                        |
| 2     | SLS 1a_90   | -56                    | 47                     | <b>-277</b>            | 6                      | 73                     | 12                         | -284                       |
| 3     | SLS 1a_45   | 72                     | 63                     | <b>-352</b>            | -6                     | 95                     | 18                         | -361                       |
| 4     | SLS 1a_0    | 0                      | -3                     | <b>-7</b>              | -2                     | 2                      | 0                          | -8                         |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_45   | 138                    | 127                    | <b>672</b>             | 8                      | -187                   | -39                        | 688                        |
| 2     | SLS 1a_0    | 63                     | -70                    | <b>327</b>             | 5                      | -94                    | -22                        | 335                        |
| 3     | SLS 7       | -19                    | -21                    | <b>92</b>              | -1                     | -28                    | -8                         | 95                         |
| 4     | SLS 1a_90   | -121                   | 112                    | <b>597</b>             | -6                     | -165                   | -33                        | 611                        |

Project: GT-RL380  
Tower: HB+0  
Number: 78



Project: GT-RL380  
 Tower: HB+0  
 Number: 78

**Conductor loads** Auteur: TBR  
Versie: v11.8

**Starting points**  
 Consequence class Verbouw CC2  
 Reference period 50 jaar

| ULS (strength)   |                            | NEN-EN50341-2-15:2019 |              |                  |            |          |          |                     |
|--|----------------------------|-----------------------|--------------|------------------|------------|----------|----------|---------------------|
| Load case  | description                | Temp °C               | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|  |                            |                       | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a   | Wind                       | 10°                   | 1.15         | 1.15             | 0.00       | 1.40     | 0.00     | 0.0                 |
| ULS 1a_0,9   | Wind 0,9Gk only tower      | 10°                   | 0.90         | 1.15             | 0.00       | 1.40     | 0.00     | 0.0                 |
| ULS 1a_0,9_0,9   | Wind 0,9Gk conductors too  | 10°                   | 0.90         | 0.90             | 0.00       | 1.40     | 0.00     | 0.0                 |
| ULS 3  | Wind+ice                   | -5°                   | 1.15         | 1.15             | 0.00       | 0.42     | 1.30     | 0.0                 |
| ULS 3_0,9  | Wind+ice 0,9Gk             | -5°                   | 0.90         | 1.15             | 0.00       | 0.42     | 1.30     | 0.0                 |
| ULS 4  | Cold+wind                  | -20°                  | 1.15         | 1.15             | 0.00       | 0.28     | 0.00     | 0.0                 |
| ULS 4_0,9  | Cold+wind 0,9Gk            | -20°                  | 0.90         | 1.15             | 0.00       | 0.28     | 0.00     | 0.0                 |
| ULS 5a   | Torsional loads            | 10°                   | 1.00         | 1.00             | 1.00       | 0.00     | 0.00     | 1.0                 |
| ULS 5b   | Longitudinal loads         | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| ULS 6  | Construction + maintenance | 5°                    | 1.15         | 1.15             | 1.30       | 0.28     | 0.00     | 0.0                 |
| ULS 6_0,9  | Construction + maintenance | 5°                    | 1.15         | 1.15             | 0.00       | 0.28     | 0.00     | 0.0                 |
| ULS 7  | Permanent                  | 10°                   | 1.30         | 1.30             | 0.00       | 0.00     | 0.00     | 0.0                 |
| ULS 8  | Special                    | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| SPLS (strength, for angle towers: absence of conductors) |                            |                       | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
|  |                            |                       | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SPLS 1a  | Wind                       | 10°                   | 1.15         | 1.15             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9  | Wind 0,9                   | 10°                   | 0.90         | 1.15             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9_0,9  | Wind 0,9                   | 10°                   | 0.90         | 0.90             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 3   | Wind+ice                   | -5°                   | 1.15         | 1.15             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 3_0,9   | Wind+ice 0,9               | -5°                   | 0.90         | 1.15             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 4   | Cold+wind                  | -20°                  | 1.15         | 1.15             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 4_0,9   | Cold+wind 0,9              | -20°                  | 0.90         | 1.15             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 6   | Maintenance                | 5°                    | 1.15         | 1.15             | 1.2        | 0.24     | 0.0      | 0.0                 |
| SPLS 6_0,9   | Maintenance                | 5°                    | 1.15         | 1.15             | 0.0        | 0.24     | 0.0      | 0.0                 |
| SLS (deformations, fatigue, EDS)                         |                            |                       | $G_k$        |                  | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SLS 1a   | Wind                       | 10°                   | 1.00         | 1.00             | 0.0        | 1.00     | 0.0      | 0.0                 |
| SLS 3  | Wind+ice                   | -5°                   | 1.00         | 1.00             | 0.0        | 0.30     | 1.00     | 0.0                 |
| SLS 4  | Wind                       | -20°                  | 1.00         | 1.00             | 0.0        | 0.20     | 0.0      | 0.0                 |
| SLS 6  | Maintenance                | 5°                    | 1.00         | 1.00             | 0.0        | 0.20     | 0.0      | 0.0                 |
| SLS 7  | EDS, no wind               | 10°                   | 1.00         | 1.00             | 0.0        | 0.00     | 0.0      | 0.0                 |

Number of wind directions 6  
 Number of load combinations for ULS 54  
 Number of load combinations for SPLS 222  
 Number of load combinations for SLS 15  
 Number of concentrated loads 5238

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**Summary table - Conductor loads**

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

**Maximum values for back and ahead span**

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -48.7         | 52.1          | 17.3          | 0.1           | 7.6           | 7.9           |
| 380ct1f1    | -120.8        | 122.8         | 45.0          | 1.8           | 22.9          | 24.8          |
| 380ct1f2    | -120.8        | 122.8         | 45.0          | 1.8           | 22.9          | 24.8          |
| 380ct1f3    | -124.1        | 125.6         | 50.0          | 1.8           | 22.9          | 24.8          |
| 380ct2f1    | -120.8        | 122.8         | 45.0          | 1.8           | 22.9          | 24.8          |
| 380ct2f2    | -120.8        | 122.8         | 45.0          | 1.8           | 22.9          | 24.8          |
| 380ct2f3    | -124.1        | 125.6         | 50.0          | 1.8           | 22.9          | 24.8          |
| bl2         | -48.0         | 52.4          | 17.1          | 0.1           | 7.5           | 7.9           |
| V-ketting 1 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |
| V-ketting 2 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |

**Min. Weight span (m)**

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 348.2  | 357.9 | 360.1 |
| 380ct1f1    | 377.4  | 377.4 | 377.4 |
| 380ct1f2    | 377.4  | 377.4 | 377.4 |
| 380ct1f3    | 377.4  | 377.4 | 377.4 |
| 380ct2f1    | 377.4  | 377.4 | 377.4 |
| 380ct2f2    | 377.4  | 377.4 | 377.4 |
| 380ct2f3    | 377.4  | 377.4 | 377.4 |
| bl2         | 348.2  | 357.5 | 360.1 |
| V-ketting 1 |        |       |       |
| V-ketting 2 |        |       |       |

**Max. Weight span (m)**

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 360.3  | 362.8 |
| 380ct1f1    | 377.4  | 377.4 |
| 380ct1f2    | 377.4  | 377.4 |
| 380ct1f3    | 377.4  | 377.4 |
| 380ct2f1    | 377.4  | 377.4 |
| 380ct2f2    | 377.4  | 377.4 |
| 380ct2f3    | 377.4  | 377.4 |
| bl2         | 360.3  | 362.7 |
| V-ketting 1 |        |       |
| V-ketting 2 |        |       |

Envelop of weight span over all combinations (incl. 0,9 combinations)

For all conductors

|                  |         | Wind / Weight span ratio |
|------------------|---------|--------------------------|
| Max. weight span | 377.4 m | 1.000 -                  |
| Min. weight span | 337.6 m | 0.895 -                  |



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**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider    | Fx    | Fy   | Fz   | Ft_ba  | Ft_ah |
|-------------|-------|------|------|--------|-------|
|             | [kN]  | [kN] | [kN] | [kN]   | [kN]  |
| bl1         | 29.9  | 12.4 | 7.9  | -51.5  | 52.2  |
| 380ct1f1    | 100.7 | 42.5 | 24.8 | -127.5 | 123.4 |
| 380ct1f2    | 100.7 | 42.5 | 24.8 | -127.5 | 123.4 |
| 380ct1f3    | 101.0 | 48.1 | 24.8 | -131.2 | 126.0 |
| 380ct2f1    | 100.7 | 42.5 | 24.8 | -127.5 | 123.4 |
| 380ct2f2    | 100.7 | 42.5 | 24.8 | -127.5 | 123.4 |
| 380ct2f3    | 101.0 | 48.1 | 24.8 | -131.2 | 126.0 |
| bl2         | 29.9  | 12.3 | 7.9  | -50.9  | 52.5  |
| V-ketting 1 | 2.4   | 2.4  | 3.9  | 0.0    |       |
| V-ketting 2 | 2.4   | 2.4  | 3.9  | 0.0    |       |

**EDS-loads conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 13.5 | 3.5  | 1.9  | -13.1 | 13.8  |
| 380ct1f1    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct1f2    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct1f3    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct2f1    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct2f2    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| 380ct2f3    | 61.7 | 16.9 | 15.1 | -63.0 | 62.7  |
| bl2         | 13.5 | 3.4  | 1.9  | -12.8 | 13.7  |
| V-ketting 1 | 0.0  | 0.0  | 3.0  | 0.0   |       |
| V-ketting 2 | 0.0  | 0.0  | 3.0  | 0.0   |       |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4 bl1            | 0.0   | 0.0   |
| 380ct1f1             | 0.0   | 0.0   |
| 380ct1f2             | 0.0   | 0.0   |
| 380ct1f3             | 0.0   | 0.0   |
| 380ct2f1             | 0.0   | 0.0   |
| 380ct2f2             | 0.0   | 0.0   |
| 380ct2f3             | 0.0   | 0.0   |
| bl2                  | 0.0   | 0.0   |
| V-ketting 1          | 0.0   |       |
| V-ketting 2          | 0.0   |       |

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**ULS foundation loads for LC 1 and 3, wind perpendicular to the line or bisector and EDS, from conductors**

| Combination       | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -11           | 279           | 217           | 9172           | -347           | 6              |
| ULS 1a_0,9_0      |             | 14            | 52            | 216           | 1730           | 457            | 59             |
| ULS 1a_0,9_0,9_90 |             | -19           | 276           | 170           | 9076           | -604           | 5              |
| ULS 3_0           |             | 20            | 77            | 324           | 2581           | 699            | 33             |
| SLS 7             |             | 8             | 36            | 189           | 1214           | 269            | 6              |

**ULS foundation loads, LC 1 and 3, wind perpendicular to the line or bisector and EDS, total conductors and tower**

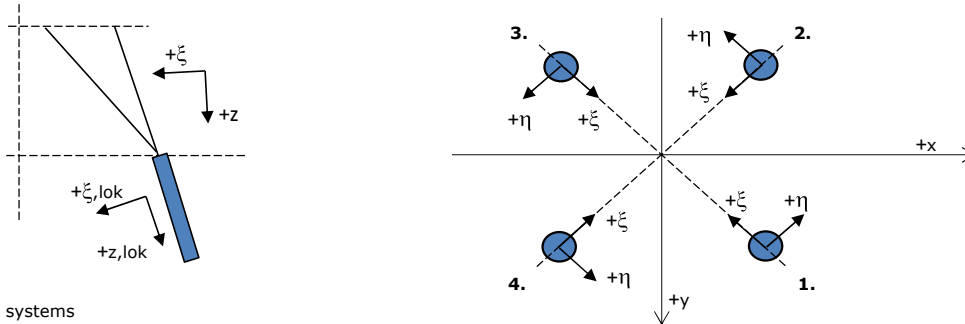
| Combination       | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -11           | 458           | 734           | 13778          | -347           | 6              |
| ULS 1a_0,9_0,9_90 | -19           | 455           | 575           | 13682          | -604           | 5              |
| SLS 7             | 8             | 36            | 639           | 1214           | 269            | 6              |

**Foundation loads, selection of load combinations based on greatest value**

| Combination              | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|--------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_74.4              | 21            | 482           | 734           | <b>14583</b>   | 352            | 20             |
| SPLS 3_74.4 Ba All Cts   | 621           | -29           | 687           | -1188          | <b>20145</b>   | 7              |
| SPLS 6a_90 Ah Ct1 Ba Ct1 | -325          | 172           | 737           | 5666           | -10540         | <b>4453</b>    |
| SPLS 3_79.6 Ah All Cts   | -604          | 252           | 679           | <b>7953</b>    | <b>-19777</b>  | 9              |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



**Maximum compression load**

| Index | Combination            | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 1a_45 Ba All Cts  | 199           | 224           | <b>1100</b>   | -18                | -299              | -56                   | 1127                |
| 2     | SPLS 3_0 Ba All Cts    | 216           | -240          | <b>1200</b>   | 17                 | -323              | -57                   | 1229                |
| 3     | SPLS 3_135 Ah All Cts  | -121          | -156          | <b>727</b>    | -25                | -196              | -36                   | 744                 |
| 4     | SPLS 3_79.6 Ah All Cts | -259          | 280           | <b>1430</b>   | 15                 | -381              | -65                   | 1465                |

**Maximum tension load**

| Index | Combination                | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|----------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_135 Ah All Cts  | -58           | -93           | <b>-416</b>   | 24                 | 107               | 15                    | -426                |
| 2     | SPLS 3_0,9_79.6 Ah All Cts | -196          | 217           | <b>-1118</b>  | -15                | 292               | 45                    | -1145               |
| 3     | SPLS 1a_0,9_45 Ba All Cts  | 135           | 162           | <b>-791</b>   | 19                 | 210               | 36                    | -810                |
| 4     | SPLS 3_0,9_0 Ba All Cts    | 153           | -175          | <b>-886</b>   | -16                | 232               | 37                    | -907                |

**Maximum torsional load (positive)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ba Ct1 | 110           | -118          | -37           | <b>161</b>         | 6                 | -2                    | -38                 |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | 21            | -232          | 671           | <b>149</b>         | -179              | -31                   | 687                 |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -48           | 167           | -331          | <b>152</b>         | 84                | 11                    | -339                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -70           | 279           | 921           | <b>148</b>         | -247              | -43                   | 943                 |

**Maximum torsional load (negative)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 31            | 242           | 716           | <b>-149</b>        | -193              | -35                   | 734                 |
| 2     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 9             | 204           | -533          | <b>-150</b>        | 138               | 20                    | -546                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 31            | -193          | 425           | <b>-158</b>        | -114              | -21                   | 435                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -57           | -157          | -286          | <b>-151</b>        | 71                | 8                     | -293                |

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#### Combination Ftensile+Fhor

| Index | Combination                  | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 6a_90 Ah All Cts Ba Ct1 | -13                    | -111                   | <b>-357</b>            | <b>69</b>              | 88                     | 9                          | -366                       |
| 2     | SPLS 3_0,9_79.6 Ah All Cts   | -196                   | 217                    | <b>-1118</b>           | <b>-15</b>             | 292                    | 45                         | -1145                      |
| 3     | SPLS 1a_0,9_74.4 Ba Ct2      | 8                      | 184                    | <b>-504</b>            | <b>125</b>             | 136                    | 24                         | -516                       |
| 4     | SPLS 3_0,9_0 Ba All Cts      | 153                    | -175                   | <b>-886</b>            | <b>-16</b>             | 232                    | 37                         | -907                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 46                     | 44                     | 227                    | 1                      | -63                    | -13                        | 233                        |
| 2     | SLS 7       | 23                     | -26                    | 117                    | 2                      | -35                    | -9                         | 120                        |
| 3     | SLS 7       | -19                    | -21                    | 92                     | -1                     | -28                    | -8                         | 95                         |
| 4     | SLS 7       | -42                    | 39                     | 203                    | -2                     | -57                    | -12                        | 208                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination                | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | SPLS 3_79.6 Ah All Cts     | -259                   | 280                    | <b>1430</b>            | 15                     | -381                   | -65                        | 1465                       |
| Max. tension         | SPLS 3_0,9_79.6 Ah All Cts | -196                   | 217                    | <b>-1118</b>           | -15                    | 292                    | 45                         | -1145                      |
| Max. pos. torsie     | SPLS 6a_90 Ah Ct1 Ba Ct1   | 110                    | -118                   | -37                    | <b>161</b>             | 6                      | -2                         | -38                        |
| Max. neg. torsie     | SPLS 6a_90 Ah Ct2 Ba Ct2   | 31                     | -193                   | 425                    | <b>-158</b>            | -114                   | -21                        | 435                        |
| Comb. tension+torsie | SPLS 3_0,9_79.6 Ah All Cts | -196                   | 217                    | <b>-1118</b>           | <b>-15</b>             | 292                    | 45                         | -1145                      |

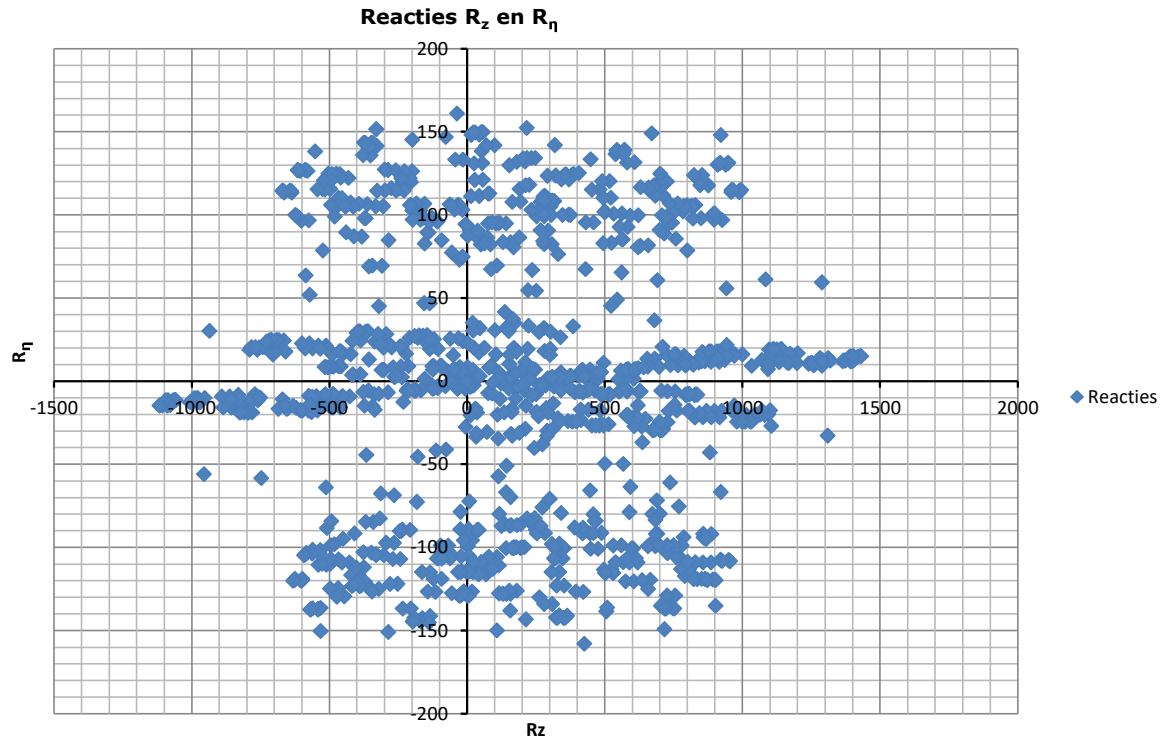
#### Maximum tension load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 46                     | 44                     | <b>227</b>             | 1                      | -63                    | -13                        | 233                        |
| 2     | SLS 1a_90   | -62                    | 52                     | <b>-304</b>            | 7                      | 80                     | 13                         | -311                       |
| 3     | SLS 1a_45   | 77                     | 68                     | <b>-378</b>            | -6                     | 103                    | 19                         | -387                       |
| 4     | SLS 1a_0    | 2                      | -6                     | <b>-20</b>             | -3                     | 6                      | 1                          | -20                        |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_45   | 143                    | 131                    | <b>697</b>             | 8                      | -194                   | -40                        | 714                        |
| 2     | SLS 1a_0    | 65                     | -73                    | <b>339</b>             | 5                      | -97                    | -22                        | 348                        |
| 3     | SLS 7       | -19                    | -21                    | <b>92</b>              | -1                     | -28                    | -8                         | 95                         |
| 4     | SLS 1a_90   | -126                   | 117                    | <b>623</b>             | -6                     | -172                   | -34                        | 638                        |

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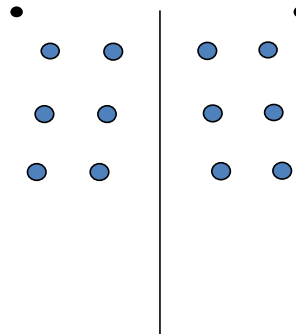
Project: GT-RLL380  
 Tower: HS  
 Number: 26

Auteur: TBR  
 Versie: v11.8

### Conductor loads

#### General

Description HS  
 Tower type Steunmast  
 Number of circuits 2  
 Configuration 2-circuit-donau  
 Number of earth wires 2



Configuratie geleiders

#### Starting points

Norm NEN-EN50341-2-15:2019  
 Consequence class CC2-0  
 Reliability level initial Afkeur CC2-0  
 Reference period initial 30 jaar  
 Consequence class modified CC2  
 Reliability level modified Verbouw  
 Reference period modified 50 jaar  
 Wind zone III  
 Wind speed (m/s) 24.5 m/s  
 Terrain category II  
 Reduction factor  $c_{dir}$  1.00  
 Ice region phase conductor B  
 Ice region earth conductor A

#### Conductors back

| Description    | Voltage | Conductor Back        | Bundle Ba | Ice region | Additional weight | Additional diameter | Catenary $P_{back}$ |
|----------------|---------|-----------------------|-----------|------------|-------------------|---------------------|---------------------|
| Circuit 1      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                |
| Circuit 2      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 1 |         | ACSR-26/7-242/39-HAWK | 1         | A          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 2 |         | OPGW 226              | 1         | A          | 2 %               | 2 %                 | 1375                |

#### Conductors ahead

| Description    | Voltage | Conductor Ahead       | Bundle Ah | Ice region | Additional weight | Additional diameter | Catenary $P_{ahead}$ |
|----------------|---------|-----------------------|-----------|------------|-------------------|---------------------|----------------------|
| Circuit 1      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Circuit 2      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 1 |         | ACSR-26/7-242/39-HAWK | 1         | A          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 2 |         | OPGW 226              | 1         | A          | 2 %               | 2 %                 | 1375                 |

#### Insulators (1)

| Description    | Suspension          | Weight [kN] | Length [m] | Wind area [m <sup>2</sup> ] |
|----------------|---------------------|-------------|------------|-----------------------------|
| Circuit 1      | Halfverankering     | 5.50        | 4.50       | 2.40                        |
| Circuit 2      | Halfverankering     | 5.50        | 4.50       | 2.40                        |
| Bliksemdraad 1 | Vast (Bliksemdraad) | 0.10        | 0.20       | 0.10                        |
| Bliksemdraad 2 | Vast (Bliksemdraad) | 0.10        | 0.20       | 0.10                        |

1. Properties apply to the entire isolator set

#### Suspension height and position in mast

| Circuits       | Designation | Number   | Suspension height | Attach point | Position in tower Horizontal distance |
|----------------|-------------|----------|-------------------|--------------|---------------------------------------|
| Circuit 1      | 10          | 380ct1f1 | 28.1 m            | 32.6 m       | -16.0 m                               |
| Circuit 1      | 11          | 380ct1f2 | 28.1 m            | 32.6 m       | -9.0 m                                |
| Circuit 1      | 12          | 380ct1f3 | 39.4 m            | 43.9 m       | -12.5 m                               |
| Circuit 2      | 20          | 380ct2f1 | 28.1 m            | 32.6 m       | 16.0 m                                |
| Circuit 2      | 21          | 380ct2f2 | 28.1 m            | 32.6 m       | 9.0 m                                 |
| Circuit 2      | 22          | 380ct2f3 | 39.4 m            | 43.9 m       | 12.5 m                                |
| Bliksemdraad 1 | 1           | bl1      | 43.7 m            | 43.9 m       | -18.5 m                               |
| Bliksemdraad 2 | 3           | bl2      | 43.7 m            | 43.9 m       | 18.5 m                                |

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**Height adjustment adjacent masts** (wind and weight span adjustment)

|                                     | Back  | Ahead |  |
|-------------------------------------|-------|-------|--|
| Height increase for wind pressure   | 0.0 m | 0.0 m | (positive: higher)                     |
| Height decrease for vertical load   | 0.0 m | 0.0 m | (negative: decrease, more weight span) |
| Decrease: Niet in 0,9EG-combinaties |       |       |  |

**Height difference adjacent tower and change of direction with respect to Line direction**

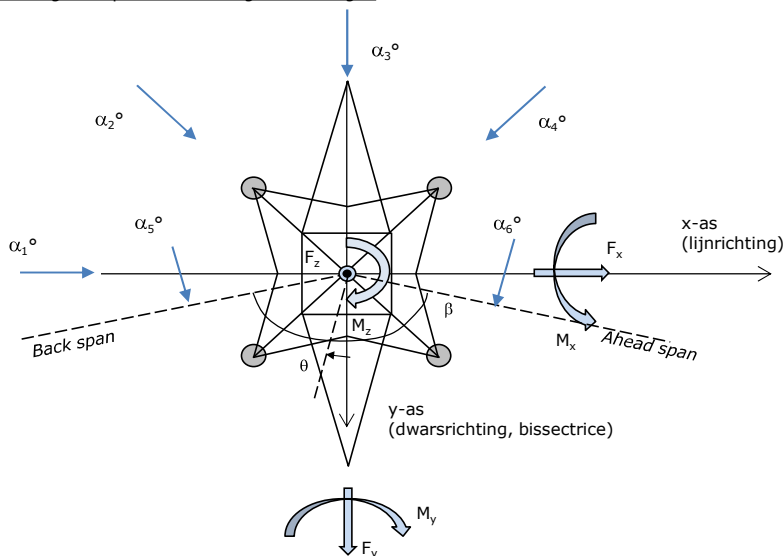
| Circuits       | Aanduiding | Nummer   | Hoogteverschil    |                    | Richtingsverandering |                    |
|----------------|------------|----------|-------------------|--------------------|----------------------|--------------------|
|                |            |          | $\Delta h_{back}$ | $\Delta h_{ahead}$ | $\Delta y_{back}$    | $\Delta y_{ahead}$ |
| Circuit 1      | 10         | 380ct1f1 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 11         | 380ct1f2 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 12         | 380ct1f3 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 20         | 380ct2f1 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 21         | 380ct2f2 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 22         | 380ct2f3 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 1 | 1          | bl1      | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 2 | 3          | bl2      | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |

**Line and tower data**

|  | Back          | Ahead       |
|--|---------------|-------------|
| Ruling span $\sqrt{(\Sigma L^3 / \Sigma L)}$ | 342.5         | 346.0 m     |
| Line angle                                   | 335.9         | 335.9 m     |
| Tower orientation with respect to bis0       | $177.3^\circ$ | $0^\circ$   |
| Section length                               | 1670          | 1670 m      |
| Height bottom of tower to ground level       | 0.5 m         |             |
| Wind directions considered                   | $\alpha_1$    | $0^\circ$   |
| Wind directions according to:                | $\alpha_2$    | $45^\circ$  |
| <i>Geleiderbelastingen</i>                   | $\alpha_3$    | $90^\circ$  |
|  | $\alpha_4$    | $135^\circ$ |
|  | $\alpha_5$    | $-^\circ$   |
|  | $\alpha_6$    | $-^\circ$   |

Wind directions apply to the main direction of mast construction, not to the bisector.

Windrichtingen en positieve richtingen belastingen



**Considered number of wind directions**

|        |   |
|--------|---|
| 1a     | 4 |
| 3      | 4 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

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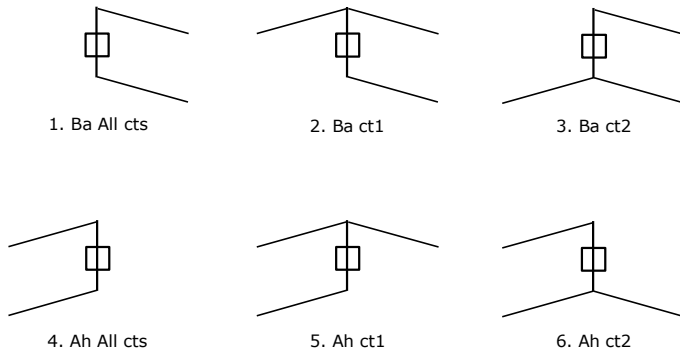
**Absence of conductors**

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 0.8                | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 0.8                | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 0.8                | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 0.8                | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 0.8                | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 0.8                | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | b2       | 0             | 1    | 1                        | 0    | 1                  | 0    |

**Load situations SPLS**

Considered situations SPLS: SPLS for suspension tower not applicable

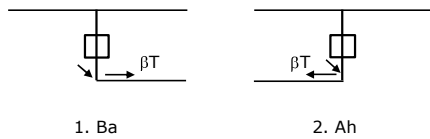
Principle of load situations:



**Load situation 5a. Conductor failure**

Considered situations conductor failure 5a: 1 and 2, all possible situations

Principle of load situations:





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**Load situations LC6. Construction and maintenance**

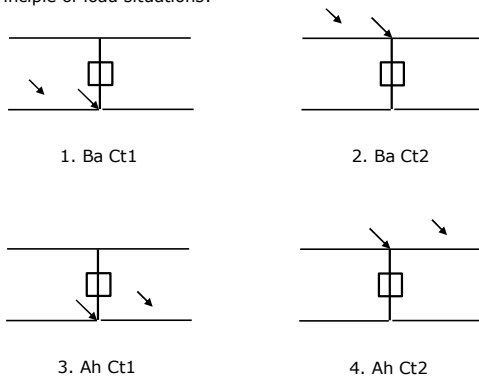
Under 6a, the load due to the presence of a line vehicle or line bicycle in combination with point load on the traverse is assessed. Combination 6b does not contain any loads in conductor or on traverse. This combination has been added to be able to combine with separate control platforms, etc. The situations are applied in ULS and in every SPLS situation (in case of angle tower).

|                             | Phase  | Earth  |
|-----------------------------|--------|--------|
| Line vehicle                | 4.0 kN | 2.0 kN |
| Concentrated load cross arm | 1.0 kN | 1.0 kN |

Beschouwde situaties bouw- en onderhoud 6a: 1 en 2, uitgangspunt is symmetrie tussen back / ahead.

Presence line vehicle: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principle of load situations:



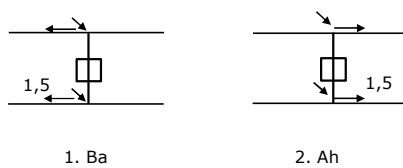
**Load situations 8. Galloping as a static load**

| Conductor                    |         |       |
|------------------------------|---------|-------|
| Suspension tower phase       | 0.866 W | 1.5 W |
| Suspension tower earth       | 1.5 EDS | 1.5 W |
| Strain tower phase and earth | 1.5 EDS | 1.5 W |

Considered situations galloping 8: 1, design assumption is symmetry back and ahead

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principle of load situations:



**Load combination 8. Galloping as a dynamic load**

Only applies to tension towers  
 Load consists of EDS tensile load in one of the conductors on one side of the tower  
 Can be converted by user to fatigue spectrum via the load spectrum of table 4.11 / NL.1

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### Tower structure

#### Properties

|                                      |            |              |
|--------------------------------------|------------|--------------|
| Tower type                           | Steunmast  |              |
| Tower designation                    | HS         |              |
| Base plate w.r.t. ground level       | 0.5 m      |              |
| Tower height w.r.t. base plate       | 47.9 m     |              |
| Tower self weight                    | 209.0 kN   |              |
| <i>Width and slope at foundation</i> |            |              |
| Leg spread                           | x-ri. 9.00 | y-ri. 9.00 m |
| Inclination of main leg              | 0.144      | 0.144 -      |
| Horizontal force factor              | 1.3        | 1.3 -        |

#### Calculation Wind load

|  |                                       |
|--|---------------------------------------|
| Dynamic factor $G_T$   | 1.00 ( <i>Masthoogte &lt; 60 m</i> )  |
| Wind load diagonally to tower body proportional to:            | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Wind load diagonally on traverse proportional to:              | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Magnification factor diagonal wind to tower body               | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor diagonal wind to cross arm                | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor wind parallel to perpendicular to cross a | 0.4                                   |

#### Properties mast sections longitudinal direction (front view, yz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 11.18    | 9.00                  | 5.79                  | 11.18     | 0.144                 | 82.66                               | 9.27                                | 0.11                                      | 3.34           |
| Eerste tussenstuk | 21.18    | 5.79                  | 4.48                  | 10.00     | 0.065                 | 51.36                               | 7.20                                | 0.14                                      | 3.21           |
| Tweede tussenstuk | 32.55    | 4.48                  | 3.00                  | 11.37     | 0.065                 | 42.55                               | 7.85                                | 0.18                                      | 3.00           |
| Bovenstuk 1       | 38.37    | 3.00                  | 2.62                  | 5.82      | 0.033                 | 16.35                               | 3.86                                | 0.24                                      | 2.78           |
| Bovenstuk 2       | 46.38    | 2.62                  | 2.00                  | 8.01      | 0.039                 | 18.49                               | 4.45                                | 0.24                                      | 2.76           |
| Topstuk           | 47.88    | 2.00                  |                       |           |                       |                                     |                                     |   |                |
| Ondertraverse     | 32.50    | 15.07                 |                       | 3.00      |                       | 22.61                               | 6.02                                | 0.27                                      | 2.66           |
| Boventraverse     | 43.80    | 17.36                 |                       | 2.53      |                       | 21.92                               | 6.19                                | 0.28                                      | 2.60           |

#### Properties tower sections transversal direction (side view, xz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 11.18    | 9.00                  | 5.79                  | 11.18     | 0.144                 | 82.66                               | 9.27                                | 0.11                                      | 3.34           |
| Eerste tussenstuk | 21.18    | 5.79                  | 4.48                  | 10.00     | 0.065                 | 51.36                               | 7.20                                | 0.14                                      | 3.21           |
| Tweede tussenstuk | 32.55    | 4.48                  | 3.00                  | 11.37     | 0.065                 | 42.55                               | 7.85                                | 0.18                                      | 3.00           |
| Bovenstuk 1       | 38.37    | 3.00                  | 2.62                  | 5.82      | 0.033                 | 16.35                               | 3.86                                | 0.24                                      | 2.78           |
| Bovenstuk 2       | 46.38    | 2.62                  | 2.00                  | 8.01      | 0.039                 | 18.49                               | 4.45                                | 0.24                                      | 2.76           |
| Topstuk           |          |                       |                       |           |                       |                                     |                                     |   |                |
| Ondertraverse     | 32.50    | 15.07                 |                       | 3.00      |                       | 22.61                               | 6.02                                | 0.27                                      | 2.66           |
| Boventraverse     | 43.80    | 17.36                 |                       | 2.53      |                       | 21.92                               | 6.19                                | 0.28                                      | 2.60           |

Note: Surface transverse direction is reduced in calculation.

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#### Wind surface feeders telecom installations

| Part              | A (m <sup>2</sup> /m) | Factor | Δh | A <sub>1</sub> |
|-------------------|-----------------------|--------|----|----------------|
| Broekstuk         |                       |        |    |                |
| Eerste tussenstuk |                       |        |    |                |
| Tweede tussenstuk |                       |        |    |                |
| Bovenstuk 1       |                       |        |    |                |
| Bovenstuk 2       |                       |        |    |                |

#### Input antennas

| Description  | A (m <sup>2</sup> ) | h (m) | C <sub>r</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. |                     |       |                    |

#### Tower section loads longitudinal (x-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 21.7                    | 18.4                    | 0.0                     | -18.4                   | 5.6                    | 121.5                    | 103.1                    | 0.0                      | -103.1                   |
| Eerste tussenstuk | 0.82                                   | 19.0                    | 16.1                    | 0.0                     | -16.1                   | 16.2                   | 307.0                    | 260.5                    | 0.0                      | -260.5                   |
| Tweede tussenstuk | 0.96                                   | 22.5                    | 19.1                    | 0.0                     | -19.1                   | 26.9                   | 605.8                    | 514.0                    | 0.0                      | -514.0                   |
| Bovenstuk 1       | 1.04                                   | 11.2                    | 9.5                     | 0.0                     | -9.5                    | 35.5                   | 395.4                    | 335.5                    | 0.0                      | -335.5                   |
| Bovenstuk 2       | 1.09                                   | 13.3                    | 11.3                    | 0.0                     | -11.3                   | 42.4                   | 565.7                    | 480.0                    | 0.0                      | -480.0                   |
| Topstuk           | 0.70                                   |                         |                         |                         |                         | 0.0                    |                          |                          |                          |                          |
| Ondertraverse     | 1.02                                   | 32.6                    | 19.4                    | 0.0                     | -19.4                   | 33.5                   | 1092.9                   | 649.1                    | 0.0                      | -649.1                   |
| Boventraverse     | 1.10                                   | 35.4                    | 21.0                    | 0.0                     | -21.0                   | 44.6                   | 1582.0                   | 939.6                    | 0.0                      | -939.6                   |
| <b>Totaal</b>     |  | <b>155.8</b>            | <b>114.9</b>            | <b>0.0</b>              | <b>-114.9</b>           |                        | <b>4670.1</b>            | <b>3281.8</b>            | <b>0.0</b>               | <b>-3281.8</b>           |

#### Tower section loads transversal (y-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 0.0                     | 18.4                    | 21.7                    | 18.4                    | 5.6                    | 0.0                      | 103.1                    | 121.5                    | 103.1                    |
| Eerste tussenstuk | 0.82                                   | 0.0                     | 16.1                    | 19.0                    | 16.1                    | 16.2                   | 0.0                      | 260.5                    | 307.0                    | 260.5                    |
| Tweede tussenstuk | 0.96                                   | 0.0                     | 19.1                    | 22.5                    | 19.1                    | 26.9                   | 0.0                      | 514.0                    | 605.8                    | 514.0                    |
| Bovenstuk 1       | 1.04                                   | 0.0                     | 9.5                     | 11.2                    | 9.5                     | 35.5                   | 0.0                      | 335.5                    | 395.4                    | 335.5                    |
| Bovenstuk 2       | 1.09                                   | 0.0                     | 11.3                    | 13.3                    | 11.3                    | 42.4                   | 0.0                      | 480.0                    | 565.7                    | 480.0                    |
| Topstuk           | 0.70                                   |                         |                         |                         |                         | 0.0                    |                          |                          |                          |                          |
| Ondertraverse     | 1.02                                   | 0.0                     | 19.4                    | 13.0                    | 19.4                    | 33.5                   | 0.0                      | 649.1                    | 437.1                    | 649.1                    |
| Boventraverse     | 1.10                                   | 0.0                     | 21.0                    | 14.2                    | 21.0                    | 44.6                   | 0.0                      | 939.6                    | 632.8                    | 939.6                    |
| <b>Total</b>      |  | <b>0.0</b>              | <b>114.9</b>            | <b>115.0</b>            | <b>114.9</b>            |                        | <b>0.0</b>               | <b>3281.8</b>            | <b>3065.2</b>            | <b>3281.8</b>            |

#### Resulting loads from mast construction incl. Antenna without conductors level foundation (char. Value)

| Load / wind direction | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|-----------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting  | 0                      | 0                      | 209                    | 0                       | 0                       | 0                       |
| Windrichting 0°       | 156                    | 0                      | 0                      | 0                       | 4670                    | 0                       |
| Windrichting 45°      | 115                    | 115                    | 0                      | 3282                    | 3282                    | 0                       |
| Windrichting 90°      | 0                      | 115                    | 0                      | 3065                    | 0                       | 0                       |
| Windrichting 135°     | -115                   | 115                    | 0                      | 3282                    | -3282                   | 0                       |

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### Intermediate results for conductor loads

#### Conductors back

| Circuit        | Geleider              | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|-----------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Circuit 2      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Bliksemdraad 1 | ACSR-26/7-242/39-HAWK | 21.8             | 281.1                   | 9.81       | 75000                     | 1.89E-05          |
| Bliksemdraad 2 | OPGW 226              | 21.7             | 264.0                   | 9.80       | 81000                     | 2.30E-05          |

#### Conductors ahead

| Circuit        | Geleider              | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|-----------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Circuit 2      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Bliksemdraad 1 | ACSR-26/7-242/39-HAWK | 21.8             | 281.1                   | 9.81       | 75000                     | 1.89E-05          |
| Bliksemdraad 2 | OPGW 226              | 21.7             | 264.0                   | 9.80       | 81000                     | 2.30E-05          |

#### Vertical load back

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Circuit 2      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Bliksemdraad 1 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Vertical load ahead

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Circuit 2      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Bliksemdraad 1 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Insulators

| Conductor | $G_{isolator}$<br>[kN] | Number | $F_{v,iso}$<br>[kN] | Length<br>[m] | Wind surf.<br>[m <sup>2</sup> ] | Wind heigth<br>[m] | Pressure<br>[kN/m <sup>2</sup> ] | Drag factor<br>[-] | $F_{h,iso}$<br>[kN] |
|-----------|------------------------|--------|---------------------|---------------|---------------------------------|--------------------|----------------------------------|--------------------|---------------------|
| 380ct1f1  | 5.50                   | 1      | 5.5                 | 4.5           | 2.4                             | 30.80              | 1.00                             | 1.2                | 2.87                |
| 380ct1f2  | 5.50                   | 1      | 5.5                 | 4.5           | 2.4                             | 30.80              | 1.00                             | 1.2                | 2.87                |
| 380ct1f3  | 5.50                   | 1      | 5.5                 | 4.5           | 2.4                             | 42.10              | 1.09                             | 1.2                | 3.13                |
| 380ct2f1  | 5.50                   | 1      | 5.5                 | 4.5           | 2.4                             | 30.80              | 1.00                             | 1.2                | 2.87                |
| 380ct2f2  | 5.50                   | 1      | 5.5                 | 4.5           | 2.4                             | 30.80              | 1.00                             | 1.2                | 2.87                |
| 380ct2f3  | 5.50                   | 1      | 5.5                 | 4.5           | 2.4                             | 42.10              | 1.09                             | 1.2                | 3.13                |
| bl1       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 44.25              | 1.10                             | 1.2                | 0.13                |
| bl2       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 44.25              | 1.10                             | 1.2                | 0.13                |

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**Wind load back**

| Conductor | Height |                      | G <sub>c_duars</sub> | G <sub>c_trek</sub> | C <sub>c</sub> | d <sub>additional</sub> | w <sub>y</sub> | w <sub>y,section</sub> | D <sub>ijs,additional</sub> | w <sub>y,ijs</sub> | w <sub>y,ijs,section</sub> |
|-----------|--------|----------------------|----------------------|---------------------|----------------|-------------------------|----------------|------------------------|-----------------------------|--------------------|----------------------------|
|           | wind   | Pressure             |                      |                     |                |                         |                |                        |                             |                    |                            |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]                  | [-]                 | [-]            | [mm]                    | [N/m]          | [N/m]                  | [mm]                        | [N/m]              | [N/m]                      |
| 380ct1f1  | 21.4   | 0.90                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.2           | 43.5                   | 47.2                        | 85.4               | 77.0                       |
| 380ct1f2  | 21.4   | 0.90                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.2           | 43.5                   | 47.2                        | 85.4               | 77.0                       |
| 380ct1f3  | 32.7   | 1.01                 | 0.60                 | 0.54                | 1.09           | 28.50                   | 56.1           | 50.5                   | 47.2                        | 102.5              | 92.3                       |
| 380ct2f1  | 21.4   | 0.90                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.2           | 43.5                   | 47.2                        | 85.4               | 77.0                       |
| 380ct2f2  | 21.4   | 0.90                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.2           | 43.5                   | 47.2                        | 85.4               | 77.0                       |
| 380ct2f3  | 32.7   | 1.01                 | 0.60                 | 0.54                | 1.09           | 28.50                   | 56.1           | 50.5                   | 47.2                        | 102.5              | 92.3                       |
| bl1       | 37.0   | 1.05                 | 0.61                 | 0.55                | 1.20           | 22.24                   | 16.9           | 15.2                   | 63.1                        | 48.1               | 43.3                       |
| bl2       | 37.0   | 1.05                 | 0.61                 | 0.55                | 1.20           | 22.13                   | 16.9           | 15.2                   | 63.0                        | 48.0               | 43.2                       |

**Wind load ahead**

| Conductor | Height |                      | G <sub>c_duars</sub> | G <sub>c_trek</sub> | C <sub>c</sub> | d <sub>additional</sub> | w <sub>y</sub> | w <sub>y,section</sub> | D <sub>ijs,additional</sub> | w <sub>y,ijs</sub> | w <sub>y,ijs,section</sub> |
|-----------|--------|----------------------|----------------------|---------------------|----------------|-------------------------|----------------|------------------------|-----------------------------|--------------------|----------------------------|
|           | wind   | Pressure             |                      |                     |                |                         |                |                        |                             |                    |                            |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]                  | [-]                 | [-]            | [mm]                    | [N/m]          | [N/m]                  | [mm]                        | [N/m]              | [N/m]                      |
| 380ct1f1  | 21.3   | 0.89                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.1           | 43.4                   | 47.2                        | 85.2               | 76.8                       |
| 380ct1f2  | 21.3   | 0.89                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.1           | 43.4                   | 47.2                        | 85.2               | 76.8                       |
| 380ct1f3  | 32.6   | 1.01                 | 0.60                 | 0.54                | 1.09           | 28.50                   | 56.0           | 50.5                   | 47.2                        | 102.3              | 92.1                       |
| 380ct2f1  | 21.3   | 0.89                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.1           | 43.4                   | 47.2                        | 85.2               | 76.8                       |
| 380ct2f2  | 21.3   | 0.89                 | 0.56                 | 0.51                | 1.12           | 28.50                   | 48.1           | 43.4                   | 47.2                        | 85.2               | 76.8                       |
| 380ct2f3  | 32.6   | 1.01                 | 0.60                 | 0.54                | 1.09           | 28.50                   | 56.0           | 50.5                   | 47.2                        | 102.3              | 92.1                       |
| bl1       | 36.9   | 1.05                 | 0.61                 | 0.54                | 1.20           | 22.24                   | 16.9           | 15.2                   | 63.1                        | 48.0               | 43.2                       |
| bl2       | 36.9   | 1.05                 | 0.61                 | 0.54                | 1.20           | 22.13                   | 16.8           | 15.2                   | 63.0                        | 48.0               | 43.2                       |

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**Conductor loads** Auteur: TBR  
Versie: v11.8

**Starting points**  
 Consequence class Afkeur CC2-0  
 Reference period 30 jaar

| ULS (strength)  |                            | NEN-EN50341-2-15:2019 |              |                  |            |          |          |                     |
|---|----------------------------|-----------------------|--------------|------------------|------------|----------|----------|---------------------|
| Load case   | description                | Temp<br>°C            | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|   |                            |                       | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a  | Wind                       | 10°                   | 1.05         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9  | Wind 0,9Gk only tower      | 10°                   | 0.90         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9_0,9  | Wind 0,9Gk conductors too  | 10°                   | 0.90         | 0.90             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 3   | Wind+ice                   | -5°                   | 1.05         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 3_0,9   | Wind+ice 0,9Gk             | -5°                   | 0.90         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 4   | Cold+wind                  | -20°                  | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 4_0,9   | Cold+wind 0,9Gk            | -20°                  | 0.90         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 5a  | Torsional loads            | 10°                   | 1.00         | 1.00             | 1.00       | 0.00     | 0.00     | 1.0                 |
| ULS 5b  | Longitudinal loads         | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| ULS 6   | Construction + maintenance | 5°                    | 1.05         | 1.05             | 1.20       | 0.22     | 0.00     | 0.0                 |
| ULS 6_0,9   | Construction + maintenance | 5°                    | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 7   | Permanent                  | 10°                   | 1.15         | 1.15             | 0.00       | 0.00     | 0.00     | 0.0                 |
| ULS 8   | Special                    | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| <b>SPLS (strength, for angle towers: absence of conductors)</b> |                            |                       | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
|   |                            |                       | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SPLS 1a   | Wind                       | 10°                   | 1.05         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9   | Wind 0,9                   | 10°                   | 0.90         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9_0,9   | Wind 0,9                   | 10°                   | 0.90         | 0.90             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 3  | Wind+ice                   | -5°                   | 1.05         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 3_0,9  | Wind+ice 0,9               | -5°                   | 0.90         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 4  | Cold+wind                  | -20°                  | 1.05         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 4_0,9  | Cold+wind 0,9              | -20°                  | 0.90         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 6  | Maintenance                | 5°                    | 1.05         | 1.05             | 1.2        | 0.24     | 0.0      | 0.0                 |
| SPLS 6_0,9  | Maintenance                | 5°                    | 1.05         | 1.05             | 0.0        | 0.24     | 0.0      | 0.0                 |
| <b>SLS (deformations, fatigue, EDS)</b>                         |                            |                       | $G_k$        |                  | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SLS 1a  | Wind                       | 10°                   | 1.00         | 1.00             | 0.0        | 0.94     | 0.0      | 0.0                 |
| SLS 3   | Wind+ice                   | -5°                   | 1.00         | 1.00             | 0.0        | 0.28     | 0.88     | 0.0                 |
| SLS 4   | Wind                       | -20°                  | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 6   | Maintenance                | 5°                    | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 7   | EDS, no wind               | 10°                   | 1.00         | 1.00             | 0.0        | 0.00     | 0.0      | 0.0                 |

Number of wind directions 4  
 Number of load combinations for ULS 43  
 Number of load combinations for SPLS 0  
 Number of load combinations for SLS 11  
 Number of concentrated loads 432

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**Summary table - Conductor loads**

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

\*For Steunmast the special combination SPLS 6 don't apply.

**Maximum values for back and ahead span**

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -41.2         | 41.2          | 3.9           | 3.9           | 5.6           | 5.7           |
| 380ct1f1 | -106.0        | 106.0         | 12.9          | 13.0          | 16.6          | 16.0          |
| 380ct1f2 | -106.0        | 106.0         | 12.9          | 13.0          | 16.6          | 16.0          |
| 380ct1f3 | -107.9        | 107.9         | 14.7          | 14.8          | 16.6          | 16.0          |
| 380ct2f1 | -106.0        | 106.0         | 12.9          | 13.0          | 16.6          | 16.0          |
| 380ct2f2 | -106.0        | 106.0         | 12.9          | 13.0          | 16.6          | 16.0          |
| 380ct2f3 | -107.9        | 107.9         | 14.7          | 14.8          | 16.6          | 16.0          |
| bl2      | -41.6         | 41.6          | 3.9           | 3.9           | 5.6           | 5.7           |

**Min. Weight span (m)**

Weight spar Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 344.3  | 344.3 | 344.3 |
| 380ct1f1 | 344.3  | 344.3 | 344.3 |
| 380ct1f2 | 344.3  | 344.3 | 344.3 |
| 380ct1f3 | 344.3  | 344.3 | 344.3 |
| 380ct2f1 | 344.3  | 344.3 | 344.3 |
| 380ct2f2 | 344.3  | 344.3 | 344.3 |
| 380ct2f3 | 344.3  | 344.3 | 344.3 |
| bl2      | 344.3  | 344.3 | 344.3 |

**Max. Weight span (m)**

Weight spar Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 344.3  | 344.3 |
| 380ct1f1 | 344.3  | 344.3 |
| 380ct1f2 | 344.3  | 344.3 |
| 380ct1f3 | 344.3  | 344.3 |
| 380ct2f1 | 344.3  | 344.3 |
| 380ct2f2 | 344.3  | 344.3 |
| 380ct2f3 | 344.3  | 344.3 |
| bl2      | 344.3  | 344.3 |

Envelop of weight span over all combinations (incl. 0,9 combinations)

For all conductors

|                  | Wind / Weight span ratio |
|------------------|--------------------------|
| Max. weight span | 344.3 m 1.000 -          |
| Min. weight span | 344.3 m 1.000 -          |

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**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider | Fx   | Fy   | Fz   | Ft_ba  | Ft_ah |
|----------|------|------|------|--------|-------|
|          | [kN] | [kN] | [kN] | [kN]   | [kN]  |
| bl1      | 20.6 | 7.8  | 11.3 | -41.3  | 41.3  |
| 380ct1f1 | 50.1 | 25.9 | 31.8 | -106.1 | 106.1 |
| 380ct1f2 | 50.1 | 25.9 | 31.8 | -106.1 | 106.1 |
| 380ct1f3 | 50.1 | 29.5 | 31.8 | -108.1 | 108.1 |
| 380ct2f1 | 50.1 | 25.9 | 31.8 | -106.1 | 106.1 |
| 380ct2f2 | 50.1 | 25.9 | 31.8 | -106.1 | 106.1 |
| 380ct2f3 | 50.1 | 29.5 | 31.8 | -108.1 | 108.1 |
| bl2      | 20.6 | 7.8  | 11.3 | -41.7  | 41.6  |

**EDS-loads conductor**

| Geleider | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|----------|------|------|------|-------|-------|
|          | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1      | 0.0  | 0.6  | 3.5  | -13.8 | 13.8  |
| 380ct1f1 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct1f2 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct1f3 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct2f1 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct2f2 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct2f3 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| bl2      | 0.0  | 0.6  | 3.5  | -13.7 | 13.7  |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4 bl1            | 1.8   | 1.8   |
| 380ct1f1             | 10.6  | 10.6  |
| 380ct1f2             | 10.6  | 10.6  |
| 380ct1f3             | 10.6  | 10.6  |
| 380ct2f1             | 10.6  | 10.6  |
| 380ct2f2             | 10.6  | 10.6  |
| 380ct2f3             | 10.6  | 10.6  |
| bl2                  | 1.8   | 1.8   |



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**ULS foundation loads for LC 1 and 3, wind perpendicular to the line or bisector and EDS, from conductors**

| Combination   | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90     |             | 0             | 178           | 141           | 6643           | 0              | 0              |
| ULS 1a_0,9_90 |             | 0             | 178           | 141           | 6643           | 0              | 0              |
| ULS 3_90      |             | 0             | 114           | 214           | 4289           | 0              | 0              |
| ULS 3_0,9_90  |             | 0             | 114           | 214           | 4289           | 0              | 0              |
| SLS 7         |             | 0             | 19            | 134           | 700            | 0              | 0              |

**ULS foundation loads, LC 1 and 3, wind perpendicular to the line or bisector and EDS, total conductors and tower**

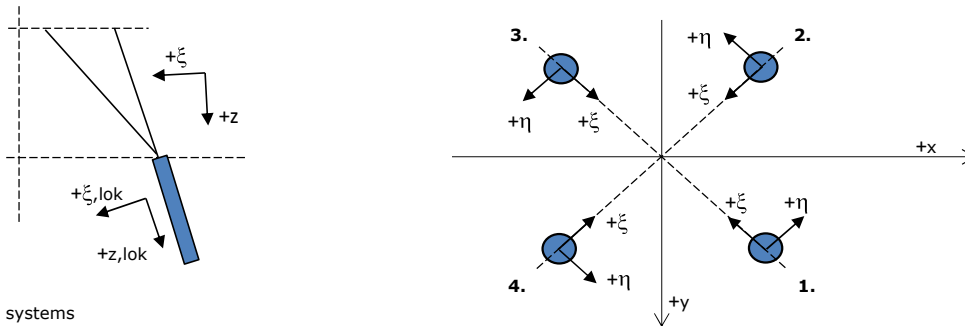
| Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90   | 0             | 307           | 360           | 10066          | 0              | 0              |
| ULS 3_90    | 0             | 153           | 433           | 5316           | 0              | 0              |
| SLS 7       | 0             | 19            | 343           | 700            | 0              | 0              |

**Foundation loads, selection of load combinations based on greatest value**

| Combination      | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90        | 0             | 307           | 360           | <b>10066</b>   | 0              | 0              |
| ULS 1a_0,9_0,9_0 | 179           | 17            | 309           | 638            | <b>5409</b>    | 0              |
| ULS 5a Ba 10     | 50            | 17            | 343           | 768            | 1632           | <b>-802</b>    |
| ULS 1a_135       | -132          | 230           | 360           | <b>7446</b>    | <b>-3805</b>   | 0              |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



**Maximum compression load**

| Index | Combination  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_45    | 127           | 114           | <b>715</b>    | 9                | -170            | -25                   | 730                 |
| 2     | ULS 8 Ah     | 48            | -67           | <b>357</b>    | 14               | -81             | -9                    | 364                 |
| 3     | ULS 5a Ah 22 | -6            | -52           | <b>179</b>    | -33              | -41             | -4                    | 183                 |
| 4     | ULS 1a_135   | -127          | 114           | <b>715</b>    | -9               | -170            | -25                   | 730                 |

**Maximum tension load**

| Index | Combination        | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 5a Ah 22       | -8            | 15            | <b>-7</b>     | -17              | -5              | -6                    | -7                  |
| 2     | ULS 1a_0,9_0,9_135 | -95           | 82            | <b>-544</b>   | 9                | 125             | 15                    | -555                |
| 3     | ULS 1a_0,9_0,9_45  | 95            | 82            | <b>-543</b>   | -9               | 125             | 15                    | -555                |
| 4     | ULS 1a_0,9_0,9_0   | 24            | -37           | <b>-188</b>   | -10              | 43              | 5                     | -192                |

**Maximum torsional load (positive)**

| Index | Combination  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 5a Ah 10 | 34            | -19           | 38            | <b>37</b>        | -11             | -3                    | 39                  |
| 2     | ULS 5a Ba 20 | 1             | -51           | 148           | <b>35</b>        | -37             | -7                    | 151                 |
| 3     | ULS 5a Ba 20 | -20           | 27            | -34           | <b>34</b>        | 5               | -2                    | -34                 |
| 4     | ULS 5a Ah 10 | -14           | 60            | 219           | <b>32</b>        | -52             | -8                    | 224                 |

**Maximum torsional load (negative)**

| Index | Combination  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 5a Ba 10 | 14            | 60            | 219           | <b>-32</b>       | -52             | -8                    | 224                 |
| 2     | ULS 5a Ah 20 | 20            | 27            | -34           | <b>-34</b>       | 5               | -2                    | -34                 |
| 3     | ULS 5a Ah 20 | -1            | -51           | 148           | <b>-35</b>       | -37             | -7                    | 151                 |
| 4     | ULS 5a Ba 10 | -34           | -19           | 38            | <b>-37</b>       | -11             | -3                    | 39                  |

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#### Combination Ftensile+Fhor

| Index | Combination        | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | ULS 5a Ah 12       | 28                     | -20                    | <b>4</b>               | <b>34</b>              | -6                     | -5                         | 4                          |
| 2     | ULS 1a_0,9_0,9_135 | -95                    | 82                     | <b>-544</b>            | <b>9</b>               | 125                    | 15                         | -555                       |
| 3     | ULS 1a_0,9_0,9_45  | 95                     | 82                     | <b>-543</b>            | <b>-9</b>              | 125                    | 15                         | -555                       |
| 4     | ULS 1a_0,9_0,9_0   | 24                     | -37                    | <b>-188</b>            | <b>-10</b>             | 43                     | 5                          | -192                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 23                     | 21                     | 125                    | 2                      | -31                    | -6                         | 127                        |
| 2     | SLS 7       | 9                      | -11                    | 47                     | 2                      | -14                    | -5                         | 48                         |
| 3     | SLS 7       | -9                     | -11                    | 47                     | -2                     | -14                    | -5                         | 48                         |
| 4     | SLS 7       | -23                    | 21                     | 125                    | -2                     | -31                    | -6                         | 127                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination        | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | ULS 1a_135         | -127                   | 114                    | <b>715</b>             | -9                     | -170                   | -25                        | 730                        |
| Max. tension         | ULS 1a_0,9_0,9_135 | -95                    | 82                     | <b>-544</b>            | 9                      | 125                    | 15                         | -555                       |
| Max. pos. torsie     | ULS 5a Ah 10       | 34                     | -19                    | 38                     | <b>37</b>              | -11                    | -3                         | 39                         |
| Max. neg. torsie     | ULS 5a Ba 10       | -34                    | -19                    | 38                     | <b>-37</b>             | -11                    | -3                         | 39                         |
| Comb. tension+torsie | ULS 1a_0,9_0,9_135 | -95                    | 82                     | <b>-544</b>            | <b>9</b>               | 125                    | 15                         | -555                       |

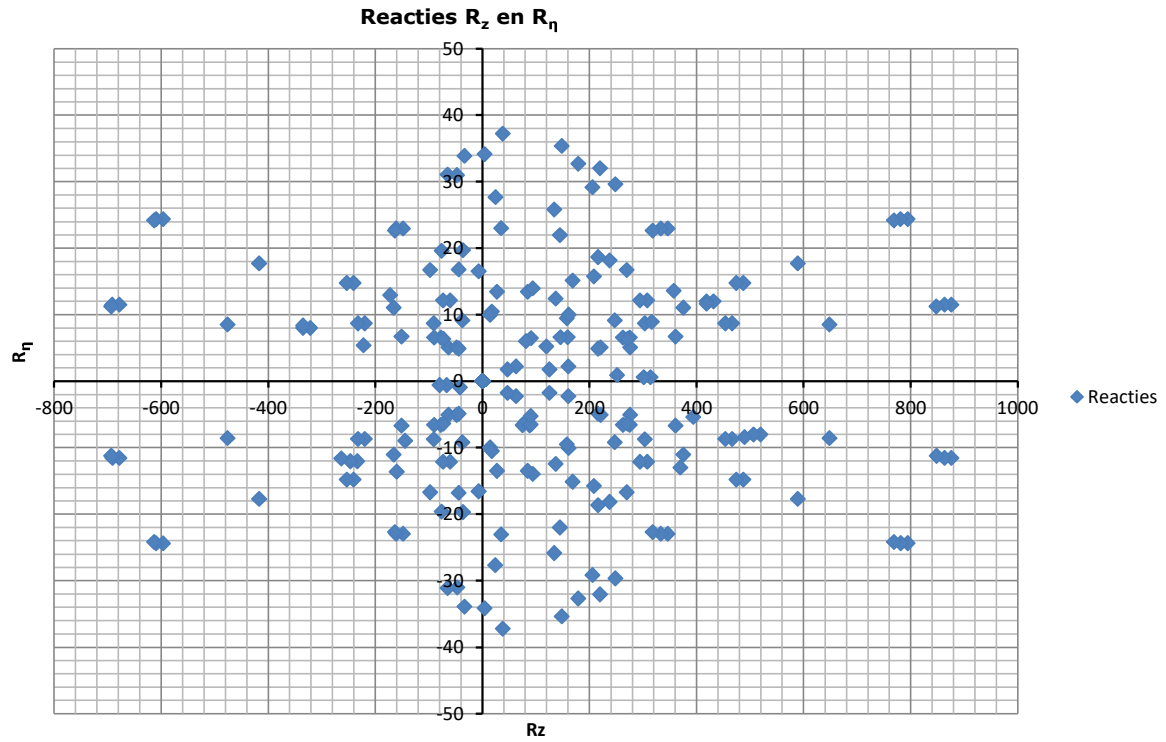
#### Maximum tension load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 23                     | 21                     | <b>125</b>             | 2                      | -31                    | -6                         | 127                        |
| 2     | SLS 1a_135  | -78                    | 66                     | <b>-446</b>            | 8                      | 102                    | 11                         | -455                       |
| 3     | SLS 1a_45   | 78                     | 66                     | <b>-446</b>            | -8                     | 102                    | 11                         | -455                       |
| 4     | SLS 1a_0    | 15                     | -27                    | <b>-129</b>            | -9                     | 29                     | 3                          | -132                       |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_45   | 110                    | 98                     | <b>618</b>             | 8                      | -147                   | -22                        | 631                        |
| 2     | SLS 1a_0    | 47                     | -59                    | <b>301</b>             | 9                      | -74                    | -13                        | 307                        |
| 3     | SLS 7       | -9                     | -11                    | <b>47</b>              | -2                     | -14                    | -5                         | 48                         |
| 4     | SLS 1a_135  | -110                   | 98                     | <b>618</b>             | -8                     | -147                   | -22                        | 631                        |

Project: GT-RL380  
Tower: HS  
Number: 26



Project: GT-RL380  
 Tower: HS  
 Number: 26

**Conductor loads** Auteur: TBR  
Versie: v11.8

**Starting points**  
 Consequence class Verbouw CC2  
 Reference period 50 jaar

| <b>ULS</b> (strength)   |                            | <b>NEN-EN50341-2-15:2019</b> |              |                  |            |          | $\gamma_a$ |          |       |
|---|----------------------------|------------------------------|--------------|------------------|------------|----------|------------|----------|-------|
| Load case   | description                | Temp °C                      | $\gamma_G$   | $\gamma_G$       | $\gamma_Q$ | $Q_{pk}$ | $Q_{wk}$   | $Q_{ik}$ | $A_k$ |
|   |                            |                              | $G_{k,mast}$ | $G_{k,geleider}$ |            |          |            |          |       |
| ULS 1a  | Wind                       | 10°                          | 1.15         | 1.15             | 0.00       | 1.40     | 0.00       | 0.00     | 0.0   |
| ULS 1a_0,9  | Wind 0,9Gk only tower      | 10°                          | 0.90         | 1.15             | 0.00       | 1.40     | 0.00       | 0.00     | 0.0   |
| ULS 1a_0,9_0,9  | Wind 0,9Gk conductors too  | 10°                          | 0.90         | 0.90             | 0.00       | 1.40     | 0.00       | 0.00     | 0.0   |
| ULS 3   | Wind+ice                   | -5°                          | 1.15         | 1.15             | 0.00       | 0.42     | 1.30       | 0.00     | 0.0   |
| ULS 3_0,9   | Wind+ice 0,9Gk             | -5°                          | 0.90         | 1.15             | 0.00       | 0.42     | 1.30       | 0.00     | 0.0   |
| ULS 4   | Cold+wind                  | -20°                         | 1.15         | 1.15             | 0.00       | 0.28     | 0.00       | 0.00     | 0.0   |
| ULS 4_0,9   | Cold+wind 0,9Gk            | -20°                         | 0.90         | 1.15             | 0.00       | 0.28     | 0.00       | 0.00     | 0.0   |
| ULS 5a  | Torsional loads            | 10°                          | 1.00         | 1.00             | 1.00       | 0.00     | 0.00       | 0.00     | 1.0   |
| ULS 5b  | Longitudinal loads         | 10°                          | 1.00         | 1.00             | 0.00       | 0.00     | 0.00       | 0.00     | 1.0   |
| ULS 6   | Construction + maintenance | 5°                           | 1.15         | 1.15             | 1.30       | 0.28     | 0.00       | 0.00     | 0.0   |
| ULS 6_0,9   | Construction + maintenance | 5°                           | 1.15         | 1.15             | 0.00       | 0.28     | 0.00       | 0.00     | 0.0   |
| ULS 7   | Permanent                  | 10°                          | 1.30         | 1.30             | 0.00       | 0.00     | 0.00       | 0.00     | 0.0   |
| ULS 8   | Special                    | 10°                          | 1.00         | 1.00             | 0.00       | 0.00     | 0.00       | 0.00     | 1.0   |
| <b>SPLS</b> (strength, for angle towers: absence of conductors) |                            |                              |              | $\gamma_G$       | $\gamma_Q$ |          |            |          |       |
|   |                            |                              |              | $G_k$            |            | $Q_{pk}$ | $Q_{wk}$   | $Q_{ik}$ | $A_k$ |
| SPLS 1a   | Wind                       | 10°                          | 1.15         | 1.15             | 0.0        | 0.78     | 0.00       | 0.00     | 0.0   |
| SPLS 1a_0,9   | Wind 0,9                   | 10°                          | 0.90         | 1.15             | 0.0        | 0.78     | 0.00       | 0.00     | 0.0   |
| SPLS 1a_0,9_0,9   | Wind 0,9                   | 10°                          | 0.90         | 0.90             | 0.0        | 0.78     | 0.00       | 0.00     | 0.0   |
| SPLS 3  | Wind+ice                   | -5°                          | 1.15         | 1.15             | 0.0        | 0.36     | 0.34       | 0.00     | 0.0   |
| SPLS 3_0,9  | Wind+ice 0,9               | -5°                          | 0.90         | 1.15             | 0.0        | 0.36     | 0.34       | 0.00     | 0.0   |
| SPLS 4  | Cold+wind                  | -20°                         | 1.15         | 1.15             | 0.0        | 0.24     | 0.00       | 0.00     | 0.0   |
| SPLS 4_0,9  | Cold+wind 0,9              | -20°                         | 0.90         | 1.15             | 0.0        | 0.24     | 0.00       | 0.00     | 0.0   |
| SPLS 6  | Maintenance                | 5°                           | 1.15         | 1.15             | 1.2        | 0.24     | 0.0        | 0.00     | 0.0   |
| SPLS 6_0,9  | Maintenance                | 5°                           | 1.15         | 1.15             | 0.0        | 0.24     | 0.0        | 0.00     | 0.0   |
| <b>SLS</b> (deformations, fatigue, EDS)                         |                            |                              |              | $G_k$            |            | $Q_{pk}$ | $Q_{wk}$   | $Q_{ik}$ | $A_k$ |
| SLS 1a  | Wind                       | 10°                          | 1.00         | 1.00             | 0.0        | 1.00     | 0.0        | 0.00     | 0.0   |
| SLS 3   | Wind+ice                   | -5°                          | 1.00         | 1.00             | 0.0        | 0.30     | 1.00       | 0.00     | 0.0   |
| SLS 4   | Wind                       | -20°                         | 1.00         | 1.00             | 0.0        | 0.20     | 0.0        | 0.00     | 0.0   |
| SLS 6   | Maintenance                | 5°                           | 1.00         | 1.00             | 0.0        | 0.20     | 0.0        | 0.00     | 0.0   |
| SLS 7   | EDS, no wind               | 10°                          | 1.00         | 1.00             | 0.0        | 0.00     | 0.0        | 0.00     | 0.0   |

Number of wind directions 4  
 Number of load combinations for ULS 43  
 Number of load combinations for SPLS 0  
 Number of load combinations for SLS 11  
 Number of concentrated loads 432

Project: GT-RLL380  
 Tower: HS  
 Number: 26

**Summary table - Conductor loads**

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

\*For Steunmast the special combination SPLS 6 don't apply.

**Maximum values for back and ahead span**

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -50.2         | 50.2          | 4.8           | 4.9           | 7.3           | 7.4           |
| 380ct1f1 | -122.4        | 122.4         | 16.0          | 16.0          | 18.5          | 18.7          |
| 380ct1f2 | -122.4        | 122.4         | 16.0          | 16.0          | 18.5          | 18.7          |
| 380ct1f3 | -124.8        | 124.8         | 18.2          | 18.3          | 18.5          | 18.7          |
| 380ct2f1 | -122.4        | 122.4         | 16.0          | 16.0          | 18.5          | 18.7          |
| 380ct2f2 | -122.4        | 122.4         | 16.0          | 16.0          | 18.5          | 18.7          |
| 380ct2f3 | -124.8        | 124.8         | 18.2          | 18.3          | 18.5          | 18.7          |
| bl2      | -50.6         | 50.6          | 4.8           | 4.9           | 7.3           | 7.4           |

**Min. Weight span (m)**

Weight spar Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 344.3  | 344.3 | 344.3 |
| 380ct1f1 | 344.3  | 344.3 | 344.3 |
| 380ct1f2 | 344.3  | 344.3 | 344.3 |
| 380ct1f3 | 344.3  | 344.3 | 344.3 |
| 380ct2f1 | 344.3  | 344.3 | 344.3 |
| 380ct2f2 | 344.3  | 344.3 | 344.3 |
| 380ct2f3 | 344.3  | 344.3 | 344.3 |
| bl2      | 344.3  | 344.3 | 344.3 |

**Max. Weight span (m)**

Weight spar Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 344.3  | 344.3 |
| 380ct1f1 | 344.3  | 344.3 |
| 380ct1f2 | 344.3  | 344.3 |
| 380ct1f3 | 344.3  | 344.3 |
| 380ct2f1 | 344.3  | 344.3 |
| 380ct2f2 | 344.3  | 344.3 |
| 380ct2f3 | 344.3  | 344.3 |
| bl2      | 344.3  | 344.3 |

Envelop of weight span over all combinations (incl. 0,9 combinations)

For all conductors

|                  | Wind / Weight span ratio |
|------------------|--------------------------|
| Max. weight span | 344.3 m<br>1.000 -       |
| Min. weight span | 344.3 m<br>1.000 -       |

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**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider | Fx   | Fy   | Fz   | Ft_ba  | Ft_ah |
|----------|------|------|------|--------|-------|
|          | [kN] | [kN] | [kN] | [kN]   | [kN]  |
| bl1      | 20.6 | 9.7  | 14.7 | -50.3  | 50.3  |
| 380ct1f1 | 50.1 | 32.0 | 37.2 | -122.6 | 122.6 |
| 380ct1f2 | 50.1 | 32.0 | 37.2 | -122.6 | 122.6 |
| 380ct1f3 | 50.1 | 36.6 | 37.2 | -125.0 | 125.0 |
| 380ct2f1 | 50.1 | 32.0 | 37.2 | -122.6 | 122.6 |
| 380ct2f2 | 50.1 | 32.0 | 37.2 | -122.6 | 122.6 |
| 380ct2f3 | 50.1 | 36.6 | 37.2 | -125.0 | 125.0 |
| bl2      | 20.6 | 9.7  | 14.7 | -50.7  | 50.7  |

**EDS-loads conductor**

| Geleider | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|----------|------|------|------|-------|-------|
|          | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1      | 0.0  | 0.6  | 3.5  | -13.8 | 13.8  |
| 380ct1f1 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct1f2 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct1f3 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct2f1 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct2f2 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| 380ct2f3 | 0.0  | 3.0  | 21.2 | -62.7 | 62.7  |
| bl2      | 0.0  | 0.6  | 3.5  | -13.7 | 13.7  |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4      bl1       | 1.8   | 1.8   |
| 380ct1f1             | 10.6  | 10.6  |
| 380ct1f2             | 10.6  | 10.6  |
| 380ct1f3             | 10.6  | 10.6  |
| 380ct2f1             | 10.6  | 10.6  |
| 380ct2f2             | 10.6  | 10.6  |
| 380ct2f3             | 10.6  | 10.6  |
| bl2                  | 1.8   | 1.8   |

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**ULS foundation loads for LC 1 and 3, wind perpendicular to the line or bisector and EDS, from conductors**

| Combination   | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90     |             | 0             | 221           | 154           | 8224           | -1             | 0              |
| ULS 1a_0,9_90 |             | 0             | 221           | 154           | 8224           | -1             | 0              |
| ULS 3_90      |             | 0             | 140           | 253           | 5264           | 0              | 0              |
| ULS 3_0,9_90  |             | 0             | 140           | 253           | 5264           | 0              | 0              |
| SLS 7         |             | 0             | 19            | 134           | 700            | 0              | 0              |

**ULS foundation loads, LC 1 and 3, wind perpendicular to the line or bisector and EDS, total conductors and tower**

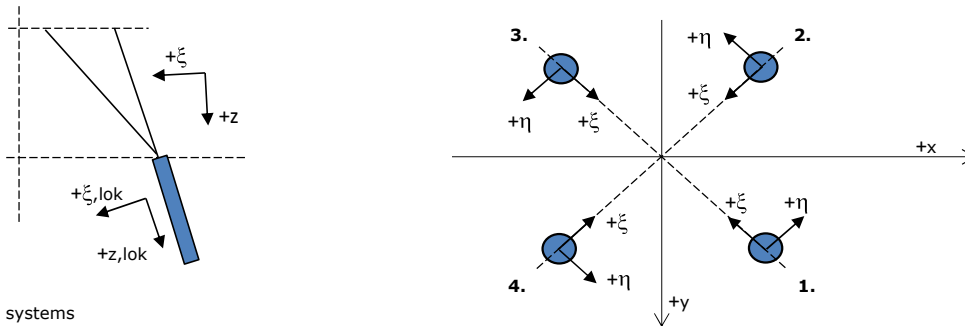
| Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90   | 0             | 382           | 395           | 12516          | -1             | 0              |
| ULS 3_90    | 0             | 188           | 493           | 6551           | 0              | 0              |
| SLS 7       | 0             | 19            | 343           | 700            | 0              | 0              |

**Foundation loads, selection of load combinations based on greatest value**

| Combination  | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|--------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90    | 0             | 382           | 395           | <b>12516</b>   | -1             | 0              |
| ULS 1a_0     | 225           | 21            | 395           | 791            | <b>6781</b>    | 0              |
| ULS 5a Ba 10 | 50            | 17            | 343           | 768            | 1632           | <b>-802</b>    |
| ULS 1a_135   | -166          | 285           | 395           | <b>9221</b>    | <b>-4770</b>   | 0              |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



Axis systems

**Maximum compression load**

| Index | Combination  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_45    | 155           | 139           | <b>876</b>    | 12               | -208            | -30                   | 894                 |
| 2     | ULS 1a_0     | 66            | -83           | <b>431</b>    | 12               | -106            | -18                   | 440                 |
| 3     | ULS 5a Ah 22 | -6            | -52           | <b>179</b>    | -33              | -41             | -4                    | 183                 |
| 4     | ULS 1a_135   | -155          | 139           | <b>876</b>    | -12              | -208            | -30                   | 894                 |

**Maximum tension load**

| Index | Combination        | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 5a Ah 22       | -8            | 15            | <b>-7</b>     | -17              | -5              | -6                    | -7                  |
| 2     | ULS 1a_0,9_0,9_135 | -121          | 106           | <b>-693</b>   | 11               | 160             | 20                    | -708                |
| 3     | ULS 1a_0,9_0,9_45  | 121           | 106           | <b>-693</b>   | -11              | 160             | 20                    | -707                |
| 4     | ULS 1a_0,9_0,9_0   | 35            | -52           | <b>-264</b>   | -12              | 61              | 8                     | -269                |

**Maximum torsional load (positive)**

| Index | Combination  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 5a Ah 10 | 34            | -19           | 38            | <b>37</b>        | -11             | -3                    | 39                  |
| 2     | ULS 5a Ba 20 | 1             | -51           | 148           | <b>35</b>        | -37             | -7                    | 151                 |
| 3     | ULS 5a Ba 20 | -20           | 27            | -34           | <b>34</b>        | 5               | -2                    | -34                 |
| 4     | ULS 5a Ah 10 | -14           | 60            | 219           | <b>32</b>        | -52             | -8                    | 224                 |

**Maximum torsional load (negative)**

| Index | Combination  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 5a Ba 10 | 14            | 60            | 219           | <b>-32</b>       | -52             | -8                    | 224                 |
| 2     | ULS 5a Ah 20 | 20            | 27            | -34           | <b>-34</b>       | 5               | -2                    | -34                 |
| 3     | ULS 5a Ah 20 | -1            | -51           | 148           | <b>-35</b>       | -37             | -7                    | 151                 |
| 4     | ULS 5a Ba 10 | -34           | -19           | 38            | <b>-37</b>       | -11             | -3                    | 39                  |

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#### Combination Ftensile+Fhor

| Index | Combination        | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | ULS 5a Ah 12       | 28                     | -20                    | <b>4</b>               | <b>34</b>              | -6                     | -5                         | 4                          |
| 2     | ULS 1a_0,9_0,9_135 | -121                   | 106                    | <b>-693</b>            | <b>11</b>              | 160                    | 20                         | -708                       |
| 3     | ULS 1a_0,9_0,9_45  | 121                    | 106                    | <b>-693</b>            | <b>-11</b>             | 160                    | 20                         | -707                       |
| 4     | ULS 1a_0,9_0,9_0   | 35                     | -52                    | <b>-264</b>            | <b>-12</b>             | 61                     | 8                          | -269                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 23                     | 21                     | 125                    | 2                      | -31                    | -6                         | 127                        |
| 2     | SLS 7       | 9                      | -11                    | 47                     | 2                      | -14                    | -5                         | 48                         |
| 3     | SLS 7       | -9                     | -11                    | 47                     | -2                     | -14                    | -5                         | 48                         |
| 4     | SLS 7       | -23                    | 21                     | 125                    | -2                     | -31                    | -6                         | 127                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination        | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | ULS 1a_135         | -155                   | 139                    | <b>876</b>             | -12                    | -208                   | -30                        | 894                        |
| Max. tension         | ULS 1a_0,9_0,9_135 | -121                   | 106                    | <b>-693</b>            | 11                     | 160                    | 20                         | -708                       |
| Max. pos. torsie     | ULS 5a Ah 10       | 34                     | -19                    | 38                     | <b>37</b>              | -11                    | -3                         | 39                         |
| Max. neg. torsie     | ULS 5a Ba 10       | -34                    | -19                    | 38                     | <b>-37</b>             | -11                    | -3                         | 39                         |
| Comb. tension+torsie | ULS 1a_0,9_0,9_135 | -121                   | 106                    | <b>-693</b>            | <b>11</b>              | 160                    | 20                         | -708                       |

#### Maximum tension load - SLS

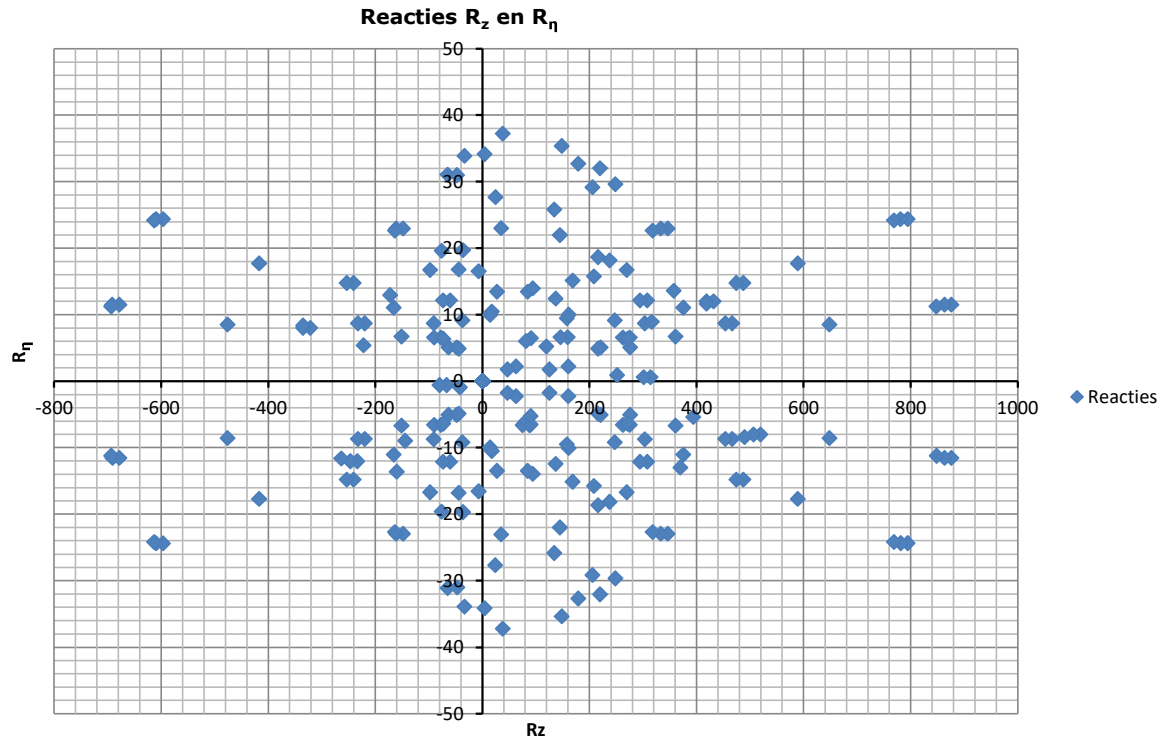
| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 23                     | 21                     | <b>125</b>             | 2                      | -31                    | -6                         | 127                        |
| 2     | SLS 1a_135  | -83                    | 71                     | <b>-476</b>            | 9                      | 109                    | 12                         | -486                       |
| 3     | SLS 1a_45   | 83                     | 71                     | <b>-476</b>            | -9                     | 109                    | 12                         | -486                       |
| 4     | SLS 1a_0    | 17                     | -29                    | <b>-144</b>            | -9                     | 33                     | 3                          | -147                       |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_45   | 115                    | 103                    | <b>648</b>             | 9                      | -154                   | -23                        | 661                        |
| 2     | SLS 1a_0    | 49                     | -62                    | <b>316</b>             | 9                      | -78                    | -14                        | 322                        |
| 3     | SLS 7       | -9                     | -11                    | <b>47</b>              | -2                     | -14                    | -5                         | 48                         |
| 4     | SLS 1a_135  | -115                   | 103                    | <b>648</b>             | -9                     | -154                   | -23                        | 661                        |



Project: GT-RL380  
Tower: HS  
Number: 26





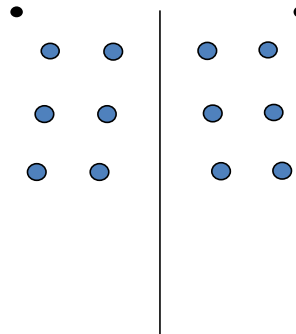
Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

Auteur: TBR  
 Versie: v11.8

### Conductor loads

#### General

Description HC+0  
 Tower type Hoekmast  
 Number of circuits 2  
 Configuration 2-circuit-donau  
 Number of earth wires 2



Configuratie geleiders

#### Starting points

Norm NEN-EN50341-2-15:2019  
 Consequence class CC2-0  
 Reliability level initial Afkeur CC2-0  
 Reference period initial 30 jaar  
 Consequence class modified CC2  
 Reliability level modified Verbouw  
 Reference period modified 50 jaar  
 Wind zone III  
 Wind speed (m/s) 24.5 m/s  
 Terrain category II  
 Reduction factor  $c_{dir}$  1.00  
 Ice region phase conductor B  
 Ice region earth conductor A

#### Conductors back

| Description    | Voltage | Conductor Back        | Bundle Ba | Ice region | Additional weight | Additional diameter | Catenary $P_{back}$ |
|----------------|---------|-----------------------|-----------|------------|-------------------|---------------------|---------------------|
| Circuit 1      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                |
| Circuit 2      | 380 kV  | St/Al 48/7-423/37-SEP | 3         | B          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 1 |         | ACSR-26/7-242/39-HAWK | 1         | A          | 2 %               | 2 %                 | 1375                |
| Bliksemdraad 2 |         | OPGW 226              | 1         | A          | 2 %               | 2 %                 | 1375                |

#### Conductors ahead

| Description    | Voltage | Conductor Ahead        | Bundle Ah | Ice region | Additional weight | Additional diameter | Catenary $P_{ahead}$ |
|----------------|---------|------------------------|-----------|------------|-------------------|---------------------|----------------------|
| Circuit 1      | 380 kV  | ACCC-Warsaw            | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Circuit 2      | 380 kV  | ACCC-Warsaw            | 3         | B          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 1 |         | AACSR 241-AL3-39-A20SA | 1         | A          | 2 %               | 2 %                 | 1375                 |
| Bliksemdraad 2 |         | OPGW AFL-226/38        | 1         | A          | 2 %               | 2 %                 | 1375                 |

#### Insulators (1)

| Description    | Suspension    | Weight [kN] | Length [m] | Wind area [m <sup>2</sup> ] |
|----------------|---------------|-------------|------------|-----------------------------|
| Circuit 1      | Afspanketting | 6.00        | 7.90       | 2.40                        |
| Circuit 2      | Afspanketting | 6.00        | 7.90       | 2.40                        |
| Bliksemdraad 1 | Afspanketting | 0.10        | 0.20       | 0.10                        |
| Bliksemdraad 2 | Afspanketting | 0.10        | 0.20       | 0.10                        |

1. Properties apply to the entire isolator set

#### Suspension height and position in mast

| Circuits       | Designation | Number   | Suspension height | Attach point | Position in tower Horizontal distance |
|----------------|-------------|----------|-------------------|--------------|---------------------------------------|
| Circuit 1      | 10          | 380ct1f1 | 27.7 m            | 27.7 m       | -17.5 m                               |
| Circuit 1      | 11          | 380ct1f2 | 27.7 m            | 27.7 m       | -9.0 m                                |
| Circuit 1      | 12          | 380ct1f3 | 39.0 m            | 39.0 m       | -13.3 m                               |
| Circuit 2      | 20          | 380ct2f1 | 27.7 m            | 27.7 m       | 9.0 m                                 |
| Circuit 2      | 21          | 380ct2f2 | 27.7 m            | 27.7 m       | 17.5 m                                |
| Circuit 2      | 22          | 380ct2f3 | 39.0 m            | 39.0 m       | 13.3 m                                |
| Bliksemdraad 1 | 1           | bl1      | 43.0 m            | 43.0 m       | -19.8 m                               |
| Bliksemdraad 2 | 3           | bl2      | 43.0 m            | 43.0 m       | 19.8 m                                |

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

**Height adjustment adjacent masts** (wind and weight span adjustment)

|                                     | Back  | Ahead |  |
|-------------------------------------|-------|-------|--|
| Height increase for wind pressure   | 0.0 m | 0.0 m | (positive: higher)                     |
| Height decrease for vertical load   | 0.0 m | 0.0 m | (negative: decrease, more weight span) |
| Decrease: Niet in 0,9EG-combinaties |       |       |  |

**Height difference adjacent tower and change of direction with respect to Line direction**

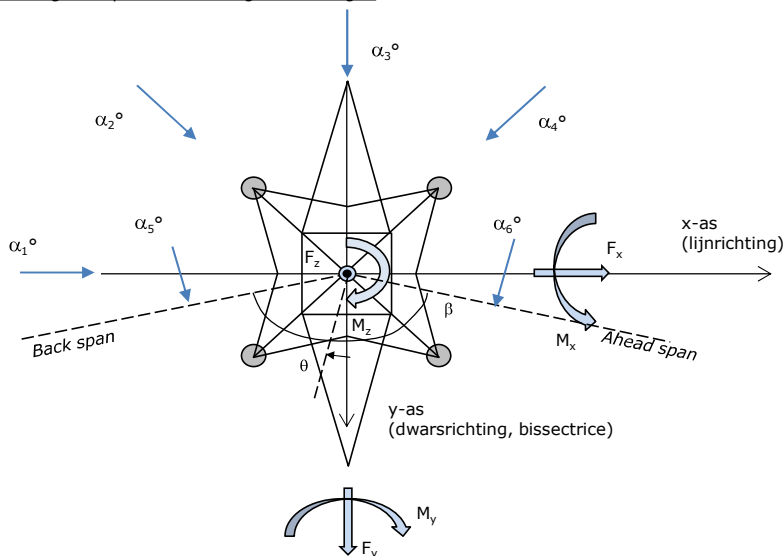
| Circuits       | Aanduiding | Nummer   | Hoogteverschil    |                    | Richtingsverandering |                    |
|----------------|------------|----------|-------------------|--------------------|----------------------|--------------------|
|                |            |          | $\Delta h_{back}$ | $\Delta h_{ahead}$ | $\Delta y_{back}$    | $\Delta y_{ahead}$ |
| Circuit 1      | 10         | 380ct1f1 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 11         | 380ct1f2 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 1      | 12         | 380ct1f3 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 20         | 380ct2f1 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 21         | 380ct2f2 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Circuit 2      | 22         | 380ct2f3 | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 1 | 1          | bl1      | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |
| Bliksemdraad 2 | 3          | bl2      | 0.0               | 0.0 m              | 0.0                  | 0.0 m              |

**Line and tower data**

|  | Back           | Ahead          |
|--|----------------|----------------|
| Ruling span $\sqrt{(\Sigma L^3 / \Sigma L)}$ | 394.2          | 269.1 m        |
| Line angle                                   | 392.9          | 269.1 m        |
| Tower orientation with respect to bis0       | $129.24^\circ$ |                |
| Section length                               | 2748           | 269 m          |
| Height bottom of tower to ground level       | 0.5 m          |                |
| Wind directions considered                   | $\alpha_1$     | $0^\circ$      |
| Wind directions according to:                | $\alpha_2$     | $45^\circ$     |
| <i>Geleiderbelastingen</i>                   | $\alpha_3$     | $90^\circ$     |
|  | $\alpha_4$     | $135^\circ$    |
|  | $\alpha_5$     | $69.62^\circ$  |
|  | $\alpha_6$     | $120.38^\circ$ |

Wind directions apply to the main direction of mast construction, not to the bisector.

Windrichtingen en positieve richtingen belastingen



**Considered number of wind directions**

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

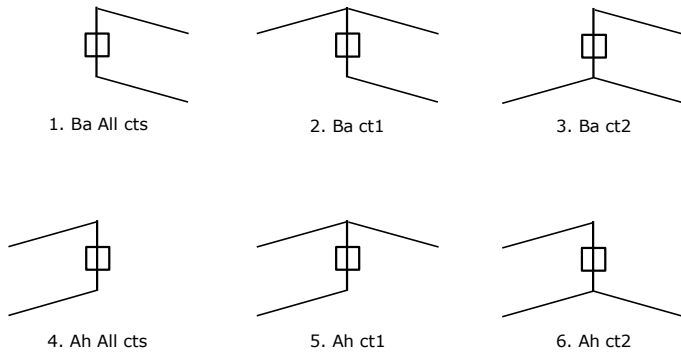
**Absence of conductors**

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 1 | b1       | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | b2       | 0             | 1    | 1                        | 0    | 1                  | 0    |

**Load situations SPLS**

Considered situations SPLS: 1 up to 6, All possible situations

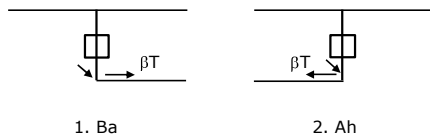
Principle of load situations:



**Load situation 5a. Conductor failure**

Considered situations conductor failure 5a: 1 and 2, all possible situations

Principle of load situations:



Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

**Load situations LC6. Construction and maintenance**

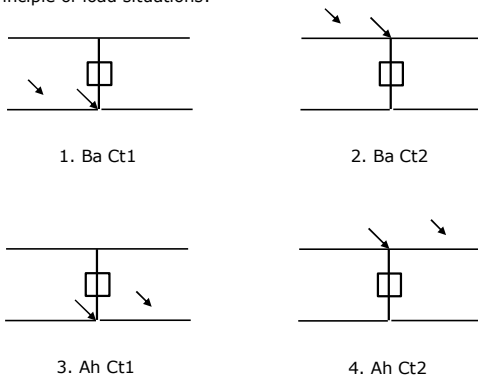
Under 6a, the load due to the presence of a line vehicle or line bicycle in combination with point load on the traverse is assessed. Combination 6b does not contain any loads in conductor or on traverse. This combination has been added to be able to combine with separate control platforms, etc. The situations are applied in ULS and in every SPLS situation (in case of angle tower).

|                             | Phase  | Earth  |
|-----------------------------|--------|--------|
| Line vehicle                | 4.0 kN | 2.0 kN |
| Concentrated load cross arm | 1.0 kN | 1.0 kN |

Beschouwde situaties bouw- en onderhoud 6a: 1 t/m 4, alle mogelijke situaties.

Presence line vehicle: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principle of load situations:



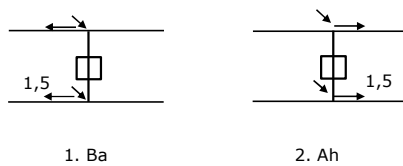
**Load situations 8. Galloping as a static load**

| Conductor                    |         |       |
|------------------------------|---------|-------|
| Suspension tower phase       | 0.866 W | 1.5 W |
| Suspension tower earth       | 1.5 EDS | 1.5 W |
| Strain tower phase and earth | 1.5 EDS | 1.5 W |

Considered situations galloping 8: None (existing structure)

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principle of load situations:



**Load combination 8. Galloping as a dynamic load**

Only applies to tension towers  
 Load consists of EDS tensile load in one of the conductors on one side of the tower  
 Can be converted by user to fatigue spectrum via the load spectrum of table 4.11 / NL.1

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

### Tower structure

#### Properties

|                                      |             |               |
|--------------------------------------|-------------|---------------|
| Tower type                           | Hoekmast    |               |
| Tower designation                    | HC+0        |               |
| Base plate w.r.t. ground level       | 0.5 m       |               |
| Tower height w.r.t. base plate       | 48.5 m      |               |
| Tower self weight                    | 500.0 kN    |               |
| <i>Width and slope at foundation</i> |             |               |
| Leg spread                           | x-ri. 11.00 | y-ri. 11.00 m |
| Inclination of main leg              | 0.156       | 0.156 -       |
| Horizontal force factor              | 1.3         | 1.3 -         |

#### Calculation Wind load

|  |                                       |
|--|---------------------------------------|
| Dynamic factor $G_T$   | 1.00 ( <i>Masthoogte &lt; 60 m</i> )  |
| Wind load diagonally to tower body proportional to:            | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Wind load diagonally on traverse proportional to:              | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Magnification factor diagonal wind to tower body               | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor diagonal wind to cross arm                | $(1+0,2\sin^2(2\phi))$                |
| Magnification factor wind parallel to perpendicular to cross a | 0.4                                   |

#### Properties mast sections longitudinal direction (front view, yz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 9.60     | 11.00                 | 8.00                  | 9.60      | 0.156                 | 91.20                               | 7.50                                | 0.08                                      | 3.50           |
| Eerste tussenstuk | 18.90    | 8.00                  | 5.84                  | 9.30      | 0.116                 | 64.36                               | 7.90                                | 0.12                                      | 3.29           |
| Tweede tussenstuk | 27.70    | 5.84                  | 3.78                  | 8.80      | 0.117                 | 42.33                               | 8.00                                | 0.19                                      | 2.98           |
| Bovenstuk 1       | 35.50    | 3.78                  | 3.18                  | 7.80      | 0.038                 | 27.14                               | 5.90                                | 0.22                                      | 2.86           |
| Bovenstuk 2       | 43.00    | 3.18                  | 2.60                  | 7.50      | 0.039                 | 21.68                               | 5.10                                | 0.24                                      | 2.78           |
| Topstuk           | 45.00    | 2.60                  |                       | 2.00      |                       | 2.60                                | 0.50                                | 0.19                                      | 2.96           |
| Ondertraverse     | 27.70    | 15.54                 |                       | 4.00      |                       | 31.08                               | 7.25                                | 0.23                                      | 2.79           |
| Boventraverse     | 39.00    | 18.05                 |                       | 4.20      |                       | 37.91                               | 8.47                                | 0.22                                      | 2.83           |

#### Properties tower sections transversal direction (side view, xz plane)

| Description       | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 9.60     | 11.00                 | 8.00                  | 9.60      | 0.156                 | 91.20                               | 7.50                                | 0.08                                      | 3.50           |
| Eerste tussenstuk | 18.90    | 8.00                  | 5.84                  | 9.30      | 0.116                 | 64.36                               | 7.90                                | 0.12                                      | 3.29           |
| Tweede tussenstuk | 27.70    | 5.84                  | 3.78                  | 8.80      | 0.117                 | 42.33                               | 8.00                                | 0.19                                      | 2.98           |
| Bovenstuk 1       | 35.50    | 3.78                  | 3.18                  | 7.80      | 0.038                 | 27.14                               | 5.90                                | 0.22                                      | 2.86           |
| Bovenstuk 2       | 43.00    | 3.18                  | 2.60                  | 7.50      | 0.039                 | 21.68                               | 5.10                                | 0.24                                      | 2.78           |
| Topstuk           | 45.00    | 2.60                  |                       | 2.00      |                       | 2.60                                | 0.50                                | 0.19                                      | 2.96           |
| Ondertraverse     | 27.70    | 15.54                 |                       | 4.00      |                       | 31.08                               | 7.25                                | 0.23                                      | 2.79           |
| Boventraverse     | 39.00    | 18.05                 |                       | 4.20      |                       | 37.91                               | 8.47                                | 0.22                                      | 2.83           |

Note: Surface transverse direction is reduced in calculation.

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

#### Wind surface feeders telecom installations

| Part              | A (m <sup>2</sup> /m) | Factor | Δh | A <sub>1</sub> |
|-------------------|-----------------------|--------|----|----------------|
| Broekstuk         |                       |        |    |                |
| Eerste tussenstuk |                       |        |    |                |
| Tweede tussenstuk |                       |        |    |                |
| Bovenstuk 1       |                       |        |    |                |
| Bovenstuk 2       |                       |        |    |                |

#### Input antennas

| Description  | A (m <sup>2</sup> ) | h (m) | C <sub>r</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. |                     |       |                    |

#### Tower section loads longitudinal (x-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 18.4                    | 15.6                    | 0.0                     | -15.6                   | 4.8                    | 88.3                     | 74.9                     | 0.0                      | -74.9                    |
| Eerste tussenstuk | 0.79                                   | 20.5                    | 17.4                    | 0.0                     | -17.4                   | 14.3                   | 292.4                    | 248.1                    | 0.0                      | -248.1                   |
| Tweede tussenstuk | 0.92                                   | 21.9                    | 18.6                    | 0.0                     | -18.6                   | 23.3                   | 510.2                    | 432.9                    | 0.0                      | -432.9                   |
| Bovenstuk 1       | 1.01                                   | 17.0                    | 14.4                    | 0.0                     | -14.4                   | 31.6                   | 536.5                    | 455.2                    | 0.0                      | -455.2                   |
| Bovenstuk 2       | 1.06                                   | 15.1                    | 12.8                    | 0.0                     | -12.8                   | 39.3                   | 592.9                    | 503.1                    | 0.0                      | -503.1                   |
| Topstuk           | 1.10                                   | 1.6                     | 1.4                     | 0.0                     | -1.4                    | 44.0                   | 71.6                     | 60.8                     | 0.0                      | -60.8                    |
| Ondertraverse     | 0.98                                   | 39.6                    | 23.5                    | 0.0                     | -23.5                   | 29.0                   | 1150.2                   | 683.2                    | 0.0                      | -683.2                   |
| Boventraverse     | 1.07                                   | 51.5                    | 30.6                    | 0.0                     | -30.6                   | 40.4                   | 2078.8                   | 1234.7                   | 0.0                      | -1234.7                  |
| <b>Totaal</b>     |  | <b>185.6</b>            | <b>134.3</b>            | <b>0.0</b>              | <b>-134.3</b>           |                        | <b>5320.9</b>            | <b>3693.0</b>            | <b>0.0</b>               | <b>-3693.0</b>           |

#### Tower section loads transversal (y-direction) per wind direction

| Description       | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0.70                                   | 0.0                     | 15.6                    | 18.4                    | 15.6                    | 4.8                    | 0.0                      | 74.9                     | 88.3                     | 74.9                     |
| Eerste tussenstuk | 0.79                                   | 0.0                     | 17.4                    | 20.5                    | 17.4                    | 14.3                   | 0.0                      | 248.1                    | 292.4                    | 248.1                    |
| Tweede tussenstuk | 0.92                                   | 0.0                     | 18.6                    | 21.9                    | 18.6                    | 23.3                   | 0.0                      | 432.9                    | 510.2                    | 432.9                    |
| Bovenstuk 1       | 1.01                                   | 0.0                     | 14.4                    | 17.0                    | 14.4                    | 31.6                   | 0.0                      | 455.2                    | 536.5                    | 455.2                    |
| Bovenstuk 2       | 1.06                                   | 0.0                     | 12.8                    | 15.1                    | 12.8                    | 39.3                   | 0.0                      | 503.1                    | 592.9                    | 503.1                    |
| Topstuk           | 1.10                                   | 0.0                     | 1.4                     | 1.6                     | 1.4                     | 44.0                   | 0.0                      | 60.8                     | 71.6                     | 60.8                     |
| Ondertraverse     | 0.98                                   | 0.0                     | 23.5                    | 15.8                    | 23.5                    | 29.0                   | 0.0                      | 683.2                    | 460.1                    | 683.2                    |
| Boventraverse     | 1.07                                   | 0.0                     | 30.6                    | 20.6                    | 30.6                    | 40.4                   | 0.0                      | 1234.7                   | 831.5                    | 1234.7                   |
| <b>Total</b>      |  | <b>0.0</b>              | <b>134.3</b>            | <b>131.0</b>            | <b>134.3</b>            |                        | <b>0.0</b>               | <b>3693.0</b>            | <b>3383.5</b>            | <b>3693.0</b>            |

#### Resulting loads from mast construction incl. Antenna without conductors level foundation (char. Value)

| Load / wind direction | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|-----------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting  | 0                      | 0                      | 500                    | 0                       | 0                       | 0                       |
| Windrichting 0°       | 186                    | 0                      | 0                      | 0                       | 5321                    | 0                       |
| Windrichting 45°      | 134                    | 134                    | 0                      | 3693                    | 3693                    | 0                       |
| Windrichting 90°      | 0                      | 131                    | 0                      | 3384                    | 0                       | 0                       |
| Windrichting 135°     | -134                   | 134                    | 0                      | 3693                    | -3693                   | 0                       |



Project: GT-RL380  
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### Intermediate results for conductor loads

#### Conductors back

| Circuit        | Geleider              | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|-----------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Circuit 2      | St/Al 48/7-423/37-SEP | 27.9             | 460.5                   | 14.90      | 64835                     | 2.03E-05          |
| Bliksemdraad 1 | ACSR-26/7-242/39-HAWK | 21.8             | 281.1                   | 9.81       | 75000                     | 1.89E-05          |
| Bliksemdraad 2 | OPGW 226              | 21.7             | 264.0                   | 9.80       | 81000                     | 2.30E-05          |

#### Conductors ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27.7             | 571.0                   | 14.98      | 62700                     | 1.88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27.7             | 571.0                   | 14.98      | 62700                     | 1.88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21.8             | 281.0                   | 9.38       | 70165                     | 1.97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21.7             | 264.0                   | 9.13       | 72000                     | 1.98E-05          |

#### Vertical load back

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Circuit 2      | 3             | 2                 | 45.6               |            | B 4+0,2d  | 9.6                  | 28.8                        |
| Bliksemdraad 1 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 10.0               |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Vertical load ahead

| Circuit        | Bundle<br>[-] | Additional<br>[%] | $w_{z,G}$<br>[N/m] | Ice region | Formula   | $w_{z,ijs}$<br>[N/m] | $w_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|-------------------|--------------------|------------|-----------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2                 | 45.8               |            | B 4+0,2d  | 9.5                  | 28.6                        |
| Circuit 2      | 3             | 2                 | 45.8               |            | B 4+0,2d  | 9.5                  | 28.6                        |
| Bliksemdraad 1 | 1             | 2                 | 9.6                |            | A 15+0,4d | 23.7                 | 23.7                        |
| Bliksemdraad 2 | 1             | 2                 | 9.3                |            | A 15+0,4d | 23.7                 | 23.7                        |

#### Insulators

| Conductor | $G_{isolator}$<br>[kN] | Number | $F_{v,iso}$<br>[kN] | Length<br>[m] | Wind surf.<br>[m <sup>2</sup> ] | Wind heigth<br>[m] | Pressure<br>[kN/m <sup>2</sup> ] | Drag factor<br>[-] | $F_{h,iso}$<br>[kN] |
|-----------|------------------------|--------|---------------------|---------------|---------------------------------|--------------------|----------------------------------|--------------------|---------------------|
| 380ct1f1  | 6.00                   | 1      | 6                   | 7.9           | 2.4                             | 28.20              | 0.97                             | 1.2                | 2.80                |
| 380ct1f2  | 6.00                   | 1      | 6                   | 7.9           | 2.4                             | 28.20              | 0.97                             | 1.2                | 2.80                |
| 380ct1f3  | 6.00                   | 1      | 6                   | 7.9           | 2.4                             | 39.50              | 1.07                             | 1.2                | 3.07                |
| 380ct2f1  | 6.00                   | 1      | 6                   | 7.9           | 2.4                             | 28.20              | 0.97                             | 1.2                | 2.80                |
| 380ct2f2  | 6.00                   | 1      | 6                   | 7.9           | 2.4                             | 28.20              | 0.97                             | 1.2                | 2.80                |
| 380ct2f3  | 6.00                   | 1      | 6                   | 7.9           | 2.4                             | 39.50              | 1.07                             | 1.2                | 3.07                |
| bl1       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 43.50              | 1.09                             | 1.2                | 0.13                |
| bl2       | 0.10                   | 1      | 0.1                 | 0.2           | 0.1                             | 43.50              | 1.09                             | 1.2                | 0.13                |

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#### Wind load back

| Conductor | Height |                      | G <sub>c_duars</sub> | G <sub>c_trek</sub> | C <sub>c</sub> | d <sub>additional</sub> | w <sub>y</sub> | w <sub>y,section</sub> | D <sub>ijs,additional</sub> | w <sub>y,ijs</sub> | w <sub>y,ijs,section</sub> |
|-----------|--------|----------------------|----------------------|---------------------|----------------|-------------------------|----------------|------------------------|-----------------------------|--------------------|----------------------------|
|           | wind   | Pressure             |                      |                     |                |                         |                |                        |                             |                    |                            |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]                  | [-]                 | [-]            | [mm]                    | [N/m]          | [N/m]                  | [mm]                        | [N/m]              | [N/m]                      |
| 380ct1f1  | 18.8   | 0.86                 | 0.55                 | 0.47                | 1.13           | 28.50                   | 46.1           | 39.5                   | 47.2                        | 80.9               | 69.3                       |
| 380ct1f2  | 18.8   | 0.86                 | 0.55                 | 0.47                | 1.13           | 28.50                   | 46.1           | 39.5                   | 47.2                        | 80.9               | 69.3                       |
| 380ct1f3  | 30.1   | 0.99                 | 0.59                 | 0.51                | 1.09           | 28.50                   | 54.8           | 46.8                   | 47.2                        | 99.4               | 85.0                       |
| 380ct2f1  | 18.8   | 0.86                 | 0.55                 | 0.47                | 1.13           | 28.50                   | 46.1           | 39.5                   | 47.2                        | 80.9               | 69.3                       |
| 380ct2f2  | 18.8   | 0.86                 | 0.55                 | 0.47                | 1.13           | 28.50                   | 46.1           | 39.5                   | 47.2                        | 80.9               | 69.3                       |
| 380ct2f3  | 30.1   | 0.99                 | 0.59                 | 0.51                | 1.09           | 28.50                   | 54.8           | 46.8                   | 47.2                        | 99.4               | 85.0                       |
| bl1       | 34.1   | 1.02                 | 0.60                 | 0.51                | 1.20           | 22.24                   | 16.5           | 14.1                   | 63.1                        | 46.7               | 39.9                       |
| bl2       | 34.1   | 1.02                 | 0.60                 | 0.51                | 1.20           | 22.13                   | 16.4           | 14.0                   | 63.0                        | 46.7               | 39.9                       |

#### Wind load ahead

| Conductor | Height |                      | G <sub>c_duars</sub> | G <sub>c_trek</sub> | C <sub>c</sub> | d <sub>additional</sub> | w <sub>y</sub> | w <sub>y,section</sub> | D <sub>ijs,additional</sub> | w <sub>y,ijs</sub> | w <sub>y,ijs,section</sub> |
|-----------|--------|----------------------|----------------------|---------------------|----------------|-------------------------|----------------|------------------------|-----------------------------|--------------------|----------------------------|
|           | wind   | Pressure             |                      |                     |                |                         |                |                        |                             |                    |                            |
|           | [m]    | [kN/m <sup>2</sup> ] | [-]                  | [-]                 | [-]            | [mm]                    | [N/m]          | [N/m]                  | [mm]                        | [N/m]              | [N/m]                      |
| 380ct1f1  | 23.8   | 0.92                 | 0.57                 | 0.65                | 1.12           | 28.25                   | 50.2           | 57.3                   | 46.9                        | 89.5               | 102.2                      |
| 380ct1f2  | 23.8   | 0.92                 | 0.57                 | 0.65                | 1.12           | 28.25                   | 50.2           | 57.3                   | 46.9                        | 89.5               | 102.2                      |
| 380ct1f3  | 35.1   | 1.03                 | 0.60                 | 0.69                | 1.09           | 28.25                   | 57.5           | 65.5                   | 46.9                        | 105.5              | 120.2                      |
| 380ct2f1  | 23.8   | 0.92                 | 0.57                 | 0.65                | 1.12           | 28.25                   | 50.2           | 57.3                   | 46.9                        | 89.5               | 102.2                      |
| 380ct2f2  | 23.8   | 0.92                 | 0.57                 | 0.65                | 1.12           | 28.25                   | 50.2           | 57.3                   | 46.9                        | 89.5               | 102.2                      |
| 380ct2f3  | 35.1   | 1.03                 | 0.60                 | 0.69                | 1.09           | 28.25                   | 57.5           | 65.5                   | 46.9                        | 105.5              | 120.2                      |
| bl1       | 39.1   | 1.06                 | 0.61                 | 0.70                | 1.20           | 22.24                   | 17.4           | 19.8                   | 63.1                        | 49.4               | 56.2                       |
| bl2       | 39.1   | 1.06                 | 0.61                 | 0.70                | 1.20           | 22.13                   | 17.3           | 19.7                   | 63.0                        | 49.3               | 56.2                       |

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 Tower: HC+0  
 Number: 16

**Conductor loads**

Auteur: TBR  
 Versie: v11.8

**Starting points**

Consequence class Afkeur CC2-0  
 Reference period 30 jaar

| ULS (strength)   |                            | NEN-EN50341-2-15:2019 |              |                  |            |          |          |                     |
|--|----------------------------|-----------------------|--------------|------------------|------------|----------|----------|---------------------|
| Load case  | description                | Temp °C               | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|  |                            |                       | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a   | Wind                       | 10°                   | 1.05         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9   | Wind 0,9Gk only tower      | 10°                   | 0.90         | 1.05             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 1a_0,9_0,9   | Wind 0,9Gk conductors too  | 10°                   | 0.90         | 0.90             | 0.00       | 1.12     | 0.00     | 0.0                 |
| ULS 3  | Wind+ice                   | -5°                   | 1.05         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 3_0,9  | Wind+ice 0,9Gk             | -5°                   | 0.90         | 1.05             | 0.00       | 0.34     | 0.97     | 0.0                 |
| ULS 4  | Cold+wind                  | -20°                  | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 4_0,9  | Cold+wind 0,9Gk            | -20°                  | 0.90         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 5a   | Torsional loads            | 10°                   | 1.00         | 1.00             | 1.00       | 0.00     | 0.00     | 1.0                 |
| ULS 5b   | Longitudinal loads         | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| ULS 6  | Construction + maintenance | 5°                    | 1.05         | 1.05             | 1.20       | 0.22     | 0.00     | 0.0                 |
| ULS 6_0,9  | Construction + maintenance | 5°                    | 1.05         | 1.05             | 0.00       | 0.22     | 0.00     | 0.0                 |
| ULS 7  | Permanent                  | 10°                   | 1.15         | 1.15             | 0.00       | 0.00     | 0.00     | 0.0                 |
| ULS 8  | Special                    | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| SPLS (strength, for angle towers: absence of conductors) |                            |                       | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
| SPLS   | description                | Temp °C               | $G_k$        |                  | $Q_k$      |          |          | $A_k$               |
|  |                            |                       | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| SPLS 1a  | Wind                       | 10°                   | 1.05         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9  | Wind 0,9                   | 10°                   | 0.90         | 1.05             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9_0,9  | Wind 0,9                   | 10°                   | 0.90         | 0.90             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 3   | Wind+ice                   | -5°                   | 1.05         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 3_0,9   | Wind+ice 0,9               | -5°                   | 0.90         | 1.05             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 4   | Cold+wind                  | -20°                  | 1.05         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 4_0,9   | Cold+wind 0,9              | -20°                  | 0.90         | 1.05             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 6   | Maintenance                | 5°                    | 1.05         | 1.05             | 1.2        | 0.24     | 0.0      | 0.0                 |
| SPLS 6_0,9   | Maintenance                | 5°                    | 1.05         | 1.05             | 0.0        | 0.24     | 0.0      | 0.0                 |
| SLS (deformations, fatigue, EDS)                         |                            |                       | $G_k$        |                  | $Q_k$      |          |          |                     |
| SLS  | description                | Temp °C               | $G_k$        |                  | $Q_k$      |          |          | $A_k$               |
|  |                            |                       | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| SLS 1a   | Wind                       | 10°                   | 1.00         | 1.00             | 0.0        | 0.94     | 0.0      | 0.0                 |
| SLS 3  | Wind+ice                   | -5°                   | 1.00         | 1.00             | 0.0        | 0.28     | 0.88     | 0.0                 |
| SLS 4  | Wind                       | -20°                  | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 6  | Maintenance                | 5°                    | 1.00         | 1.00             | 0.0        | 0.19     | 0.0      | 0.0                 |
| SLS 7  | EDS, no wind               | 10°                   | 1.00         | 1.00             | 0.0        | 0.00     | 0.0      | 0.0                 |

Number of wind directions 6  
 Number of load combinations for ULS 54  
 Number of load combinations for SPLS 222  
 Number of load combinations for SLS 15  
 Number of concentrated loads 5238

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

### Summary table - Conductor loads

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

#### Maximum values for back and ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -38.6         | 33.2          | 17.7          | 22.1          | 6.5           | 5.1           |
| 380ct1f1    | -97.2         | 91.8          | 42.8          | 59.7          | 21.8          | 18.8          |
| 380ct1f2    | -97.2         | 91.8          | 42.8          | 59.7          | 21.8          | 18.8          |
| 380ct1f3    | -98.6         | 93.8          | 46.6          | 64.4          | 21.8          | 18.8          |
| 380ct2f1    | -97.2         | 91.8          | 42.8          | 59.7          | 21.8          | 18.8          |
| 380ct2f2    | -97.2         | 91.8          | 42.8          | 59.7          | 21.8          | 18.8          |
| 380ct2f3    | -98.6         | 93.8          | 46.6          | 64.4          | 21.8          | 18.8          |
| bl2         | -38.8         | 32.7          | 17.8          | 21.8          | 6.5           | 5.0           |
| V-ketting 1 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |
| V-ketting 2 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 331.7  | 331.7 | 331.7 |
| 380ct1f1    | 331.7  | 331.7 | 331.7 |
| 380ct1f2    | 331.7  | 331.7 | 331.7 |
| 380ct1f3    | 331.7  | 331.7 | 331.7 |
| 380ct2f1    | 331.7  | 331.7 | 331.7 |
| 380ct2f2    | 331.7  | 331.7 | 331.7 |
| 380ct2f3    | 331.7  | 331.7 | 331.7 |
| bl2         | 331.7  | 331.7 | 331.7 |
| V-ketting 1 |        |       |       |
| V-ketting 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 331.7  | 331.7 |
| 380ct1f1    | 331.7  | 331.7 |
| 380ct1f2    | 331.7  | 331.7 |
| 380ct1f3    | 331.7  | 331.7 |
| 380ct2f1    | 331.7  | 331.7 |
| 380ct2f2    | 331.7  | 331.7 |
| 380ct2f3    | 331.7  | 331.7 |
| bl2         | 331.7  | 331.7 |
| V-ketting 1 |        |       |
| V-ketting 2 |        |       |

#### Envelop of weight span over all combinations (incl. 0,9 combinations)

| For all conductors | Wind / Weight span ratio |
|--------------------|--------------------------|
| Max. weight span   | 331.7 m / 1.000 -        |
| Min. weight span   | 331.7 m / 1.000 -        |

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 Tower: HC+0  
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**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider    | Fx   | Fy    | Fz   | Ft_ba  | Ft_ah |
|-------------|------|-------|------|--------|-------|
|             | [kN] | [kN]  | [kN] | [kN]   | [kN]  |
| bl1         | 26.9 | 37.8  | 6.5  | -42.3  | 39.8  |
| 380ct1f1    | 90.8 | 98.6  | 21.8 | -106.1 | 109.4 |
| 380ct1f2    | 90.8 | 98.6  | 21.8 | -106.1 | 109.4 |
| 380ct1f3    | 90.9 | 101.4 | 21.8 | -108.0 | 112.0 |
| 380ct2f1    | 90.8 | 98.6  | 21.8 | -106.1 | 109.4 |
| 380ct2f2    | 90.8 | 98.6  | 21.8 | -106.1 | 109.4 |
| 380ct2f3    | 90.9 | 101.4 | 21.8 | -108.0 | 112.0 |
| bl2         | 27.0 | 37.6  | 6.5  | -42.6  | 39.2  |
| V-ketting 1 | 1.9  | 1.9   | 3.5  | 0.0    |       |
| V-ketting 2 | 1.9  | 1.9   | 3.5  | 0.0    |       |

**EDS-loads conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 11.3 | 6.6  | 2.1  | -13.8 | 13.1  |
| 380ct1f1    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct1f2    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct1f3    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct2f1    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct2f2    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct2f3    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| bl2         | 11.0 | 6.5  | 2.1  | -13.7 | 12.8  |
| V-ketting 1 | 0.0  | 0.0  | 3.0  | 0.0   |       |
| V-ketting 2 | 0.0  | 0.0  | 3.0  | 0.0   |       |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4 bl1            | 0.0   | 0.0   |
| 380ct1f1             | 0.0   | 0.0   |
| 380ct1f2             | 0.0   | 0.0   |
| 380ct1f3             | 0.0   | 0.0   |
| 380ct2f1             | 0.0   | 0.0   |
| 380ct2f2             | 0.0   | 0.0   |
| 380ct2f3             | 0.0   | 0.0   |
| bl2                  | 0.0   | 0.0   |
| V-ketting 1          | 0.0   |       |
| V-ketting 2          | 0.0   |       |

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 Number: 16

**ULS foundation loads for LC 1 and 3, wind purpendicular to the line or bisector and EDS, from conductors**

| Combination       | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -14           | 609           | 185           | 19885          | -478           | -5             |
| ULS 1a_0,9_0      |             | 2             | 367           | 184           | 11921          | 72             | 41             |
| ULS 1a_0,9_0,9_90 |             | -5            | 580           | 158           | 18969          | -183           | -4             |
| ULS 3_0           |             | -50           | 585           | 254           | 19224          | -1713          | 0              |
| SLS 7             |             | -30           | 345           | 176           | 11187          | -976           | -6             |

**ULS foundation loads, LC 1 and 3, wind purpendicular to the line or bisector and EDS, total conductors and tower**

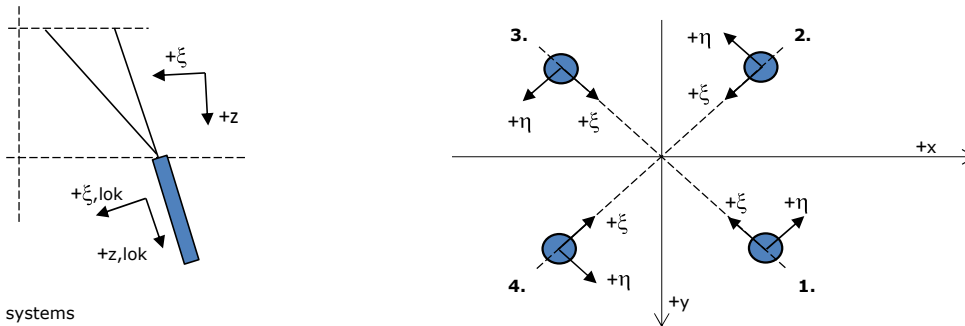
| Combination       | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -14           | 755           | 710           | 23664          | -478           | -5             |
| ULS 1a_0,9_0,9_90 | -5            | 727           | 608           | 22748          | -183           | -4             |
| SLS 7             | -30           | 345           | 676           | 11187          | -976           | -6             |

**Foundation loads, selection of load combinations based on greatest value**

| Combination              | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|--------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_120.38            | 33            | 756           | 710           | <b>23729</b>   | 1739           | -29            |
| SPLS 3_135 Ah All Cts    | -536          | 241           | 681           | 7609           | <b>-17087</b>  | -13            |
| SPLS 6a_90 Ba Ct1 Ah Ct1 | 286           | 416           | 715           | 13524          | 9285           | <b>-4331</b>   |
| SPLS 3_120.38 Ba All Cts | 500           | 393           | 657           | <b>12588</b>   | <b>16482</b>   | -14            |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



**Maximum compression load**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 3_120.38 Ba All Cts | 274           | 284           | <b>1486</b>   | -7                 | -395              | -67                   | 1522                |
| 2     | SPLS 1a_0 Ba All Cts     | 101           | -133          | <b>601</b>    | 23                 | -166              | -33                   | 616                 |
| 3     | SPLS 3_135 Ah All Cts    | -98           | -132          | <b>601</b>    | -24                | -163              | -30                   | 615                 |
| 4     | SPLS 3_69.62 Ah All Cts  | -245          | 260           | <b>1342</b>   | 11                 | -358              | -61                   | 1374                |

**Maximum tension load**

| Index | Combination                  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_135 Ah All Cts    | -34           | -67           | <b>-280</b>   | 23                 | 71                | 9                     | -287                |
| 2     | SPLS 3_0,9_69.62 Ah All Cts  | -180          | 195           | <b>-1020</b>  | -11                | 265               | 40                    | -1045               |
| 3     | SPLS 3_0,9_120.38 Ba All Cts | 212           | 221           | <b>-1175</b>  | 6                  | 306               | 46                    | -1204               |
| 4     | SPLS 1a_0,9_0 Ba All Cts     | 40            | -70           | <b>-296</b>   | -21                | 78                | 13                    | -303                |

**Maximum torsional load (positive)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ah Ct2 | 223           | 9             | 615           | <b>152</b>         | -164              | -28                   | 630                 |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -112          | -116          | 2             | <b>161</b>         | -3                | -2                    | 2                   |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | 59            | 252           | -842          | <b>136</b>         | 219               | 33                    | -862                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -130          | 306           | 1152          | <b>125</b>         | -308              | -54                   | 1180                |

**Maximum torsional load (negative)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_{\eta}$<br>[kN] | $R_{\xi}$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|--------------------|-------------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 134           | 325           | 1216          | <b>-135</b>        | -324              | -56                   | 1245                |
| 2     | SPLS 6a_90 Ah Ct2 Ah Ct2 | -3            | 183           | -500          | <b>-127</b>        | 132               | 21                    | -512                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 79            | -130          | 126           | <b>-147</b>        | -36               | -8                    | 129                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -188          | -44           | 371           | <b>-164</b>        | -102              | -20                   | 380                 |

Project: GT-RLL380  
 Tower: HC+0  
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#### Combination Ftensile+Fhor

| Index | Combination                  | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 6a_90 Ah All Cts Ba Ct1 | 10                     | -84                    | <b>-222</b>            | <b>66</b>              | 52                     | 3                          | -227                       |
| 2     | SPLS 3_0,9_90 Ah Ct1         | -243                   | 79                     | <b>-881</b>            | <b>116</b>             | 228                    | 33                         | -903                       |
| 3     | SPLS 3_0,9_120.38 Ba Ct1     | 259                    | 92                     | <b>-969</b>            | <b>-118</b>            | 248                    | 34                         | -993                       |
| 4     | SPLS 1a_0,9_0 Ba All Cts     | 40                     | -70                    | <b>-296</b>            | <b>-21</b>             | 78                     | 13                         | -303                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 130                    | 112                    | 633                    | 13                     | -171                   | -31                        | 648                        |
| 2     | SLS 7       | -76                    | 61                     | -384                   | 11                     | 97                     | 12                         | -393                       |
| 3     | SLS 7       | 62                     | 43                     | -295                   | -13                    | 74                     | 9                          | -302                       |
| 4     | SLS 7       | -145                   | 129                    | 722                    | -11                    | -194                   | -35                        | 739                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination                  | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | SPLS 3_120.38 Ba All Cts     | 274                    | 284                    | <b>1486</b>            | -7                     | -395                   | -67                        | 1522                       |
| Max. tension         | SPLS 3_0,9_120.38 Ba All Cts | 212                    | 221                    | <b>-1175</b>           | 6                      | 306                    | 46                         | -1204                      |
| Max. pos. torsie     | SPLS 6a_90 Ba Ct2 Ah Ct2     | -112                   | -116                   | 2                      | <b>161</b>             | -3                     | -2                         | 2                          |
| Max. neg. torsie     | SPLS 6a_90 Ba Ct1 Ah Ct1     | -188                   | -44                    | 371                    | <b>-164</b>            | -102                   | -20                        | 380                        |
| Comb. tension+torsie | SPLS 3_0,9_120.38 Ba Ct1     | 259                    | 92                     | <b>-969</b>            | <b>-118</b>            | 248                    | 34                         | -993                       |

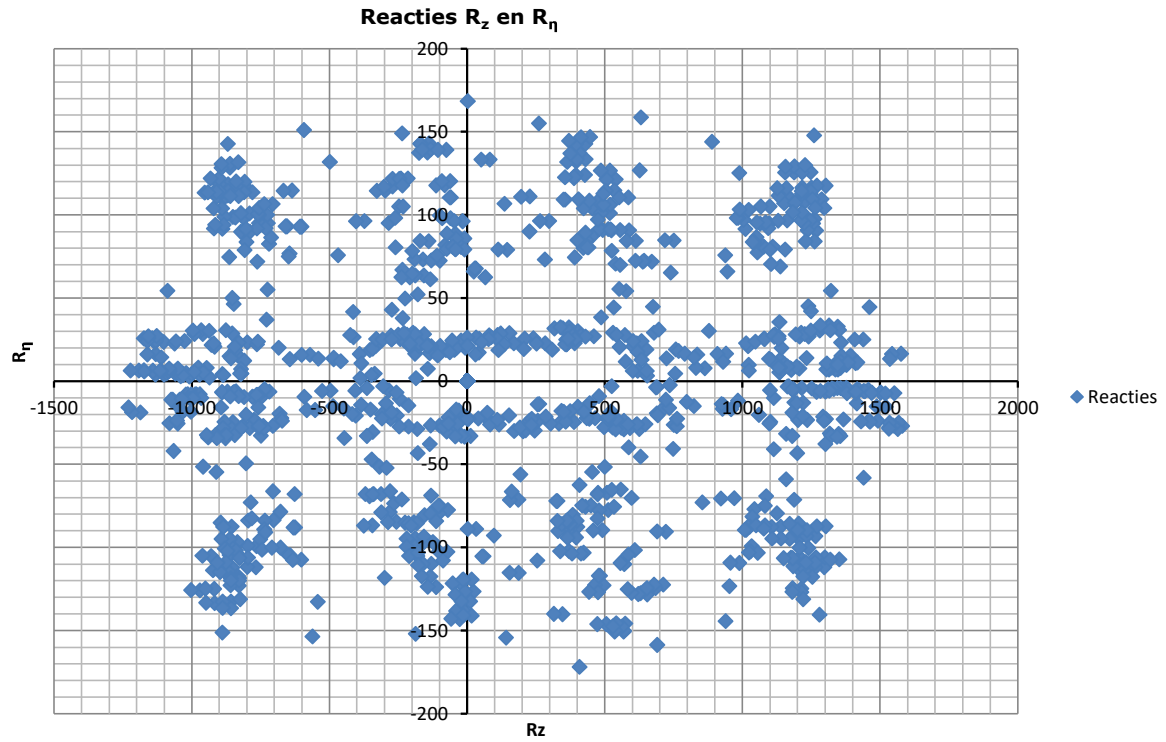
#### Maximum tension load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 130                    | 112                    | <b>633</b>             | 13                     | -171                   | -31                        | 648                        |
| 2     | SLS 3_90    | -174                   | 145                    | <b>-875</b>            | 21                     | 225                    | 32                         | -896                       |
| 3     | SLS 1a_90   | 157                    | 129                    | <b>-769</b>            | -20                    | 203                    | 33                         | -787                       |
| 4     | SLS 1a_0    | -95                    | 77                     | <b>461</b>             | -13                    | -122                   | -20                        | 472                        |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_90   | 226                    | 198                    | <b>1107</b>            | 19                     | -300                   | -55                        | 1133                       |
| 2     | SLS 1a_0    | -28                    | 7                      | <b>-123</b>            | 15                     | 25                     | -2                         | -126                       |
| 3     | SLS 7       | 62                     | 43                     | <b>-295</b>            | -13                    | 74                     | 9                          | -302                       |
| 4     | SLS 3_90    | -250                   | 219                    | <b>1244</b>            | -22                    | -332                   | -57                        | 1274                       |

Project: GT-RL380  
Tower: HC+0  
Number: 16





Project: GT-RL380  
 Tower: HC+0  
 Number: 16

**Conductor loads** Auteur: TBR  
Versie: v11.8

**Starting points**  
 Consequence class Verbouw CC2  
 Reference period 50 jaar

| ULS (strength)   |                            | NEN-EN50341-2-15:2019 |              |                  |            |          |          |                     |
|--|----------------------------|-----------------------|--------------|------------------|------------|----------|----------|---------------------|
| Load case  | description                | Temp<br>°C            | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|  |                            |                       | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a   | Wind                       | 10°                   | 1.15         | 1.15             | 0.00       | 1.40     | 0.00     | 0.0                 |
| ULS 1a_0,9   | Wind 0,9Gk only tower      | 10°                   | 0.90         | 1.15             | 0.00       | 1.40     | 0.00     | 0.0                 |
| ULS 1a_0,9_0,9   | Wind 0,9Gk conductors too  | 10°                   | 0.90         | 0.90             | 0.00       | 1.40     | 0.00     | 0.0                 |
| ULS 3  | Wind+ice                   | -5°                   | 1.15         | 1.15             | 0.00       | 0.42     | 1.30     | 0.0                 |
| ULS 3_0,9  | Wind+ice 0,9Gk             | -5°                   | 0.90         | 1.15             | 0.00       | 0.42     | 1.30     | 0.0                 |
| ULS 4  | Cold+wind                  | -20°                  | 1.15         | 1.15             | 0.00       | 0.28     | 0.00     | 0.0                 |
| ULS 4_0,9  | Cold+wind 0,9Gk            | -20°                  | 0.90         | 1.15             | 0.00       | 0.28     | 0.00     | 0.0                 |
| ULS 5a   | Torsional loads            | 10°                   | 1.00         | 1.00             | 1.00       | 0.00     | 0.00     | 1.0                 |
| ULS 5b   | Longitudinal loads         | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| ULS 6  | Construction + maintenance | 5°                    | 1.15         | 1.15             | 1.30       | 0.28     | 0.00     | 0.0                 |
| ULS 6_0,9  | Construction + maintenance | 5°                    | 1.15         | 1.15             | 0.00       | 0.28     | 0.00     | 0.0                 |
| ULS 7  | Permanent                  | 10°                   | 1.30         | 1.30             | 0.00       | 0.00     | 0.00     | 0.0                 |
| ULS 8  | Special                    | 10°                   | 1.00         | 1.00             | 0.00       | 0.00     | 0.00     | 1.0                 |
| SPLS (strength, for angle towers: absence of conductors) |                            |                       | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
|  |                            |                       | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SPLS 1a  | Wind                       | 10°                   | 1.15         | 1.15             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9  | Wind 0,9                   | 10°                   | 0.90         | 1.15             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 1a_0,9_0,9  | Wind 0,9                   | 10°                   | 0.90         | 0.90             | 0.0        | 0.78     | 0.00     | 0.0                 |
| SPLS 3   | Wind+ice                   | -5°                   | 1.15         | 1.15             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 3_0,9   | Wind+ice 0,9               | -5°                   | 0.90         | 1.15             | 0.0        | 0.36     | 0.34     | 0.0                 |
| SPLS 4   | Cold+wind                  | -20°                  | 1.15         | 1.15             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 4_0,9   | Cold+wind 0,9              | -20°                  | 0.90         | 1.15             | 0.0        | 0.24     | 0.00     | 0.0                 |
| SPLS 6   | Maintenance                | 5°                    | 1.15         | 1.15             | 1.2        | 0.24     | 0.0      | 0.0                 |
| SPLS 6_0,9   | Maintenance                | 5°                    | 1.15         | 1.15             | 0.0        | 0.24     | 0.0      | 0.0                 |
| SLS (deformations, fatigue, EDS)                         |                            |                       | $G_k$        |                  | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SLS 1a   | Wind                       | 10°                   | 1.00         | 1.00             | 0.0        | 1.00     | 0.0      | 0.0                 |
| SLS 3  | Wind+ice                   | -5°                   | 1.00         | 1.00             | 0.0        | 0.30     | 1.00     | 0.0                 |
| SLS 4  | Wind                       | -20°                  | 1.00         | 1.00             | 0.0        | 0.20     | 0.0      | 0.0                 |
| SLS 6  | Maintenance                | 5°                    | 1.00         | 1.00             | 0.0        | 0.20     | 0.0      | 0.0                 |
| SLS 7  | EDS, no wind               | 10°                   | 1.00         | 1.00             | 0.0        | 0.00     | 0.0      | 0.0                 |

Number of wind directions 6  
 Number of load combinations for ULS 54  
 Number of load combinations for SPLS 222  
 Number of load combinations for SLS 15  
 Number of concentrated loads 5238

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

### Summary table - Conductor loads

The four tables below show:

- The maximum conductor load in the global axis system, split into proportion of back and ahead span
- The combined conductor load (Ba+Ah) in the global axis system with the maximum tensile force in the local axes. Components Fx and Fy as absolute values
- The everyday (EDS) values of the combined conductor loads (Ba+Ah) with corresponding tensile forces
- Check for uplift, where a negative value indicates uplift

Note: Maximum values for Fx, Fy and Fz do not necessarily belong to the same load combination.

#### Maximum values for back and ahead span

| Geleider    | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|-------------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1         | -47.4         | 39.7          | 21.8          | 26.6          | 8.5           | 5.7           |
| 380ct1f1    | -112.8        | 105.3         | 50.3          | 69.9          | 24.6          | 20.5          |
| 380ct1f2    | -112.8        | 105.3         | 50.3          | 69.9          | 24.6          | 20.5          |
| 380ct1f3    | -114.6        | 107.7         | 55.4          | 75.8          | 24.6          | 20.5          |
| 380ct2f1    | -112.8        | 105.3         | 50.3          | 69.9          | 24.6          | 20.5          |
| 380ct2f2    | -112.8        | 105.3         | 50.3          | 69.9          | 24.6          | 20.5          |
| 380ct2f3    | -114.6        | 107.7         | 55.4          | 75.8          | 24.6          | 20.5          |
| bl2         | -47.7         | 39.2          | 21.9          | 26.3          | 8.4           | 5.7           |
| V-ketting 1 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |
| V-ketting 2 | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           | 0.0           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider    | SLS 1a | SLS 4 | SLS 7 |
|-------------|--------|-------|-------|
| bl1         | 331.7  | 331.7 | 331.7 |
| 380ct1f1    | 331.7  | 331.7 | 331.7 |
| 380ct1f2    | 331.7  | 331.7 | 331.7 |
| 380ct1f3    | 331.7  | 331.7 | 331.7 |
| 380ct2f1    | 331.7  | 331.7 | 331.7 |
| 380ct2f2    | 331.7  | 331.7 | 331.7 |
| 380ct2f3    | 331.7  | 331.7 | 331.7 |
| bl2         | 331.7  | 331.7 | 331.7 |
| V-ketting 1 |        |       |       |
| V-ketting 2 |        |       |       |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider    | ULS 1a | ULS 3 |
|-------------|--------|-------|
| bl1         | 331.7  | 331.7 |
| 380ct1f1    | 331.7  | 331.7 |
| 380ct1f2    | 331.7  | 331.7 |
| 380ct1f3    | 331.7  | 331.7 |
| 380ct2f1    | 331.7  | 331.7 |
| 380ct2f2    | 331.7  | 331.7 |
| 380ct2f3    | 331.7  | 331.7 |
| bl2         | 331.7  | 331.7 |
| V-ketting 1 |        |       |
| V-ketting 2 |        |       |

#### Envelop of weight span over all combinations (incl. 0,9 combinations)

| For all conductors | Wind / Weight span ratio |
|--------------------|--------------------------|
| Max. weight span   | 331.7 m / 1.000 -        |
| Min. weight span   | 331.7 m / 1.000 -        |

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 Tower: HC+0  
 Number: 16

**Maximum values back + ahead span      Maximum tension in conductor**

| Geleider    | Maximum values back + ahead span |            |            | Maximum tension in conductor |               |
|-------------|----------------------------------|------------|------------|------------------------------|---------------|
|             | Fx<br>[kN]                       | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN]                | Ft_ah<br>[kN] |
| bl1         | 27.9                             | 46.1       | 8.5        | -52.0                        | 47.7          |
| 380ct1f1    | 94.7                             | 114.5      | 24.6       | -123.3                       | 125.7         |
| 380ct1f2    | 94.7                             | 114.5      | 24.6       | -123.3                       | 125.7         |
| 380ct1f3    | 94.8                             | 118.0      | 24.6       | -125.7                       | 129.0         |
| 380ct2f1    | 94.7                             | 114.5      | 24.6       | -123.3                       | 125.7         |
| 380ct2f2    | 94.7                             | 114.5      | 24.6       | -123.3                       | 125.7         |
| 380ct2f3    | 94.8                             | 118.0      | 24.6       | -125.7                       | 129.0         |
| bl2         | 28.0                             | 45.9       | 8.4        | -52.3                        | 47.1          |
| V-ketting 1 | 2.4                              | 2.4        | 3.9        | 0.0                          |               |
| V-ketting 2 | 2.4                              | 2.4        | 3.9        | 0.0                          |               |

**EDS-loads conductor**

| Geleider    | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|-------------|------|------|------|-------|-------|
|             | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1         | 11.3 | 6.6  | 2.1  | -13.8 | 13.1  |
| 380ct1f1    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct1f2    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct1f3    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct2f1    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct2f2    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| 380ct2f3    | 54.4 | 31.9 | 15.0 | -62.7 | 63.0  |
| bl2         | 11.0 | 6.5  | 2.1  | -13.7 | 12.8  |
| V-ketting 1 | 0.0  | 0.0  | 3.0  | 0.0   |       |
| V-ketting 2 | 0.0  | 0.0  | 3.0  | 0.0   |       |

**1 Control uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4 bl1            | 0.0   | 0.0   |
| 380ct1f1             | 0.0   | 0.0   |
| 380ct1f2             | 0.0   | 0.0   |
| 380ct1f3             | 0.0   | 0.0   |
| 380ct2f1             | 0.0   | 0.0   |
| 380ct2f2             | 0.0   | 0.0   |
| 380ct2f3             | 0.0   | 0.0   |
| bl2                  | 0.0   | 0.0   |
| V-ketting 1          | 0.0   |       |
| V-ketting 2          | 0.0   |       |

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

**ULS foundation loads for LC 1 and 3, wind perpendicular to the line or bisector and EDS, from conductors**

| Combination       | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | -17           | 711           | 202           | 23232          | -574           | -6             |
| ULS 1a_0,9_0      |             | 8             | 400           | 201           | 12991          | 267            | 52             |
| ULS 1a_0,9_0,9_90 |             | -2            | 670           | 158           | 21898          | -101           | -5             |
| ULS 3_0           |             | -68           | 677           | 297           | 22267          | -2335          | 1              |
| SLS 7             |             | -30           | 345           | 176           | 11187          | -976           | -6             |

**ULS foundation loads, LC 1 and 3, wind perpendicular to the line or bisector and EDS, total conductors and tower**

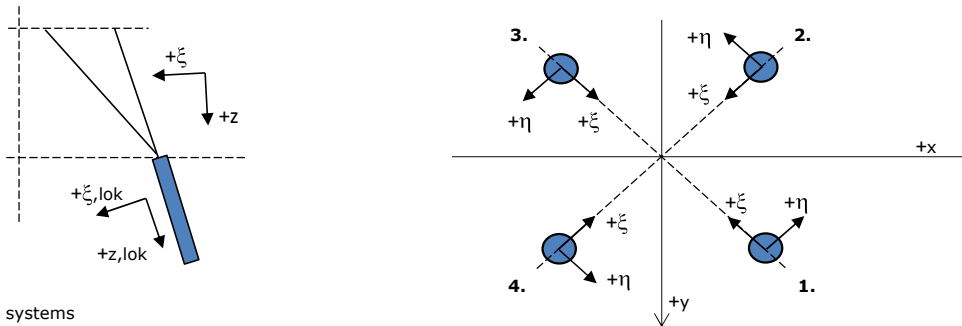
| Combination       | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | -17           | 894           | 777           | 27969          | -574           | -6             |
| ULS 1a_0,9_0,9_90 | -2            | 853           | 608           | 26635          | -101           | -5             |
| SLS 7             | -30           | 345           | 676           | 11187          | -976           | -6             |

**Foundation loads, selection of load combinations based on greatest value**

| Combination              | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|--------------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90                | -17           | 894           | 777           | <b>27969</b>   | -574           | -6             |
| SPLS 3_135 Ah All Cts    | -570          | 253           | 744           | 8017           | <b>-18165</b>  | -13            |
| SPLS 6a_90 Ba Ct1 Ah Ct1 | 296           | 438           | 780           | 14269          | 9595           | <b>-4536</b>   |
| ULS 1a_0,9_0,9_120.38    | 95            | 848           | 608           | <b>26522</b>   | <b>3899</b>    | -36            |

Note: Largest values can appear in multiple combinations, one combination is displayed.

**Support reactions per leg**



**Maximum compression load**

| Index | Combination           | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|-----------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_120.38         | 309           | 286           | <b>1576</b>   | 16               | -421            | -73                   | 1614                |
| 2     | SPLS 1a_0 Ba All Cts  | 106           | -141          | <b>633</b>    | 24               | -175            | -35                   | 648                 |
| 3     | SPLS 3_135 Ah All Cts | -106          | -143          | <b>647</b>    | -26              | -176            | -33                   | 663                 |
| 4     | ULS 3_90              | -316          | 278           | <b>1580</b>   | -27              | -420            | -71                   | 1618                |

**Maximum tension load**

| Index | Combination               | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|---------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 3_0,9_135 Ah All Cts | -38           | -73           | <b>-308</b>   | 25               | 78              | 10                    | -315                |
| 2     | ULS 3_0,9_90              | -233          | 197           | <b>-1175</b>  | 26               | 304             | 45                    | -1203               |
| 3     | ULS 1a_0,9_0,9_120.38     | 239           | 216           | <b>-1231</b>  | -16              | 322             | 50                    | -1260               |
| 4     | SPLS 1a_0,9_0 Ba All Cts  | 42            | -74           | <b>-310</b>   | -22              | 82              | 13                    | -318                |

**Maximum torsional load (positive)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ah Ct1 Ah Ct2 | 231           | 7             | 631           | <b>159</b>       | -168            | -29                   | 646                 |
| 2     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -117          | -121          | 2             | <b>169</b>       | -3              | -3                    | 2                   |
| 3     | SPLS 6a_90 Ba Ct2 Ah Ct2 | 59            | 261           | -870          | <b>143</b>       | 227             | 34                    | -891                |
| 4     | SPLS 6a_90 Ah Ct1 Ba Ct1 | -140          | 324           | 1227          | <b>130</b>       | -328            | -57                   | 1256                |

**Maximum torsional load (negative)**

| Index | Combination              | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | SPLS 6a_90 Ba Ct1 Ah Ct1 | 142           | 341           | 1280          | <b>-140</b>      | -341            | -59                   | 1311                |
| 2     | SPLS 6a_90 Ah Ct2 Ah Ct1 | -7            | 195           | -543          | <b>-133</b>      | 143             | 23                    | -556                |
| 3     | SPLS 6a_90 Ah Ct2 Ba Ct2 | 81            | -138          | 140           | <b>-154</b>      | -40             | -9                    | 144                 |
| 4     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -201          | -43           | 407           | <b>-172</b>      | -112            | -22                   | 417                 |

Project: GT-RLL380  
 Tower: HC+0  
 Number: 16

#### Combination Ftensile+Fhor

| Index | Combination                  | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SPLS 6a_90 Ah All Cts Ba Ct1 | 8                      | -87                    | <b>-235</b>            | <b>67</b>              | 55                     | 4                          | -241                       |
| 2     | SPLS 3_0,9_90 Ah Ct1         | -256                   | 84                     | <b>-932</b>            | <b>122</b>             | 241                    | 35                         | -954                       |
| 3     | SPLS 3_0,9_120.38 Ba Ct1     | 271                    | 93                     | <b>-1003</b>           | <b>-126</b>            | 257                    | 36                         | -1027                      |
| 4     | SPLS 1a_0,9_0 Ba All Cts     | 42                     | -74                    | <b>-310</b>            | <b>-22</b>             | 82                     | 13                         | -318                       |

#### Permanent load

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 130                    | 112                    | 633                    | 13                     | -171                   | -31                        | 648                        |
| 2     | SLS 7       | -76                    | 61                     | -384                   | 11                     | 97                     | 12                         | -393                       |
| 3     | SLS 7       | 62                     | 43                     | -295                   | -13                    | 74                     | 9                          | -302                       |
| 4     | SLS 7       | -145                   | 129                    | 722                    | -11                    | -194                   | -35                        | 739                        |

#### Envelope of load combinations for all of the legs

| Index                | Combination              | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|----------------------|--------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. pressure        | ULS 3_90                 | -316                   | 278                    | <b>1580</b>            | -27                    | -420                   | -71                        | 1618                       |
| Max. tension         | ULS 1a_0,9_0,9_120.38    | 239                    | 216                    | <b>-1231</b>           | -16                    | 322                    | 50                         | -1260                      |
| Max. pos. torsie     | SPLS 6a_90 Ba Ct2 Ah Ct2 | -117                   | -121                   | 2                      | <b>169</b>             | -3                     | -3                         | 2                          |
| Max. neg. torsie     | SPLS 6a_90 Ba Ct1 Ah Ct1 | -201                   | -43                    | 407                    | <b>-172</b>            | -112                   | -22                        | 417                        |
| Comb. tension+torsie | SPLS 3_0,9_120.38 Ba Ct1 | 271                    | 93                     | <b>-1003</b>           | <b>-126</b>            | 257                    | 36                         | -1027                      |

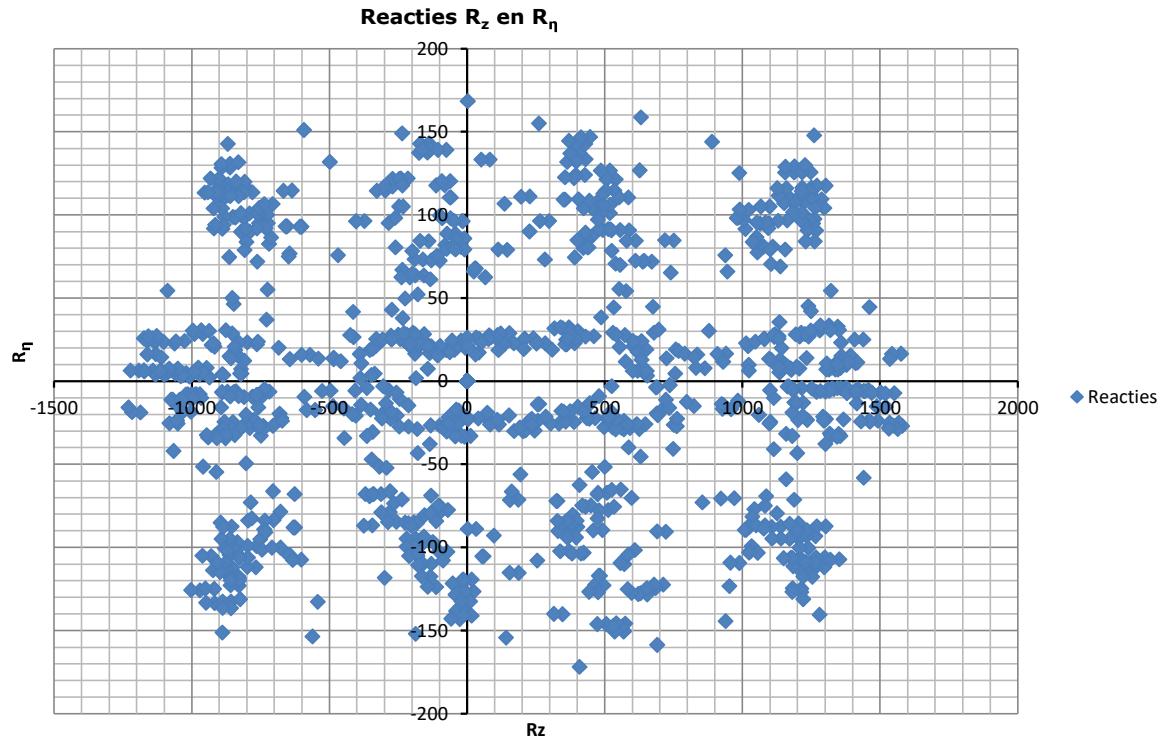
#### Maximum tension load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7       | 130                    | 112                    | <b>633</b>             | 13                     | -171                   | -31                        | 648                        |
| 2     | SLS 3_90    | -185                   | 154                    | <b>-929</b>            | 22                     | 239                    | 34                         | -951                       |
| 3     | SLS 1a_90   | 164                    | 136                    | <b>-803</b>            | -20                    | 212                    | 34                         | -823                       |
| 4     | SLS 1a_0    | -92                    | 74                     | <b>445</b>             | -13                    | -117                   | -19                        | 456                        |

#### Maximum compression load - SLS

| Index | Combination | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_90   | 233                    | 204                    | <b>1141</b>            | 20                     | -309                   | -57                        | 1169                       |
| 2     | SLS 1a_0    | -25                    | 3                      | <b>-107</b>            | 15                     | 20                     | -3                         | -110                       |
| 3     | SLS 7       | 62                     | 43                     | <b>-295</b>            | -13                    | 74                     | 9                          | -302                       |
| 4     | SLS 3_90    | -261                   | 229                    | <b>1303</b>            | -23                    | -347                   | -59                        | 1335                       |

Project: GT-RLL380  
Tower: HC+0  
Number: 16





## **APPENDIX B**

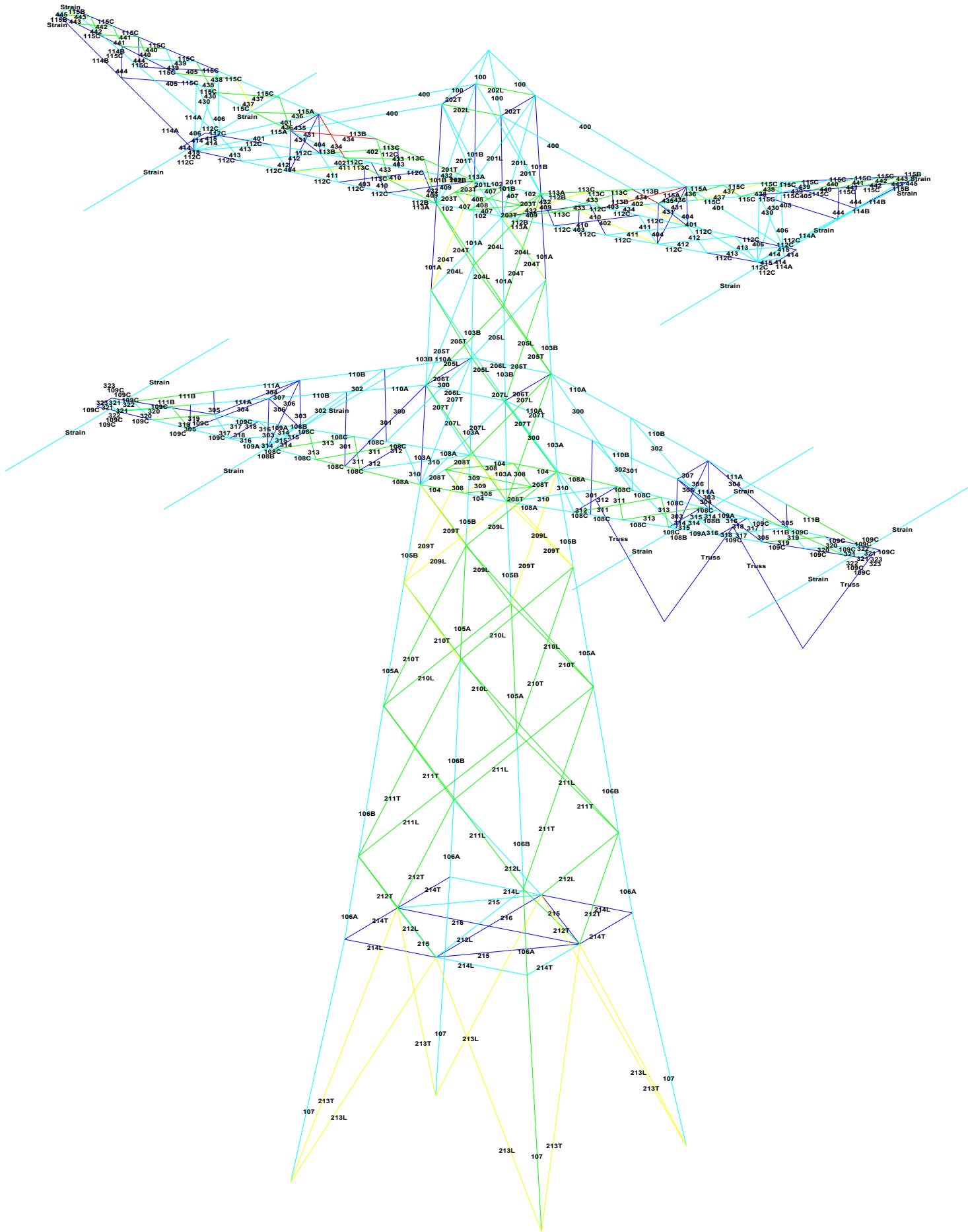
### **Resultaten PLS-TOWER**

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Deze Appendix bevat de resultaten uit PLS-TOWER voor de verschillende masten.

Resultaten opgenomen voor:

- Masttype HB+0 (68)
- Masttype HB+0 (78)
- Masttype HC+0 (16)
- Masttype HS+0 (26)



1 (m)









21-05-21  
 Date  
 Author  
 Version

Assessment of groups for initial mast (aft/fore level).

ZW380 Oost  
 HB+0  
 68

| Group Label | Description                     | Profile    | Steel Quality | Brk       | RLX  | RLY  | RLZ  | Slenderness | Compression | Load Case (Compression)          | Buckling | Shear (Comp) | Bearing (Comp) | U.C. (Comp) | Exceedance (Comp) | Tension | Load Case (Tension)          | Net Section | Shear (Tens) | Bearing (Tens) | U.C. (Tens) | Exceedance (Tens) |
|-------------|---------------------------------|------------|---------------|-----------|------|------|------|-------------|-------------|----------------------------------|----------|--------------|----------------|-------------|-------------------|---------|------------------------------|-------------|--------------|----------------|-------------|-------------------|
| 402         | Twede DWSRM - Diagonal bracing  | 55x55x6    | S235          | 1916e-8.R | 1.00 | 1.00 | 1.00 | 326         | -10.1       | U.S 8a Bb 12                     | 12.9     | 60.3         | 51.8           | 0.78        | 0.00              | 27.0    | U.S 3_0                      | 55.3        | 50.4         | 39.2           | 0.00        | 0.00              |
| 403         | Twede DWSRM - Vertical bracing  | 50x50x5    | S235          | 1916e-8.R | 1.00 | 1.00 | 1.00 | 82          | 0.0         | SPLS 6a_90 Ah All Cts Ba C11     | 55.5     | 60.3         | 43.2           | 0.00        | 0.00              | 2.7     | U.S 5a Ah 22                 | 37.4        | 60.3         | 25.7           | 0.11        | 0.11              |
| 404         | Twede DWSRM - Vertical bracing  | 65x65x6    | S235          | 2916e-8.R | 1.00 | 1.00 | 1.00 | 132         | -10.5       | SPLS 6a_90 Ah All Cts Ba C11     | 73.0     | 120.6        | 103.7          | 0.14        | 0.14              | 9.8     | SPLS 3_105.975 Ba All Cts    | 80.5        | 120.6        | 89.5           | 0.12        | 0.12              |
| 405         | Twede DWSRM - Vertical bracing  | 55x55x6    | S235          | 1916e-8.R | 0.50 | 1.00 | 0.50 | 161         | -13.4       | SPLS 6a_90 Ah All Cts Ba C11     | 29.1     | 60.3         | 51.8           | 0.45        | 0.45              | 6.3     | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 36.2           | 0.16        | 0.16              |
| 406         | Twede DWSRM - Vertical bracing  | 55x55x6    | S235          | 1916e-8.R | 0.50 | 1.00 | 0.50 | 161         | -15.4       | SPLS 6a_90 Ba C11 Ah C11         | 28.1     | 406.7        | 311.0          | 0.57        | 0.57              | 167.5   | SPLS 6a_90 Ba C11 Ah C11     | 263.0       | 406.7        | 285.8          | 0.64        | 0.64              |
| 407         | Twede DWSRM - Diagonal diphragm | 120x120x8  | S235          | 3924e-8.R | 1.00 | 1.00 | 1.00 | 87          | -12.0       | U.S 7                            | 16.9     | 60.3         | 43.2           | 0.71        | 0.71              | 6.0     | SPLS 6a_90 Ba All Cts Ah C11 | 37.4        | 60.3         | 25.7           | 0.00        | 0.00              |
| 408         | Twede DWSRM - Crossing diagonal | 80x80x8    | S235          | 1916e-8.R | 0.50 | 1.00 | 0.50 | 193         | -49.4       | SPLS 6a_90 Ba All Cts Ah C11     | 149.6    | 188.2        | 172.8          | 0.33        | 0.33              | 51.7    | SPLS 6a_90 Ba All Cts Ah C11 | 162.8       | 188.2        | 157.1          | 0.17        | 0.17              |
| 409         | Twede DWSRM - Crossing diagonal | 80x80x8    | S235          | 2920e-8.R | 0.52 | 0.52 | 0.52 | 114         | -24.5       | SPLS 6a_90 Ba C11 Ah C11         | 138.2    | 188.2        | 172.8          | 0.16        | 0.16              | 35.1    | SPLS 6a_90 Ba All Cts Ah C11 | 167.8       | 188.2        | 157.1          | 0.22        | 0.22              |
| 410         | Twede DWSRM - Crossing diagonal | 80x80x8    | S235          | 2920e-8.R | 0.53 | 0.53 | 0.53 | 111         | -38.3       | SPLS 6a_90 Ba C11 Ah C11         | 141.6    | 188.2        | 172.8          | 0.27        | 0.27              | 25.9    | SPLS 6a_90 Ba All Cts Ah C11 | 174.4       | 188.2        | 157.1          | 0.17        | 0.17              |
| 411         | Twede DWSRM - Crossing diagonal | 80x80x8    | S235          | 3920e-8.R | 0.53 | 0.53 | 0.53 | 105         | -49.4       | SPLS 6a_90 Ba All Cts Ah C11     | 149.6    | 282.2        | 259.2          | 0.33        | 0.33              | 51.7    | SPLS 6a_90 Ba All Cts Ah C11 | 162.8       | 282.2        | 223.4          | 0.32        | 0.32              |
| 412         | Twede DWSRM - Crossing diagonal | 80x80x8    | S235          | 3920e-8.R | 0.53 | 0.53 | 0.53 | 105         | -49.4       | SPLS 6a_90 Ba All Cts Ah C11     | 149.6    | 282.2        | 259.2          | 0.33        | 0.33              | 51.7    | SPLS 6a_90 Ba All Cts Ah C11 | 162.8       | 282.2        | 223.4          | 0.32        | 0.32              |
| 413         | Twede DWSRM - Crossing diagonal | 80x80x8    | S235          | 2920e-8.R | 0.50 | 1.00 | 0.50 | 191         | -40.3       | SPLS 6a_90 Ba All Cts Ah C11     | 142.4    | 188.2        | 172.8          | 0.40        | 0.40              | 62.6    | SPLS 6a_90 Ba All Cts Ah C11 | 167.8       | 188.2        | 157.1          | 0.22        | 0.22              |
| 414         | Twede DWSRM - Crossing diagonal | 100x100x11 | S235          | 3916e-8.R | 1.00 | 1.00 | 1.00 | 101         | -40.3       | SPLS 6a_90 Ba All Cts Ah C11     | 142.4    | 188.2        | 172.8          | 0.40        | 0.40              | 62.6    | SPLS 6a_90 Ba All Cts Ah C11 | 167.8       | 188.2        | 157.1          | 0.22        | 0.22              |
| 415         | Twede DWSRM - Diagonal          | 65x65x6    | S235          | 1916e-8.R | 0.55 | 0.55 | 0.55 | 166         | -25.2       | SPLS 6a_90 Ba All Cts Ah C11     | 106.7    | 180.9        | 155.5          | 0.25        | 0.25              | 25.3    | SPLS 6a_90 Ba All Cts Ah C11 | 101.1       | 180.9        | 134.4          | 0.25        | 0.25              |
| 430         | Twede DWSRM - Crossing diagonal | 55x55x6    | S235          | 1916e-8.R | 0.35 | 0.35 | 0.35 | 174         | -12.6       | SPLS 6a_90 Ah All Cts Ba C11     | 35.1     | 60.3         | 51.8           | 0.36        | 0.36              | 11.3    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 39.2           | 0.29        | 0.29              |
| 431         | Twede DWSRM - Crossing diagonal | 55x55x6    | S235          | 2916e-8.R | 0.51 | 0.51 | 0.51 | 174         | -14.5       | SPLS 6a_90 Ah All Cts Ba C11     | 35.9     | 120.6        | 103.7          | 0.14        | 0.14              | 10.8    | SPLS 6a_90 Ah All Cts Ba C11 | 55.7        | 120.6        | 89.5           | 0.52        | 0.52              |
| 432         | Twede DWSRM - Crossing diagonal | 55x55x6    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 177         | -24.7       | SPLS 6a_90 Ah All Cts Ba C11     | 35.7     | 60.3         | 51.8           | 0.69        | 0.69              | 27.0    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 39.2           | 0.69        | 0.69              |
| 433         | Twede DWSRM - Crossing diagonal | 55x55x6    | S235          | 1916e-8.R | 0.54 | 0.54 | 0.54 | 173         | -34.5       | SPLS 6a_90 Ah All Cts Ba C11     | 33.2     | 60.3         | 51.8           | 1.04        | 1.04              | 31.8    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 39.2           | 0.81        | 0.81              |
| 434         | Twede DWSRM - Horizontal        | 55x55x6    | S235          | 1916e-8.R | 1.00 | 1.00 | 1.00 | 143         | -25.2       | SPLS 3_106.025 Ah All Cts Ba C11 | 11.7     | 60.3         | 51.8           | 0.08        | 0.08              | 1.0     | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 39.2           | 0.00        | 0.00              |
| 435         | Twede DWSRM - Horizontal        | 55x55x6    | S235          | 1916e-8.R | 1.00 | 1.00 | 1.00 | 143         | -25.2       | SPLS 3_106.025 Ah All Cts Ba C11 | 11.7     | 60.3         | 51.8           | 0.08        | 0.08              | 1.0     | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 39.2           | 0.00        | 0.00              |
| 436         | Twede DWSRM - Horizontal        | 55x55x6    | S235          | 1916e-8.R | 1.00 | 1.00 | 1.00 | 143         | -25.2       | SPLS 3_106.025 Ah All Cts Ba C11 | 11.7     | 60.3         | 51.8           | 0.08        | 0.08              | 1.0     | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 39.2           | 0.00        | 0.00              |
| 437         | Twede DWSRM - Crossing diagonal | 50x50x5    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 143         | -20.0       | SPLS 6a_90 Ah All Cts Ba C11     | 33.9     | 60.3         | 43.2           | 0.59        | 0.59              | 10.8    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 25.7           | 0.77        | 0.77              |
| 438         | Twede DWSRM - Crossing diagonal | 50x50x5    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 131         | -16.1       | SPLS 6a_90 Ah All Cts Ba C11     | 37.4     | 60.3         | 43.2           | 0.43        | 0.43              | 16.7    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 25.7           | 0.65        | 0.65              |
| 439         | Twede DWSRM - Crossing diagonal | 50x50x5    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 107         | -10.6       | SPLS 6a_90 Ah All Cts Ba C11     | 46.0     | 60.3         | 43.2           | 0.54        | 0.54              | 10.8    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 25.7           | 0.41        | 0.41              |
| 440         | Twede DWSRM - Crossing diagonal | 50x50x5    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 88          | -14.6       | SPLS 6a_90 Ah All Cts Ba C11     | 53.6     | 60.3         | 43.2           | 0.34        | 0.34              | 14.9    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 25.7           | 0.58        | 0.58              |
| 441         | Twede DWSRM - Crossing diagonal | 50x50x5    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 88          | -14.6       | SPLS 6a_90 Ah All Cts Ba C11     | 53.6     | 60.3         | 43.2           | 0.34        | 0.34              | 14.9    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 25.7           | 0.58        | 0.58              |
| 442         | Twede DWSRM - Crossing diagonal | 50x50x5    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 77          | -16.7       | SPLS 6a_90 Ah All Cts Ba C11     | 58.7     | 60.3         | 43.2           | 0.39        | 0.39              | 15.7    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 25.7           | 0.61        | 0.61              |
| 443         | Twede DWSRM - Crossing diagonal | 50x50x5    | S235          | 1916e-8.R | 0.53 | 0.53 | 0.53 | 73          | -18.2       | SPLS 6a_90 Ah All Cts Ba C11     | 58.0     | 60.3         | 43.2           | 0.42        | 0.42              | 16.8    | SPLS 6a_90 Ah All Cts Ba C11 | 55.3        | 60.3         | 25.7           | 0.77        | 0.77              |
| 444         | Twede DWSRM - Crossing diagonal | 160x160x12 | S235          | 2920e-8.R | 1.00 | 1.00 | 1.00 | 47          | 0.0         | SPLS 3_14_106.025 Ba All Cts     | 443.0    | 188.2        | 162.0          | 0.00        | 0.00              | 39.0    | U.S 3_0 9_106.025            | 547.9       | 188.2        | 156.9          | 0.30        | 0.30              |





Assessment of groups for strengthened mast (afkeur level)

Date 21-05-21  
 Author KCh  
 Version 1.0

ZW380 Oost  
 HB+0  
 68

| Stalgroep | Omschrijving Profiel  | Staalsoort | Bouten    | RLX  | RLY  | RZ   | Slankheid | Drak Combinatie trek        | Krak  | Afschaving | Stuik (Gru) | U.C. (Gru) | Opm. | Trek Combinatie trek        | Nettoopp. | Afschuur | Stuik (trek) | U.C. (trek) |
|-----------|-----------------------|------------|-----------|------|------|------|-----------|-----------------------------|-------|------------|-------------|------------|------|-----------------------------|-----------|----------|--------------|-------------|
| 322       | Eerste DWSR 1004120X8 | S235       | 2M26-8-8T | 1,00 | 1,00 | 1,00 | 2,00      | -14,3 ULS 3_0,9,9,10,5      | 396,5 | 270,1      | 311,5       | 0,07       |      | 34 SMLS 68_90 BA CII Ah     | 225,1     | 270,9    | 313,7        | 0,06        |
| 323       | Tweede DWSR 1004120X8 | S235       | 2M26-8-8T | 1,00 | 1,00 | 1,00 | 2,00      | -14,3 ULS 3_0,9,9,10,5      | 396,5 | 270,1      | 311,5       | 0,07       |      | 34 SMLS 68_90 BA CII Ah     | 225,1     | 270,9    | 313,7        | 0,06        |
| 400       | Tweede DWSR 1204120X8 | S235       | 4M26-8-8T | 1,00 | 1,00 | 1,00 | 3,02      | -0,8 SMLS 11_0,9,9,10,5     | 113,0 | 54,2       | 414,7       | 0,00       |      | 160,7 SMLS 68_90 AN All Cts | 343,3     | 542,2    | 354,5        | 0,47        |
| 401       | Tweede DWSR 1204120X8 | S235       | 4M26-8-8T | 1,00 | 1,00 | 1,00 | 3,02      | -0,8 SMLS 11_0,9,9,10,5     | 113,0 | 54,2       | 414,7       | 0,00       |      | 126,3 ULS 3_0               | 343,3     | 542,2    | 354,5        | 0,37        |
| 402       | Tweede DWSR 55X55X6   | S235       | 1M16-8-8T | 1,00 | 1,00 | 1,00 | 3,02      | -10,1 ULS 5a B12            | 12,9  | 6,3        | 51,8        | 0,78       |      | 0,0 ULS 6a B12              | 55,3      | 60,3     | 39,2         | 0,00        |
| 403       | Tweede DWSR 55X55X6   | S235       | 1M16-8-8T | 1,00 | 1,00 | 1,00 | 3,02      | -10,1 ULS 5a B12            | 12,9  | 6,3        | 51,8        | 0,78       |      | 0,0 ULS 6a B12              | 55,3      | 60,3     | 39,2         | 0,00        |
| 404       | Tweede DWSR 55X55X6   | S235       | 2M16-8-8T | 1,00 | 1,00 | 1,00 | 3,02      | -10,2 SMLS 6a_90 AN All Cts | 73,0  | 120,6      | 103,7       | 0,14       |      | 5,6 SMLS 3_105,97,5 Ba All  | 80,5      | 120,6    | 85,5         | 0,12        |
| 405       | Tweede DWSR 55X55X6   | S235       | 2M16-8-8T | 1,00 | 1,00 | 1,00 | 3,02      | -10,2 SMLS 6a_90 AN All Cts | 73,0  | 120,6      | 103,7       | 0,14       |      | 5,6 SMLS 3_105,97,5 Ba All  | 80,5      | 120,6    | 85,5         | 0,12        |
| 406       | Tweede DWSR 55X55X6   | S235       | 1M16-8-8T | 0,50 | 1,00 | 1,00 | 1,00      | -13,1 SMLS 6a_90 AN All Cts | 29,1  | 60,3       | 51,8        | 0,45       |      | 6,3 SMLS 6a_90 AN All Cts   | 55,3      | 60,3     | 25,7         | 0,21        |
| 407       | Tweede DWSR 1204120X8 | S235       | 3M26-8-8T | 1,00 | 1,00 | 1,00 | 1,00      | -13,1 SMLS 6a_90 AN All Cts | 29,1  | 60,3       | 51,8        | 0,45       |      | 6,3 SMLS 6a_90 AN All Cts   | 55,3      | 60,3     | 25,7         | 0,21        |
| 408       | Tweede DWSR 55X55X6   | S235       | 3M26-8-8T | 1,00 | 1,00 | 1,00 | 1,00      | -13,1 SMLS 6a_90 AN All Cts | 29,1  | 60,3       | 51,8        | 0,45       |      | 6,3 SMLS 6a_90 AN All Cts   | 55,3      | 60,3     | 25,7         | 0,21        |
| 409       | Tweede DWSR 55X55X6   | S235       | 2M26-8-8T | 0,52 | 0,52 | 0,52 | 1,19      | -13,1 SMLS 6a_90 AN All Cts | 29,1  | 60,3       | 51,8        | 0,45       |      | 167,5 SMLS 68_90 BA CII Ah  | 263,0     | 406,7    | 268,9        | 0,64        |
| 410       | Tweede DWSR 55X55X6   | S235       | 2M26-8-8T | 0,52 | 0,52 | 0,52 | 1,19      | -13,1 SMLS 6a_90 AN All Cts | 29,1  | 60,3       | 51,8        | 0,45       |      | 167,5 SMLS 68_90 BA CII Ah  | 263,0     | 406,7    | 268,9        | 0,64        |
| 411       | Tweede DWSR 80X80X8   | S235       | 2M26-8-8T | 0,52 | 0,52 | 0,52 | 1,14      | -22,5 SMLS 6a_90 BA CII Ah  | 138,2 | 188,2      | 172,8       | 0,54       |      | 17,7 SMLS 68_90 BA All Cts  | 138,0     | 188,2    | 152,8        | 0,13        |
| 412       | Tweede DWSR 80X80X8   | S235       | 2M26-8-8T | 0,52 | 0,52 | 0,52 | 1,14      | -22,5 SMLS 6a_90 BA CII Ah  | 138,2 | 188,2      | 172,8       | 0,54       |      | 17,7 SMLS 68_90 BA All Cts  | 138,0     | 188,2    | 152,8        | 0,13        |
| 413       | Tweede DWSR 80X80X8   | S235       | 2M26-8-8T | 0,53 | 0,53 | 0,53 | 1,11      | -38,3 SMLS 6a_90 BA CII Ah  | 141,6 | 188,2      | 172,8       | 0,27       |      | 35,1 SMLS 6a_90 BA CII Ah   | 167,8     | 188,2    | 157,1        | 0,22        |
| 414       | Tweede DWSR 100465X11 | S235       | 3M26-8-8T | 0,53 | 0,53 | 0,53 | 1,03      | -38,3 SMLS 6a_90 BA CII Ah  | 141,6 | 188,2      | 172,8       | 0,27       |      | 35,1 SMLS 6a_90 BA CII Ah   | 167,8     | 188,2    | 157,1        | 0,22        |
| 415       | Tweede DWSR 100465X11 | S235       | 3M26-8-8T | 0,53 | 0,53 | 0,53 | 1,03      | -38,3 SMLS 6a_90 BA CII Ah  | 141,6 | 188,2      | 172,8       | 0,27       |      | 35,1 SMLS 6a_90 BA CII Ah   | 167,8     | 188,2    | 157,1        | 0,22        |
| 416       | Tweede DWSR 100465X11 | S235       | 3M26-8-8T | 0,53 | 0,53 | 0,53 | 1,03      | -38,3 SMLS 6a_90 BA CII Ah  | 141,6 | 188,2      | 172,8       | 0,27       |      | 35,1 SMLS 6a_90 BA CII Ah   | 167,8     | 188,2    | 157,1        | 0,22        |
| 417       | Tweede DWSR 100465X11 | S235       | 3M26-8-8T | 0,53 | 0,53 | 0,53 | 1,03      | -38,3 SMLS 6a_90 BA CII Ah  | 141,6 | 188,2      | 172,8       | 0,27       |      | 35,1 SMLS 6a_90 BA CII Ah   | 167,8     | 188,2    | 157,1        | 0,22        |
| 418       | Tweede DWSR 100465X11 | S235       | 3M26-8-8T | 0,53 | 0,53 | 0,53 | 1,03      | -38,3 SMLS 6a_90 BA CII Ah  | 141,6 | 188,2      | 172,8       | 0,27       |      | 35,1 SMLS 6a_90 BA CII Ah   | 167,8     | 188,2    | 157,1        | 0,22        |
| 419       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 62,6 ULS 3_106,025          | 401,4     | 188,2    | 322,4        | 0,33        |
| 420       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 421       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 422       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 423       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 424       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 425       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 426       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 427       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 428       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 429       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 430       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 431       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 432       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 433       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 434       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 435       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 436       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 437       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 438       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 439       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 440       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 441       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 442       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 443       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 444       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 445       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 446       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 447       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      | 25,3 SMLS 6a_90 BA All Cts  | 101,1     | 188,2    | 134,4        | 0,25        |
| 448       | Tweede DWSR 100465X11 | S235       | 3M16-8-8T | 1,00 | 2,00 | 1,00 | 1,04      | -0,3 SMLS 11_0,9,13,5 Ah    | 242,4 | 188,2      | 322,4       | 0,00       |      |                             |           |          |              |             |



**Assessment of groups for strengthened mast (verbouw level)**

Date 21-05-21  
Author KCh  
Version 1.0

ZW380 Oost  
HB+0  
68

| Stafgroep | Omschrijving Profiel  | Stafsoort | Bouten  | RLX  | RLY  | RLZ  | Stankheid | Druk Combinatie druk    | Knik | Afschuiving | Stuik (druk) | U.C. (druk) | Opm.                   | Trek Combinatie trek | Nettoelast. | Afschuif | Stuik (trek) | U.C. (trek) |
|-----------|-----------------------|-----------|---------|------|------|------|-----------|-------------------------|------|-------------|--------------|-------------|------------------------|----------------------|-------------|----------|--------------|-------------|
| 534       | Tweede DIVERSIFIKASIE | 5355      | M16-8.8 | 0.54 | 0.54 | 0.54 | 173       | -3642 SFS 6a_30 All Cts | 3177 | 60.3        | 706          | 0.96        | 3372 SFS 6a_30 All Cts | 75.3                 | 60.3        | 534      | 0.62         |             |









21-05-21  
KCh  
1.0

Assessment of groups for initial mast (aft/fore level).

ZW380 Oost  
HB+0  
78

| Group Label | Description                      | Profile    | Steel Quality | Brk        | RLX  | RLY  | RLZ  | Slenderness | Compression | Load Case (Compression)      | Buckling | Shear (Comp) | Bearing | Shear (Comp) | U.C. (Comp) | Exceedance (Comp) | Tension                      | Load Case (Tension) | Net Section | Shear (Tens) | Bearing (Tens) | U.C. (Tens) | Exceedance (Tens) |
|-------------|----------------------------------|------------|---------------|------------|------|------|------|-------------|-------------|------------------------------|----------|--------------|---------|--------------|-------------|-------------------|------------------------------|---------------------|-------------|--------------|----------------|-------------|-------------------|
| 402         | Tweede DWDRM - Diagonal bracing  | 55x55x6    | S235          | 191x68.8R  | 1.00 | 1.00 | 1.00 | 326         | -10.2       | U.S 59 Ah 12                 | 12.9     | 60.3         | 51.8    | 51.8         | 0.79        | 42.6              | U.S 59 Ah 12                 | 51.8                | 51.8        | 51.8         | 0.79           | 42.6        |                   |
| 403         | Tweede DWDRM - Vertical bracing  | 50x50x5    | S235          | 191x68.8R  | 1.00 | 1.00 | 1.00 | 82          | 0.0         | U.S 59 Ah 12                 | 55.5     | 60.3         | 43.2    | 43.2         | 0.00        | 2.8               | U.S 59 Ah 12                 | 55.5                | 60.3        | 60.3         | 0.00           | 2.8         |                   |
| 404         | Tweede DWDRM - Vertical bracing  | 65x65x6    | S235          | 202x68.8R  | 1.00 | 1.00 | 1.00 | 132         | -10.4       | SPLS 69_90 Ba All Cts Ah Ctl | 73.0     | 120.6        | 103.7   | 103.7        | 0.14        | 9.6               | SPLS 3_79.6 Ah All Cts       | 103.7               | 120.6       | 120.6        | 0.14           | 9.6         |                   |
| 405         | Tweede DWDRM - Vertical bracing  | 55x55x6    | S235          | 191x68.8R  | 1.00 | 1.00 | 1.00 | 161         | -13.2       | SPLS 69_90 Ba All Cts Ba Ctl | 29.1     | 60.3         | 51.8    | 51.8         | 0.45        | 6.2               | SPLS 69_90 Ba All Cts Ba Ctl | 51.8                | 60.3        | 60.3         | 0.45           | 6.2         |                   |
| 406         | Tweede DWDRM - Vertical bracing  | 55x55x6    | S235          | 191x68.8R  | 1.00 | 1.00 | 1.00 | 161         | -15.9       | SPLS 69_90 Ah Ctl Ba Ctl     | 285.1    | 406.7        | 311.0   | 311.0        | 0.57        | 167.9             | SPLS 69_90 Ah Ctl Ba Ctl     | 311.0               | 406.7       | 406.7        | 0.57           | 167.9       |                   |
| 407         | Tweede DWDRM - Diagonal diphraem | 120x120x8  | S235          | 392x48.8R  | 1.00 | 1.00 | 1.00 | 87          | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 408         | Tweede DWDRM - Crossing diagonal | 80x80x8    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 193         | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 409         | Tweede DWDRM - Crossing diagonal | 80x80x8    | S235          | 202x68.8R  | 0.50 | 1.00 | 0.50 | 114         | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 410         | Tweede DWDRM - Crossing diagonal | 80x80x8    | S235          | 202x68.8R  | 0.50 | 1.00 | 0.50 | 114         | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 411         | Tweede DWDRM - Crossing diagonal | 80x80x8    | S235          | 202x68.8R  | 0.50 | 1.00 | 0.50 | 111         | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 412         | Tweede DWDRM - Crossing diagonal | 80x80x8    | S235          | 202x68.8R  | 0.50 | 1.00 | 0.50 | 105         | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 413         | Tweede DWDRM - Crossing diagonal | 80x80x8    | S235          | 202x68.8R  | 0.50 | 1.00 | 0.50 | 101         | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 414         | Tweede DWDRM - Crossing diagonal | 80x80x8    | S235          | 202x68.8R  | 0.50 | 1.00 | 0.50 | 101         | -11.9       | U.S 7                        | 16.9     | 60.3         | 43.2    | 43.2         | 0.70        | 6.0               | SPLS 69_90 Ah Cts Ba Ctl     | 43.2                | 60.3        | 60.3         | 0.70           | 6.0         |                   |
| 415         | Tweede DWDRM - Crossing diagonal | 65x65x6    | S235          | 102x55x11  | 1.00 | 1.00 | 1.00 | 93          | -25.1       | SPLS 69_90 Ba All Cts Ba Ctl | 106.7    | 180.9        | 155.5   | 155.5        | 0.25        | 25.2              | SPLS 69_90 Ba All Cts Ba Ctl | 155.5               | 180.9       | 180.9        | 0.25           | 25.2        |                   |
| 430         | Tweede DWDRM - Crossing diagonal | 55x55x6    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 166         | -12.6       | SPLS 69_90 Ah All Cts Ba Ctl | 35.1     | 60.3         | 51.8    | 51.8         | 0.36        | 11.2              | SPLS 69_90 Ah All Cts Ba Ctl | 51.8                | 60.3        | 60.3         | 0.36           | 11.2        |                   |
| 431         | Tweede DWDRM - Crossing diagonal | 55x55x6    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 174         | -12.6       | SPLS 69_90 Ah All Cts Ba Ctl | 35.1     | 60.3         | 51.8    | 51.8         | 0.36        | 11.2              | SPLS 69_90 Ah All Cts Ba Ctl | 51.8                | 60.3        | 60.3         | 0.36           | 11.2        |                   |
| 432         | Tweede DWDRM - Crossing diagonal | 55x55x6    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 174         | -12.6       | SPLS 69_90 Ah All Cts Ba Ctl | 35.1     | 60.3         | 51.8    | 51.8         | 0.36        | 11.2              | SPLS 69_90 Ah All Cts Ba Ctl | 51.8                | 60.3        | 60.3         | 0.36           | 11.2        |                   |
| 433         | Tweede DWDRM - Crossing diagonal | 55x55x6    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 164         | -24.8       | SPLS 69_90 Ba All Cts Ah Ctl | 35.7     | 60.3         | 51.8    | 51.8         | 0.70        | 27.4              | SPLS 69_90 Ba All Cts Ah Ctl | 51.8                | 60.3        | 60.3         | 0.70           | 27.4        |                   |
| 434         | Tweede DWDRM - Crossing diagonal | 55x55x6    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 173         | -24.8       | SPLS 69_90 Ba All Cts Ah Ctl | 35.7     | 60.3         | 51.8    | 51.8         | 0.70        | 27.4              | SPLS 69_90 Ba All Cts Ah Ctl | 51.8                | 60.3        | 60.3         | 0.70           | 27.4        |                   |
| 435         | Tweede DWDRM - Horizontal        | 55x55x6    | S235          | 191x68.8R  | 1.00 | 1.00 | 1.00 | 143         | -10.3       | SPLS 69_90 Ba All Cts Ah Ctl | 33.2     | 60.3         | 51.8    | 51.8         | 1.05        | knik              | SPLS 69_90 Ba All Cts Ah Ctl | 51.8                | 60.3        | 60.3         | 1.05           | knik        |                   |
| 436         | Tweede DWDRM - Horizontal        | 55x55x6    | S235          | 191x68.8R  | 1.00 | 1.00 | 1.00 | 143         | -10.3       | SPLS 69_90 Ba All Cts Ah Ctl | 33.2     | 60.3         | 51.8    | 51.8         | 1.05        | knik              | SPLS 69_90 Ba All Cts Ah Ctl | 51.8                | 60.3        | 60.3         | 1.05           | knik        |                   |
| 437         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 143         | -20.0       | SPLS 69_90 Ba All Cts Ah Ctl | 33.9     | 60.3         | 43.2    | 43.2         | 0.59        | 10.9              | SPLS 69_90 Ba All Cts Ah Ctl | 43.2                | 60.3        | 60.3         | 0.59           | 10.9        |                   |
| 438         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 131         | -16.3       | SPLS 69_90 Ba All Cts Ah Ctl | 37.4     | 60.3         | 43.2    | 43.2         | 0.43        | 16.8              | SPLS 69_90 Ba All Cts Ah Ctl | 43.2                | 60.3        | 60.3         | 0.43           | 16.8        |                   |
| 439         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 107         | -10.8       | SPLS 69_90 Ba All Cts Ah Ctl | 46.0     | 60.3         | 43.2    | 43.2         | 0.35        | 10.7              | SPLS 69_90 Ba All Cts Ah Ctl | 43.2                | 60.3        | 60.3         | 0.35           | 10.7        |                   |
| 440         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 88          | -14.8       | SPLS 69_90 Ba All Cts Ah Ctl | 53.6     | 60.3         | 43.2    | 43.2         | 0.34        | 15.1              | SPLS 69_90 Ba All Cts Ah Ctl | 43.2                | 60.3        | 60.3         | 0.34           | 15.1        |                   |
| 441         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 88          | -14.8       | SPLS 69_90 Ba All Cts Ah Ctl | 53.6     | 60.3         | 43.2    | 43.2         | 0.34        | 15.1              | SPLS 69_90 Ba All Cts Ah Ctl | 43.2                | 60.3        | 60.3         | 0.34           | 15.1        |                   |
| 442         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 77          | -16.8       | SPLS 69_90 Ba All Cts Ah Ctl | 58.7     | 60.3         | 43.2    | 43.2         | 0.39        | 16.0              | SPLS 69_90 Ba All Cts Ah Ctl | 43.2                | 60.3        | 60.3         | 0.39           | 16.0        |                   |
| 443         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 191x68.8R  | 0.50 | 1.00 | 0.50 | 73          | -18.6       | SPLS 69_90 Ba All Cts Ah Ctl | 58.0     | 60.3         | 43.2    | 43.2         | 0.43        | 20.0              | SPLS 69_90 Ba All Cts Ah Ctl | 43.2                | 60.3        | 60.3         | 0.43           | 20.0        |                   |
| 444         | Tweede DWDRM - Crossing diagonal | 50x50x5    | S235          | 202x68.8R  | 1.00 | 1.00 | 1.00 | 47          | 0.0         | SPLS 14_74.4 Ah Ctl          | 443.0    | 188.2        | 162.0   | 162.0        | 0.00        | 30.5              | SPLS 69_90 Ba All Cts Ah Ctl | 162.0               | 188.2       | 188.2        | 0.00           | 30.5        |                   |
| 445         | Tweede DWDRM - Horizontal        | 160x160x11 | S235          | 160x160x11 | 1.00 | 1.00 | 1.00 | 47          | 0.0         | SPLS 14_74.4 Ah Ctl          | 443.0    | 188.2        | 162.0   | 162.0        | 0.00        | 30.5              | SPLS 69_90 Ba All Cts Ah Ctl | 162.0               | 188.2       | 188.2        | 0.00           | 30.5        |                   |





Date 21-05-21  
 Author KCh  
 Version 1.0

Assessment of groups for strengthened mast (afkeur level)

ZW380 Oost  
 HB+0  
 78

| Stafgroep | Omschrijving                 | Profiel | Standaard | Bouten | RLX  | RLY  | RZ   | Slankheid | Drink | Combinatie | Kruik | Afschaving | Stuik | U.C. | Drukt | Opm. | Nettoflsh. | Afkeur | Stuik | U.C. |
|-----------|------------------------------|---------|-----------|--------|------|------|------|-----------|-------|------------|-------|------------|-------|------|-------|------|------------|--------|-------|------|
| 100A      | BV1STK - Top 120x120x8       | S355    | 163       | 163    | 0.52 | 0.52 | 0.52 | 163       | 163   | 163        | 163   | 163        | 163   | 0.52 | 0.52  | 0.52 | 163        | 163    | 163   | 0.52 |
| 100B      | BV1STK - Main 120x120x8      | S355    | 163       | 163    | 0.52 | 0.52 | 0.52 | 163       | 163   | 163        | 163   | 163        | 163   | 0.52 | 0.52  | 0.52 | 163        | 163    | 163   | 0.52 |
| 100C      | Cross profile (m 150x150x14) | S355    | 64        | 64     | 0.50 | 0.50 | 0.50 | 64        | 64    | 64         | 64    | 64         | 64    | 0.50 | 0.50  | 0.50 | 64         | 64     | 64    | 0.50 |
| 100D      | Cross profile (m 150x150x12) | S355    | 64        | 64     | 0.50 | 0.50 | 0.50 | 64        | 64    | 64         | 64    | 64         | 64    | 0.50 | 0.50  | 0.50 | 64         | 64     | 64    | 0.50 |
| 100E      | Cross profile (m 160x160x15) | S355    | 77        | 77     | 0.50 | 0.50 | 0.50 | 77        | 77    | 77         | 77    | 77         | 77    | 0.50 | 0.50  | 0.50 | 77         | 77     | 77    | 0.50 |
| 100F      | Cross profile (m 160x160x17) | S355    | 77        | 77     | 0.50 | 0.50 | 0.50 | 77        | 77    | 77         | 77    | 77         | 77    | 0.50 | 0.50  | 0.50 | 77         | 77     | 77    | 0.50 |
| 100G      | Tweede/SHK - 160x160x17      | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100H      | Tweede/SHK - 160x160x15      | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100I      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100J      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100K      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100L      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100M      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100N      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100O      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100P      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100Q      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100R      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100S      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100T      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100U      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100V      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100W      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100X      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100Y      | Erste/DWDRM - 160x160x15     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 100Z      | Erste/DWDRM - 160x160x17     | S355    | 109       | 109    | 0.48 | 0.48 | 0.48 | 109       | 109   | 109        | 109   | 109        | 109   | 0.48 | 0.48  | 0.48 | 109        | 109    | 109   | 0.48 |
| 101A      | BV1STK - Cross 100x100x8     | S235    | 146       | 146    | 0.53 | 0.53 | 0.53 | 146       | 146   | 146        | 146   | 146        | 146   | 0.53 | 0.53  | 0.53 | 146        | 146    | 146   | 0.53 |
| 101B      | BV1STK - Horiz 160x160       | S235    | 177       | 177    | 0.50 | 0.50 | 0.50 | 177       | 177   | 177        | 177   | 177        | 177   | 0.50 | 0.50  | 0.50 | 177        | 177    | 177   | 0.50 |
| 101C      | BV1STK - Horiz 200x200       | S235    | 203       | 203    | 0.50 | 0.50 | 0.50 | 203       | 203   | 203        | 203   | 203        | 203   | 0.50 | 0.50  | 0.50 | 203        | 203    | 203   | 0.50 |
| 101D      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101E      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101F      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101G      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101H      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101I      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101J      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101K      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101L      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101M      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101N      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101O      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101P      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101Q      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101R      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101S      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101T      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101U      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101V      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101W      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101X      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101Y      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 101Z      | BV1STK - Cross 150x150x12    | S235    | 106       | 106    | 0.54 | 0.54 | 0.54 | 106       | 106   | 106        | 106   | 106        | 106   | 0.54 | 0.54  | 0.54 | 106        | 106    | 106   | 0.54 |
| 102A      | Derste/SHK - H 120x120x12    | S235    | 123       | 123    | 0.53 | 0.53 | 0.53 | 123       | 123   | 123        | 123   | 123        | 123   | 0.53 | 0.53  | 0.53 | 123        | 123    | 123   | 0.53 |
| 102B      | Derste/SHK - H 120x120x12    | S235    | 123       | 123    | 0.53 | 0.53 | 0.53 | 123       | 123   | 123        | 123   | 123        | 123   | 0.53 | 0.53  | 0.53 | 123        | 123    | 123   | 0.53 |
| 102C      | Derste/SHK - H 120x120x12    | S235    | 123       | 123    | 0.53 | 0.53 | 0.53 | 123       | 123   | 123        | 123   | 123        | 123   | 0.53 | 0.53  | 0.53 | 123        | 123    | 123   | 0.53 |



Date 21-05-21  
 Author KCh  
 Version 1.0

Assessment of groups for strengthened mast (afkeur level)

ZW380 Oost  
 HB+0  
 78

| Stalgroep | Omschrijving Profiel           | Staalsoort | Bouten   | RLX  | RLY  | RZ Slimheid | Drak Combinatie/ruik        | Kruik | Afschaving | Stuik (ruik) | U.C. (ruik) | Opm.                       | Trek Combinatie trek | Nettoopp. | Afschuif | Stuik (trek) | U.C. (trek) |
|-----------|--------------------------------|------------|----------|------|------|-------------|-----------------------------|-------|------------|--------------|-------------|----------------------------|----------------------|-----------|----------|--------------|-------------|
| 322       | Erste DWSR 1004120x8           | S235       | 2M2x8-8T | 1,00 | 1,00 | 2,00        | 14,0 ULS 3,74,4             | 396,5 | 270,1      | 311,5        | 0,07        | 3,0 SLS 68,90 AN C12 Ba    | 225,1                | 270,9     | 215,7    | 0,06         |             |
| 323       | Tweede DWSR 1004120x8          | S235       | 2M2x8-8T | 1,00 | 1,00 | 2,00        | 14,0 ULS 3,74,4             | 396,5 | 270,1      | 311,5        | 0,07        | 3,0 SLS 68,90 AN C12 Ba    | 225,1                | 270,9     | 215,7    | 0,06         |             |
| 400       | Tweede DWSR 1204120x8          | S235       | 4M2x8-8T | 1,00 | 1,00 | 3,02        | 0,0                         | 113,0 | 54,2       | 414,7        | 0,00        | 161,6 SLS 68,90 AN All Cts | 343,3                | 542,2     | 354,5    | 0,47         |             |
| 401       | Tweede DWSR 1204120x8          | S235       | 4M2x8-8T | 1,00 | 1,00 | 3,02        | 0,0                         | 113,0 | 54,2       | 414,7        | 0,00        | 161,6 SLS 68,90 AN All Cts | 343,3                | 542,2     | 354,5    | 0,47         |             |
| 402       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 1,00 | 1,00 | 1,00        | -10,2 ULS 5a Ah 12          | 12,9  | 60,3       | 51,8         | 0,79        | 0,0 ULS 5a Ah 12           | 55,3                 | 60,3      | 39,2     | 0,00         |             |
| 403       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 1,00 | 1,00 | 1,00        | -10,2 ULS 5a Ah 12          | 12,9  | 60,3       | 51,8         | 0,79        | 0,0 ULS 5a Ah 12           | 55,3                 | 60,3      | 39,2     | 0,00         |             |
| 404       | Tweede DWSR 55x55x6            | S235       | 2M1x8-8T | 1,00 | 1,00 | 1,00        | 13,2                        | 73,0  | 120,6      | 103,7        | 0,14        | 9,6 ULS 5a Ah 12           | 80,5                 | 120,6     | 85,5     | 0,12         |             |
| 405       | Tweede DWSR 50x50x5            | S235       | 2M1x8-8T | 1,00 | 1,00 | 1,00        | -10,4 SLS 6a, 90 Ba All Cts | 9,2   | 60,3       | 43,2         | 0,00        | 9,6 ULS 3,74,4 All Cts     | 37,4                 | 60,3      | 25,7     | 0,22         |             |
| 406       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 0,50 | 1,00 | 0,50        | -13,2 SLS 6a, 90 Ah All Cts | 29,1  | 60,3       | 51,8         | 0,45        | 6,2 SLS 6a, 90 Ah All Cts  | 55,3                 | 60,3      | 39,2     | 0,16         |             |
| 407       | Tweede DWSR 1204120x8          | S235       | 3M2x8-8T | 1,00 | 1,00 | 1,00        | -13,2 SLS 6a, 90 Ah All Cts | 29,1  | 406,7      | 311,0        | 0,57        | 167,9 SLS 68,90 AN C12 Ba  | 263,0                | 406,7     | 268,9    | 0,64         |             |
| 408       | Tweede DWSR 1204120x8          | S235       | 3M2x8-8T | 1,00 | 1,00 | 1,00        | -13,2 SLS 6a, 90 Ah All Cts | 29,1  | 406,7      | 311,0        | 0,57        | 167,9 SLS 68,90 AN C12 Ba  | 263,0                | 406,7     | 268,9    | 0,64         |             |
| 409       | Tweede DWSR 50x80x8            | S235       | 2M2x8-8T | 0,52 | 0,52 | 0,52        | -31,5 SLS 6a, 90 Ah C11 Ba  | 132,3 | 188,2      | 172,8        | 0,24        | 12,4 SLS 68,90 AN All Cts  | 138,0                | 188,2     | 152,8    | 0,13         |             |
| 410       | Tweede DWSR 50x80x8            | S235       | 2M2x8-8T | 0,52 | 0,52 | 0,52        | -31,5 SLS 6a, 90 Ah C11 Ba  | 132,3 | 188,2      | 172,8        | 0,24        | 12,4 SLS 68,90 AN All Cts  | 138,0                | 188,2     | 152,8    | 0,13         |             |
| 411       | Tweede DWSR 50x80x8            | S235       | 2M2x8-8T | 0,53 | 0,53 | 0,53        | -37,9 SLS 6a, 90 Ah C11 Ba  | 141,6 | 188,2      | 172,8        | 0,27        | 34,7 SLS 68,90 AN C11 Ba   | 167,8                | 188,2     | 157,1    | 0,16         |             |
| 412       | Tweede DWSR 50x80x8            | S235       | 2M2x8-8T | 0,53 | 0,53 | 0,53        | -37,9 SLS 6a, 90 Ah C11 Ba  | 141,6 | 188,2      | 172,8        | 0,27        | 34,7 SLS 68,90 AN C11 Ba   | 167,8                | 188,2     | 157,1    | 0,16         |             |
| 413       | Tweede DWSR 50x80x8            | S235       | 3M2x8-8T | 0,53 | 0,53 | 0,53        | -41,6 SLS 6a, 90 Ah C12 Ba  | 154,7 | 283,2      | 259,2        | 0,40        | 25,6 SLS 68,90 AN C12 Ba   | 174,4                | 283,2     | 177,1    | 0,16         |             |
| 414       | Tweede DWSR 100465x11          | S235       | 2M2x8-8T | 1,00 | 2,00 | 1,00        | -0,3 SLS 14, 0,5 Ba All Cts | 242,4 | 188,2      | 323,4        | 0,00        | 63,2 ULS 3,74,4 All Cts    | 401,4                | 188,2     | 323,4    | 0,34         |             |
| 415       | Tweede DWSR 155x55x6           | S235       | 3M1x8-8T | 1,00 | 1,00 | 1,00        | -25,1 SLS 6a, 90 Ah All Cts | 100,7 | 186,9      | 155,5        | 0,25        | 25,2 SLS 68,90 AN All Cts  | 101,1                | 186,9     | 134,4    | 0,25         |             |
| 430       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 0,55 | 0,55 | 0,55        | -12,6 SLS 6a, 90 Ah All Cts | 35,1  | 60,3       | 51,8         | 0,38        | 11,2 SLS 68,90 Ba All Cts  | 55,3                 | 60,3      | 39,2     | 0,29         |             |
| 431       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 0,55 | 0,55 | 0,55        | -12,6 SLS 6a, 90 Ah All Cts | 35,1  | 60,3       | 51,8         | 0,38        | 11,2 SLS 68,90 Ba All Cts  | 55,3                 | 60,3      | 39,2     | 0,29         |             |
| 432       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -24,9 SLS 6a, 90 Ba All Cts | 32,2  | 60,3       | 51,8         | 0,77        | 21,0 SLS 68,90 Ba All Cts  | 55,3                 | 60,3      | 39,2     | 0,54         |             |
| 433       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -24,9 SLS 6a, 90 Ba All Cts | 32,2  | 60,3       | 51,8         | 0,77        | 21,0 SLS 68,90 Ba All Cts  | 55,3                 | 60,3      | 39,2     | 0,54         |             |
| 434       | Tweede DWSR 55x55x6            | S355       | 1M1x8-8T | 0,54 | 0,54 | 0,54        | -35,0 SLS 6a, 90 Ba All Cts | 37,7  | 60,3       | 70,6         | 0,93        | 37,0 SLS 68,90 Ba All Cts  | 55,3                 | 60,3      | 39,2     | 0,70         |             |
| 435       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 1,00 | 1,00 | 1,00        | -24,4 ULS 2,74,5 Ba All Cts | 31,7  | 60,3       | 51,8         | 0,09        | 10,0 SLS 68,90 Ba All Cts  | 51,2                 | 60,3      | 45,9     | 0,00         |             |
| 436       | Tweede DWSR 55x55x6            | S235       | 1M1x8-8T | 1,00 | 1,00 | 1,00        | -24,4 ULS 2,74,5 Ba All Cts | 31,7  | 60,3       | 51,8         | 0,09        | 10,0 SLS 68,90 Ba All Cts  | 51,2                 | 60,3      | 45,9     | 0,00         |             |
| 437       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -30,0 SLS 6a, 90 Ba All Cts | 33,9  | 60,3       | 43,2         | 0,59        | 19,9 SLS 68,90 Ba All Cts  | 37,4                 | 60,3      | 25,7     | 0,77         |             |
| 438       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -16,3 SLS 6a, 90 Ba All Cts | 37,4  | 60,3       | 43,2         | 0,43        | 16,8 SLS 68,90 Ba All Cts  | 37,4                 | 60,3      | 25,7     | 0,65         |             |
| 439       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -10,8 SLS 6a, 90 Ba C11 Ah  | 46,0  | 60,3       | 43,2         | 0,25        | 10,7 SLS 68,90 Ba C11 Ah   | 37,4                 | 60,3      | 25,7     | 0,42         |             |
| 440       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -14,8 SLS 6a, 90 Ba All Cts | 53,6  | 60,3       | 43,2         | 0,34        | 15,1 SLS 68,90 Ba All Cts  | 37,4                 | 60,3      | 25,7     | 0,58         |             |
| 441       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -14,8 SLS 6a, 90 Ba All Cts | 53,6  | 60,3       | 43,2         | 0,34        | 15,1 SLS 68,90 Ba All Cts  | 37,4                 | 60,3      | 25,7     | 0,58         |             |
| 442       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -16,9 SLS 6a, 90 Ba All Cts | 56,7  | 60,3       | 43,2         | 0,39        | 16,0 SLS 68,90 Ba All Cts  | 37,4                 | 60,3      | 25,7     | 0,62         |             |
| 443       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 0,53 | 0,53 | 0,53        | -18,6 SLS 6a, 90 Ba All Cts | 56,7  | 60,3       | 43,2         | 0,43        | 20,0 SLS 68,90 Ba All Cts  | 37,4                 | 60,3      | 25,7     | 0,78         |             |
| 444       | Tweede DWSR 50x50x5            | S235       | 1M1x8-8T | 1,00 | 1,00 | 1,00        | -2,5 SLS 18,74,4 Ah All C1  | 35,0  | 60,3       | 43,2         | 0,06        | 0,0                        | 37,4                 | 60,3      | 25,7     | 0,00         |             |
| 445       | Tweede DWSR 160x65x7,5 (W)S235 |            | 2M2x8-8T | 1,00 | 1,00 | 1,00        | 0,0                         | 443,8 | 186,2      | 186,2        | 0,00        | 39,9 ULS 3,0, 74,4         | 547,9                | 186,2     | 136,9    | 0,30         |             |

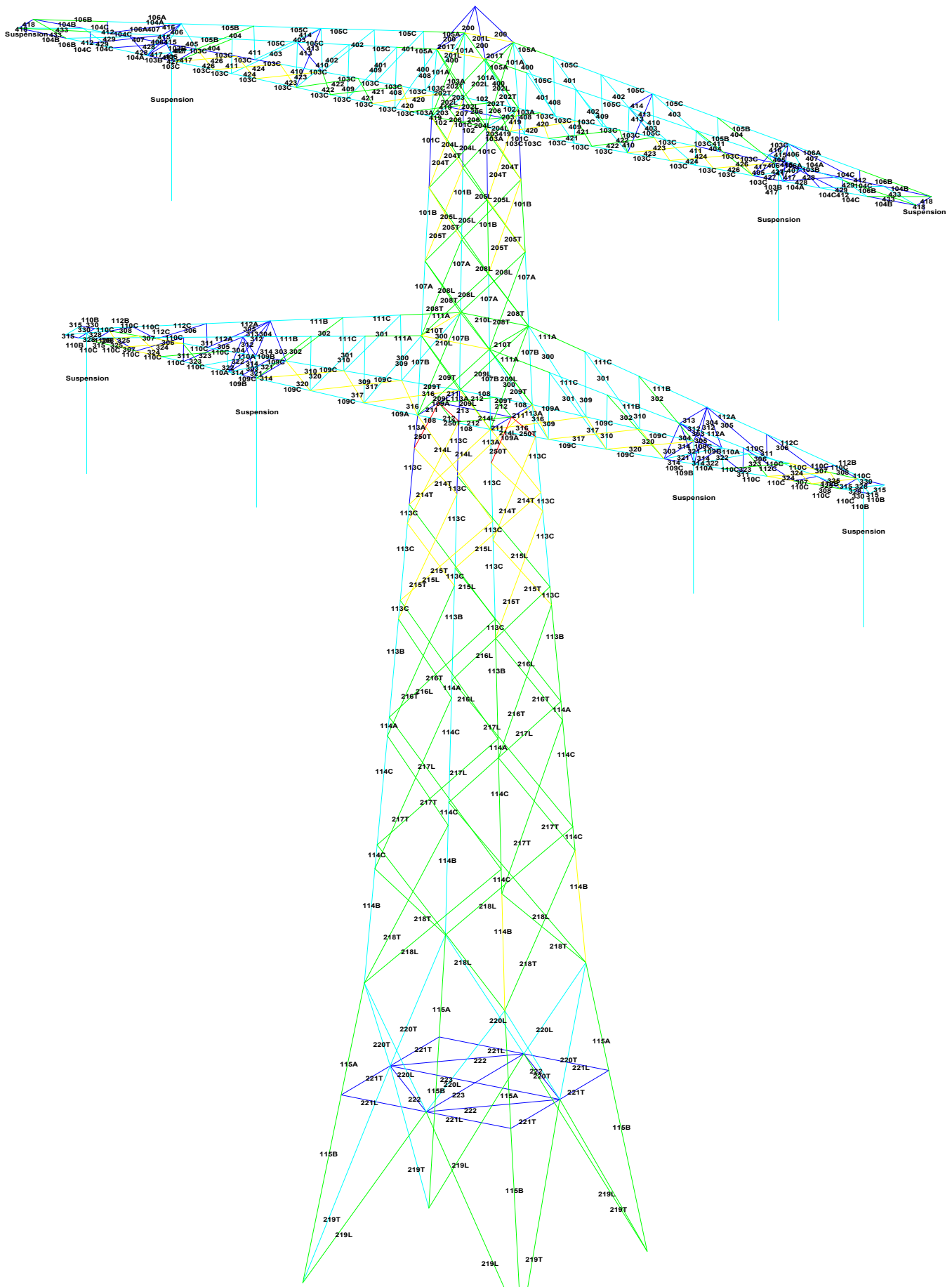


**Assessment of groups for strengthened mast (verbouw level)**

Date 21-05-21  
Author KCh  
Version 1.0

ZW380 Oost  
HB+0  
78

| Stafgroep | Omschrijving  | Profiel | Stafhoogte | Bouten | RLX  | RLX  | RLX  | RLZ  | Stankheid | Druk  | Combinatie druk      | Knik | Afschuiving | Stuik (druk) | U.C. (druk) | Opm. | Trak | Combinatie trak      | Nettoelast. | Afschuif | Stuik (trak) | U.C. (trak) |
|-----------|---------------|---------|------------|--------|------|------|------|------|-----------|-------|----------------------|------|-------------|--------------|-------------|------|------|----------------------|-------------|----------|--------------|-------------|
| 334       | Tweede DIVERS | EXX55x6 | 3395       | M16x81 | 0,54 | 0,54 | 0,54 | 0,54 | 173       | -3647 | SFS 6a_30 Ba All Cts | 3177 | 60,3        | 706          | 0,97        |      | 334  | SFS 6a_30 Ba All Cts | 75,3        | 60,3     | 334          | 0,62        |



1 (m)





Date  
Author  
Version

Assessment of groups for initial mast (aft/fore level).

ZW380 Oost  
HS+0  
26

| Group Label | Description                        | Steel Quality | Profile    | RLX  | RLY  | RLZ  | Slenderness | Compression | Lead Case (Compression) | Buckling | Shear (Comp) | Bearing (Comp) | U.C. (Comp) | Exceedance (Comp) | Tension | Load Case (Tension) | Net Section | Shear (Tens) | Bearing (Tens) | U.C. (Tens) | Exceedance (Tens) |
|-------------|------------------------------------|---------------|------------|------|------|------|-------------|-------------|-------------------------|----------|--------------|----------------|-------------|-------------------|---------|---------------------|-------------|--------------|----------------|-------------|-------------------|
| 304         | Erste DWSRM - Front diag 4         | S235          | 50x50x5    | 1.00 | 1.00 | 1.00 | 163         | -16.2       | ULS 5a Bt 12            | 36.7     | 120.6        | 66.4           | 0.00        | 0.00              | 10.3    | ULS 5a At 22        | 56.2        | 120.6        | 66.4           | 0.18        | 0.18              |
| 305         | Erste DWSRM - Front diag 5         | S235          | 50x50x5    | 1.00 | 1.00 | 1.00 | 163         | 0.0         | ULS 5a Bt 10            | 11.8     | 60.3         | 37.4           | 0.00        | 0.00              | 6.5     | ULS 5a Bt 10        | 37.4        | 60.3         | 37.4           | 0.00        | 0.15              |
| 306         | Erste DWSRM - Front diag 6         | S235          | 50x50x5    | 1.00 | 1.00 | 1.00 | 229         | 0.0         | ULS 5a Bt 11            | 18.0     | 60.3         | 43.2           | 0.00        | 0.00              | 6.5     | ULS 5a Bt 11        | 37.4        | 60.3         | 37.4           | 0.00        | 0.16              |
| 307         | Erste DWSRM - Front diag 7         | S235          | 50x50x5    | 1.00 | 1.00 | 1.00 | 229         | 0.0         | ULS 5a Bt 11            | 18.0     | 60.3         | 43.2           | 0.00        | 0.00              | 6.5     | ULS 5a Bt 11        | 37.4        | 60.3         | 37.4           | 0.00        | 0.16              |
| 308         | Erste DWSRM - Front diag 8         | S235          | 50x50x5    | 1.00 | 1.00 | 1.00 | 229         | 0.0         | ULS 5a Bt 11            | 18.0     | 60.3         | 43.2           | 0.00        | 0.00              | 6.5     | ULS 5a Bt 11        | 37.4        | 60.3         | 37.4           | 0.00        | 0.16              |
| 309         | Erste DWSRM - Front diag 9         | S235          | 50x50x5    | 1.00 | 1.00 | 1.00 | 229         | 0.0         | ULS 5a Bt 11            | 18.0     | 60.3         | 43.2           | 0.00        | 0.00              | 6.5     | ULS 5a Bt 11        | 37.4        | 60.3         | 37.4           | 0.00        | 0.16              |
| 310         | Erste DWSRM - Front vert 1         | S235          | 65x65x6    | 1.00 | 1.00 | 1.00 | 166         | -15.5       | ULS 3_135               | 41.7     | 60.3         | 51.8           | 0.32        | 0.32              | 0.0     | ULS 3_135           | 89.9        | 60.3         | 0.00           | 0.00        | 0.00              |
| 311         | Erste DWSRM - Front vert 2         | S235          | 65x65x6    | 1.00 | 1.00 | 1.00 | 166         | 0.0         | ULS 3_135               | 44.3     | 60.3         | 51.8           | 0.35        | 0.35              | 0.0     | ULS 3_135           | 81.2        | 60.3         | 0.00           | 0.00        | 0.00              |
| 312         | Erste DWSRM - Doorrede AA          | S235          | 100x100x8  | 1.00 | 1.00 | 1.00 | 129         | 0.0         | ULS 5a Bt 10            | 38.2     | 60.3         | 43.2           | 0.00        | 0.00              | 5.4     | ULS 5a Bt 10        | 37.4        | 60.3         | 0.00           | 0.00        | 0.00              |
| 313         | Erste DWSRM - Doorrede AA horiz    | S235          | 100x100x8  | 1.00 | 1.00 | 1.00 | 129         | -24.1       | ULS 1_90                | 24.6     | 60.3         | 58.8           | 0.08        | 0.08              | 0.0     | ULS 1_90            | 51.0        | 60.3         | 0.00           | 0.00        | 0.00              |
| 109A        | Erste DWSRM - Main member 1 bottom | S355          | 150x150x12 | 1.00 | 1.00 | 1.00 | 78          | -308.7      | ULS 5a Bt 10            | 798.9    | 866.0        | 1481.8         | 0.39        | 0.39              | 123.4   | ULS 5a At 21        | 869.3       | 848.0        | 1481.8         | 0.15        | 0.15              |
| 109B        | Erste DWSRM - Main member 1 top    | S355          | 150x150x12 | 1.00 | 1.00 | 1.00 | 78          | 0.0         | ULS 5a Bt 10            | 798.9    | 866.0        | 1481.8         | 0.39        | 0.39              | 123.4   | ULS 5a At 21        | 869.3       | 848.0        | 1481.8         | 0.15        | 0.15              |
| 109C        | Erste DWSRM - Main member 2 bottom | S355          | 150x150x12 | 1.00 | 1.00 | 1.00 | 78          | -81.3       | ULS 5a Bt 10            | 798.9    | 866.0        | 1481.8         | 0.35        | 0.35              | 112.2   | ULS 5a At 21        | 1235.4      | 81.3         | 0.00           | 0.00        | 0.00              |
| 109D        | Erste DWSRM - Main member 2 top    | S355          | 150x150x12 | 1.00 | 1.00 | 1.00 | 78          | 0.0         | ULS 5a Bt 10            | 798.9    | 866.0        | 1481.8         | 0.35        | 0.35              | 112.2   | ULS 5a At 21        | 1235.4      | 81.3         | 0.00           | 0.00        | 0.00              |
| 110A        | Erste DWSRM - Main member 1 top    | S355          | 100x100x8  | 1.00 | 1.00 | 1.00 | 64          | -188.3      | ULS 5a Bt 10            | 514.0    | 813.3        | 1058.4         | 0.37        | 0.37              | 105.8   | ULS 5a At 21        | 493.9       | 813.3        | 0.00           | 0.00        | 0.17              |
| 110B        | Erste DWSRM - Main member 2 bottom | S355          | 100x100x8  | 1.00 | 1.00 | 1.00 | 64          | 0.0         | ULS 5a Bt 10            | 514.0    | 813.3        | 1058.4         | 0.37        | 0.37              | 105.8   | ULS 5a At 21        | 493.9       | 813.3        | 0.00           | 0.00        | 0.17              |
| 110C        | Erste DWSRM - Main member 1 bottom | S355          | 100x100x8  | 1.00 | 1.00 | 1.00 | 39          | -5.6        | ULS 5a Bt 21            | 61.7     | 0.0          | 0.0            | 0.01        | 0.01              | 6.2     | ULS 5a Bt 10        | 681.6       | 0.0          | 0.00           | 0.00        | 0.01              |
| 110D        | Erste DWSRM - Main member 2 bottom | S355          | 100x100x8  | 1.00 | 1.00 | 1.00 | 37          | 0.0         | ULS 5a Bt 21            | 58.7     | 54.2         | 44.7           | 0.00        | 0.00              | 14.5    | ULS 5a Bt 21        | 681.6       | 54.2         | 0.00           | 0.00        | 0.09              |
| 110E        | Erste DWSRM - Main member 1 top    | S355          | 100x100x8  | 1.00 | 1.00 | 1.00 | 254         | 0.0         | ULS 5a Bt 21            | 58.7     | 54.2         | 44.7           | 0.00        | 0.00              | 14.5    | ULS 5a Bt 21        | 681.6       | 54.2         | 0.00           | 0.00        | 0.09              |
| 110F        | Erste DWSRM - Main member 2 top    | S355          | 100x100x8  | 1.00 | 1.00 | 1.00 | 254         | 0.0         | ULS 5a Bt 21            | 58.7     | 54.2         | 44.7           | 0.00        | 0.00              | 14.5    | ULS 5a Bt 21        | 681.6       | 54.2         | 0.00           | 0.00        | 0.09              |
| 111A        | Erste DWSRM - Main member 1 top    | S355          | 80x80x8    | 1.00 | 1.00 | 1.00 | 236         | 0.0         | ULS 5a Bt 21            | 66.5     | 0.0          | 0.0            | 0.00        | 0.00              | 126.5   | ULS 5a Bt 21        | 364.3       | 0.0          | 0.00           | 0.35        | 0.35              |
| 111B        | Erste DWSRM - Main member 2 top    | S355          | 80x80x8    | 1.00 | 1.00 | 1.00 | 236         | 0.0         | ULS 5a Bt 21            | 66.5     | 0.0          | 0.0            | 0.00        | 0.00              | 126.5   | ULS 5a Bt 21        | 364.3       | 0.0          | 0.00           | 0.35        | 0.35              |
| 112A        | Erste DWSRM - Main member 1 bottom | S355          | 80x80x8    | 1.00 | 1.00 | 1.00 | 236         | 0.0         | ULS 5a Bt 21            | 66.5     | 0.0          | 0.0            | 0.00        | 0.00              | 126.5   | ULS 5a Bt 21        | 364.3       | 0.0          | 0.00           | 0.35        | 0.35              |
| 112B        | Erste DWSRM - Main member 2 bottom | S355          | 80x80x8    | 1.00 | 1.00 | 1.00 | 236         | 0.0         | ULS 5a Bt 21            | 66.5     | 0.0          | 0.0            | 0.00        | 0.00              | 126.5   | ULS 5a Bt 21        | 364.3       | 0.0          | 0.00           | 0.35        | 0.35              |
| 112C        | Erste DWSRM - Main member 1 top    | S355          | 80x80x8    | 1.00 | 1.00 | 1.00 | 295         | 0.0         | ULS 3_0                 | 37.7     | 46.2         | 37.7           | 0.00        | 0.00              | 91.8    | ULS 3_0             | 289.1       | 46.2         | 0.00           | 0.32        | 0.32              |
| 112D        | Erste DWSRM - Main member 2 top    | S355          | 80x80x8    | 1.00 | 1.00 | 1.00 | 295         | 0.0         | ULS 3_0                 | 37.7     | 46.2         | 37.7           | 0.00        | 0.00              | 91.8    | ULS 3_0             | 289.1       | 46.2         | 0.00           | 0.32        | 0.32              |
| 113A        | Twede TS/NSTK - Main member        | S355          | 150x150x12 | 1.00 | 1.42 | 1.00 | 43          | -328.2      | ULS 13_135              | 1086.7   | 1084.4       | 1693.4         | 0.30        | 0.30              | 212.1   | ULS 13_0_9_135      | 1007.6      | 1084.4       | 0.00           | 0.21        | 0.21              |
| 113B        | Twede TS/NSTK - Main member        | S355          | 150x150x12 | 1.00 | 1.42 | 1.00 | 43          | 0.0         | ULS 13_135              | 1086.7   | 1084.4       | 1693.4         | 0.30        | 0.30              | 212.1   | ULS 13_0_9_135      | 1007.6      | 1084.4       | 0.00           | 0.21        | 0.21              |
| 113C        | Twede TS/NSTK - Main member        | S355          | 150x150x12 | 1.00 | 1.42 | 1.00 | 43          | 0.0         | ULS 13_135              | 1086.7   | 1084.4       | 1693.4         | 0.30        | 0.30              | 212.1   | ULS 13_0_9_135      | 1007.6      | 1084.4       | 0.00           | 0.21        | 0.21              |
| 113D        | Twede TS/NSTK - Main member        | S355          | 150x150x12 | 1.00 | 1.42 | 1.00 | 43          | 0.0         | ULS 13_135              | 1086.7   | 1084.4       | 1693.4         | 0.30        | 0.30              | 212.1   | ULS 13_0_9_135      | 1007.6      | 1084.4       | 0.00           | 0.21        | 0.21              |
| 114C        | Twede TS/NSTK - CD 1 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 78          | -100.2      | ULS 5a Bt 21            | 170.3    | 282.2        | 324.0          | 0.59        | 0.59              | 94.1    | ULS 5a Bt 21        | 111.2       | 282.2        | 275.6          | 0.85        | 0.85              |
| 114D        | Twede TS/NSTK - CD 1 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 78          | 0.0         | ULS 5a Bt 21            | 170.3    | 282.2        | 324.0          | 0.59        | 0.59              | 94.1    | ULS 5a Bt 21        | 111.2       | 282.2        | 275.6          | 0.85        | 0.85              |
| 114E        | Twede TS/NSTK - CD 1 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 78          | 0.0         | ULS 5a Bt 21            | 170.3    | 282.2        | 324.0          | 0.59        | 0.59              | 94.1    | ULS 5a Bt 21        | 111.2       | 282.2        | 275.6          | 0.85        | 0.85              |
| 114F        | Twede TS/NSTK - CD 1 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 78          | 0.0         | ULS 5a Bt 21            | 170.3    | 282.2        | 324.0          | 0.59        | 0.59              | 94.1    | ULS 5a Bt 21        | 111.2       | 282.2        | 275.6          | 0.85        | 0.85              |
| 115L        | Twede TS/NSTK - CD 2 front         | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 86          | -92.7       | ULS 5a Bt 21            | 166.1    | 282.2        | 226.8          | 0.56        | 0.56              | 95.6    | ULS 5a Bt 21        | 111.4       | 282.2        | 187.9          | 0.86        | 0.86              |
| 115M        | Twede TS/NSTK - CD 2 front         | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 86          | 0.0         | ULS 5a Bt 21            | 166.1    | 282.2        | 226.8          | 0.56        | 0.56              | 95.6    | ULS 5a Bt 21        | 111.4       | 282.2        | 187.9          | 0.86        | 0.86              |
| 116L        | Twede TS/NSTK - CD 3 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 102         | -74.1       | ULS 5a Bt 21            | 140.1    | 282.2        | 324.0          | 0.55        | 0.55              | 79.0    | ULS 5a Bt 21        | 111.2       | 282.2        | 275.6          | 0.66        | 0.66              |
| 116M        | Twede TS/NSTK - CD 3 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 102         | 0.0         | ULS 5a Bt 21            | 140.1    | 282.2        | 324.0          | 0.55        | 0.55              | 79.0    | ULS 5a Bt 21        | 111.2       | 282.2        | 275.6          | 0.66        | 0.66              |
| 116N        | Twede TS/NSTK - CD 3 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 102         | 0.0         | ULS 5a Bt 21            | 140.1    | 282.2        | 324.0          | 0.55        | 0.55              | 79.0    | ULS 5a Bt 21        | 111.2       | 282.2        | 275.6          | 0.66        | 0.66              |
| 114A        | Erste TS/NSTK - Main member        | S355          | 150x150x14 | 1.00 | 3.83 | 4.07 | 100         | -592.7      | ULS 13_135              | 1087.4   | 1616.2       | 2993.5         | 0.55        | 0.55              | 449.8   | ULS 13_0_9_135      | 1159.3      | 1616.2       | 0.00           | 0.39        | 0.39              |
| 114B        | Erste TS/NSTK - Main member        | S355          | 150x150x14 | 1.00 | 3.83 | 4.07 | 100         | 0.0         | ULS 13_135              | 1087.4   | 1616.2       | 2993.5         | 0.55        | 0.55              | 449.8   | ULS 13_0_9_135      | 1159.3      | 1616.2       | 0.00           | 0.39        | 0.39              |
| 114C        | Erste TS/NSTK - Main member        | S355          | 150x150x14 | 1.00 | 3.83 | 4.07 | 100         | -666.6      | ULS 13_135              | 895.0    | 1846.3       | 3574.0         | 0.74        | 0.74              | 523.5   | ULS 13_0_9_135      | 1425.0      | 1846.3       | 0.00           | 0.37        | 0.37              |
| 114D        | Erste TS/NSTK - Main member        | S355          | 150x150x14 | 1.00 | 3.83 | 4.07 | 100         | 0.0         | ULS 13_135              | 895.0    | 1846.3       | 3574.0         | 0.74        | 0.74              | 523.5   | ULS 13_0_9_135      | 1425.0      | 1846.3       | 0.00           | 0.37        | 0.37              |
| 117L        | Erste TS/NSTK - CD 1 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 114         | -72.8       | ULS 5a Bt 21            | 126.8    | 188.2        | 216.0          | 0.49        | 0.49              | 65.5    | ULS 5a Bt 21        | 96.5        | 188.2        | 190.1          | 0.71        | 0.71              |
| 117M        | Erste TS/NSTK - CD 1 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 117         | 0.0         | ULS 5a Bt 21            | 123.0    | 188.2        | 216.0          | 0.59        | 0.59              | 66.3    | ULS 5a Bt 21        | 96.5        | 188.2        | 190.1          | 0.71        | 0.71              |
| 117N        | Erste TS/NSTK - CD 1 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.25 | 117         | 0.0         | ULS 5a Bt 21            | 123.0    | 188.2        | 216.0          | 0.59        | 0.59              | 66.3    | ULS 5a Bt 21        | 96.5        | 188.2        | 190.1          | 0.71        | 0.71              |
| 218T        | Erste TS/NSTK - CD 2 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.26 | 119         | -54.1       | ULS 5a Bt 21            | 123.5    | 188.2        | 216.0          | 0.44        | 0.44              | 56.8    | ULS 5a Bt 21        | 94.3        | 188.2        | 187.4          | 0.60        | 0.60              |
| 218U        | Erste TS/NSTK - CD 2 side          | S235          | 100x57x7   | 1.00 | 0.53 | 0.26 | 119         | 0.0         | ULS 5a Bt 21            | 123.5    | 188.2        | 216.0          | 0.44        | 0.44              | 56.8    |                     |             |              |                |             |                   |







Assessment of groups for strengthened mast (afkeur level)

Date 26-05-21
Author KCh
Version 1.0

ZW380 Oost
HS+0
26

Table with columns: Strafgroep, Omschrijving Profiel, Staalksoort, Bouten, RLK, RLY, RLZ, Slimkheid, Druk Combinatie trek, Krakk, Afschaving, Stuk (graat), U.C. (graat), Opm., Trek Combinatie trek, Nettofsh., Afschaf., Stuk (trek), U.C. (trek). Rows include various steel grades and profiles like S235, S355, and T250.



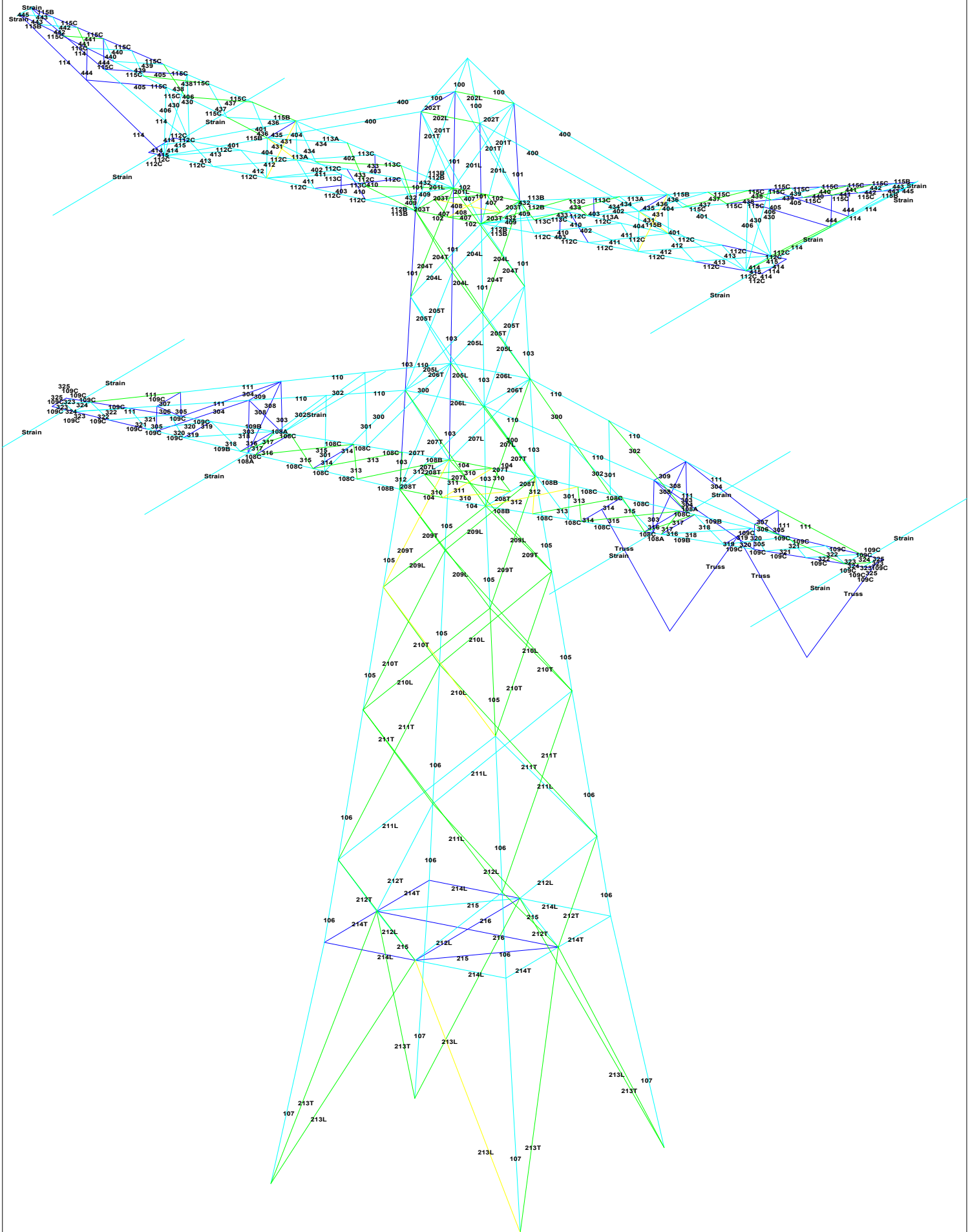


**Assessment of groups for strengthened mast (verbouw level)**

Date 26-05-21  
Author KCh  
Version 1.0

ZW380 Oost  
HS+0  
26

| Staafgroep | Omschrijving Profiel  | Staatsoort | Bouten  | RLX  | RLY  | RLZ  | Stankheid | Druk            | Combinatie druk | Knik  | Afschuiving | Stuik (druk) | U.C. (druk) | Opm. | Trek | Combinatie trek | Nettoinst. | Afschuif | Stuik (trek) | U.C. (trek) |
|------------|-----------------------|------------|---------|------|------|------|-----------|-----------------|-----------------|-------|-------------|--------------|-------------|------|------|-----------------|------------|----------|--------------|-------------|
| E501       | Tweede TSNSTR 707/0x7 | 5355       | 3x20x81 | 1,00 | 0,50 | 0,50 | 94        | <del>99,9</del> | UIS Sa Ba Z1    | 148,3 | 282,2       | 388,7        | 0,67        |      | 97,0 | UIS Sa Ba Z1    | 165,3      | 282,2    | 280,8        | 0,55        |





Assessment of groups for initial mast (afkeur level)

Date 05-05-21  
 Author KCH  
 Version 1.0

ZW380 Oost  
 HC+0  
 16

| Group Label | Description                         | Profile     | Steel Quality | Balls     | RLX  | RLY  | RLZ  | Slenderness | Compression Load Case (Compression) | Buckling | Shear (Comp) | Bearing (Comp) | U.C. (Comp) | Exceedance (Comp) | Tension                         | Load Case (Tension) | Net Section | Shear (Tens) | Bearing (Tens) | U.C. (Tens) | Exceedance (Tens) |
|-------------|-------------------------------------|-------------|---------------|-----------|------|------|------|-------------|-------------------------------------|----------|--------------|----------------|-------------|-------------------|---------------------------------|---------------------|-------------|--------------|----------------|-------------|-------------------|
| 407         | Tweside DWSRH - Diagonal (diagonal) | 200x200x8   | S235          | 302x2-Ø8T | 1.00 | 1.00 | 1.00 | 86          | -154.9 SPl.5_30 BA CH Ah C11        | 265.3    | 406.7        | 311.0          | 0.59        | 0.59              | 172.9 SPl.5_30 BA CH Ah C11     | 283.0               | 283.0       | 406.7        | 255.9          | 0.66        | 0.66              |
| 408         | Tweside DWSRH - Diagonal (diagonal) | 200x200x8   | S235          | 302x2-Ø8T | 1.00 | 1.00 | 1.00 | 86          | -25.7 SPl.5_30 BA CH Ah C11         | 71.9     | 188.2        | 129.6          | 0.36        | 0.36              | 15.3 SPl.5_30 BA CH Ah C11      | 86.8                | 86.8        | 188.2        | 110.3          | 0.17        | 0.17              |
| 409         | Tweside DWSRH - Diagonal (diagonal) | 200x200x8   | S235          | 202x2-Ø8R | 0.54 | 0.54 | 0.54 | 142         | -20.1 SPl.5_30 BA CH Ah C11         | 77.0     | 188.2        | 129.6          | 0.26        | 0.26              | 28.6 SPl.5_30 BA CH Ah C11      | 117.5               | 117.5       | 188.2        | 117.8          | 0.24        | 0.24              |
| 410         | Tweside DWSRH - Crossing diagonal   | 70x70x6     | S235          | 202x2-Ø8R | 0.52 | 0.52 | 0.52 | 134         | -30.2 SPl.5_30 BA CH Ah C11         | 111.3    | 188.2        | 129.6          | 0.27        | 0.27              | 22.6 SPl.5_30 BA CH Ah C11      | 145.9               | 145.9       | 188.2        | 117.8          | 0.19        | 0.19              |
| 411         | Tweside DWSRH - Crossing diagonal   | 80x80x6     | S235          | 202x2-Ø8R | 0.53 | 0.53 | 0.53 | 108         | -25.7 SPl.5_30 BA CH Ah C11         | 152.9    | 271.1        | 207.4          | 0.38        | 0.38              | 55.4 SPl.5_30 BA CH Ah C11      | 168.0               | 168.0       | 271.1        | 177.2          | 0.33        | 0.33              |
| 412         | Tweside DWSRH - Crossing diagonal   | 80x80x6     | S235          | 202x2-Ø8R | 0.53 | 0.53 | 0.53 | 102         | -25.7 SPl.5_30 BA CH Ah C11         | 152.9    | 271.1        | 207.4          | 0.38        | 0.38              | 55.4 SPl.5_30 BA CH Ah C11      | 168.0               | 168.0       | 271.1        | 177.2          | 0.33        | 0.33              |
| 413         | Tweside DWSRH - Crossing diagonal   | 80x80x6     | S235          | 202x2-Ø8R | 0.53 | 0.53 | 0.53 | 102         | -25.7 SPl.5_30 BA CH Ah C11         | 152.9    | 271.1        | 207.4          | 0.38        | 0.38              | 55.4 SPl.5_30 BA CH Ah C11      | 168.0               | 168.0       | 271.1        | 177.2          | 0.33        | 0.33              |
| 414         | Tweside DWSRH - Horizontal          | 100x65x41   | S355          | 202x2-Ø8T | 1.00 | 2.00 | 1.00 | 103         | 0.0 SPl.5_1_0 BA All C15            | 245.2    | 188.2        | 129.6          | 0.00        | 0.00              | 56.1 ULS 3_120.38               | 401.4               | 401.4       | 188.2        | 323.4          | 0.30        | 0.30              |
| 415         | Tweside DWSRH - Diagonal            | 50x50x5     | S235          | 202x2-Ø8T | 1.00 | 1.00 | 1.00 | 112         | -25.6 SPl.5_30 BA All C15 Ah C12    | 60.8     | 120.6        | 71.0           | 0.42        | 0.42              | 25.6 SPl.5_30 BA All C15 Ah C12 | 71.0                | 71.0        | 120.6        | 130.8          | 0.36        | 0.36              |
| 416         | Tweside DWSRH - Diagonal            | 50x50x5     | S235          | 202x2-Ø8T | 1.00 | 1.00 | 1.00 | 112         | -25.6 SPl.5_30 BA All C15 Ah C12    | 60.8     | 120.6        | 71.0           | 0.42        | 0.42              | 25.6 SPl.5_30 BA All C15 Ah C12 | 71.0                | 71.0        | 120.6        | 130.8          | 0.36        | 0.36              |
| 417         | Tweside DWSRH - Diagonal            | 50x50x5     | S235          | 202x2-Ø8T | 1.00 | 1.00 | 1.00 | 112         | -25.6 SPl.5_30 BA All C15 Ah C12    | 60.8     | 120.6        | 71.0           | 0.42        | 0.42              | 25.6 SPl.5_30 BA All C15 Ah C12 | 71.0                | 71.0        | 120.6        | 130.8          | 0.36        | 0.36              |
| 418         | Tweside DWSRH - Diagonal            | 50x50x5     | S235          | 202x2-Ø8T | 1.00 | 1.00 | 1.00 | 112         | -25.6 SPl.5_30 BA All C15 Ah C12    | 60.8     | 120.6        | 71.0           | 0.42        | 0.42              | 25.6 SPl.5_30 BA All C15 Ah C12 | 71.0                | 71.0        | 120.6        | 130.8          | 0.36        | 0.36              |
| 419         | Tweside DWSRH - Diagonal            | 50x50x5     | S235          | 202x2-Ø8T | 1.00 | 1.00 | 1.00 | 112         | -25.6 SPl.5_30 BA All C15 Ah C12    | 60.8     | 120.6        | 71.0           | 0.42        | 0.42              | 25.6 SPl.5_30 BA All C15 Ah C12 | 71.0                | 71.0        | 120.6        | 130.8          | 0.36        | 0.36              |
| 420         | Tweside DWSRH - Diagonal            | 50x50x5     | S235          | 202x2-Ø8T | 1.00 | 1.00 | 1.00 | 112         | -25.6 SPl.5_30 BA All C15 Ah C12    | 60.8     | 120.6        | 71.0           | 0.42        | 0.42              | 25.6 SPl.5_30 BA All C15 Ah C12 | 71.0                | 71.0        | 120.6        | 130.8          | 0.36        | 0.36              |
| 421         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.50 | 0.50 | 0.50 | 143         | -14.2 SPl.5_30 BA All C15 Ah C12    | 33.9     | 60.3         | 43.2           | 0.42        | 0.42              | 20.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.9           | 0.78        | 0.78              |
| 422         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.52 | 0.52 | 0.52 | 153         | -29.2 SPl.5_30 BA All C15 Ah C12    | 48.9     | 94.1         | 64.8           | 0.60        | 0.60              | 24.0 SPl.5_30 BA All C15 Ah C12 | 74.3                | 74.3        | 94.1         | 57.4           | 0.42        | 0.42              |
| 423         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.52 | 0.52 | 0.52 | 148         | -29.4 SPl.5_30 BA All C15 Ah C12    | 50.9     | 94.1         | 64.8           | 0.58        | 0.58              | 24.0 SPl.5_30 BA All C15 Ah C12 | 74.3                | 74.3        | 94.1         | 57.4           | 0.38        | 0.38              |
| 424         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.52 | 0.52 | 0.52 | 148         | -29.4 SPl.5_30 BA All C15 Ah C12    | 50.9     | 94.1         | 64.8           | 0.58        | 0.58              | 24.0 SPl.5_30 BA All C15 Ah C12 | 74.3                | 74.3        | 94.1         | 57.4           | 0.38        | 0.38              |
| 425         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.52 | 0.52 | 0.52 | 148         | -29.4 SPl.5_30 BA All C15 Ah C12    | 50.9     | 94.1         | 64.8           | 0.58        | 0.58              | 24.0 SPl.5_30 BA All C15 Ah C12 | 74.3                | 74.3        | 94.1         | 57.4           | 0.38        | 0.38              |
| 426         | Tweside DWSRH - Horizontal          | 65x65x6     | S235          | 102x2-Ø8R | 1.00 | 1.00 | 1.00 | 178         | -14.5 ULS 3_30                      | 151.8    | 188.2        | 129.6          | 0.12        | 0.12              | 60.9 SPl.5_30 BA All C15 Ah C12 | 81.2                | 81.2        | 188.2        | 44.6           | 0.00        | 0.00              |
| 427         | Tweside DWSRH - Crossing diagonal   | 55x55x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 141         | -14.2 SPl.5_30 BA All C15 Ah C12    | 38.2     | 60.3         | 43.2           | 0.37        | 0.37              | 15.0 SPl.5_30 BA All C15 Ah C12 | 92.2                | 92.2        | 60.3         | 65.4           | 0.25        | 0.25              |
| 428         | Tweside DWSRH - Crossing diagonal   | 55x55x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 134         | -21.3 SPl.5_30 BA All C15 Ah C12    | 40.5     | 60.3         | 43.2           | 0.33        | 0.33              | 21.1 SPl.5_30 BA All C15 Ah C12 | 92.2                | 92.2        | 60.3         | 65.4           | 0.35        | 0.35              |
| 429         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 430         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 431         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 432         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 433         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 434         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 435         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 436         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 437         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 438         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 439         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 440         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 109         | -10.3 SPl.5_30 BA All C15 Ah C12    | 45.0     | 60.3         | 43.2           | 0.29        | 0.29              | 10.1 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.89        | 0.89              |
| 441         | Tweside DWSRH - Crossing diagonal   | 50x50x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 89          | -14.1 SPl.5_30 BA All C15 Ah C12    | 52.1     | 60.3         | 43.2           | 0.33        | 0.33              | 14.4 SPl.5_30 BA All C15 Ah C12 | 37.4                | 37.4        | 60.3         | 25.7           | 0.56        | 0.56              |
| 442         | Tweside DWSRH - Crossing diagonal   | 60x60x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 68          | -17.4 SPl.5_30 BA All C15 Ah C12    | 74.3     | 94.1         | 64.8           | 0.32        | 0.32              | 17.3 SPl.5_30 BA All C15 Ah C12 | 57.4                | 57.4        | 94.1         | 41.6           | 0.48        | 0.48              |
| 443         | Tweside DWSRH - Crossing diagonal   | 60x60x5     | S235          | 102x2-Ø8R | 0.53 | 0.53 | 0.53 | 68          | -17.4 SPl.5_30 BA All C15 Ah C12    | 74.3     | 94.1         | 64.8           | 0.32        | 0.32              | 17.3 SPl.5_30 BA All C15 Ah C12 | 57.4                | 57.4        | 94.1         | 41.6           | 0.48        | 0.48              |
| 444         | Tweside DWSRH - Vertical bracing    | 50x50x5     | S235          | 102x2-Ø8R | 1.00 | 1.00 | 1.00 | 131         | -2.8 ULS 7                          | 37.3     | 60.3         | 43.2           | 0.07        | 0.07              | 0.0                             | 37.4                | 37.4        | 60.3         | 25.7           | 0.00        | 0.00              |
| 445         | Tweside DWSRH - UWP Member          | 160x65x7.5i | S235          | 202x2-Ø8R | 1.00 | 1.00 | 1.00 | 47          | 0.0                                 | 443.0    | 182.0        | 182.0          | 0.00        | 0.00              | 33.7 ULS 3_0_3_120.38           | 547.9               | 547.9       | 182.0        | 127.6          | 0.26        | 0.26              |

## APPENDIX C

### Knikverkorters

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Niet in PLS-TOWER gemodelleerde elementen in de constructie worden aanvullend getoetst. Hieronder vallen de knikverkorters van de randstijl en profielen onderdeel van stabiliteitsverbanden. De staven worden getoetst op:

- voldoende trek- of druksterkte als steungevend profiel voor randstijl, 1% van de knikcapaciteit van de randstijl;
- slankheid
- klimbelasting

Profielen uit horizontaalverbanden van het onderstuk zijn in PLS-TOWER aanwezig maar worden in deze Appendix aanvullend getoetst op buiging.

Indien bestaande profielen niet voldoen ten aanzien van slankheid, dan wordt deze overschrijding geaccepteerd, aangezien dit niet de sterkte van de mast beïnvloed.



**Knikverkorters initial construction (afkeur)**

Date: 2021-05-20  
 Author: K Chan  
 Version: 1.8

ZW380 Oost  
 HB+0  
 68&78

| Posnr. | Section           | Schematization               | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Sfender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes   |
|--------|-------------------|------------------------------|---------|---------------|--------------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------|-------------------|-----------------------|-------------------|--------------|-----------------|---------|
| 934    | Broekstuk         | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 0.574     | 0            | 24.1              | 0.14         | 61.8               | 60.3           | 30.3              | 31.7                  | 0.72              | 0.79         |                 |         |
| 920    | Broekstuk         | Enkele staaf                 | L75x7   | S235          | M16          | 8.8        | 1.71      | 73           | 117               | 24.1         | 0.00               | 88.9           | 60.3              | 44.8                  | 104.8             | 2.27         | 0.54            |         |
| 933    | Broekstuk         | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 0.98      | 0            | 101               | 24.1         | 0.25               | 48.3           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.79            |         |
| 930    | Broekstuk         | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.24      | 0            | 127               | 24.1         | 0.31               | 38.5           | 60.3              | 31.7                  | 0.72              | 0.79         |                 |         |
| 918    | Broekstuk         | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 1.93      | 57           | 180               | 24.1         | 0.48               | 33.1           | 60.3              | 37.8                  | 55.3              | 1.03         | 0.73            |         |
| 929    | Broekstuk         | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 1.91      | 0            | 178               | 24.1         | 0.48               | 33.8           | 60.3              | 37.8                  | 55.3              | 1.03         | 0.71            |         |
| 916    | Broekstuk         | Enkele staaf                 | L60x6   | S235          | M16          | 8.8        | 2.34      | 44           | 200               | 24.1         | 0.00               | 31.5           | 60.3              | 38.4                  | 72.6              | 1.24         | 0.76            |         |
| 928    | Broekstuk         | Enkele staaf                 | L65x6   | S235          | M16          | 8.8        | 2.57      | 0            | 203               | 24.1         | 0.64               | 33.6           | 60.3              | 38.4                  | 72.6              | 1.46         | 0.72            |         |
| 914    | Broekstuk         | Enkele staaf                 | L65x6   | S235          | M16          | 8.8        | 2.85      | 35           | 224               | 24.1         | 0.00               | 29.1           | 60.3              | 38.4                  | 72.6              | 1.46         | 0.83            |         |
| 927    | Broekstuk         | Enkele staaf                 | L75x6   | S235          | M16          | 8.8        | 3.24      | 0            | 220               | 24.1         | 0.81               | 34.7           | 60.3              | 38.4                  | 89.9              | 1.96         | 0.69            |         |
| 912    | Broekstuk         | Enkele staaf                 | L75x6   | S235          | M16          | 8.8        | 3.19      | 29           | 217               | 24.1         | 0.70               | 35.5           | 60.3              | 38.4                  | 89.9              | 1.96         | 0.68            |         |
| 974    | Pootverband       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 0.84      | 0            | 86                | 3.8          | 0.21               | 54.4           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.29            |         |
| 972    | Pootverband       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.75      | 0            | 115               | 3.8          | 0.22               | 32.9           | 60.3              | 30.3                  | 31.7              | 0.54         | 0.42            |         |
| 970    | Pootverband       | Kniksteun en verticale steun | L50x5   | S235          | M16          | 8.8        | 2.73      | 0            | 180               | 3.8          | 0.34               | 20.2           | 60.3              | 30.3                  | 31.7              | 0.54         | 0.66            |         |
| 968    | Pootverband       | Kniksteun en verticale steun | L50x5   | S235          | M16          | 8.8        | 3.68      | 0            | 243               | 3.8          | 0.46               | 13.7           | 60.3              | 30.3                  | 31.7              | 0.54         | 0.89            |         |
| 966    | Pootverband       | Kniksteun en verticale steun | L50x5   | S235          | M16          | 8.8        | 4.63      | 0            | 306               | 3.8          | 0.58               | 9.8            | 60.3              | 30.3                  | 31.7              | 0.54         | 1.11            | Bending |
| 973    | Pootverband       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.90      | 77           | 195               | 3.8          | 0.00               | 22.6           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.17            |         |
| 971    | Pootverband       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.04      | 64           | 210               | 3.8          | 0.00               | 20.4           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.19            |         |
| 969    | Pootverband       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.28      | 53           | 234               | 3.8          | 0.00               | 17.4           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.22            |         |
| 967    | Pootverband       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.59      | 45           | 266               | 3.8          | 0.00               | 14.3           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.37            |         |
| 965    | Pootverband       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.87      | 36           | 295               | 3.8          | 0.00               | 12.2           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.51            |         |
| 937    | Tussenschot +9,6m | Enkele staaf                 | L120x8  | S235          | M24          | 8.8        | 3.63      | 0            | 162               | 24.1         | 0.96               | 113.8          | 135.6             | 149.5                 | 365.5             | 7.71         | 0.21            |         |
| 936    | Tussenschot +9,6m | Kniksteun en verticale steun | L60x6   | S235          | M16          | 8.8        | 5.29      | 0            | 291               | 1.8          | 0.66               | 15.2           | 60.3              | 38.4                  | 72.6              | 0.93         | 0.74            |         |
| 935    | Tussenschot +9,6m | Kniksteun en verticale steun | L80x6   | S235          | M20          | 8.8        | 7.85      | 0            | 321               | 1.8          | 0.98               | 17.7           | 94.1              | 52.4                  | 100.2             | 2.2          | 0.44            |         |
| 992    | Tussenstuk1       | Enkele staaf                 | L65x6   | S235          | M16          | 8.8        | 2.45      | 43           | 193               | 24.0         | 0.00               | 36.0           | 60.3              | 38.4                  | 72.6              | 1.46         | 0.67            |         |
| 9100   | Tussenstuk1       | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 1.89      | 0            | 176               | 24.0         | 0.47               | 34.2           | 60.3              | 37.8                  | 55.3              | 1.03         | 0.70            |         |
| 998    | Tussenstuk1       | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 1.56      | 0            | 145               | 24.0         | 0.39               | 43.6           | 60.3              | 37.8                  | 55.3              | 1.03         | 0.81            |         |
| 991    | Tussenstuk1       | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 2.11      | 48           | 197               | 24.0         | 0.00               | 29.5           | 60.3              | 37.8                  | 55.3              | 1.03         | 0.63            |         |
| 996    | Tussenstuk1       | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 2.99      | 0            | 203               | 24.0         | 0.75               | 38.9           | 60.3              | 37.8                  | 89.9              | 1.96         | 0.62            |         |
| 987    | Tussenstuk1       | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 2.18      | 39           | 203               | 24.0         | 0.00               | 28.1           | 60.3              | 37.8                  | 55.3              | 1.03         | 0.85            |         |
| 995    | Tussenstuk1       | Enkele staaf                 | L55x6   | S235          | M16          | 8.8        | 1.52      | 0            | 142               | 24.0         | 0.38               | 44.9           | 60.3              | 37.8                  | 55.3              | 1.0          | 0.63            |         |
| 9180   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.28      | 0            | 132               | 17.0         | 0.32               | 37.1           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.56            |         |
| 9171   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.72      | 47           | 177               | 17.0         | 0.00               | 25.9           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.66            |         |
| 9179   | Tussenstuk2       | Enkele staaf                 | L50x6   | S235          | M16          | 8.8        | 2.41      | 0            | 225               | 17.0         | 0.00               | 24.3           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.69            |         |
| 9168   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.79      | 39           | 183               | 17.0         | 0.00               | 24.7           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.56            |         |
| 9178   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.25      | 0            | 128               | 17.0         | 0.31               | 38.3           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.56            |         |
| 9176   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.05      | 0            | 107               | 17.0         | 0.26               | 45.6           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.56            |         |
| 9166   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.37      | 46           | 141               | 17.0         | 0.00               | 34.4           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.56            |         |
| 9175   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.90      | 0            | 196               | 17.0         | 0.48               | 22.6           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.75            |         |
| 9163   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.44      | 39           | 147               | 17.0         | 0.00               | 32.6           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.56            |         |
| 9174   | Tussenstuk2       | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 0.99      | 0            | 102               | 17.0         | 0.25               | 47.8           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.56            |         |
| 9133   | Bovenstuk1        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.66      | 0            | 170               | 9.0          | 0.41               | 27.3           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.58            |         |



**Knikverkorters initial construction (afkeur)**

Date: 2021-05-20  
 Author: K Chan  
 Version: 1.8

ZW380 Oost  
 HB+0  
 68878

| Posnr. | Section    | Schematizaton | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Slenderness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|------------|---------------|---------|---------------|--------------|------------|-----------|-------------|-------------------|--------------|--------------------|----------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
|        |            |               |         |               |              |            |           |             |                   |              |                    |                |                   |                       |                   |              |                 |       |
| g130   | Bovenstuk1 | Enkele staaf  | L50x5   | S235          | M16          | 1.50       | 0         | 154         | 9.0               | 0.38         | 30.9               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.52         |                 |       |
| g215   | Bovenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.39       | 0         | 143         | 4.2               | 0.35         | 33.9               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.48         |                 |       |
| g213   | Bovenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.29       | 0         | 132         | 4.2               | 0.32         | 37.1               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.45         |                 |       |



**Knikverkorters adjusted construction (verbouw)**

ZW380 Oost  
 HB+0  
 68&78

Date: 2021-05-20  
 Author: K. Chan  
 Version: 1.8

| Posnr. | Section     | Schematization    | Profile | Steel Quality | Bolt | Quality | Length (m) | Angle (°) | Slenderness (λ) | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Bolt (kN) | Shear Cap. (kN) | Bearing Cap. (kN) | Block Tearing Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type   | Mitigation |
|--------|-------------|-------------------|---------|---------------|------|---------|------------|-----------|-----------------|-------------------|--------------|--------------------|-----------------|-----------------|-------------------|-------------------------|-------------------|--------------|-------------------|------------|
| 966    | Pootverband | Kniksteun en vert | L70x7   | S355          | M16  | 8.8     | 4.63       | 0         | 218             | 3.8               | 0.75         | 35.3               | 60.3            | 61.0            | 170.1             | 2.99                    | 0.35              |              | Profile exchanged |            |





**Knikverkorters initial construction (afkeur)**

Date: 2021-05-26  
 Author: K Chan  
 Version: 1.8

ZW380 Oost  
 HS+0  
 26

| Posnr. | Section          | Schematization               | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Sfender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|------------------|------------------------------|---------|---------------|--------------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
| 946    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 0.65      | 0            | 10.6              | 0.16         | 59.7               | 60.3           | 30.3              | 31.7                  | 0.72              | 0.35         |                 |       |
| 929    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.53      | 68           | 158               | 10.6         | 0.00               | 30.1           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.35            |       |
| 942    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.35      | 0            | 139               | 10.6         | 0.34               | 35.1           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.47            |       |
| 926    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.85      | 50           | 190               | 10.6         | 0.00               | 23.5           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.45            |       |
| 938    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.05      | 0            | 191               | 10.6         | 0.51               | 25.8           | 60.3              | 31.5                  | 46.1              | 0.87         | 0.59            |       |
| 923    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.34      | 37           | 240               | 10.6         | 0.00               | 16.7           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.63            |       |
| 936    | Broekstuk        | Enkele staaf                 | L60x6   | S235          | M16          | 8.8        | 2.75      | 0            | 235               | 10.6         | 0.69               | 24.9           | 60.3              | 38.4                  | 72.6              | 1.24         | 0.55            |       |
| 920    | Broekstuk        | Enkele staaf                 | L55x5   | S235          | M16          | 8.8        | 2.92      | 29           | 272               | 10.6         | 0.64               | 15.3           | 60.3              | 31.5                  | 46.1              | 0.87         | 0.74            |       |
| 917    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.81      | 28           | 288               | 10.6         | 0.62               | 12.6           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.86            |       |
| 934    | Broekstuk        | Enkele staaf                 | L60x6   | S235          | M16          | 8.8        | 2.27      | 0            | 194               | 10.6         | 0.57               | 32.9           | 60.3              | 38.4                  | 72.6              | 1.24         | 0.48            |       |
| 914    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.95      | 47           | 200               | 10.6         | 0.00               | 21.9           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.46            |       |
| 930    | Broekstuk        | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.10      | 0            | 113               | 10.6         | 0.27               | 43.7           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.38            |       |
| 9127   | Pootverband      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.48      | 0            | 152               | 1.3          | 0.37               | 31.3           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.52            |       |
| 9125   | Pootverband      | Kniksteun en verticale steun | L50x5   | S235          | M16          | 8.8        | 3.16      | 0            | 209               | 1.3          | 0.39               | 16.8           | 60.3              | 30.3                  | 31.7              | 0.54         | 0.76            |       |
| 9126   | Pootverband      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 2.86      | 75           | 294               | 1.3          | 0.00               | 12.2           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.11            |       |
| 9124   | Pootverband      | Enkele staaf                 | L55x5   | S235          | M16          | 8.8        | 3.09      | 59           | 288               | 1.3          | 0.00               | 14.0           | 60.3              | 31.5                  | 46.1              | 0.87         | 0.09            |       |
| 9122   | Tussenschot + 7m | Enkele staaf                 | L65x6   | S235          | M16          | 8.8        | 3.44      | 0            | 271               | 10.6         | 0.86               | 21.8           | 60.3              | 38.4                  | 72.6              | 1.46         | 0.59            |       |
| 9120   | Tussenschot + 7m | Kniksteun en verticale steun | L75x6   | S235          | M16          | 8.8        | 4.65      | 0            | 204               | 0.2          | 0.58               | 31.6           | 60.3              | 38.4                  | 89.9              | 1.54         | 0.40            |       |
| 9121   | Tussenschot + 7m | Kruisende staaf halverwege   | L65x6   | S235          | M16          | 8.8        | 6.86      | 0            | 348               | 0.2          | 0.86               | 12.6           | 60.3              | 38.4                  | 72.6              | 1.46         | 0.59            |       |
| 9100   | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.29      | 0            | 133               | 10.9         | 0.32               | 36.9           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.45            |       |
| 990    | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.89      | 50           | 194               | 10.9         | 0.00               | 22.8           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.48            |       |
| 998    | Tussenstuk1      | Enkele staaf                 | L60x6   | S235          | M16          | 8.8        | 2.57      | 0            | 218               | 10.9         | 0.64               | 23.4           | 60.3              | 32.0                  | 60.5              | 1.05         | 0.61            |       |
| 988    | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.83      | 48           | 188               | 10.9         | 0.00               | 23.8           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.46            |       |
| 9162   | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.71      | 50           | 176               | 10.9         | 0.00               | 26.1           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.42            |       |
| 997    | Tussenstuk1      | Enkele staaf                 | L60x6   | S235          | M16          | 8.8        | 2.24      | 0            | 191               | 10.9         | 0.56               | 28.4           | 60.3              | 32.0                  | 60.5              | 1.1          | 0.53            |       |
| 985    | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.64      | 50           | 169               | 10.9         | 0.00               | 27.6           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.39            |       |
| 996*   | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.73      | 43           | 178               | 10.9         | 0.00               | 25.7           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.42            |       |
| 9104   | Tussenstuk1      | Enkele staaf                 | L60x6   | S235          | M16          | 8.8        | 2.58      | 0            | 220               | 10.9         | 0.65               | 23.1           | 60.3              | 32.0                  | 60.5              | 1.05         | 0.61            |       |
| 995    | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.70      | 43           | 175               | 10.9         | 0.00               | 26.3           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.41            |       |
| 993    | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.77      | 50           | 182               | 10.9         | 0.00               | 25.0           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.44            |       |
| 9102   | Tussenstuk1      | Enkele staaf                 | L60x6   | S235          | M16          | 8.8        | 2.29      | 0            | 195               | 10.9         | 0.57               | 27.5           | 60.3              | 32.0                  | 60.5              | 1.05         | 0.55            |       |
| 992    | Tussenstuk1      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.70      | 50           | 174               | 10.9         | 0.00               | 26.4           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.41            |       |
| 9164   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.54      | 51           | 159               | 11.0         | 0.00               | 29.9           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.37            |       |
| 9177   | Tussenstuk2      | Enkele staaf                 | L55x5   | S235          | M16          | 8.8        | 1.95      | 0            | 182               | 11.0         | 0.49               | 27.7           | 60.3              | 31.5                  | 46.1              | 0.87         | 0.56            |       |
| 9162   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.46      | 52           | 150               | 11.0         | 0.00               | 31.9           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.36            |       |
| 9161   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.30      | 50           | 134               | 11.0         | 0.00               | 36.5           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.36            |       |
| 9176   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.69      | 0            | 173               | 11.0         | 0.42               | 26.6           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.59            |       |
| 9158   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.24      | 51           | 127               | 11.0         | 0.00               | 38.7           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.36            |       |
| 9159   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.20      | 53           | 123               | 11.0         | 0.00               | 40.1           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.36            |       |
| 9175   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.46      | 0            | 150               | 11.0         | 0.36               | 32.0           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.51            |       |
| 9156   | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.12      | 54           | 115               | 11.0         | 0.00               | 42.9           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.36            |       |
| 9174*  | Tussenstuk2      | Enkele staaf                 | L50x5   | S235          | M16          | 8.8        | 1.56      | 51           | 160               | 11.0         | 0.00               | 29.5           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.37            |       |



Date: 2021-05-26  
 Author: K Chan  
 Version: 1.8

**Knikverkorters initial construction (afkeur)**

ZW380 Oost  
 HS+0  
 26

| Posnr. | Section     | Schematizatie | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Sfender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|-------------|---------------|---------|---------------|--------------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
| 9183   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.99       | 0         | 186          | 11.0              | 0.50         | 26.9               | 60.3           | 31.5              | 46.1                  | 0.9               | 0.57         |                 |       |
| 9173   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.48       | 51        | 152          | 11.0              | 0.00         | 31.4               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.36         |                 |       |
| 9171   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.31       | 50        | 135          | 11.0              | 0.00         | 36.2               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.36         |                 |       |
| 9181   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.73       | 0         | 178          | 11.0              | 0.43         | 25.7               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.60         |                 |       |
| 9170   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.25       | 50        | 128          | 11.0              | 0.00         | 38.2               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.36         |                 |       |
| 9168   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.10       | 48        | 113          | 11.0              | 0.00         | 43.5               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.36         |                 |       |
| 9179   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.52       | 0         | 157          | 11.0              | 0.38         | 30.3               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.53         |                 |       |
| 9167   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 1.05       | 48        | 107          | 11.0              | 0.00         | 45.6               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.36         |                 |       |
| 9165   | Tussenstuk2 | Enkele staaf  | L50x5   | S235          | M16          | 0.79       | 29        | 81           | 11.0              | 0.17         | 55.7               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.36         |                 |       |
| 9308   | Bovenstuk1  | Enkele staaf  | L50x5   | S235          | M16          | 1.34       | 0         | 137          | 4.7               | 0.33         | 35.5               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.46         |                 |       |
| 9306   | Bovenstuk1  | Enkele staaf  | L50x5   | S235          | M16          | 1.23       | 0         | 126          | 4.7               | 0.31         | 38.8               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.43         |                 |       |
| 9304   | Bovenstuk2  | Enkele staaf  | L50x5   | S235          | M16          | 1.14       | 0         | 117          | 2.4               | 0.29         | 42.0               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.40         |                 |       |
| 9302   | Bovenstuk2  | Enkele staaf  | L50x5   | S235          | M16          | 1.04       | 0         | 107          | 2.4               | 0.26         | 45.8               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.36         |                 |       |



**Knikverkorters initial construction (afkeur)**

Date: 2021-05-11  
 Author: K Chan  
 Version: 1.8

ZW380 Oost  
 HC+0  
 16

| Posnr. | Section     | Schematization                     | Profile | Steel Quality | Bolt Quality | Length (m) | Angle (°) | Sfenderness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes   |  |
|--------|-------------|------------------------------------|---------|---------------|--------------|------------|-----------|-------------|-------------------|--------------|--------------------|----------------|-------------------|-----------------------|-------------------|--------------|-----------------|---------|--|
| 940    | Broekstuk   | Enkele staaf                       | L60x5   | S235          | M20          | 8.8        | 0.575     | 0           | 28.5              | 0.14         | 78.3               | 94.1           | 39.6              | 1.05                  | 0.72              |              |                 |         |  |
| 930    | Broekstuk   | Enkele staaf                       | L75x7   | S235          | M20          | 8.8        | 1.49      | 84          | 102               | 0.00         | 100.7              | 94.1           | 61.1              | 96.8                  | 2.27              | 0.47         |                 |         |  |
| 936    | Broekstuk   | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.03      | 0           | 106               | 0.26         | 46.3               | 60.3           | 30.3              | 31.7                  | 0.72              | 0.94         |                 |         |  |
| 939    | Broekstuk   | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.27      | 0           | 130               | 0.32         | 37.6               | 60.3           | 30.3              | 31.7                  | 0.72              | 0.94         |                 |         |  |
| 927    | Broekstuk   | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 1.93      | 56          | 164               | 0.48         | 34.6               | 60.3           | 32.0              | 60.5                  | 1.05              | 0.89         |                 |         |  |
| 935    | Broekstuk   | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 1.93      | 0           | 164               | 0.48         | 34.7               | 60.3           | 32.0              | 60.5                  | 1.05              | 0.89         |                 |         |  |
| 924    | Broekstuk   | Enkele staaf                       | L60x6   | S235          | M16          | 8.8        | 2.34      | 43          | 200               | 0.85         | 31.5               | 60.3           | 38.4              | 72.6                  | 1.24              | 0.91         |                 |         |  |
| 934    | Broekstuk   | Enkele staaf                       | L50x6   | S235          | M16          | 8.8        | 2.59      | 0           | 204               | 0.85         | 33.4               | 60.3           | 38.4              | 72.6                  | 1.46              | 0.85         |                 |         |  |
| 921    | Broekstuk   | Enkele staaf                       | L70x6   | S235          | M16          | 8.8        | 2.85      | 34          | 207               | 0.85         | 35.2               | 60.3           | 38.4              | 89.9                  | 1.71              | 0.81         |                 |         |  |
| 918    | Broekstuk   | Enkele staaf                       | L75x6   | S235          | M16          | 8.8        | 3.24      | 0           | 221               | 0.85         | 34.6               | 60.3           | 38.4              | 89.9                  | 1.96              | 0.82         |                 |         |  |
| 913    | Broekstuk   | Enkele staaf                       | L75x7   | S235          | M16          | 8.8        | 3.18      | 29          | 217               | 0.85         | 41.0               | 60.3           | 44.8              | 104.8                 | 2.27              | 0.70         |                 |         |  |
| 969    | Pootverband | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 0.88      | 0           | 91                | 4.1          | 0.22               | 52.4           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.31            |         |  |
| 968    | Pootverband | Kniksteun en verticale steun       | L50x5   | S235          | M16          | 8.8        | 1.82      | 0           | 120               | 4.1          | 0.23               | 31.7           | 60.3              | 30.3                  | 31.7              | 0.54         | 0.44            |         |  |
| 967    | Pootverband | Kniksteun en verticale steun       | L50x5   | S235          | M16          | 8.8        | 2.76      | 0           | 182               | 4.1          | 0.34               | 20.0           | 60.3              | 30.3                  | 31.7              | 0.54         | 0.66            |         |  |
| 966    | Pootverband | Kniksteun en verticale steun       | L50x5   | S235          | M16          | 8.8        | 3.69      | 0           | 244               | 4.1          | 0.46               | 13.6           | 60.3              | 30.3                  | 31.7              | 0.54         | 0.89            |         |  |
| 965    | Pootverband | Kniksteun en verticale steun       | L50x5   | S235          | M16          | 8.8        | 4.63      | 0           | 306               | 4.1          | 0.58               | 9.8            | 60.3              | 30.3                  | 31.7              | 0.54         | 1.11            | Bending |  |
| 964    | Pootverband | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.88      | 76          | 193               | 4.1          | 0.00               | 22.9           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.18            |         |  |
| 963    | Pootverband | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 2.03      | 63          | 209               | 4.1          | 0.00               | 20.6           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.20            |         |  |
| 962    | Pootverband | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 2.27      | 53          | 233               | 4.1          | 0.00               | 17.5           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.24            |         |  |
| 961    | Pootverband | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 2.58      | 44          | 265               | 4.1          | 0.00               | 14.4           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.28            |         |  |
| 960    | Pootverband | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 2.88      | 36          | 293               | 4.1          | 0.00               | 12.3           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.33            |         |  |
| 915    | Tussenschot | +9,6m Enkele staaf                 | L120x10 | S235          | M16          | 8.8        | 3.84      | 0           | 162               | 0.96         | 140.9              | 60.3           | 64.0              | 293.8                 | 8.49              | 0.47         |                 |         |  |
| 917    | Tussenschot | +9,6m Kniksteun en verticale steun | L60x6   | S235          | M16          | 8.8        | 5.28      | 0           | 291               | 1.7          | 0.66               | 15.2           | 60.3              | 38.4                  | 72.6              | 1.05         | 0.44            |         |  |
| 914    | Tussenschot | +9,6m Kniksteun en verticale steun | L80x6   | S235          | M16          | 8.8        | 7.84      | 0           | 321               | 1.7          | 0.98               | 17.8           | 60.3              | 38.4                  | 107.1             | 2.2          | 0.44            |         |  |
| 994    | Tussenstuk1 | Enkele staaf                       | L65x6   | S235          | M16          | 8.8        | 2.43      | 45          | 192               | 28.4         | 0.47               | 35.6           | 60.3              | 38.4                  | 72.6              | 1.46         | 0.78            |         |  |
| 999    | Tussenstuk1 | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 1.89      | 0           | 161               | 28.4         | 0.00               | 36.4           | 60.3              | 32.0                  | 60.5              | 1.05         | 0.89            |         |  |
| 997    | Tussenstuk1 | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 1.56      | 0           | 133               | 28.4         | 0.39               | 44.8           | 60.3              | 32.0                  | 60.5              | 1.05         | 0.89            |         |  |
| 990    | Tussenstuk1 | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 2.11      | 48          | 179               | 28.4         | 0.00               | 30.9           | 60.3              | 32.0                  | 60.5              | 1.05         | 0.92            |         |  |
| 996    | Tussenstuk1 | Enkele staaf                       | L70x6   | S235          | M16          | 8.8        | 3.00      | 0           | 218               | 0.75         | 32.7               | 60.3           | 38.4              | 89.9                  | 1.71              | 0.87         |                 |         |  |
| 989    | Tussenstuk1 | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 2.18      | 39          | 185               | 28.4         | 0.00               | 29.5           | 60.3              | 32.0                  | 60.5              | 1.05         | 0.96            |         |  |
| 995    | Tussenstuk1 | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 1.52      | 0           | 129               | 28.4         | 0.38               | 46.0           | 60.3              | 32.0                  | 60.5              | 1.1          | 0.89            |         |  |
| 9144   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.24      | 0           | 128               | 20.2         | 0.31               | 38.4           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.67            |         |  |
| 9137   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.69      | 48          | 174               | 20.2         | 0.00               | 26.5           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.76            |         |  |
| 9143   | Tussenstuk2 | Enkele staaf                       | L60x5   | S235          | M16          | 8.8        | 2.37      | 0           | 202               | 0.59         | 26.2               | 60.3           | 32.0              | 60.5                  | 1.05              | 0.77         |                 |         |  |
| 9133   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.76      | 39          | 180               | 20.2         | 0.00               | 25.2           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.80            |         |  |
| 9142   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.21      | 0           | 124               | 20.2         | 0.30               | 39.7           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.67            |         |  |
| 9140   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 0.99      | 0           | 102               | 20.2         | 0.25               | 47.9           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.67            |         |  |
| 9132   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.35      | 48          | 138               | 20.2         | 0.00               | 35.2           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.67            |         |  |
| 9139   | Tussenstuk2 | Enkele staaf                       | L55x5   | S235          | M16          | 8.8        | 1.87      | 0           | 174               | 20.2         | 0.47               | 29.3           | 60.3              | 31.5                  | 46.1              | 0.87         | 0.69            |         |  |
| 9130   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.41      | 40          | 144               | 20.2         | 0.00               | 33.5           | 60.3              | 30.3                  | 31.7              | 0.72         | 0.67            |         |  |
| 9138   | Tussenstuk2 | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 0.95      | 0           | 98                | 20.2         | 0.24               | 49.5           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.67            |         |  |
| 9178   | Bovenstuk1  | Enkele staaf                       | L50x5   | S235          | M16          | 8.8        | 1.65      | 0           | 170               | 11.1         | 0.41               | 27.4           | 60.3              | 30.3                  | 31.7              | 0.7          | 0.57            |         |  |



**Knikverkorters initial construction (afkeur)**

Date: 2021-05-11  
 Author: K Chan  
 Version: 1.8

ZW380 Oost  
 HC+0  
 16

| Posnr. | Section    | Schematizatie | Profile | Steel Quality | Bolt | Quality | Length (m) | Angle (°) | Slenderness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type | Notes |
|--------|------------|---------------|---------|---------------|------|---------|------------|-----------|-------------|-------------------|--------------|--------------------|----------------|-------------------|-----------------------|-------------------|--------------|-----------------|-------|
|        |            |               |         |               |      |         |            |           |             |                   |              |                    |                |                   |                       |                   |              |                 |       |
| g176   | Bovenstuk1 | Enkele staaf  | L50x5   | S235          | M16  | 8.8     | 1.50       | 0         | 154         | 11.1              | 0.37         | 31.0               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.52         |                 |       |
| g309   | Bovenstuk2 | Enkele staaf  | L50x5   | S235          | M16  | 8.8     | 1.40       | 0         | 143         | 5.4               | 0.35         | 33.8               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.49         |                 |       |
| g307   | Bovenstuk2 | Enkele staaf  | L50x5   | S235          | M16  | 8.8     | 1.26       | 0         | 129         | 5.4               | 0.32         | 37.9               | 60.3           | 30.3              | 31.7                  | 0.7               | 0.44         |                 |       |



**Knikverkorters adjusted construction (verbouw)**

ZW380 Oost  
 HC+0  
 16

Date: 2021-05-11  
 Author: K. Chan  
 Version: 1.8

| Posnr. | Section     | Schematization    | Profile      | Steel Quality | Bolt       | Quality | Length (m) | Angle (°) | Slenderness (λ) | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Bolt (kN) | Shear Cap. (kN) | Bearing Cap. (kN) | Block Tearing Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Exceedance Type   | Mitigation |
|--------|-------------|-------------------|--------------|---------------|------------|---------|------------|-----------|-----------------|-------------------|--------------|--------------------|-----------------|-----------------|-------------------|-------------------------|-------------------|--------------|-------------------|------------|
| 965    | Pootverband | Kniksteun en vert | <b>L70x7</b> | <b>S355</b>   | <b>M16</b> | 8.8     | 4.63       | 0         | 218             | 4.1               | 0.75         | 35.3               | 60.3            | 61.0            | 170.1             | 2.99                    | 0.35              |              | Profile exchanged |            |

## APPENDIX D

### Blokdeuvels

De belastingen op de fundatie uit Appendix A zijn uitgangspunt voor de berekening van de ingestorte rand met blokdeuvels. De belastingen in de richting van de randstijl zijn van toepassing. In de tabellen is dit opgenomen in de laatste kolom  $R_{z,lok}$ . De controles zijn uitgevoerd met een spreadsheet. Vanwege de helling van de drukdiagonaal wordt per krachtrichting bepaald hoeveel deuvels effectief zijn.

Voor de berekening van de blokdeuvels zijn de masttypen als volgt samengevoegd:

- Masttype HB+0 (68 & 78)
- Masttype HC+0
- Masttype HS+0

De blokdeuvels worden getoetst op de maatgevende belasting per masttype. De belastingen waaraan getoetst worden zijn onderstaand weergegeven.

#### Masttype HB+0 (68 & 78)

Envelope of load combinations for all of the legs

| Index                | Combination                   | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|----------------------|-------------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| Max. pressure        | SPLS 3_105.975 Ba All Cts     | 249           | 270           | <b>1378</b>   | -15              | -367            | -62                   | 1411                |
| Max. tension         | SPLS 3_0,9_105.975 Ba All Cts | 191           | 211           | <b>-1089</b>  | 14               | 284             | 43                    | -1116               |
| Max. pos. torsie     | SPLS 6a_90 Ba Ct2 Ah Ct2      | -24           | -186          | 426           | <b>149</b>       | -114            | -20                   | 436                 |
| Max. neg. torsie     | SPLS 6a_90 Ba Ct1 Ah Ct1      | -96           | -119          | -75           | <b>-152</b>      | 16              | -1                    | -77                 |
| Comb. tension+torsie | SPLS 3_0,9_105.975 Ba All Cts | 191           | 211           | <b>-1089</b>  | <b>14</b>        | 284             | 43                    | -1116               |

#### Masttype HC+0

Envelope of load combinations for all of the legs

| Index                | Combination                  | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|----------------------|------------------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| Max. pressure        | SPLS 3_120.38 Ba All Cts     | 274           | 284           | <b>1486</b>   | -7               | -395            | -67                   | 1522                |
| Max. tension         | SPLS 3_0,9_120.38 Ba All Cts | 212           | 221           | <b>-1175</b>  | 6                | 306             | 46                    | -1204               |
| Max. pos. torsie     | SPLS 6a_90 Ba Ct2 Ah Ct2     | -112          | -116          | 2             | <b>161</b>       | -3              | -2                    | 2                   |
| Max. neg. torsie     | SPLS 6a_90 Ba Ct1 Ah Ct1     | -188          | -44           | 371           | <b>-164</b>      | -102            | -20                   | 380                 |
| Comb. tension+torsie | SPLS 3_0,9_120.38 Ba Ct1     | 259           | 92            | <b>-969</b>   | <b>-118</b>      | 248             | 34                    | -993                |

#### Masttype HS+0

Envelope of load combinations for all of the legs

| Index                | Combination        | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|----------------------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| Max. pressure        | ULS 1a_135         | -127          | 114           | <b>715</b>    | -9               | -170            | -25                   | 730                 |
| Max. tension         | ULS 1a_0,9_0,9_135 | -95           | 82            | <b>-544</b>   | 9                | 125             | 15                    | -555                |
| Max. pos. torsie     | ULS 5a Ah 10       | 34            | -19           | 38            | <b>37</b>        | -11             | -3                    | 39                  |
| Max. neg. torsie     | ULS 5a Ba 10       | -34           | -19           | 38            | <b>-37</b>       | -11             | -3                    | 39                  |
| Comb. tension+torsie | ULS 1a_0,9_0,9_135 | -95           | 82            | <b>-544</b>   | <b>9</b>         | 125             | 15                    | -555                |

Project: ZW380-Oost  
Mast: HB+0 (68&78)

### Shear blocks

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-05-25

Auteur: TBR

Versie: 1.4

| Load        |            |         | Results     |      |                |
|-------------|------------|---------|-------------|------|----------------|
| Compression | $F_{Ed,c}$ | 1411 kN | Compression | U.C. | 0.81 < 1,00 OK |
| Tension     | $F_{Ed,t}$ | 1116 kN | Tension     | U.C. | 0.81 < 1,00 OK |

#### Main leg

|                    |          |                      |
|--------------------|----------|----------------------|
| Profile            |          | <b>L200.20</b>       |
| Steel material     |          | S355                 |
| Cross section      |          | 7635 mm <sup>2</sup> |
| Axial capacity     | $N_{pl}$ | 2710 kN              |
| Width              | $b$      | 200 mm               |
| Thickness          | $t$      | 20 mm                |
| Length in concrete |          | 1500 mm              |

#### Shear blocks main leg

|                    |       |        |
|--------------------|-------|--------|
| Width              | $b$   | 30 mm  |
| Thickness          | $h$   | 30 mm  |
| Length             | $L$   | 200 mm |
| Welds              | $a$   | 4 mm   |
| c.t.c. separation  | $s$   | 240 mm |
| Number for compr.  | $n_c$ | 11 -   |
| Number for tension | $n_t$ | 11 -   |

#### Foot plate

|             |     |       |
|-------------|-----|-------|
| Thickness   | $t$ | 30 mm |
| Ext. length | $m$ | 30 mm |
| Welds       | $a$ | 5 mm  |

#### Pile

|                   |  |                       |
|-------------------|--|-----------------------|
| Name              |  | Buispaal              |
| Diameter          |  | 609 mm                |
| Thickness         |  | 10 mm                 |
| Cross section     |  | 18818 mm <sup>2</sup> |
| Steel material    |  | S355                  |
| Capacity          |  | 6680 kN               |
| Concrete strength |  | C30/37                |

#### Shear blocks pile

|                    |       |        |
|--------------------|-------|--------|
| Width              | $b$   | 30 mm  |
| Thickness          | $h$   | 30 mm  |
| Length             | $L$   | 750 mm |
| Welds              | $a$   | 5 mm   |
| c.t.c. separation  | $s$   | 300 mm |
| Number for compr.  | $n_c$ | 6 -    |
| Number for tension | $n_t$ | 6 -    |

#### Design value concrete strength

|                  |            |                        |
|------------------|------------|------------------------|
| Material factor  | $\gamma_c$ | 1.5                    |
| Add. mat. factor | $\gamma_m$ | 1.25 -                 |
| $f_{cd} =$       |            | 16.0 N/mm <sup>2</sup> |

#### Steel tower stub

|                  |            |                       |
|------------------|------------|-----------------------|
| Yield strength   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Tensile strength | $f_{ud} =$ | 490 N/mm <sup>2</sup> |

#### Capacity shear blocks main leg

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 6000 mm <sup>2</sup>   |
| $A_{f2} =$                                     | 20448 mm <sup>2</sup>  |
| Slope  | 1 : 5                  |
| $C_A = \sqrt{A_{f2}/A_{f1}} =$                 | 1.85                   |
| $f_{jd} = C_A \times f_{cd} =$                 | 29.5 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | 1949 kN                |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | 1949 kN                |

#### Capacity foot plate

|   |                        |
|---|------------------------|
| $k_d =$                                 | 1.73 -                 |
| $f_{jd} = C_A \times f_{cd} =$          | 27.7 N/mm <sup>2</sup> |
| $c = t\sqrt{(f_{yd} / 3f_{jd})} =$      | 60 mm                  |
| $m^* = \min(c, m) =$                    | 30 mm                  |
| Type foot plate                         | Extending              |
| Effective for                           | Compr. and tension     |
| $A_{p,c} =$                             | 35235 mm <sup>2</sup>  |
| $F_{Rd,c} = A_{p,druk} \times f_{jd} =$ | 976 kN                 |
| $A_{p,t} =$                             | 27600 mm <sup>2</sup>  |
| $F_{Rd,t} = A_{p,t} \times f_{jd} =$    | 765 kN                 |

#### Capacities

|   |                |
|---|----------------|
| $F_{rd,c,plate} =$                                      | 956 kN         |
| $F_{rd,blocks,c} =$                                     | 1949 kN        |
| $F_{rd,c} = F_{rd,blk} + F_{rd,footplate} =$            | <b>2905 kN</b> |
| U.C. compression  | 0.49 < 1,00 OK |
| Welds foot plate (see next page)                        | 956 kN         |
| $F_{rd,t} = \min. (\text{welds} / \text{foot plate}) =$ | 765 kN         |
| $F_{rd,blocks,t} =$                                     | 1949 kN        |
| $F_{rd,t} = F_{rd,blk} + F_{rd,footplate} =$            | <b>2714 kN</b> |
| U.C. tension  | 0.41 < 1,00 OK |
| U.C. welds  | 0.81 < 1,00 OK |

#### Capacity shear blocks pile

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 22500 mm <sup>2</sup>  |
| $A_{f2} =$                                     | 67500 mm <sup>2</sup>  |
| $C_A = \sqrt{A_{f2}/A_{f1}} =$                 | 1.73 -                 |
| $f_{jd} = k_d \times f_{cd} =$                 | 27.7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | <b>3741 kN</b>         |
| U.C. compression                               | 0.38 < 1,00 OK         |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | <b>3741 kN</b>         |
| U.C. tension                                   | 0.30 < 1,00 OK         |
| U.C. welds                                     | 0.49 < 1,00 OK         |

#### "Splitting" of pile

|                       |            |                       |
|-----------------------|------------|-----------------------|
| Spread of forces      |            | 45 °                  |
| Length force flow     |            | 1206 mm               |
| Splitting force       |            | 463 kN/m              |
| Yield strength wall   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Capacity tubular pile |            | 7100 kN/m             |
| U.C.                  |            | 0.07 < 1,00 OK        |

Project: ZW380-Oost  
Mast: HB+0 (68&78)

### Welds of shear blocks of main leg

Out-of-plane loading

#### Plate

t = 30 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

#### Member forces

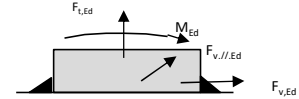
Factor 1.2  
F<sub>t,Ed</sub> = 0 kN  
F<sub>v,Ed</sub> = F<sub>rd,c</sub> / n = 213 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 3.19 kNm

#### Check

σ<sub>w,Ed</sub> = 355 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 177 N/mm<sup>2</sup> ≤

#### Welds

a = 4 mm  
l = 200 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



#### Stress components

σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 4al = 0 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 4al = 94 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 4al = 94 N/mm<sup>2</sup>  
b\* = b + 2/3av<sup>2</sup> = 33.8 mm  
σ<sub>1</sub> = τ<sub>1</sub> = 0,706M<sub>Ed</sub> / al b\* = 83 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>w,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 355 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.81 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.50 OK

### Welds of shear blocks of pile

Out-of-plane loading

#### Plate

t = 30 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

#### Member forces

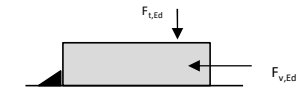
Factor 1.2  
F<sub>t,Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 374 kN  
F<sub>v,Ed</sub> = 748 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 0.00 kNm

#### Check

σ<sub>w,Ed</sub> = 212 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 106 N/mm<sup>2</sup> ≤

#### Welds

a = 5 mm  
l = 750 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



#### Stress components

σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 2al = 35 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 2al = 71 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 2al = 106 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>w,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 212 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.49 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.30 OK

### Welds of foot plate

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup>  
Weld size a = 5 mm  
Length l = 2b + 2b - t = 760 mm  
Capacity F<sub>Rd</sub> = a x l x f<sub>w,d</sub> / √3 = 956 kN



Project: ZW380-Oost  
 Mast: HS+0 (26)

**Shear blocks**

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-05-26

Auteur: TBR

Versie: 1.4

| Load        |            |        | Results     |      |                |
|-------------|------------|--------|-------------|------|----------------|
| Compression | $F_{Ed,c}$ | 730 kN | Compression | U.C. | 0.69 < 1,00 OK |
| Tension     | $F_{Ed,t}$ | 555 kN | Tension     | U.C. | 0.69 < 1,00 OK |

**Main leg**

|                    |          |                      |
|--------------------|----------|----------------------|
| Profile            |          | <b>L150.12</b>       |
| Steel material     |          | S355                 |
| Cross section      |          | 3480 mm <sup>2</sup> |
| Axial capacity     | $N_{pl}$ | 1235 kN              |
| Width              | b        | 150 mm               |
| Thickness          | t        | 12 mm                |
| Length in concrete |          | 1400 mm              |

**Shear blocks main leg**

|                    |       |        |
|--------------------|-------|--------|
| Width              | b     | 30 mm  |
| Thickness          | h     | 30 mm  |
| Length             | L     | 130 mm |
| Welds              | a     | 4 mm   |
| c.t.c. separation  | s     | 150 mm |
| Number for compr.  | $n_c$ | 18 -   |
| Number for tension | $n_t$ | 18 -   |

**Foot plate**

|             |   |       |
|-------------|---|-------|
| Thickness   | t | 30 mm |
| Ext. length | m | 30 mm |
| Welds       | a | 5 mm  |

**Pile**

|                   |  |                       |
|-------------------|--|-----------------------|
| Name              |  | Buispaal              |
| Diameter          |  | 609 mm                |
| Thickness         |  | 10 mm                 |
| Cross section     |  | 18818 mm <sup>2</sup> |
| Steel material    |  | S355                  |
| Capacity          |  | 6680 kN               |
| Concrete strength |  | C30/37                |

**Shear blocks pile**

|                    |       |        |
|--------------------|-------|--------|
| Width              | b     | 30 mm  |
| Thickness          | h     | 30 mm  |
| Length             | L     | 450 mm |
| Welds              | a     | 5 mm   |
| c.t.c. separation  | s     | 300 mm |
| Number for compr.  | $n_c$ | 5 -    |
| Number for tension | $n_t$ | 5 -    |

**Design value concrete strength**

|                  |            |                        |
|------------------|------------|------------------------|
| Material factor  | $\gamma_c$ | 1.5                    |
| Add. mat. factor | $\gamma_m$ | 1.25 -                 |
| $f_{cd} =$       |            | 16.0 N/mm <sup>2</sup> |

**Steel tower stub**

|                  |            |                       |
|------------------|------------|-----------------------|
| Yield strength   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Tensile strength | $f_{ud} =$ | 490 N/mm <sup>2</sup> |

**Capacity shear blocks main leg**

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 3900 mm <sup>2</sup>   |
| $A_{f2} =$                                     | 9612 mm <sup>2</sup>   |
| Slope  | 1: 5                   |
| $C_A = \sqrt{(A_{f2}/A_{f1})} =$               | 1.57                   |
| $f_{jd} = C_A \times f_{cd} =$                 | 25.1 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | 1763 kN                |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | 1763 kN                |

**Capacity foot plate**

|   |                        |
|---|------------------------|
| $k_d =$                                 | 1.73 -                 |
| $f_{jd} = C_A \times f_{cd} =$          | 27.7 N/mm <sup>2</sup> |
| $c = t\sqrt{(f_{yd} / 3f_{jd})} =$      | 65 mm                  |
| $m^* = \min(c, m) =$                    | 30 mm                  |
| Type foot plate                         | Extending              |
| Effective for                           | Compr. and tension     |
| $A_{p,c} =$                             | 25080 mm <sup>2</sup>  |
| $F_{Rd,c} = A_{p,druk} \times f_{jd} =$ | 695 kN                 |
| $A_{p,t} =$                             | 21600 mm <sup>2</sup>  |
| $F_{Rd,t} = A_{p,t} \times f_{jd} =$    | 599 kN                 |

**Capacities**

|   |                |
|---|----------------|
| $F_{rd,c,plate} =$                                      | 695 kN         |
| $F_{rd,blocks,c} =$                                     | 1763 kN        |
| $F_{rd,c} = F_{rd,blk} + F_{rd,footplate} =$            | <b>2458 kN</b> |
| U.C. compression  | 0.30 < 1,00 OK |
| Welds foot plate (see next page)                        | 724 kN         |
| $F_{rd,t} = \min. (\text{welds} / \text{foot plate}) =$ | 599 kN         |
| $F_{rd,blocks,t} =$                                     | 1763 kN        |
| $F_{rd,t} = F_{rd,blk} + F_{rd,footplate} =$            | <b>2362 kN</b> |
| U.C. tension  | 0.23 < 1,00 OK |
| U.C. welds  | 0.69 < 1,00 OK |

**Capacity shear blocks pile**

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 13500 mm <sup>2</sup>  |
| $A_{f2} =$                                     | 40500 mm <sup>2</sup>  |
| $C_A = \sqrt{(A_{f2}/A_{f1})} =$               | 1.73 -                 |
| $f_{jd} = k_d \times f_{cd} =$                 | 27.7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | <b>1871 kN</b>         |
| U.C. compression                               | 0.39 < 1,00 OK         |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | <b>1871 kN</b>         |
| U.C. tension                                   | 0.30 < 1,00 OK         |
| U.C. welds                                     | 0.49 < 1,00 OK         |

**"Splitting" of pile**

|                       |            |                       |
|-----------------------|------------|-----------------------|
| Spread of forces      | $f_{yd} =$ | 45 °                  |
| Length force flow     |            | 1106 mm               |
| Splitting force       |            | 251 kN/m              |
| Yield strength wall   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Capacity tubular pile |            | 7100 kN/m             |
| U.C.                  |            | 0.04 < 1,00 OK        |

Project: ZW380-Oost  
Mast: HS+0 (26)

### Welds of shear blocks of main leg

Out-of-plane loading

#### Plate

t = 30 mm  
Grade S355  
 $f_{yd} = 355 \text{ N/mm}^2$   
 $f_u = 490 \text{ N/mm}^2$

#### Member forces

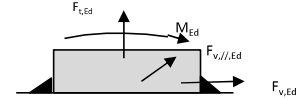
Factor 1.2  
 $F_{t,Ed} = 0 \text{ kN}$   
 $F_{v,Ed} = F_{rd,c} / n = 118 \text{ kN}$   
 $F_{v//,Ed} = 0 \text{ kN}$   
 $M_{Ed} = 1/2 b / h \times F_{v,Ed} = 1.76 \text{ kNm}$

#### Check

$\sigma_{w,Ed} = 302 \text{ N/mm}^2 \leq$   
 $\sigma_1 = 151 \text{ N/mm}^2 \leq$

#### Welds

a = 4 mm  
l = 130 mm  
 $\beta_w = 0.9 -$   
 $\gamma_{M2} = 1.25 -$



#### Stress components

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 4al = 0 \text{ N/mm}^2$   
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 4al = 80 \text{ N/mm}^2$   


---

80 N/mm<sup>2</sup>  
b\* = b + 2/3av<sup>2</sup> = 33.8 mm  
 $\sigma_1 = \tau_1 = 0.706M_{Ed} / al b^* = 71 \text{ N/mm}^2$   
 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$   
 $\sigma_{w,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 302 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$  U.C. = **0.69 OK**  
 $0.9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$  U.C. = **0.43 OK**

### Welds of shear blocks of pile

Out-of-plane loading

#### Plate

t = 30 mm  
Grade S355  
 $f_{yd} = 355 \text{ N/mm}^2$   
 $f_u = 490 \text{ N/mm}^2$

#### Member forces

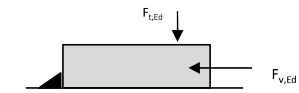
Factor 1.2  
 $F_{t,Ed} = 1/2 b / h \times F_{v,Ed} = 224 \text{ kN}$   
 $F_{v,Ed} = 449 \text{ kN}$   
 $F_{v//,Ed} = 0 \text{ kN}$   
 $M_{Ed} = 0.00 \text{ kNm}$

#### Check

$\sigma_{w,Ed} = 212 \text{ N/mm}^2 \leq$   
 $\sigma_1 = 106 \text{ N/mm}^2 \leq$

#### Welds

a = 5 mm  
l = 450 mm  
 $\beta_w = 0.9 -$   
 $\gamma_{M2} = 1.25 -$



#### Stress components

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 2al = 35 \text{ N/mm}^2$   
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 2al = 71 \text{ N/mm}^2$   


---

106 N/mm<sup>2</sup>  
 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$   
 $\sigma_{w,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 212 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$  U.C. = **0.49 OK**  
 $0.9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$  U.C. = **0.30 OK**

### Welds of foot plate

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$   
Weld size a = 5 mm  
Length l = 2b + 2b - t = 576 mm  
Capacity  $F_{Rd} = a \times l \times f_{w,d} / \sqrt{3} = 724 \text{ kN}$

Project: ZW380-Oost  
 Mast: HC+0 (16)

**Shear blocks**

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-05-25

Auteur: TBR

Versie: 1.4

| Load        |            | Results |                     |
|-------------|------------|---------|---------------------|
| Compression | $F_{Ed,c}$ | 1522 kN | U.C. 0.82 < 1,00 OK |
| Tension     | $F_{Ed,t}$ | 1204 kN | U.C. 0.82 < 1,00 OK |

**Main leg**

|                    |          |                      |
|--------------------|----------|----------------------|
| Profile            |          | <b>L200.24</b>       |
| Steel material     |          | S355                 |
| Cross section      |          | 9059 mm <sup>2</sup> |
| Axial capacity     | $N_{pl}$ | 3216 kN              |
| Width              | b        | 200 mm               |
| Thickness          | t        | 24 mm                |
| Length in concrete |          | 1500 mm              |

**Capacity shear blocks main leg**

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 6675 mm <sup>2</sup>   |
| $A_{f2} =$                                     | 18592 mm <sup>2</sup>  |
| Slope  | 1: 5                   |
| $C_A = \sqrt{(A_{f2}/A_{f1})} =$               | 1.67                   |
| $f_{jd} = C_A \times f_{cd} =$                 | 26.7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | 2139 kN                |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | 2139 kN                |

**Shear blocks main leg**

|                    |       |          |
|--------------------|-------|----------|
| Width              | b     | 30 mm    |
| Thickness          | h     | 30 mm    |
| Length             | L     | 222.5 mm |
| Welds              | a     | 4 mm     |
| c.t.c. separation  | s     | 200 mm   |
| Number for compr.  | $n_c$ | 12 -     |
| Number for tension | $n_t$ | 12 -     |

**Capacity foot plate**

|   |                        |
|---|------------------------|
| $k_d =$                                 | 1.73 -                 |
| $f_{jd} = C_A \times f_{cd} =$          | 27.7 N/mm <sup>2</sup> |
| $c = t\sqrt{(f_{yd} / 3f_{jd})} =$      | 63 mm                  |
| $m^* = \min(c, m) =$                    | 30 mm                  |
| Type foot plate                         | Extending              |
| Effective for                           | Compr. and tension     |
| $A_{p,c} =$                             | 36659 mm <sup>2</sup>  |
| $F_{Rd,c} = A_{p,druk} \times f_{jd} =$ | 1016 kN                |
| $A_{p,t} =$                             | 27600 mm <sup>2</sup>  |
| $F_{Rd,t} = A_{p,t} \times f_{jd} =$    | 765 kN                 |

**Foot plate**

|             |   |       |
|-------------|---|-------|
| Thickness   | t | 30 mm |
| Ext. length | m | 30 mm |
| Welds       | a | 5 mm  |

**Pile**

|                   |  |                       |
|-------------------|--|-----------------------|
| Name              |  | Buispaal              |
| Diameter          |  | 609 mm                |
| Thickness         |  | 10 mm                 |
| Cross section     |  | 18818 mm <sup>2</sup> |
| Steel material    |  | S355                  |
| Capacity          |  | 6680 kN               |
| Concrete strength |  | C30/37                |

**Capacities**

|   |                |
|---|----------------|
| $F_{rd,c,plate} =$                                      | 946 kN         |
| $F_{rd,blocks,c} =$                                     | 2139 kN        |
| $F_{rd,c} = F_{rd,blk} + F_{rd,footplate} =$            | <b>3084 kN</b> |
| U.C. compression  | 0.49 < 1,00 OK |
| Welds foot plate (see next page)                        | 946 kN         |
| $F_{rd,t} = \min. (\text{welds} / \text{foot plate}) =$ | 765 kN         |
| $F_{rd,blocks,t} =$                                     | 2139 kN        |
| $F_{rd,t} = F_{rd,blk} + F_{rd,footplate} =$            | <b>2904 kN</b> |
| U.C. tension  | 0.41 < 1,00 OK |
| U.C. welds  | 0.82 < 1,00 OK |

**Shear blocks pile**

|                    |       |        |
|--------------------|-------|--------|
| Width              | b     | 30 mm  |
| Thickness          | h     | 30 mm  |
| Length             | L     | 750 mm |
| Welds              | a     | 5 mm   |
| c.t.c. separation  | s     | 300 mm |
| Number for compr.  | $n_c$ | 6 -    |
| Number for tension | $n_t$ | 6 -    |

**Capacity shear blocks pile**

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 22500 mm <sup>2</sup>  |
| $A_{f2} =$                                     | 67500 mm <sup>2</sup>  |
| $C_A = \sqrt{(A_{f2}/A_{f1})} =$               | 1.73 -                 |
| $f_{jd} = k_d \times f_{cd} =$                 | 27.7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | <b>3741 kN</b>         |
| U.C. compression                               | 0.41 < 1,00 OK         |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | <b>3741 kN</b>         |
| U.C. tension                                   | 0.32 < 1,00 OK         |
| U.C. welds                                     | 0.49 < 1,00 OK         |

**Design value concrete strength**

|                  |            |                        |
|------------------|------------|------------------------|
| Material factor  | $\gamma_c$ | 1.5                    |
| Add. mat. factor | $\gamma_m$ | 1.25 -                 |
| $f_{cd} =$       |            | 16.0 N/mm <sup>2</sup> |

**Steel tower stub**

|                  |            |                       |
|------------------|------------|-----------------------|
| Yield strength   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Tensile strength | $f_{ud} =$ | 490 N/mm <sup>2</sup> |

**"Splitting" of pile**

|                       |            |                       |
|-----------------------|------------|-----------------------|
| Spread of forces      |            | 45 °                  |
| Length force flow     |            | 1206 mm               |
| Splitting force       |            | 499 kN/m              |
| Yield strength wall   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Capacity tubular pile |            | 7100 kN/m             |
| U.C.                  |            | 0.07 < 1,00 OK        |

Project: ZW380-Oost  
 Mast: HC+0 (16)

### Welds of shear blocks of main leg

Out-of-plane loading

#### Plate

t = 30 mm  
 Grade S355  
 $f_{yd} = 355 \text{ N/mm}^2$   
 $f_u = 490 \text{ N/mm}^2$

#### Member forces

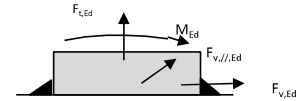
Factor 1.2  
 $F_{t,Ed} = 0 \text{ kN}$   
 $F_{v,Ed} = F_{rd,c} / n = 214 \text{ kN}$   
 $F_{v//,Ed} = 0 \text{ kN}$   
 $M_{Ed} = 1/2 b / h \times F_{v,Ed} = 3.21 \text{ kNm}$

#### Check

$\sigma_{w,Ed} = 357 \text{ N/mm}^2 \leq$   
 $\sigma_1 = 178 \text{ N/mm}^2 \leq$

#### Welds

a = 4 mm  
 l = 200 mm  
 $\beta_w = 0.9 -$   
 $\gamma_{M2} = 1.25 -$



#### Stress components

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 4al = 0 \text{ N/mm}^2$   
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 4al = 95 \text{ N/mm}^2$   


---

 $95 \text{ N/mm}^2$   
 $b^* = b + 2/3av^2 = 33.8 \text{ mm}$   
 $\sigma_1 = \tau_1 = 0.706M_{Ed} / al b^* = 84 \text{ N/mm}^2$   
 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$   
 $\sigma_{w,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 357 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$  U.C. = **0.82 OK**  
 $0.9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$  U.C. = **0.51 OK**

### Welds of shear blocks of pile

Out-of-plane loading

#### Plate

t = 30 mm  
 Grade S355  
 $f_{yd} = 355 \text{ N/mm}^2$   
 $f_u = 490 \text{ N/mm}^2$

#### Member forces

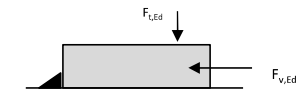
Factor 1.2  
 $F_{t,Ed} = 1/2 b / h \times F_{v,Ed} = 374 \text{ kN}$   
 $F_{v,Ed} = 748 \text{ kN}$   
 $F_{v//,Ed} = 0 \text{ kN}$   
 $M_{Ed} = 0.00 \text{ kNm}$

#### Check

$\sigma_{w,Ed} = 212 \text{ N/mm}^2 \leq$   
 $\sigma_1 = 106 \text{ N/mm}^2 \leq$

#### Welds

a = 5 mm  
 l = 750 mm  
 $\beta_w = 0.9 -$   
 $\gamma_{M2} = 1.25 -$



#### Stress components

$\sigma_1 = \tau_1 = F_{t,Ed} \sqrt{2} / 2al = 35 \text{ N/mm}^2$   
 $\sigma_1 = \tau_1 = F_{v,Ed} \sqrt{2} / 2al = 71 \text{ N/mm}^2$   


---

 $106 \text{ N/mm}^2$   
 $\tau_{//} = F_{v//,Ed} / 2al = 0 \text{ N/mm}^2$   
 $\sigma_{w,Ed} = \sqrt{(\sigma_1^2 + 3\tau_1^2 + 3\tau_{//}^2)} = 212 \text{ N/mm}^2$

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$  U.C. = **0.49 OK**  
 $0.9f_u / \gamma_{M2} = 353 \text{ N/mm}^2$  U.C. = **0.30 OK**

### Welds of foot plate

$f_u / \beta_w \gamma_{M2} = 436 \text{ N/mm}^2$   
 Weld size a = 5 mm  
 Length l = 2b + 2b - t = 752 mm  
 Capacity  $F_{Rd} = a \times l \times f_{w,d} / \sqrt{3} = 946 \text{ kN}$



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## B.12 Mastrapportage steunmasten reconstructie



ZUID-WEST 380 KV OOST VERBINDINGEN

# Mastrapportage GT-RLL S+32/n

TenneT TSO B.V.

**Meridian doc.nr.:** 002.678.00 0934575

**Rapport nr.:** 21-0890, Rev. 0

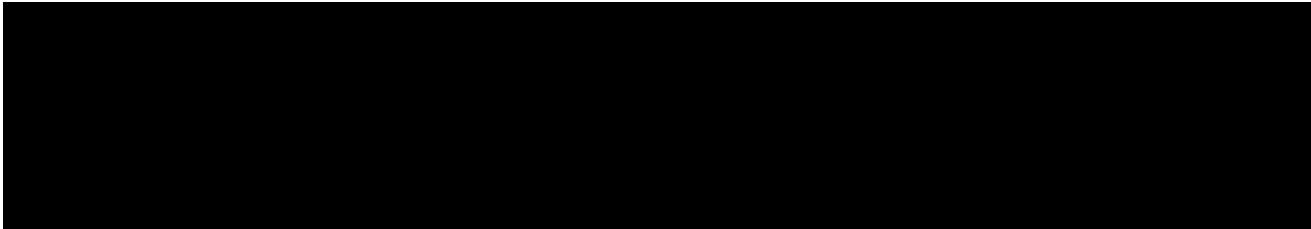
**Datum:** 2021-07-16





Projectnaam: Zuid-West 380 kV Oost Verbindingen  
Rapport titel: Mastrapportage GT-RLL S+32/n  
Klant: TenneT TSO B.V.,  
Contactpersoon klant: [REDACTED]  
Datum uitgave: 2021-07-16  
Project nr.: 10124719  
Organisatie unit: TDT  
Meridian doc.nr.: 002.678.00 0934575  
Rapport nr.: 21-0890, Rev. 0

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## 1 INLEIDING

In het basisontwerp van de vakwerkmasten voor de verbinding GT-RLL380 in het project Zuid-West 380 kV-Oost zijn voor het vaststellen van de haalbaarheid constructieve berekeningen uitgevoerd aan de masten en fundaties. In de Definitief Ontwerpfase, moeten berekeningen verder worden uitgewerkt om te kunnen dienen voor de benodigde vergunningsdocumentatie, voor de aanbesteding en als voorbereiding voor de uitvoeringsfase. Het DO omvat het ontwerp van de mastconstructies, de fundaties en de opstijpunten in de verbinding.

Deze rapportage bevat de resultaten van de toetsing van masttype S+32/n voor de reconstructie. Deze mast is gebaseerd op het bestaande S+24 masttype uit de verbinding GT-RLL380 met de aanpassingen om te voldoen aan de belasting uit de nieuwe situatie en de huidige ontwerpeisen van TenneT.

In deze rapportage is de toetsing van de mast van de steunmast S+32/n opgenomen. De toetsing bestaat uit controle van:

- de profielen en boutverbindingen onderdeel van de hoofddraagconstructie;
- de knikverkorters;
- de verbinding met de fundatie via blokdeuvels;
- de liggers voor de isolatorkettingen.

Buiten de scope van dit DO-rapport valt de controle van de schetsplaten en overige verbindingdetails in de constructie. Dit moet in de UO-fase worden uitgewerkt. Ook de voorzieningen voor de bordessen vallen onder uitwerking in UO-fase.

In hoofdstuk 2 zijn de uitgangspunten en randvoorwaarden vanuit de van toepassing zijnde normen en TenneT-specificaties opgenomen. Hoofdstuk 3 beschrijft de gevolgde aanpak van de berekening. In hoofdstuk 4 is de toetsing opgenomen.

## 2 UITGANGSPUNTEN EN RANDVOORWAARDEN

### 2.1 Normen

Er is gebruik gemaakt van de normen volgens Tabel 1.

**Tabel 1 Gebruikgemaakte normen, voorschriften en richtlijnen**

| Norm                                       | Titel  |
|--|--|
| NEN-EN 50341-1:2013                        | “Overhead electrical lines exceeding AC 1 kV - Part 1: General requirements – Common”                        |
| NEN-EN 50341-2-15:2019                     | “Overhead electrical lines exceeding AC 1 kV Part 2 National Normative Aspects (NNA) for THE NETHERLANDS”    |
| NEN-EN 1990+A1+A1/C2:2019/NB:2019nl        | “Grondslagen van het ontwerp”  |
| NEN-EN 1991-1-4+A1+C2:2011/NB:2019+C1:2020 | “Deel 1-4: Windbelasting op constructies”  |
| NEN-EN 1992-1-1+C2:2011/NB:2016+A1:2020    | “Eurocode 2: Ontwerp en berekening van betonconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-1-1+C2+A1:2016 nl              | “Eurocode 3: Ontwerp en berekening van staalconstructies, deel 1-1: algemene regels en regels voor gebouwen” |
| NEN-EN 1993-3-1:2007/NB:2011 nl            | “Deel 3-1: Torens, masten en schoorstenen - Torens en masten”  |
| NEN-EN 1993-1-8+C2:2011/NB:2011 nl         | “Ontwerp en berekening van staalconstructies, deel 1-8: ontwerp en berekening van verbindingen”              |

### 2.2 TenneT-specificaties

In Tabel 2 zijn de documenten opgenomen die relevant zijn voor de berekeningen en toetsingen die binnen dit project in de mastrapportage uitgevoerd zullen worden.

**Tabel 2 Relevante documenten t.b.v. mechanische rapportages**

| Nummer          | Onderwerp                           |
|-----------------|-------------------------------------|
| PVE.05.000 v3.2 | PvE Lijnen                          |
| sPVE.05.001     | sPvE Lijnen                         |
| SPE.05.346 v1.3 | Algemene specificatie stalen masten |

### 2.3 Eisenverificatie

Voor de eisenverificatie wordt verwezen naar het rapport “Verificatierapport eisen reconstructies”.

### 2.4 Ontwerprapporten

Voor de achtergrond van het ontwerp wordt verwezen naar het uitgangspuntenrapport “D1.3 Uitgangspunten reconstructies”, DNV GL rapport 21-0702, Meridiannummer 002.678.00 0927721.

### 2.5 Materialen

Voor het ontwerp van de mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 3.

**Tabel 3 Materialen aangepaste constructie**

|                |   |
|----------------|---|
| Staalsoort     | S355J0 (t≤16 mm)<br>S355J2 (16<t≤40 mm) |
| Boutkwaliteit  | 8.8 gerolde draad                       |
| Betonkwaliteit | C30/37                                  |
| Wapeningsstaal | B500                                    |



Voor de constructie geldt conform TenneT-specificatie:

- Toe te passen bouten: M16/M20/M24;
- Voor hoekstaal is de minimale afmeting L50x5 mm;
- Minimale plaatdikte 6 mm.

Mocht het noodzakelijk zijn M30 toe te passen, bij grote plaatdiktes is dit als afwijking door TenneT toegestaan.

## 2.6 Software

De gebruikte software wordt benoemd in Tabel 4.

**Tabel 4 Toegepaste software**

| Software              |           | Versie |
|-----------------------|-----------|--------|
| Mastontwerp           | PLS-CADD  | 16.65  |
| Mastberekeningen      | PLS-TOWER | 16.65  |
| Constructieve analyse | AxisVM    | X5 R4h |

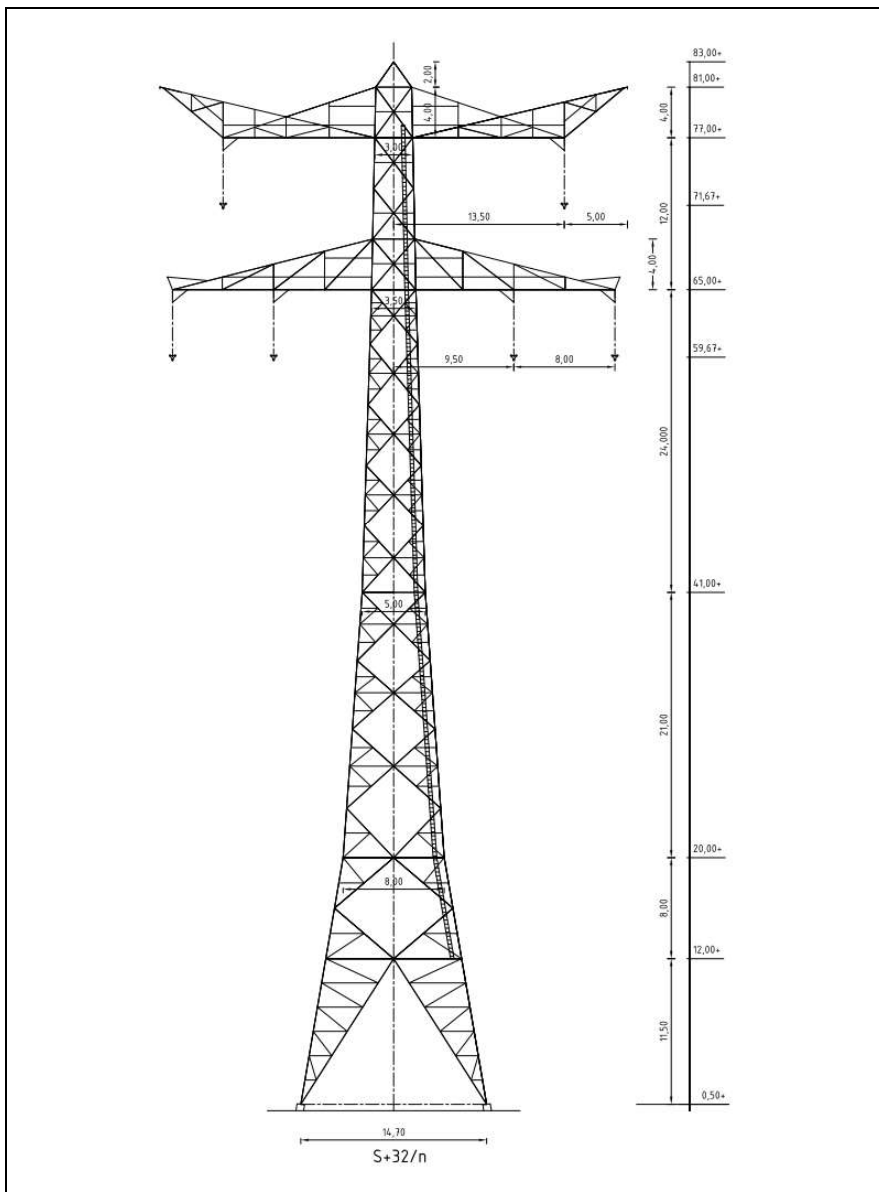
### 3 MASTONTWERP

#### 3.1 Mastbeelden

In dit hoofdstuk worden het mastbeeld weergegeven met de belangrijkste maatvoering, voor volledige tekeningen van het masttype wordt verwezen naar onderstaande tekeningen:

- Mastbeeldtekening nieuwbouwmasten GT-RLL, Meridiannummer 002.678.00 0928568
- Overzichtstekening S+32/n, Meridiannummer 002.678.00 0934592
- Principedetails GT-RLL, Meridiannummer 002.678.00 0935108

Masttype reconstructie S+32/n is een steunmast voor twee circuits 380 kV.



**Figuur 1 Mastbeeld masttype S+32/n**

### 3.2 Uitgangspunten berekening

De uitgangspunten volgens Tabel 5 zijn van toepassing.

**Tabel 5 Uitgangspunten**

|                             |                       |
|-----------------------------|-----------------------|
| Norm                        | NEN-EN50341-2-15:2019 |
| Gevolgklasse initieel       | CC2                   |
| Betrouwbaarheidsniveau      | Nieuwbouw             |
| Referentieperiode           | 50 jaar               |
| Windgebied                  | III                   |
| Windsnelheid (m/s)          | 24,5                  |
| Terreincategorie            | II                    |
| Reductiefactor $c_{dir}$    | 1,00                  |
| IJsg gebied fasegeleider    | B                     |
| IJsg gebied bliksemgeleider | A                     |

### 3.3 Mastenlijst

In Tabel 6 zijn alle masten in het tracé van het type S+32/n opgenomen. De mast met grootste wind span is vetgedrukt aangegeven. Het masttype zal niet met deze wind en weight span worden berekend maar met generieke wind en weight span, zie uitgangspuntenrapport.

**Tabel 6 Mastenlijst S+32/n**

| Mast-nummer | Masttype | Lijnhoek (°) | Wind span (m) | Weight span (m) | Hoogteverschil ba+ah (m) | Hoogteverschil back (m) | Hoogteverschil ahead (m) |
|-------------|----------|--------------|---------------|-----------------|--------------------------|-------------------------|--------------------------|
| <b>72N</b>  | S+32_n   | 180,0        | 397,2         | 511,6           | 32,6                     | 32,5                    | 0,1                      |
| 71N         | S+32_n   | 180,0        | 346,9         | 475,5           | 27,4                     | -0,1                    | 27,5                     |

### 3.4 Geleiderbelastingen

De berekening is uitgevoerd met het geleiderbelastingprogramma van DNV. De belastingen op de mastconstructie zijn bepaald op basis van de modellering in PLS-TOWER (staafoppervlaktes). Voor de toeslagen op eigen gewicht en windoppervlakte wordt verwezen naar het uitgangspuntenrapport. In Appendix A zijn de resultaten van de geleiderbelastingen samengevat.

### 3.5 Reacties op de fundering

De oplegreacties op de fundering worden ontleend aan de uitvoer van het geleiderbelastingenprogramma. Zie Appendix A.

### 3.6 Modelling

Op basis van de ontwerptekeningen is de mast in PLS-TOWER ingevoerd. De toetsing wordt per staafgroep uitgevoerd. De hoofdelementen zijn gemodelleerd, niet-dragende profielen als knikverkorters zijn weggelaten, deze worden separaat getoetst. De profielen zijn in PLS-TOWER inclusief de boutverbindingen ingevoerd en getoetst, de controle van de schetsplaten en andere detailverbindingen valt buiten de scope.

De geleiderbelastingen vanuit het geleiderbelastingenprogramma zijn als invoer voor de belastingen gebruikt.

De gewichts- en windbelasting op de mastconstructie wordt door PLS-TOWER automatisch bepaald. Via toeslagfactoren wordt de invloed van niet gemodelleerde elementen als knikverkorters, bordesconstructies en

Klimvoorzieningen meegenomen. Voor schetsplaten, zinklaag en bouten is een aanvullende toeslag op het gewicht van 15% toeslag gerekend.

Diagonalen in voor- en achtervlak respectievelijk de twee zijvlakken zijn samengenomen in een groep.

### **3.7 Overige controles**

In PLS-TOWER zijn niet alle elementen getoetst. Knikverkorteprofielen en overige profielen voor beloopbaarheid worden separaat getoetst. In Appendix C is dit opgenomen. De verbinding met de fundatie bestaat uit ingestorte profielen voorzien van blokdeuvels. Dit is in Appendix D opgenomen. De liggers van isolatorkettingen worden belast op buiging. Deze zijn hierop onderzocht, dit is in Appendix E opgenomen.

### **3.8 Mastgewicht**

Het totale mastgewicht per masttype is met de uitgangspunten van paragraaf 3.6 bepaald op:

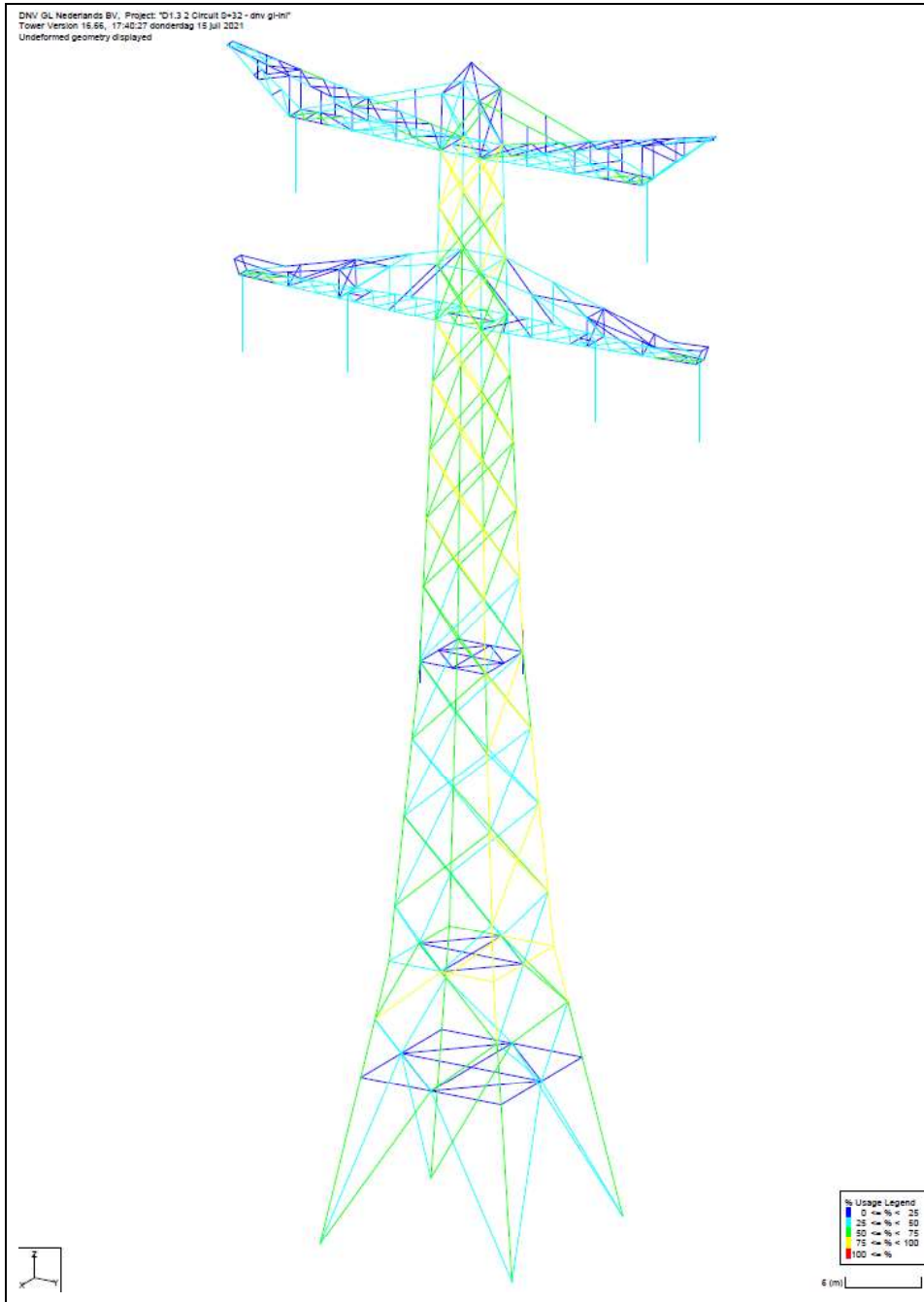
- Masttype S+32/n: 71,7 ton.

## 4 TOETSING

### 4.1 Resultaat PLS-TOWER

Het resultaat van de toetsing met PLS-TOWER is weergegeven in Figuur 2. De belastingen zijn bepaald voor het masttype S+32/n, inclusief bouwfase.

De uitnuttig van de constructie loopt op van blauw (0-25%) tot geel (75-100%). Uit de figuur wordt geconcludeerd dat alle profielen en boutverbindingen voldoen.



**Figuur 2 Resultaat PLS-TOWER voor de steunmast S+32/n**



## 4.2 Toetsing overige onderdelen

In Tabel 7 zijn de resultaten van de uitgevoerde toetsingen weergegeven.

**Tabel 7 Samenvatting uitgevoerde controles**

| Controle van          | Beoordeling | Referentie             |
|-----------------------|-------------|------------------------|
| Profielen             | Voldoen     | Figuur 2<br>Appendix B |
| Knikverkorters        | Voldoen     | Appendix C             |
| Blokdeuvels randstijl | Voldoen     | Appendix D             |
| Liggers               | Voldoet     | Appendix E             |

## APPENDIX A

### Geleiderbelastingen

---

Geleiderbelastingen opgenomen:

- Masttype S+32/n
- Masttype S+32/n bouwfase



Project: GT-RLL380  
 Tower: S+32  
 Number: 72N

Auteur: TBR  
 Versie: v12.0

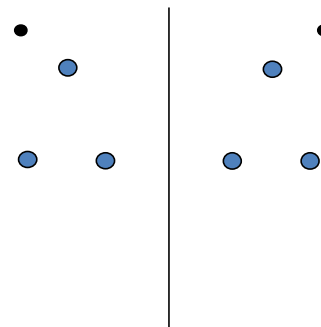
### Geleiderbelastingen

#### Algemeen

Benaming S+32  
 Masttype Steunmast  
 Aantal circuits 2  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 2

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 50 jaar  
 Betrouwbaarheidsniveau na aanpassing 0  
 n.v.t.  
 Windgebied III  
 Windsnelheid (m/s) 24,5  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsg gebied fasegeleider B  
 IJsg gebied bliksemgeleider A



Configuratie geleiders

#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A           | 2 %             | 2 %              | 1600                     |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsg gebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-------------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Circuit 2      | 380 kV   | ACCC-Warsaw            | 3         | B           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A           | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 2 |          | OPGW AFL-226/38        | 1         | A           | 2 %             | 2 %              | 1600                      |

#### Isolatoren (1)

| Omschrijving   | Ophanging           | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------------|--------------|------------|----------------------------|
| Circuit 1      | Halfverankering     | 5,60         | 4,50       | 2,40                       |
| Circuit 2      | Halfverankering     | 5,60         | 4,50       | 2,40                       |
| Bliksemdraad 1 | Vast (Bliksemdraad) | 0,10         | 0,20       | 0,10                       |
| Bliksemdraad 2 | Vast (Bliksemdraad) | 0,10         | 0,20       | 0,10                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 60,0 m       | 64,5 m       | -17,5 m                                |
| Circuit 1      | 11         | 380ct1f2 | 60,0 m       | 64,5 m       | -9,5 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 72,0 m       | 76,5 m       | -13,5 m                                |
| Circuit 2      | 20         | 380ct2f1 | 60,0 m       | 64,5 m       | 9,5 m                                  |
| Circuit 2      | 21         | 380ct2f2 | 60,0 m       | 64,5 m       | 17,5 m                                 |
| Circuit 2      | 22         | 380ct2f3 | 72,0 m       | 76,5 m       | 13,5 m                                 |
| Bliksemdraad 1 | 1          | bl1      | 80,3 m       | 80,5 m       | -18,5 m                                |
| Bliksemdraad 2 | 3          | bl2      | 80,3 m       | 80,5 m       | 18,5 m                                 |

Project: GT-RLL380  
 Tower: S+32  
 Number: 72N

**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead |   |
|------------------------------------|---------------------------|-------|---|
| Verhoging voor windbelasting       | 0,0 m                     | 0,0 m | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -32,0 m                   | 0,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |       |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

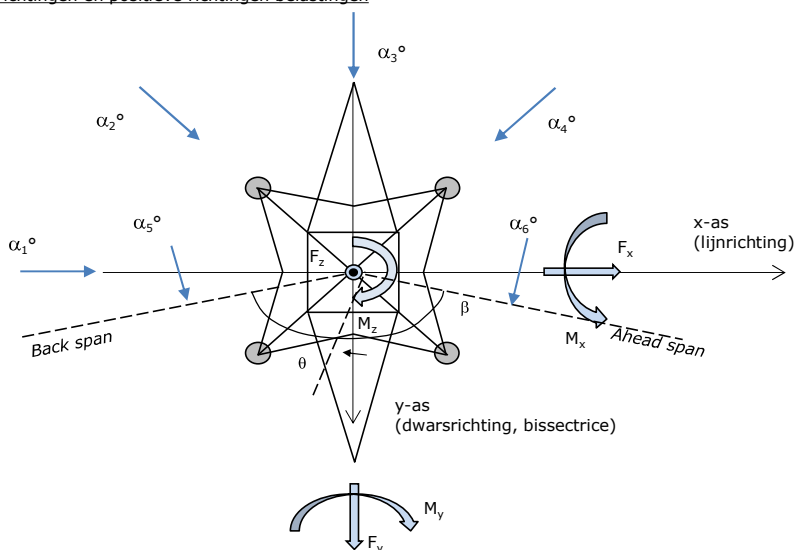
| Circuits       | Aanduiding | Nummer   | Hoogteverschil  |                  | Richtingsverandering |                  |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
|                |            |          | $\Delta h$ back | $\Delta h$ ahead | $\Delta y$ back      | $\Delta y$ ahead |
| Circuit 1      | 10         | 380ct1f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 11         | 380ct1f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 12         | 380ct1f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 20         | 380ct2f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 21         | 380ct2f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 22         | 380ct2f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 1 | 1          | bl1      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 2 | 3          | bl2      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek $\beta$                           | 180 °      |         |
| Rotatie mast t.o.v. bissectrice $\theta$   | 0 °        |         |
| Vaklengte                                  | 800        | 800 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 45 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 135 °   |
|  | $\alpha_5$ | - °     |
|  | $\alpha_6$ | - °     |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



**Beschouwd aantal windrichtingen**

|        |   |
|--------|---|
| 1a     | 4 |
| 3      | 4 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

Project: GT-RLL380  
 Tower: S+32  
 Number: 72N

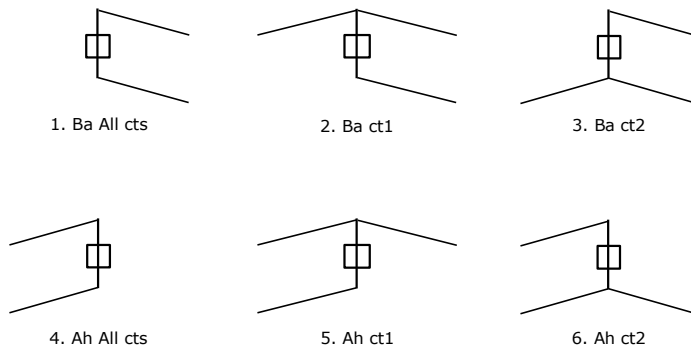
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 0,8                | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 0,8                | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 0,8                | 0    |
| Circuit 2      | 380ct2f1 | 0             | 1    | 1                        | 0    | 0,8                | 0    |
| Circuit 2      | 380ct2f2 | 0             | 1    | 1                        | 0    | 0,8                | 0    |
| Circuit 2      | 380ct2f3 | 0             | 1    | 1                        | 0    | 0,8                | 0    |
| Bliksemdraad 1 | bl1      | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | bl2      | 0             | 1    | 1                        | 0    | 1                  | 0    |

### Belastingsituaties SPLS

Beschouwde situaties SPLS: SPLS voor steunmast niet van toepassing

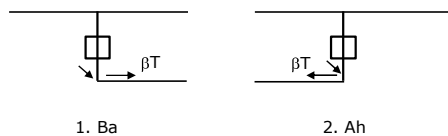
Principe belastingssituaties:



### Belastingsituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



Project: GT-RLL380  
 Tower: S+32  
 Number: 72N

### Belastingsituaties 6. Bouw- en onderhoud

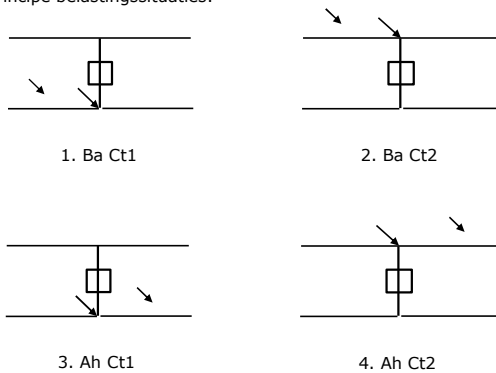
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 en 2, uitgangspunt is symmetrie tussen back / ahead.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



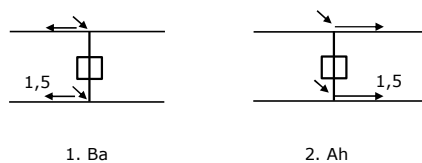
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten  
 Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast  
 Door gebruiker via het belastingsspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

Project: GT-RLL380  
 Tower: S+32  
 Number: 72N

## Mastconstructie

### Eigenschappen

|   |           |         |
|---|-----------|---------|
| Masttype                                    | Steunmast |         |
| Mastbenaming                                | S+32      |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m     |         |
| Masthoogte t.o.v. voetplaat                 | 82,5 m    |         |
| Gewicht mast                                | 703,7 kN  |         |
| <i>Breedte en helling mast bij fundatie</i> |           |         |
|   | x-ri.     | y-ri.   |
| Pootsprei                                   | 14,70     | 14,70 m |
| Helling van de randstijl                    | 0,172     | 0,172 - |
| Factor spatkracht                           | 1,1       | 1,1 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,05                                  |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 19,50    | 14,70                 | 8,00                  | 19,50     | 0,172                 | 221,33                              | 37,50                               | 0,17                                      | 3,07           |
| Eerste tussenstuk | 40,50    | 8,00                  | 5,00                  | 21,00     | 0,071                 | 136,50                              | 26,74                               | 0,20                                      | 2,95           |
| Tweede tussenstuk | 64,50    | 5,00                  | 3,50                  | 24,00     | 0,031                 | 102,00                              | 22,19                               | 0,22                                      | 2,86           |
| Bovenstuk 1       | 72,50    | 3,50                  | 3,17                  | 8,00      | 0,021                 | 26,67                               | 6,27                                | 0,24                                      | 2,78           |
| Bovenstuk 2       | 80,50    | 3,17                  | 2,83                  | 8,00      | 0,021                 | 24,00                               | 5,86                                | 0,24                                      | 2,75           |
| Topstuk           | 82,50    | 2,83                  |                       | 2,00      |                       | 2,83                                | 0,41                                | 0,15                                      | 3,18           |
| Ondertraverse     | 64,50    | 15,75                 |                       | 4,00      |                       | 31,50                               | 8,71                                | 0,28                                      | 2,62           |
| Boventraverse     | 76,50    | 17,00                 |                       | 4,00      |                       | 34,00                               | 9,30                                | 0,27                                      | 2,63           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 19,50    | 14,70                 | 8,00                  | 19,50     | 0,172                 | 221,33                              | 37,50                               | 0,17                                      | 3,07           |
| Eerste tussenstuk | 40,50    | 8,00                  | 5,00                  | 21,00     | 0,071                 | 136,50                              | 26,74                               | 0,20                                      | 2,95           |
| Tweede tussenstuk | 64,50    | 5,00                  | 3,50                  | 24,00     | 0,031                 | 102,00                              | 22,19                               | 0,22                                      | 2,86           |
| Bovenstuk 1       | 72,50    | 3,50                  | 3,17                  | 8,00      | 0,021                 | 26,67                               | 6,27                                | 0,24                                      | 2,78           |
| Bovenstuk 2       | 80,50    | 3,17                  | 2,83                  | 8,00      | 0,021                 | 24,00                               | 5,86                                | 0,24                                      | 2,75           |
| Topstuk           | 82,50    | 2,83                  |                       | 2,00      |                       | 2,83                                | 0,41                                | 0,15                                      | 3,18           |
| Ondertraverse     | 64,50    | 15,75                 |                       | 4,00      |                       | 31,50                               | 8,71                                | 0,28                                      | 2,62           |
| Boventraverse     | 76,50    | 17,00                 |                       | 4,00      |                       | 34,00                               | 9,30                                | 0,27                                      | 2,63           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traverses.



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#### Windoppervlak feeders telecominstallaties

| Onderdeel         | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk         | 0,20                  | 0,71   | 19,5 | 2,8            |
| Eerste tussenstuk | 0,20                  | 0,71   | 21,0 | 3,0            |
| Tweede tussenstuk |                       |        |      |                |
| Bovenstuk 1       |                       |        |      |                |
| Bovenstuk 2       |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>i</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,7                 | 40,5  | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 80,7                    | 68,4                    | 0,0                     | -68,4                   | 9,8                    | 786,4                    | 667,2                    | 0,0                      | -667,2                   |
| Eerste tussenstuk | 0,99                                   | 77,9                    | 66,1                    | 0,0                     | -66,1                   | 30,0                   | 2338,2                   | 1984,0                   | 0,0                      | -1984,0                  |
| Tweede tussenstuk | 1,15                                   | 72,9                    | 61,8                    | 0,0                     | -61,8                   | 52,5                   | 3825,5                   | 3246,0                   | 0,0                      | -3246,0                  |
| Bovenstuk 1       | 1,23                                   | 21,5                    | 18,2                    | 0,0                     | -18,2                   | 68,5                   | 1472,8                   | 1249,7                   | 0,0                      | -1249,7                  |
| Bovenstuk 2       | 1,26                                   | 20,3                    | 17,3                    | 0,0                     | -17,3                   | 76,5                   | 1556,0                   | 1320,3                   | 0,0                      | -1320,3                  |
| Topstuk           | 1,28                                   | 1,7                     | 1,4                     | 0,0                     | -1,4                    | 81,5                   | 137,0                    | 116,3                    | 0,0                      | -116,3                   |
| Ondertraverse     | 1,22                                   | 55,6                    | 33,0                    | 0,0                     | -33,0                   | 65,8                   | 3661,0                   | 2174,5                   | 0,0                      | -2174,5                  |
| Boventraverse     | 1,27                                   | 62,2                    | 36,9                    | 0,0                     | -36,9                   | 77,8                   | 4839,1                   | 2874,3                   | 0,0                      | -2874,3                  |

|               |              |              |            |               |  |                |                |            |                 |
|---------------|--------------|--------------|------------|---------------|--|----------------|----------------|------------|-----------------|
| <b>Totaal</b> | <b>392,8</b> | <b>303,3</b> | <b>0,0</b> | <b>-303,3</b> |  | <b>18615,8</b> | <b>13632,3</b> | <b>0,0</b> | <b>-13632,3</b> |
|---------------|--------------|--------------|------------|---------------|--|----------------|----------------|------------|-----------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 0,0                     | 68,4                    | 80,7                    | 68,4                    | 9,8                    | 0,0                      | 667,2                    | 786,4                    | 667,2                    |
| Eerste tussenstuk | 0,99                                   | 0,0                     | 66,1                    | 77,9                    | 66,1                    | 30,0                   | 0,0                      | 1984,0                   | 2338,2                   | 1984,0                   |
| Tweede tussenstuk | 1,15                                   | 0,0                     | 61,8                    | 72,9                    | 61,8                    | 52,5                   | 0,0                      | 3246,0                   | 3825,5                   | 3246,0                   |
| Bovenstuk 1       | 1,23                                   | 0,0                     | 18,2                    | 21,5                    | 18,2                    | 68,5                   | 0,0                      | 1249,7                   | 1472,8                   | 1249,7                   |
| Bovenstuk 2       | 1,26                                   | 0,0                     | 17,3                    | 20,3                    | 17,3                    | 76,5                   | 0,0                      | 1320,3                   | 1556,0                   | 1320,3                   |
| Topstuk           | 1,28                                   | 0,0                     | 1,4                     | 1,7                     | 1,4                     | 81,5                   | 0,0                      | 116,3                    | 137,0                    | 116,3                    |
| Ondertraverse     | 1,22                                   | 0,0                     | 33,0                    | 22,2                    | 33,0                    | 65,8                   | 0,0                      | 2174,5                   | 1464,4                   | 2174,5                   |
| Boventraverse     | 1,27                                   | 0,0                     | 36,9                    | 24,9                    | 36,9                    | 77,8                   | 0,0                      | 2874,3                   | 1935,6                   | 2874,3                   |

|               |            |              |              |              |  |            |                |                |                |
|---------------|------------|--------------|--------------|--------------|--|------------|----------------|----------------|----------------|
| <b>Totaal</b> | <b>0,0</b> | <b>303,3</b> | <b>322,1</b> | <b>303,3</b> |  | <b>0,0</b> | <b>13632,3</b> | <b>13515,8</b> | <b>13632,3</b> |
|---------------|------------|--------------|--------------|--------------|--|------------|----------------|----------------|----------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting     | 0                      | 0                      | 704                    | 0                       | 0                       | 0                       |
| Windrichting 0°          | 400                    | 0                      | 0                      | 0                       | 19869                   | 0                       |
| Windrichting 45°         | 309                    | 309                    | 0                      | 14542                   | 14542                   | 0                       |
| Windrichting 90°         | 0                      | 330                    | 0                      | 14514                   | 0                       | 0                       |
| Windrichting 135°        | -309                   | 309                    | 0                      | 14542                   | -14542                  | 0                       |

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### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | OPGW AFL-226/38        | 21,7             | 264,0                   | 9,13       | 72000                     | 1,98E-05          |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 1             | 2              | 9,3                | A         | 15+0,4d | 23,7                 | 23,7                        |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 62,75             | 1,20                             | 1,2               | 3,47                |
| 380ct1f2 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 62,75             | 1,20                             | 1,2               | 3,47                |
| 380ct1f3 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 74,75             | 1,26                             | 1,2               | 3,62                |
| 380ct2f1 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 62,75             | 1,20                             | 1,2               | 3,47                |
| 380ct2f2 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 62,75             | 1,20                             | 1,2               | 3,47                |
| 380ct2f3 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 74,75             | 1,26                             | 1,2               | 3,62                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 80,90             | 1,28                             | 1,2               | 0,15                |
| bl2      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 80,90             | 1,28                             | 1,2               | 0,15                |

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#### Windbelasting back

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f2 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f3 | 64,2   | 1,21                 | 0,64           | 0,64          | 1,04  | 28,25         | 67,9  | 67,9        | 46,9              | 130,2       | 130,2           |
| 380ct2f1 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct2f2 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct2f3 | 64,2   | 1,21                 | 0,64           | 0,64          | 1,04  | 28,25         | 67,9  | 67,9        | 46,9              | 130,2       | 130,2           |
| bl1      | 72,5   | 1,25                 | 0,65           | 0,65          | 1,16  | 22,24         | 20,8  | 20,8        | 63,1              | 61,0        | 61,0            |
| bl2      | 72,5   | 1,25                 | 0,65           | 0,65          | 1,17  | 22,13         | 20,8  | 20,8        | 63,0              | 61,0        | 61,0            |

#### Windbelasting ahead

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f2 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f3 | 64,2   | 1,21                 | 0,64           | 0,64          | 1,04  | 28,25         | 67,9  | 67,9        | 46,9              | 130,2       | 130,2           |
| 380ct2f1 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct2f2 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct2f3 | 64,2   | 1,21                 | 0,64           | 0,64          | 1,04  | 28,25         | 67,9  | 67,9        | 46,9              | 130,2       | 130,2           |
| bl1      | 72,5   | 1,25                 | 0,65           | 0,65          | 1,16  | 22,24         | 20,8  | 20,8        | 63,1              | 61,0        | 61,0            |
| bl2      | 72,5   | 1,25                 | 0,65           | 0,65          | 1,17  | 22,13         | 20,8  | 20,8        | 63,0              | 61,0        | 61,0            |

NB: belastingen  $w_v$  gelden voor bundel

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 Masttype: S+32  
 Mast: 72N

Auteur: TBR  
 Versie: v12.0

**Geleiderbelastingen**

**Uitgangspunten**

Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 50 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |                            |                                | $\gamma_Q$ |          |          | $\gamma_a$ |
|--|---------------------------|------------------------------|----------------------------|--------------------------------|------------|----------|----------|------------|
| Belastingsgeval  | omschrijving              | Temp °C                      | $\gamma_G$<br>$G_{k,mast}$ | $\gamma_G$<br>$G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$      |
| ULS 1a   | Wind                      | 10°                          | 1,20                       | 1,20                           | 0,00       | 1,50     | 0,00     | 0,0        |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90                       | 1,20                           | 0,00       | 1,50     | 0,00     | 0,0        |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90                       | 0,90                           | 0,00       | 1,50     | 0,00     | 0,0        |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20                       | 1,20                           | 0,00       | 0,45     | 1,50     | 0,0        |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90                       | 1,20                           | 0,00       | 0,45     | 1,50     | 0,0        |
| ULS 4  | Koude+wind                | -20°                         | 1,20                       | 1,20                           | 0,00       | 0,30     | 0,00     | 0,0        |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90                       | 1,20                           | 0,00       | 0,30     | 0,00     | 0,0        |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00                       | 1,00                           | 1,00       | 0,00     | 0,00     | 1,0        |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00                       | 1,00                           | 0,00       | 0,00     | 0,00     | 1,0        |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 1,50       | 0,30     | 0,00     | 0,0        |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 0,00       | 0,30     | 0,00     | 0,0        |
| ULS 7  | Permanent                 | 10°                          | 1,35                       | 1,35                           | 0,00       | 0,00     | 0,00     | 0,0        |
| ULS 8  | Special                   | 10°                          | 1,00                       | 1,00                           | 0,00       | 0,00     | 0,00     | 1,0        |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              |                            | $\gamma_G$<br>$G_k$            | $\gamma_Q$ |          |          | $A_k$      |
| SPLS 1a  | Wind                      | 10°                          | 1,20                       | 1,20                           | 0,0        | 0,78     | 0,00     | 0,0        |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90                       | 1,20                           | 0,0        | 0,78     | 0,00     | 0,0        |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90                       | 0,90                           | 0,0        | 0,78     | 0,00     | 0,0        |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20                       | 1,20                           | 0,0        | 0,36     | 0,34     | 0,0        |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90                       | 1,20                           | 0,0        | 0,36     | 0,34     | 0,0        |
| SPLS 4   | Koude+wind                | -20°                         | 1,20                       | 1,20                           | 0,0        | 0,24     | 0,00     | 0,0        |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90                       | 1,20                           | 0,0        | 0,24     | 0,00     | 0,0        |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 1,2        | 0,24     | 0,0      | 0,0        |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20                       | 1,20                           | 0,0        | 0,24     | 0,0      | 0,0        |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              |                            | $G_k$                          | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$      |
| SLS 1a   | Wind                      | 10°                          | 1,00                       | 1,00                           | 0,0        | 1,00     | 0,0      | 0,0        |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00                       | 1,00                           | 0,0        | 0,30     | 1,00     | 0,0        |
| SLS 4  | Wind                      | -20°                         | 1,00                       | 1,00                           | 0,0        | 0,20     | 0,0      | 0,0        |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00                       | 1,00                           | 0,0        | 0,20     | 0,0      | 0,0        |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00                       | 1,00                           | 0,0        | 0,00     | 0,0      | 0,0        |

Aantal windrichtingen 4  
 Aantal belastingcombinaties ULS 44  
 Aantal belastingcombinaties SPLS 0  
 Aantal belastingcombinaties SLS 11  
 Aantal knooplasten 440

Project: GT-RLL380  
 Masttype: S+32  
 Mast: 72N

### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -64,3         | 64,3          | 6,4           | 6,4           | 14,6          | 9,5           |
| bl2      | -63,4         | 63,4          | 6,3           | 6,3           | 14,5          | 9,4           |
| 380ct1f1 | -162,7        | 162,7         | 21,7          | 21,7          | 36,0          | 22,9          |
| 380ct1f2 | -162,7        | 162,7         | 21,7          | 21,7          | 36,0          | 22,9          |
| 380ct1f3 | -165,3        | 165,3         | 23,1          | 23,1          | 36,2          | 22,9          |
| 380ct2f1 | -162,7        | 162,7         | 21,7          | 21,7          | 36,0          | 22,9          |
| 380ct2f2 | -162,7        | 162,7         | 21,7          | 21,7          | 36,0          | 22,9          |
| 380ct2f3 | -165,3        | 165,3         | 23,1          | 23,1          | 36,2          | 22,9          |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 528,0  | 553,1 | 528,0 |
| bl2      | 528,0  | 553,7 | 528,0 |
| 380ct1f1 | 528,0  | 546,6 | 528,0 |
| 380ct1f2 | 528,0  | 546,6 | 528,0 |
| 380ct1f3 | 528,0  | 547,2 | 528,0 |
| 380ct2f1 | 528,0  | 546,6 | 528,0 |
| 380ct2f2 | 528,0  | 546,6 | 528,0 |
| 380ct2f3 | 528,0  | 547,2 | 528,0 |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 699,4  | 509,3 |
| bl2      | 704,1  | 508,7 |
| 380ct1f1 | 625,9  | 532,9 |
| 380ct1f2 | 625,9  | 532,9 |
| 380ct1f3 | 635,0  | 535,0 |
| 380ct2f1 | 625,9  | 532,9 |
| 380ct2f2 | 625,9  | 532,9 |
| 380ct2f3 | 635,0  | 535,0 |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

|                  |         |
|------------------|---------|
| Max. weight span | 704,1 m |
| Min. weight span | 400,0 m |

Wind / Weight span verhouding

|         |
|---------|
| 1,760 - |
| 1,000 - |

Project: GT-RLL380  
 Masttype: S+32  
 Mast: 72N

**Maximale waarden back+ahead span      Maximale waarden trekkracht geleider**

| Geleider | Fx   | Fy   | Fz   | Ft_ba  | Ft_ah |
|----------|------|------|------|--------|-------|
|          | [kN] | [kN] | [kN] | [kN]   | [kN]  |
| bl1      | 22,9 | 12,7 | 24,1 | -64,3  | 64,3  |
| bl2      | 22,3 | 12,7 | 23,9 | -63,4  | 63,4  |
| 380ct1f1 | 58,7 | 43,5 | 58,9 | -162,7 | 162,7 |
| 380ct1f2 | 58,7 | 43,5 | 58,9 | -162,7 | 162,7 |
| 380ct1f3 | 58,7 | 46,2 | 59,1 | -165,3 | 165,3 |
| 380ct2f1 | 58,7 | 43,5 | 58,9 | -162,7 | 162,7 |
| 380ct2f2 | 58,7 | 43,5 | 58,9 | -162,7 | 162,7 |
| 380ct2f3 | 58,7 | 46,2 | 59,1 | -165,3 | 165,3 |

**EDS-belastingen geleiders**

| Geleider | Fx   | Fy   | Fz   | Ft_ba | Ft_ah |
|----------|------|------|------|-------|-------|
|          | [kN] | [kN] | [kN] | [kN]  | [kN]  |
| bl1      | 0,0  | 0,0  | 5,1  | -15,3 | 15,3  |
| bl2      | 0,0  | 0,0  | 5,0  | -14,9 | 14,9  |
| 380ct1f1 | 0,0  | 0,0  | 29,8 | -73,3 | 73,3  |
| 380ct1f2 | 0,0  | 0,0  | 29,8 | -73,3 | 73,3  |
| 380ct1f3 | 0,0  | 0,0  | 29,8 | -73,3 | 73,3  |
| 380ct2f1 | 0,0  | 0,0  | 29,8 | -73,3 | 73,3  |
| 380ct2f2 | 0,0  | 0,0  | 29,8 | -73,3 | 73,3  |
| 380ct2f3 | 0,0  | 0,0  | 29,8 | -73,3 | 73,3  |

**Controle uplift SLS-wind**

| Combinatie: Geleider | Fz_ba | Fz_ah |
|----------------------|-------|-------|
|                      | [kN]  | [kN]  |
| SLS 4    bl1         | 3,4   | 2,0   |
| bl2                  | 3,3   | 1,9   |
| 380ct1f1             | 18,7  | 12,0  |
| 380ct1f2             | 18,7  | 12,0  |
| 380ct1f3             | 18,7  | 12,0  |
| 380ct2f1             | 18,7  | 12,0  |
| 380ct2f2             | 18,7  | 12,0  |
| 380ct2f3             | 18,7  | 12,0  |

Project: GT-RLL380  
 Masttype: S+32  
 Mast: 72N

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie    | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|---------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90     |             | 0             | 292           | 264           | 20330          | 0              | 0              |
| ULS 1a_0,9_90 |             | 0             | 292           | 182           | 20331          | 0              | 0              |
| ULS 3_90      |             | 0             | 165           | 402           | 11602          | 0              | 0              |
| ULS 3_0,9_90  |             | 0             | 165           | 313           | 11603          | 0              | 0              |
| SLS 7         |             | 0             | 0             | 189           | -2             | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

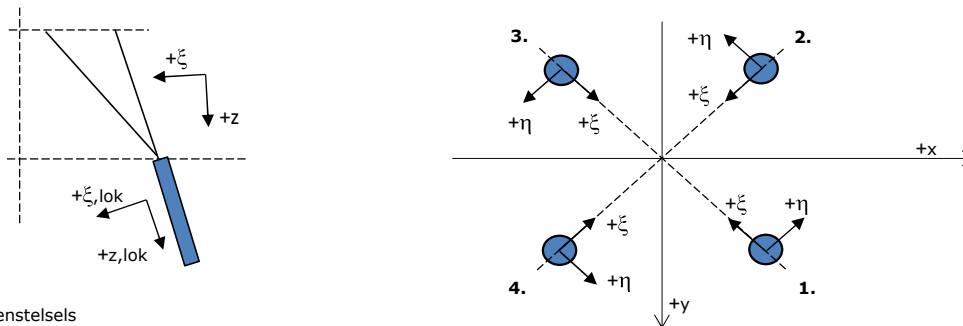
| Combinatie | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90  | 0             | 786           | 1109          | 42100          | 0              | 0              |
| ULS 3_90   | 0             | 313           | 1246          | 18133          | 0              | 0              |
| SLS 7      | 0             | 0             | 893           | -2             | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_0,9_0,9_90 | 0             | 786           | 770           | <b>42102</b>   | 0              | 0              |
| ULS 1a_0          | 609           | 0             | 1070          | -3             | <b>30383</b>   | 0              |
| ULS 5a Ba 10      | 59            | 0             | 886           | 261            | 3784           | <b>-1027</b>   |
| ULS 1a_0,9_0,9_45 | 469           | 615           | 770           | <b>32435</b>   | <b>22223</b>   | 0              |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_45  | 377           | 348           | <b>2130</b>   | 20               | -513            | 5                     | 2192                |
| 2     | ULS 1a_0   | 203           | -246          | <b>1301</b>   | 30               | -317            | -1                    | 1339                |
| 3     | ULS 8 Ba   | -89           | -124          | <b>660</b>    | -25              | -151            | 9                     | 679                 |
| 4     | ULS 1a_135 | -377          | 348           | <b>2130</b>   | -20              | -513            | 5                     | 2192                |

**Maximale trekbelasting**

| Stijl | Combinatie         | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 8 Ba           | 3             | -33           | <b>-175</b>   | 26               | 21              | -21                   | -180                |
| 2     | ULS 1a_0,9_0,9_135 | -289          | 260           | <b>-1667</b>  | 20               | 389             | -16                   | -1715               |
| 3     | ULS 1a_0,9_0,9_45  | 289           | 260           | <b>-1667</b>  | -20              | 389             | -16                   | -1715               |
| 4     | ULS 1a_0,9_0,9_0   | 116           | -159          | <b>-841</b>   | -30              | 194             | -10                   | -866                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie         | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_0,9_0,9_135 | 128           | 47            | 540           | <b>57</b>        | -124            | 7                     | 555                 |
| 2     | ULS 1a_0,9_0,9_45  | -55           | -25           | -155          | <b>57</b>        | 21              | -17                   | -159                |
| 3     | ULS 5a Ba 21       | -46           | 0             | 102           | <b>33</b>        | -33             | -8                    | 105                 |
| 4     | ULS 5a Ah 10       | -40           | 84            | 357           | <b>31</b>        | -88             | -1                    | 367                 |

**Maximale torsiebelasting (negatief)**

| Index | Combinatie         | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_0           | 203           | 246           | 1301          | <b>-30</b>       | -317            | -1                    | 1339                |
| 2     | ULS 5a Ah 21       | 46            | 0             | 100           | <b>-32</b>       | -33             | -9                    | 103                 |
| 3     | ULS 1a_0,9_0,9_135 | 55            | -25           | -155          | <b>-57</b>       | 21              | -17                   | -159                |
| 4     | ULS 1a_0,9_0,9_45  | -128          | 47            | 540           | <b>-57</b>       | -124            | 7                     | 555                 |

Project: GT-RLL380  
 Masttype: S+32  
 Mast: 72N

#### Combinatie Ftrek+Fhor

| Stijl | Combinatie         | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | ULS 8 Ba           | 3                      | -33                    | <b>-175</b>            | <b>26</b>              | 21                     | -21                        | -180                       |
| 2     | ULS 1a_0,9_0,9_135 | -289                   | 260                    | <b>-1667</b>           | <b>20</b>              | 389                    | -16                        | -1715                      |
| 3     | ULS 1a_0,9_0,9_45  | 289                    | 260                    | <b>-1667</b>           | <b>-20</b>             | 389                    | -16                        | -1715                      |
| 4     | ULS 1a_0,9_0,9_0   | 116                    | -159                   | <b>-841</b>            | <b>-30</b>             | 194                    | -10                        | -866                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 42                     | 42                     | 223                    | 0                      | -60                    | -5                         | 230                        |
| 2     | SLS 7      | 42                     | -42                    | 223                    | 0                      | -60                    | -5                         | 230                        |
| 3     | SLS 7      | -42                    | -42                    | 223                    | 0                      | -60                    | -5                         | 230                        |
| 4     | SLS 7      | -42                    | 42                     | 223                    | 0                      | -60                    | -5                         | 230                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie         | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | ULS 1a_45          | 377                    | 348                    | <b>2130</b>            | 20                     | -513                   | 5                          | 2192                       |
| Max. trek         | ULS 1a_0,9_0,9_45  | 289                    | 260                    | <b>-1667</b>           | -20                    | 389                    | -16                        | -1715                      |
| Max. pos. torsie  | ULS 1a_0,9_0,9_45  | -55                    | -25                    | -155                   | <b>57</b>              | 21                     | -17                        | -159                       |
| Max. neg. torsie  | ULS 1a_0,9_0,9_135 | 55                     | -25                    | -155                   | <b>-57</b>             | 21                     | -17                        | -159                       |
| Comb. trek+torsie | ULS 1a_0,9_0,9_45  | 289                    | 260                    | <b>-1667</b>           | <b>-20</b>             | 389                    | -16                        | -1715                      |

#### Maximale trekbelasting SLS

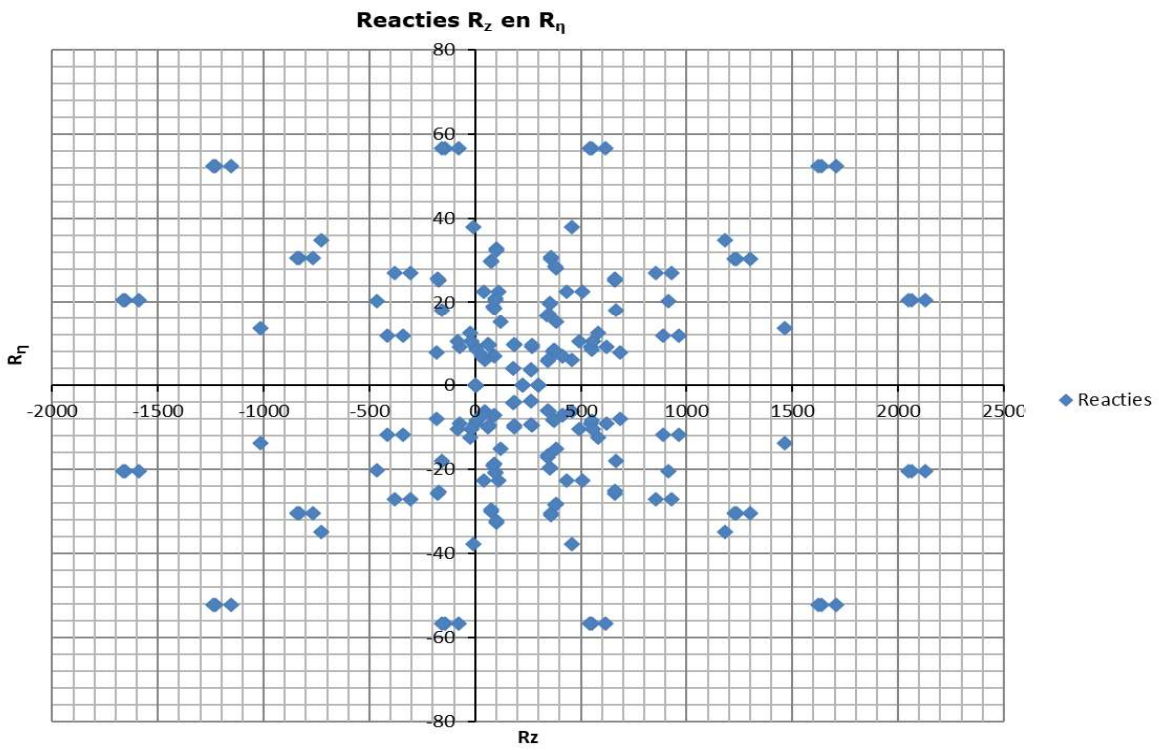
| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 42                     | 42                     | <b>223</b>             | 0                      | -60                    | -5                         | 230                        |
| 2     | SLS 1a_135 | -175                   | 155                    | <b>-1014</b>           | 14                     | 233                    | -13                        | -1044                      |
| 3     | SLS 1a_45  | 175                    | 155                    | <b>-1014</b>           | -14                    | 233                    | -13                        | -1044                      |
| 4     | SLS 1a_0   | 59                     | -88                    | <b>-466</b>            | -20                    | 104                    | -9                         | -479                       |

#### Maximale drukbelasting SLS

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_45  | 260                    | 240                    | <b>1465</b>            | 14                     | -354                   | 2                          | 1507                       |
| 2     | SLS 1a_0   | 144                    | -172                   | <b>912</b>             | 20                     | -223                   | -2                         | 939                        |
| 3     | SLS 7      | -42                    | -42                    | <b>223</b>             | 0                      | -60                    | -5                         | 230                        |
| 4     | SLS 1a_135 | -260                   | 240                    | <b>1465</b>            | -14                    | -354                   | 2                          | 1507                       |



Project: GT-RLL380  
Masttype: S+32  
Mast: 72N





Project: GT-RLL380  
 Tower: S+32 (bouwfase)  
 Number: 72N

Auteur: TBR  
 Versie: v12.0

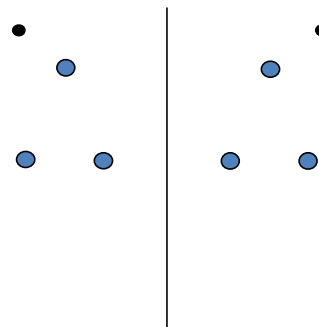
### Geleiderbelastingen

#### Algemeen

Benaming S+32 (bouwfase)  
 Masttype Steunmast  
 Aantal circuits 2  
 Configuratie 2-circuit-donau  
 Aantal bliksemgeleiders 2

#### Uitgangspunten

Norm NEN-EN50341-2-15:2019  
 Gevolgklasse initieel CC2  
 Betrouwbaarheidsniveau initieel Nieuwbouw  
 Referentieperiode initieel 15 jaar  
 Betrouwbaarheidsniveau na aanpassing n.v.t.  
 Windgebied III  
 Windsnelheid (m/s) 24,5 m/s  
 Terreincategorie II  
 Reductiefactor  $C_{dir}$  1,00  
 IJsgebied fasegeleider B  
 IJsgebied bliksemgeleider A



Configuratie geleiders

#### Geleiders Back

| Omschrijving   | Spanning | Geleider Back          | Bundel Ba | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{back}$ |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|--------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                     |
| Circuit 2      | 0 kV     | 0                      | 0         | 0         | 0 %             | 0 %              | 0                        |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A         | 2 %             | 2 %              | 1600                     |
| Bliksemdraad 2 |          | 0                      | 0         | 0         | 0 %             | 0 %              | 0                        |

#### Geleiders Ahead

| Omschrijving   | Spanning | Geleider Ahead         | Bundel Ah | IJsgebied | Toeslag gewicht | Toeslag diameter | Intrekwaarden $P_{ahead}$ |
|----------------|----------|------------------------|-----------|-----------|-----------------|------------------|---------------------------|
| Circuit 1      | 380 kV   | ACCC-Warsaw            | 3         | B         | 2 %             | 2 %              | 1600                      |
| Circuit 2      | 0 kV     | 0                      | 0         | 0         | 0 %             | 0 %              | 0                         |
| Bliksemdraad 1 |          | AACSR 241-AL3-39-A20SA | 1         | A         | 2 %             | 2 %              | 1600                      |
| Bliksemdraad 2 |          | 0                      | 0         | 0         | 0 %             | 0 %              | 0                         |

#### Isolatoren (1)

| Omschrijving   | Ophanging           | Gewicht [kN] | Lengte [m] | Windopp. [m <sup>2</sup> ] |
|----------------|---------------------|--------------|------------|----------------------------|
| Circuit 1      | Halfverankering     | 5,60         | 4,50       | 2,40                       |
| Circuit 2      | Halfverankering     | 5,60         | 4,50       | 2,40                       |
| Bliksemdraad 1 | Vast (Bliksemdraad) | 0,10         | 0,20       | 0,10                       |
| Bliksemdraad 2 | Vast (Bliksemdraad) | 0,10         | 0,20       | 0,10                       |

1. Eigenschappen gelden voor geheel van de isolatorset

#### Ophanghoogte en positie in mast

| Circuits       | Aanduiding | Nummer   | Ophanghoogte | Aangrijppunt | Positie in mast<br>Horizontale afstand |
|----------------|------------|----------|--------------|--------------|--|
| Circuit 1      | 10         | 380ct1f1 | 60,0 m       | 64,5 m       | -17,5 m                                |
| Circuit 1      | 11         | 380ct1f2 | 60,0 m       | 64,5 m       | -9,5 m                                 |
| Circuit 1      | 12         | 380ct1f3 | 72,0 m       | 76,5 m       | -13,5 m                                |
| Circuit 2      | 20         | 0ct2f1   | -4,5 m       | 0,0 m        | 0,0 m                                  |
| Circuit 2      | 21         | 0ct2f2   | -4,5 m       | 0,0 m        | 0,0 m                                  |
| Circuit 2      | 22         | 0ct2f3   | -4,5 m       | 0,0 m        | 0,0 m                                  |
| Bliksemdraad 1 | 1          | bl1      | 80,3 m       | 80,5 m       | -18,5 m                                |
| Bliksemdraad 2 | 3          | bl2      | -0,2 m       | 0,0 m        | 0,0 m                                  |

Project: GT-RL380  
 Tower: S+32 (bouwfase)  
 Number: 72N

**Hoogteaanpassing naastgelegen masten** (aanpassing wind- en weight span)

|                                    | Back                      | Ahead |   |
|------------------------------------|---------------------------|-------|---|
| Verhoging voor windbelasting       | 0,0 m                     | 0,0 m | (positief: omhoog)                      |
| Verlaging voor verticale belasting | -32,0 m                   | 0,0 m | (negatief: omlaag, grotere weight span) |
| Verlaging:                         | Niet in 0,9EG-combinaties |       |   |

**Hoogteafwijking mastbeeld naastgelegen masten en richtingsverandering t.o.v. Lijnrichting**

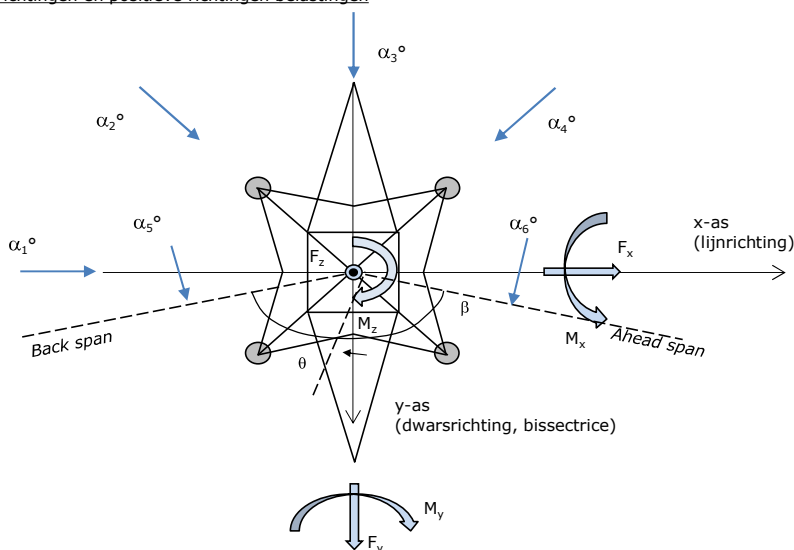
| Circuits       | Aanduiding | Nummer   | Hoogteverschil  |                  | Richtingsverandering |                  |
|----------------|------------|----------|-----------------|------------------|----------------------|------------------|
|                |            |          | $\Delta h$ back | $\Delta h$ ahead | $\Delta y$ back      | $\Delta y$ ahead |
| Circuit 1      | 10         | 380ct1f1 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 11         | 380ct1f2 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 1      | 12         | 380ct1f3 | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 20         | 0ct2f1   | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 21         | 0ct2f2   | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Circuit 2      | 22         | 0ct2f3   | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 1 | 1          | bl1      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |
| Bliksemdraad 2 | 3          | bl2      | 0,0             | 0,0 m            | 0,0                  | 0,0 m            |

**Lijn- en mastgegevens**

|  | Back       | Ahead   |
|--|------------|---------|
| Ruling span $\sqrt{(\Sigma L^3)/\Sigma L}$ | 400,0      | 400,0 m |
| Lijnhoek $\beta$                           | 180 °      |         |
| Rotatie mast t.o.v. bissectrice $\theta$   | 0 °        |         |
| Vaklengte                                  | 800        | 800 m   |
| Hoogte onderkant mast t.o.v. maaiveld      | 0,5 m      |         |
| Beschouwde windrichtingen                  | $\alpha_1$ | 0 °     |
| Windrichtingen volgens:                    | $\alpha_2$ | 45 °    |
| Geleiderbelastingen                        | $\alpha_3$ | 90 °    |
|  | $\alpha_4$ | 135 °   |
|  | $\alpha_5$ | 225 °   |
|  | $\alpha_6$ | 270 °   |

Windrichtingen gelden t.o.v. hoofdrichting mastconstructie, niet t.o.v. bissectrice.

Windrichtingen en positieve richtingen belastingen



**Beschouwd aantal windrichtingen**

|        |   |
|--------|---|
| 1a     | 6 |
| 3      | 6 |
| 4      | 1 |
| 6      | 1 |
| Overig | 1 |

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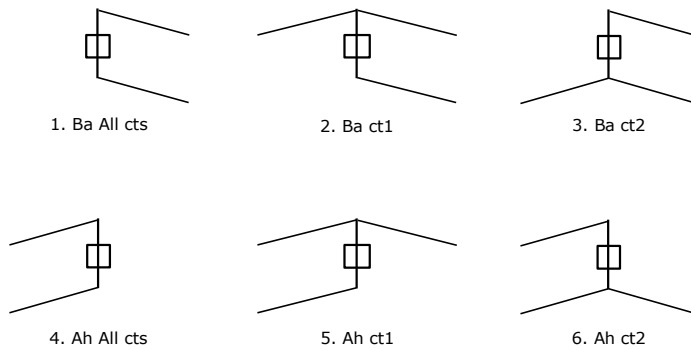
### Geleiderafval

|                |          | SPLS - torsie |      | SPLS - Enkelzijdige trek |      | 5a - geleiderbreuk |      |
|----------------|----------|---------------|------|--------------------------|------|--------------------|------|
|                |          | Aanw.         | Afw. | Aanw.                    | Afw. | Aanw.              | Afw. |
| Circuit 1      | 380ct1f1 | 1             | 0    | 1                        | 0    | 0,8                | 0    |
| Circuit 1      | 380ct1f2 | 1             | 0    | 1                        | 0    | 0,8                | 0    |
| Circuit 1      | 380ct1f3 | 1             | 0    | 1                        | 0    | 0,8                | 0    |
| Circuit 2      | 0ct2f1   | 0             | 1    | 1                        | 0    | 0,8                | 0    |
| Circuit 2      | 0ct2f2   | 0             | 1    | 1                        | 0    | 0,8                | 0    |
| Circuit 2      | 0ct2f3   | 0             | 1    | 1                        | 0    | 0,8                | 0    |
| Bliksemdraad 1 | bl1      | 1             | 0    | 1                        | 0    | 1                  | 0    |
| Bliksemdraad 2 | bl2      | 0             | 1    | 1                        | 0    | 1                  | 0    |

### Belastingsituaties SPLS

Beschouwde situaties SPLS: SPLS voor steunmast niet van toepassing

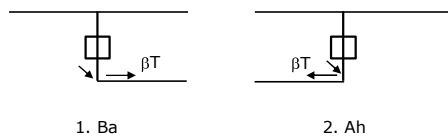
Principe belastingssituaties:



### Belastingsituaties 5a. Geleiderbreuk

Beschouwde situaties geleiderbreuk 5a: 1 en 2, alle mogelijke situaties.

Principe belastingssituaties:



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### Belastingsituaties 6. Bouw- en onderhoud

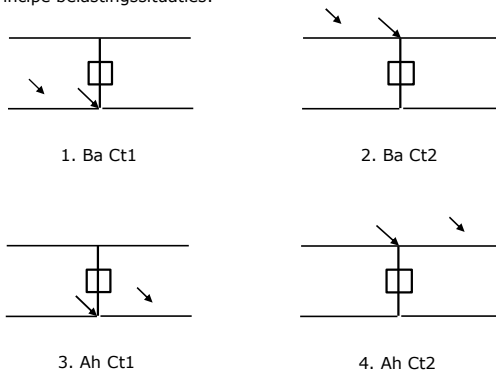
Onder 6a wordt de belasting door aanwezigheid lijnwagen of lijnfiets in combinatie met puntlast op traverse in rekening gebracht. Combinatie 6b bevat geen belastingen in geleider of op traverse. Deze combinatie is toegevoegd om te kunnen combineren met separate controle bordessen etc. De situaties worden in ULS en in iedere SPLS-situatie (in geval van hoekmast) toegepast.

|                      | Fase   | Bliksem |
|----------------------|--------|---------|
| Lijnwagen            | 4,0 kN | 2,0 kN  |
| Puntlast op traverse | 1,0 kN | 1,0 kN  |

Beschouwde situaties bouw- en onderhoud 6a: 1 en 2, uitgangspunt is symmetrie tussen back / ahead.

Aanwezigheid lijnwagen: Circuit, belasting tegelijk aanwezig in alle geleiders per circuit.

Principe belastingssituaties:



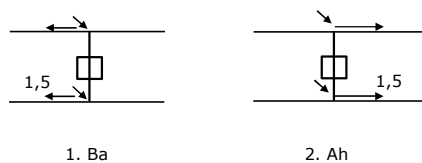
### Belastingsituaties 8. Lijndansen als statische belasting

| Geleider                 |         |       |
|--------------------------|---------|-------|
| Steunmast fase           | 0,866 W | 1,5 W |
| Steunmast bliksem        | 1,5 EDS | 1,5 W |
| Hoekmast fase en bliksem | 1,5 EDS | 1,5 W |

Beschouwde situaties lijndansen 8: 1 en 2, alle mogelijke situaties.

Belasting tegelijk aanwezig in alle geleiders van het circuit.

Principe belastingssituaties:



### Belastingcombinatie 8. Lijndansen als dynamische belasting

Alleen van toepassing op hoek- en eindmasten  
 Belasting bestaat uit EDS-trekbelasting in één van de geleiders aan één zijde van de mast  
 Door gebruiker via het belastingspectrum van tabel 4.11/NL.1 om te zetten naar spanningspectrum

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## Mastconstructie

### Eigenschappen

|   |                 |         |
|---|-----------------|---------|
| Masttype                                    | Steunmast       |         |
| Mastbenaming                                | S+32 (bouwfase) |         |
| Voetplaat t.o.v. maaiveld                   | 0,5 m           |         |
| Masthoogte t.o.v. voetplaat                 | 82,5 m          |         |
| Gewicht mast                                | 703,7 kN        |         |
| <i>Breedte en helling mast bij fundatie</i> |                 |         |
|   | x-ri.           | y-ri.   |
| Pootsprei                                   | 14,70           | 14,70 m |
| Helling van de randstijl                    | 0,172           | 0,172 - |
| Factor spatkracht                           | 1,1             | 1,1 -   |

### Berekening windbelasting

|   |                                       |
|---|---------------------------------------|
| Dynamische invloed $G_T$                              | 1,05                                  |
| Windbelasting overhoeks op mastlichaam evenredig met: | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Windbelasting overhoeks op traverse evenredig met:    | $(A1C1\sin^2(\phi)+A2C2\cos^2(\phi))$ |
| Vergroting wind overhoeks mastlichaam                 | $(1+0,2\sin^2(2\phi))$                |
| Vergroting wind overhoeks traverse                    | $(1+0,2\sin^2(2\phi))$                |
| Factor wind evenwijdig t.o.v. haaks op traverse       | 0,4                                   |

### Eigenschappen mastsecties langsrichting (vooraanzicht, yz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 19,50    | 14,70                 | 8,00                  | 19,50     | 0,172                 | 221,33                              | 37,50                               | 0,17                                      | 3,07           |
| Eerste tussenstuk | 40,50    | 8,00                  | 5,00                  | 21,00     | 0,071                 | 136,50                              | 26,74                               | 0,20                                      | 2,95           |
| Tweede tussenstuk | 64,50    | 5,00                  | 3,50                  | 24,00     | 0,031                 | 102,00                              | 22,19                               | 0,22                                      | 2,86           |
| Bovenstuk 1       | 72,50    | 3,50                  | 3,17                  | 8,00      | 0,021                 | 26,67                               | 6,27                                | 0,24                                      | 2,78           |
| Bovenstuk 2       | 80,50    | 3,17                  | 2,83                  | 8,00      | 0,021                 | 24,00                               | 5,86                                | 0,24                                      | 2,75           |
| Topstuk           | 82,50    | 2,83                  |                       | 2,00      |                       | 2,83                                | 0,41                                | 0,15                                      | 3,18           |
| Ondertraverse     | 64,50    | 15,75                 |                       | 4,00      |                       | 31,50                               | 8,71                                | 0,28                                      | 2,62           |
| Boventraverse     | 76,50    | 17,00                 |                       | 4,00      |                       | 34,00                               | 9,30                                | 0,27                                      | 2,63           |

### Eigenschappen mastsecties dwarsrichting (zijaanzicht, xz-vlak)

| Omschrijving      | h<br>[m] | b <sub>1</sub><br>[m] | b <sub>2</sub><br>[m] | Δh<br>[m] | Δ <sub>x</sub><br>[m] | A <sub>0</sub><br>[m <sup>2</sup> ] | A <sub>1</sub><br>[m <sup>2</sup> ] | χ = A <sub>1</sub> /A <sub>0</sub><br>[-] | C <sub>t</sub> |
|-------------------|----------|-----------------------|-----------------------|-----------|-----------------------|-------------------------------------|-------------------------------------|---|----------------|
| Broekstuk         | 19,50    | 14,70                 | 8,00                  | 19,50     | 0,172                 | 221,33                              | 37,50                               | 0,17                                      | 3,07           |
| Eerste tussenstuk | 40,50    | 8,00                  | 5,00                  | 21,00     | 0,071                 | 136,50                              | 26,74                               | 0,20                                      | 2,95           |
| Tweede tussenstuk | 64,50    | 5,00                  | 3,50                  | 24,00     | 0,031                 | 102,00                              | 22,19                               | 0,22                                      | 2,86           |
| Bovenstuk 1       | 72,50    | 3,50                  | 3,17                  | 8,00      | 0,021                 | 26,67                               | 6,27                                | 0,24                                      | 2,78           |
| Bovenstuk 2       | 80,50    | 3,17                  | 2,83                  | 8,00      | 0,021                 | 24,00                               | 5,86                                | 0,24                                      | 2,75           |
| Topstuk           | 82,50    | 2,83                  |                       | 2,00      |                       | 2,83                                | 0,41                                | 0,15                                      | 3,18           |
| Ondertraverse     | 64,50    | 15,75                 |                       | 4,00      |                       | 31,50                               | 8,71                                | 0,28                                      | 2,62           |
| Boventraverse     | 76,50    | 17,00                 |                       | 4,00      |                       | 34,00                               | 9,30                                | 0,27                                      | 2,63           |

NB: oppervlakte traverse dwarsrichting van de tabel wordt in berekening gereduceerd.  
 NB: oppervlakte traverse per zijde, dus helft van totaal van twee traveres.

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#### Windoppervlak feeders telecominstallaties

| Onderdeel         | A (m <sup>2</sup> /m) | Factor | Δh   | A <sub>1</sub> |
|-------------------|-----------------------|--------|------|----------------|
| Broekstuk         | 0,20                  | 0,71   | 19,5 | 2,8            |
| Eerste tussenstuk | 0,20                  | 0,71   | 21,0 | 3,0            |
| Tweede tussenstuk |                       |        |      |                |
| Bovenstuk 1       |                       |        |      |                |
| Bovenstuk 2       |                       |        |      |                |

#### Invoer antennes

| Omschrijving | A (m <sup>2</sup> ) | h (m) | C <sub>i</sub> (m) |
|--------------|---------------------|-------|--------------------|
| Antenne top  |                     |       |                    |
| Antenne o.t. | 4,7                 | 40,5  | 1,5                |

#### Belastingen mastsectie langsrichting (x-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>x1</sub><br>[kN] | F <sub>x2</sub><br>[kN] | F <sub>x3</sub><br>[kN] | F <sub>x4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>y1</sub><br>[kNm] | M <sub>y2</sub><br>[kNm] | M <sub>y3</sub><br>[kNm] | M <sub>y4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 80,7                    | 68,4                    | 0,0                     | -68,4                   | 9,8                    | 786,4                    | 667,2                    | 0,0                      | -667,2                   |
| Eerste tussenstuk | 0,99                                   | 77,9                    | 66,1                    | 0,0                     | -66,1                   | 30,0                   | 2338,2                   | 1984,0                   | 0,0                      | -1984,0                  |
| Tweede tussenstuk | 1,15                                   | 72,9                    | 61,8                    | 0,0                     | -61,8                   | 52,5                   | 3825,5                   | 3246,0                   | 0,0                      | -3246,0                  |
| Bovenstuk 1       | 1,23                                   | 21,5                    | 18,2                    | 0,0                     | -18,2                   | 68,5                   | 1472,8                   | 1249,7                   | 0,0                      | -1249,7                  |
| Bovenstuk 2       | 1,26                                   | 20,3                    | 17,3                    | 0,0                     | -17,3                   | 76,5                   | 1556,0                   | 1320,3                   | 0,0                      | -1320,3                  |
| Topstuk           | 1,28                                   | 1,7                     | 1,4                     | 0,0                     | -1,4                    | 81,5                   | 137,0                    | 116,3                    | 0,0                      | -116,3                   |
| Ondertraverse     | 1,22                                   | 55,6                    | 33,0                    | 0,0                     | -33,0                   | 65,8                   | 3661,0                   | 2174,5                   | 0,0                      | -2174,5                  |
| Boventraverse     | 1,27                                   | 62,2                    | 36,9                    | 0,0                     | -36,9                   | 77,8                   | 4839,1                   | 2874,3                   | 0,0                      | -2874,3                  |

|               |              |              |            |               |  |                |                |            |                 |
|---------------|--------------|--------------|------------|---------------|--|----------------|----------------|------------|-----------------|
| <b>Totaal</b> | <b>392,8</b> | <b>303,3</b> | <b>0,0</b> | <b>-303,3</b> |  | <b>18615,8</b> | <b>13632,3</b> | <b>0,0</b> | <b>-13632,3</b> |
|---------------|--------------|--------------|------------|---------------|--|----------------|----------------|------------|-----------------|

#### Belastingen mastsectie dwarsrichting (y-richting) per windrichting

| Omschrijving      | P <sub>w</sub><br>[kN/m <sup>2</sup> ] | F <sub>y1</sub><br>[kN] | F <sub>y2</sub><br>[kN] | F <sub>y3</sub><br>[kN] | F <sub>y4</sub><br>[kN] | h <sub>ef</sub><br>[m] | M <sub>x1</sub><br>[kNm] | M <sub>x2</sub><br>[kNm] | M <sub>x3</sub><br>[kNm] | M <sub>x4</sub><br>[kNm] |
|-------------------|--|-------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Broekstuk         | 0,70                                   | 0,0                     | 68,4                    | 80,7                    | 68,4                    | 9,8                    | 0,0                      | 667,2                    | 786,4                    | 667,2                    |
| Eerste tussenstuk | 0,99                                   | 0,0                     | 66,1                    | 77,9                    | 66,1                    | 30,0                   | 0,0                      | 1984,0                   | 2338,2                   | 1984,0                   |
| Tweede tussenstuk | 1,15                                   | 0,0                     | 61,8                    | 72,9                    | 61,8                    | 52,5                   | 0,0                      | 3246,0                   | 3825,5                   | 3246,0                   |
| Bovenstuk 1       | 1,23                                   | 0,0                     | 18,2                    | 21,5                    | 18,2                    | 68,5                   | 0,0                      | 1249,7                   | 1472,8                   | 1249,7                   |
| Bovenstuk 2       | 1,26                                   | 0,0                     | 17,3                    | 20,3                    | 17,3                    | 76,5                   | 0,0                      | 1320,3                   | 1556,0                   | 1320,3                   |
| Topstuk           | 1,28                                   | 0,0                     | 1,4                     | 1,7                     | 1,4                     | 81,5                   | 0,0                      | 116,3                    | 137,0                    | 116,3                    |
| Ondertraverse     | 1,22                                   | 0,0                     | 33,0                    | 22,2                    | 33,0                    | 65,8                   | 0,0                      | 2174,5                   | 1464,4                   | 2174,5                   |
| Boventraverse     | 1,27                                   | 0,0                     | 36,9                    | 24,9                    | 36,9                    | 77,8                   | 0,0                      | 2874,3                   | 1935,6                   | 2874,3                   |

|               |            |              |              |              |  |            |                |                |                |
|---------------|------------|--------------|--------------|--------------|--|------------|----------------|----------------|----------------|
| <b>Totaal</b> | <b>0,0</b> | <b>303,3</b> | <b>322,1</b> | <b>303,3</b> |  | <b>0,0</b> | <b>13632,3</b> | <b>13515,8</b> | <b>13632,3</b> |
|---------------|------------|--------------|--------------|--------------|--|------------|----------------|----------------|----------------|

#### Resulterende belastingen vanuit mastconstructie incl. antenne zonder geleiders niveau fundatie (kar. waarde)

| Belasting / windrichting | F <sub>x</sub><br>[kN] | F <sub>y</sub><br>[kN] | F <sub>z</sub><br>[kN] | M <sub>x</sub><br>[kNm] | M <sub>y</sub><br>[kNm] | M <sub>z</sub><br>[kNm] |
|--------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Permanente belasting     | 0                      | 0                      | 704                    | 0                       | 0                       | 0                       |
| Windrichting 0°          | 400                    | 0                      | 0                      | 0                       | 19869                   | 0                       |
| Windrichting 45°         | 309                    | 309                    | 0                      | 14542                   | 14542                   | 0                       |
| Windrichting 90°         | 0                      | 330                    | 0                      | 14514                   | 0                       | 0                       |
| Windrichting 135°        | -309                   | 309                    | 0                      | 14542                   | -14542                  | 0                       |



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### Tussenresultaten geleiderbelastingen

#### Geleiders back

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | 0                      |                  |                         |            |                           |                   |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | 0                      |                  |                         |            |                           |                   |

#### Geleiders ahead

| Circuit        | Geleider               | Diameter<br>[mm] | A<br>[mm <sup>2</sup> ] | G<br>[N/m] | E<br>[N/mm <sup>2</sup> ] | $\alpha T$<br>[-] |
|----------------|------------------------|------------------|-------------------------|------------|---------------------------|-------------------|
| Circuit 1      | ACCC-Warsaw            | 27,7             | 571,0                   | 14,98      | 62700                     | 1,88E-05          |
| Circuit 2      | 0                      |                  |                         |            |                           |                   |
| Bliksemdraad 1 | AACSR 241-AL3-39-A20SA | 21,8             | 281,0                   | 9,38       | 70165                     | 1,97E-05          |
| Bliksemdraad 2 | 0                      |                  |                         |            |                           |                   |

#### Verticale belasting back

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 0             | 0              |                    | 0         |         |                      |                             |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 0             | 0              |                    | 0         |         |                      |                             |

#### Verticale belasting ahead

| Circuit        | Bundel<br>[-] | Toeslag<br>[%] | $W_{z,G}$<br>[N/m] | IJsgebied | Formule | $W_{z,ijs}$<br>[N/m] | $W_{z,ijs,bundel}$<br>[N/m] |
|----------------|---------------|----------------|--------------------|-----------|---------|----------------------|-----------------------------|
| Circuit 1      | 3             | 2              | 45,8               | B         | 4+0,2d  | 9,5                  | 28,6                        |
| Circuit 2      | 0             | 0              |                    | 0         |         |                      |                             |
| Bliksemdraad 1 | 1             | 2              | 9,6                | A         | 15+0,4d | 23,7                 | 23,7                        |
| Bliksemdraad 2 | 0             | 0              |                    | 0         |         |                      |                             |

#### Isolatoren

| Geleider | $G_{isolator}$<br>[kN] | Aantal | $F_{v,iso}$<br>[kN] | Lengte<br>[m] | Windopp.<br>[m <sup>2</sup> ] | Windhoogte<br>[m] | Stuwdruk<br>[kN/m <sup>2</sup> ] | Vormfactor<br>[-] | $F_{h,iso}$<br>[kN] |
|----------|------------------------|--------|---------------------|---------------|-------------------------------|-------------------|----------------------------------|-------------------|---------------------|
| 380ct1f1 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 62,75             | 1,20                             | 1,2               | 3,47                |
| 380ct1f2 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 62,75             | 1,20                             | 1,2               | 3,47                |
| 380ct1f3 | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | 74,75             | 1,26                             | 1,2               | 3,62                |
| 0ct2f1   | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | -1,75             | 0,49                             | 1,2               | 1,42                |
| 0ct2f2   | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | -1,75             | 0,49                             | 1,2               | 1,42                |
| 0ct2f3   | 5,60                   | 1      | 5,6                 | 4,5           | 2,4                           | -1,75             | 0,49                             | 1,2               | 1,42                |
| bl1      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 80,90             | 1,28                             | 1,2               | 0,15                |
| bl2      | 0,10                   | 1      | 0,1                 | 0,2           | 0,1                           | 0,40              | 0,49                             | 1,2               | 0,06                |

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 Number: 72N

**Windbelasting back**

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f2 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f3 | 64,2   | 1,21                 | 0,64           | 0,64          | 1,04  | 28,25         | 67,9  | 67,9        | 46,9              | 130,2       | 130,2           |
| Oct2f1   |        |                      |                |               |       |               |       |             |                   |             |                 |
| Oct2f2   |        |                      |                |               |       |               |       |             |                   |             |                 |
| Oct2f3   |        |                      |                |               |       |               |       |             |                   |             |                 |
| bl1      | 72,5   | 1,25                 | 0,65           | 0,65          | 1,16  | 22,24         | 20,8  | 20,8        | 63,1              | 61,0        | 61,0            |
| bl2      |        |                      |                |               |       |               |       |             |                   |             |                 |

**Windbelasting ahead**

| Geleider | hoogte |                      | $G_{c\_dwars}$ | $G_{c\_trek}$ | $C_c$ | $d_{toeslag}$ | $w_y$ | $w_{y,vak}$ | $D_{ijs,toeslag}$ | $w_{y,ijs}$ | $w_{y,ijs,vak}$ |
|----------|--------|----------------------|----------------|---------------|-------|---------------|-------|-------------|-------------------|-------------|-----------------|
|          | wind   | Stuwdruk             |                |               |       |               |       |             |                   |             |                 |
|          | [m]    | [kN/m <sup>2</sup> ] | [-]            | [-]           | [-]   | [mm]          | [N/m] | [N/m]       | [mm]              | [N/m]       | [N/m]           |
| 380ct1f1 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f2 | 52,2   | 1,15                 | 0,62           | 0,62          | 1,06  | 28,25         | 63,8  | 63,8        | 46,9              | 120,4       | 120,4           |
| 380ct1f3 | 64,2   | 1,21                 | 0,64           | 0,64          | 1,04  | 28,25         | 67,9  | 67,9        | 46,9              | 130,2       | 130,2           |
| Oct2f1   |        |                      |                |               |       |               |       |             |                   |             |                 |
| Oct2f2   |        |                      |                |               |       |               |       |             |                   |             |                 |
| Oct2f3   |        |                      |                |               |       |               |       |             |                   |             |                 |
| bl1      | 72,5   | 1,25                 | 0,65           | 0,65          | 1,16  | 22,24         | 20,8  | 20,8        | 63,1              | 61,0        | 61,0            |
| bl2      |        |                      |                |               |       |               |       |             |                   |             |                 |

NB: belastingen  $w_v$  gelden voor bundel

Project: GT-RL380  
 Masttype: S+32 (bouw fase)  
 Mast: 72N

Auteur: TBR  
 Versie: v12.0

**Geleiderbelastingen**

**Uitgangspunten**  
 Betrouwbaarheidsniveau Nieuwbouw CC2  
 Referentieperiode 15 jaar

| <b>ULS</b> (bezwijksterkte)  |                           | <b>NEN-EN50341-2-15:2019</b> |              |                  |            |          |          |                     |
|--|---------------------------|------------------------------|--------------|------------------|------------|----------|----------|---------------------|
| Belastingsgeval  | omschrijving              | Temp<br>°C                   | $\gamma_G$   |                  | $\gamma_Q$ |          |          | $\gamma_a$<br>$A_k$ |
|  |                           |                              | $G_{k,mast}$ | $G_{k,geleider}$ | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ |                     |
| ULS 1a   | Wind                      | 10°                          | 1,20         | 1,20             | 0,00       | 1,25     | 0,00     | 0,0                 |
| ULS 1a_0,9   | Wind 0,9Gk alleen mast    | 10°                          | 0,90         | 1,20             | 0,00       | 1,25     | 0,00     | 0,0                 |
| ULS 1a_0,9_0,9   | Wind 0,9Gk ook geleider   | 10°                          | 0,90         | 0,90             | 0,00       | 1,25     | 0,00     | 0,0                 |
| ULS 3  | Wind+ijs                  | -5°                          | 1,20         | 1,20             | 0,00       | 0,38     | 1,07     | 0,0                 |
| ULS 3_0,9  | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20             | 0,00       | 0,38     | 1,07     | 0,0                 |
| ULS 4  | Koude+wind                | -20°                         | 1,20         | 1,20             | 0,00       | 0,25     | 0,00     | 0,0                 |
| ULS 4_0,9  | Koude+wind 0,9            | -20°                         | 0,90         | 1,20             | 0,00       | 0,25     | 0,00     | 0,0                 |
| ULS 5a   | Torsiebelastingen         | 10°                          | 1,00         | 1,00             | 1,00       | 0,00     | 0,00     | 1,0                 |
| ULS 5b   | Longitudinale belastingen | 10°                          | 1,00         | 1,00             | 0,00       | 0,00     | 0,00     | 1,0                 |
| ULS 6  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 1,50       | 0,25     | 0,00     | 0,0                 |
| ULS 6_0,9  | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 0,00       | 0,25     | 0,00     | 0,0                 |
| ULS 7  | Permanent                 | 10°                          | 1,35         | 1,35             | 0,00       | 0,00     | 0,00     | 0,0                 |
| ULS 8  | Special                   | 10°                          | 1,00         | 1,00             | 0,00       | 0,00     | 0,00     | 1,0                 |
| <b>SPLS</b> (Bezwijksterkte, enkel voor hoekmasten: afwezigheid geleiders) |                           |                              |              | $\gamma_G$       | $\gamma_Q$ |          |          |                     |
|  |                           |                              | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SPLS 1a  | Wind                      | 10°                          | 1,20         | 1,20             | 0,0        | 0,78     | 0,00     | 0,0                 |
| SPLS 1a_0,9  | Wind 0,9                  | 10°                          | 0,90         | 1,20             | 0,0        | 0,78     | 0,00     | 0,0                 |
| SPLS 1a_0,9_0,9  | Wind 0,9                  | 10°                          | 0,90         | 0,90             | 0,0        | 0,78     | 0,00     | 0,0                 |
| SPLS 3   | Wind+ijs                  | -5°                          | 1,20         | 1,20             | 0,0        | 0,36     | 0,34     | 0,0                 |
| SPLS 3_0,9   | Wind+ijs 0,9              | -5°                          | 0,90         | 1,20             | 0,0        | 0,36     | 0,34     | 0,0                 |
| SPLS 4   | Koude+wind                | -20°                         | 1,20         | 1,20             | 0,0        | 0,24     | 0,00     | 0,0                 |
| SPLS 4_0,9   | Koude+wind 0,9            | -20°                         | 0,90         | 1,20             | 0,0        | 0,24     | 0,00     | 0,0                 |
| SPLS 6   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 1,2        | 0,24     | 0,0      | 0,0                 |
| SPLS 6_0,9   | Bouw en onderhoud         | 5°                           | 1,20         | 1,20             | 0,0        | 0,24     | 0,0      | 0,0                 |
| <b>SLS</b> (controle van de vervormingen, vermoeiing, EDS)                 |                           |                              | $\gamma_G$   |                  | $\gamma_Q$ |          |          |                     |
|  |                           |                              | $G_k$        | $G_k$            | $Q_{pk}$   | $Q_{wk}$ | $Q_{ik}$ | $A_k$               |
| SLS 1a   | Wind                      | 10°                          | 1,00         | 1,00             | 0,0        | 0,87     | 0,0      | 0,0                 |
| SLS 3  | Wind+ijs                  | -5°                          | 1,00         | 1,00             | 0,0        | 0,26     | 0,71     | 0,0                 |
| SLS 4  | Wind                      | -20°                         | 1,00         | 1,00             | 0,0        | 0,17     | 0,0      | 0,0                 |
| SLS 6  | Bouw en onderhoud         | 5°                           | 1,00         | 1,00             | 0,0        | 0,17     | 0,0      | 0,0                 |
| SLS 7  | PB (EDS, geen wind)       | 10°                          | 1,00         | 1,00             | 0,0        | 0,00     | 0,0      | 0,0                 |

Aantal windrichtingen 6  
 Aantal belastingcombinaties ULS 54  
 Aantal belastingcombinaties SPLS 0  
 Aantal belastingcombinaties SLS 15  
 Aantal knooplasten 552

Project: GT-RLL380  
 Masttype: S+32 (bouwfase)  
 Mast: 72N

### Samenvattingstabellen geleiderbelastingen

In de onderstaande vier tabellen is weergegeven:

- De maximale geleiderbelasting in het globale assenstelsel, gesplitst in aandeel van back en ahead span
- De gecombineerde geleiderbelasting (Ba+Ah) in het globale assenstelsel met in het lokale assenstelsel de maximaal optredende trekkracht. Componenten Fx en Fy als absolute waarde
- De alledaagse (EDS) waarden van de gecombineerde geleiderbelastingen (Ba+Ah) met bijbehorende trekkrachten
- Controle op uplift, waar een negatieve waarde duidt op uplift

#### Maximale waarden voor back en ahead span

| Geleider | Fx_ba<br>[kN] | Fx_ah<br>[kN] | Fy_ba<br>[kN] | Fy_ah<br>[kN] | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------|---------------|---------------|---------------|---------------|---------------|---------------|
| bl1      | -52,2         | 52,2          | 5,3           | 5,3           | 11,1          | 6,9           |
| bl2      | 0,0           | 0,0           | 0,0           | 0,0           | 0,8           | 0,8           |
| 380ct1f1 | -144,7        | 144,7         | 18,2          | 18,2          | 32,1          | 20,5          |
| 380ct1f2 | -144,7        | 144,7         | 18,2          | 18,2          | 32,1          | 20,5          |
| 380ct1f3 | -146,9        | 146,9         | 19,3          | 19,3          | 32,2          | 20,5          |
| Oct2f1   | -0,2          | 0,2           | 0,9           | 0,9           | 4,1           | 4,1           |
| Oct2f2   | -0,2          | 0,2           | 0,9           | 0,9           | 4,1           | 4,1           |
| Oct2f3   | -0,2          | 0,2           | 0,9           | 0,9           | 4,1           | 4,1           |

#### Min. Weight span (m)

Weight spar Combinatie1

| Geleider | SLS 1a | SLS 4 | SLS 7 |
|----------|--------|-------|-------|
| bl1      | 528,0  | 550,6 | 528,0 |
| bl2      | 0,0    | 0,0   | 0,0   |
| 380ct1f1 | 528,0  | 545,5 | 528,0 |
| 380ct1f2 | 528,0  | 545,5 | 528,0 |
| 380ct1f3 | 528,0  | 545,9 | 528,0 |
| Oct2f1   | 0,0    | 0,0   | 0,0   |
| Oct2f2   | 0,0    | 0,0   | 0,0   |
| Oct2f3   | 0,0    | 0,0   | 0,0   |

#### Max. Weight span (m)

Weight spar Combinatie1

| Geleider | ULS 1a | ULS 3 |
|----------|--------|-------|
| bl1      | 664,9  | 521,5 |
| bl2      | 0,0    | 0,0   |
| 380ct1f1 | 603,0  | 535,2 |
| 380ct1f2 | 603,0  | 535,2 |
| 380ct1f3 | 610,5  | 537,2 |
| Oct2f1   | 0,0    | 0,0   |
| Oct2f2   | 0,0    | 0,0   |
| Oct2f3   | 0,0    | 0,0   |

Omhullende weight span over alle combinaties (incl. 0,9 combinaties)

Voor alle geleiders

Max. weight span 664,9 m  
 Min. weight span 0,0 m

Wind / Weight span verhouding

1,662 -  
 0,000 -

Project: GT-RLL380  
 Masttype: S+32 (bouwfase)  
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**Maximale waarden back+ahead span      Maximale waarden trekkracht geleider**

| Geleider | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN] | Ft_ah<br>[kN] |
|----------|------------|------------|------------|---------------|---------------|
| bl1      | 22,9       | 10,6       | 18,0       | -52,2         | 52,2          |
| bl2      | 0,1        | 0,1        | 1,6        | 0,0           | 0,0           |
| 380ct1f1 | 58,7       | 36,3       | 52,6       | -144,7        | 144,7         |
| 380ct1f2 | 58,7       | 36,3       | 52,6       | -144,7        | 144,7         |
| 380ct1f3 | 58,7       | 38,6       | 52,7       | -146,9        | 146,9         |
| Oct2f1   | 0,4        | 1,8        | 8,2        | 0,0           | 0,0           |
| Oct2f2   | 0,4        | 1,8        | 8,2        | 0,0           | 0,0           |
| Oct2f3   | 0,4        | 1,8        | 8,2        | 0,0           | 0,0           |

**EDS-belastingen geleiders**

| Geleider | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Ft_ba<br>[kN] | Ft_ah<br>[kN] |
|----------|------------|------------|------------|---------------|---------------|
| bl1      | 0,0        | 0,0        | 5,1        | -15,3         | 15,3          |
| bl2      | 0,0        | 0,0        | 0,1        | 0,0           | 0,0           |
| 380ct1f1 | 0,0        | 0,0        | 29,8       | -73,3         | 73,3          |
| 380ct1f2 | 0,0        | 0,0        | 29,8       | -73,3         | 73,3          |
| 380ct1f3 | 0,0        | 0,0        | 29,8       | -73,3         | 73,3          |
| Oct2f1   | 0,0        | 0,0        | 5,6        | 0,0           | 0,0           |
| Oct2f2   | 0,0        | 0,0        | 5,6        | 0,0           | 0,0           |
| Oct2f3   | 0,0        | 0,0        | 5,6        | 0,0           | 0,0           |

**Controle uplift SLS-wind**

| Combinatie: Geleider | Fz_ba<br>[kN] | Fz_ah<br>[kN] |
|----------------------|---------------|---------------|
| SLS 4                |               |               |
| bl1                  | 3,4           | 2,0           |
| bl2                  | 0,1           | 0,1           |
| 380ct1f1             | 18,6          | 12,0          |
| 380ct1f2             | 18,6          | 12,0          |
| 380ct1f3             | 18,7          | 12,0          |
| Oct2f1               | 2,8           | 2,8           |
| Oct2f2               | 2,8           | 2,8           |
| Oct2f3               | 2,8           | 2,8           |

Project: GT-RLL380  
 Masttype: S+32 (bouwfase)  
 Mast: 72N

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, vanuit geleiders**

| Combinatie        | Combination | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|-------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         |             | 0             | 127           | 148           | 6729           | 0              | 0              |
| ULS 1a_0,9_0      |             | 5             | 0             | 111           | -1250          | 242            | -48            |
| ULS 1a_0,9_0,9_90 |             | 0             | 127           | 83            | 7556           | 0              | 0              |
| ULS 3_0           |             | 1             | 0             | 192           | -2407          | 73             | -14            |
| SLS 7             |             | 0             | 0             | 111           | -1302          | 0              | 0              |

**ULS-fundatiebelasting combinatie 1 en 3 wind haaks op de lijn of bissectrice en EDS, totaal geleiders en mast**

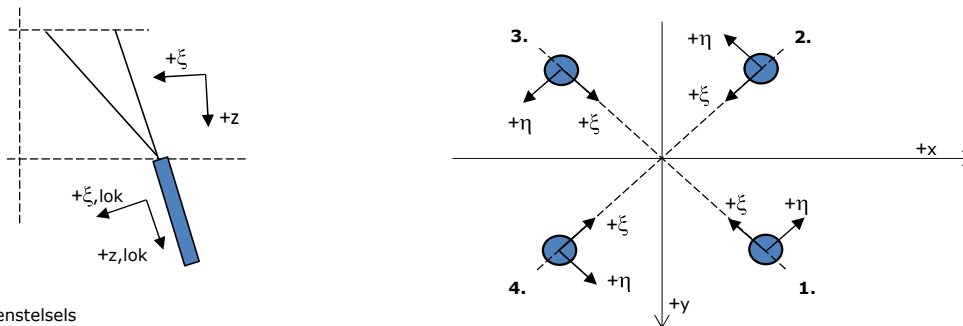
| Combinatie        | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|-------------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_90         | 0             | 540           | 993           | 24916          | 0              | 0              |
| ULS 1a_0,9_0,9_90 | 0             | 540           | 717           | 25743          | 0              | 0              |
| SLS 7             | 0             | 0             | 815           | -1302          | 0              | 0              |

**Fundatiebelastingen, selectie belastingcombinaties op basis grootste waarde**

| Combinatie | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|------------|---------------|---------------|---------------|----------------|----------------|----------------|
| ULS 1a_270 | 0             | -540          | 993           | <b>-28445</b>  | 0              | 0              |
| ULS 1a_0   | 507           | 0             | 978           | -1556          | <b>25139</b>   | -48            |
| ULS 8 Ah   | 86            | 0             | 854           | -1839          | 6155           | <b>-1273</b>   |
| ULS 1a_225 | -390          | -454          | 983           | <b>-24285</b>  | <b>-18393</b>  | 34             |

*Noot: grootste waarden kunnen in meerdere combinaties voorkomen, een combinatie is weergegeven.*

**Oplegreacties op fundering per randstijl**



Assenstelsels

**Maximale drukbelasting**

| Stijl | Combinatie | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_45  | 279           | 279           | <b>1587</b>   | 0                | -394            | -9                    | 1633                |
| 2     | ULS 1a_270 | 230           | -182          | <b>1216</b>   | -34              | -291            | 4                     | 1251                |
| 3     | ULS 1a_225 | -301          | -278          | <b>1697</b>   | 16               | -409            | 3                     | 1747                |
| 4     | ULS 1a_135 | -279          | 279           | <b>1587</b>   | 0                | -394            | -9                    | 1633                |

**Maximale trekbelasting**

| Stijl | Combinatie         | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 1a_0,9_225     | -215          | -197          | <b>-1253</b>  | -13              | 292             | -13                   | -1289               |
| 2     | ULS 1a_0,9_0,9_135 | -204          | 197           | <b>-1185</b>  | 5                | 284             | -4                    | -1220               |
| 3     | ULS 1a_0,9_0,9_45  | 204           | 197           | <b>-1185</b>  | -5               | 284             | -4                    | -1220               |
| 4     | ULS 1a_0,9_270     | 144           | -100          | <b>-764</b>   | 31               | 173             | -13                   | -786                |

**Maximale torsiebelasting (positief)**

| Stijl | Combinatie        | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|-------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 8 Ba          | 29            | -21           | -58           | <b>35</b>        | -6              | -20                   | -60                 |
| 2     | ULS 1a_0,9_0,9_45 | -8            | -38           | 66            | <b>32</b>        | -21             | -5                    | 68                  |
| 3     | ULS 1a_270        | -230          | -182          | 1216          | <b>34</b>        | -291            | 4                     | 1251                |
| 4     | ULS 8 Ba          | -28           | 102           | 360           | <b>52</b>        | -92             | -4                    | 371                 |

**Maximale torsiebelasting (negatief)**

| Stijl | Combinatie         | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| 1     | ULS 8 Ah           | 28            | 102           | 360           | <b>-52</b>       | -92             | -4                    | 371                 |
| 2     | ULS 1a_225         | 104           | -42           | 446           | <b>-44</b>       | -104            | 5                     | 459                 |
| 3     | ULS 1a_0,9_0,9_135 | 8             | -38           | 66            | <b>-32</b>       | -21             | -5                    | 68                  |
| 4     | ULS 8 Ah           | -29           | -21           | -58           | <b>-35</b>       | -6              | -20                   | -60                 |

Project: GT-RLL380  
 Masttype: S+32 (bouwfase)  
 Mast: 72N

#### Combinatie Ftrek+Fhor

| Stijl | Combinatie         | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | ULS 1a_0,9_225     | -215                   | -197                   | <b>-1253</b>           | <b>-13</b>             | 292                    | -13                        | -1289                      |
| 2     | ULS 1a_0,9_0,9_135 | -204                   | 197                    | <b>-1185</b>           | <b>5</b>               | 284                    | -4                         | -1220                      |
| 3     | ULS 1a_0,9_0,9_45  | 204                    | 197                    | <b>-1185</b>           | <b>-5</b>              | 284                    | -4                         | -1220                      |
| 4     | ULS 1a_0,9_270     | 144                    | -100                   | <b>-764</b>            | <b>31</b>              | 173                    | -13                        | -786                       |

#### Permanente belasting

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 30                     | 39                     | 160                    | -6                     | -49                    | -10                        | 164                        |
| 2     | SLS 7      | 47                     | -39                    | 248                    | -6                     | -60                    | 0                          | 255                        |
| 3     | SLS 7      | -47                    | -39                    | 248                    | 6                      | -60                    | 0                          | 255                        |
| 4     | SLS 7      | -30                    | 39                     | 160                    | 6                      | -49                    | -10                        | 164                        |

#### Omhullenden ongeacht stijl

| Belasting         | Combinatie     | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|----------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | ULS 1a_225     | -301                   | -278                   | <b>1697</b>            | 16                     | -409                   | 3                          | 1747                       |
| Max. trek         | ULS 1a_0,9_225 | -215                   | -197                   | <b>-1253</b>           | -13                    | 292                    | -13                        | -1289                      |
| Max. pos. torsie  | ULS 8 Ba       | -28                    | 102                    | 360                    | <b>52</b>              | -92                    | -4                         | 371                        |
| Max. neg. torsie  | ULS 8 Ah       | 28                     | 102                    | 360                    | <b>-52</b>             | -92                    | -4                         | 371                        |
| Comb. trek+torsie | ULS 1a_0,9_225 | -215                   | -197                   | <b>-1253</b>           | <b>-13</b>             | 292                    | -13                        | -1289                      |

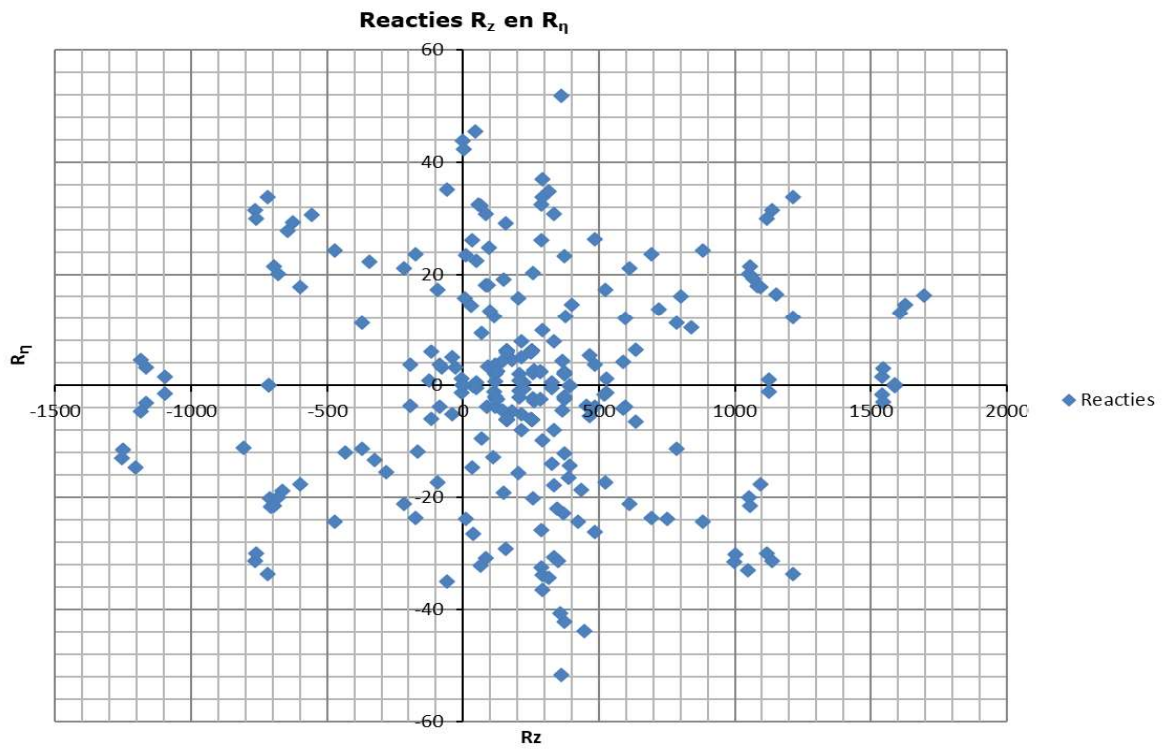
#### Maximale trekbelasting SLS

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 7      | 30                     | 39                     | <b>160</b>             | -6                     | -49                    | -10                        | 164                        |
| 2     | SLS 1a_135 | -121                   | 121                    | <b>-715</b>            | 0                      | 171                    | -2                         | -736                       |
| 3     | SLS 1a_45  | 121                    | 121                    | <b>-715</b>            | 0                      | 171                    | -2                         | -736                       |
| 4     | SLS 1a_0   | 57                     | -74                    | <b>-432</b>            | -12                    | 92                     | -13                        | -444                       |

#### Maximale drukbelasting SLS

| Stijl | Combinatie | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>η</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| 1     | SLS 1a_45  | 198                    | 199                    | <b>1124</b>            | -1                     | -281                   | -8                         | 1157                       |
| 2     | SLS 1a_0   | 135                    | -150                   | <b>839</b>             | 10                     | -201                   | 3                          | 864                        |
| 3     | SLS 7      | -47                    | -39                    | <b>248</b>             | 6                      | -60                    | 0                          | 255                        |
| 4     | SLS 1a_135 | -198                   | 199                    | <b>1124</b>            | 1                      | -281                   | -8                         | 1157                       |

Project: GT-RLL380  
Masttype: S+32 (bouwfase)  
Mast: 72N







## Dynamische factor CsCd

Masttype S+32\_n is hoger dan 60 m en daardoor moet de dynamische factor berekend worden.

De procedure van NEN-EN 50341-2-15 artikel 4.4.3.1 is gevolgd.

Gemiddelde breedte is genomen op het niveau van de ondertraverse: 3,5 m.

Hoogte van de mast voor de turbulentie-intensiteit is genomen op 60% van de hoogte volgens NEN-EN 1991-1-4 clause 6.3.1.

Voor de resonantiefactor  $R^2$  zijn de volgende uitgangspunten gebruikt:

Logaritmische demping volgens NEN-EN 1991-1-4 Appendix F: "stalen Bruggen en vakwerktorens, bouten met hoge kwaliteit":  $\delta_s = 0,030$ .

Equivalenten massa  $m_e$  is genomen als de massa per eenheid van lengte. Deze is berekend door het mastgewicht te delen door de totale hoogte.

Factoren  $K_y$  and  $K_z$  op basis van parabolische vervormingslijn.

$$G_y = 1/2$$

$$G_z = 5/18$$

De drag coefficient is genomen als het product van het product of  $\chi$  (solidity ratio) en  $C_t$  (drag factor voor een open vakwerk).  $C_t = 0,24 \times 2,8 = 0,67$ .

Peak factor is gezet op 3,5 volgens NEN-EN 50341-2-15.

Zie verder uitvoer.

De berekende waarde voor  $c_{scd}$  bedraagt 1,05.

**Bouwwerfactor  $c_s c_d$**

$$c_s c_d = 1 + 2 k_p l_v(z_s) \sqrt{(B^2 + R^2)} / 1 + 7 l_v(z) \quad 1,05 -$$

$k_p$  piekfactor

$l_v$  turbulentieintensiteit 0,166051

$B^2$  achtergrondresponsiefactor, brengt het volledige gebrek aan correlatie in rekening

$R^2$  resonantieresponsfactor

$z_s$  referentiehoogte, temnminste gelijk aan  $z_{min}$

Piekfactor  $k_p$

$$k_p = \sqrt{2 \ln(vT)} + 0,6 / \sqrt{2 \ln(vT)} \geq 3,0 \quad 3,50 -$$

$T = 600$  s

$$v = n_1 \sqrt{R^2 / (B^2 + R^2)} \geq 0,08 \quad 0,56 -$$

Achtergrondresponsiefactor  $B^2$

$b = 3,50$  m

$d = 3,50$  m

$h = 82,5$  m

$z_s = h = 49,5$  m

$L(z_s) = L_t (z_s / z_t)^\alpha = 131,7$  m

$L_t = 300$  m (referentielengteschaal)

$z_t = 200$  m (referentiehoogte  $z_{max}$ )

$\alpha = 0,67 + 0,05 \ln(z_0) = 0,59$

$B^2 = 0,52$

Resonantieresponsfactor  $R^2$

$$R^2 = \pi^2 / 2 \delta \times S_L K_s = 0,7747$$

$$\delta = \delta_s + \delta_a + \delta_d = 0,05$$

Type constructie **Stalen toren, bout met hoge weerstand**

$\delta_s = 0,03$

$$\delta_a = c_f r b v_m(z_s) / 2 n_1 m_e = 0,01995$$

$c_f = 0,67$  (krachtcoefficient windrichting, solidity  $\times$  cf)

$n_1 = 0,73$  (eigenfrequentie, benaderd met  $f_e = 60 / h$ )

$m_e = 853,0$  (equivalente massa)

$\delta_d = 0,0$

$S_L = 0,0614765$  (dimensieloze spectrale dichtheidsfunctie)

$f_L = 3,3$

$K_s = 0,1276$  (afmetingsreductiefunctie)

$\Psi_y = 1,0$

$\Psi_z = 23,4$

$c_y = c_z = 11,5$

$G_y = 0,50$

$G_z = 0,28$

$K_y = 1$

$K_z = 1,67$

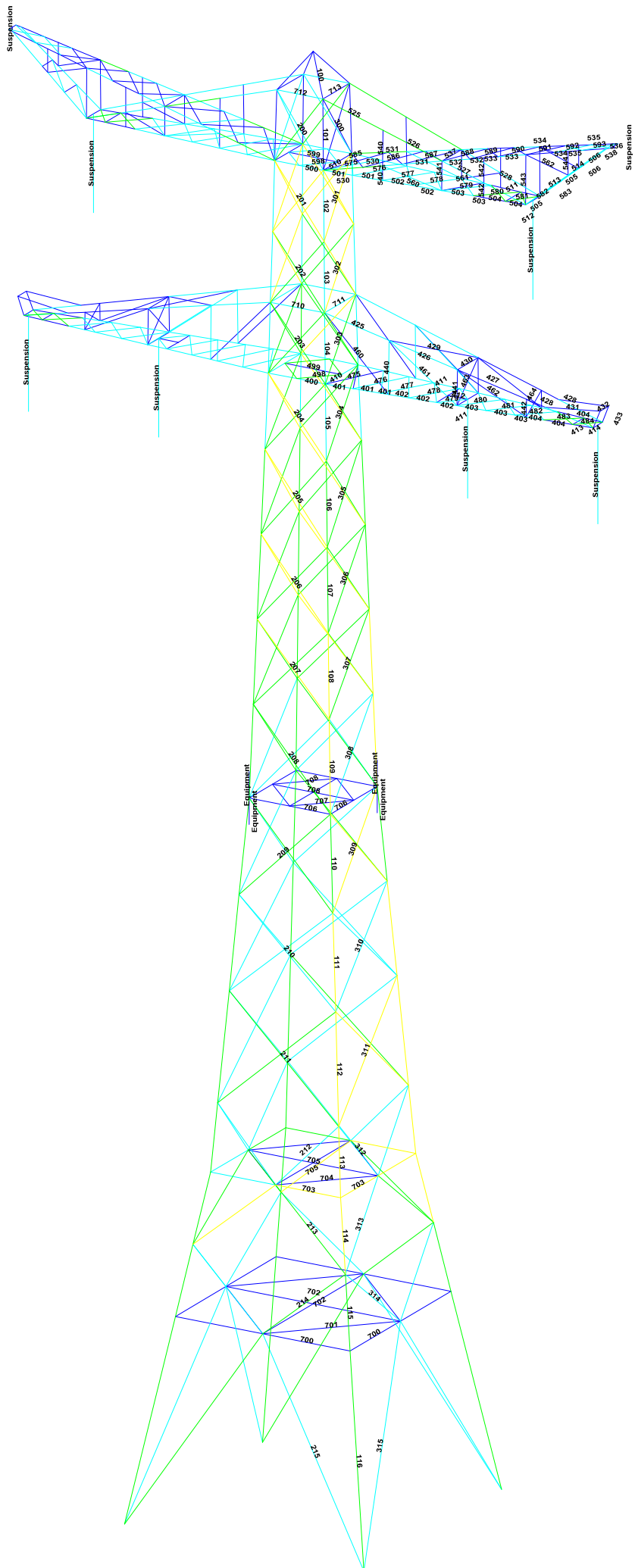


## **APPENDIX B**

### **Resultaten PLS tower**

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Deze Appendix bevat de resultaten voor de toetsing van profielen en bouten uit PLS Tower voor masttype S+32/n.







## APPENDIX C

### Knikverkorters

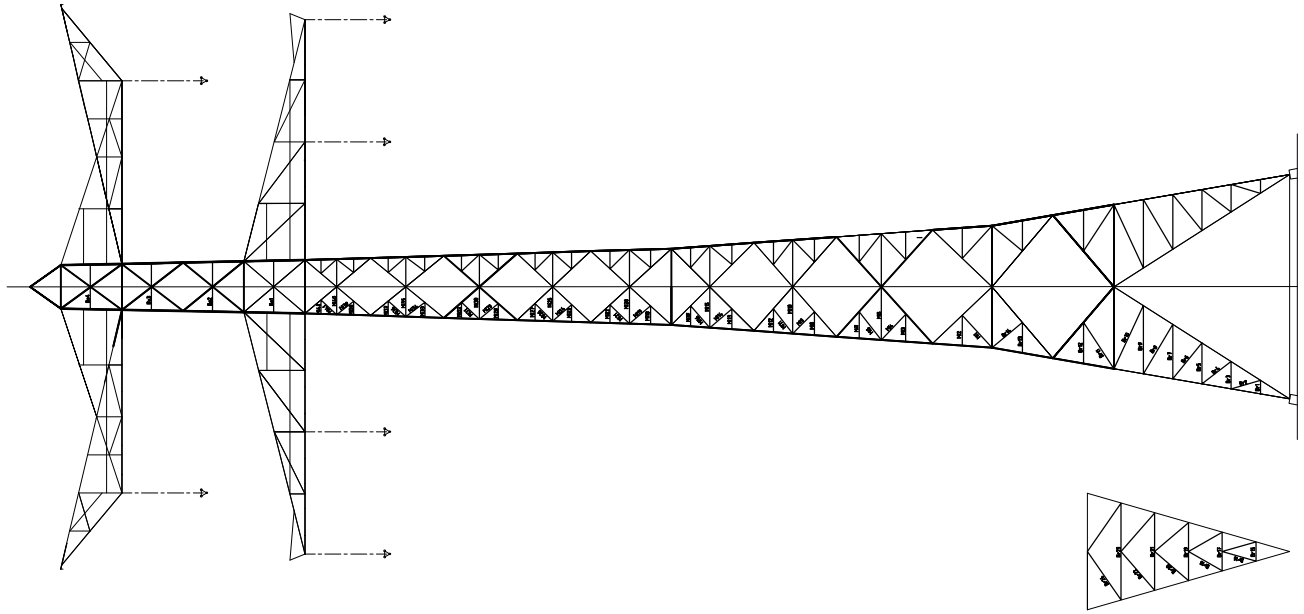
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Niet in PLS-TOWER gemodelleerde elementen in de constructie worden aanvullend getoetst. Hieronder vallen de knikverkorters van de randstijl en profielen onderdeel van stabiliteitsverbanden. De staven worden getoetst op:

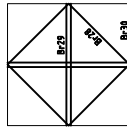
- voldoende trek- of druksterkte als steungevend profiel voor randstijl, 1% van de knikcapaciteit van de randstijl;
- slankheid;
- klimbelasting.

Profielen uit horizontaalverbanden van het onderstuk zijn in PLS-TOWER aanwezig maar worden in deze Appendix aanvullend getoetst op buiging. Profielafmeting en boutverbinding uit PLS-TOWER is leidend.

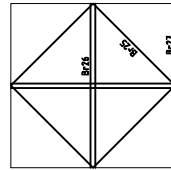
Overzicht knikverkorters - S-32\_n



Tussenschot +4,1m



Tussenschot +20m



Tussenschot +12m

De ondervlakken van de traverses worden niet weergegeven omdat daar geen knikverkorters aanwezig zijn. Voor de beloopbaarheid worden de traverses voorzien van kruip ladders.





**Redundant members**

Date: 2021-07-15  
 Author: JSN  
 Version: 1.9

GT-RLL  
 S+32\_n

| Posnr. | Section          | Schematization             | Profile | Steel Quality | Boft | Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Max. usage | Notes |
|--------|------------------|----------------------------|---------|---------------|------|---------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|------------|-------|
| Br1    | Broekstuk        | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 0.90       | 0         | 92           | 36.6              | 0.34         | 65.6               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.89         | Bearing    |       |
| Br2    | Broekstuk        | Enkele staaf               | L60x6   | S355J0        | M16  | 8.8     | 2.00       | 73        | 171          | 36.6              | 0.00         | 44.3               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.83         | Buckling   |       |
| Br3    | Broekstuk        | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 1.79       | 0         | 167          | 36.6              | 0.87         | 41.8               | 60.3                 | 51.5              | 75.3                  | 1.15              | 0.88         | Buckling   |       |
| Br4    | Broekstuk        | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 2.41       | 52        | 176          | 36.6              | 0.00         | 50.1               | 60.3                 | 52.3              | 122.3                 | 1.99              | 0.73         | Buckling   |       |
| Br5    | Broekstuk        | Enkele staaf               | L70x7   | S355J0        | M16  | 8.8     | 2.69       | 0         | 196          | 36.6              | 1.01         | 42.7               | 60.3                 | 52.3              | 122.3                 | 1.99              | 0.86         | Buckling   |       |
| Br6    | Broekstuk        | Enkele staaf               | L80x6   | S355J0        | M16  | 8.8     | 3.04       | 39        | 223          | 36.6              | 0.00         | 40.5               | 60.3                 | 61.0              | 142.7                 | 2.23              | 0.90         | Buckling   |       |
| Br7    | Broekstuk        | Enkele staaf               | L80x6   | S355J0        | M16  | 8.8     | 3.58       | 0         | 228          | 36.6              | 1.34         | 38.9               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.94         | Buckling   |       |
| Br8    | Broekstuk        | Enkele staaf               | L100x8  | S355J0        | M16  | 8.8     | 3.78       | 30        | 242          | 36.6              | 1.23         | 64.4               | 60.3                 | 69.7              | 194.4                 | 3.33              | 0.79         | Buckling   |       |
| Br9    | Broekstuk        | Enkele staaf               | L100x8  | S355J0        | M16  | 8.8     | 4.48       | 0         | 227          | 36.6              | 1.68         | 64.7               | 60.3                 | 69.7              | 257.2                 | 5.49              | 0.61         | shear      |       |
| Br10   | Broekstuk        | Enkele staaf               | L80x6   | S355J0        | M16  | 8.8     | 3.63       | 33        | 231          | 36.3              | 0.00         | 38.1               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.95         | Buckling   |       |
| Br11   | Broekstuk        | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 2.69       | 0         | 196          | 36.3              | 1.01         | 44.7               | 60.3                 | 52.3              | 122.3                 | 1.99              | 0.85         | Buckling   |       |
| Br12   | Broekstuk        | Enkele staaf               | L60x6   | S355J0        | M16  | 8.8     | 2.00       | 0         | 171          | 36.3              | 0.00         | 44.9               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.82         | Buckling   |       |
| Br13   | Broekstuk        | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 2.60       | 50        | 189          | 36.3              | 0.00         | 44.9               | 60.3                 | 52.3              | 122.3                 | 1.99              | 0.81         | Buckling   |       |
| Br14   | Broekstuk        | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.27       | 0         | 130          | 3.8               | 0.47         | 44.6               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.61         | Bending    |       |
| Br15   | Broekstuk        | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 2.30       | 74        | 236          | 3.8               | 0.00         | 18.9               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.20         | Buckling   |       |
| Br16   | Broekstuk        | Kniksteun op 0,5L          | L50x5   | S355J0        | M16  | 8.8     | 2.53       | 0         | 167          | 3.8               | 0.95         | 25.9               | 60.3                 | 41.3              | 43.1                  | 0.81              | 0.88         | Bending    |       |
| Br17   | Broekstuk        | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 2.55       | 60        | 238          | 3.8               | 0.00         | 24.5               | 60.3                 | 51.5              | 75.3                  | 1.15              | 0.15         | Buckling   |       |
| Br18   | Broekstuk        | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 3.80       | 0         | 229          | 3.8               | 1.43         | 22.0               | 60.3                 | 51.5              | 75.3                  | 1.15              | 0.15         | Buckling   |       |
| Br19   | Broekstuk        | Kniksteun op 0,5L          | L60x6   | S355J0        | M16  | 8.8     | 2.91       | 49        | 249          | 3.8               | 0.00         | 24.9               | 60.3                 | 52.3              | 98.8                  | 1.40              | 0.15         | Buckling   |       |
| Br20   | Broekstuk        | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 5.07       | 0         | 238          | 3.8               | 1.90         | 26.9               | 60.3                 | 52.3              | 122.3                 | 2.58              | 0.74         | Bending    |       |
| Br21   | Broekstuk        | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 3.36       | 41        | 245          | 3.8               | 0.00         | 30.1               | 60.3                 | 52.3              | 122.3                 | 1.99              | 0.13         | Buckling   |       |
| Br22   | Broekstuk        | Enkele staaf               | L90x8   | S355J0        | M16  | 8.8     | 6.33       | 0         | 231          | 3.8               | 2.38         | 47.9               | 60.3                 | 69.7              | 225.8                 | 5.70              | 0.42         | Bending    |       |
| Br23   | Broekstuk        | Enkele staaf               | L80x6   | S355J0        | M16  | 8.8     | 3.86       | 34        | 245          | 3.8               | 0.00         | 34.5               | 60.3                 | 52.3              | 145.8                 | 2.68              | 0.11         | Buckling   |       |
| Br24   | Broekstuk        | Enkele staaf               | L100x8  | S355J0        | M16  | 8.8     | 7.60       | 0         | 247          | 0.0               | 2.85         | 48.5               | 60.3                 | 69.7              | 257.2                 | 7.19              | 0.40         | Bending    | 1     |
| Br25   | Tussenschot +12m | Kniksteun op 0,5L          | L100x8  | S355J0        | M16  | 8.8     | 10.75      | 0         | 249          | 0.0               | 2.02         | 76.2               | 60.3                 | 87.1              | 360.6                 | 10.69             | 0.19         | Bending    | 1     |
| Br26   | Tussenschot +12m | Kruisende staaf halverwege | L110x10 | S355J0        | M16  | 8.8     | 5.37       | 0         | 249          | 0.0               | 2.02         | 76.2               | 60.3                 | 87.1              | 360.6                 | 8.0               | 0.26         | Bending    | 1     |
| Br27   | Tussenschot +12m | Enkele staaf               | L120x10 | S355J0        | M16  | 8.8     | 5.66       | 0         | 238          | 0.0               | 2.12         | 90.0               | 60.3                 | 87.1              | 399.8                 | 9.8               | 0.23         | Bending    | 1     |
| Br28   | Tussenschot +20m | Enkele staaf               | L120x10 | S355J0        | M16  | 8.8     | 8.00       | 0         | 254          | 0.0               | 1.50         | 32.6               | 60.3                 | 52.3              | 145.8                 | 3.4               | 0.44         | Bending    | 1, 2  |
| Br29   | Tussenschot +20m | Kruisende staaf halverwege | L80x6   | S355J0        | M16  | 8.8     | 4.00       | 0         | 157          | 0.0               | 1.50         | 216.9              | 60.3                 | 104.5             | 620.9                 | 13.4              | 0.12         | Bending    | 1     |
| Br30   | Tussenschot +20m | Enkele staaf               | L130x12 | S355J0        | M16  | 8.8     | 8.00       | 0         | 211          | 36.7              | 0.00         | 38.1               | 60.3                 | 52.3              | 122.3                 | 2.0               | 0.96         | Buckling   |       |
| M1     | Tussenstuk1      | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 2.90       | 42        | 171          | 36.7              | 0.75         | 44.3               | 60.3                 | 52.3              | 98.8                  | 1.4               | 0.83         | Buckling   |       |
| M2     | Tussenstuk1      | Enkele staaf               | L60x6   | S355J0        | M16  | 8.8     | 2.00       | 0         | 168          | 37.7              | 0.88         | 41.3               | 60.3                 | 51.5              | 75.3                  | 1.2               | 0.91         | Buckling   |       |
| M3     | Tussenstuk1      | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 2.32       | 43        | 169          | 37.7              | 0.00         | 53.0               | 60.3                 | 52.3              | 122.3                 | 2.0               | 0.72         | Bearing    |       |
| M4     | Tussenstuk1      | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 3.48       | 0         | 221          | 37.7              | 0.00         | 40.7               | 60.3                 | 52.3              | 145.8                 | 2.7               | 0.93         | Buckling   |       |
| M5     | Tussenstuk1      | Enkele staaf               | L80x6   | S355J0        | M16  | 8.8     | 2.36       | 38        | 172          | 37.7              | 0.85         | 51.7               | 60.3                 | 52.3              | 122.3                 | 2.0               | 0.73         | Buckling   |       |
| M6     | Tussenstuk1      | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 1.74       | 0         | 162          | 37.7              | 0.00         | 43.6               | 60.3                 | 51.5              | 75.3                  | 1.2               | 0.87         | Buckling   |       |
| M7     | Tussenstuk1      | Enkele staaf               | L60x6   | S355J0        | M16  | 8.8     | 1.74       | 0         | 138          | 37.7              | 0.85         | 34.6               | 60.3                 | 41.3              | 43.1                  | 0.5               | 0.85         | Buckling   |       |
| M8     | Tussenstuk1      | Enkele staaf               | L90x9   | S355J0        | M16  | 8.8     | 3.53       | 0         | 138          | 29.3              | 0.00         | 34.6               | 60.3                 | 51.5              | 75.3                  | 1.2               | 0.84         | Buckling   |       |
| M9     | Tussenstuk1      | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 2.05       | 45        | 229          | 29.3              | 0.00         | 34.8               | 60.3                 | 52.3              | 122.3                 | 2.0               | 0.84         | Buckling   |       |
| M10    | Tussenstuk1      | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 3.03       | 0         | 199          | 29.3              | 0.00         | 34.1               | 60.3                 | 52.3              | 145.8                 | 2.7               | 0.85         | Buckling   |       |
| M11    | Tussenstuk1      | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 2.06       | 38        | 199          | 29.3              | 0.00         | 34.1               | 60.3                 | 52.3              | 145.8                 | 2.7               | 0.85         | Buckling   |       |
| M12    | Tussenstuk1      | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.53       | 0         | 158          | 29.3              | 0.97         | 34.6               | 60.3                 | 41.3              | 43.1                  | 0.5               | 0.88         | Buckling   |       |
| M13    | Tussenstuk1      | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.34       | 0         | 138          | 29.3              | 0.50         | 41.5               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.71         | Bearing    |       |
| M14    | Tussenstuk1      | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 1.90       | 49        | 178          | 29.3              | 0.00         | 38.3               | 60.3                 | 51.5              | 75.3                  | 1.2               | 0.77         | Buckling   |       |
| M15    | Tussenstuk1      | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 2.68       | 0         | 195          | 29.3              | 0.00         | 42.9               | 60.3                 | 52.3              | 122.3                 | 2.0               | 0.68         | Buckling   |       |
| M16    | Tussenstuk1      | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 1.90       | 41        | 178          | 29.3              | 0.00         | 38.3               | 60.3                 | 52.3              | 75.3                  | 1.2               | 0.77         | Buckling   |       |
| M17    | Tussenstuk1      | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.34       | 0         | 138          | 29.3              | 0.50         | 41.5               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.71         | Bearing    |       |



## Redundant members

Date: 2021-07-15  
 Author: JSN  
 Version: 1.9

GT-RLL  
 S+32\_n

| Posnr. | Section     | Schematization             | Profile | Steel Quality | Boft | Quality | Length (m) | Angle (°) | Slender ness | Normal Force (kN) | Moment (kNm) | Buckling Cap. (kN) | Shear Cap. Bolt (kN) | Bearing Cap. (kN) | Net Section Cap. (kN) | Moment Cap. (kNm) | Highest U.C. | Max. usage | Notes |
|--------|-------------|----------------------------|---------|---------------|------|---------|------------|-----------|--------------|-------------------|--------------|--------------------|----------------------|-------------------|-----------------------|-------------------|--------------|------------|-------|
| M118   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.21       | 0         | 124          | 22.6              | 0.45         | 47.4               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.58         | Bending    |       |
| M119   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.80       | 49        | 185          | 22.6              | 0.00         | 27.5               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.82         | Buckling   |       |
| M120   | Tussenstuk2 | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 2.41       | 0         | 225          | 22.6              | 0.90         | 26.7               | 60.3                 | 51.5              | 75.3                  | 1.2               | 0.85         | Buckling   |       |
| M121   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.79       | 45        | 184          | 22.6              | 0.00         | 27.8               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.81         | Buckling   |       |
| M122   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.21       | 0         | 124          | 22.6              | 0.45         | 47.4               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.58         | Bending    |       |
| M123   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.13       | 0         | 116          | 23.0              | 0.42         | 51.4               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.56         | Bearing    |       |
| M124   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.65       | 48        | 170          | 23.0              | 0.00         | 31.2               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.74         | Buckling   |       |
| M125   | Tussenstuk2 | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 2.25       | 0         | 210          | 23.0              | 0.85         | 29.7               | 60.3                 | 51.5              | 75.3                  | 1.2               | 0.77         | Buckling   |       |
| M126   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.64       | 44        | 169          | 23.0              | 0.00         | 31.3               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.73         | Buckling   |       |
| M127   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.13       | 0         | 116          | 23.0              | 0.42         | 51.4               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.56         | Bearing    |       |
| M128   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.05       | 0         | 108          | 18.1              | 0.39         | 55.6               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.50         | Bearing    |       |
| M129   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.60       | 50        | 165          | 18.1              | 0.00         | 32.5               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.56         | Buckling   |       |
| M130   | Tussenstuk2 | Enkele staaf               | L55x6   | S355J0        | M16  | 8.8     | 2.11       | 0         | 197          | 18.1              | 0.79         | 33.0               | 60.3                 | 51.5              | 75.3                  | 1.2               | 0.71         | Bending    |       |
| M131   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.59       | 46        | 163          | 18.1              | 0.00         | 32.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.55         | Buckling   |       |
| M132   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.05       | 0         | 108          | 18.1              | 0.39         | 55.6               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.50         | Bearing    |       |
| M133   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 0.98       | 0         | 100          | 18.1              | 0.37         | 60.2               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.47         | Bending    |       |
| M134   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 0.98       | 0         | 100          | 18.1              | 0.37         | 60.2               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.50         | Bearing    |       |
| M135   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.56       | 53        | 160          | 18.1              | 0.00         | 33.7               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.54         | Buckling   |       |
| M136   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.96       | 0         | 201          | 18.1              | 0.73         | 24.3               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.93         | Bending    |       |
| M137   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.54       | 48        | 158          | 18.1              | 0.00         | 34.5               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.52         | Buckling   |       |
| M138   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 0.98       | 0         | 100          | 18.1              | 0.37         | 60.2               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.45         | Bearing    |       |
| M139   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 0.91       | 0         | 93           | 18.5              | 0.34         | 64.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.47         | Bending    |       |
| M140   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.42       | 52        | 145          | 18.5              | 0.00         | 38.6               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.48         | Buckling   |       |
| M141   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.81       | 0         | 186          | 18.5              | 0.68         | 27.1               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.87         | Bending    |       |
| M142   | Tussenstuk2 | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.40       | 47        | 144          | 18.5              | 0.00         | 39.3               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.45         | Bearing    |       |
| M143   | Tussenstuk2 | Enkele staaf               | L80x6   | S355J0        | M16  | 8.8     | 3.54       | 0         | 225          | 0.0               | 1.33         | 39.7               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.47         | Buckling   |       |
| M144   | Tussenstuk2 | Enkele staaf               | L70x6   | S355J0        | M16  | 8.8     | 3.99       | 0         | 255          | 0.0               | 1.33         | 64.9               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.45         | Bearing    |       |
| M145   | Tussenstuk2 | Kruisende staaf halverwege | L100x8  | S355J0        | M16  | 8.8     | 5.00       | 0         | 182          | 0.0               | 0.94         | 47.5               | 60.3                 | 52.3              | 145.8                 | 2.7               | 0.52         | Bending    | 1     |
| B01    | Bovenstuk1  | Kniksteun op 0,5L          | L100x8  | S355J0        | M16  | 8.8     | 5.00       | 0         | 162          | 0.0               | 1.88         | 86.9               | 60.3                 | 52.3              | 122.3                 | 2.6               | 0.36         | Bending    | 1     |
| B02    | Bovenstuk1  | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.70       | 0         | 175          | 8.8               | 0.64         | 29.9               | 60.3                 | 69.7              | 297.2                 | 7.2               | 0.26         | Bending    |       |
| B03    | Bovenstuk1  | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.62       | 0         | 166          | 8.8               | 0.61         | 32.0               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.81         | Bending    |       |
| B04    | Bovenstuk2  | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.54       | 0         | 158          | 5.8               | 0.58         | 34.4               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.74         | Bending    |       |
| B04    | Bovenstuk2  | Enkele staaf               | L50x5   | S355J0        | M16  | 8.8     | 1.46       | 0         | 150          | 5.5               | 0.55         | 37.0               | 60.3                 | 41.3              | 43.1                  | 0.8               | 0.70         | Bending    |       |

- Ook gecontroleerd in PLS-TOWER
- In werkelijkheid is de staaf korter omdat die verbonden is met een knooppunt. Daarom zal de slankheid in werkelijkheid niet groter zijn dan de maximale toelatenbare slankheid van 250.

## APPENDIX D

### Blokdeuvels

De belastingen op de fundatie uit Appendix A zijn uitgangspunt voor de berekening van de ingestorte rand met blokdeuvels. De belastingen in de richting van de randstijl zijn van toepassing. In de tabellen is dit opgenomen in de laatste kolom  $R_{z,lok}$ . De controles zijn uitgevoerd met een spreadsheet. Vanwege de helling van de drukdiagonaal wordt per krachtrichting bepaald hoeveel deuvels effectief zijn.

De belastingen waaraan getoetst worden zijn onderstaand weergegeven.

#### Masttype S+32/n

##### Omhullenden ongeacht stijl

| Belasting         | Combinatie         | $R_x$<br>[kN] | $R_y$<br>[kN] | $R_z$<br>[kN] | $R_\eta$<br>[kN] | $R_\xi$<br>[kN] | $R_{\xi,lok}$<br>[kN] | $R_{z,lok}$<br>[kN] |
|-------------------|--------------------|---------------|---------------|---------------|------------------|-----------------|-----------------------|---------------------|
| Max. druk         | ULS 1a_45          | 377           | 348           | <b>2130</b>   | 20               | -513            | 5                     | 2192                |
| Max. trek         | ULS 1a_0,9_0,9_45  | 289           | 260           | <b>-1667</b>  | -20              | 389             | -16                   | -1715               |
| Max. pos. torsie  | ULS 1a_0,9_0,9_45  | -55           | -25           | -155          | <b>57</b>        | 21              | -17                   | -159                |
| Max. neg. torsie  | ULS 1a_0,9_0,9_135 | 55            | -25           | -155          | <b>-57</b>       | 21              | -17                   | -159                |
| Comb. trek+torsie | ULS 1a_0,9_0,9_45  | 289           | 260           | <b>-1667</b>  | <b>-20</b>       | 389             | -16                   | -1715               |



Project: GT-RLL  
Mast: S+32\_n

**Shear blocks**

NEN-EN 1993-1-1 en NEN-EN 1994-1-1

Datum: 2021-07-15

Auteur: JSN

Versie: 1.4

| Load        |            |         | Results     |      |                |
|-------------|------------|---------|-------------|------|----------------|
| Compression | $F_{Ed,c}$ | 2192 kN | Compression | U.C. | 0.88 < 1,00 OK |
| Tension     | $F_{Ed,t}$ | 1715 kN | Tension     | U.C. | 0.69 < 1,00 OK |

**Main leg**

|                    |          |                       |
|--------------------|----------|-----------------------|
| Profile            |          | <b>L250.24</b>        |
| Steel material     |          | S355                  |
| Cross section      |          | 11467 mm <sup>2</sup> |
| Axial capacity     | $N_{pl}$ | 4071 kN               |
| Width              | $b$      | 250 mm                |
| Thickness          | $t$      | 24 mm                 |
| Length in concrete |          | 1500 mm               |

**Shear blocks main leg**

|                    |       |        |
|--------------------|-------|--------|
| Width              | $b$   | 50 mm  |
| Thickness          | $h$   | 30 mm  |
| Length             | $L$   | 250 mm |
| Welds              | $a$   | 5 mm   |
| c.t.c. separation  | $s$   | 200 mm |
| Number for compr.  | $n_c$ | 10 -   |
| Number for tension | $n_t$ | 10 -   |

**Foot plate**

|             |     |       |
|-------------|-----|-------|
| Thickness   | $t$ | 25 mm |
| Ext. length | $m$ | 30 mm |
| Welds       | $a$ | 5 mm  |

**Pile**

|                   |  |                       |
|-------------------|--|-----------------------|
| Name              |  | Buispaal              |
| Diameter          |  | 762 mm                |
| Thickness         |  | 10 mm                 |
| Cross section     |  | 23625 mm <sup>2</sup> |
| Steel material    |  | S355                  |
| Capacity          |  | 8387 kN               |
| Concrete strength |  | C30/37                |

**Shear blocks pile**

|                    |       |        |
|--------------------|-------|--------|
| Width              | $b$   | 50 mm  |
| Thickness          | $h$   | 30 mm  |
| Length             | $L$   | 250 mm |
| Welds              | $a$   | 5 mm   |
| c.t.c. separation  | $s$   | 500 mm |
| Number for compr.  | $n_c$ | 12 -   |
| Number for tension | $n_t$ | 12 -   |

**Design value concrete strength**

|                  |            |                        |
|------------------|------------|------------------------|
| Material factor  | $\gamma_c$ | 1.5                    |
| Add. mat. factor | $\gamma_m$ | 1.25 -                 |
| $f_{cd} =$       |            | 16.0 N/mm <sup>2</sup> |

**Steel tower stub**

|                  |            |                       |
|------------------|------------|-----------------------|
| Yield strength   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Tensile strength | $f_{ud} =$ | 490 N/mm <sup>2</sup> |

**Capacity shear blocks main leg**

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 7500 mm <sup>2</sup>   |
| $A_{f2} =$                                     | 18600 mm <sup>2</sup>  |
| Slope  | 1: 5                   |
| $C_A = \sqrt{A_{f2}/A_{f1}} =$                 | 1.57                   |
| $f_{jd} = C_A \times f_{cd} =$                 | 25.2 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | 1890 kN                |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | 1890 kN                |

**Capacity foot plate**

|   |                        |
|---|------------------------|
| $k_d =$                                 | 1.73 -                 |
| $f_{jd} = C_A \times f_{cd} =$          | 27.7 N/mm <sup>2</sup> |
| $c = t\sqrt{f_{yd} / 3f_{jd}} =$        | 54 mm                  |
| $m^* = \min(c,m) =$                     | 30 mm                  |
| Type foot plate                         | Extending              |
| Effective for                           | Compr. and tension     |
| $A_{p,c} =$                             | 45067 mm <sup>2</sup>  |
| $F_{Rd,c} = A_{p,druk} \times f_{jd} =$ | 1249 kN                |
| $A_{p,t} =$                             | 33600 mm <sup>2</sup>  |
| $F_{Rd,t} = A_{p,t} \times f_{jd} =$    | 931 kN                 |

**Capacities**

|   |                |
|---|----------------|
| $F_{rd,c,plate} =$                                      | 1197 kN        |
| $F_{rd,blocks,c} =$                                     | 1890 kN        |
| $F_{rd,c} = F_{rd,blk} + F_{rd,footplate} =$            | <b>3087 kN</b> |
| U.C. compression  | 0.71 < 1,00 OK |
| Welds foot plate (see next page)                        | 1197 kN        |
| $F_{rd,t} = \min. (\text{welds} / \text{foot plate}) =$ | 931 kN         |
| $F_{rd,blocks,t} =$                                     | 1890 kN        |
| $F_{rd,t} = F_{rd,blk} + F_{rd,footplate} =$            | <b>2821 kN</b> |
| U.C. tension  | 0.61 < 1,00 OK |
| U.C. welds  | 0.46 < 1,00 OK |

**Capacity shear blocks pile**

|  |                        |
|--|------------------------|
| $A_{f1} =$                                     | 7500 mm <sup>2</sup>   |
| $A_{f2} =$                                     | 22500 mm <sup>2</sup>  |
| $C_A = \sqrt{A_{f2}/A_{f1}} =$                 | 1.73 -                 |
| $f_{jd} = k_d \times f_{cd} =$                 | 27.7 N/mm <sup>2</sup> |
| $F_{Rd,c} = n_c \times A_{f1} \times f_{jd} =$ | <b>2494 kN</b>         |
| U.C. compression                               | 0.88 < 1,00 OK         |
| $F_{Rd,t} = n_t \times A_{f1} \times f_{jd} =$ | <b>2494 kN</b>         |
| U.C. tension                                   | 0.69 < 1,00 OK         |
| U.C. welds                                     | 0.42 < 1,00 OK         |

**"Splitting" of pile**

|                       |            |                       |
|-----------------------|------------|-----------------------|
| Spread of forces      |            | 45 °                  |
| Length force flow     |            | 1129 mm               |
| Splitting force       |            | 760 kN/m              |
| Yield strength wall   | $f_{yd} =$ | 355 N/mm <sup>2</sup> |
| Capacity tubular pile |            | 7100 kN/m             |
| U.C.                  |            | 0.11 < 1,00 OK        |

Project: GT-RLL  
Mast: S+32\_n

**Welds of shear blocks of main leg**

Out-of-plane loading

**Plate**

t = 50 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

**Member forces**

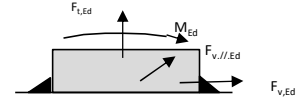
Factor 1.2  
F<sub>t,Ed</sub> = 0 kN  
F<sub>v,Ed</sub> = F<sub>rd,c</sub> / n = 227 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 3.40 kNm

**Check**

σ<sub>w,Ed</sub> = 199 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 99 N/mm<sup>2</sup> ≤

**Welds**

a = 5 mm  
l = 250 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



**Stress components**

σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 4al = 0 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 4al = 64 N/mm<sup>2</sup>  
64 N/mm<sup>2</sup>  
b\* = b + 2/3av2 = 54.7 mm  
σ<sub>1</sub> = τ<sub>1</sub> = 0,706M<sub>Ed</sub> / al b\* = 35 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>w,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 199 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.46 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.28 OK

**Welds of shear blocks of pile**

Out-of-plane loading

**Plate**

t = 50 mm  
Grade S355  
f<sub>yd</sub> = 355 N/mm<sup>2</sup>  
f<sub>u</sub> = 490 N/mm<sup>2</sup>

**Member forces**

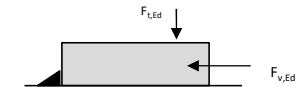
Factor 1.2  
F<sub>t,Ed</sub> = 1/2 b / h x F<sub>v,Ed</sub> = 75 kN  
F<sub>v,Ed</sub> = 249 kN  
F<sub>v//,Ed</sub> = 0 kN  
M<sub>Ed</sub> = 0.00 kNm

**Check**

σ<sub>w,Ed</sub> = 183 N/mm<sup>2</sup> ≤  
σ<sub>1</sub> = 92 N/mm<sup>2</sup> ≤

**Welds**

a = 5 mm  
l = 250 mm  
β<sub>w</sub> = 0.9 -  
γ<sub>M2</sub> = 1.25 -



**Stress components**

σ<sub>1</sub> = τ<sub>1</sub> = F<sub>t,Ed</sub> √2 / 2al = 21 N/mm<sup>2</sup>  
σ<sub>1</sub> = τ<sub>1</sub> = F<sub>v,Ed</sub> √2 / 2al = 71 N/mm<sup>2</sup>  
71 N/mm<sup>2</sup>  
τ<sub>//</sub> = F<sub>v//,Ed</sub> / 2al = 0 N/mm<sup>2</sup>  
σ<sub>w,Ed</sub> = √(σ<sub>1</sub><sup>2</sup> + 3τ<sub>1</sub><sup>2</sup> + 3τ<sub>//</sub><sup>2</sup>) = 183 N/mm<sup>2</sup>

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup> U.C. = 0.42 OK  
0,9f<sub>u</sub> / γ<sub>M2</sub> = 353 N/mm<sup>2</sup> U.C. = 0.26 OK

**Welds of foot plate**

f<sub>u</sub> / β<sub>w</sub> γ<sub>M2</sub> = 436 N/mm<sup>2</sup>  
Weld size a = 5 mm  
Length l = 2b + 2b - t = 952 mm  
Capacity F<sub>rd</sub> = a x l x f<sub>w,d</sub> / √3 = 1197 kN



## **APPENDIX E**

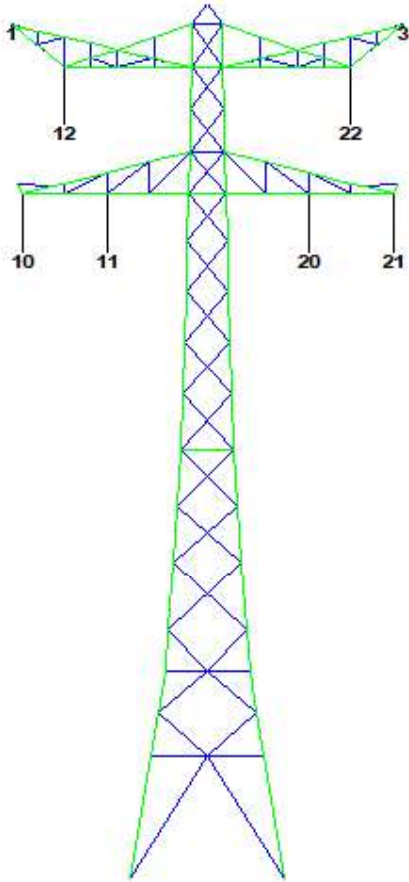
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### **Liggers**

De liggers uit HE-profiel voor de isolatoren zijn met het programma AxisVM op buiging gecontroleerd.

## 1 INTRODUCTION

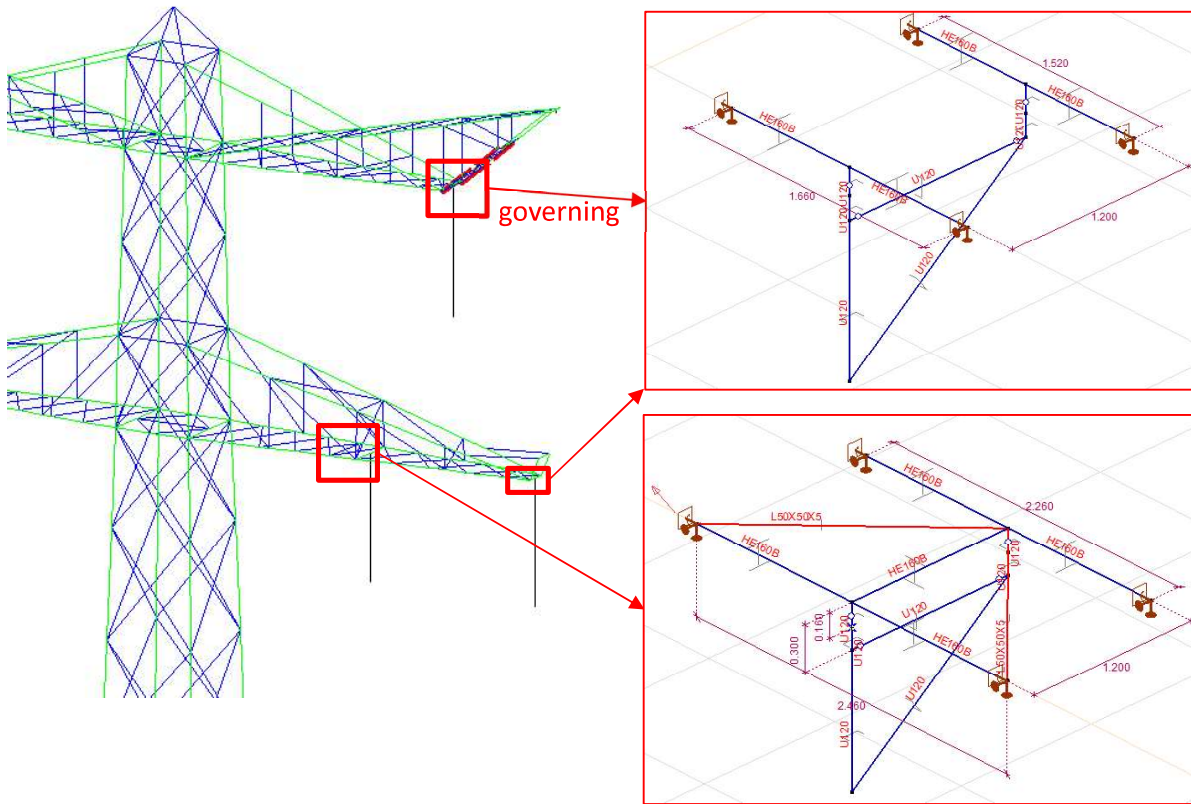
The beams for insulators of tower 2-circuit S+32\_n tower in the “ZWO-project” is investigated in the following report. The PLS-tower model of the tower with its insulator configuration is shown in Figure 1. The insulators are vertical suspension insulators that are attached via triangular assemblies, which lower the application point of the insulator to the cross arm.



**Figure 1 (a) S+32 PLS tower model**

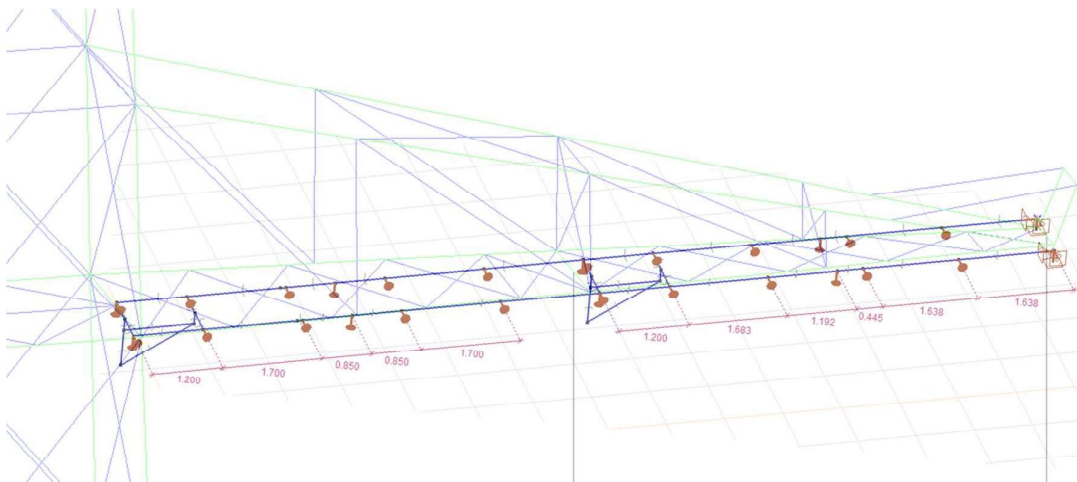
Figure 1 was taken from the PLS-Tower application for visualization. The insulators ID's: 10-12 and 20-22 are shown in black in the figure. The earth wire location is indicated by 1 and 3. The following report explores the effect of bending in the bottom chord of the cross-arms and beams housing the insulators for the S+32 tower. The report highlights the geometry and the loading on the cross arm. The parts of the tower are analysed in isolation with the rest of the tower body. The individual parts of the tower under focus are shown in Figure 2. Axis VM report is attached as “ Appendix – report AXIS-VM”.





**Figure 2 Location of the v-ketting insulator assembly in S+32 tower**

Figure 2 shows a side view of the location of the insulators supports in the cross-arms. The insulator support for 20 and 22 are governing. The insulator 21 has support scheme similar to insulator 21. The local axis VM models are shown in the right.

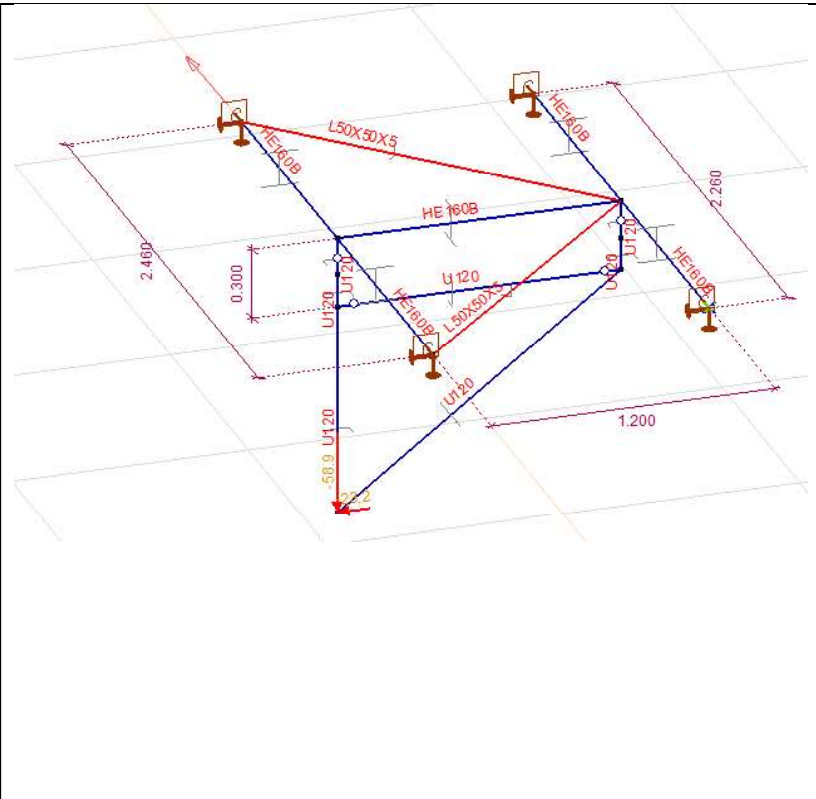
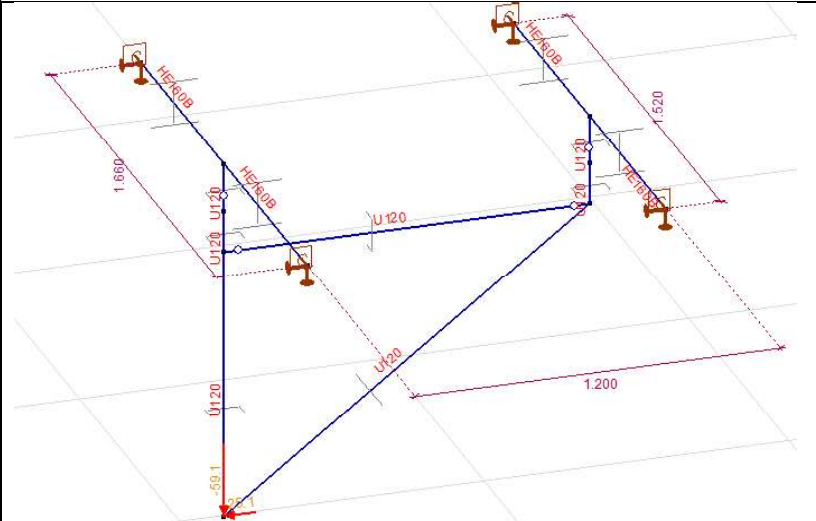


**Figure 3 Superimposed axis VM model on the tower image of the bottom cross arm**

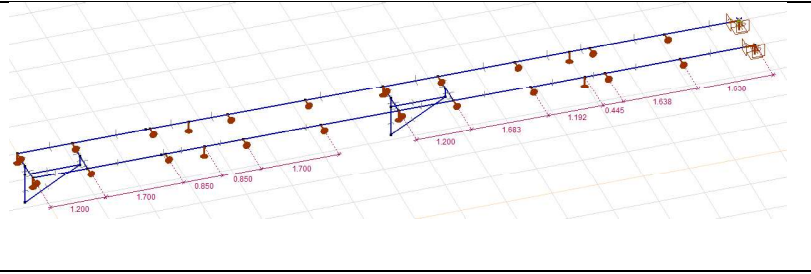
Figure 3 shows the simplified axisVM model of the bottom chord superimposed on the image of the cross arm from PLS tower pre processing. This is done to correlate the positions of the supports in the axis VM model explained in the later section. The upper cross arm has span smaller span the lower cross arm. Hence its not critical and thus not shown in the current report.

## 2 GEOMETRY

The details of the geometry of the individual parts are given in the table below.

|  |  |
|--|--|
| <p><b>Insulator 20:</b> The insulator is supported via a triangular assembly of UNP 120 sections. The longitudinal hinge is at a distance of 160 mm from the plane of bottom chord. Furthermore additional K brace (L50x5) and HEB 160 members is added between HEB members supported on the bottom chord. This is done to reduce the torsion in the beam. The lengths of the primary HEB beams at the bottom chord is taken from the PLS tower model. Supports are given at the end of the primary HEB beams for translation and torsion. This is done in consideration with the end plate connecting the HEB profile and bottom chord.</p> |   |
| <p><b>Insulator 22:</b> The beams housing the insulator are similar to insulator 20. Insulator 21 has similar supporting schemes.</p>  |  |

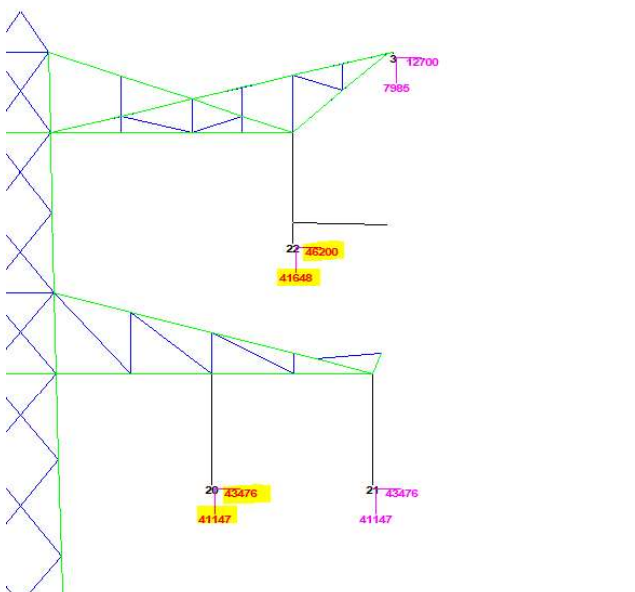
**Bottom chord:** The bottom chord is modelled in isolation. Horizontal supports are added at the location of horizontal braces. Vertical supports are given at the location of vertical in the cross arms.

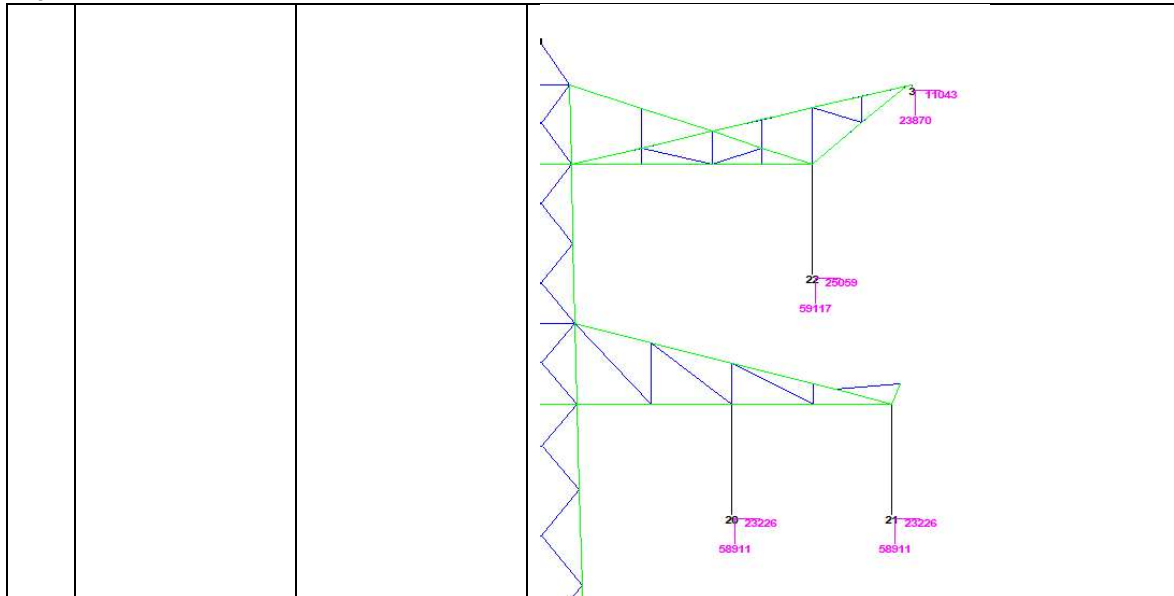


### 3 LOADING

The loads are applied in the Axis VM model for the critical load cases. The loads are in conjunction with the loads applied in the PLS Tower model for the existing model. The loads are applied at the tip of the insulator housing beams. The ID of the isolator is given in figure 2. The ID is matched with the PLS tower model. The ID of the isolators is used to identify and load the cross arms in Axis VM. The name of the load cases in the AxisVM model is also consistent with their counterparts in the PLS tower model. Load case 1 is the worst wind and self-weight of the cross arm. Load case 3 has loaded from both self-weight, wind and ice with relevant partial load factors. The conductor failure in conductor 20, 21 and 22 along with failure in earth conductor is simulated in Axis VM simulation. Table 2 shows the details of the individual load cases.

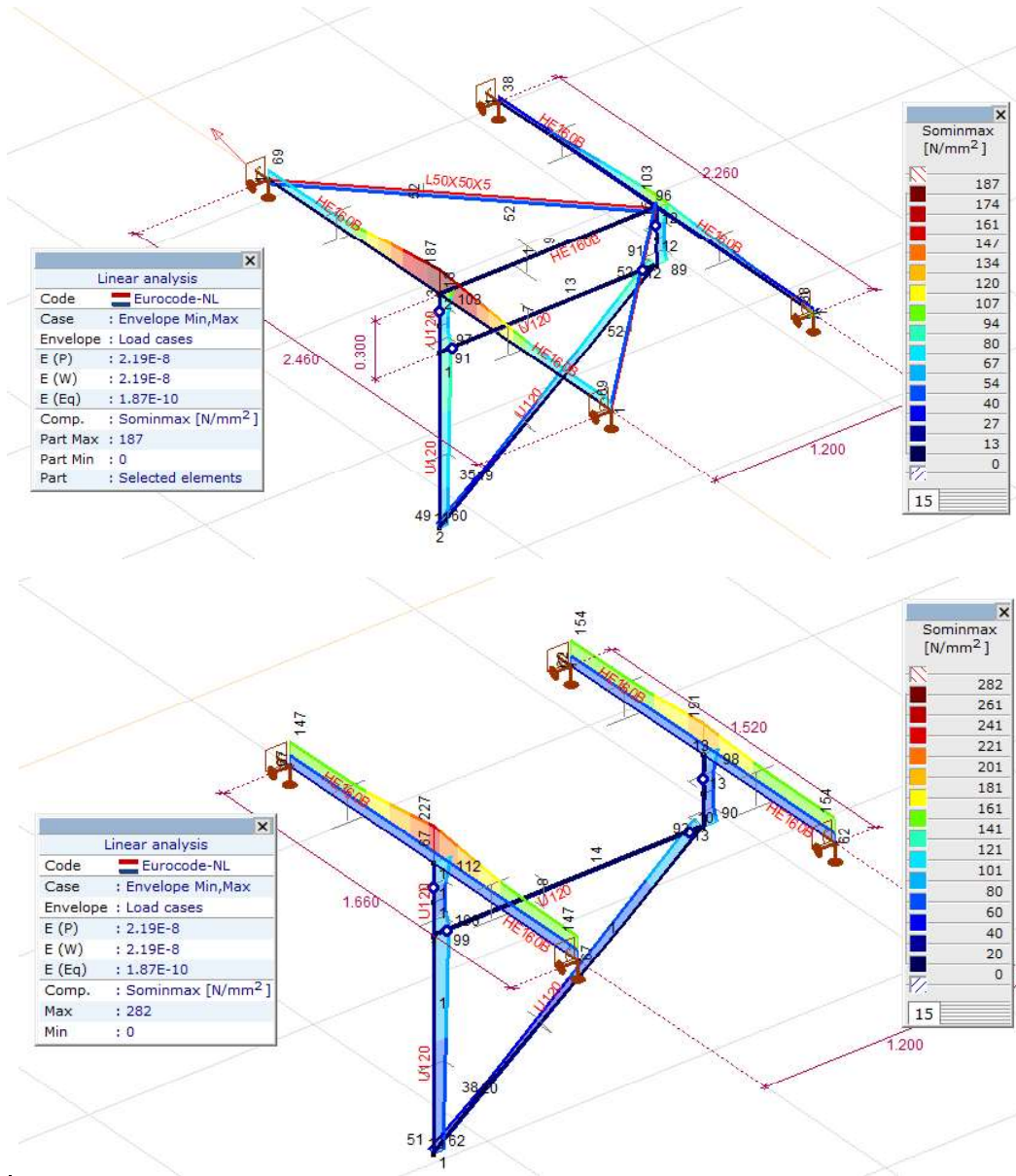
**Table 1 Details of load cases**

| Sr. No. | Load Case                         | Particular   | The load applied in the PLS tower model   |
|---------|-----------------------------------|--|---|
| 1       | 03 ULA_1a_90:                     | Wind load – Critical for the max horizontal load. The isolators are modelled and thus the loads are applied at the tip of the v-ketting and horizontal insulators. The loads governs the stresses in bottom chord due to bending action. |  |
| 2       | 15 ULA 3_90 max – vertical load): | Wind + ice + s.f : The horizontal load is smaller compared to 1a_90. This load has higher vertical loads.  |   |



## 4 RESULTS

The stresses in the insulator housing schemes are shown in Figure 4. Max stress of 187 MPa develops in the HEB profile for insulator 20. Max stress of 227 MPa develops in the HEB profile for insulator 22. A detailed view of the parts is given in the table below.



**Figure 4 Max stress for the insulator attachment assemblies.**

Figure 5 shows the max stress in the bottom chord of the lower cross arm. The load case 3\_90 is critical as it has maximum vertical load. The max stress is 177 MPa.







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## 5 CONCLUSION

The existing suspension towers of the S+32 serie is to be replaced by a new tower. The main structure of the tower has been checked via the PLS tower application. The structure is further checked in AxisVM locally as the bending in the structure is neglected in the PLS tower. The report explains the geometry and loading assumptions for the beams housing the insulator assembly in the 2 circuits S+32-tower in the ZWO-project. The loading is taken from PLS tower visualization. The loads on the beams housing the insulators and the supporting bottom chord and tower leg members are checked against the yield stress.

The initial check with same design of beams as existing tower showed considerable over-utilizations in the beams at the inner phase of the lower cross arm. The design was modified with additional K brace from L50x5 and HEB 160 between the primary HEB profiles between the bottom chord.

The max stress bottom chord is 179 MPa, with a usage of 0.50. The max stress across the UNP and HEB-profiles is 227 MPa (peak value) with the usage of 0.64. Thus the structure is considered safe.



# Project: DLE

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Rapport

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# Project: DLE

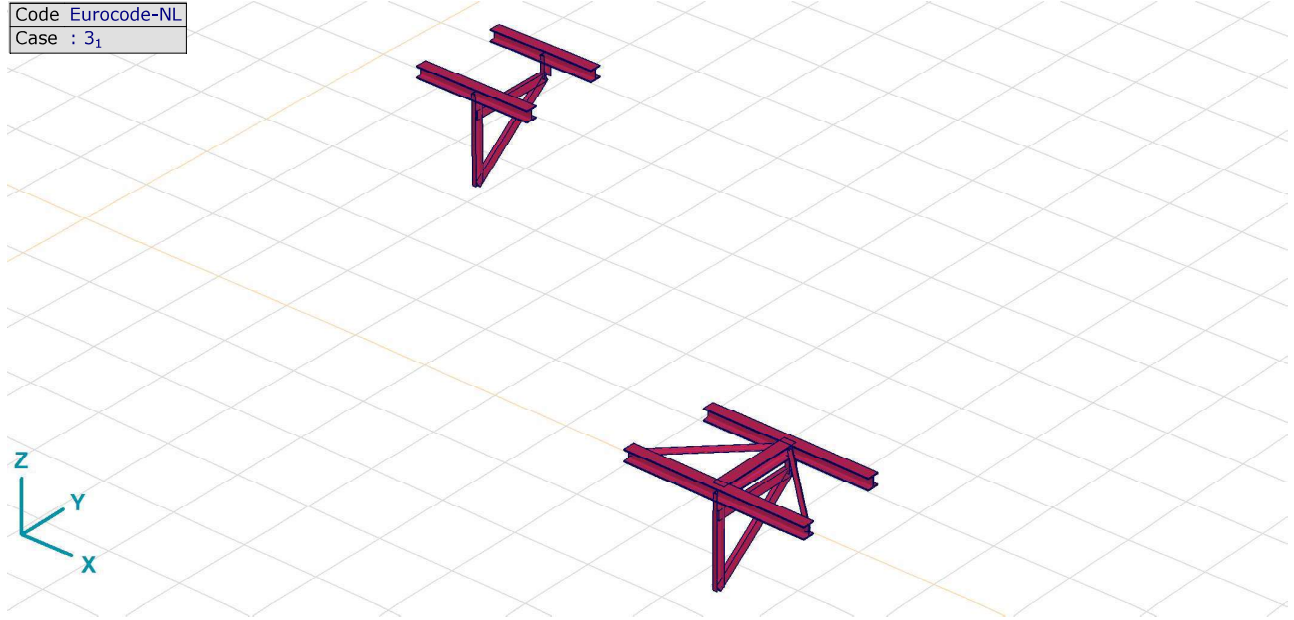
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Model: Ligger kruisingmast\_1.axs

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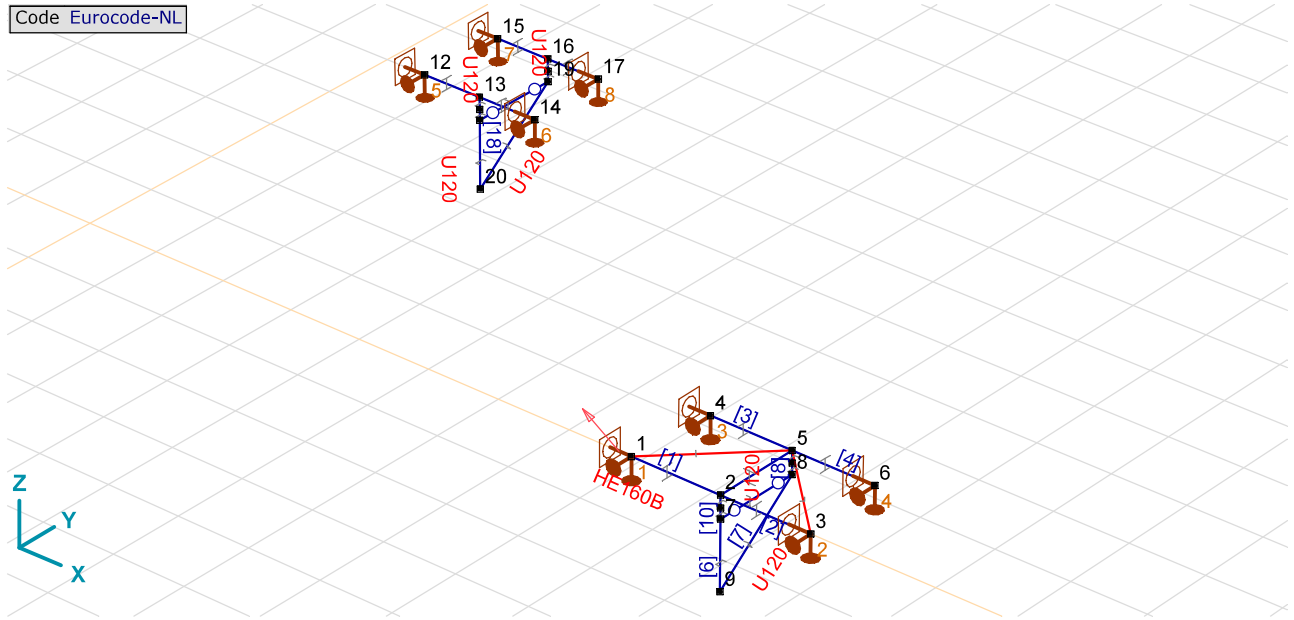
Page 3

Code Eurocode-NL  
Case : 3<sub>1</sub>



render

Code Eurocode-NL



Nummering en profielen

**Project: DLE**




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Model: **Ligger kruisingmast\_1.axs**

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## Cross-sections

|   | Name        | Drawing   | Process | Shape | h<br>[mm] | b<br>[mm] | tw<br>[mm] | tf<br>[mm] | r <sub>1</sub><br>[mm] | r <sub>2</sub><br>[mm] | r <sub>3</sub><br>[mm] |
|---|-------------|---|---------|-------|-----------|-----------|------------|------------|------------------------|------------------------|------------------------|
| 1 | HE 160 B    |  | Rolled  | I     | 160.0     | 160.0     | 8.0        | 13.0       | 15.0                   | 0                      | 0                      |
| 2 | U 120       |  | Rolled  | U     | 120.0     | 55.0      | 7.0        | 9.0        | 9.0                    | 4.5                    | 0                      |
| 3 | L 50X 50X 5 |  | Rolled  | L     | 50.0      | 50.0      | 5.0        | 5.0        | 7.0                    | 3.5                    | 0                      |

|   | Name        | A <sub>x</sub><br>[mm <sup>2</sup> ] | A <sub>y</sub><br>[mm <sup>2</sup> ] | A <sub>z</sub><br>[mm <sup>2</sup> ] | I <sub>x</sub><br>[mm <sup>4</sup> ] | I <sub>y</sub><br>[mm <sup>4</sup> ] | I <sub>z</sub><br>[mm <sup>4</sup> ] | I <sub>yz</sub><br>[mm <sup>4</sup> ] |
|---|-------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------------------------------|
| 1 | HE 160 B    | 5426.04                              | 3754.44                              | 1237.48                              | 317826.300                           | 2.492E+07                            | 8892444.000                          | 0                                     |
| 2 | U 120       | 1698.73                              | 617.80                               | 752.09                               | 41830.660                            | 3643327.000                          | 430614.100                           | 0                                     |
| 3 | L 50X 50X 5 | 480.28                               | 210.38                               | 213.29                               | 4408.870                             | 109629.100                           | 109629.100                           | -64162.800                            |

|   | Name        | I <sub>1</sub><br>[mm <sup>4</sup> ] | I <sub>2</sub><br>[mm <sup>4</sup> ] | α<br>[°] | I <sub>ω</sub><br>[mm <sup>6</sup> ] | W <sub>1,el,t</sub><br>[mm <sup>3</sup> ] | W <sub>1,el,b</sub><br>[mm <sup>3</sup> ] |
|---|-------------|--------------------------------------|--------------------------------------|----------|--------------------------------------|---|---|
| 1 | HE 160 B    | 2.492E+07                            | 8892443.000                          | 0        | 4.7E+10                              | 311542.700                                | 311542.700                                |
| 2 | U 120       | 3643327.000                          | 430614.100                           | 0        | 8.9E+08                              | 60722.120                                 | 60722.120                                 |
| 3 | L 50X 50X 5 | 173791.900                           | 45466.320                            | 45.00    | 678722                               | 4915.578                                  | 4915.578                                  |

|   | Name        | W <sub>2,el,t</sub><br>[mm <sup>3</sup> ] | W <sub>2,el,b</sub><br>[mm <sup>3</sup> ] | W <sub>1,pl</sub><br>[mm <sup>3</sup> ] | W <sub>2,pl</sub><br>[mm <sup>3</sup> ] | i <sub>y</sub><br>[mm] | i <sub>z</sub><br>[mm] | H <sub>y</sub><br>[mm] | H <sub>z</sub><br>[mm] |
|---|-------------|---|---|---|---|------------------------|------------------------|------------------------|------------------------|
| 1 | HE 160 B    | 111155.500                                | 111155.500                                | 354020.600                              | 169972.200                              | 67.8                   | 40.5                   | 160.0                  | 160.0                  |
| 2 | U 120       | 11058.300                                 | 26813.420                                 | 72702.590                               | 21257.590                               | 46.3                   | 15.9                   | 55.0                   | 120.0                  |
| 3 | L 50X 50X 5 | 2584.399                                  | 2290.666                                  | 7830.310                                | 4045.387                                | 15.1                   | 15.1                   | 50.0                   | 50.0                   |

|   | Name        | y <sub>G</sub><br>[mm] | z <sub>G</sub><br>[mm] | y <sub>s</sub><br>[mm] | z <sub>s</sub><br>[mm] | β <sub>y</sub><br>[mm] | β <sub>z</sub><br>[mm] | β <sub>w</sub><br>[°] | S.p. |
|---|-------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------|------|
| 1 | HE 160 B    | 80.0                   | 80.0                   | 0                      | 0                      | 0                      | 0                      | 0                     | 9    |
| 2 | U 120       | 16.1                   | 60.0                   | -29.6                  | 0                      | 0                      | 122.3                  | 0                     | 8    |
| 3 | L 50X 50X 5 | 14.0                   | 14.0                   | -11.0                  | -11.0                  | 45.0                   | 45.0                   | 0                     | 4    |

**Name:** Cross-section name; **Process:** Manufacturing process; **h:** Cross-section height; **b:** Cross-section width; **tw:** Web thickness; **tf:** Flange thickness; **r<sub>1</sub>, r<sub>2</sub>, r<sub>3</sub>:** Rounding radius;

**A<sub>x</sub>:** Cross-section area; **A<sub>y</sub>, A<sub>z</sub>:** Shear area; **I<sub>x</sub>:** Torsional inertia; **I<sub>y</sub>, I<sub>z</sub>:** Flexural inertia; **I<sub>yz</sub>:** Centrifugal inertia; **I<sub>1</sub>, I<sub>2</sub>:** Principal flexural inertia; **α:** Principal directions; **I<sub>ω</sub>:** Warping constant;

**W<sub>1,el,t</sub>, W<sub>1,el,b</sub>, W<sub>2,el,t</sub>, W<sub>2,el,b</sub>:** Elastic modulus; **W<sub>1,pl</sub>, W<sub>2,pl</sub>:** Plastic modulus; **i<sub>y</sub>, i<sub>z</sub>:** Radius of inertia; **H<sub>y</sub>:** Dimension in local y direction; **H<sub>z</sub>:** Dimension in local z direction;

**y<sub>G</sub>:** y coordinate of the center of gravity; **z<sub>G</sub>:** z coordinate of the center of gravity; **y<sub>s</sub>:** y coordinate of the shear (torsion) center relative to the center of gravity;

**z<sub>s</sub>:** z coordinate of the shear (torsion) center relative to the center of gravity; **β<sub>y</sub>, β<sub>z</sub>, β<sub>w</sub>:** Wagner's coefficient; **S.p.:** Stress calculation points;

## Nodes

|   | X [m]  | Y [m] | Z [m]  |    | X [m] | Y [m] | Z [m]  |    | X [m] | Y [m] | Z [m]  |
|---|--------|-------|--------|----|-------|-------|--------|----|-------|-------|--------|
| 1 | 7.870  | 0     | 0      | 9  | 9.100 | 0     | -1.200 | 17 | 2.160 | 6.200 | 0      |
| 2 | 9.100  | 0     | 0      | 10 | 9.100 | 1.200 | -0.160 | 18 | 1.400 | 5.000 | -0.300 |
| 3 | 10.330 | 0     | 0      | 11 | 9.100 | 0     | -0.160 | 19 | 1.400 | 6.200 | -0.300 |
| 4 | 7.970  | 1.200 | 0      | 12 | 0.570 | 5.000 | 0      | 20 | 1.400 | 5.000 | -1.200 |
| 5 | 9.100  | 1.200 | 0      | 13 | 1.400 | 5.000 | 0      | 21 | 1.400 | 6.200 | -0.160 |
| 6 | 10.230 | 1.200 | 0      | 14 | 2.230 | 5.000 | 0      | 22 | 1.400 | 5.000 | -0.160 |
| 7 | 9.100  | 0     | -0.300 | 15 | 0.640 | 6.200 | 0      |    |       |       |        |
| 8 | 9.100  | 1.200 | -0.300 | 16 | 1.400 | 6.200 | 0      |    |       |       |        |

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**Nodal supports**

|   | Node | X [m]  | Y [m] | Z [m] | Type  | Name <sub>x</sub>     | K <sub>x</sub><br>[kN/m] | K <sub>xV</sub><br>[kN/m] | Name <sub>y</sub>     | K <sub>y</sub><br>[kN/m] |
|---|------|--------|-------|-------|-------|-----------------------|--------------------------|---------------------------|-----------------------|--------------------------|
| 1 | 1    | 7.870  | 0     | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |
| 2 | 3    | 10.330 | 0     | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |
| 3 | 4    | 7.970  | 1.200 | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |
| 4 | 6    | 10.230 | 1.200 | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |
| 5 | 12   | 0.570  | 5.000 | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |
| 6 | 14   | 2.230  | 5.000 | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |
| 7 | 15   | 0.640  | 6.200 | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |
| 8 | 17   | 2.160  | 6.200 | 0     | Glob. | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Translational | 1E+10                    |

|   | Node | K <sub>yV</sub><br>[kN/m] | Name <sub>z</sub>     | K <sub>z</sub><br>[kN/m] | K <sub>zV</sub><br>[kN/m] | Name <sub>xx</sub> | K <sub>xx</sub><br>[kNm/rad] | K <sub>xxV</sub><br>[kNm/rad] | Name <sub>yy</sub> |
|---|------|---------------------------|-----------------------|--------------------------|---------------------------|--------------------|------------------------------|-------------------------------|--------------------|
| 1 | 1    | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |
| 2 | 3    | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |
| 3 | 4    | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |
| 4 | 6    | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |
| 5 | 12   | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |
| 6 | 14   | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |
| 7 | 15   | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |
| 8 | 17   | 1E+10                     | Rigid - Translational | 1E+10                    | 1E+10                     | Rigid - Rotational | 1E+10                        | 1E+10                         | —                  |

|   | Node | K <sub>yy</sub><br>[kNm/rad] | K <sub>yyV</sub><br>[kNm/rad] | Name <sub>zz</sub> | K <sub>zz</sub><br>[kNm/rad] | K <sub>zzV</sub><br>[kNm/rad] |
|---|------|------------------------------|-------------------------------|--------------------|------------------------------|-------------------------------|
| 1 | 1    | —                            | —                             | —                  | —                            | —                             |
| 2 | 3    | —                            | —                             | —                  | —                            | —                             |
| 3 | 4    | —                            | —                             | —                  | —                            | —                             |
| 4 | 6    | —                            | —                             | —                  | —                            | —                             |
| 5 | 12   | —                            | —                             | —                  | —                            | —                             |
| 6 | 14   | —                            | —                             | —                  | —                            | —                             |
| 7 | 15   | —                            | —                             | —                  | —                            | —                             |
| 8 | 17   | —                            | —                             | —                  | —                            | —                             |

Node: Supported node; Type: Support type; K<sub>x</sub>, K<sub>y</sub>, K<sub>z</sub>, K<sub>xx</sub>, K<sub>yy</sub>, K<sub>zz</sub>: Initial stiffness;

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Model: **Ligger kruisingmast\_1.axs**

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## Beam internal forces [Linear, Envelope (Load cases)]

|      | Sh. | Cross-section name | C  | min.<br>max. | Case | Loc.<br>[m] | Node | Nx<br>[kN]   | Vy<br>[kN] | Vz<br>[kN] |
|------|-----|--------------------|----|--------------|------|-------------|------|--------------|------------|------------|
| Ext. |     |                    |    |              |      |             |      |              |            |            |
| 19   | 2   | U 120              | Nx | min          | 1a   | 0           | (20) | <b>-63.0</b> | 0          | -2.8       |
| 18   | 2   | U 120              |    | max          | 1a   | 0           | (20) | <b>81.7</b>  | 0          | 2.5        |
| 22   | 2   | U 120              |    | max          | 1a   | 0           | (22) | <b>81.7</b>  | 0          | -21.8      |
| 23   | 2   | U 120              |    | max          | 1a   | 0           | (18) | <b>81.7</b>  | 0          | -21.8      |
| 15   | 1   | HE 160 B           | Tx | min          | 1a_1 | 0           | (15) | 0            | -12.2      | -20.0      |
| 16   | 1   | HE 160 B           |    | min          | 1a   | 0           | (16) | 0            | -12.2      | -20.0      |
| 15   | 1   | HE 160 B           |    | max          | 1a   | 0           | (15) | 0            | 12.2       | 20.0       |
| 16   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (16) | 0            | 12.2       | 20.0       |
| 1    | 1   | HE 160 B           | My | min          | 1a   | 1.230       | (2)  | 0            | 1.9        | -42.1      |
| 2    | 1   | HE 160 B           |    | min          | 1a   | 0           | (2)  | 0            | -1.9       | 42.1       |
| 3    | 1   | HE 160 B           |    | max          | 1a   | 1.130       | (5)  | 0            | 2.4        | 21.5       |
| 4    | 1   | HE 160 B           |    | max          | 1a   | 0           | (5)  | 0            | -2.4       | -21.5      |
| 15   | 1   | HE 160 B           | Mz | min          | 1a   | 0.760       | (16) | 0            | 12.2       | 20.0       |
| 16   | 1   | HE 160 B           |    | min          | 1a   | 0           | (16) | 0            | -12.2      | -20.0      |
| 15   | 1   | HE 160 B           |    | max          | 1a_1 | 0.760       | (16) | 0            | -12.2      | -20.0      |
| 16   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (16) | 0            | 12.2       | 20.0       |

|      | Sh. | Cross-section name | C  | min.<br>max. | Case | Loc.<br>[m] | Node | Tx<br>[kNm] | My<br>[kNm]  | Mz<br>[kNm] | B<br>[kNm <sup>2</sup> ] |
|------|-----|--------------------|----|--------------|------|-------------|------|-------------|--------------|-------------|--------------------------|
| Ext. |     |                    |    |              |      |             |      |             |              |             |                          |
| 19   | 2   | U 120              | Nx | min          | 1a   | 0           | (20) | 0           | 0.8          | 0           | 0                        |
| 18   | 2   | U 120              |    | max          | 1a   | 0           | (20) | 0           | 0.8          | 0           | 0                        |
| 22   | 2   | U 120              |    | max          | 1a   | 0           | (22) | 0           | 0            | 0           | 0                        |
| 23   | 2   | U 120              |    | max          | 1a   | 0           | (18) | 0           | 3.1          | 0           | 0                        |
| 15   | 1   | HE 160 B           | Tx | min          | 1a_1 | 0           | (15) | <b>-1.9</b> | 0            | 0           | 0                        |
| 16   | 1   | HE 160 B           |    | min          | 1a   | 0           | (16) | <b>-1.9</b> | 15.2         | -9.3        | 0                        |
| 15   | 1   | HE 160 B           |    | max          | 1a   | 0           | (15) | <b>1.9</b>  | 0            | 0           | 0                        |
| 16   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (16) | <b>1.9</b>  | -15.2        | 9.3         | 0                        |
| 1    | 1   | HE 160 B           | My | min          | 1a   | 1.230       | (2)  | 0.1         | <b>-51.8</b> | -2.3        | 0                        |
| 2    | 1   | HE 160 B           |    | min          | 1a   | 0           | (2)  | -0.1        | <b>-51.8</b> | -2.3        | 0                        |
| 3    | 1   | HE 160 B           |    | max          | 1a   | 1.130       | (5)  | 0.1         | <b>24.3</b>  | -2.7        | 0                        |
| 4    | 1   | HE 160 B           |    | max          | 1a   | 0           | (5)  | -0.1        | <b>24.3</b>  | -2.7        | 0                        |
| 15   | 1   | HE 160 B           | Mz | min          | 1a   | 0.760       | (16) | 1.9         | 15.2         | <b>-9.3</b> | 0                        |
| 16   | 1   | HE 160 B           |    | min          | 1a   | 0           | (16) | -1.9        | 15.2         | <b>-9.3</b> | 0                        |
| 15   | 1   | HE 160 B           |    | max          | 1a_1 | 0.760       | (16) | -1.9        | -15.2        | <b>9.3</b>  | 0                        |
| 16   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (16) | 1.9         | -15.2        | <b>9.3</b>  | 0                        |

Sh.: Cross-section; C: Extremal component; min. max.: Extreme type; Case: Load case of extreme; Loc.: Cross-section local x position on the beam; Nx: Axial force; Vy: Shear force in local y direction; Vz: Shear force in local z direction; Tx: Torsional moment; My: Flexural moment about local y axis; Mz: Flexural moment about local z axis;

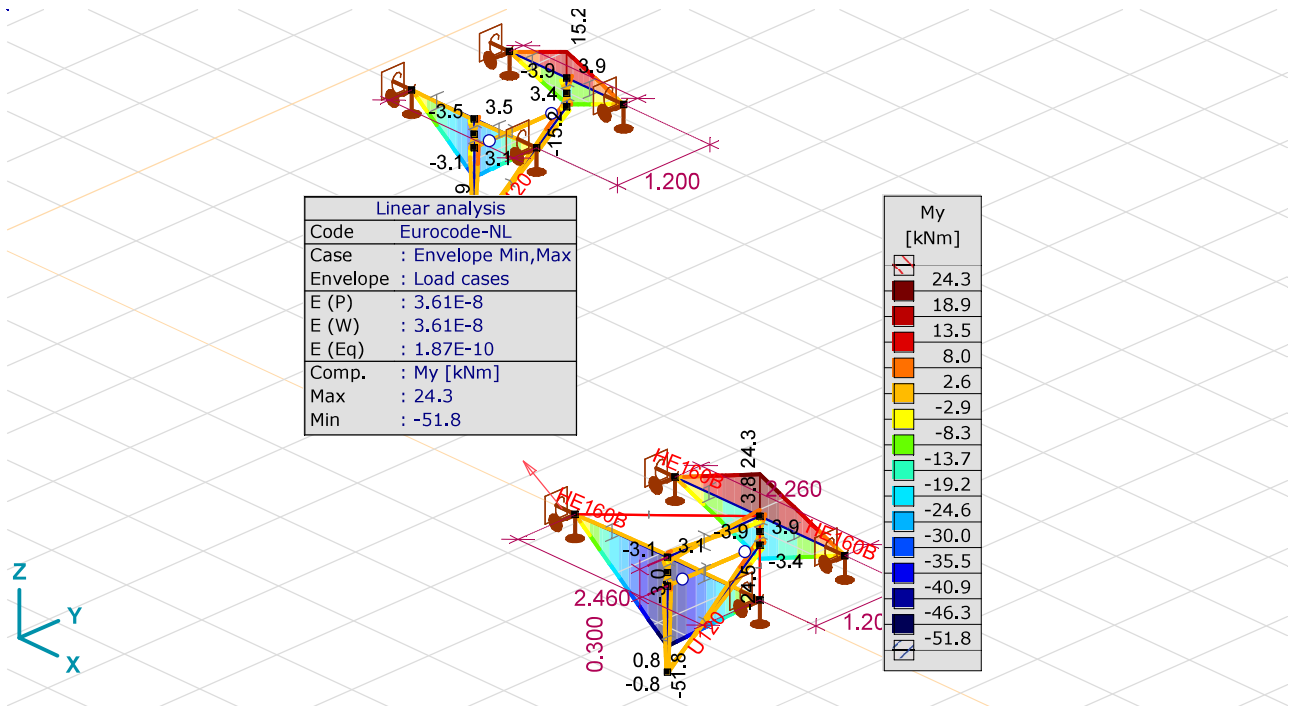
**Project: DLE**

Constructeur: DNV GL - Energy

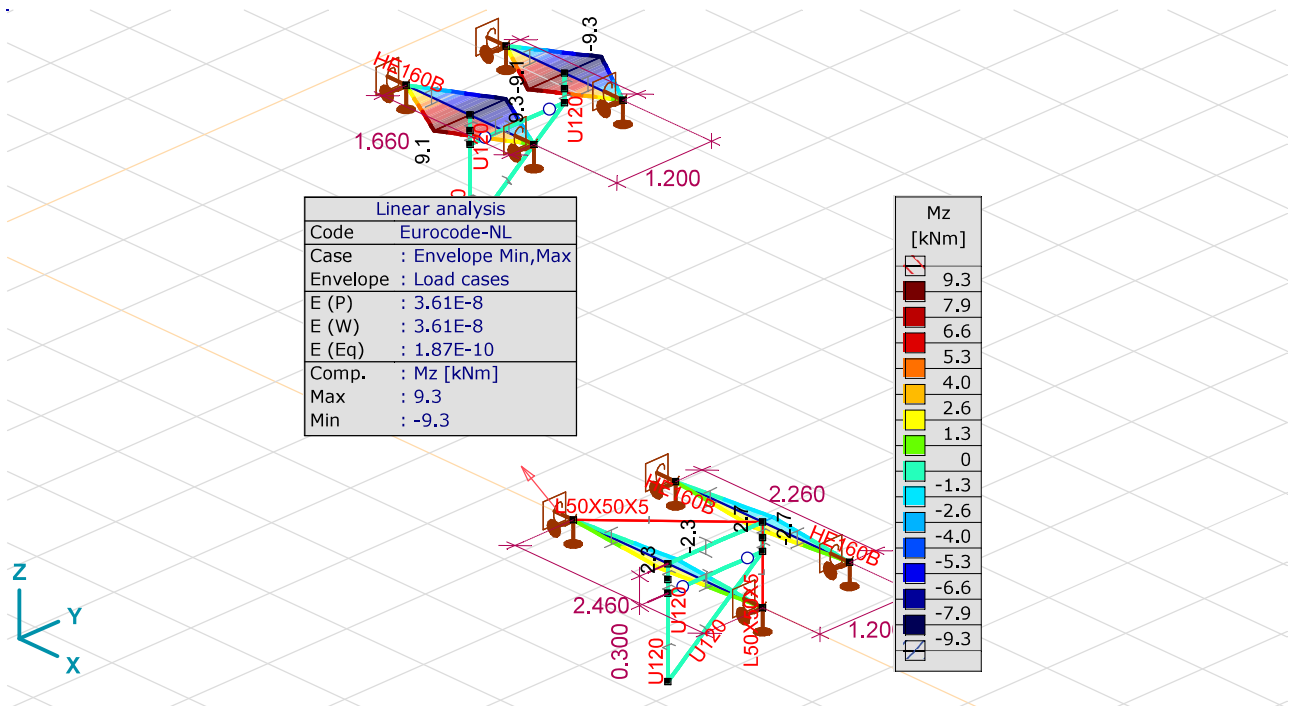
Model: **Ligger kruisingmast\_1.axs**

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[I], Linear, Envelope (Load cases), My [kNm], Filled diagram



[I], Linear, Envelope (Load cases), Mz [kNm], Filled diagram

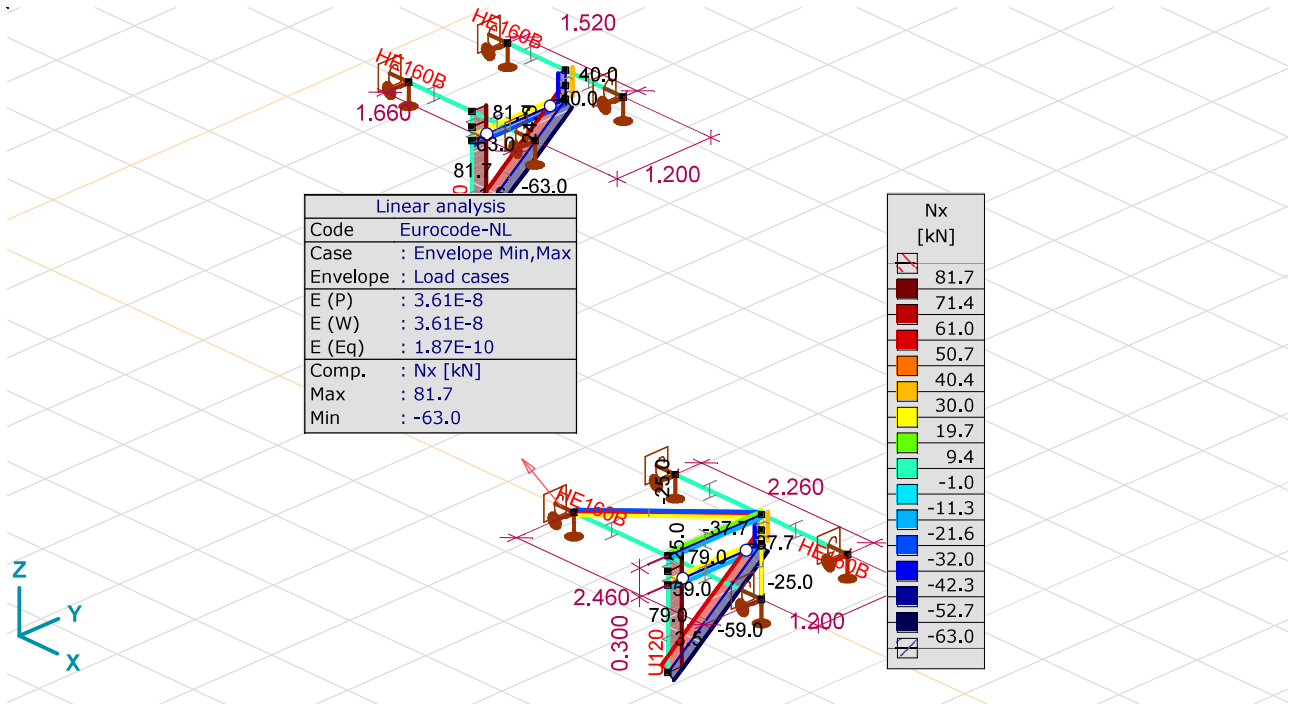
**Project: DLE**

Constructeur: DNV GL - Energy

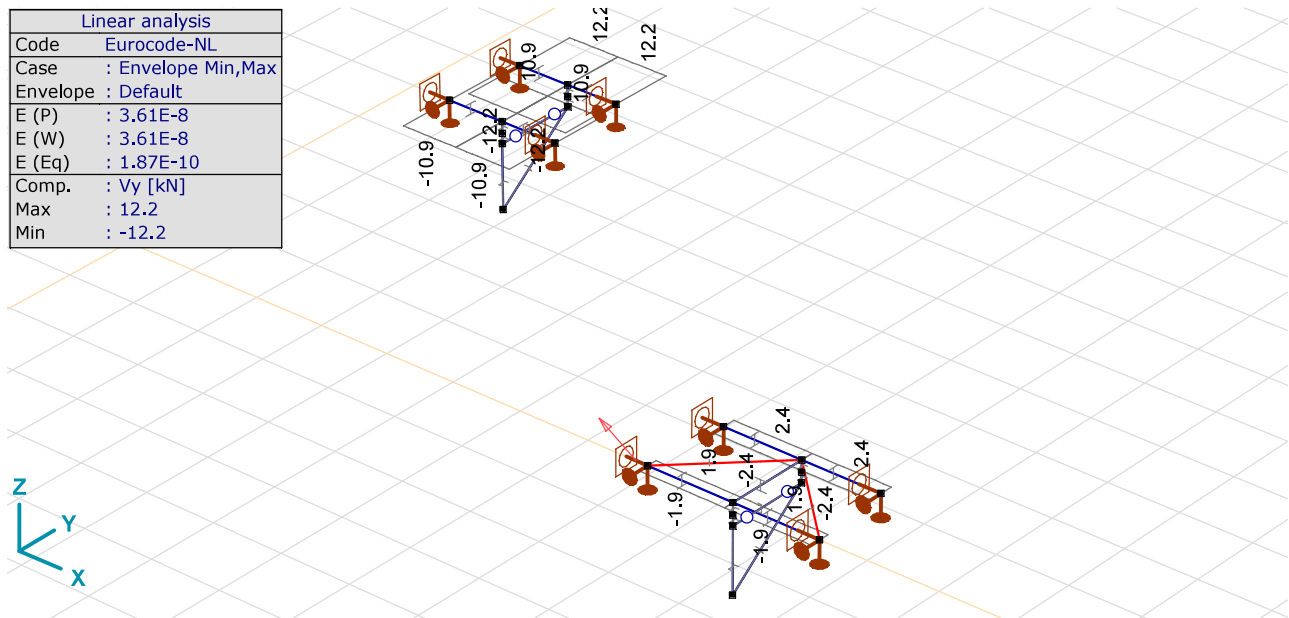
Model: **Ligger kruisingmast\_1.axs**

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[I], Linear, Envelope (Load cases), Nx [kN], Filled diagram



[I], Linear, Envelope (Default), Vy [kN], Diagram



# Project: DLE

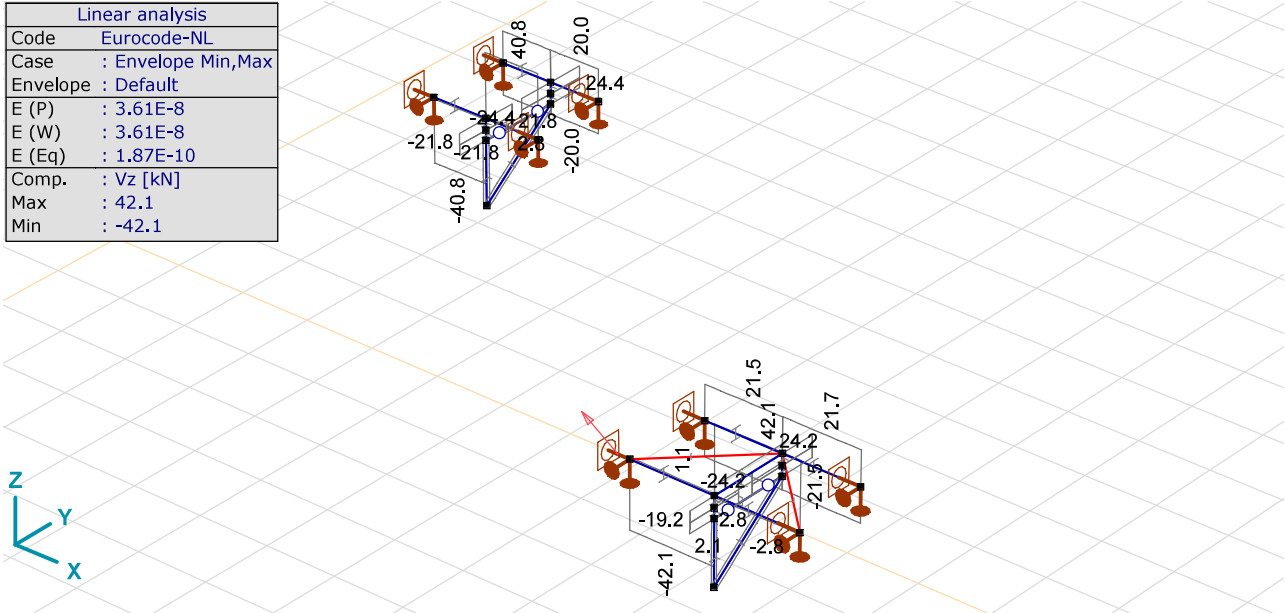
Constructeur: DNV GL - Energy

Model: **Ligger kruisingmast\_1.axs**

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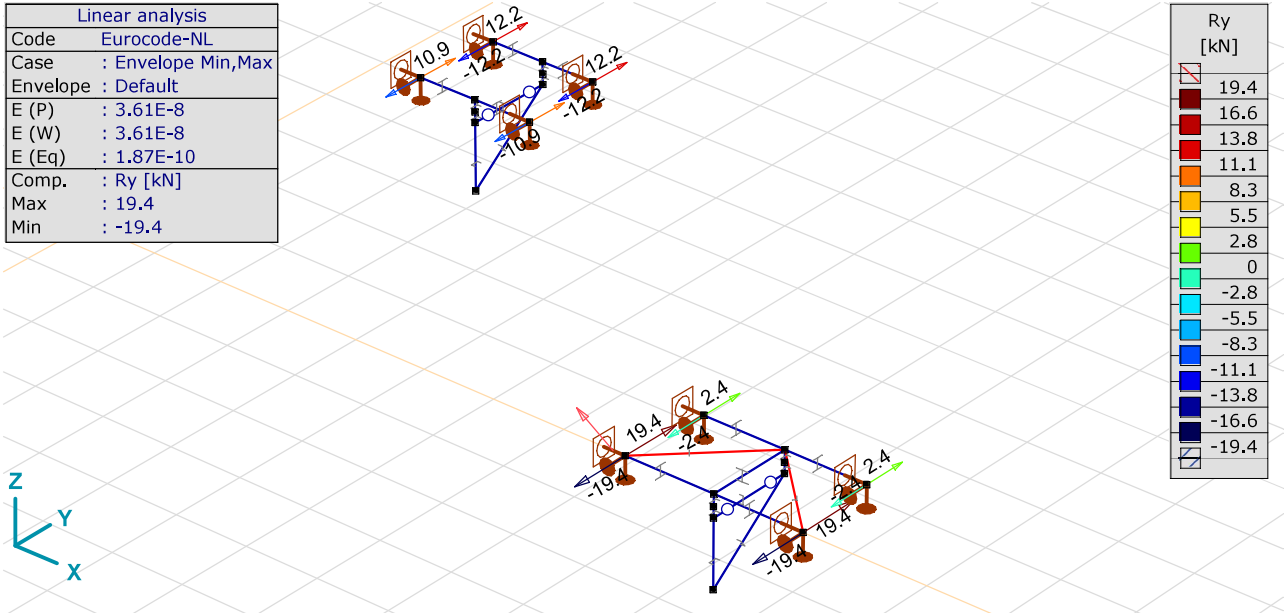
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| Linear analysis |                    |
|-----------------|--------------------|
| Code            | Eurocode-NL        |
| Case            | : Envelope Min,Max |
| Envelope        | : Default          |
| E (P)           | : 3.61E-8          |
| E (W)           | : 3.61E-8          |
| E (Eq)          | : 1.87E-10         |
| Comp.           | : Vz [kN]          |
| Max             | : 42.1             |
| Min             | : -42.1            |



[I], Linear, Envelope (Default), Vz [kN], Diagram

| Linear analysis |                    |
|-----------------|--------------------|
| Code            | Eurocode-NL        |
| Case            | : Envelope Min,Max |
| Envelope        | : Default          |
| E (P)           | : 3.61E-8          |
| E (W)           | : 3.61E-8          |
| E (Eq)          | : 1.87E-10         |
| Comp.           | : Ry [kN]          |
| Max             | : 19.4             |
| Min             | : -19.4            |



[I], Linear, Envelope (Default), Ry [kN] (nodal supp.), Diagram



**Project: DLE**

Constructeur: DNV GL - Energy

Model: **Ligger kruisingmast\_1.axs**

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## Beam internal forces [Linear, Envelope (Default), HE 160 B]

| Sh. | Cross-section name | C        | min.<br>max. | Case | Loc.<br>[m] | Node | Nx<br>[kN] | Vy<br>[kN]  | Vz<br>[kN]   |
|-----|--------------------|----------|--------------|------|-------------|------|------------|-------------|--------------|
|     |                    |          | max          | 1a_1 | 0           | (2)  | <b>0</b>   | 1.9         | -1.1         |
|     |                    | Vy       | min          | 1a   | 0           | (2)  | 0          | <b>-1.9</b> | 42.1         |
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0          | <b>1.9</b>  | -1.1         |
|     |                    | Vz       | min          | 1a_1 | 0           | (2)  | 0          | 1.9         | <b>-1.1</b>  |
|     |                    |          | max          | 1a   | 0           | (2)  | 0          | -1.9        | <b>42.1</b>  |
|     |                    | Tx       | min          | 1a   | 0           | (2)  | 0          | -1.9        | 42.1         |
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0          | 1.9         | -1.1         |
|     |                    | My       | min          | 1a   | 0           | (2)  | 0          | -1.9        | 42.1         |
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0          | 1.9         | -1.1         |
|     |                    | Mz       | min          | 1a   | 0           | (2)  | 0          | -1.9        | 42.1         |
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0          | 1.9         | -1.1         |
| 3   | 1                  | HE 160 B |              |      | L=1.130     |      |            |             |              |
|     |                    | Nx       | min          | 1a   | 0           | (4)  | <b>0</b>   | 2.4         | 21.5         |
|     |                    |          | max          | 1a   | 0           | (4)  | <b>0</b>   | 2.4         | 21.5         |
|     |                    | Vy       | min          | 1a_1 | 0           | (4)  | 0          | <b>-2.4</b> | -21.7        |
|     |                    |          | max          | 1a   | 0           | (4)  | 0          | <b>2.4</b>  | 21.5         |
|     |                    | Vz       | min          | 1a_1 | 0           | (4)  | 0          | -2.4        | <b>-21.7</b> |
|     |                    |          | max          | 1a   | 0           | (4)  | 0          | 2.4         | <b>21.5</b>  |
|     |                    | Tx       | min          | 1a_1 | 0           | (4)  | 0          | -2.4        | -21.7        |
|     |                    |          | max          | 1a   | 0           | (4)  | 0          | 2.4         | 21.5         |
|     |                    | My       | min          | 1a_1 | 1.130       | (5)  | 0          | -2.4        | -21.7        |
|     |                    |          | max          | 1a   | 1.130       | (5)  | 0          | 2.4         | 21.5         |
|     |                    | Mz       | min          | 1a   | 1.130       | (5)  | 0          | 2.4         | 21.5         |
|     |                    |          | max          | 1a_1 | 1.130       | (5)  | 0          | -2.4        | -21.7        |
| 4   | 1                  | HE 160 B |              |      | L=1.130     |      |            |             |              |
|     |                    | Nx       | min          | 1a   | 0           | (5)  | <b>0</b>   | -2.4        | -21.5        |
|     |                    |          | max          | 1a   | 0           | (5)  | <b>0</b>   | -2.4        | -21.5        |

| Sh. | Cross-section name | C        | min.<br>max. | Case | Loc.<br>[m] | Node | Tx<br>[kNm] | My<br>[kNm]  | Mz<br>[kNm] | B<br>[kNm <sup>2</sup> ] |
|-----|--------------------|----------|--------------|------|-------------|------|-------------|--------------|-------------|--------------------------|
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0           | 1.3          | 2.3         | 0                        |
|     |                    | Vy       | min          | 1a   | 0           | (2)  | -0.1        | -51.8        | -2.3        | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0           | 1.3          | 2.3         | 0                        |
|     |                    | Vz       | min          | 1a_1 | 0           | (2)  | 0           | 1.3          | 2.3         | 0                        |
|     |                    |          | max          | 1a   | 0           | (2)  | -0.1        | -51.8        | -2.3        | 0                        |
|     |                    | Tx       | min          | 1a   | 0           | (2)  | <b>-0.1</b> | -51.8        | -2.3        | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (2)  | <b>0</b>    | 1.3          | 2.3         | 0                        |
|     |                    | My       | min          | 1a   | 0           | (2)  | -0.1        | <b>-51.8</b> | -2.3        | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0           | <b>1.3</b>   | 2.3         | 0                        |
|     |                    | Mz       | min          | 1a   | 0           | (2)  | -0.1        | -51.8        | <b>-2.3</b> | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (2)  | 0           | 1.3          | <b>2.3</b>  | 0                        |
| 3   | 1                  | HE 160 B |              |      | L=1.130     |      |             |              |             |                          |
|     |                    | Nx       | min          | 1a   | 0           | (4)  | 0.1         | 0            | 0           | 0                        |
|     |                    |          | max          | 1a   | 0           | (4)  | 0.1         | 0            | 0           | 0                        |
|     |                    | Vy       | min          | 1a_1 | 0           | (4)  | 0           | 0            | 0           | 0                        |
|     |                    |          | max          | 1a   | 0           | (4)  | 0.1         | 0            | 0           | 0                        |
|     |                    | Vz       | min          | 1a_1 | 0           | (4)  | 0           | 0            | 0           | 0                        |
|     |                    |          | max          | 1a   | 0           | (4)  | 0.1         | 0            | 0           | 0                        |
|     |                    | Tx       | min          | 1a_1 | 0           | (4)  | <b>0</b>    | 0            | 0           | 0                        |
|     |                    |          | max          | 1a   | 0           | (4)  | <b>0.1</b>  | 0            | 0           | 0                        |
|     |                    | My       | min          | 1a_1 | 1.130       | (5)  | 0           | <b>-24.5</b> | 2.7         | 0                        |
|     |                    |          | max          | 1a   | 1.130       | (5)  | 0.1         | <b>24.3</b>  | -2.7        | 0                        |
|     |                    | Mz       | min          | 1a   | 1.130       | (5)  | 0.1         | 24.3         | <b>-2.7</b> | 0                        |
|     |                    |          | max          | 1a_1 | 1.130       | (5)  | 0           | -24.5        | <b>2.7</b>  | 0                        |
| 4   | 1                  | HE 160 B |              |      | L=1.130     |      |             |              |             |                          |
|     |                    | Nx       | min          | 1a   | 0           | (5)  | -0.1        | 24.3         | -2.7        | 0                        |
|     |                    |          | max          | 1a   | 0           | (5)  | -0.1        | 24.3         | -2.7        | 0                        |

**Project: DLE**

Constructeur: DNV GL - Energy

Model: **Ligger kruisingmast\_1.axs**

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## Beam internal forces [Linear, Envelope (Default), HE 160 B]

|    | Sh. | Cross-section name | C  | min.<br>max. | Case | Loc.<br>[m] | Node | Nx<br>[kN] | Vy<br>[kN] | Vz<br>[kN] |
|----|-----|--------------------|----|--------------|------|-------------|------|------------|------------|------------|
|    |     |                    | Vy | min          | 1a   | 0           | (5)  | 0          | -2.4       | -21.5      |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0          | 2.4        | 21.7       |
|    |     |                    | Vz | min          | 1a   | 0           | (5)  | 0          | -2.4       | -21.5      |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0          | 2.4        | 21.7       |
|    |     |                    | Tx | min          | 1a   | 0           | (5)  | 0          | -2.4       | -21.5      |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0          | 2.4        | 21.7       |
|    |     |                    | My | min          | 1a_1 | 0           | (5)  | 0          | 2.4        | 21.7       |
|    |     |                    |    | max          | 1a   | 0           | (5)  | 0          | -2.4       | -21.5      |
|    |     |                    | Mz | min          | 1a   | 0           | (5)  | 0          | -2.4       | -21.5      |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0          | 2.4        | 21.7       |
| 12 | 1   | HE 160 B           |    |              |      | L=1.200     |      |            |            |            |
|    |     |                    | Nx | min          | 1a   | 0           | (2)  | -15.5      | 0          | -5.4       |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 15.5       | 0          | 5.7        |
|    |     |                    | Vy | min          | 1a   | 0           | (2)  | -15.5      | 0          | -5.4       |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 15.5       | 0          | 5.7        |
|    |     |                    | Vz | min          | 1a   | 0           | (2)  | -15.5      | 0          | -5.4       |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 15.5       | 0          | 5.7        |
|    |     |                    | Tx | min          | 1a   | 0           | (2)  | -15.5      | 0          | -5.4       |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 15.5       | 0          | 5.7        |
|    |     |                    | My | min          | 1a   | 1.200       | (5)  | -15.5      | 0          | -5.4       |
|    |     |                    |    | max          | 1a_1 | 1.200       | (5)  | 15.5       | 0          | 5.7        |
|    |     |                    | Mz | min          | 1a   | 0           | (2)  | -15.5      | 0          | -5.4       |
|    |     |                    |    | max          | 1a   | 1.200       | (5)  | -15.5      | 0          | -5.4       |
| 13 | 1   | HE 160 B           |    |              |      | L=0.830     |      |            |            |            |
|    |     |                    | Nx | min          | 1a   | 0           | (12) | 0          | 10.9       | -40.8      |
|    |     |                    |    | max          | 1a   | 0           | (12) | 0          | 10.9       | -40.8      |
|    |     |                    | Vy | min          | 1a_1 | 0           | (12) | 0          | -10.9      | -0.8       |

|    | Sh. | Cross-section name | C  | min.<br>max. | Case | Loc.<br>[m] | Node | Tx<br>[kNm] | My<br>[kNm] | Mz<br>[kNm] | B<br>[kNm <sup>2</sup> ] |
|----|-----|--------------------|----|--------------|------|-------------|------|-------------|-------------|-------------|--------------------------|
|    |     |                    | Vy | min          | 1a   | 0           | (5)  | -0.1        | 24.3        | -2.7        | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0           | -24.5       | 2.7         | 0                        |
|    |     |                    | Vz | min          | 1a   | 0           | (5)  | -0.1        | 24.3        | -2.7        | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0           | -24.5       | 2.7         | 0                        |
|    |     |                    | Tx | min          | 1a   | 0           | (5)  | -0.1        | 24.3        | -2.7        | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0           | -24.5       | 2.7         | 0                        |
|    |     |                    | My | min          | 1a_1 | 0           | (5)  | 0           | -24.5       | 2.7         | 0                        |
|    |     |                    |    | max          | 1a   | 0           | (5)  | -0.1        | 24.3        | -2.7        | 0                        |
|    |     |                    | Mz | min          | 1a   | 0           | (5)  | -0.1        | 24.3        | -2.7        | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (5)  | 0           | -24.5       | 2.7         | 0                        |
| 12 | 1   | HE 160 B           |    |              |      | L=1.200     |      |             |             |             |                          |
|    |     |                    | Nx | min          | 1a   | 0           | (2)  | 0           | 2.8         | 0           | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 0           | -3.0        | 0           | 0                        |
|    |     |                    | Vy | min          | 1a   | 0           | (2)  | 0           | 2.8         | 0           | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 0           | -3.0        | 0           | 0                        |
|    |     |                    | Vz | min          | 1a   | 0           | (2)  | 0           | 2.8         | 0           | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 0           | -3.0        | 0           | 0                        |
|    |     |                    | Tx | min          | 1a   | 0           | (2)  | 0           | 2.8         | 0           | 0                        |
|    |     |                    |    | max          | 1a_1 | 0           | (2)  | 0           | -3.0        | 0           | 0                        |
|    |     |                    | My | min          | 1a   | 1.200       | (5)  | 0           | -3.6        | 0           | 0                        |
|    |     |                    |    | max          | 1a_1 | 1.200       | (5)  | 0           | 3.8         | 0           | 0                        |
|    |     |                    | Mz | min          | 1a   | 0           | (2)  | 0           | 2.8         | 0           | 0                        |
|    |     |                    |    | max          | 1a   | 1.200       | (5)  | 0           | -3.6        | 0           | 0                        |
| 13 | 1   | HE 160 B           |    |              |      | L=0.830     |      |             |             |             |                          |
|    |     |                    | Nx | min          | 1a   | 0           | (12) | 1.7         | 0           | 0           | 0                        |
|    |     |                    |    | max          | 1a   | 0           | (12) | 1.7         | 0           | 0           | 0                        |
|    |     |                    | Vy | min          | 1a_1 | 0           | (12) | -1.7        | 0           | 0           | 0                        |

**Project: DLE**

Constructeur: DNV GL - Energy

Model: **Ligger kruisingmast\_1.axs**

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## Beam internal forces [Linear, Envelope (Default), HE 160 B]

| Sh. | Cross-section name | C        | min.<br>max. | Case | Loc.<br>[m] | Node | Nx<br>[kN] | Vy<br>[kN]   | Vz<br>[kN]   |
|-----|--------------------|----------|--------------|------|-------------|------|------------|--------------|--------------|
|     |                    |          | max          | 1a   | 0           | (12) | 0          | <b>10.9</b>  | -40.8        |
|     |                    | Vz       | min          | 1a   | 0           | (12) | 0          | 10.9         | <b>-40.8</b> |
|     |                    |          | max          | 1a_1 | 0           | (12) | 0          | -10.9        | <b>-0.8</b>  |
|     |                    | Tx       | min          | 1a_1 | 0           | (12) | 0          | -10.9        | -0.8         |
|     |                    |          | max          | 1a   | 0           | (12) | 0          | 10.9         | -40.8        |
|     |                    | My       | min          | 1a   | 0.830       | (13) | 0          | 10.9         | -40.8        |
|     |                    |          | max          | 1a_1 | 0           | (12) | 0          | -10.9        | -0.8         |
|     |                    | Mz       | min          | 1a   | 0.830       | (13) | 0          | 10.9         | -40.8        |
|     |                    |          | max          | 1a_1 | 0.830       | (13) | 0          | -10.9        | -0.8         |
| 14  | I                  | HE 160 B |              |      | L=0.830     |      |            |              |              |
|     |                    | Nx       | min          | 1a   | 0           | (13) | <b>0</b>   | -10.9        | 40.8         |
|     |                    |          | max          | 1a   | 0           | (13) | <b>0</b>   | -10.9        | 40.8         |
|     |                    | Vy       | min          | 1a   | 0           | (13) | 0          | <b>-10.9</b> | 40.8         |
|     |                    |          | max          | 1a_1 | 0           | (13) | 0          | <b>10.9</b>  | 0.8          |
|     |                    | Vz       | min          | 1a_1 | 0           | (13) | 0          | 10.9         | <b>0.8</b>   |
|     |                    |          | max          | 1a   | 0           | (13) | 0          | -10.9        | <b>40.8</b>  |
|     |                    | Tx       | min          | 1a   | 0           | (13) | 0          | -10.9        | 40.8         |
|     |                    |          | max          | 1a_1 | 0           | (13) | 0          | 10.9         | 0.8          |
|     |                    | My       | min          | 1a   | 0           | (13) | 0          | -10.9        | 40.8         |
|     |                    |          | max          | 1a   | 0.830       | (14) | 0          | -10.9        | 40.8         |
|     |                    | Mz       | min          | 1a   | 0           | (13) | 0          | -10.9        | 40.8         |
|     |                    |          | max          | 1a_1 | 0           | (13) | 0          | 10.9         | 0.8          |
| 15  | I                  | HE 160 B |              |      | L=0.760     |      |            |              |              |
|     |                    | Nx       | min          | 1a   | 0           | (15) | <b>0</b>   | 12.2         | 20.0         |
|     |                    |          | max          | 1a   | 0           | (15) | <b>0</b>   | 12.2         | 20.0         |
|     |                    | Vy       | min          | 1a_1 | 0           | (15) | 0          | <b>-12.2</b> | -20.0        |
|     |                    |          | max          | 1a   | 0           | (15) | 0          | <b>12.2</b>  | 20.0         |

| Sh. | Cross-section name | C        | min.<br>max. | Case | Loc.<br>[m] | Node | Tx<br>[kNm] | My<br>[kNm]  | Mz<br>[kNm] | B<br>[kNm <sup>2</sup> ] |
|-----|--------------------|----------|--------------|------|-------------|------|-------------|--------------|-------------|--------------------------|
|     |                    |          | max          | 1a   | 0           | (12) | 1.7         | 0            | 0           | 0                        |
|     |                    | Vz       | min          | 1a   | 0           | (12) | 1.7         | 0            | 0           | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (12) | -1.7        | 0            | 0           | 0                        |
|     |                    | Tx       | min          | 1a_1 | 0           | (12) | <b>-1.7</b> | 0            | 0           | 0                        |
|     |                    |          | max          | 1a   | 0           | (12) | <b>1.7</b>  | 0            | 0           | 0                        |
|     |                    | My       | min          | 1a   | 0.830       | (13) | 1.7         | <b>-33.9</b> | -9.1        | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (12) | -1.7        | <b>0</b>     | 0           | 0                        |
|     |                    | Mz       | min          | 1a   | 0.830       | (13) | 1.7         | -33.9        | <b>-9.1</b> | 0                        |
|     |                    |          | max          | 1a_1 | 0.830       | (13) | -1.7        | -0.7         | <b>9.1</b>  | 0                        |
| 14  | I                  | HE 160 B |              |      | L=0.830     |      |             |              |             |                          |
|     |                    | Nx       | min          | 1a   | 0           | (13) | -1.7        | -33.9        | -9.1        | 0                        |
|     |                    |          | max          | 1a   | 0           | (13) | -1.7        | -33.9        | -9.1        | 0                        |
|     |                    | Vy       | min          | 1a   | 0           | (13) | -1.7        | -33.9        | -9.1        | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (13) | 1.7         | -0.7         | 9.1         | 0                        |
|     |                    | Vz       | min          | 1a_1 | 0           | (13) | 1.7         | -0.7         | 9.1         | 0                        |
|     |                    |          | max          | 1a   | 0           | (13) | -1.7        | -33.9        | -9.1        | 0                        |
|     |                    | Tx       | min          | 1a   | 0           | (13) | <b>-1.7</b> | -33.9        | -9.1        | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (13) | <b>1.7</b>  | -0.7         | 9.1         | 0                        |
|     |                    | My       | min          | 1a   | 0           | (13) | -1.7        | <b>-33.9</b> | -9.1        | 0                        |
|     |                    |          | max          | 1a   | 0.830       | (14) | -1.7        | <b>0</b>     | 0           | 0                        |
|     |                    | Mz       | min          | 1a   | 0           | (13) | -1.7        | -33.9        | <b>-9.1</b> | 0                        |
|     |                    |          | max          | 1a_1 | 0           | (13) | 1.7         | -0.7         | <b>9.1</b>  | 0                        |
| 15  | I                  | HE 160 B |              |      | L=0.760     |      |             |              |             |                          |
|     |                    | Nx       | min          | 1a   | 0           | (15) | 1.9         | 0            | 0           | 0                        |
|     |                    |          | max          | 1a   | 0           | (15) | 1.9         | 0            | 0           | 0                        |
|     |                    | Vy       | min          | 1a_1 | 0           | (15) | -1.9        | 0            | 0           | 0                        |
|     |                    |          | max          | 1a   | 0           | (15) | 1.9         | 0            | 0           | 0                        |

**Project: DLE**

Constructeur: DNV GL - Energy

Model: **Ligger kruisingmast\_1.axs**

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## Beam internal forces [Linear, Envelope (Default), HE 160 B]

|      | Sh. | Cross-section name | C  | min.<br>max. | Case | Loc.<br>[m] | Node | Nx<br>[kN]   | Vy<br>[kN]   | Vz<br>[kN]   |
|------|-----|--------------------|----|--------------|------|-------------|------|--------------|--------------|--------------|
|      |     |                    | Vz | min          | 1a_1 | 0           | (15) | 0            | -12.2        | <b>-20.0</b> |
|      |     |                    |    | max          | 1a   | 0           | (15) | 0            | 12.2         | <b>20.0</b>  |
|      |     |                    | Tx | min          | 1a_1 | 0           | (15) | 0            | -12.2        | -20.0        |
|      |     |                    |    | max          | 1a   | 0           | (15) | 0            | 12.2         | 20.0         |
|      |     |                    | My | min          | 1a_1 | 0.760       | (16) | 0            | -12.2        | -20.0        |
|      |     |                    |    | max          | 1a   | 0.760       | (16) | 0            | 12.2         | 20.0         |
|      |     |                    | Mz | min          | 1a   | 0.760       | (16) | 0            | 12.2         | 20.0         |
|      |     |                    |    | max          | 1a_1 | 0.760       | (16) | 0            | -12.2        | -20.0        |
| 16   | 1   | HE 160 B           |    |              |      | L=0.760     |      |              |              |              |
|      |     |                    | Nx | min          | 1a   | 0           | (16) | <b>0</b>     | -12.2        | -20.0        |
|      |     |                    |    | max          | 1a   | 0           | (16) | <b>0</b>     | -12.2        | -20.0        |
|      |     |                    | Vy | min          | 1a   | 0           | (16) | 0            | <b>-12.2</b> | -20.0        |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | 0            | <b>12.2</b>  | 20.0         |
|      |     |                    | Vz | min          | 1a   | 0           | (16) | 0            | -12.2        | <b>-20.0</b> |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | 0            | 12.2         | <b>20.0</b>  |
|      |     |                    | Tx | min          | 1a   | 0           | (16) | 0            | -12.2        | -20.0        |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | 0            | 12.2         | 20.0         |
|      |     |                    | My | min          | 1a_1 | 0           | (16) | 0            | 12.2         | 20.0         |
|      |     |                    |    | max          | 1a   | 0           | (16) | 0            | -12.2        | -20.0        |
|      |     |                    | Mz | min          | 1a   | 0           | (16) | 0            | -12.2        | -20.0        |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | 0            | 12.2         | 20.0         |
| Ext. |     |                    |    |              |      |             |      |              |              |              |
| 12   | 1   | HE 160 B           | Nx | min          | 1a   | 0           | (2)  | <b>-15.5</b> | 0            | -5.4         |
| 12   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (2)  | <b>15.5</b>  | 0            | 5.7          |
| 15   | 1   | HE 160 B           | Vy | min          | 1a_1 | 0           | (15) | 0            | <b>-12.2</b> | -20.0        |
| 16   | 1   | HE 160 B           |    | min          | 1a   | 0           | (16) | 0            | <b>-12.2</b> | -20.0        |
| 15   | 1   | HE 160 B           |    | max          | 1a   | 0           | (15) | 0            | <b>12.2</b>  | 20.0         |
| 16   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (16) | 0            | <b>12.2</b>  | 20.0         |

|      | Sh. | Cross-section name | C  | min.<br>max. | Case | Loc.<br>[m] | Node | Tx<br>[kNm] | My<br>[kNm]  | Mz<br>[kNm] | B<br>[kNm <sup>2</sup> ] |
|------|-----|--------------------|----|--------------|------|-------------|------|-------------|--------------|-------------|--------------------------|
|      |     |                    | Vz | min          | 1a_1 | 0           | (15) | -1.9        | 0            | 0           | 0                        |
|      |     |                    |    | max          | 1a   | 0           | (15) | 1.9         | 0            | 0           | 0                        |
|      |     |                    | Tx | min          | 1a_1 | 0           | (15) | <b>-1.9</b> | 0            | 0           | 0                        |
|      |     |                    |    | max          | 1a   | 0           | (15) | <b>1.9</b>  | 0            | 0           | 0                        |
|      |     |                    | My | min          | 1a_1 | 0.760       | (16) | -1.9        | <b>-15.2</b> | 9.3         | 0                        |
|      |     |                    |    | max          | 1a   | 0.760       | (16) | 1.9         | <b>15.2</b>  | -9.3        | 0                        |
|      |     |                    | Mz | min          | 1a   | 0.760       | (16) | 1.9         | 15.2         | <b>-9.3</b> | 0                        |
|      |     |                    |    | max          | 1a_1 | 0.760       | (16) | -1.9        | -15.2        | <b>9.3</b>  | 0                        |
| 16   | 1   | HE 160 B           |    |              |      | L=0.760     |      |             |              |             |                          |
|      |     |                    | Nx | min          | 1a   | 0           | (16) | -1.9        | 15.2         | -9.3        | 0                        |
|      |     |                    |    | max          | 1a   | 0           | (16) | -1.9        | 15.2         | -9.3        | 0                        |
|      |     |                    | Vy | min          | 1a   | 0           | (16) | -1.9        | 15.2         | -9.3        | 0                        |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | 1.9         | -15.2        | 9.3         | 0                        |
|      |     |                    | Vz | min          | 1a   | 0           | (16) | -1.9        | 15.2         | -9.3        | 0                        |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | 1.9         | -15.2        | 9.3         | 0                        |
|      |     |                    | Tx | min          | 1a   | 0           | (16) | <b>-1.9</b> | 15.2         | -9.3        | 0                        |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | <b>1.9</b>  | -15.2        | 9.3         | 0                        |
|      |     |                    | My | min          | 1a_1 | 0           | (16) | 1.9         | <b>-15.2</b> | 9.3         | 0                        |
|      |     |                    |    | max          | 1a   | 0           | (16) | -1.9        | <b>15.2</b>  | -9.3        | 0                        |
|      |     |                    | Mz | min          | 1a   | 0           | (16) | -1.9        | 15.2         | <b>-9.3</b> | 0                        |
|      |     |                    |    | max          | 1a_1 | 0           | (16) | 1.9         | -15.2        | <b>9.3</b>  | 0                        |
| Ext. |     |                    |    |              |      |             |      |             |              |             |                          |
| 12   | 1   | HE 160 B           | Nx | min          | 1a   | 0           | (2)  | 0           | 2.8          | 0           | 0                        |
| 12   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (2)  | 0           | -3.0         | 0           | 0                        |
| 15   | 1   | HE 160 B           | Vy | min          | 1a_1 | 0           | (15) | -1.9        | 0            | 0           | 0                        |
| 16   | 1   | HE 160 B           |    | min          | 1a   | 0           | (16) | -1.9        | 15.2         | -9.3        | 0                        |
| 15   | 1   | HE 160 B           |    | max          | 1a   | 0           | (15) | 1.9         | 0            | 0           | 0                        |
| 16   | 1   | HE 160 B           |    | max          | 1a_1 | 0           | (16) | 1.9         | -15.2        | 9.3         | 0                        |

### Project: DLE

Constructeur: DNV GL - Energy

Model: **Ligger kruisingmast\_1.axs**

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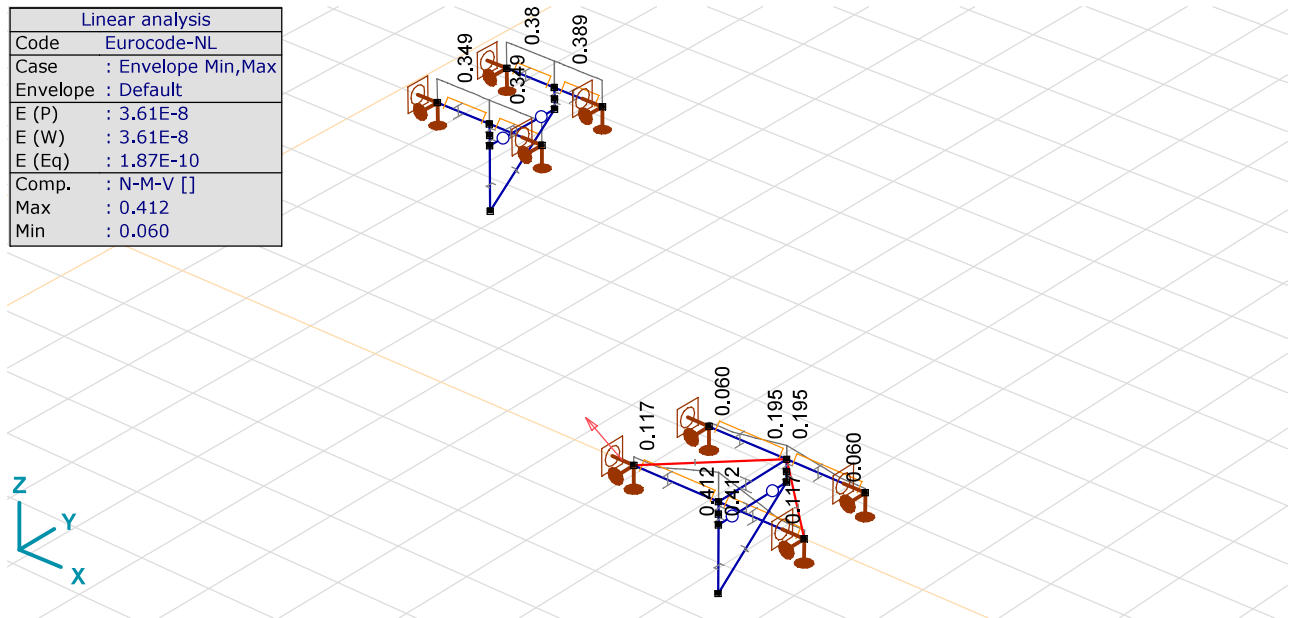
#### Beam internal forces [Linear, Envelope (Default), HE 160 B]

|    | Sh. | Cross-section name | C  | min. max. | Case | Loc. [m] | Node | Nx [kN] | Vy [kN] | Vz [kN]      |
|----|-----|--------------------|----|-----------|------|----------|------|---------|---------|--------------|
| 1  | 1   | HE 160 B           | Vz | min       | 1a   | 0        | (1)  | 0       | 1.9     | <b>-42.1</b> |
| 2  | 1   | HE 160 B           |    | max       | 1a   | 0        | (2)  | 0       | -1.9    | <b>42.1</b>  |
| 15 | 1   | HE 160 B           | Tx | min       | 1a_1 | 0        | (15) | 0       | -12.2   | -20.0        |
| 16 | 1   | HE 160 B           |    | min       | 1a   | 0        | (16) | 0       | -12.2   | -20.0        |
| 15 | 1   | HE 160 B           |    | max       | 1a   | 0        | (15) | 0       | 12.2    | 20.0         |
| 16 | 1   | HE 160 B           |    | max       | 1a_1 | 0        | (16) | 0       | 12.2    | 20.0         |
| 1  | 1   | HE 160 B           | My | min       | 1a   | 1.230    | (2)  | 0       | 1.9     | -42.1        |
| 2  | 1   | HE 160 B           |    | min       | 1a   | 0        | (2)  | 0       | -1.9    | 42.1         |
| 3  | 1   | HE 160 B           |    | max       | 1a   | 1.130    | (5)  | 0       | 2.4     | 21.5         |
| 4  | 1   | HE 160 B           |    | max       | 1a   | 0        | (5)  | 0       | -2.4    | -21.5        |
| 15 | 1   | HE 160 B           | Mz | min       | 1a   | 0.760    | (16) | 0       | 12.2    | 20.0         |
| 16 | 1   | HE 160 B           |    | min       | 1a   | 0        | (16) | 0       | -12.2   | -20.0        |
| 15 | 1   | HE 160 B           |    | max       | 1a_1 | 0.760    | (16) | 0       | -12.2   | -20.0        |
| 16 | 1   | HE 160 B           |    | max       | 1a_1 | 0        | (16) | 0       | 12.2    | 20.0         |

|    | Sh. | Cross-section name | C  | min. max. | Case | Loc. [m] | Node | Tx [kNm]    | My [kNm]     | Mz [kNm]    | B [kNm <sup>2</sup> ] |
|----|-----|--------------------|----|-----------|------|----------|------|-------------|--------------|-------------|-----------------------|
| 1  | 1   | HE 160 B           | Vz | min       | 1a   | 0        | (1)  | 0.1         | 0            | 0           | 0                     |
| 2  | 1   | HE 160 B           |    | max       | 1a   | 0        | (2)  | -0.1        | -51.8        | -2.3        | 0                     |
| 15 | 1   | HE 160 B           | Tx | min       | 1a_1 | 0        | (15) | <b>-1.9</b> | 0            | 0           | 0                     |
| 16 | 1   | HE 160 B           |    | min       | 1a   | 0        | (16) | <b>-1.9</b> | 15.2         | -9.3        | 0                     |
| 15 | 1   | HE 160 B           |    | max       | 1a   | 0        | (15) | <b>1.9</b>  | 0            | 0           | 0                     |
| 16 | 1   | HE 160 B           |    | max       | 1a_1 | 0        | (16) | <b>1.9</b>  | -15.2        | 9.3         | 0                     |
| 1  | 1   | HE 160 B           | My | min       | 1a   | 1.230    | (2)  | 0.1         | <b>-51.8</b> | -2.3        | 0                     |
| 2  | 1   | HE 160 B           |    | min       | 1a   | 0        | (2)  | -0.1        | <b>-51.8</b> | -2.3        | 0                     |
| 3  | 1   | HE 160 B           |    | max       | 1a   | 1.130    | (5)  | 0.1         | <b>24.3</b>  | -2.7        | 0                     |
| 4  | 1   | HE 160 B           |    | max       | 1a   | 0        | (5)  | -0.1        | <b>24.3</b>  | -2.7        | 0                     |
| 15 | 1   | HE 160 B           | Mz | min       | 1a   | 0.760    | (16) | 1.9         | 15.2         | <b>-9.3</b> | 0                     |
| 16 | 1   | HE 160 B           |    | min       | 1a   | 0        | (16) | -1.9        | 15.2         | <b>-9.3</b> | 0                     |
| 15 | 1   | HE 160 B           |    | max       | 1a_1 | 0.760    | (16) | -1.9        | -15.2        | <b>9.3</b>  | 0                     |
| 16 | 1   | HE 160 B           |    | max       | 1a_1 | 0        | (16) | 1.9         | -15.2        | <b>9.3</b>  | 0                     |

Sh.: Cross-section; C: Extremal component; min, max.: Extreme type; Case: Load case of extreme; Loc.: Cross-section local x position on the beam; Nx: Axial force; Vy: Shear force in local y direction; Vz: Shear force in local z direction; Tx: Torsional moment; My: Flexural moment about local y axis; Mz: Flexural moment about local z axis;

| Linear analysis |                    |
|-----------------|--------------------|
| Code            | Eurocode-NL        |
| Case            | : Envelope Min,Max |
| Envelope        | : Default          |
| E (P)           | : 3.61E-8          |
| E (W)           | : 3.61E-8          |
| E (Eq)          | : 1.87E-10         |
| Comp.           | : N-M-V []         |
| Max             | : 0.412            |
| Min             | : 0.060            |



[Stl], Linear, Envelope (Default), N-M-V [], Diagram

### Project: DLE

Constructeur: DNV GL - Energy

Model: **Ligger kruisingmast\_1.axs**

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#### Beam stresses [Linear, Envelope (Load cases)]

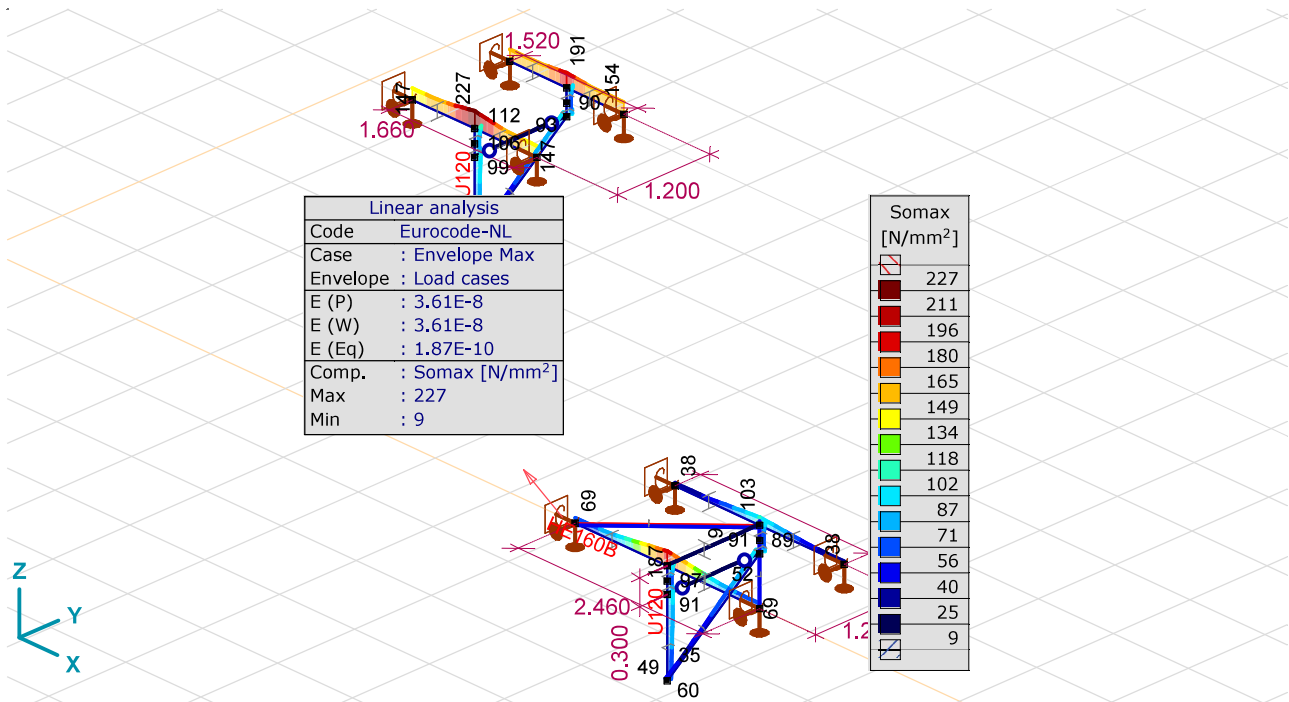
| Ext. | Sh. | Cross-section name | C     | min. max. | Case | Loc. [m] | Node | Smin [N/mm <sup>2</sup> ] | Smax [N/mm <sup>2</sup> ] | Vmin [N/mm <sup>2</sup> ] | Vmax [N/mm <sup>2</sup> ] |
|------|-----|--------------------|-------|-----------|------|----------|------|---------------------------|---------------------------|---------------------------|---------------------------|
| 12   | 1   | HE 160 B           | Somin | min       | 1a   | 0.360    |      | -6                        | 0                         | 0                         | 5                         |
| 13   | 1   | HE 160 B           |       | max       | 1a   | 0.830    | (13) | -190                      | 190                       | 71                        | 85                        |
| 14   | 1   | HE 160 B           |       | max       | 1a   | 0        | (13) | -190                      | 190                       | 71                        | 85                        |
| 1    | 1   | HE 160 B           | Somax | min       | 1a_1 | 0        | (1)  | 0                         | 0                         | 2                         | 3                         |
| 2    | 1   | HE 160 B           |       | min       | 1a_1 | 1.230    | (3)  | 0                         | 0                         | 2                         | 3                         |
| 13   | 1   | HE 160 B           |       | max       | 1a   | 0.830    | (13) | -190                      | 190                       | 71                        | 85                        |
| 14   | 1   | HE 160 B           |       | max       | 1a   | 0        | (13) | -190                      | 190                       | 71                        | 85                        |

| Ext. | Sh. | Cross-section name | C     | min. max. | Case | Loc. [m] | Node | Somin [N/mm <sup>2</sup> ] | Somax [N/mm <sup>2</sup> ] | Vymean [N/mm <sup>2</sup> ] | Vzmean [N/mm <sup>2</sup> ] |
|------|-----|--------------------|-------|-----------|------|----------|------|----------------------------|----------------------------|-----------------------------|-----------------------------|
| 12   | 1   | HE 160 B           | Somin | min       | 1a   | 0.360    |      | 0                          | 9                          | 0                           | -1                          |
| 13   | 1   | HE 160 B           |       | max       | 1a   | 0.830    | (13) | 127                        | 227                        | 2                           | -8                          |
| 14   | 1   | HE 160 B           |       | max       | 1a   | 0        | (13) | 127                        | 227                        | -2                          | 8                           |
| 1    | 1   | HE 160 B           | Somax | min       | 1a_1 | 0        | (1)  | 3                          | 4                          | 0                           | 0                           |
| 2    | 1   | HE 160 B           |       | min       | 1a_1 | 1.230    | (3)  | 3                          | 4                          | 0                           | 0                           |
| 13   | 1   | HE 160 B           |       | max       | 1a   | 0.830    | (13) | 127                        | 227                        | 2                           | -8                          |
| 14   | 1   | HE 160 B           |       | max       | 1a   | 0        | (13) | 127                        | 227                        | -2                          | 8                           |

**Sh.:** Cross-section; **C:** Extremal component; **min, max.:** Extreme type; **Case:** Load case of extreme; **Loc.:** Cross-section local x position on the beam;

**Smin:** Axial stress cross-Section minimum; **Smax:** Axial stress cross-Section maximum; **Vmin:** Shear stress cross-section minimum; **Vmax:** Shear stress cross-section maximum;

**Somin:** Von Mises stress cross-section minimum; **Somax:** Von Mises stress cross-section maximum; **Vymean:** Shear stress in local y direction; **Vzmean:** Shear stress in local z direction;



[1], Linear, Envelope Max (Load cases), Somax [N/mm<sup>2</sup>], Filled diagram



# Project: DLE

Constructeur: DNV GL - Energy

AxisVM X6 R1h · Registered to DNV GL - Energy  
bottom\_chord\_s+32\_check.axs

Rapport

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| Tekening knopen  | 5           |
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| Tekening profielen   | 6           |
| Tekening staven  | 6           |
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| Custom load combinations by load cases   | 8           |
| [I], Linear, Co #1 (ULS), Nx [kN], Filled diagram  | 8           |
| [I], Linear, Co #1 (ULS), My [kNm], Filled diagram   | 9           |
| [I], Linear, Co #1 (ULS), Mz [kNm], Filled diagram   | 9           |
| [I], Linear, Co #1 (ULS), Vy [kN], Filled diagram  | 10          |
| [I], Linear, Co #1 (ULS), Vz [kN], Filled diagram  | 10          |
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**Project: DLE**

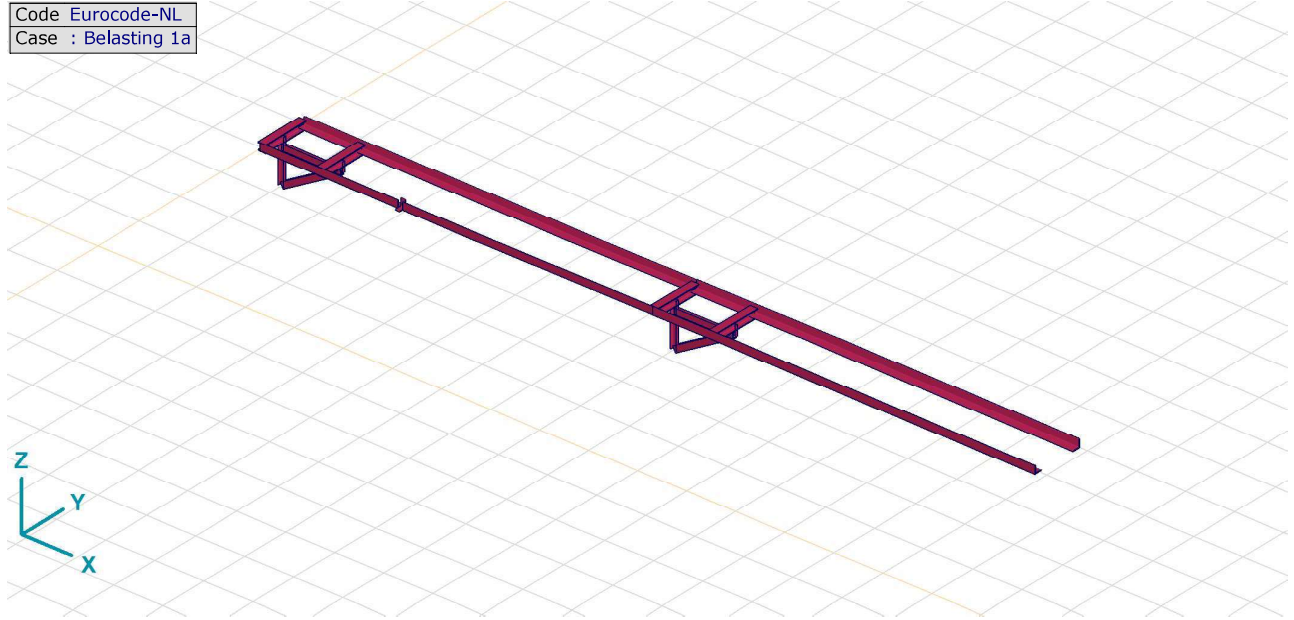
Constructeur: DNV GL - Energy

Model: **bottom\_chord\_s+32\_check.axs**

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Code Eurocode-NL  
Case : Belasting 1a



*Tekening render*

**Project: DLE**






Constructeur: DNV GL - Energy

Model: **bottom\_chord\_s+32\_check.axs**

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## Cross-sections

|   | Name         | Drawing   | Process | Shape | h<br>[mm] | b<br>[mm] | tw<br>[mm] | tf<br>[mm] | r <sub>1</sub><br>[mm] | r <sub>2</sub><br>[mm] | r <sub>3</sub><br>[mm] |
|---|--------------|---|---------|-------|-----------|-----------|------------|------------|------------------------|------------------------|------------------------|
| 1 | L 160X160X15 |  | Rolled  | L     | 160.0     | 160.0     | 15.0       | 15.0       | 17.0                   | 8.5                    | 0                      |
| 2 | L 150X150X12 |  | Rolled  | L     | 150.0     | 150.0     | 12.0       | 12.0       | 16.0                   | 8.0                    | 0                      |
| 3 | L 180X180X16 |  | Rolled  | L     | 180.0     | 180.0     | 16.0       | 16.0       | 18.0                   | 9.0                    | 0                      |
| 4 | HE 160 B     |  | Rolled  | I     | 160.0     | 160.0     | 8.0        | 13.0       | 15.0                   | 0                      | 0                      |
| 5 | U 120        |  | Rolled  | U     | 120.0     | 55.0      | 7.0        | 9.0        | 9.0                    | 4.5                    | 0                      |

|   | Name         | A <sub>x</sub><br>[mm <sup>2</sup> ] | A <sub>y</sub><br>[mm <sup>2</sup> ] | A <sub>z</sub><br>[mm <sup>2</sup> ] | I <sub>x</sub><br>[mm <sup>4</sup> ] | I <sub>y</sub><br>[mm <sup>4</sup> ] | I <sub>z</sub><br>[mm <sup>4</sup> ] | I <sub>yz</sub><br>[mm <sup>4</sup> ] |
|---|--------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------------------------------|
| 1 | L 160X160X15 | 4606.15                              | 2011.73                              | 2029.76                              | 365558.200                           | 1.099E+07                            | 1.099E+07                            | -6461627.000                          |
| 2 | L 150X150X12 | 3483.60                              | 1505.64                              | 1521.61                              | 179274.100                           | 7368515.000                          | 7368513.000                          | -4334081.000                          |
| 3 | L 180X180X16 | 5538.93                              | 2403.86                              | 2433.89                              | 499973.800                           | 1.682E+07                            | 1.682E+07                            | -9905372.000                          |
| 4 | HE 160 B     | 5426.04                              | 3754.44                              | 1237.48                              | 317826.300                           | 2.492E+07                            | 8892444.000                          | 0                                     |
| 5 | U 120        | 1698.73                              | 617.80                               | 752.09                               | 41830.660                            | 3643327.000                          | 430614.100                           | 0                                     |

|   | Name         | I <sub>1</sub><br>[mm <sup>4</sup> ] | I <sub>2</sub><br>[mm <sup>4</sup> ] | α<br>[°] | I <sub>ω</sub><br>[mm <sup>6</sup> ] | W <sub>1,el,t</sub><br>[mm <sup>3</sup> ] | W <sub>1,el,b</sub><br>[mm <sup>3</sup> ] |
|---|--------------|--------------------------------------|--------------------------------------|----------|--------------------------------------|---|---|
| 1 | L 160X160X15 | 1.745E+07                            | 4525910.000                          | 45.00    | 6.2E+08                              | 154230.300                                | 154230.300                                |
| 2 | L 150X150X12 | 1.17E+07                             | 3034433.000                          | 45.00    | 2.7E+08                              | 110333.100                                | 110333.100                                |
| 3 | L 180X180X16 | 2.673E+07                            | 6917778.000                          | 45.00    | 1.1E+09                              | 209999.100                                | 209999.100                                |
| 4 | HE 160 B     | 2.492E+07                            | 8892443.000                          | 0        | 4.7E+10                              | 311542.700                                | 311542.700                                |
| 5 | U 120        | 3643327.000                          | 430614.100                           | 0        | 8.9E+08                              | 60722.120                                 | 60722.120                                 |

|   | Name         | W <sub>2,el,t</sub><br>[mm <sup>3</sup> ] | W <sub>2,el,b</sub><br>[mm <sup>3</sup> ] | W <sub>1,pl</sub><br>[mm <sup>3</sup> ] | W <sub>2,pl</sub><br>[mm <sup>3</sup> ] | i <sub>y</sub><br>[mm] | i <sub>z</sub><br>[mm] | H <sub>y</sub><br>[mm] | H <sub>z</sub><br>[mm] |
|---|--------------|---|---|---|---|------------------------|------------------------|------------------------|------------------------|
| 1 | L 160X160X15 | 79787.940                                 | 71275.720                                 | 243874.600                              | 124879.600                              | 48.8                   | 48.8                   | 160.0                  | 160.0                  |
| 2 | L 150X150X12 | 57321.540                                 | 52048.100                                 | 173526.600                              | 89044.110                               | 46.0                   | 46.0                   | 150.0                  | 150.0                  |
| 3 | L 180X180X16 | 108387.800                                | 97377.670                                 | 331133.400                              | 169336.000                              | 55.1                   | 55.1                   | 180.0                  | 180.0                  |
| 4 | HE 160 B     | 111155.500                                | 111155.500                                | 354020.600                              | 169972.200                              | 67.8                   | 40.5                   | 160.0                  | 160.0                  |
| 5 | U 120        | 11058.300                                 | 26813.420                                 | 72702.590                               | 21257.590                               | 46.3                   | 15.9                   | 55.0                   | 120.0                  |

|   | Name         | y <sub>G</sub><br>[mm] | z <sub>G</sub><br>[mm] | y <sub>s</sub><br>[mm] | z <sub>s</sub><br>[mm] | β <sub>y</sub><br>[mm] | β <sub>z</sub><br>[mm] | β <sub>w</sub><br>[°] | S.p. |
|---|--------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------|------|
| 1 | L 160X160X15 | 44.9                   | 44.9                   | -36.2                  | -36.2                  | 146.2                  | 146.2                  | 0                     | 4    |
| 2 | L 150X150X12 | 41.2                   | 41.2                   | -34.2                  | -34.2                  | 138.8                  | 138.8                  | 0                     | 4    |
| 3 | L 180X180X16 | 50.2                   | 50.2                   | -41.0                  | -41.0                  | 165.5                  | 165.5                  | 0                     | 4    |
| 4 | HE 160 B     | 80.0                   | 80.0                   | 0                      | 0                      | 0                      | 0                      | 0                     | 9    |
| 5 | U 120        | 16.1                   | 60.0                   | -29.6                  | 0                      | 0                      | 122.3                  | 0                     | 8    |

**Name:** Cross-section name; **Process:** Manufacturing process; **h:** Cross-section height; **b:** Cross-section width; **tw:** Web thickness; **tf:** Flange thickness; **r<sub>1</sub>, r<sub>2</sub>, r<sub>3</sub>:** Rounding radius;

**A<sub>x</sub>:** Cross-section area; **A<sub>y</sub>, A<sub>z</sub>:** Shear area; **I<sub>x</sub>:** Torsional inertia; **I<sub>y</sub>, I<sub>z</sub>:** Flexural inertia; **I<sub>yz</sub>:** Centrifugal inertia; **I<sub>1</sub>, I<sub>2</sub>:** Principal flexural inertia; **α:** Principal directions; **I<sub>ω</sub>:** Warping constant;

**W<sub>1,el,t</sub>, W<sub>1,el,b</sub>, W<sub>2,el,t</sub>, W<sub>2,el,b</sub>:** Elastic modulus; **W<sub>1,pl</sub>, W<sub>2,pl</sub>:** Plastic modulus; **i<sub>y</sub>, i<sub>z</sub>:** Radius of inertia; **H<sub>y</sub>:** Dimension in local y direction; **H<sub>z</sub>:** Dimension in local z direction;

**y<sub>G</sub>:** y coordinate of the center of gravity; **z<sub>G</sub>:** z coordinate of the center of gravity; **y<sub>s</sub>:** y coordinate of the shear (torsion) center relative to the center of gravity;

**z<sub>s</sub>:** z coordinate of the shear (torsion) center relative to the center of gravity; **β<sub>y</sub>, β<sub>z</sub>, β<sub>w</sub>:** Wagner's coefficient; **S.p.:** Stress calculation points;

# Project: DLE

Constructeur: DNV GL - Energy

Model: **bottom\_chord\_s+32\_check.axs**

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## Materials

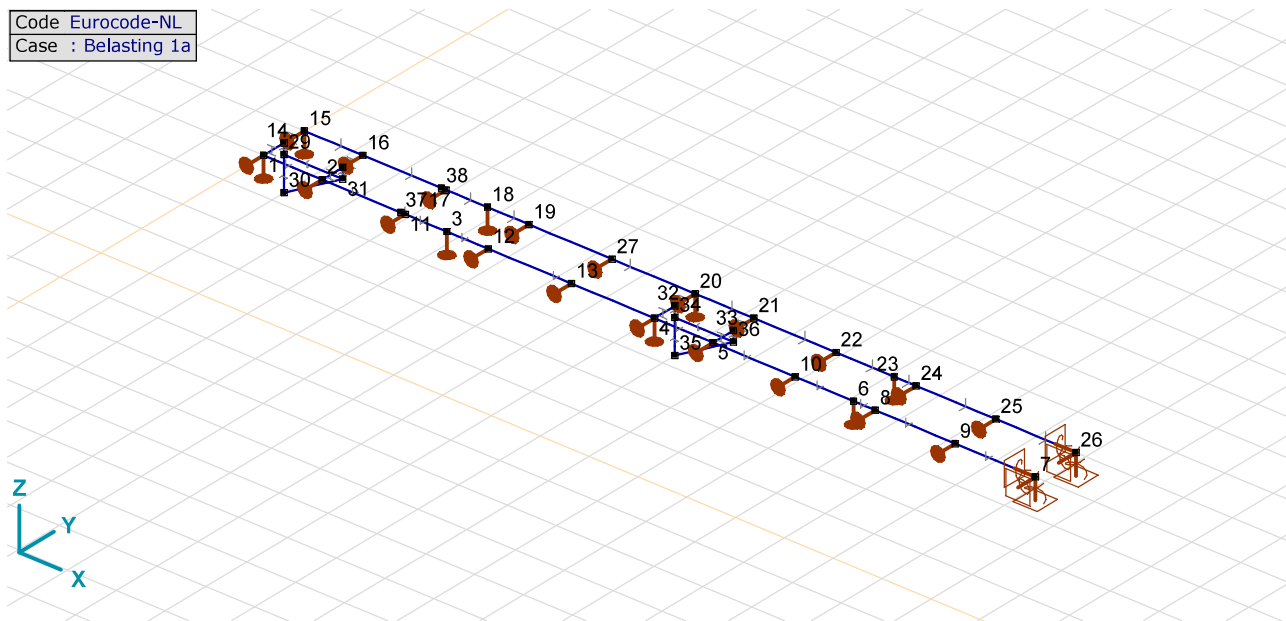
|   | Name  | Type  | National design code | Material code | Model  | $E_x$ [N/mm <sup>2</sup> ] | $E_y$ [N/mm <sup>2</sup> ] |
|---|-------|-------|----------------------|---------------|--------|----------------------------|----------------------------|
| 1 | S 235 | Steel | Eurocode-NL          | 10025-2       | Linear | 210000                     | 210000                     |

|   | Name  | $\nu$ | $\alpha_T$ [1/°C] | $\rho$ [kg/m <sup>3</sup> ] | Material color | Contour color | Texture | $P_1$                               | $P_2$                               |
|---|-------|-------|-------------------|-----------------------------|----------------|---------------|---------|-------------------------------------|-------------------------------------|
| 1 | S 235 | 0.30  | 1.2E-5            | 7850                        |                |               | Steel   | $f_y$ [N/mm <sup>2</sup> ] = 235.00 | $f_u$ [N/mm <sup>2</sup> ] = 360.00 |

|   | Name  | $P_3$                                 | $P_4$                                 | $P_5$ | $P_6$ | $P_7$ | $P_8$ | $P_9$ | $P_{10}$ | $P_{11}$ | $P_{12}$ | $P_{13}$ | $P_{14}$ |
|---|-------|---------------------------------------|---------------------------------------|-------|-------|-------|-------|-------|----------|----------|----------|----------|----------|
| 1 | S 235 | $f_y^*$ [N/mm <sup>2</sup> ] = 215.00 | $f_u^*$ [N/mm <sup>2</sup> ] = 360.00 |       |       |       |       |       |          |          |          |          |          |

Name: Material name; Type: Type of material; Model: Material model;  $E_x$ : Young's modulus of elasticity in local x direction;  $E_y$ : Young's modulus of elasticity in local y direction;  $\nu$ : Poisson's ratio;  $\alpha_T$ : Thermal expansion coefficient;  $\rho$ : Density; Contour color: Material outline color;  $P_1, P_2, P_3, P_4, P_5, P_6, P_7, P_8, P_9, P_{10}, P_{11}, P_{12}, P_{13}, P_{14}$ : Design parameter;

Code Eurocode-NL  
Case : Belasting 1a



Tekening knopen

## Nodes

|    | X [m]  | Y [m] | Z [m] |    | X [m]  | Y [m] | Z [m] |    | X [m] | Y [m] | Z [m]  |
|----|--------|-------|-------|----|--------|-------|-------|----|-------|-------|--------|
| 1  | 0      | 4.000 | 0     | 14 | 0      | 4.500 | 0     | 27 | 6.300 | 5.000 | 0      |
| 2  | 1.200  | 4.000 | 0     | 15 | 0      | 5.000 | 0     | 28 | 1.200 | 4.500 | 0      |
| 3  | 3.750  | 4.000 | 0     | 16 | 1.200  | 5.000 | 0     | 29 | 0     | 4.500 | -0.210 |
| 4  | 8.000  | 4.000 | 0     | 17 | 2.900  | 5.000 | 0     | 30 | 0     | 4.500 | -0.900 |
| 5  | 9.200  | 4.000 | 0     | 18 | 3.750  | 5.000 | 0     | 31 | 1.200 | 4.500 | -0.210 |
| 6  | 12.075 | 4.000 | 0     | 19 | 4.600  | 5.000 | 0     | 32 | 8.000 | 4.500 | 0      |
| 7  | 15.796 | 4.000 | 0     | 20 | 8.000  | 5.000 | 0     | 33 | 9.200 | 4.500 | 0      |
| 8  | 12.520 | 4.000 | 0     | 21 | 9.200  | 5.000 | 0     | 34 | 8.000 | 4.500 | -0.210 |
| 9  | 14.158 | 4.000 | 0     | 22 | 10.883 | 5.000 | 0     | 35 | 8.000 | 4.500 | -0.900 |
| 10 | 10.883 | 4.000 | 0     | 23 | 12.075 | 5.000 | 0     | 36 | 9.200 | 4.500 | -0.210 |
| 11 | 2.900  | 4.000 | 0     | 24 | 12.520 | 5.000 | 0     | 37 | 2.808 | 4.000 | 0      |
| 12 | 4.600  | 4.000 | 0     | 25 | 14.158 | 5.000 | 0     | 38 | 2.808 | 5.000 | 0      |
| 13 | 6.300  | 4.000 | 0     | 26 | 15.796 | 5.000 | 0     |    |       |       |        |

# Project: DLE

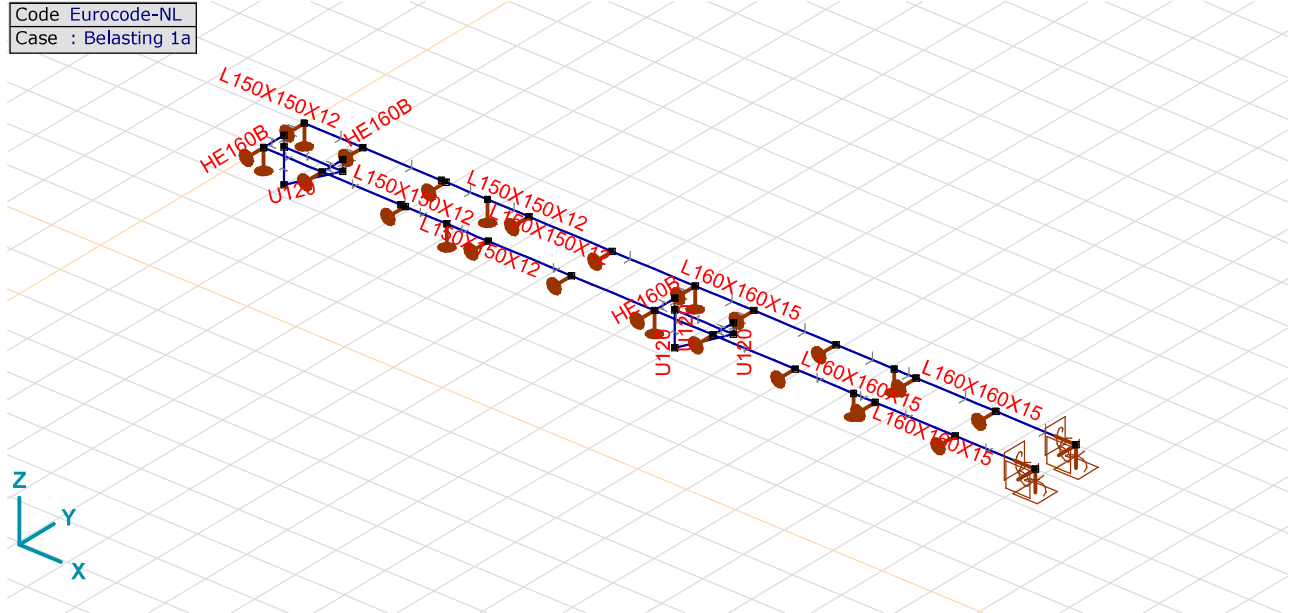
Constructeur: DNV GL - Energy

Model: bottom\_chord\_s+32\_check.axs

7/15/2021

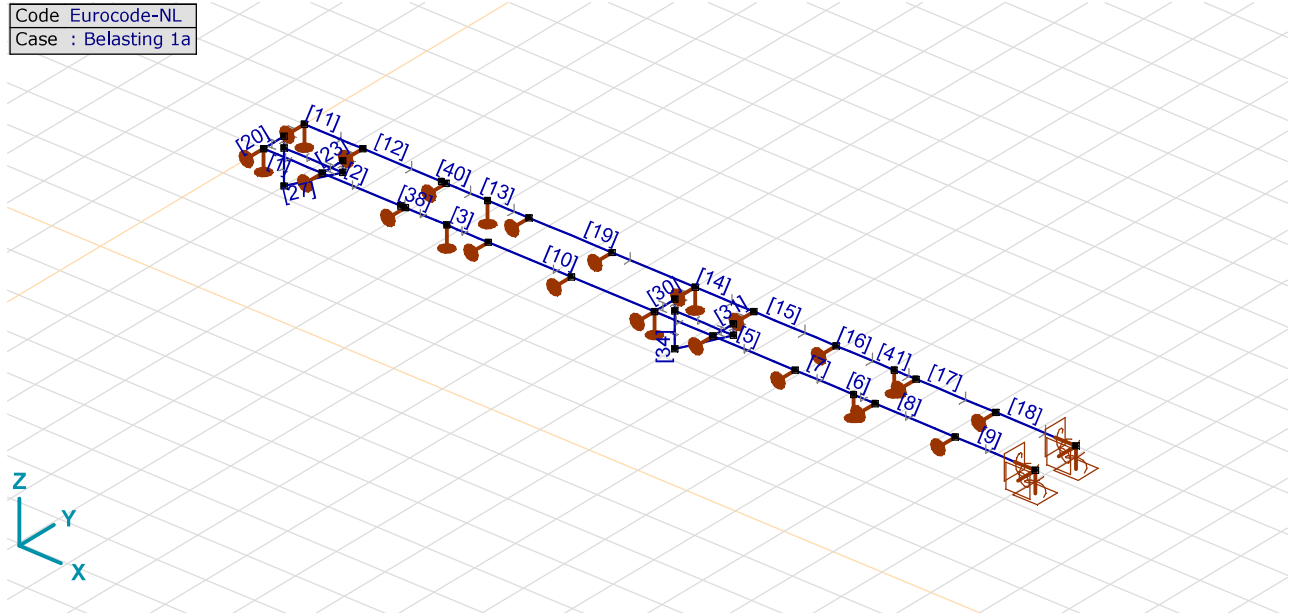
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Code Eurocode-NL  
Case : Belasting 1a



Tekening profielen

Code Eurocode-NL  
Case : Belasting 1a



Tekening staven

# Project: DLE

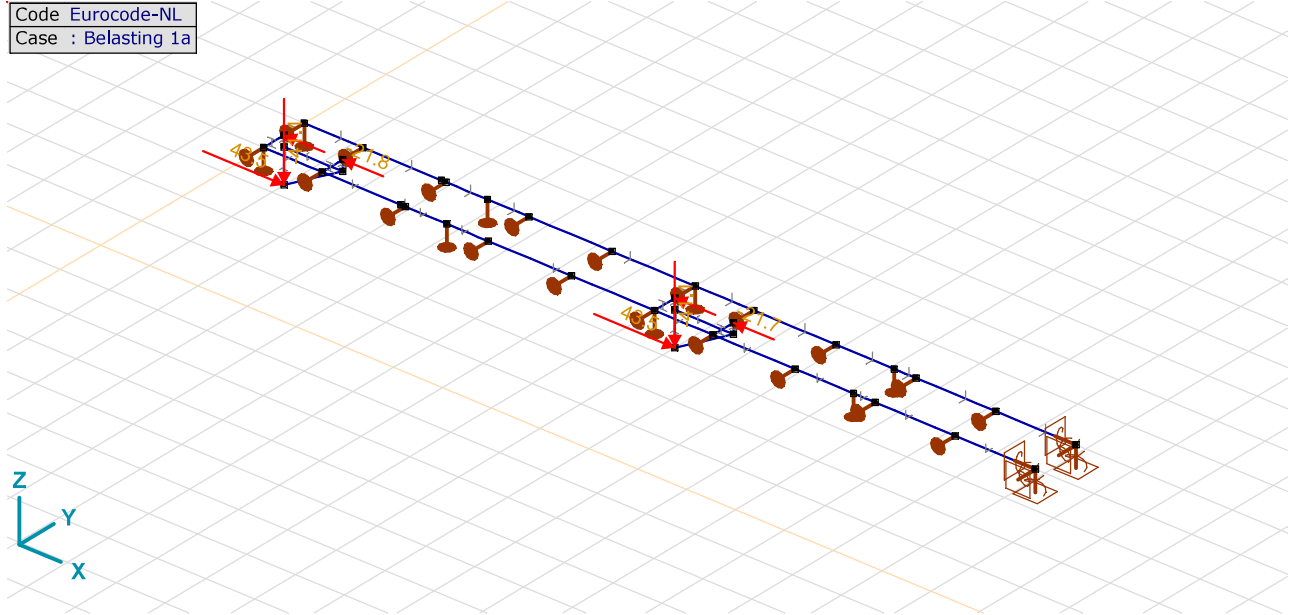
Constructeur: DNV GL - Energy

Model: **bottom\_chord\_s+32\_check.axs**

7/15/2021

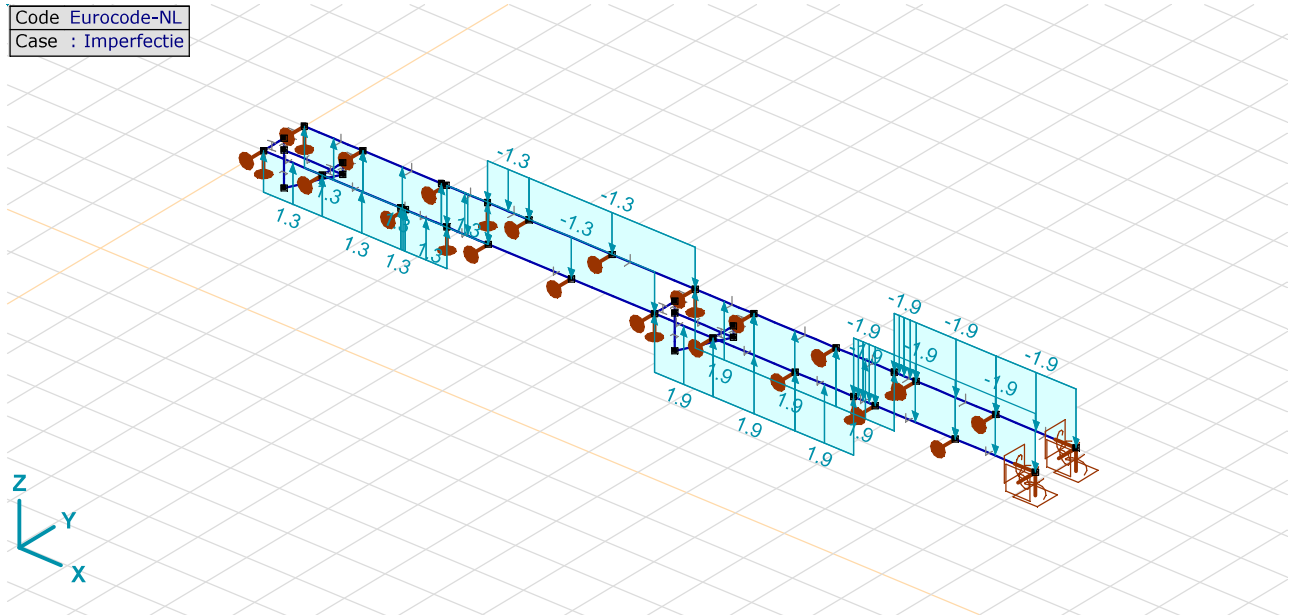
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Code Eurocode-NL  
Case : Belasting 1a



Belasting 1a

Code Eurocode-NL  
Case : Imperfectie



Imperfectie

# Project: DLE

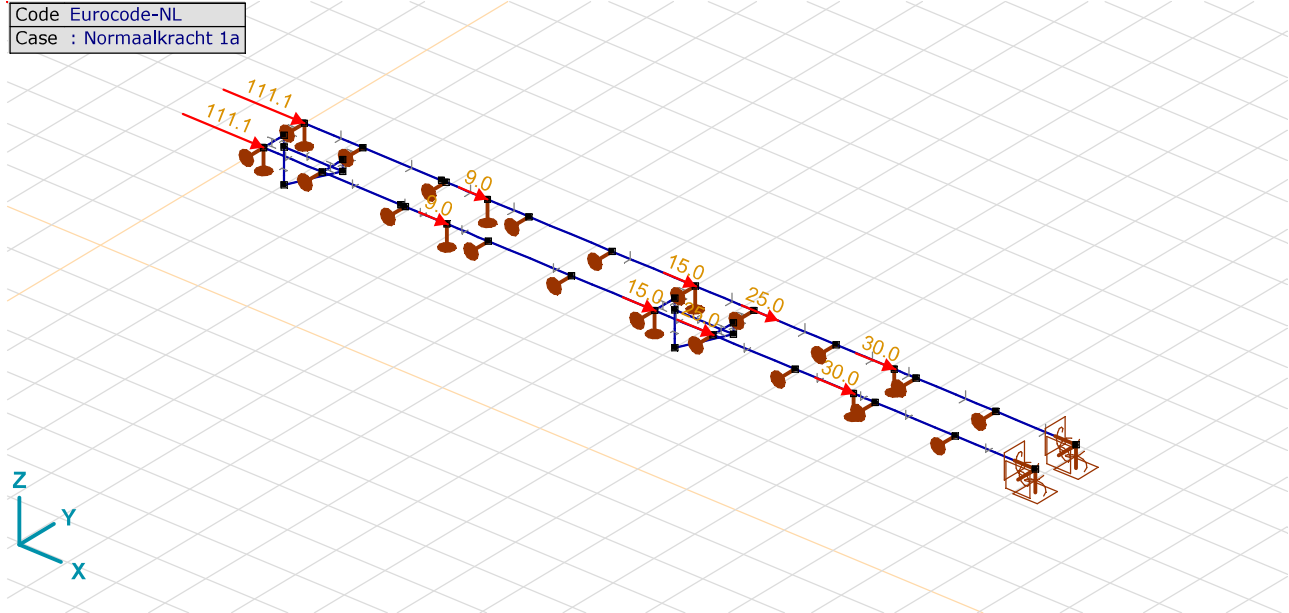
Constructeur: DNV GL - Energy

Model: bottom\_chord\_s+32\_check.axs

7/15/2021

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Code Eurocode-NL  
Case : Normaalkracht 1a



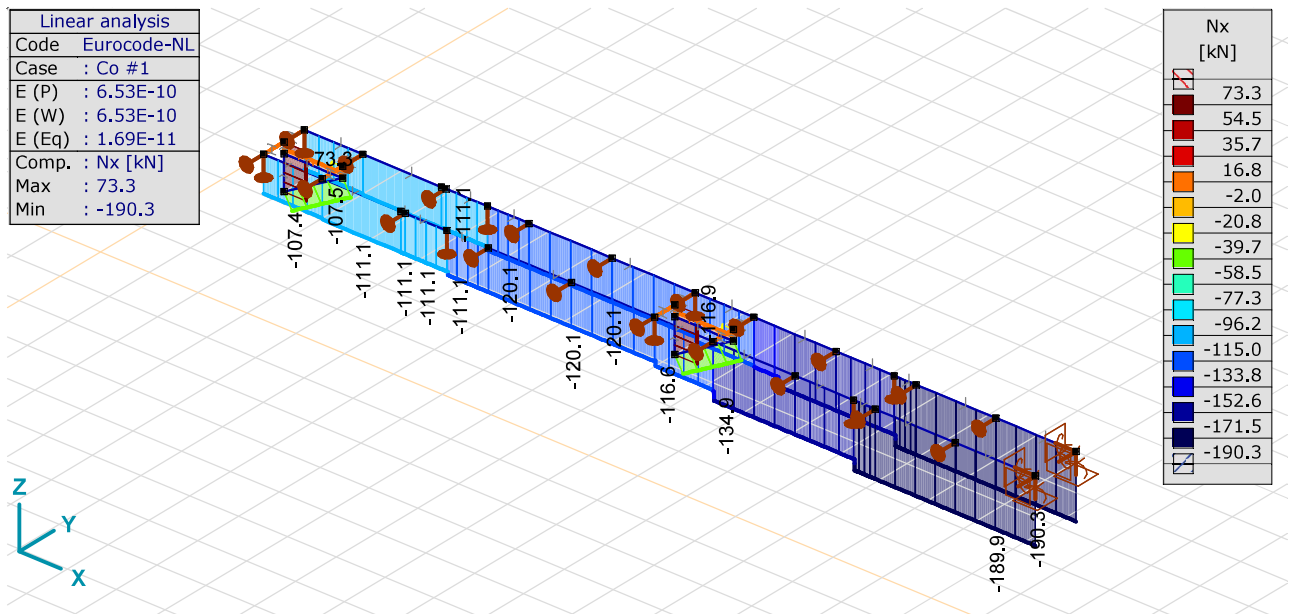
Normaalkracht 1a

## Custom load combinations by load cases

|   | Name  | Type | Belasting 1a | Normaalkracht 1a | Imperfectie | Comment |
|---|-------|------|--------------|------------------|-------------|---------|
| 1 | Co #1 | ULS  | 1.00         | 1.00             | 1.00        |         |

Name: Load combination name; Type: Load combination type; Belasting 1a, Normaalkracht 1a, Imperfectie: Factor;

Linear analysis  
Code Eurocode-NL  
Case : Co #1  
E (P) : 6.53E-10  
E (W) : 6.53E-10  
E (Eq) : 1.69E-11  
Comp. : Nx [kN]  
Max : 73.3  
Min : -190.3



[1], Linear, Co #1 (ULS), Nx [kN], Filled diagram





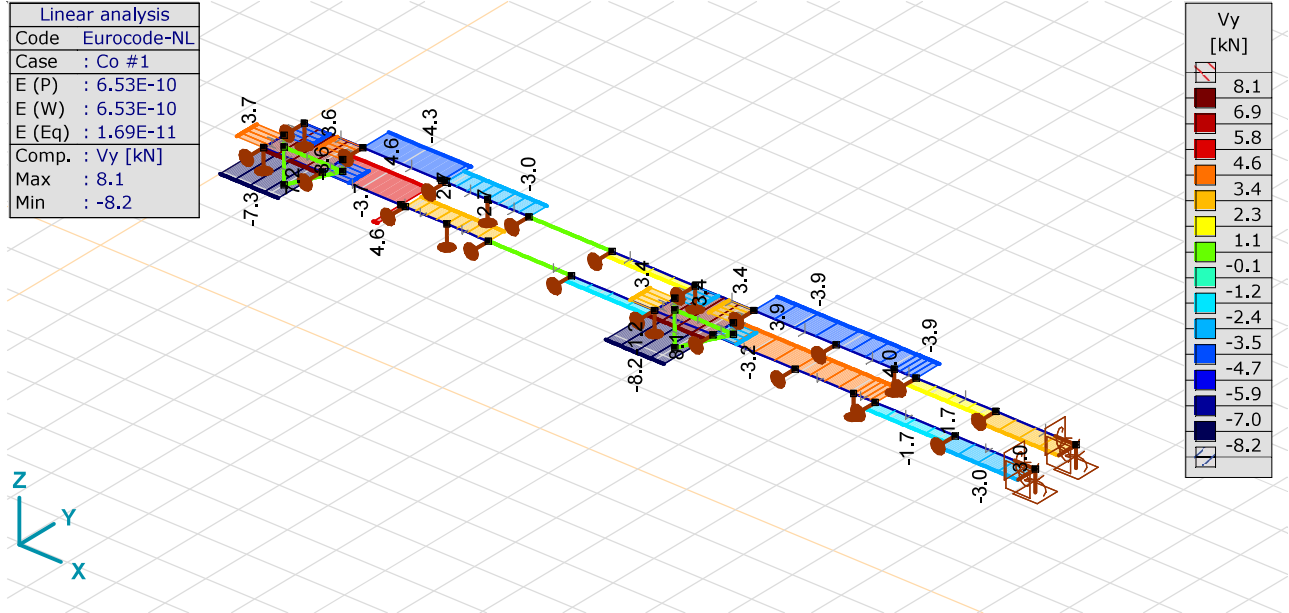
# Project: DLE

Constructeur: DNV GL - Energy

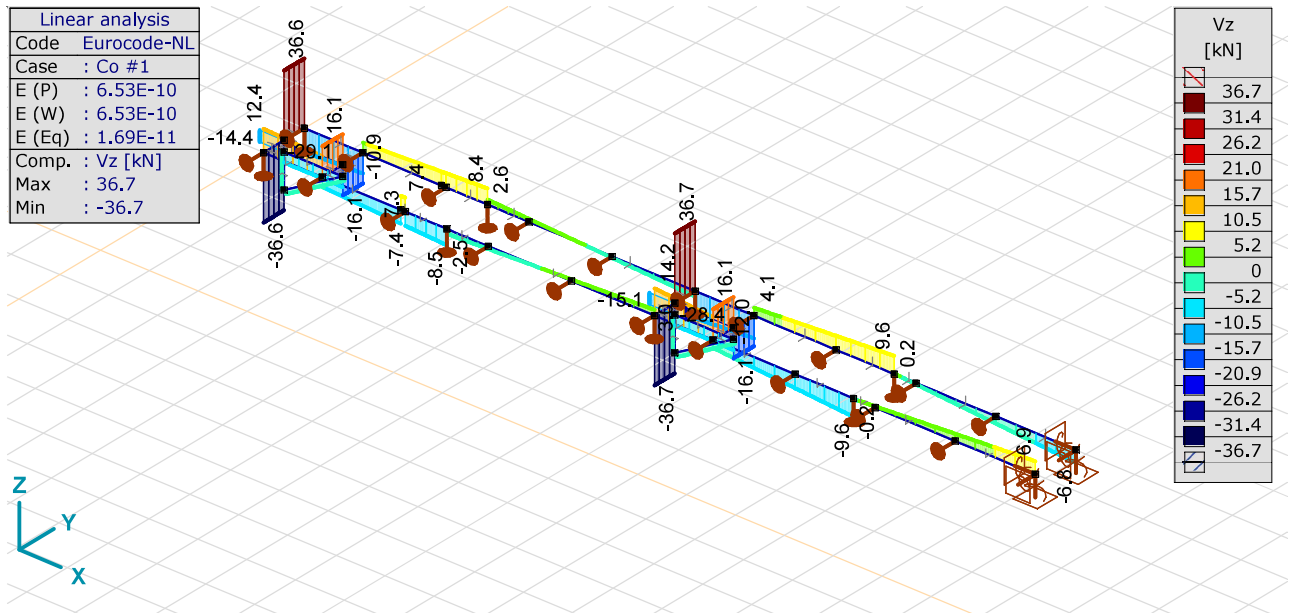
Model: **bottom\_chord\_s+32\_check.axs**

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[I], Linear, Co #1 (ULS), Vy [kN], Filled diagram



[I], Linear, Co #1 (ULS), Vz [kN], Filled diagram

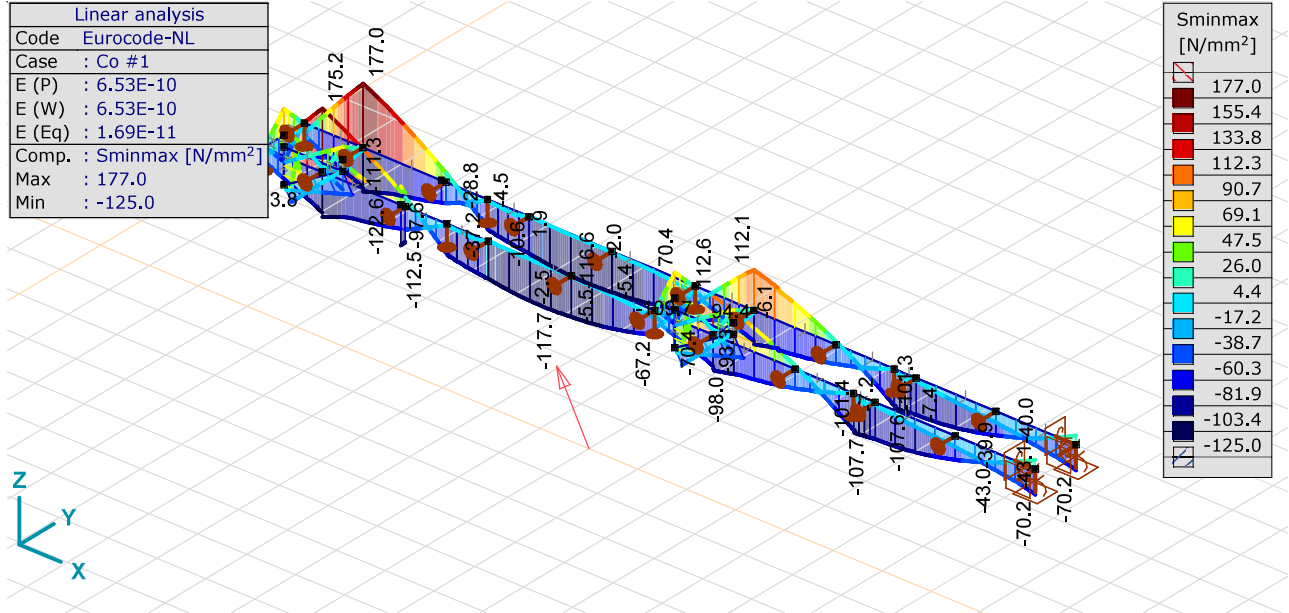
# Project: DLE

Constructeur: DNV GL - Energy

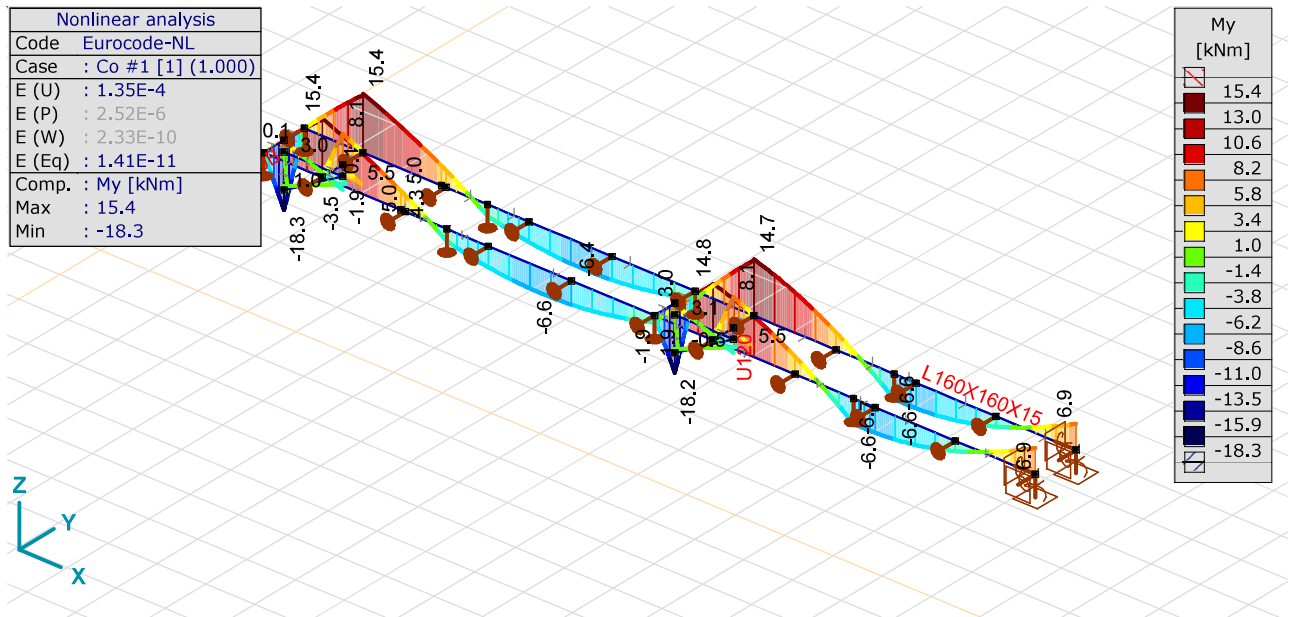
Model: bottom\_chord\_s+32\_check.axs

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[I], Linear, Co #1 (ULS), Sminmax [N/mm<sup>2</sup>], Filled diagram



[II], Nonlin., Co #1 [1] (1.000), Initial deflection, My [kNm], Filled diagram

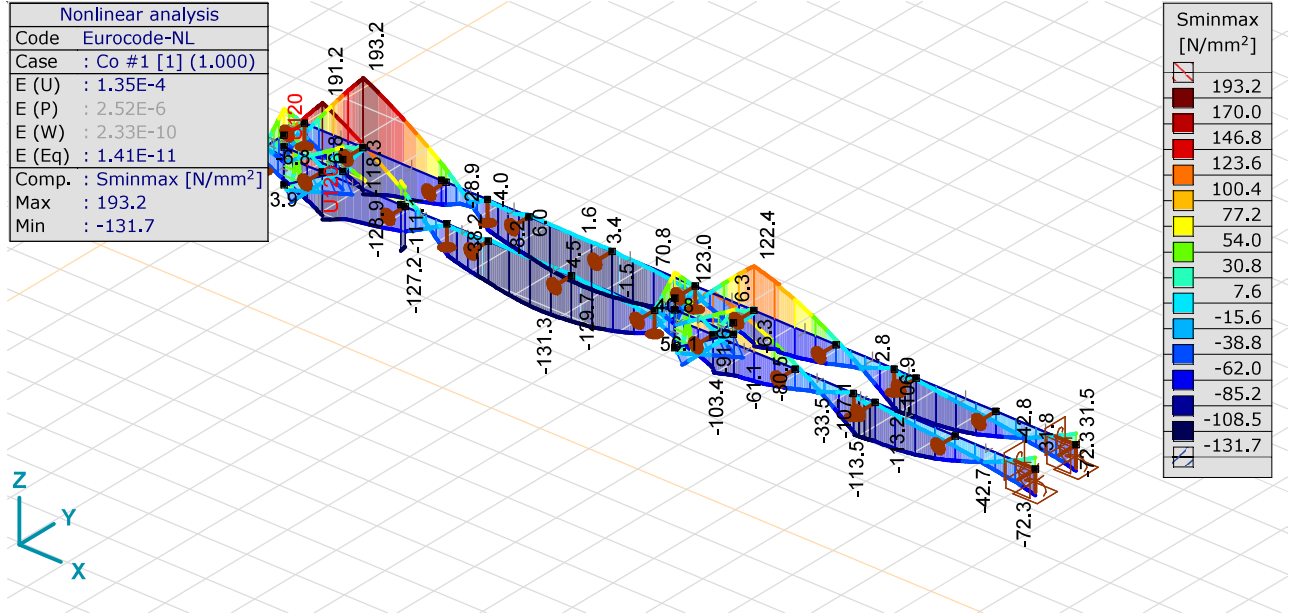
**Project: DLE**

Constructeur: DNV GL - Energy

Model: **bottom\_chord\_s+32\_check.axs**

7/15/2021

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[II], Nonlin., Co #1 [1] (1.000), Initial deflection, Sminmax [N/mm<sup>2</sup>], Filled diagram



## **APPENDIX F**

---

### **Galloping**

Niet van toepassing voor dit masttype.



## **About DNV**

DNV is the independent expert in risk management and assurance, operating in more than 100 countries. Through its broad experience and deep expertise DNV advances safety and sustainable performance, sets industry benchmarks, and inspires and invents solutions.

Whether assessing a new ship design, optimizing the performance of a wind farm, analyzing sensor data from a gas pipeline or certifying a food company's supply chain, DNV enables its customers and their stakeholders to make critical decisions with confidence.

Driven by its purpose, to safeguard life, property, and the environment, DNV helps tackle the challenges and global transformations facing its customers and the world today and is a trusted voice for many of the world's most successful and forward-thinking companies.

## B.13 Fundatierapportage reconstructiemasten

ZUID-WEST 380 KV OOST VERBINDINGEN

# Definitief ontwerp fundaties reconstructiemasten GT-RLL

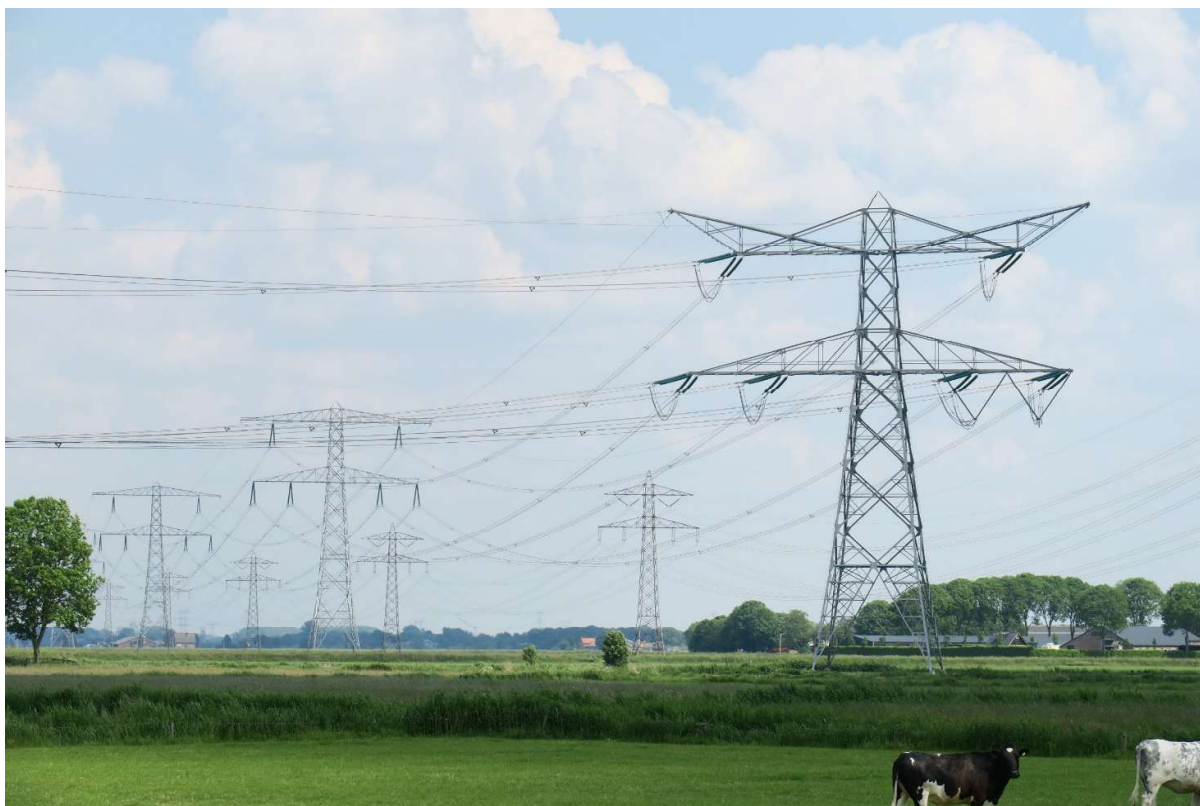
TenneT TSO B.V.

Rapport nr.: 21-1254, Rev. 1

Meridian doc.nr.: 002.678.00 0950646

Datum: 2021-12-21

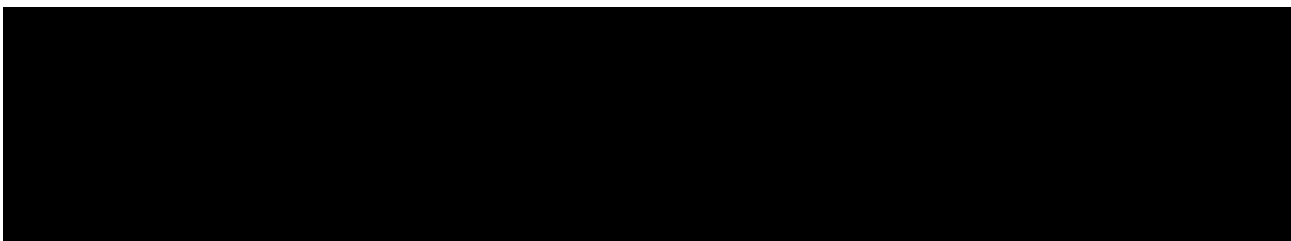
|                 |            |
|-----------------|------------|
|                 |            |
| DATUM:          | 05-01-2022 |
| STATUS TENNET:  | DEFINITIEF |
| REVISIE TENNET: | 1.0        |







Projectnaam: Zuid-West 380 kV Oost Verbindingen Energy Systems  
Rapport titel: Definitief ontwerp fundaties reconstructiemasten GT-RLL DNV Netherlands B.V.  
Klant: TenneT TSO B.V., Utrechtseweg 310-B50 6812 AR Arnhem  
Utrechtseweg 310-B50, 6812 AR Arnhem  
Contactpersoon klant: XXXXXXXXXX  
Datum uitgave: 2021-12-21  
Project nr.: 10124719 Tel: 026 356 9111  
Organisatie unit: Overhead Lines (OHL) Handelsregister Arnhem 09006404  
Meridian doc.nr.: 002.678.00 0950646  
Rapport nr.: 21-1254, Rev. 1



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| Rev. | Datum      | Reden van uitgave       | Auteur   | Beoordelaar  | Goedkeuder   |
|------|------------|-------------------------|--|--|--|
| 0    | 2021-11-12 | Eerste uitgave          | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> |
| 1    | 2021-12-21 | RFA-commentaar verwerkt | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> | <span style="background-color: black; color: black;">XXXXXXXXXX</span> |

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## 1 INLEIDING

In het basisontwerp van de 2ct-reconstructiemasten GT-RLL in het project Zuid-West 380 kV-Oost zijn voor het vaststellen van de haalbaarheid constructieve berekeningen uitgevoerd aan de masten en fundaties. In de Definitief Ontwerpfase, moeten berekeningen verder worden uitgewerkt om te kunnen dienen voor de benodigde vergunningsdocumentatie, voor de aanbesteding en als voorbereiding voor de uitvoeringsfase. Het DO omvat het ontwerp van de mastconstructies, de fundaties en de opstijpunten in de verbinding.

Het definitieve tracé van de hoogspanningslijn is nog niet vastgesteld. Daardoor zijn sonderingen op de precieze mastlocaties nog niet in uitvoering. Dit heeft tot gevolg dat voor het ontwerp van de fundaties nog geen sonderingen beschikbaar zijn. Om toch een ontwerp op te kunnen stellen is door TenneT een geotechnisch lengteprofiel opgesteld uitgaande van sonderingen in de nabijheid van het tracé. Dit lengteprofiel vormt het uitgangspunt voor de berekeningen.

De uitvoeringsfase van de fundaties zal in de vorm van een UAV GC contractvorm plaatsvinden. Dat houdt in dat in de uitvoeringsfase de sonderingen door de opdrachtnemer worden uitgevoerd. Vervolgens kan de opdrachtnemer het definitieve fundatieontwerp opstellen. De voorliggende rapportage is bedoeld om richting te geven aan het ontwerp op basis van de nu beschikbare gegevens. Het is een indicatie wat verwacht wordt in de uitvoeringsfase.

In het project worden voor mastfundaties enkelpaalsfunderingen en meerpaalsfunderingen toegepast afhankelijk van de bodemgesteldheid, het masttype en de belasting.

Deze rapportage bevat de beschrijving van het constructieve ontwerp van de fundaties voor 2ct-reconstructiemasten en de toetsing aan de eisen uit de geotechnische normen en TenneT-specificaties. Het aardingsontwerp wordt in een aparte rapportage behandeld.

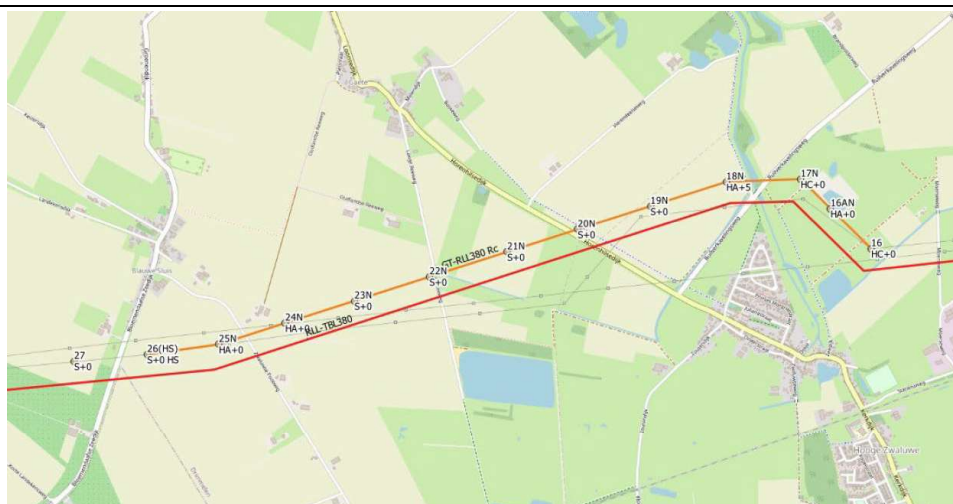
In hoofdstuk 2 zijn de uitgangspunten en randvoorwaarden vanuit de van toepassing zijnde normen en TenneT-specificaties opgenomen. Hoofdstuk 3 beschrijft het ontwerp van de fundatie. De gevolgde aanpak van de berekening is hoofdstuk 4 opgenomen. Hoofdstuk 5 bevat de resultaten van de uitgevoerde toetsing.

## 1.1 Tracé

De reconstructie betreft vier deeltracés. Twee komen voor in de verbinding GT-RLL en twee in de bestaande verbinding GT-EHV. Deze verbinding zal worden onderbroken door de nieuwbouw van het station TLB380 en zal komen te bestaan uit de verbinding GT-TLB en de verbinding TLB-EHV. In deze rapportage zijn de twee deeltracés in de verbinding GT-RLL opgenomen.



*Reconstructie Standdaarbuiten. De reconstructie van GT-RLL wordt westelijk van het huidige tracé geplaatst. De verbinding loopt evenwijdig met de nieuwe verbinding RLL-TLB (in rood). De reconstructie wordt begrensd door twee bestaande hoekmasten.*



*Reconstructie Hooge Zwaluwe, hier wordt het tracé van GT-RLL in een geleidelijkere bocht en gebundeld met de nieuwe verbinding RLL-TLB om de plaats heen geleid. Van de overgangsmasten is mast 26 een steunmast, Mast 16 is een hoekmast.*

## 2 UITGANGSPUNTEN EN RANDVOORWAARDEN

### 2.1 Normen

Er is gebruik gemaakt van de normen volgens Tabel 1.

**Tabel 1 Gebruikgemaakte normen, voorschriften en richtlijnen**

| Norm                                    | Titel  |
|---|--|
| NEN-EN 50341-1:2013                     | "Overhead electrical lines exceeding AC 1 kV - Part 1: General requirements – Common"                        |
| NEN-EN 50341-2-15:2019                  | "Overhead electrical lines exceeding AC 1 kV Part 2 National Normative Aspects (NNA) for THE NETHERLANDS"    |
| NEN-EN 1990+A1+A1/C2:2011               | "Grondslagen van het ontwerp"  |
| NEN-EN 1991-1-4+A1+C2:2011              | "Deel 1-4: Windbelasting op constructies"  |
| NEN-EN 1992-1-1+C2:2011/NB:2016+A1:2020 | "Eurocode 2: Ontwerp en berekening van betonconstructies, deel 1-1: algemene regels en regels voor gebouwen" |
| NEN-EN 1993-1-1+C2+A1:2016 nl           | "Eurocode 3: Ontwerp en berekening van staalconstructies, deel 1-1: algemene regels en regels voor gebouwen" |
| NEN-EN 1993-1-8+C2:2011/NB:2011 nl      | "Ontwerp en berekening van staalconstructies, deel 1-8: ontwerp en berekening van verbindingen"              |
| NEN-EN 1997-1+C1+A1:2016/NB:2016 nl     | "Geotechnisch – Algemeen"  |
| CUR 2001-4                              | "Ontwerpregels voor trekpalen"   |

### 2.2 TenneT-specificaties

In Tabel 2 zijn de documenten opgenomen die relevant zijn voor de berekeningen en toetsingen die binnen dit project in de mastrapportage uitgevoerd zullen worden.

**Tabel 2 Relevante documenten t.b.v. mechanische rapportages**

| Nummer          | Onderwerp       |
|-----------------|-----------------|
| PVE.05.000 v3.2 | PvE Lijnen      |
| sPVE.05.001     | sPvE Lijnen     |
| SPE 04.009      | paalfunderingen |

### 2.3 Ontwerp en eisenverificatie

In Tabel 3 is de lijst opgenomen met documenten die gerelateerd zijn aan deze ontwerprapportage van de fundaties van steunmasten. De belastingen in deze rapportage zijn ontleend aan de berekeningen van de mastconstructie zoals beschreven in de volgende rapportages. Daarbij zijn de reacties op de fundatie zoals berekend met PLS-TOWER gebruikt.

**Tabel 3 Gerelateerde documenten**

| Titel   | DNV-nummer | Meridiannummer     |
|---|------------|--------------------|
| Uitgangspunten reconstructiemasten                              | 21-0702    | 002.678.00 0927721 |
| Verificatierapport reconstructiemasten                          | 21-1444    | 002.678.00 0935197 |
| Mastrapportage bestaande reconstructiemasten HB+0, HS+0 en HC+0 | 21-0888    | 002.678.00 0934573 |
| Mastrapportage S+0/n  | 21-0889    | 002.678.00 0934574 |
| Mastrapportage S+32/n   | 21-0890    | 002.678.00 0934575 |
| Mastrapportage HA+0/n en HA+5/n                                 | 21-0886    | 002.678.00 0934571 |
| Mastrapportage HB+5/n   | 21-0887    | 002.678.00 0934572 |
| Mastrapportage HC+0/n   | 21-1059    | 002.678.00 0942342 |

## 2.4 Materialen

### 2.4.1 Nieuwe constructie

Voor het ontwerp van de mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 4.

**Tabel 4 Materialen nieuwe constructie**

|                | Aanduiding                              |
|----------------|---|
| Staalsoort     | S355J0 (t≤16 mm)<br>S355J2 (16<t≤40 mm) |
| Boutkwaliteit  | 8.8 gerolde draad                       |
| Betonkwaliteit | C30/37                                  |
| Wapeningsstaal | B500                                    |

### 2.4.2 Bestaande constructie

Voor controle van de bestaande mastconstructies en fundaties wordt uitgegaan van de eigenschappen volgens Tabel 5.

**Tabel 5 Materialen bestaande constructie**

|                | Oorspronkelijke aanduiding | Huidige aanduiding |
|----------------|----------------------------|--------------------|
| Staalsoort     | St.37<br>St.52             | S235JR<br>S355JR   |
| Boutkwaliteit  | 5.6                        | 5.6 gerolde draad  |
| Betonkwaliteit | K225                       | C20/25             |
| Wapeningsstaal | FeB400                     | B400               |

## 2.5 Software

De gebruikte software wordt benoemd in Tabel 6.

**Tabel 6 Toegepaste software**

| Software              |                            | Versie |
|-----------------------|----------------------------|--------|
| Mastontwerp           | PLS-CADD                   | 16.65  |
| Mastberekeningen      | PLS-TOWER                  | 16.65  |
| Paalberekening        | Technosoft Paalfunderingen | V6     |
| Constructieve analyse | AxisVM                     | X5 R4h |

## 2.6 Sonderingen

### 2.6.1 Nieuwe mastfundaties

Bij het opstellen van deze rapportage zijn nog geen sonderingen beschikbaar aangezien de mastlocaties nog niet definitief zijn vastgesteld. Om te komen tot een ontwerp is door TenneT een geotechnisch lengteprofiel samengesteld. In dit profiel zijn over de lengte van het tracé de hoogtegegevens van het maaiveld weergegeven vanuit de Algemene Hoogtekaart Nederland 3. De vanuit openbare bron (Dino-loket) beschikbare sonderingen in de nabijheid van het tracé zijn weergegeven. Dit betreft elektrische sonderingen in digitaal formaat. Van de mechanische sonderingen die beschikbaar zijn uit de asset-gegevens vanuit de hoogspanningslijnen in de nabijheid van het nieuwe tracé is geen gebruik gemaakt.

De sonderingen bevinden zich doorgaans in de directe nabijheid van het tracé (< 500 m afstand). Voor het verkrijgen van een indicatie is dit voldoende nauwkeurig. Lokaal kunnen echter grote verschillen optreden.

### 2.6.2 Bestaande mastfundaties

Voor de bestaande masten zijn de beschikbare sonderingen uit de bouwperiode gebruikt, deze zijn principe op de betreffende mastlocatie genomen.

## 2.7 Beschrijving grondopbouw

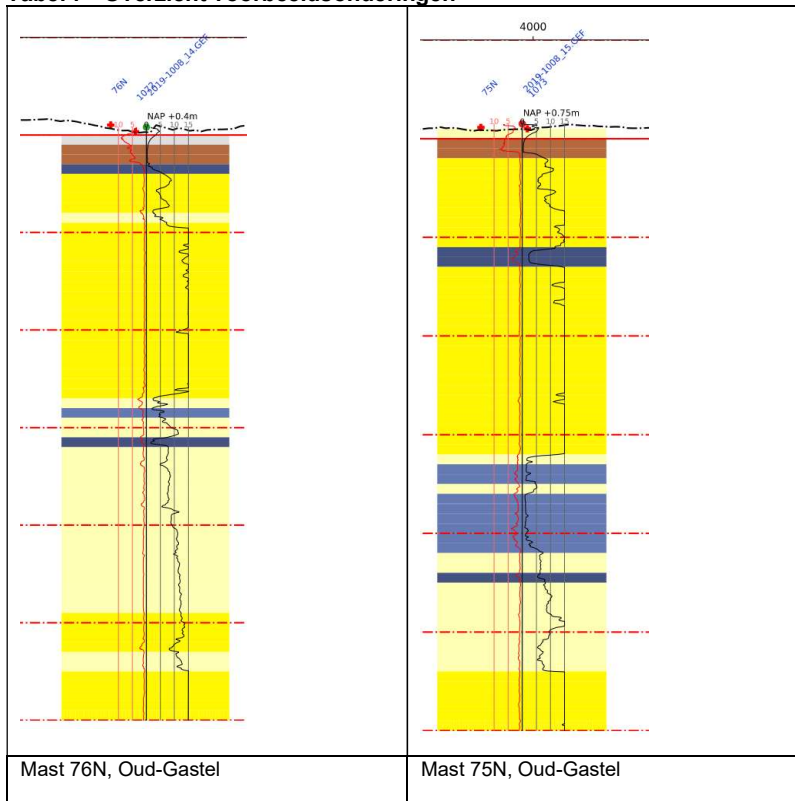
In onderstaande voorbeelden (zie Tabel 7) is de bodemopbouw opgenomen. Voor het beschrijven van de grondopbouw maken we gebruik van de sonderingen die beschikbaar zijn gesteld.

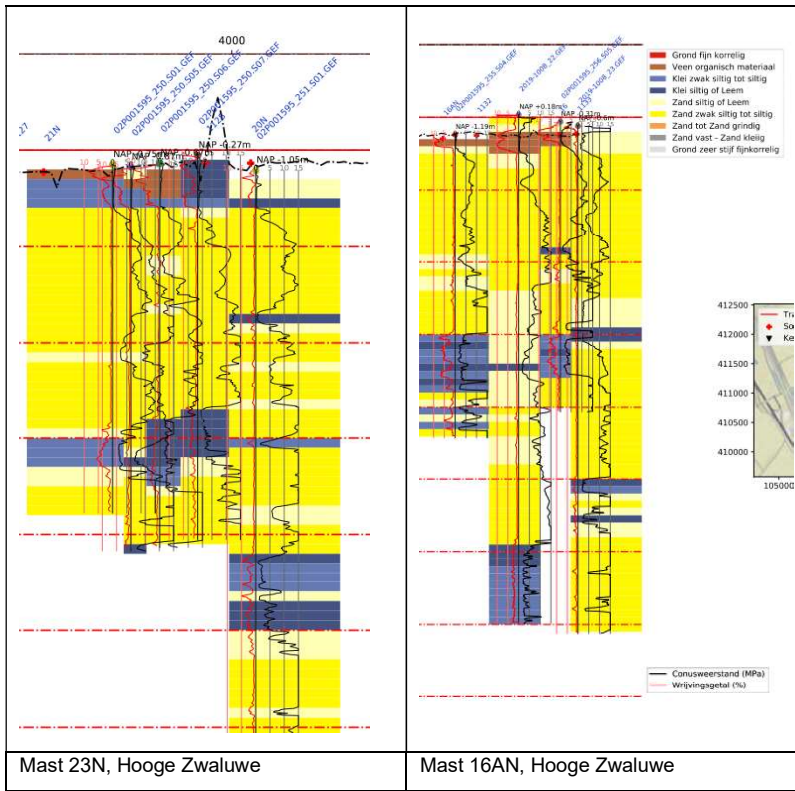
De sonderingen laten over de lengte verschillen zien in ondergrond. Westelijk van Geertruidenberg en dat betekent over circa twee derde van de lengte van het tracé is er een wisselend beeld van zandlagen en cohesieve lagen.

Noemenswaardig is hierbij dat de slappere lagen ook op vrij grote diepte voorkomen en een dikte van meerdere meters. De pakking van de zandlagen is over het algemeen tussen los en matig. Maar er zijn ook locaties met dicht gepakte lagen. Ondiep gelegen slappere lagen komen vooral voor tussen Standdaarbuiten en Moerdijk. Voor afdracht horizontale belastingen is dat ongunstig.

Globaal bevindt zich oostelijk van Geertruidenberg over de gehele diepte van de sondering een draagkrachtig zandpakket. Aandachtspunt zijn hier wel dieper gelegen kleilagen, die voor de weerstand van de paalpunt op druk nadelige invloed hebben.

**Tabel 7** Overzicht voorbeeldsonderingen





## 2.8 Uitgangspunten geotechniek

### 2.8.1 Paalklassefactoren paaltypes

In tabel 8 zijn de paalklassefactoren van de paaltypes uit deze rapportage op basis van NEN-EN 1997-1 samengevat waarmee de berekeningen worden uitgevoerd.

**Tabel 8 Paalklassefactoren**

|   | SI Ø508/670     | SI Ø610/850     | SI Ø762/950     | MV Ø914/1074 | RP-53-124-GI  | RP-53-124       |
|---|-----------------|-----------------|-----------------|--------------|---------------|-----------------|
| Paaltipe                                | Schroefinjectie | Schroefinjectie | Schroefinjectie | MV-paal      | Groutinjectie | Stalen buispaal |
| Diameter stalen buis (m)                | 0,508           | 0,61            | 0,762           | 0,914        | 0,579         | 0,579           |
| Diameter in berekening (m) <sup>1</sup> | 0,59            | 0,73            | 0,86            | 0,994        | 0,796         | 0,579           |
| Factor $\alpha_s$                       | 0,009           | 0,009           | 0,009           | 0,014        | 0,014         | 0,010           |
| Factor $\alpha_t$                       | 0,009           | 0,009           | 0,009           | 0,012        | 0,012         | 0,007           |
| Factor $\alpha_p$                       | 0,63            | 0,63            | 0,63            | 0,70         | 1,0           | 1,0             |
| Factor $\beta$                          | 1,0             | 1,0             | 1,0             | 1,0          | 1,0           | 1,0             |

### 2.8.2 Kleef cohesieve lagen

In de berekeningen wordt de weerstand van de cohesieve lagen boven de draagkrachtige zandlaag meegenomen.

Volgens opmerking (b) van 7.6.3.3 (8) van NEN-EN 1997-1 is de schachtwrijving tot 50% gereduceerd. Negatieve kleef is gerekend over de hoogte van de cohesieve laag en de grondlagen daarboven.

<sup>1</sup> Uitgangspunt voor de palen met groutomhulling is in de berekening de halve dikte van de groutschil



### 2.8.3 Correlatiefactoren

De correlatiefactoren ksi3 en ksi4 worden toegepast bij de bepaling van de karakteristieke weerstand van een paal. De waarden zijn afhankelijk van de aard van de constructie en het aantal beschikbare sonderingen. De correlatiefactoren zijn ontleend aan NEN-EN 1997-1:2016, bijlage A, tabel 10.

Fundaties met één paal per hoekpunt vallen onder “niet-stijf” met factoren volgens Tabel 9. Het aantal sonderingen dat wordt gebruikt hangt af van het dekkingsbereik van de sonderingen voor een van de vier hoekpunten. Voor het DO, waarin nog geen volledig grondonderzoek beschikbaar is, wordt uitgegaan van een dekkingsbereik per hoekpunt van één sondering: Zowel 1,39 voor ksi 3 als ksi4.

**Tabel 9 Correlatiefactoren niet-stijf bouwwerk**

| Aantal sonderingen | 1    | 2    | 3    | 4    |
|--------------------|------|------|------|------|
| ksi3               | 1,39 | 1,32 | 1,30 | 1,28 |
| ksi4               | 1,39 | 1,32 | 1,30 | 1,03 |

### 2.8.4 Materiaalfactor $\gamma_{m,var,qc}$

De parameter die de berekende draagkracht reduceert is de partiele factor  $\gamma_{m,var,qc}$ , volgens NEN-EN 1997-1 artikel 7.6.3.3 (8) opmerking (d). Voor een paal die een wisselende belasting ondergaat tussen trek- en druk treedt een vermindering op van de schuifweerstand. Afhankelijk van de verhouding tussen uiterste trek- en drukkracht in de SLS is de  $\gamma_{m,var,qc}$  tussen de 1,0 en 1,5.

$$\gamma_{m,var,qc} = 1 + 0,25 \cdot \frac{F_{t,max,rep} - F_{t,min,rep}}{F_{t,max,rep}} \text{ en } \gamma_{m,var,qc} \leq 1,5$$

Voor steunmasten met variatie waarbij de maximale drukbelasting minimaal gelijk is aan de trekbelasting levert de formule de waarde van 1,50 op. Deze waarde zal worden gebruikt voor steunmasten. Bij hoekmasten is een factor 1,25 als uitgangspunt genomen. Hierbij is in het geval van afwezigheid van geleiders in een veld sprake van een permanente trekbelasting.

### 2.8.5 Staaldikte funderingspalen

Voor het dimensioneren van stalen palen dient volgens TenneT-specificatie 04.009 rekening te worden gehouden met afname van staaldikte op basis van NEN 1993-5. Dit komt overeen met de CUR-aanbeveling 166 voor damwanden. Op dit moment is nog geen milieukundig onderzoek beschikbaar waaruit de agressiviteit of zuurtegraad van het grondwater (pH-waarde) kan worden afgeleid. De invloed van het zoutgehalte in het grondwater is gering<sup>2</sup>. Er moet uitgegaan worden van 100 jaar ontwerplevensduur.

Tabel 9.2. Aantasting (mm) van damwanden in bodem en ophogingen met of zonder grondwater (per blootgestelde zijde)\*.

| Beoogde levensduur (jaar)  | 5 *** | 25 *** | 50   | 75   | 100  |
|--|-------|--------|------|------|------|
| Ongeroerde, schone bodem   | 0,00  | 0,30   | 0,60 | 0,90 | 1,20 |
| Verontreinigde bodem, geroerde grond                             | 0,15  | 0,75   | 1,50 | 2,25 | 3,00 |
| Zure bodem (veen, moeras)  | 0,20  | 1,00   | 1,75 | 2,50 | 3,25 |
| Onverdichte grond (klei, zand) **                                | 0,18  | 0,70   | 1,20 | 1,70 | 2,20 |
| Onverdicht, agressief ophogmateriaal (bodemas, slakken, sintels) | 0,50  | 2,00   | 3,25 | 4,50 | 5,75 |

**Figuur 1 Tabel 9.2 uit CUR 166**

Voor het DO wordt uitgegaan van zure grond en minimaal 12,5 mm dikte. Met de gereduceerde dikte van 12,5-3,25=9,25 mm is gerekend.

Voor bestaande palen kan uitgegaan worden van  $((45 \text{ jaar} + 50 \text{ jaar}) / 100 \text{ jaar} \cdot 3,25 \text{ mm}) = 3,1 \text{ mm}$ .

<sup>2</sup> Deltares, rapport 1209030, Corrosie van stalen damwandplanken in de grond;

## 2.8.6 Horizontale bedding

De beddingwaardes worden gebaseerd op ontwerprichtlijn CUR228. Waarden in Tabel 10 zijn hieruit afgeleid en gelden als gemiddelde waarden. De breedte van de grond die wordt gemobiliseerd door een paal ten opzichte van de breedte van de paal wordt uitgedrukt in de schelpfactor. Empirische waarden voor de schelpfactor worden gebruikt volgens Tabel 10.

**Tabel 10 Aan te houden waarden voor grondbeddingen en schelpfactoren**

| Grond | $k_n$                | schelpfactor | passieve druk |
|-------|----------------------|--------------|---------------|
|       | [kN/m <sup>3</sup> ] | [-]          | [-]           |
| Klei  | 3000                 | 1,3          | 2             |
| Veen  | 1500                 | 1,2          | 2             |
| Zand  | 15000                | 2,0          | 3             |

Volgens NEN-EN 50341-2-15:2019 art. 8.2. NL.4 moet het effect van variatie van bedding op de krachtsverdeling worden beschouwd. De berekeningen worden uitgevoerd voor een beddingwaarde die  $\sqrt{2}$  lager is en  $\sqrt{2}$  hoger is dan de tabelwaarde.

De reactie van de paalbedding is gelimiteerd tot de grenswaarde van de maximale passieve gronddruk die zich kan ontwikkelen afhankelijk van de diepte.

In Appendix E wordt verder ingegaan op de gehanteerde waarden in de berekening.

## 2.8.7 Verticale bedding

Bij de berekening van de eenpaalsfundering heeft de verticale bedding van de paalpunt geen invloed op de krachtsverdeling. In de berekening is een starre steun gehanteerd.

## 2.9 Vermoeiing

De fundaties worden belast door vakwerkmasten. Deze zijn vanwege de aard van de constructie niet gevoelig voor vortex shedding of andere opslingeringen door wind. De wisselende belasting van wind is een quasi-statische belasting. Dit is op basis van art. 7.3.10 van NEN-EN 50341-1:2013. Toetsing op vermoeiing door galloping, voor zover al relevant voor fundaties, is voor bestaande constructies niet vereist op basis NEN 8701.

## 2.10 Omgeving

De voorgestelde versterkingsoplossing met betonpoeren vereist ruimte buiten de huidige mastvoeten. Een gedetailleerde studie naar eventuele obstakels valt buiten de scope van deze rapportage, op basis van huidige verstrekte informatie zijn er voor de betreffende mastlocatie geen obstakels bekend.

## 2.11 Aarding

Uitwerking van aardingsvoorzieningen vallen buiten de scope van deze rapportage. In de UO-fase dient de aarding in de betonpoeren te worden ontworpen op basis van de van toepassing zijnde TenneT-specificaties.

## 2.12 Sterkte-coördinatie

Overeenkomstig de bepaling AM-req-1077 in het PVE-lijnen worden geen eisen gesteld aan sterkte-coördinatie. Vanwege de onvolledig beschikbare geotechnische gegevens wordt in het DO een maximale unity-check van 0,9 aangehouden.

Deze eis geldt niet voor de bestaande mastfundaties.

### 3 FUNDERINGSONTWERP

#### 3.1 Inleiding

Voor de steunmasten in de hoogspanningslijn is de enkelpaalsfundering met schroefinjectiepalen in de basis het uitgangspunt. Bij een tekort in draagvermogen bij de enkelpaalsfundering voor de steunmasten zal voor het DO een tweepaalsfundering worden gekozen. Als alternatief kan ook de geheide MV-paal als enkelpaalsfundering worden toegepast. Aangezien het streven van TenneT is om zoveel mogelijk enkelpaalsfunderingen toe te passen moet de mogelijkheid daarvan in de UO-fase worden onderzocht, waarbij ook het effect van heitellingen op de omgeving moet worden meegenomen. In het geval van bijzondere situaties, bijvoorbeeld als de fundatie zich bevindt in een wateroverloopgebied is een speciale, verhoogde fundatie het uitgangspunt.

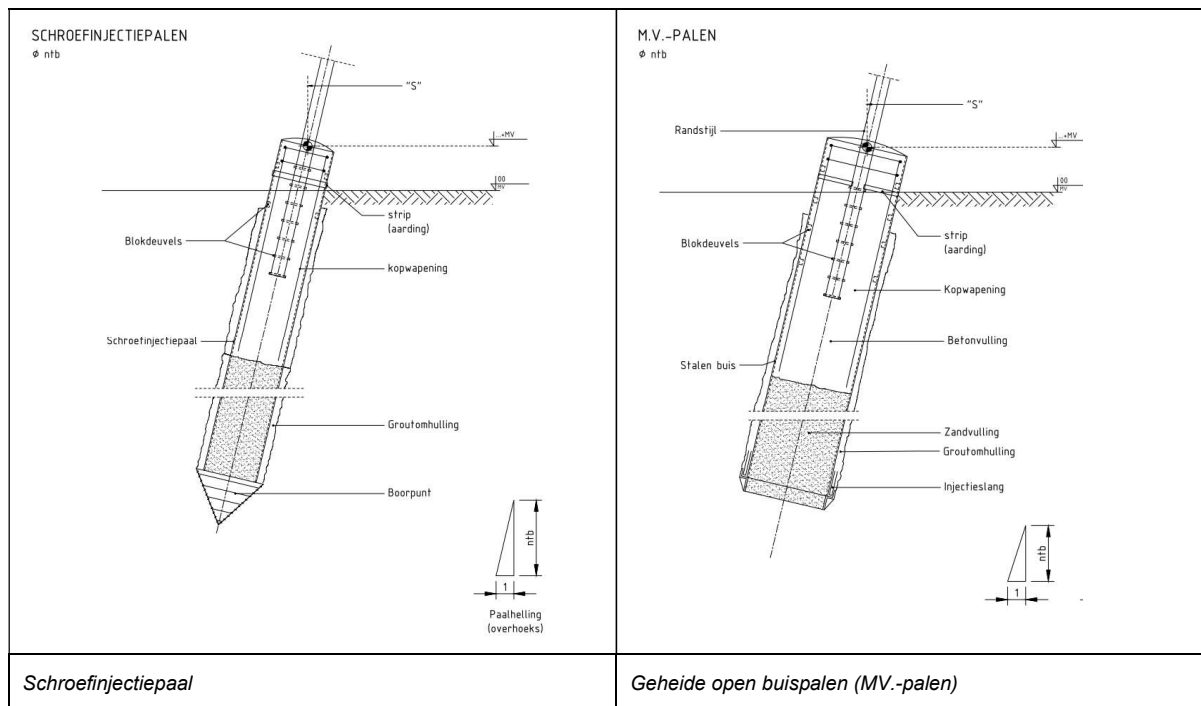
#### 3.2 Paaltypes - nieuw

##### 3.2.1 Schroefinjectiepaal

De schroefinjectiepaal als enkelpaalsfundering kan bij alle steunmasttypes worden toegepast, op voorwaarde dat met de bodemgesteldheid voldoende draagvermogen ontwikkeld kan worden. De paal is grondverdringend en wordt schroevend op diepte gebracht. De ruimte tussen schroefpunt en stalen buis wordt tijdens het inbrengen opgevuld met grout. Voor de maximale paallengte van de schroefinjectiepaal wordt op basis referentieprojecten uitgegaan van 25 meter. De buispaal wordt over de bovenste 2,5 m á 3 m voorzien van een betonvulling. Onder het beton komt een zandvulling. Ingeval van bijzondere gevallen of agressieve gronden dient de betonvulling tot paalpunt door te lopen. Zie Figuur 2.

##### 3.2.2 MV-paal

De MV-paal is een geheide stalen buispaal met open punt. Met dit paalttype is een zeer hoog draagvermogen haalbaar. De detaillering van de paalkop is gelijk aan die van de schroefinjectiepaal. De diameters waarmee in het project wordt gerekend zijn 914 mm en 1016 mm. Beide gaat uit van een groutschil van 80 mm. Zie Figuur 2.



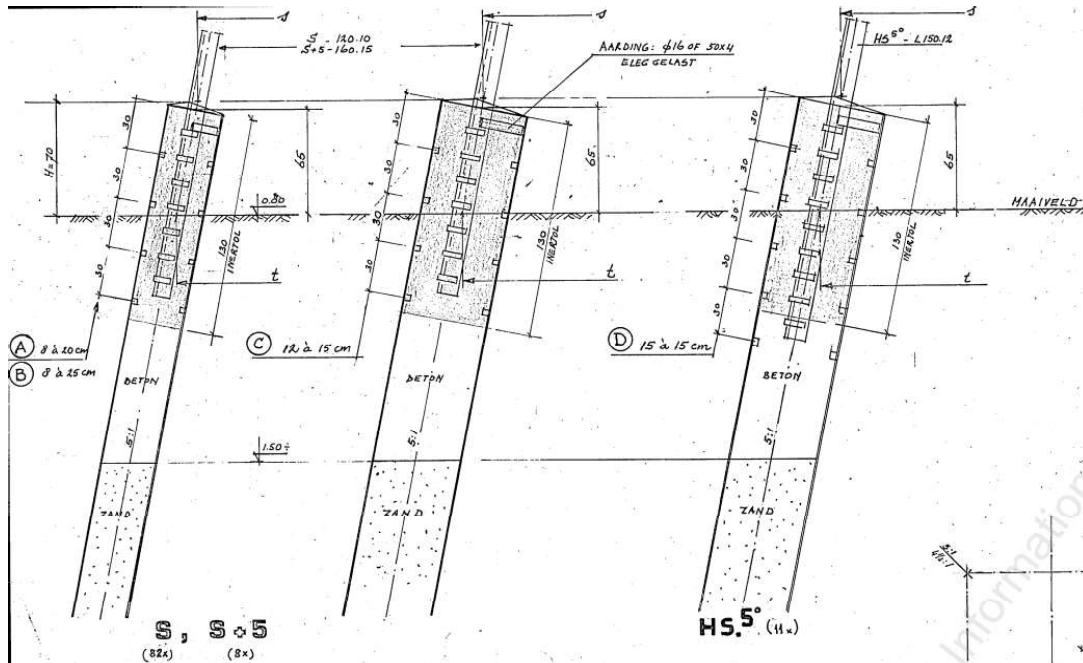
**Figuur 2 Principe schroefinjectiepalen en MV-palen**

### 3.3 Paaltypes – bestand

Vier masten zullen de overgang vormen van huidig tracé naar nieuw tracé. Het betreft mast 16, 26, 68 en 78. Ten opzichte van huidige situatie wijzigt de belasting op de fundatie in geringe mate, echter de fundatie moet voldoen aan het afkeurniveau.

#### 3.3.1 Stalen buispaal

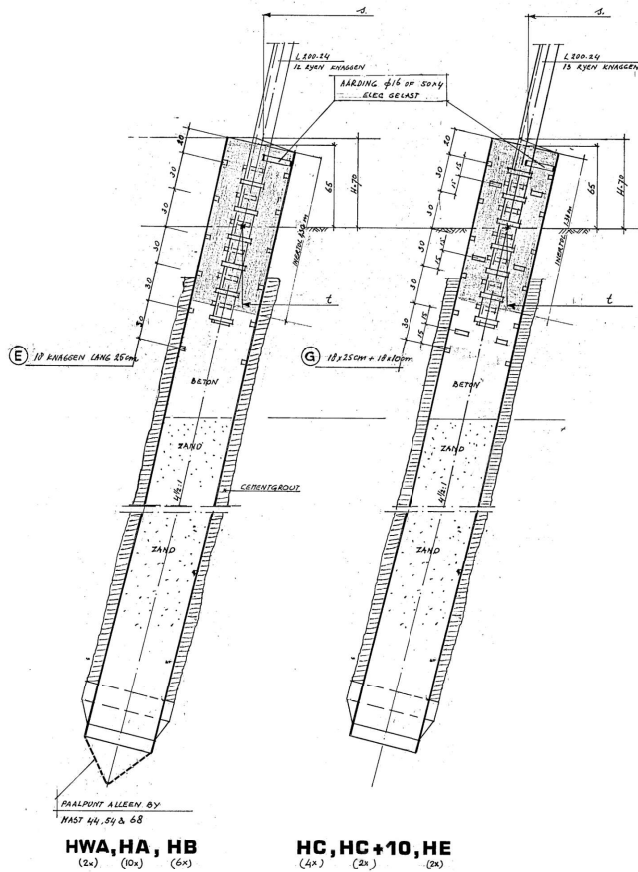
Mast 26 van het type HS (hoek-steenmast) is gefundeerd op stalen buispalen met punt zonder groutomhulling, zie Figuur 3.



Figuur 3 Paalfundering mast 26

### 3.3.2 Grout-injectiepaal

Mast 16, 68 en 78 zijn gefundeerd op grout-injectiepalen. Het zijn uit stalen damwandsegmenten opgebouwde buisprofielen met open of gesloten punt. De groutomhulling zorgt voor een verbeterde kleefkracht met de grond. De palen zijn berekend als MV-palen. Zie Figuur 4.



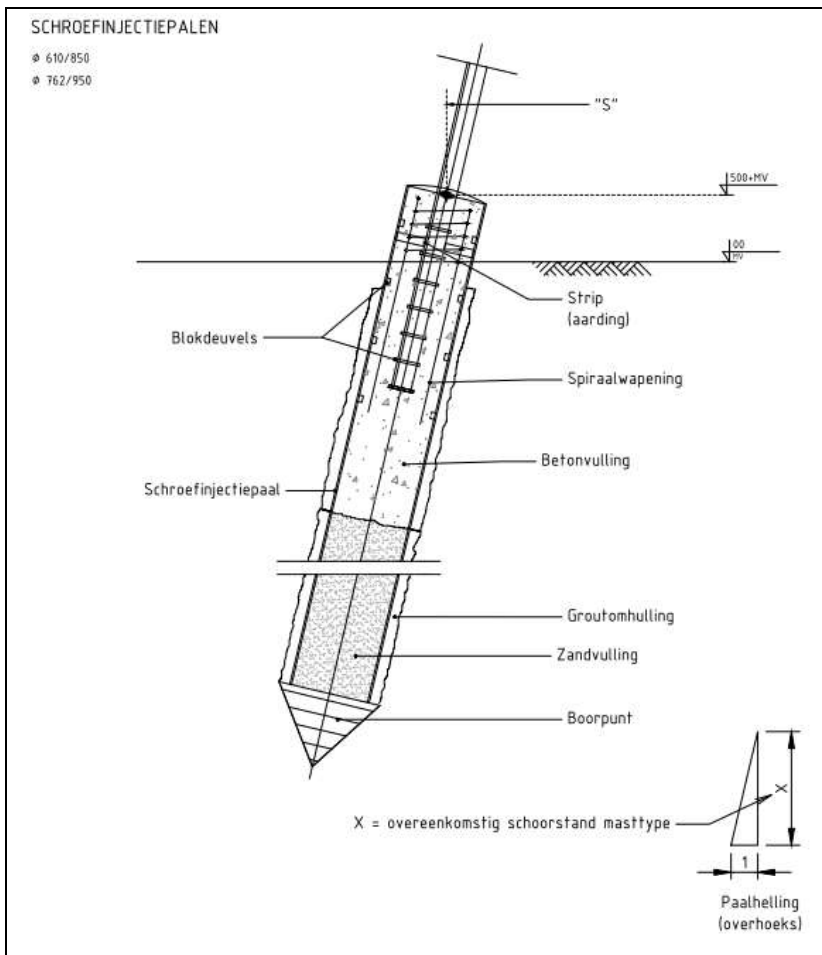
Figuur 4 Paalfundering mast 16, 68 en 78

### 3.4 Enkelpaalsfundering

Eigenschappen van de enkelpaalsfundering voor nieuwe masten:

- de funderingspaal is in schoor en heeft dezelfde helling en richting als de randstijl, de richting is naar buiten vanuit het centrum van de mast gezien, in de overhoekse richting. De schoorstand varieert tussen 5:1 tot 8:1, afhankelijk van het masttype;
- de minimale afmeting is 610 mm voor het kunnen instorten van de randstijl rekening houdend met een paalafwijking van 0,1 m;
- de bovenkant van de paal bevindt zich op 0,5 m+ maaiveld;
- de paal wordt aan bovenzijde voorzien van gelaste blokdeuvels voor de krachtsoverdracht met de ingestorte rand van de mastconstructie;
- de paal wordt over de bovenste circa 2,5 m voorzien van een betonvulling. De betonvulling moet met een afbolling worden gestort. Onder de beton komt een zandvulling. Ingeval van bijzondere gevallen of agressieve gronden dient de betonvulling tot paalpunt door te lopen;
- in de betonvulling wordt een spiraalwapening geplaatst;
- de randstijl wordt voor de aarding galvanisch verbonden met de wand van de paal via aangelaste stripjes;

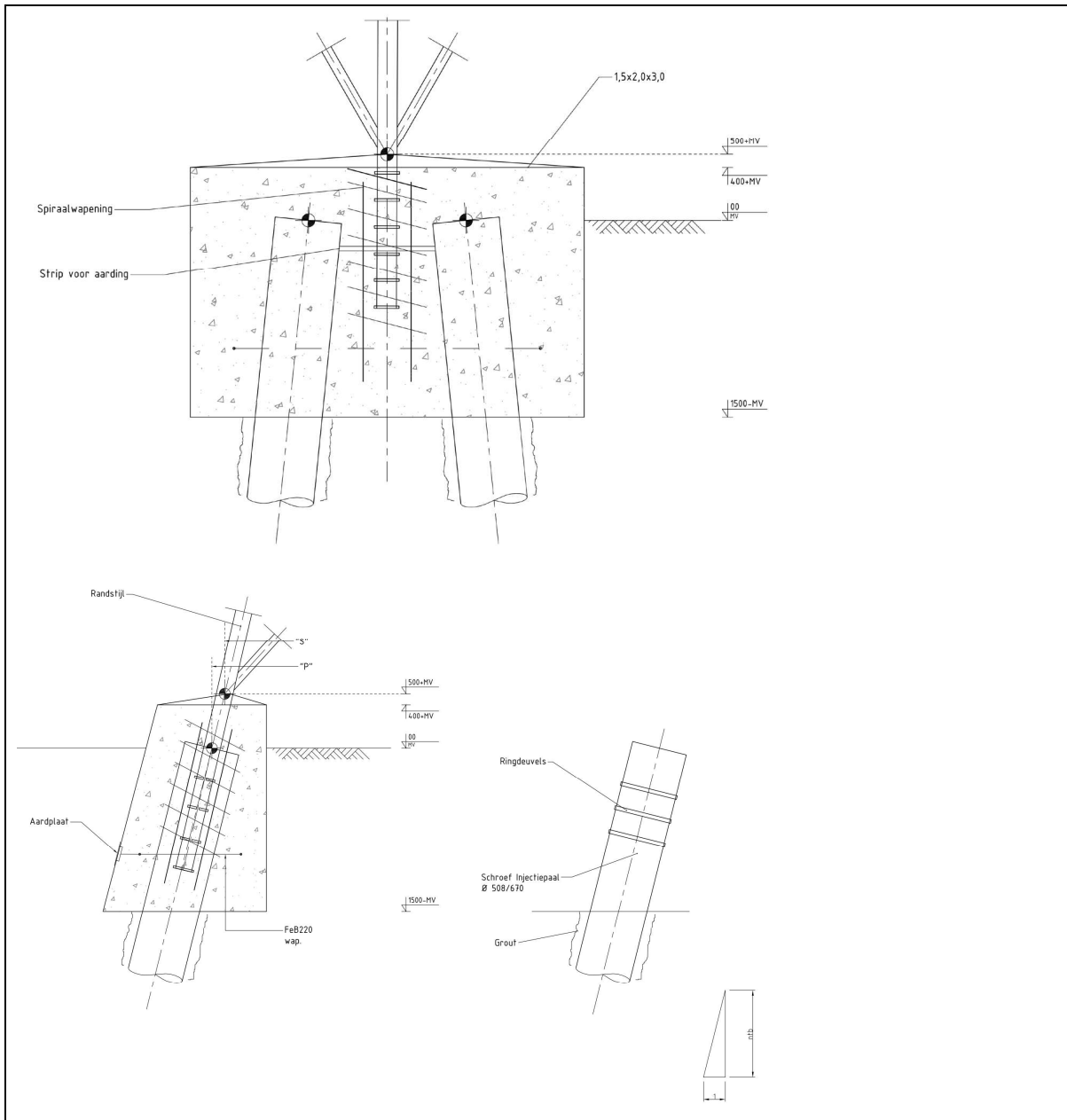
In Figuur 5 is de principetekening opgenomen.



**Figuur 5 Principe van de schroefinjectiepaal met ingestorte randstijl**

### 3.5 Tweepaalsfundering

Bij onvoldoende draagvermogen wordt uitgegaan van de tweepaalsfundering. Hierbij worden twee palen opgenomen in een rechthoekige betonnen poer. Als paaltype is voor dit DO de schroefinjectiepaal het uitgangspunt omdat deze het breedst inzetbaar is. Als alternatief kan in het UO ook een vibro-paal of FGI (Fundex)-paal worden toegepast. In Figuur 6 is het principe opgenomen.



**Figuur 6** Principe van de tweepaalsfundering

## 4 AANPAK

### 4.1 Inleiding

Voor alle mastlocaties in het tracé zal uitgaande van de beschikbare sonderingsgegevens het poertype en paallengte indicatief worden bepaald. De berekening wordt uitgevoerd met TS/paalfunderingen. De toetsing vindt plaats ten aanzien van trek- en drukbelasting.

In deze DO-rapportage zal de enkelpaalsfundering worden getoetst met de grootste horizontale belastingen binnen de groep van masttypes waar dit fundatietype wordt toegepast. Dit betreft de volgende indeling naar paaltype:

- SI Ø610/850 – S+0, HA+0, HA+5 en HB+5;
- SI Ø762/950 – S+32 en HC+0;
- Bestaande palen – mast 16, mast 26, mast 68 en mast 78.

Indien uit berekening blijkt dat een enkelpaalsfundering niet voldoet, dat zal er worden gekozen voor een tweepaalsfundering met twee schroefinjectiepalen Ø508/670.

### 4.2 Belasting

De fundatiebelastingen van de mastconstructies zijn opgenomen in Appendix A. Deze zijn ontleend aan de uitvoer vanuit PLS-TOWER. Voor de toetsing met TS/paalfunderingen wordt gebruik gemaakt van de belasting in de richting van de randstijl (lokale richting) voor trek- en drukbelasting.

De belastingcombinaties die in het DO worden gehanteerd voor de berekening van de horizontale afdracht bestaat uit de volgende belastingen, alle voor de uiterste grenstoestand. De belastingen gelden voor één van de vier hoekpunten.

- maximale drukbelasting, in deze combinatie belast de randstijl de fundatie met een neerwaartse kracht en een horizontale kracht naar buiten;
- maximale trekbelasting, in deze combinatie belast de randstijl de fundatie met een opwaarts gerichte kracht en een horizontale kracht naar binnen;
- maximale torsiebelasting, hierbij wordt de fundatie haaks op de diagonale richting van het grondvlak belast. De positieve en negatieve horizontale richting wordt onderzocht. De verticale belasting kan van ondergeschikte grootte zijn.
- maximale combinatie van trekbelasting en torsie. Bij een meerpaalspoer leidt de horizontale kracht door torsie tot een vergroting van de trekkracht. In combinatie met een eveneens significante trekkracht vanuit de mast kan dit maatgevend zijn voor een van de palen in de fundatie. Zie hiervoor de toelichting in Appendix C.

### 4.3 Draagvermogen

Vanuit het geotechnisch lengteprofiel is een representatieve selectie gemaakt waarmee berekeningen zijn uitgevoerd. Bovendien is zoveel mogelijk gebruik gemaakt van sonderingen met een diepte van meer dan 30 meter, omdat paallengtes tot 25 m oplopen. Per deeltracé zijn een aantal representatieve sonderingen genomen. In tabel zijn de in de berekening gebruikte sonderingen gegeven. De berekeningen zijn bij voor alle paaltypes bij iedere sondering uitgevoerd.



**Tabel 11 Gebruikte sonderingen**

| CPT bestand           | type | RD_x_sond | RD_y_sond | RD_m_sond | sondeerlengte | gemeente    |
|-----------------------|------|-----------|-----------|-----------|---------------|-------------|
| 2019-1008_14.GEF      | GEF  | 93021,7   | 401221,1  | 0,4       | 34,991        | Halderberge |
| 2019-1008_15.GEF      | GEF  | 93130,2   | 401568,5  | 0,75      | 35,164        | Halderberge |
| 02P001595_202.S03.GEF | GEF  | 94044,9   | 403745,4  | 0,03      | 39,982        | Moerdijk    |
| 02P001595_251.S01.GEF | GEF  | 109537,3  | 411798    | -1,05     | 39,831        | Drimmelen   |
| 2019-1008_22.GEF      | GEF  | 110558,5  | 411564,8  | 0,18      | 35,1          | Drimmelen   |

De sonderingen zijn in digitaal formaat (gef-bestand) ingelezen in het programma Technosoft Paalfunderingen. Aan de hand van de sonderingen en de beschikbare boringen is een grondprofiel geconstrueerd. De gebieden waarin negatieve en positieve schachtwrijving optreedt worden ingesteld per sondering.

Aanvullend op de berekening in Technosoft is een controle op het kluitgewicht uitgevoerd volgens art. 7.6.3.3 (g) van NEN-EN 1997-1, waaruit de minimale lengte voor voldoende te mobiliseren grondmassa volgt.

Geotechnische berekeningen zijn opgenomen in Appendix D. In de uitvoer zijn van toepassing zijnde paalpuntniveau's omkaderd.

## 4.4 Horizontale krachtafdracht

### 4.4.1 Krachtsverdeling

Met een staafwerkmodel in het programma AxisVM is de horizontale krachtafdracht berekend. De palen zijn als elastisch ondersteunde liggers zijn ingevoerd. Er wordt geen steun uit de grond tussen maaiveld en 1 m onder maaiveld of tegen de poeren gerekend, alsof de fundaties grenzen aan een waterloop. De horizontale gronddruk is begrensd tot de passieve gronddruk die kan worden ontwikkeld.

De berekening voor de horizontale krachtafdracht is uitgevoerd uitgaande van een globaal beeld van de bodemgelaagdheid van de sonderingen. Hiervoor is het volgende aangehouden:

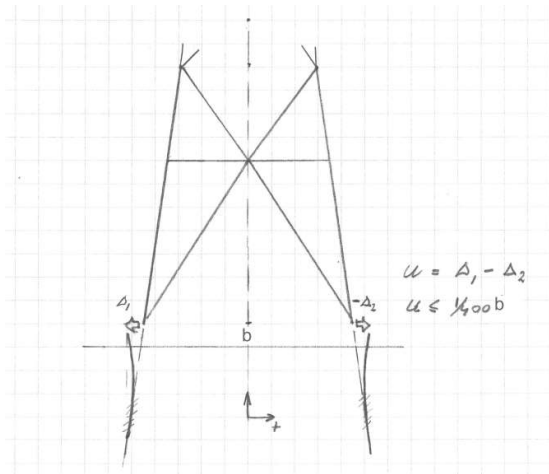
- Maaiveld tot 3 m – maaiveld           Klei
- 3 m – maaiveld en dieper            Zand

Eventuele kleine versturende diepe lagen hebben beperkte invloed op de krachtafdracht en worden buiten beschouwing gelaten.

De berekening van de horizontale afdracht verschaft informatie over de combinatie van axiale krachten en buiging in de paalschacht. De aldus gevonden spanningen worden gebruikt in de toetsing van de doorsnede van de buispaal. De berekening is opgenomen in Appendix E.

#### 4.4.2 Horizontale verplaatsing

De TenneT-specificatie "Paalfunderingen" stelt eisen aan de maximale onderlinge verplaatsing van de fundatie bij de randstijl. Deze mag niet meer bedragen dan  $1/400 b$ . Verplaatsingseisen worden gesteld voor de karakteristieke belastingen, zonder belastingfactoren. In Appendix C is verdere invulling gegeven aan deze eis.



**Figuur 7** Eis aan de horizontale verplaatsing

#### 4.5 Wapening

Het detailleren van de wapening in de paal(kop) valt buiten de scope van dit rapport. De benodigde wapening is in de UO-fase door opdrachtnemer te bepalen.

## 5 RESULTATEN – NIEUWE MASTFUNDATIES

### 5.1 Verticaal draagvermogen

#### 5.1.1 Nieuwe mastfundaties

De resultaten van de berekeningen zijn samengevat in Appendix D. Voor alle van toepassing zijnde locaties is de toetsing uitgedrukt in de Unity-Check. De toetsing voor trek en druk is opgenomen. Alle Unity-checks zijn kleiner dan 0,9, dus voldoen de fundaties aan het gestelde uitgangspunt. De paallengte is groter dan de minimale lengte benodigd voor het kluitgewicht.

In Tabel 12 is per sondering weergegeven in hoeverre de enkelpaalsfundering toepasbaar is. Enkel bij mast 71N (masttype S+32/n) is een tweepaalspoer gekozen als alternatief.

**Tabel 12 Toetsing nieuwe mastfundaties**

| Mast | Masttype | Sondering             | Poertype    | Paaltype    | U.C. trek | U.C. druk |
|------|----------|-----------------------|-------------|-------------|-----------|-----------|
| 16AN | HA+0     | 2019-1008_22.GEF      | 1-paals 610 | SI Ø610/850 | 0,89      | 0,56      |
| 17N  | HC+0     | 2019-1008_22.GEF      | 1-paals 762 | SI Ø762/950 | 0,90      | 0,58      |
| 18N  | HA+5     | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,87      | 0,74      |
| 19N  | S+0      | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,86      | 0,57      |
| 20N  | S+0      | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,86      | 0,57      |
| 21N  | S+0      | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,86      | 0,57      |
| 22N  | S+0      | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,86      | 0,57      |
| 23N  | S+0      | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,86      | 0,57      |
| 24N  | HA+0     | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,88      | 0,68      |
| 25N  | HA+0     | 02P001595_251.S01.GEF | 1-paals 610 | SI Ø610/850 | 0,88      | 0,68      |
| 69N  | HB+5     | 02P001595_202.S03.GEF | 1-paals 610 | SI Ø610/850 | 0,87      | 0,44      |
| 70N  | HA+5     | 02P001595_202.S03.GEF | 1-paals 610 | SI Ø610/850 | 0,87      | 0,43      |
| 71N  | S+32     | 02P001595_202.S03.GEF | 2-paalspoer | SI Ø508/670 | 0,90      | 0,58      |
| 72N  | S+32     | 2019-1008_15.GEF      | 1-paals 762 | SI Ø762/950 | 0,89      | 0,54      |
| 73N  | HA+0     | 2019-1008_15.GEF      | 1-paals 610 | SI Ø610/850 | 0,87      | 0,63      |
| 74N  | S+0      | 2019-1008_15.GEF      | 1-paals 610 | SI Ø610/850 | 0,85      | 0,28      |
| 75N  | S+0      | 2019-1008_15.GEF      | 1-paals 610 | SI Ø610/850 | 0,85      | 0,28      |
| 76N  | HA+0     | 2019-1008_14.GEF      | 1-paals 610 | SI Ø610/850 | 0,89      | 0,60      |

### 5.2 Horizontale krachtsafdracht

#### 5.2.1 Nieuwe mastfundaties

In Appendix E is het resultaat beschreven van de horizontale krachtsafdracht. Uit Tabel 13 en Tabel 14. blijkt dat de toetsing van de spanning in de buispaal en de horizontale verplaatsing voldoen voor de verschillende paaltypen. Voor één van de twee masten van het masttype S+32/n is een tweepaalsfundering het uitgangspunt in het DO vanwege het ontoereikende draagvermogen van de enkele paal. In het UO kan nader bepaald worden of hier toch een enkelpaalsfundering mogelijk is.

**Tabel 13 Toetsing horizontale krachtsafdracht – Ø610/850**

|                             | Berekend | Toelaatbaar           | Unity-check |
|-----------------------------|----------|-----------------------|-------------|
| Spanningscheck buispaal     | 91       | 355 N/mm <sup>2</sup> | 0,26 OK     |
| Verplaatsing Max. trek/druk | 9,5      | 15,2 mm               | 0,63 OK     |
| Verplaatsing Max. torsie    | 9,4      | 22,5 mm               | 0,42 OK     |

**Tabel 14 Toetsing horizontale krachtsafdracht – Ø762/950**

|                             | Berekend | Toelaatbaar           | Unity-check |
|-----------------------------|----------|-----------------------|-------------|
| Spanningscheck buispaal     | 130      | 355 N/mm <sup>2</sup> | 0,37 OK     |
| Verplaatsing Max. trek/druk | 8,7      | 18,6 mm               | 0,47 OK     |
| Verplaatsing Max. torsie    | 24,3     | 27,5 mm               | 0,88 OK     |

### 5.3 Hoeveelheden

In Tabel 15 is als samenvatting het aantal palen, de lengte en maximale lengte opgenomen. Dit is gebaseerd op de resultaten per locatie volgens Appendix B.

**Tabel 15 Hoeveelheden**

| Paaltype                 | Aantal locaties | Aantal palen | Gem. paallengte (m) | Max. paallengte (m) |
|--------------------------|-----------------|--------------|---------------------|---------------------|
| SI Ø610/850              | 15              | 60           | 17,4                | 25                  |
| SI Ø762/950              | 2               | 8            | 23,1                | 23,4                |
| SI Ø508/670 <sup>3</sup> | 1               | 8            | 21,5                | 21,5                |

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<sup>3</sup> onderdeel van tweepaalsfundering

## 6 RESULTATEN – BESTAANDE MASTFUNDATIES

### 6.1 Verticaal draagvermogen

Zie Tabel 16 voor resultaten van de toetsing van de masten. De palen van mast 26 hebben onvoldoende capaciteit op trek, maar voldoende capaciteit op druk. Alle andere masten hebben voldoende capaciteit op trek en druk.

Opgemerkt moet worden dat er bij mast 68 geen restcapaciteit is op het trekdraagvermogen. Geadviseerd wordt om voor, in ieder geval, deze mast in de UO-fase nieuwe sonderingen te maken en het gevonden trekdraagvermogen hieraan te verifiëren.

**Tabel 16 Toetsing bestaande mastfundaties**

| Mast   | Masttype  | Sondering | Paaltype     | U.C. trek | U.C. druk |
|--------|-----------|-----------|--------------|-----------|-----------|
| 16     | HC+0 (16) | M16-oud   | RP-53-124+GI | 0,62      | 0,31      |
| 26(HS) | S+0 HS    | 26-oud    | RP-53-124    | 1,04      | 0,37      |
| 68     | HB+0 (68) | M68-oud   | RP-53-124+GI | 1,00      | 0,42      |
| 78     | HB+0 (78) | 78-oud    | RP-53-124+GI | 0,59      | 0,35      |

### 6.2 Horizontaal draagvermogen

De bestaande palen worden enkel op sterkte getoetst. De maximale optredende spanning is 195 MPa en voldoet aan de vloeispanning van 235 MPa (UC = 0,83). Deze spanning is wel zonder staalafname. De maximale afname die nog door de doorsnede opgenomen kan worden is ca. (12 mm – (0,83 · 12mm =)) 2 mm. Dit is minder dan de omschreven waarde van 3,1 mm in hoofdstuk 2.8.5. Het lijkt echter niet aannemelijk dat de afname werkelijk 3,1 mm zal kunnen worden ter plaatse van het maximale moment, omdat:

- De stalen paal is omhuld door een groutschil en daardoor grotendeels beschermd zal zijn;
- De grondlaag op deze diepte waarschijnlijk niet vervuild of zuur zal zijn, waardoor de afname maximaal 1,2 mm in 100 jaar is.

Om deze reden zal de bestaande paal naar verwachting voldoen. Na uitvoeren van het bodemonderzoek moet bevestigd worden dat er daadwerkelijk geen verontreinigde bodem is aangetroffen.

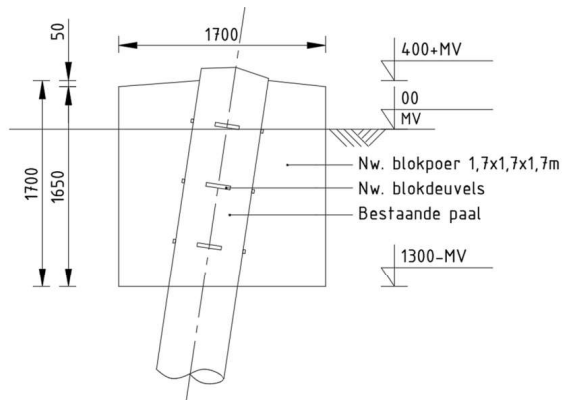
### 6.3 Versterkingsvoorstel

In dit subhoofdstuk wordt een versterkingsvoorstel gegeven, waarmee bereikt kan worden dat de funderingen voldoen aan de eisen.

#### 6.3.1 Ballastverzwaring

De optredende overschrijding van het trekdraagvermogen is met 25 kN beperkt. Het is goed mogelijk om deze relatief kleine overschrijding te compenseren met extra gewicht aan de paal in de vorm van een betonpoer. De beschikbare restcapaciteit op het drukdraagvermogen laat deze ballastverzwaring ook toe. Bij het uitwerken van dit voorstel zal er uitgegaan worden van de belastingen op basis van het afkeurniveau van NEN 8700.

De aanhechting van de nieuwe poer aan de bestaande paal kan bestaan uit een aantal nieuw aan de paal gelaste blokdeuvels. De conservering van het gedeelte van de paal dat wordt opgenomen in de poer moet hiervoor worden verwijderd. Vanuit duurzaamheidsoogpunt wordt er geadviseerd het gedeelte van de paal op de overgang tussen staal en beton te metalliseren.



**Figuur 8 Voorstel ballastverzwaring**

### 6.3.2 Aanpak berekening

Bij het berekenen van het gewicht van de nieuwe poer worden de volgende aannamen gedaan:

- Inhoud van de nieuwe poer wordt verminderd met inhoud van de gedeelte paal dat in de poer wordt gestort (effectief blijft er ca. 85% van het poer gewicht over);
- Conservatief wordt aangehouden dat de nieuwe poer volledig onder water kan staan;
- Streven is om ca. 5% restcapaciteit over te houden van het trekdraagvermogen na aanbrengen van de poer.

## 6.4 Toetsing versterkte fundatie

In deze paragraaf wordt de toetsing van de bestaande palen met nieuw aangebrachte poeren beschreven. De bestaande palen zijn zowel op trek als op druk gecontroleerd, waarbij de belasting is gehanteerd op basis van het afkeurniveau.

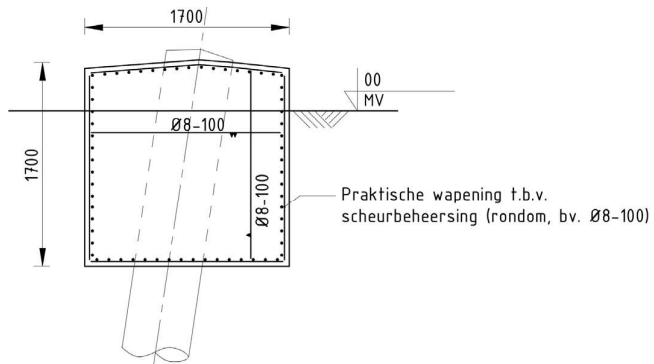
Uit berekening blijkt dat alle paalfunderingen na versterking voldoen. De extra horizontale belasting die ontstaat door het aanbrengen van de poer, valt binnen de marge van horizontale belasting van masttype HC+0 waaraan de bestaande palen getoetst zijn.

**Tabel 17 Toetsing verzwaarde mastfundatie**

| Mast   | Masttype | Sondering | Paaltype  | U.C. trek | U.C. druk |
|--------|----------|-----------|-----------|-----------|-----------|
| 26(HS) | S+0 HS   | 26-oud    | RP-53-124 | 0,95      | 0,43      |

### 6.4.1 Wapening

De poeren hebben geen dragende functie behalve voor hun eigen gewicht. Geadviseerd wordt om de poeren rondom te voorzien van een praktische wapening voor scheurbeheersing, bijvoorbeeld Ø8-100 rondom.



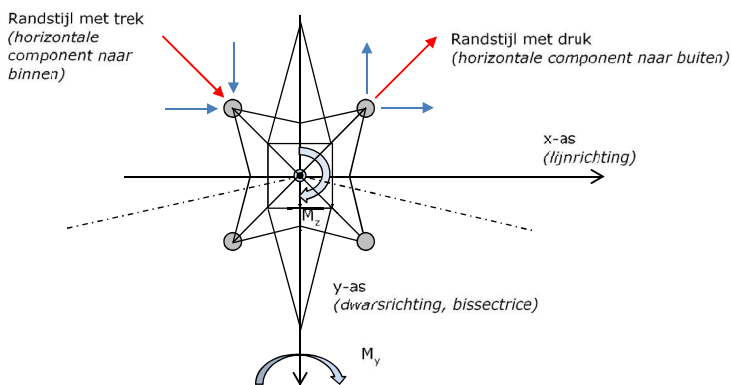
**Figuur 9** Principe wapening

## APPENDIX A

### Fundatiebelastingen

De reacties van de mastconstructie op de fundering worden in deze appendix gepresenteerd. Het gaat om de maatgevende waarden per masttype van de druk-, trek- en horizontale reacties. Vanwege de oriëntatie van de funderingspaal, zijn de waarden beschreven in de X-, Y-, en Z-coördinaat van het globale assenstelsel en in het lokale assenstelsel van de randstijl ("leg direction"). De gegeven waarden zijn een samenvatting over alle berekende belastingcombinaties en zijn gebaseerd op de grootste waarden van elk van de vier fundatiepunten van de mast. De reacties zijn ontleend aan de berekening van PLS-TOWER.

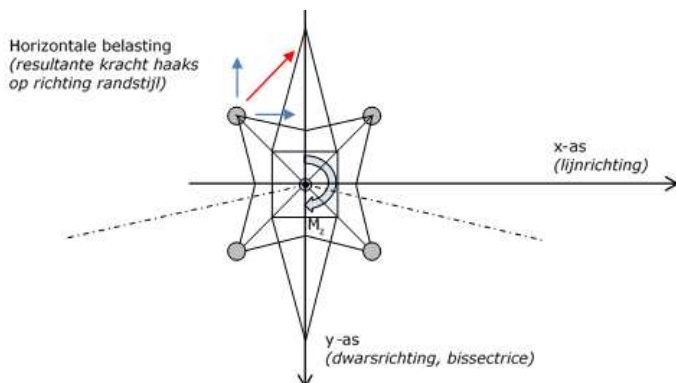
De twee belangrijkste waarden van de funderingsreacties worden gevormd door de trek- en de drukkracht vanuit de randstijl. In geval van een drukkracht zal gezien in het *globale* assenstelsel bij een hellende randstijl een naar buiten gerichte horizontale kracht werken, zie Figuur 10. In geval van een trekkracht in de randstijl is de horizontale component naar binnen gericht.



**Figuur 10** Belasting bij maximale trek- of drukbelasting vanuit de mast

In het geval van torsiebelasting op de mast, bij steunmasten is dat onder de combinatie 5a (geleiderbreuk), bij hoekmasten door de afwezigheid van geleiders aan één zijde van de mast (special limit state), werkt er een significante horizontale kracht op de fundering *haaks* op de richting van de randstijl. Voor de berekening van de horizontale krachtsafdracht van de fundering moet met de belasting door torsie rekening worden gehouden.

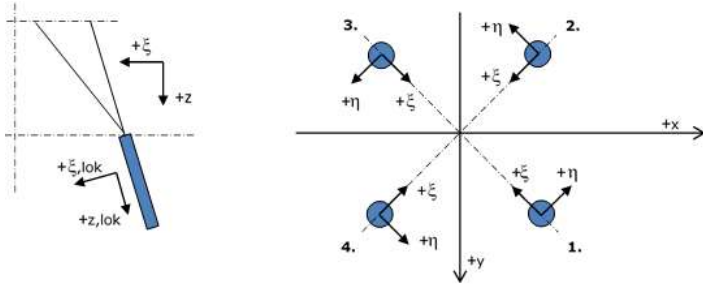
In tegenstelling tot de horizontaalkracht bij maximale verticale druk- of trekkracht, is de horizontale belasting door torsie niet gerelateerd aan de trek- of drukkracht in de randstijl. Op de bladzijde "max. trekbelasting en torsie" zijn de combinaties opgezocht waarbij zowel een grote trekkracht optreedt als een horizontale kracht door torsie.



**Figuur 11** Belasting bij torsiebelasting vanuit de mast



Belastingen op de fundatie in het lokale coördinatenstelsel zijn uitgedrukt in de radiale en tangentiële richting eta en xi, zie Figuur 12.



**Figuur 12** Lokaal assenstelsel



Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft: **Trekbelasting**  
 Richting: **Globale assenstelsel**

|        | <b>Mastnummer</b> | <b>Masttype</b> | <b>Verticaal trek [kN]</b> | <b>X-richting [kN]</b> | <b>Y-richting [kN]</b> | <b>Betrouwbaarheidsniveau</b> | <b>Bijbehorende loadcase</b>  |
|--------|-------------------|-----------------|----------------------------|------------------------|------------------------|-------------------------------|-------------------------------|
| 25N    | HA+0              |                 | 1339,8                     | 229,5                  | -229,2                 | Nieuwbouw CC2                 | SPLS 1a_0,9_90 Ah All Cts     |
| 18N    | HA+5              |                 | 1466,0                     | 235,6                  | -242,9                 | Nieuwbouw CC2                 | SPLS 1a_0,9_90 Ah All Cts     |
| 68     | HB+0 (68)         |                 | 1096,2                     | -188,2                 | -180,3                 | Afkeur CC2-0                  | SPLS 3_0,9_105.975 Ba All Cts |
| 78     | HB+0 (78)         |                 | 1081,5                     | 185,7                  | -178,0                 | Afkeur CC2-0                  | SPLS 3_0,9_79.6 Ah All Cts    |
| 69N    | HB+5              |                 | 1526,7                     | 233,6                  | -259,9                 | Nieuwbouw CC2                 | ULS 1a_0,9_70_140 deg         |
| 17N    | HC+0              |                 | 1573,3                     | 256,2                  | -280,6                 | Nieuwbouw CC2                 | ULS 1a_0,9_60                 |
| 16     | HC+0 (16)         |                 | 1170,5                     | -203,4                 | -188,9                 | Afkeur CC2-0                  | SPLS 3_0,9_120.38 Ba All Cts  |
| 22N    | S+0               |                 | 774,2                      | 138,6                  | -128,3                 | Nieuwbouw CC2                 | ULS 1a_0,9_0,9_135            |
| 26(HS) | S+0 HS            |                 | 561,3                      | 100,3                  | -90,6                  | Afkeur CC2-0                  | ULS 1a_0,9_0,9_135            |
| 72N    | S+32              |                 | 1698,8                     | 280,6                  | -272,3                 | Nieuwbouw CC2                 | ULS 1a_0,9_0,9_135            |



Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft **Drukbelasting**  
 Richting **Globale assenstelsel**

| Mastnummer | Masttype  | Verticaal druk [kN] | X-richting [kN] | Y-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase     |
|------------|-----------|---------------------|-----------------|-----------------|------------------------|---------------------------|
| 25N        | HA+0      | -1650,2             | 274,4           | -285,9          | Nieuwbouw CC2          | SPLS 1a_90 Ah All Cts     |
| 18N        | HA+5      | -1795,2             | 281,3           | -303,0          | Nieuwbouw CC2          | SPLS 1a_90 Ah All Cts     |
| 68         | HB+0 (68) | -1362,0             | -221,9          | -231,1          | Afkeur CC2-0           | SPLS 3_105.975 Ba All Cts |
| 78         | HB+0 (78) | -1352,5             | 220,8           | -229,3          | Afkeur CC2-0           | SPLS 3_79.6 Ah All Cts    |
| 69N        | HB+5      | -1920,7             | 295,2           | -331,2          | Nieuwbouw CC2          | ULS 1a_70_140 deg         |
| 17N        | HC+0      | -2015,4             | -334,0          | -342,2          | Nieuwbouw CC2          | ULS 3_90                  |
| 16         | HC+0 (16) | -1458,0             | -233,1          | -250,0          | Afkeur CC2-0           | SPLS 3_120.38 Ba All Cts  |
| 22N        | S+0       | -983,8              | -177,1          | -166,7          | Nieuwbouw CC2          | ULS 1a_45                 |
| 26(HS)     | S+0 HS    | -726,5              | 131,7           | -121,3          | Afkeur CC2-0           | ULS 1a_135                |
| 72N        | S+32      | -2163,9             | -360,9          | -353,2          | Nieuwbouw CC2          | ULS 1a_45                 |



Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft: **Trekbelasting**  
 Richting: **Lokale assenstelsel**

| Mastnummer | Masttype  | Verticaal trek [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase         |
|------------|-----------|---------------------|------------------|-------------------|------------------------|-------------------------------|
| 25N        | HA+0      | 1378,3              | -28,3            | 0,2               | Nieuwbouw CC2          | SPLS 1a_0,9_90 Ah All Cts     |
| 18N        | HA+5      | 1503,8              | -47,3            | -5,1              | Nieuwbouw CC2          | SPLS 1a_0,9_90 Ah All Cts     |
| 68         | HB+0 (68) | 1126,6              | -18,3            | -5,6              | Afkeur CC2-0           | SPLS 3_0,9_105.975 Ba All Cts |
| 78         | HB+0 (78) | 1111,5              | -18,2            | 5,4               | Afkeur CC2-0           | SPLS 3_0,9_79.6 Ah All Cts    |
| 69N        | HB+5      | 1565,4              | -46,9            | -18,6             | Nieuwbouw CC2          | ULS 1a_0,9_70_140 deg         |
| 17N        | HC+0      | 1618,2              | -31,9            | -17,3             | Nieuwbouw CC2          | ULS 1a_0,9_60                 |
| 16         | HC+0 (16) | 1202,8              | -18,7            | -10,3             | Afkeur CC2-0           | SPLS 3_0,9_120.38 Ba All Cts  |
| 22N        | S+0       | 796,3               | -31,4            | 7,3               | Nieuwbouw CC2          | ULS 1a_0,9_0,9_135            |
| 26(HS)     | S+0 HS    | 576,9               | -20,8            | 6,8               | Afkeur CC2-0           | ULS 1a_0,9_0,9_135            |
| 72N        | S+32      | 1743,1              | 21,8             | 5,9               | Nieuwbouw CC2          | ULS 1a_0,9_0,9_135            |



Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft: **Drukbelasting**  
 Richting: **Lokale assenstelsel**

| Mastnummer | Masttype  | Verticaal druk [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase     |
|------------|-----------|---------------------|------------------|-------------------|------------------------|---------------------------|
| 25N        | HA+0      | -1696,8             | 31,6             | 8,2               | Nieuwbouw CC2          | SPLS 1a_90 Ah All Cts     |
| 18N        | HA+5      | -1841,3             | 56,7             | 15,4              | Nieuwbouw CC2          | SPLS 1a_90 Ah All Cts     |
| 68         | HB+0 (68) | -1399,0             | 19,4             | -6,5              | Afkeur CC2-0           | SPLS 3_105.975 Ba All Cts |
| 78         | HB+0 (78) | -1389,3             | 19,4             | 6,0               | Afkeur CC2-0           | SPLS 3_79.6 Ah All Cts    |
| 69N        | HB+5      | -1970,2             | 63,0             | 25,4              | Nieuwbouw CC2          | ULS 1a_70_140 deg         |
| 17N        | HC+0      | -2071,1             | 32,8             | -5,8              | Nieuwbouw CC2          | ULS 3_90                  |
| 16         | HC+0 (16) | -1497,4             | 19,4             | -11,9             | Afkeur CC2-0           | SPLS 3_120.38 Ba All Cts  |
| 22N        | S+0       | -1012,5             | 43,2             | 7,4               | Nieuwbouw CC2          | ULS 1a_45                 |
| 26(HS)     | S+0 HS    | -747,6              | 31,2             | -7,4              | Afkeur CC2-0           | ULS 1a_135                |
| 72N        | S+32      | -2222,0             | -20,8            | 5,5               | Nieuwbouw CC2          | ULS 1a_45                 |



Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft: **Torsiebelasting positief**  
 Richting: **Lokale assenstelsel**

| Mastrnummer | Masttype  | Verticaal [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase            |
|-------------|-----------|----------------|------------------|-------------------|------------------------|----------------------------------|
| 25N         | HA+0      | -278,1         | 13,0             | 152,4             | Nieuwbouw CC2          | SPLS 1a_80 Ba Ct2                |
| 18N         | HA+5      | -987,2         | 35,2             | 162,9             | Nieuwbouw CC2          | SPLS 3_80 Ah All Cts_(bouw)      |
| 68          | HB+0 (68) | -41,8          | 2,8              | -145,3            | Afkeur CC2-0           | SPLS 6a_90 Ah Ct2 Ah Ct1         |
| 78          | HB+0 (78) | -173,2         | 5,6              | -134,7            | Afkeur CC2-0           | SPLS 6a_90 Ah Ct2 Ah Ct1         |
| 69N         | HB+5      | -284,2         | 14,5             | 158,5             | Nieuwbouw CC2          | SPLS 6a_90 Ba Ct2 Ba Ct1_160 deg |
| 17N         | HC+0      | 60,0           | -2,6             | 165,8             | Nieuwbouw CC2          | SPLS 3_0_9_110 Ah Ct1_(140 gr)   |
| 16          | HC+0 (16) | 59,5           | -5,1             | -146,5            | Afkeur CC2-0           | SPLS 6a_90 Ba Ct1 Ah Ct1         |
| 22N         | S+0       | -3,1           | 3,1              | 41,7              | Nieuwbouw CC2          | ULS 5a Ba 21                     |
| 26(HS)      | S+0 HS    | -33,3          | 3,7              | -39,2             | Afkeur CC2-0           | ULS 5a Ba 10                     |
| 72N         | S+32      | -186,0         | -1,7             | 50,6              | Nieuwbouw CC2          | ULS 8 Ba_Bouwfase                |



Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft: **Torsiebelasting negatief**  
 Richting: **Lokale assenstelsel**

| Mastnummer | Masttype  | Verticaal [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase               |
|------------|-----------|----------------|------------------|-------------------|------------------------|-------------------------------------|
| 25N        | HA+0      | -43,7          | -5,8             | -153,8            | Nieuwbouw CC2          | SPLS 1a_0.9_80 Ba Ct1               |
| 18N        | HA+5      | -947,1         | 35,1             | -159,1            | Nieuwbouw CC2          | SPLS 6a_90 Ba All Cts Ah Ct1_(bouw) |
| 68         | HB+0 (68) | -41,8          | 2,8              | -145,3            | Afkeur CC2-0           | SPLS 6a_90 Ah Ct2 Ah Ct1            |
| 78         | HB+0 (78) | -173,2         | 5,6              | -134,7            | Afkeur CC2-0           | SPLS 6a_90 Ah Ct2 Ah Ct1            |
| 69N        | HB+5      | -933,5         | 36,3             | -165,4            | Nieuwbouw CC2          | SPLS 6a_90 Ba All Cts Ah Ct1_(bouw) |
| 17N        | HC+0      | 60,1           | -2,6             | -165,8            | Nieuwbouw CC2          | SPLS 3_0,9_70 Ba Ct1_(140 gr)       |
| 16         | HC+0 (16) | 59,5           | -5,1             | -146,5            | Afkeur CC2-0           | SPLS 6a_90 Ba Ct1 Ah Ct1            |
| 22N        | S+0       | -3,0           | 3,1              | -41,7             | Nieuwbouw CC2          | ULS 5a Ah 21                        |
| 26(HS)     | S+0 HS    | -33,3          | 3,7              | -39,2             | Afkeur CC2-0           | ULS 5a Ba 10                        |
| 72N        | S+32      | 1206,9         | 27,4             | -43,5             | Nieuwbouw CC2          | ULS 1a_90                           |



Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft **Max. trekbelasting + torsie**  
 Richting **Lokale assenstelsel**

| Mastnummer | Masttype  | Verticaal [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase         |
|------------|-----------|----------------|------------------|-------------------|------------------------|-------------------------------|
| 25N        | HA+0      | 992,0          | -25,0            | -138,8            | Nieuwbouw CC2          | SPLS 1a_0,9_90 Ah Ct2         |
| 18N        | HA+5      | 1503,8         | -47,3            | -5,1              | Nieuwbouw CC2          | SPLS 1a_0,9_90 Ah All Cts     |
| 68         | HB+0 (68) | 1126,6         | -18,3            | -5,6              | Afkeur CC2-0           | SPLS 3_0,9_105.975 Ba All Cts |
| 78         | HB+0 (78) | 1111,5         | -18,2            | 5,4               | Afkeur CC2-0           | SPLS 3_0,9_79.6 Ah All Cts    |
| 69N        | HB+5      | 1565,4         | -46,9            | -18,6             | Nieuwbouw CC2          | ULS 1a_0,9_70_140 deg         |
| 17N        | HC+0      | 1236,8         | -20,1            | 140,2             | Nieuwbouw CC2          | SPLS 3_0,9_90 Ah Ct1          |
| 16         | HC+0 (16) | 878,1          | -14,8            | -146,4            | Afkeur CC2-0           | SPLS 6a_90 Ba Ct1 Ah Ct1      |
| 22N        | S+0       | 702,7          | -23,5            | 33,5              | Nieuwbouw CC2          | ULS 1a_0,9_0,9_90             |
| 26(HS)     | S+0 HS    | 576,3          | -20,6            | 7,1               | Afkeur CC2-0           | ULS 1a_0,9_135                |
| 72N        | S+32      | 1743,1         | 21,8             | 5,9               | Nieuwbouw CC2          | ULS 1a_0,9_0,9_135            |





Project: **RLL-TLB**  
 Uitgangspunt: **Nieuwbouw**  
 Datum: **10-11-2021**

Betreft: **Torsiebelasting hoekmasten**  
 Richting: **Lokale assenstelsel**

| Mastnummer | Masttype  | Verticaal trek [kN] | Xi-richting [kN] | Eta-richting [kN] | Betrouwbaarheidsniveau | Bijbehorende loadcase         |
|------------|-----------|---------------------|------------------|-------------------|------------------------|-------------------------------|
| 25N        | HA+0      | 992,0               | -25,0            | -138,8            | Nieuwbouw CC2          | SPLS 1a_0,9_90 Ah Ct2         |
| 18N        | HA+5      | 1503,8              | -47,3            | -5,1              | Nieuwbouw CC2          | SPLS 1a_0,9_90 Ah All Cts     |
| 68         | HB+0 (68) | 1126,6              | -18,3            | -5,6              | Afkeur CC2-0           | SPLS 3_0,9_105.975 Ba All Cts |
| 78         | HB+0 (78) | 1111,5              | -18,2            | 5,4               | Afkeur CC2-0           | SPLS 3_0,9_79.6 Ah All Cts    |
| 69N        | HB+5      | 1565,4              | -46,9            | -18,6             | Nieuwbouw CC2          | ULS 1a_0,9_70_140 deg         |
| 17N        | HC+0      | 1236,8              | -20,1            | 140,2             | Nieuwbouw CC2          | SPLS 3_0,9_90 Ah Ct1          |
| 16         | HC+0 (16) | 878,1               | -14,8            | -146,4            | Afkeur CC2-0           | SPLS 6a_90 Ba Ct1 Ah Ct1      |

## APPENDIX B

### Fundatiegegevens

| Paalgegevens |           |              |              |                |                         |                              |                         |                                   |                            |                               |
|--------------|-----------|--------------|--------------|----------------|-------------------------|------------------------------|-------------------------|-----------------------------------|----------------------------|-------------------------------|
| Mastnr.      | Masttype  | Aantal palen | Paaltype     | Paallengte [m] | Paal boven maaiveld [m] | Paalpuntniveau t.o.v. MV [m] | Maaiveld t.o.v. NAP [m] | Bovenkant fundatie t.o.v. NAP [m] | Paal tov. bk. fundatie [m] | Paalpuntniveau t.o.v. NAP [m] |
| 16           | HC+0 (16) | 1            | RP-53-124+GI | 19,35          | 0,50                    | -18,85                       | 0,00                    | 0,50                              | 0,00                       | -18,85                        |
| 16AN         | HA+0      | 1            | SI Ø610/850  | 23,20          | 0,50                    | -22,70                       | 0,20                    | 0,70                              | 0,00                       | -22,50                        |
| 17N          | HC+0      | 1            | SI Ø762/950  | 22,70          | 0,50                    | -22,20                       | 0,20                    | 0,70                              | 0,00                       | -22,00                        |
| 18N          | HA+5      | 1            | SI Ø610/850  | 19,90          | 0,50                    | -19,40                       | -1,10                   | -0,60                             | 0,00                       | -20,50                        |
| 19N          | S+0       | 1            | SI Ø610/850  | 14,40          | 0,50                    | -13,90                       | -1,10                   | -0,60                             | 0,00                       | -15,00                        |
| 20N          | S+0       | 1            | SI Ø610/850  | 14,40          | 0,50                    | -13,90                       | -1,10                   | -0,60                             | 0,00                       | -15,00                        |
| 21N          | S+0       | 1            | SI Ø610/850  | 14,40          | 0,50                    | -13,90                       | -1,10                   | -0,60                             | 0,00                       | -15,00                        |
| 22N          | S+0       | 1            | SI Ø610/850  | 14,40          | 0,50                    | -13,90                       | -1,10                   | -0,60                             | 0,00                       | -15,00                        |
| 23N          | S+0       | 1            | SI Ø610/850  | 14,40          | 0,50                    | -13,90                       | -1,10                   | -0,60                             | 0,00                       | -15,00                        |
| 24N          | HA+0      | 1            | SI Ø610/850  | 18,40          | 0,50                    | -17,90                       | -1,10                   | -0,60                             | 0,00                       | -19,00                        |
| 25N          | HA+0      | 1            | SI Ø610/850  | 18,40          | 0,50                    | -17,90                       | -1,10                   | -0,60                             | 0,00                       | -19,00                        |
| 26(HS)       | S+0 HS    | 1            | RP-53-124    | 15,85          | 0,50                    | -15,35                       | 0,00                    | 0,50                              | 0,00                       | -15,35                        |
| 68           | HB+0 (68) | 1            | RP-53-124+GI | 20,35          | 0,50                    | -19,85                       | 0,00                    | 0,50                              | 0,00                       | -19,85                        |
| 69N          | HB+5      | 1            | SI Ø610/850  | 25,00          | 0,50                    | -24,50                       | 0,00                    | 0,50                              | 0,00                       | -24,50                        |
| 70N          | HA+5      | 1            | SI Ø610/850  | 24,50          | 0,50                    | -24,00                       | 0,00                    | 0,50                              | 0,00                       | -24,00                        |
| 71N          | S+32      | 2            | SI Ø508/670  | 21,50          | 0,00                    | -21,50                       | 0,00                    | 0,50                              | 0,50                       | -21,50                        |
| 72N          | S+32      | 1            | SI Ø762/950  | 23,40          | 0,50                    | -22,90                       | 0,40                    | 0,90                              | 0,00                       | -22,50                        |
| 73N          | HA+0      | 1            | SI Ø610/850  | 15,90          | 0,50                    | -15,40                       | 0,40                    | 0,90                              | 0,00                       | -15,00                        |
| 74N          | S+0       | 1            | SI Ø610/850  | 12,40          | 0,50                    | -11,90                       | 0,40                    | 0,90                              | 0,00                       | -11,50                        |
| 75N          | S+0       | 1            | SI Ø610/850  | 12,40          | 0,50                    | -11,90                       | 0,40                    | 0,90                              | 0,00                       | -11,50                        |
| 76N          | HA+0      | 1            | SI Ø610/850  | 18,80          | 0,50                    | -18,30                       | 0,80                    | 1,30                              | 0,00                       | -17,50                        |
| 78           | HB+0 (78) | 1            | RP-53-124+GI | 13,35          | 0,50                    | -12,85                       | 0,00                    | 0,50                              | 0,00                       | -12,85                        |

| Poergegevens - nieuw |          |             |       |       |       |                             |   |                            |                       |                               |                         |
|----------------------|----------|-------------|-------|-------|-------|-----------------------------|---|----------------------------|-----------------------|-------------------------------|-------------------------|
| Mastnr.              | Masttype | Poertype    | L [m] | b [m] | h [m] | Bovenkant poer tov. NAP [m] | Bovenkant poer tov. MV [m] <sup>(1)</sup> | Onderkant poer tov. MV [m] | Volume. onder GWS [m] | Volume poer [m <sup>3</sup> ] | EG <sub>poer</sub> [kN] |
| 71N                  | S+32     | 2-paalspoer | 3,00  | 1,50  | 2,00  | 0,50                        | 0,50                                      | -1,50                      | 5,91                  | 7,88                          | 197                     |

| Poergegevens – verzwaarde fundatie mast 26 |          |                  |       |       |       |                             |   |                            |                       |                               |                         |
|--|----------|------------------|-------|-------|-------|-----------------------------|---|----------------------------|-----------------------|-------------------------------|-------------------------|
| Mastnr.                                    | Masttype | Poertype         | L [m] | b [m] | h [m] | Bovenkant poer tov. NAP [m] | Bovenkant poer tov. MV [m] <sup>(1)</sup> | Onderkant poer tov. MV [m] | Volume. onder GWS [m] | Volume poer [m <sup>3</sup> ] | EG <sub>poer</sub> [kN] |
| 26(HS)                                     | S+0 HS   | RP-53-124 + poer | 1,70  | 1,70  | 1,70  | 0,50                        | 0,50                                      | -1,20                      | 4,18                  | 4,18                          | 104                     |

## APPENDIX C

### Resultaten

#### Toetsing funderingen op trekbelasting

| Mast   | Masttype     | Sondering             | Poertype         | Paaltype     | PP<br>niveau<br>[m-<br>NAP] | F <sub>Ed,mast</sub><br>[kN] | Aantal<br>palen<br>per<br>randstijl | Effecti-<br>viteit<br>palen | F <sub>poer,d</sub><br>[kN] | F <sub>Ed,paal</sub><br>[kN] | F <sub>R,d,trek</sub><br>[kN] | U.C. |
|--------|--------------|-----------------------|------------------|--------------|-----------------------------|------------------------------|-------------------------------------|-----------------------------|-----------------------------|------------------------------|-------------------------------|------|
| 16     | HC+0<br>(16) | M16-oud               | RP-53-<br>124+GI | RP-53-124+GI | -18,9                       | -1203                        | 1                                   | 100%                        | 0                           | 1203                         | 1934                          | 0,62 |
| 16AN   | HA+0         | 2019-1008_22.GEF      | 1-paals 610      | SI Ø610/850  | -22,5                       | -1378                        | 1                                   | 100%                        | 0                           | 1378                         | 1547                          | 0,89 |
| 17N    | HC+0         | 2019-1008_22.GEF      | 1-paals 762      | SI Ø762/950  | -22,0                       | -1618                        | 1                                   | 100%                        | 0                           | 1618                         | 1800                          | 0,90 |
| 18N    | HA+5         | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -20,5                       | -1504                        | 1                                   | 100%                        | 0                           | 1504                         | 1733                          | 0,87 |
| 19N    | S+0          | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -15,0                       | -796                         | 1                                   | 100%                        | 0                           | 796                          | 923                           | 0,86 |
| 20N    | S+0          | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -15,0                       | -796                         | 1                                   | 100%                        | 0                           | 796                          | 923                           | 0,86 |
| 21N    | S+0          | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -15,0                       | -796                         | 1                                   | 100%                        | 0                           | 796                          | 923                           | 0,86 |
| 22N    | S+0          | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -15,0                       | -796                         | 1                                   | 100%                        | 0                           | 796                          | 923                           | 0,86 |
| 23N    | S+0          | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -15,0                       | -796                         | 1                                   | 100%                        | 0                           | 796                          | 923                           | 0,86 |
| 24N    | HA+0         | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -19,0                       | -1378                        | 1                                   | 100%                        | 0                           | 1378                         | 1560                          | 0,88 |
| 25N    | HA+0         | 02P001595_251.S01.GEF | 1-paals 610      | SI Ø610/850  | -19,0                       | -1378                        | 1                                   | 100%                        | 0                           | 1378                         | 1560                          | 0,88 |
| 26(HS) | S+0 HS       | 26-oud                | RP-53-124        | RP-53-124    | -15,4                       | -577                         | 1                                   | 100%                        | 0                           | 577                          | 553                           | 1,04 |
| 68     | HB+0<br>(68) | M68-oud               | RP-53-<br>124+GI | RP-53-124+GI | -19,9                       | -1127                        | 1                                   | 100%                        | 0                           | 1127                         | 1127                          | 1,00 |
| 69N    | HB+5         | 02P001595_202.S03.GEF | 1-paals 610      | SI Ø610/850  | -24,5                       | -1565                        | 1                                   | 100%                        | 0                           | 1565                         | 1793                          | 0,87 |
| 70N    | HA+5         | 02P001595_202.S03.GEF | 1-paals 610      | SI Ø610/850  | -24,0                       | -1504                        | 1                                   | 100%                        | 0                           | 1504                         | 1724                          | 0,87 |
| 71N    | S+32         | 02P001595_202.S03.GEF | 2-paalspoer      | SI Ø508/670  | -21,5                       | -1743                        | 2                                   | 95%                         | 118                         | 855                          | 955                           | 0,90 |
| 72N    | S+32         | 2019-1008_15.GEF      | 1-paals 762      | SI Ø762/950  | -22,5                       | -1743                        | 1                                   | 100%                        | 0                           | 1743                         | 1950                          | 0,89 |
| 73N    | HA+0         | 2019-1008_15.GEF      | 1-paals 610      | SI Ø610/850  | -15,0                       | -1378                        | 1                                   | 100%                        | 0                           | 1378                         | 1581                          | 0,87 |
| 74N    | S+0          | 2019-1008_15.GEF      | 1-paals 610      | SI Ø610/850  | -11,5                       | -796                         | 1                                   | 100%                        | 0                           | 796                          | 935                           | 0,85 |
| 75N    | S+0          | 2019-1008_15.GEF      | 1-paals 610      | SI Ø610/850  | -11,5                       | -796                         | 1                                   | 100%                        | 0                           | 796                          | 935                           | 0,85 |
| 76N    | HA+0         | 2019-1008_14.GEF      | 1-paals 610      | SI Ø610/850  | -17,5                       | -1378                        | 1                                   | 100%                        | 0                           | 1378                         | 1557                          | 0,89 |
| 78     | HB+0<br>(78) | 78-oud                | RP-53-<br>124+GI | RP-53-124+GI | -12,9                       | -1112                        | 1                                   | 100%                        | 0                           | 1112                         | 1896                          | 0,59 |

#### Toetsing funderingen op trekbelasting – verzwaarde fundatie mast 26

| Mast   | Masttype | Sondering | Poertype         | Paaltype  | PP<br>niveau<br>[m-<br>NAP] | F <sub>Ed,mast</sub><br>[kN] | Aantal<br>palen<br>per<br>randstijl | Effectiviteit<br>palen | F <sub>poer,d</sub><br>[kN] | F <sub>Ed,paal</sub><br>[kN] | F <sub>R,d,trek</sub><br>[kN] | U.C. |
|--------|----------|-----------|------------------|-----------|-----------------------------|------------------------------|-------------------------------------|------------------------|-----------------------------|------------------------------|-------------------------------|------|
| 26(HS) | S+0 HS   | 26-oud    | RP-53-124 + poer | RP-53-124 | -15,4                       | -577                         | 1                                   | 100%                   | 52                          | 525                          | 553                           | 0,95 |

**Toetsing funderingen op drukbelasting**

| Mast   | Masttype  | Sondering             | Poertype     | Paaltype     | PP niveau [m-NAP] | F <sub>Ed,mast</sub> [kN] | Aantal palen per randstijl | Effectiviteit palen | F <sub>poer,d</sub> [kN] | F <sub>Ed,paal</sub> [kN] | F <sub>R,d,druk</sub> [kN] | U.C. |
|--------|-----------|-----------------------|--------------|--------------|-------------------|---------------------------|----------------------------|---------------------|--------------------------|---------------------------|----------------------------|------|
| 16     | HC+0 (16) | M16-oud               | RP-53-124+GI | RP-53-124+GI | -18,9             | 1497                      | 1                          | 100%                | 0                        | 1497                      | 4794                       | 0,31 |
| 16AN   | HA+0      | 2019-1008_22.GEF      | 1-paals 610  | SI Ø610/850  | -22,5             | 1697                      | 1                          | 100%                | 0                        | 1697                      | 3009                       | 0,56 |
| 17N    | HC+0      | 2019-1008_22.GEF      | 1-paals 762  | SI Ø762/950  | -22,0             | 2071                      | 1                          | 100%                | 0                        | 2071                      | 3546                       | 0,58 |
| 18N    | HA+5      | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -20,5             | 1841                      | 1                          | 100%                | 0                        | 1841                      | 2505                       | 0,74 |
| 19N    | S+0       | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -15,0             | 1013                      | 1                          | 100%                | 0                        | 1013                      | 1790                       | 0,57 |
| 20N    | S+0       | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -15,0             | 1013                      | 1                          | 100%                | 0                        | 1013                      | 1790                       | 0,57 |
| 21N    | S+0       | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -15,0             | 1013                      | 1                          | 100%                | 0                        | 1013                      | 1790                       | 0,57 |
| 22N    | S+0       | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -15,0             | 1013                      | 1                          | 100%                | 0                        | 1013                      | 1790                       | 0,57 |
| 23N    | S+0       | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -15,0             | 1013                      | 1                          | 100%                | 0                        | 1013                      | 1790                       | 0,57 |
| 24N    | HA+0      | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -19,0             | 1697                      | 1                          | 100%                | 0                        | 1697                      | 2507                       | 0,68 |
| 25N    | HA+0      | 02P001595_251.S01.GEF | 1-paals 610  | SI Ø610/850  | -19,0             | 1697                      | 1                          | 100%                | 0                        | 1697                      | 2507                       | 0,68 |
| 26(HS) | S+0 HS    | 26-oud                | RP-53-124    | RP-53-124    | -15,4             | 748                       | 1                          | 100%                | 0                        | 748                       | 2011                       | 0,37 |
| 68     | HB+0 (68) | M68-oud               | RP-53-124+GI | RP-53-124+GI | -19,9             | 1399                      | 1                          | 100%                | 0                        | 1399                      | 3366                       | 0,42 |
| 69N    | HB+5      | 02P001595_202.S03.GEF | 1-paals 610  | SI Ø610/850  | -24,5             | 1970                      | 1                          | 100%                | 0                        | 1970                      | 4443                       | 0,44 |
| 70N    | HA+5      | 02P001595_202.S03.GEF | 1-paals 610  | SI Ø610/850  | -24,0             | 1841                      | 1                          | 100%                | 0                        | 1841                      | 4323                       | 0,43 |
| 71N    | S+32      | 02P001595_202.S03.GEF | 2-paalspoer  | SI Ø508/670  | -21,5             | 2222                      | 2                          | 95%                 | 236                      | 1294                      | 2242                       | 0,58 |
| 72N    | S+32      | 2019-1008_15.GEF      | 1-paals 762  | SI Ø762/950  | -22,5             | 2222                      | 1                          | 100%                | 0                        | 2222                      | 4137                       | 0,54 |
| 73N    | HA+0      | 2019-1008_15.GEF      | 1-paals 610  | SI Ø610/850  | -15,0             | 1697                      | 1                          | 100%                | 0                        | 1697                      | 2704                       | 0,63 |
| 74N    | S+0       | 2019-1008_15.GEF      | 1-paals 610  | SI Ø610/850  | -11,5             | 1013                      | 1                          | 100%                | 0                        | 1013                      | 3588                       | 0,28 |
| 75N    | S+0       | 2019-1008_15.GEF      | 1-paals 610  | SI Ø610/850  | -11,5             | 1013                      | 1                          | 100%                | 0                        | 1013                      | 3588                       | 0,28 |
| 76N    | HA+0      | 2019-1008_14.GEF      | 1-paals 610  | SI Ø610/850  | -17,5             | 1697                      | 1                          | 100%                | 0                        | 1697                      | 2812                       | 0,60 |
| 78     | HB+0 (78) | 78-oud                | RP-53-124+GI | RP-53-124+GI | -12,9             | 1389                      | 1                          | 100%                | 0                        | 1389                      | 4004                       | 0,35 |

**Toetsing funderingen op drukbelasting – verzwaarde fundatie mast 26**

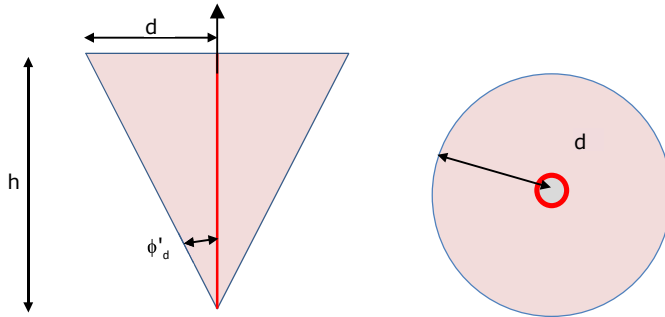
| Mast   | Masttype | Sondering | Poertype         | Paaltype  | PP niveau [m-NAP] | F <sub>Ed,mast</sub> [kN] | Aantal palen per randstijl | Effectiviteit palen | F <sub>poer,d</sub> [kN] | F <sub>Ed,paal</sub> [kN] | F <sub>R,d,druk</sub> [kN] | U.C. |
|--------|----------|-----------|------------------|-----------|-------------------|---------------------------|----------------------------|---------------------|--------------------------|---------------------------|----------------------------|------|
| 26(HS) | S+0 HS   | 26-oud    | RP-53-124 + poer | RP-53-124 | -15,4             | 748                       | 1                          | 100%                | 125                      | 873                       | 2011                       | 0,43 |

## Controle kluitgewicht

De minimaal benodigde diepte op basis van het kluitgewicht is onderzocht.

Uit voorgaande appendix blijkt dat paalpuntniveau minimaal 11,9 m beneden maaiveld is. Uit de berekening blijkt dat met 11,9 m diepte voldoende grondgewicht gemobiliseerd kan worden voor de maximaal optredende trekbelasting. Het kluitgewicht is voldoende.

### Controle kluitgewicht



|                             |                                    |                      |
|-----------------------------|------------------------------------|----------------------|
| Volumiek gewicht grond      |                                    | 18 kN/m <sup>3</sup> |
| Volumiek gewicht water      |                                    | 10 kN/m <sup>3</sup> |
| Veiligheidsfactor           | $\gamma_s =$                       | 0,9 -                |
| Hoek van inwendige wrijving | $f'$                               | 27,5 °               |
| Veiligheidsfactor           | $g_r =$                            | 1,25 -               |
| Diepte                      | $h =$                              | 11,9 m               |
| Radius kegel op mv.         | $d = L \times (\tan \alpha / g) =$ | 4,96 m               |
| Grondoppervlak kegel        | $A = \pi d^2 =$                    | 77,2 m <sup>2</sup>  |
| Inhoud kegel                | $I_{kluit} = 1/3Gh =$              | 306,1 m <sup>3</sup> |
| Gewicht grond               | $F_{gr} =$                         | 5509 kN              |
| Opwaartse kracht water      | $F_w =$                            | 3061 kN              |
| Rekenwaarde                 | $F_{r,d} = 0,9F_{gr} - F_w =$      | 1898 kN              |



## **APPENDIX D**

### **Uitvoer TS paalfunderingen**

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De uitvoer is opgedeeld in de volgende drie delen:

- Deel 1: Uitvoer nieuwe palen – steunmasten
- Deel 2: Uitvoer nieuwe palen – hoekmasten
- Deel 3: Uitvoer bestaande palen

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**ALGEMENE GEGEVENS**

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek  
 Datum : 29-09-2020  
 Bestand : P:\EANL\_Projects\10124719 - TenneT Engineering  
 ZW380 kV Oost\2 Content\010 D1.3  
 Reconstructiemasten\Technosoft\D1.3  
 Reconstructiemasten steun druk en trek.pvw  
 Berekeningstype : Verticaal belaste paal  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

**Toegepaste normen volgens Eurocode met Nederlandse NB**

|             |                    |            |         |
|-------------|--------------------|------------|---------|
| Geotechniek | EN 1997-1:2004     | AC:2009    |         |
|             | NEN-EN 1997-1:2005 | C1+A1:2013 | NB:2016 |
|             | NEN 9997-1:2016    | C2:2017    |         |

**BODEMPROFIELGEGEVENS: 14**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

| Laag | Van [m] | Tot [m] | Omschrijving                 | Grondwaterstand [m] | OCR | Aandeel pos. kleef [%] | $\alpha_s$ | $d_{50}$ [mm] |
|------|---------|---------|------------------------------|---------------------|-----|------------------------|------------|---------------|
| 1    | 0.40    | -1.35   | Klei - Organisch - Matig     |                     | 1.0 | 50.0                   |            |               |
| 2    | -1.35   | -1.55   | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 3    | -1.55   | -1.75   | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 4    | -1.75   | -2.65   | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 5    | -2.65   | -2.85   | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 6    | -2.85   | -3.75   | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 7    | -3.75   | -4.15   | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 8    | -4.15   | -12.95  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 9    | -12.95  | -13.45  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 10   | -13.45  | -13.65  | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 11   | -13.65  | -13.85  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 12   | -13.85  | -14.05  | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 13   | -14.05  | -14.97  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 14   | -14.97  | -15.37  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 15   | -15.37  | -15.77  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 16   | -15.77  | -16.17  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 17   | -16.17  | -16.37  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 18   | -16.37  | -16.67  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 19   | -16.67  | -16.97  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 20   | -16.97  | -18.27  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 21   | -18.27  | -18.47  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 22   | -18.47  | -18.77  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 23   | -18.77  | -19.07  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 24   | -19.07  | -20.66  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 25   | -20.66  | -20.96  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 26   | -20.96  | -21.16  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 27   | -21.16  | -21.46  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 28   | -21.46  | -21.76  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 29   | -21.76  | -22.06  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 30   | -22.06  | -22.76  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 31   | -22.76  | -23.46  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 32   | -23.46  | -25.96  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 33   | -25.96  | -26.36  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 34   | -26.36  | -26.75  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 35   | -26.75  | -26.95  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 36   | -26.95  | -27.15  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 37   | -27.15  | -27.35  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 38   | -27.35  | -29.37  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 39   | -29.37  | -29.56  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 40   | -29.56  | -30.86  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 41   | -30.86  | -31.26  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 42   | -31.26  | -31.46  | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 43   | -31.46  | -31.66  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 44   | -31.66  | -31.88  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 45   | -31.88  | -32.51  | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 46   | -32.51  | -32.73  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 47   | -32.73  | -32.93  | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 48   | -32.93  | -33.16  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 49   | -33.16  | -34.45  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 50   | -34.45  | -34.59  | Grind - Zwak siltig - Vast   |                     | 1.0 | 50.0                   |            |               |

**BODEMPROFIELGEGEVENS: 15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

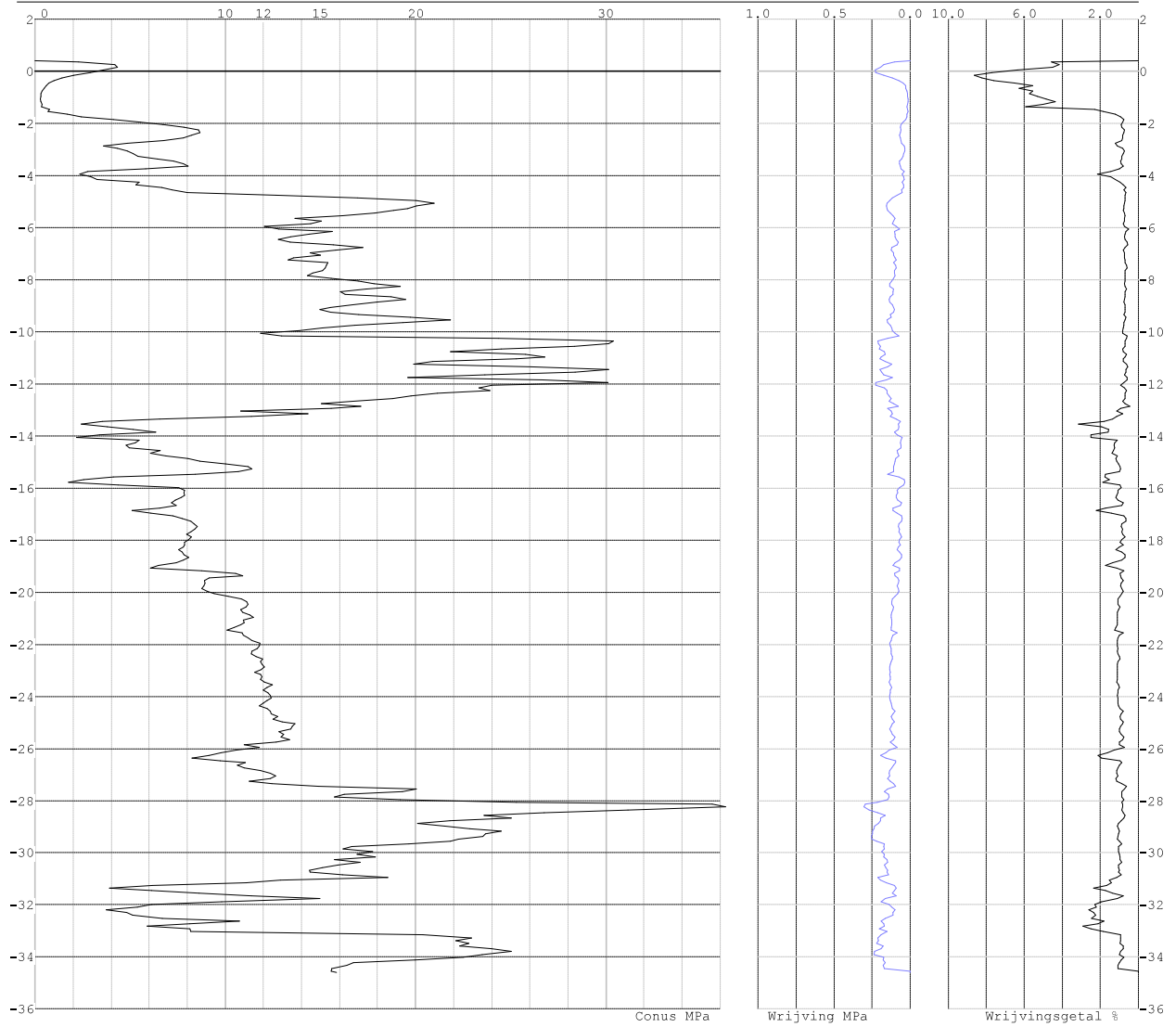
| Laag | Van [m] | Tot [m] | Omschrijving                 | Grondwaterstand [m] | OCR | Aandeel pos. kleef [%] | $\alpha_s$ | $d_{50}$ [mm] |
|------|---------|---------|------------------------------|---------------------|-----|------------------------|------------|---------------|
| 1    | 0.75    | -0.60   | Klei - Organisch - Matig     |                     | 1.0 | 50.0                   |            |               |
| 2    | -0.60   | -5.90   | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 3    | -5.90   | -6.20   | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 4    | -6.20   | -15.89  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 5    | -15.89  | -20.68  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 6    | -20.68  | -32.95  | Zand - Schoon - Matig        |                     | 1.0 | 100.0                  |            |               |
| 7    | -32.95  | -33.18  | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 8    | -33.18  | -33.40  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 9    | -33.40  | -33.64  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |
| 10   | -33.64  | -33.88  | Zand - Sterk siltig - Kleiig |                     | 1.0 | 100.0                  |            |               |
| 11   | -33.88  | -34.24  | Klei - Zwak zandig - Vast    |                     | 1.0 | 50.0                   |            |               |
| 12   | -34.24  | -34.41  | Zand - Schoon - Vast         |                     | 1.0 | 100.0                  |            |               |





Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SONDERINGSGEGEVENS GRAFIEK: 19-1008-14**

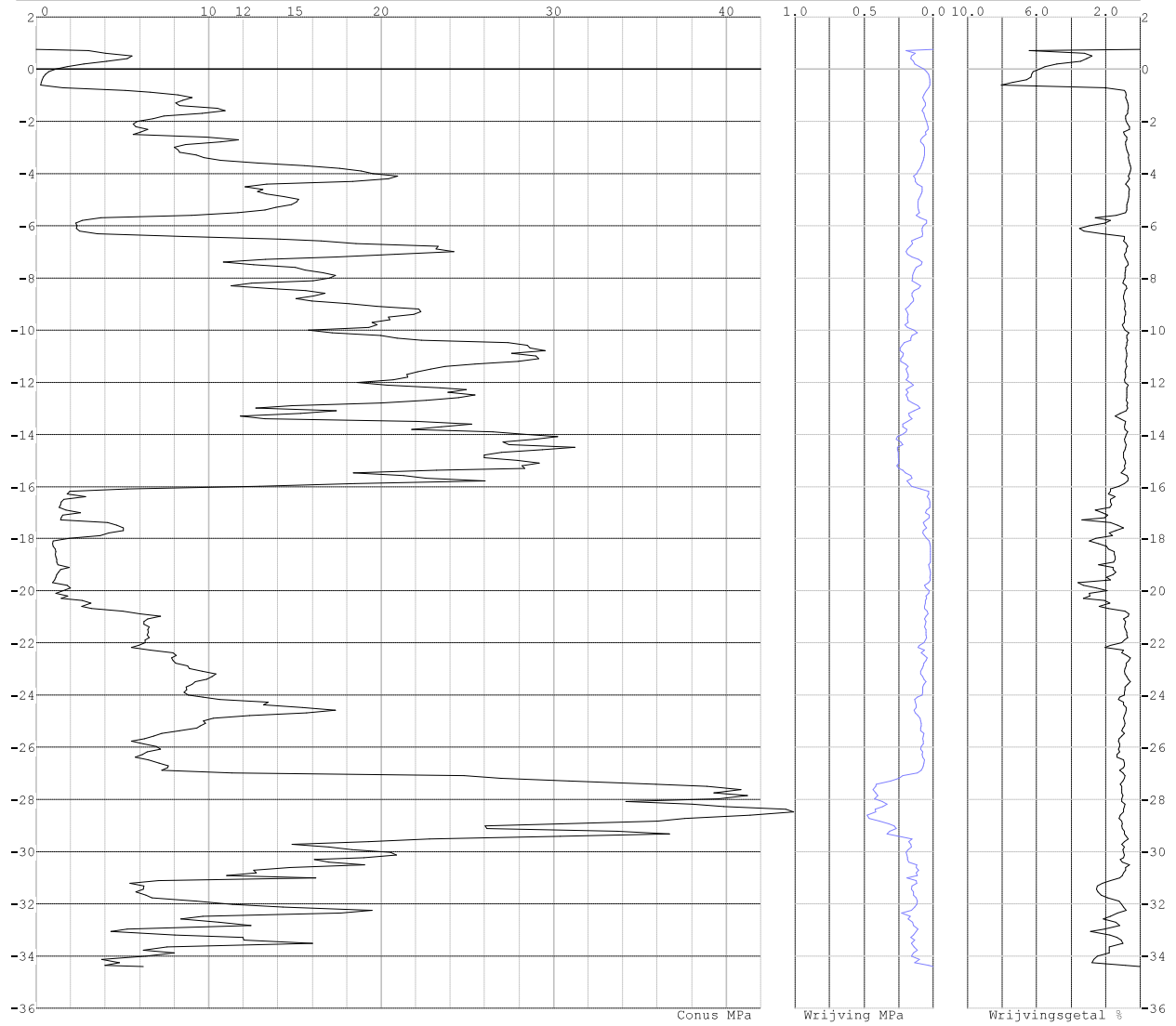


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : 0.75 Bodemprofiel: 15  
Traject negatieve kleeft : 0.75 tot -0.59 [m]  
Traject positieve kleeft : -0.60 tot -34.41 [m]

**SONDERINGSGEGEVENS GRAFIEK: 19-1008-15**

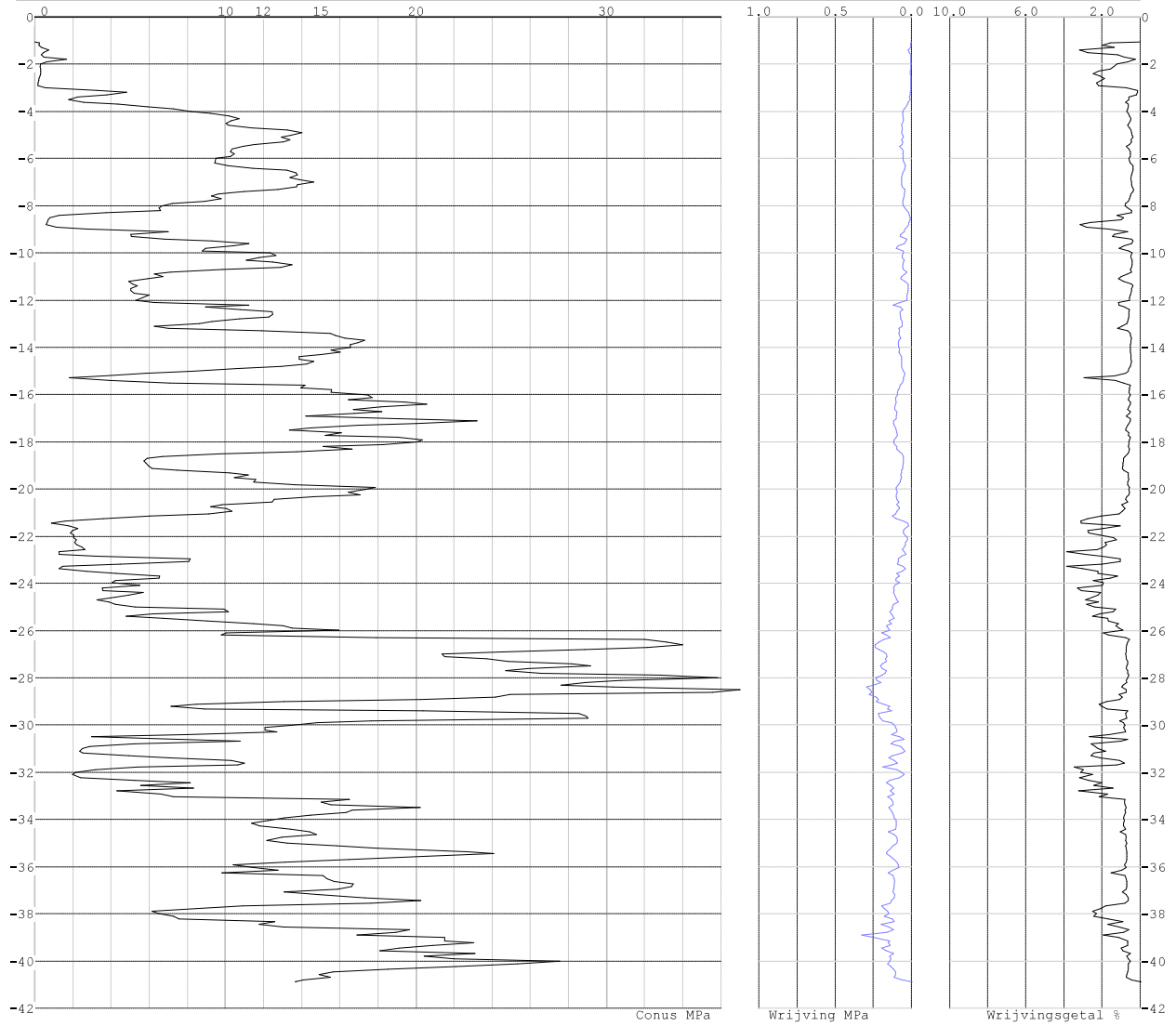


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : -1.05 Bodemprofiel: 251.S01  
Traject negatieve kleeft : -1.05 tot -3.60 [m]  
Traject positieve kleeft : -3.60 tot -40.88 [m]

**SONDERINGSGEGEVENS GRAFIEK: 251.S01**

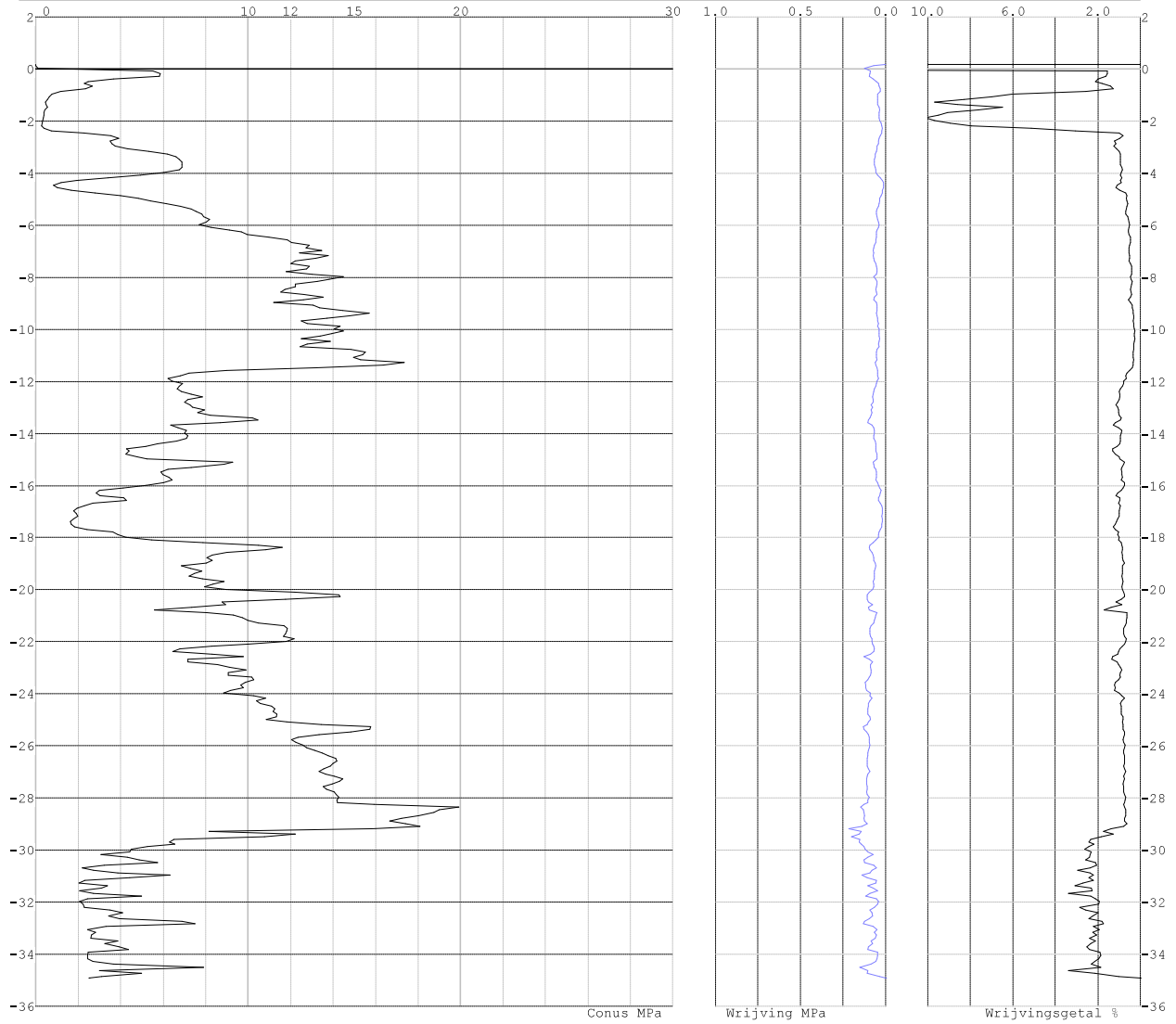


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 19-1008-22**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : 0.18 Bodemprofiel: 22  
Traject negatieve kleeft : 0.18 tot -2.46 [m]  
Traject positieve kleeft : -2.47 tot -34.92 [m]

**SONDERINGSGEGEVENS GRAFIEK: 19-1008-22**

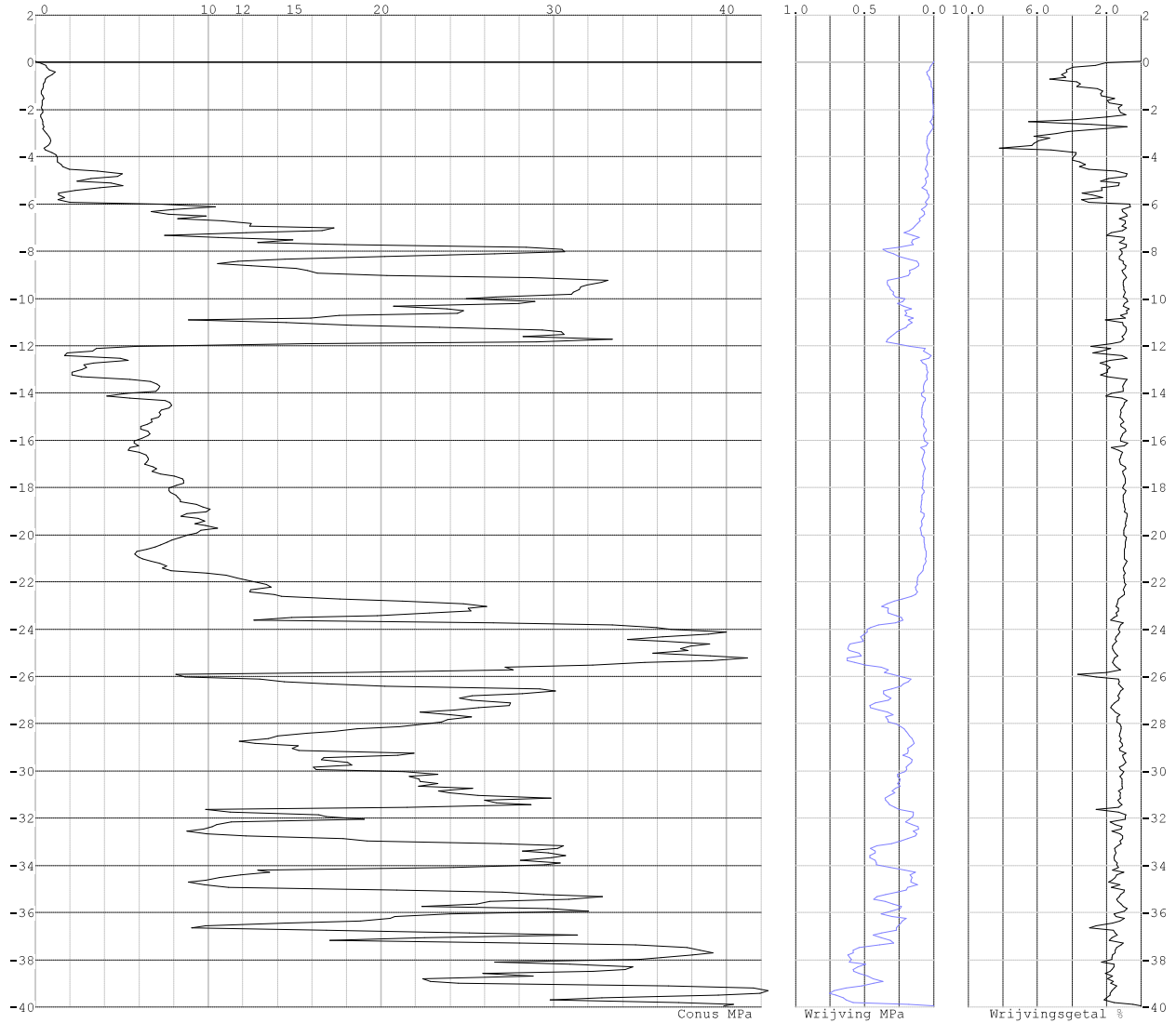


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
 Hoogte maaiveld [m] : 0.03 Bodemprofiel: 202.S03 wrijf  
 Traject negatieve kleeft : 0.03 tot -4.50 [m]  
 Traject positieve kleeft : -4.50 tot -39.95 [m]

**SONDERINGSGEGEVENS GRAFIEK: 202.S03**



**REKENGEGEVENS SI Ø508/670 druk**

Berekening : Ontwerpend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_3 (n=1)$  : 1.39 (handmatig)  
 Factor  $\xi_3 (gem)$  : 1.39 (handmatig)  
 Factor  $\xi_4 (min)$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{f;nk}$  : 1.0  
 $R_{s,calc,max;1}$  begrenzen op  $0.75 * R_{u,calc,max;1}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø508/670  
 Niveau paalkop [m] : N.A.P. 0.00  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS SI Ø508/670**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|-----------------|----------------|-----------------|
| 1  | -6.00           | -25.00         | 0.50            |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**RESULTATEN SI Ø508/670 druk (n=1)**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Sondering 19-1008-14 19-1008-15 251.S01 19-1008-22 202.S03

| Niveau<br>[m] | F <sub>nettoerd</sub><br>[kN] | F <sub>nettoerd</sub><br>[kN] | F <sub>nettoerd</sub><br>[kN] | F <sub>nettoerd</sub><br>[kN] | F <sub>nettoerd</sub><br>[kN] |
|---------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|
| -6.00         | <b>1303</b>                   | 797                           | 621                           | 746                           | <u>411</u>                    |
| -6.50         | <b>1473</b>                   | 1382                          | <u>526</u>                    | 995                           | 613                           |
| -7.00         | <b>1599</b>                   | 1449                          | <u>556</u>                    | 1105                          | 727                           |
| -7.50         | <b>1754</b>                   | 1550                          | <u>554</u>                    | 1222                          | 1086                          |
| -8.00         | <b>1837</b>                   | 1629                          | <u>558</u>                    | 1336                          | 1161                          |
| -8.50         | <b>1960</b>                   | 1893                          | <u>542</u>                    | 1448                          | 1245                          |
| -9.00         | 2081                          | <b>2161</b>                   | <u>788</u>                    | 1628                          | 1513                          |
| -9.50         | 2160                          | <b>2292</b>                   | <u>921</u>                    | 1396                          | 1599                          |
| -10.00        | <b>2546</b>                   | 2534                          | <u>979</u>                    | 1416                          | 1127                          |
| -10.50        | 2578                          | <b>2753</b>                   | <u>1029</u>                   | 1448                          | 1085                          |
| -11.00        | 2053                          | <b>2581</b>                   | <u>1062</u>                   | 1484                          | 1071                          |
| -11.50        | 1728                          | <b>2636</b>                   | 1121                          | 1490                          | <u>1061</u>                   |
| -12.00        | 1668                          | <b>2706</b>                   | 1315                          | 1509                          | <u>956</u>                    |
| -12.50        | 1675                          | <b>2730</b>                   | 1403                          | 1396                          | <u>989</u>                    |
| -13.00        | 1674                          | <b>2727</b>                   | 1280                          | 1429                          | <u>1014</u>                   |
| -13.50        | 1661                          | <b>3282</b>                   | 1344                          | 1456                          | <u>1173</u>                   |
| -14.00        | 1720                          | <b>2293</b>                   | 1386                          | 1375                          | <u>1247</u>                   |
| -14.50        | 1766                          | <b>2187</b>                   | 1392                          | 1322                          | <u>1306</u>                   |
| -15.00        | 1809                          | <b>2122</b>                   | 1353                          | <u>1303</u>                   | 1355                          |
| -15.50        | 1765                          | <b>2092</b>                   | 1939                          | <u>1312</u>                   | 1404                          |
| -16.00        | 1958                          | 2020                          | <b>2161</b>                   | <u>1321</u>                   | 1446                          |
| -16.50        | 1999                          | <b>2032</b>                   | 1962                          | <u>1329</u>                   | 1536                          |
| -17.00        | <b>2105</b>                   | 2050                          | 2012                          | <u>1331</u>                   | 1616                          |
| -17.50        | <b>2167</b>                   | 2035                          | 2089                          | <u>1396</u>                   | 1739                          |
| -18.00        | <b>2226</b>                   | 2036                          | 2111                          | <u>1663</u>                   | 1808                          |
| -18.50        | <b>2284</b>                   | 2044                          | 2102                          | <u>1714</u>                   | 1801                          |
| -19.00        | <b>2447</b>                   | 2052                          | 2013                          | <u>1781</u>                   | 1845                          |
| -19.50        | <b>2535</b>                   | 2065                          | 1970                          | <u>1857</u>                   | 1889                          |
| -20.00        | <b>2696</b>                   | 2094                          | 1973                          | 1943                          | <u>1913</u>                   |
| -20.50        | <b>2801</b>                   | 2232                          | 1981                          | 1955                          | <u>1932</u>                   |
| -21.00        | <b>2881</b>                   | 2369                          | 2027                          | 2101                          | <u>2019</u>                   |
| -21.50        | <b>2996</b>                   | 2425                          | <u>2049</u>                   | 2175                          | 2242                          |
| -22.00        | <b>3101</b>                   | 2505                          | <u>2061</u>                   | 2211                          | 2439                          |
| -22.50        | <b>3202</b>                   | 2661                          | <u>2099</u>                   | 2300                          | 2732                          |
| -23.00        | <b>3295</b>                   | 2786                          | <u>2162</u>                   | 2430                          | 2866                          |
| -23.50        | <b>3374</b>                   | 2784                          | <u>2256</u>                   | 2495                          | 3317                          |
| -24.00        | <b>3266</b>                   | 2838                          | <u>2305</u>                   | 2622                          | 3113                          |
| -24.50        | <b>3326</b>                   | 2898                          | <u>2353</u>                   | 2735                          | 3228                          |
| -25.00        | <b>3384</b>                   | 2940                          | <u>2530</u>                   | 2908                          | 3200                          |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SAMENVATTINGSTABEL SI Ø508/670 druk (n=1)**

**Uitgangspunten**

- paal : SI Ø508/670  
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie  
 - schachtafmeting : 590 mm  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld niveau | paalpunt niveau | Bezijskdraagvermogen |                   |                   | Rekenwaarden   |                 |                      |
|------------|-----------------|-----------------|----------------------|-------------------|-------------------|----------------|-----------------|----------------------|
|            |                 |                 | $R_{b,real}$ [kN]    | $R_{s,real}$ [kN] | $R_{c,real}$ [kN] | $R_{c;d}$ [kN] | $F_{nk;d}$ [kN] | $R_{c,netto;d}$ [kN] |
| 19-1008-14 | 0.40            | -6.00           | 1606.6               | 586.5             | 2193.1            | 1314.8         | -11.9           | 1302.9               |
|            |                 | -6.50           | 1782.9               | 693.1             | 2476.0            | 1484.4         | -11.9           | 1472.5               |
|            |                 | -7.00           | 1883.5               | 804.1             | 2687.5            | 1611.2         | -11.9           | 1599.3               |
|            |                 | -7.50           | 2030.3               | 915.1             | 2945.4            | 1765.8         | -11.9           | 1753.9               |
|            |                 | -8.00           | 2054.6               | 1029.6            | 3084.2            | 1849.0         | -11.9           | 1837.1               |
|            |                 | -8.50           | 2134.9               | 1154.7            | 3289.6            | 1972.2         | -11.9           | 1960.3               |
|            |                 | -9.00           | 2210.6               | 1279.8            | 3490.5            | 2092.6         | -11.9           | 2080.7               |
|            |                 | -9.50           | 2227.5               | 1395.1            | 3622.6            | 2171.8         | -11.9           | 2159.9               |
|            |                 | -10.00          | 2761.1               | 1505.8            | 4266.9            | 2558.1         | -11.9           | 2546.2               |
|            |                 | -10.50          | 2696.0               | 1624.0            | 4319.9            | 2589.9         | -11.9           | 2578.0               |
|            |                 | -11.00          | 1694.4               | 1749.1            | 3443.5            | 2064.5         | -11.9           | 2052.6               |
|            |                 | -11.50          | 1027.8               | 1874.2            | 2902.0            | 1739.8         | -11.9           | 1727.9               |
|            |                 | -12.00          | 802.3                | 1999.3            | 2801.7            | 1679.6         | -11.9           | 1667.8               |
|            |                 | -12.50          | 689.2                | 2124.4            | 2813.6            | 1686.8         | -11.9           | 1674.9               |
|            |                 | -13.00          | 563.9                | 2249.0            | 2812.8            | 1686.3         | -11.9           | 1674.4               |
|            |                 | -13.50          | 463.5                | 2326.4            | 2789.9            | 1672.6         | -11.9           | 1660.7               |
|            |                 | -14.00          | 515.6                | 2373.6            | 2889.2            | 1732.1         | -11.9           | 1720.2               |
|            |                 | -14.50          | 552.2                | 2413.3            | 2965.5            | 1777.9         | -11.9           | 1766.0               |
|            |                 | -15.00          | 565.2                | 2472.8            | 3038.1            | 1821.4         | -11.9           | 1809.5               |
|            |                 | -15.50          | 405.5                | 2558.7            | 2964.2            | 1777.1         | -11.9           | 1765.2               |
|            |                 | -16.00          | 693.3                | 2593.2            | 3286.5            | 1970.3         | -11.9           | 1958.4               |
|            |                 | -16.50          | 695.8                | 2657.6            | 3353.4            | 2010.4         | -11.9           | 1998.5               |
|            |                 | -17.00          | 818.6                | 2711.9            | 3530.6            | 2116.6         | -11.9           | 2104.7               |
|            |                 | -17.50          | 856.6                | 2777.7            | 3634.4            | 2178.9         | -11.9           | 2167.0               |
|            |                 | -18.00          | 887.6                | 2845.9            | 3733.5            | 2238.3         | -11.9           | 2226.4               |
| -18.50     | 919.2           | 2910.7          | 3829.9               | 2296.1            | -11.9             | 2284.2         |                 |                      |
| -19.00     | 1127.3          | 2973.8          | 4101.1               | 2458.7            | -11.9             | 2446.8         |                 |                      |
| -19.50     | 1198.9          | 3048.8          | 4247.7               | 2546.6            | -11.9             | 2534.7         |                 |                      |
| -20.00     | 1394.2          | 3123.2          | 4517.3               | 2708.2            | -11.9             | 2696.3         |                 |                      |
| -20.50     | 1481.3          | 3210.7          | 4691.9               | 2812.9            | -11.9             | 2801.0         |                 |                      |
| -21.00     | 1522.1          | 3303.2          | 4825.4               | 2892.9            | -11.9             | 2881.0         |                 |                      |
| -21.50     | 1625.4          | 3392.4          | 5017.8               | 3008.3            | -11.9             | 2996.4         |                 |                      |
| -22.00     | 1706.9          | 3485.7          | 5192.6               | 3113.1            | -11.9             | 3101.2         |                 |                      |
| -22.50     | 1777.8          | 3582.2          | 5360.0               | 3213.5            | -11.9             | 3201.6         |                 |                      |
| -23.00     | 1834.5          | 3681.5          | 5516.1               | 3307.0            | -11.9             | 3295.1         |                 |                      |
| -23.50     | 1867.0          | 3780.3          | 5647.2               | 3385.6            | -11.9             | 3373.7         |                 |                      |
| -24.00     | 1587.1          | 3880.4          | 5467.5               | 3277.9            | -11.9             | 3266.0         |                 |                      |
| -24.50     | 1587.5          | 3980.4          | 5567.9               | 3338.1            | -11.9             | 3326.2         |                 |                      |
| -25.00     | 1580.4          | 4084.4          | 5664.8               | 3396.2            | -11.9             | 3384.3         |                 |                      |
| 19-1008-15 | 0.75            | -6.00           | 512.7                | 824.0             | 1336.7            | 801.4          | -4.3            | 797.1                |
|            |                 | -6.50           | 1441.9               | 869.8             | 2311.7            | 1385.9         | -4.3            | 1381.6               |
|            |                 | -7.00           | 1453.8               | 969.9             | 2423.7            | 1453.0         | -4.3            | 1448.7               |
|            |                 | -7.50           | 1522.9               | 1068.9            | 2591.8            | 1553.9         | -4.3            | 1549.6               |
|            |                 | -8.00           | 1555.2               | 1169.0            | 2724.2            | 1633.2         | -4.3            | 1628.9               |
|            |                 | -8.50           | 1890.4               | 1273.5            | 3164.0            | 1896.9         | -4.3            | 1892.6               |
|            |                 | -9.00           | 2213.5               | 1398.6            | 3612.1            | 2165.6         | -4.3            | 2161.2               |
|            |                 | -9.50           | 2306.0               | 1523.8            | 3829.7            | 2296.0         | -4.3            | 2291.7               |
|            |                 | -10.00          | 2584.5               | 1648.9            | 4233.4            | 2538.0         | -4.3            | 2533.7               |
|            |                 | -10.50          | 2825.5               | 1774.0            | 4599.4            | 2757.5         | -4.3            | 2753.2               |
|            |                 | -11.00          | 2412.7               | 1899.1            | 4311.8            | 2585.0         | -4.3            | 2580.7               |
|            |                 | -11.50          | 2379.1               | 2024.2            | 4403.3            | 2639.9         | -4.3            | 2635.6               |
|            |                 | -12.00          | 2372.2               | 2149.3            | 4521.5            | 2710.7         | -4.3            | 2706.4               |
|            |                 | -12.50          | 2286.3               | 2274.4            | 4560.8            | 2734.3         | -4.3            | 2730.0               |
|            |                 | -13.00          | 2158.5               | 2397.5            | 4556.0            | 2731.4         | -4.3            | 2727.1               |
|            |                 | -13.50          | 2974.7               | 2506.6            | 5481.4            | 3286.2         | -4.3            | 3281.9               |
|            |                 | -14.00          | 1200.6               | 2631.7            | 3832.4            | 2297.6         | -4.3            | 2293.3               |
|            |                 | -14.50          | 897.6                | 2756.9            | 3654.5            | 2190.9         | -4.3            | 2186.6               |
|            |                 | -15.00          | 664.9                | 2882.0            | 3546.9            | 2126.4         | -4.3            | 2122.1               |
|            |                 | -15.50          | 490.3                | 3007.1            | 3497.4            | 2096.8         | -4.3            | 2092.5               |
|            |                 | -16.00          | 244.5                | 3131.2            | 3375.7            | 2023.8         | -4.3            | 2019.5               |
|            |                 | -16.50          | 234.5                | 3161.3            | 3395.8            | 2035.9         | -4.3            | 2031.5               |
|            |                 | -17.00          | 251.9                | 3174.9            | 3426.8            | 2054.4         | -4.3            | 2050.1               |
|            |                 | -17.50          | 205.6                | 3195.6            | 3401.2            | 2039.1         | -4.3            | 2034.8               |
|            |                 | -18.00          | 171.8                | 3230.7            | 3402.5            | 2039.9         | -4.3            | 2035.6               |
| -18.50     | 177.2           | 3239.9          | 3417.1               | 2048.6            | -4.3              | 2044.3         |                 |                      |
| -19.00     | 179.7           | 3249.7          | 3429.4               | 2056.0            | -4.3              | 2051.7         |                 |                      |
| -19.50     | 190.6           | 3261.4          | 3452.0               | 2069.5            | -4.3              | 2065.2         |                 |                      |
| -20.00     | 226.5           | 3273.4          | 3500.0               | 2098.3            | -4.3              | 2094.0         |                 |                      |
| -20.50     | 441.1           | 3289.7          | 3730.8               | 2236.7            | -4.3              | 2232.4         |                 |                      |
| -21.00     | 631.3           | 3327.9          | 3959.1               | 2373.6            | -4.3              | 2369.3         |                 |                      |
| -21.50     | 670.2           | 3381.6          | 4051.7               | 2429.1            | -4.3              | 2424.8         |                 |                      |
| -22.00     | 750.1           | 3435.3          | 4185.4               | 2509.2            | -4.3              | 2504.9         |                 |                      |
| -22.50     | 953.8           | 3491.3          | 4445.1               | 2664.9            | -4.3              | 2660.6         |                 |                      |
| -23.00     | 1094.3          | 3560.2          | 4654.5               | 2790.4            | -4.3              | 2786.1         |                 |                      |
| -23.50     | 1009.0          | 3642.2          | 4651.2               | 2788.5            | -4.3              | 2784.2         |                 |                      |
| -24.00     | 1025.7          | 3715.6          | 4741.3               | 2842.5            | -4.3              | 2838.2         |                 |                      |
| -24.50     | 1032.1          | 3808.9          | 4841.1               | 2902.3            | -4.3              | 2898.0         |                 |                      |
| -25.00     | 1008.3          | 3903.3          | 4911.6               | 2944.6            | -4.3              | 2940.3         |                 |                      |
| 251.S01    | -1.05           | -6.00           | 673.9                | 400.4             | 1074.3            | 644.1          | -23.1           | 621.0                |
|            |                 | -6.50           | 430.4                | 486.2             | 916.6             | 549.5          | -23.1           | 526.4                |
|            |                 | -7.00           | 379.8                | 586.3             | 966.1             | 579.2          | -23.1           | 556.1                |
|            |                 | -7.50           | 278.9                | 683.1             | 962.0             | 576.7          | -23.1           | 553.7                |
|            |                 | -8.00           | 196.5                | 772.0             | 968.5             | 580.6          | -23.1           | 557.6                |
| -8.50      | 110.3           | 831.9           | 942.2                | 564.9             | -23.1             | 541.8          |                 |                      |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld paalpunt |        | Bezwijkdraagvermogen        |                             |                             | Rekenwaarden           |                          |                                |
|------------|-------------------|--------|-----------------------------|-----------------------------|-----------------------------|------------------------|--------------------------|--------------------------------|
|            | niveau            | niveau | R <sub>b,real</sub><br>[kN] | R <sub>v,real</sub><br>[kN] | R <sub>c,real</sub><br>[kN] | R <sub>d</sub><br>[kN] | F <sub>hkd</sub><br>[kN] | R <sub>z netto;d</sub><br>[kN] |
| 251.S01    | -1.05             | -9.00  | 512.4                       | 840.9                       | 1353.3                      | 811.3                  | -23.1                    | 788.3                          |
|            |                   | -9.50  | 679.2                       | 896.2                       | 1575.4                      | 944.5                  | -23.1                    | 921.4                          |
|            |                   | -10.00 | 691.9                       | 980.1                       | 1671.9                      | 1002.4                 | -23.1                    | 979.3                          |
|            |                   | -10.50 | 676.5                       | 1078.7                      | 1755.2                      | 1052.3                 | -23.1                    | 1029.2                         |
|            |                   | -11.00 | 657.0                       | 1153.5                      | 1810.5                      | 1085.4                 | -23.1                    | 1062.4                         |
|            |                   | -11.50 | 709.0                       | 1199.0                      | 1908.0                      | 1143.9                 | -23.1                    | 1120.8                         |
|            |                   | -12.00 | 988.0                       | 1244.2                      | 2232.2                      | 1338.3                 | -23.1                    | 1315.2                         |
|            |                   | -12.50 | 1058.4                      | 1321.1                      | 2379.4                      | 1426.5                 | -23.1                    | 1403.5                         |
|            |                   | -13.00 | 761.7                       | 1411.9                      | 2173.6                      | 1303.1                 | -23.1                    | 1280.0                         |
|            |                   | -13.50 | 782.8                       | 1497.5                      | 2280.3                      | 1367.1                 | -23.1                    | 1344.0                         |
|            |                   | -14.00 | 733.8                       | 1616.5                      | 2350.3                      | 1409.1                 | -23.1                    | 1386.0                         |
|            |                   | -14.50 | 624.8                       | 1734.8                      | 2359.6                      | 1414.6                 | -23.1                    | 1391.6                         |
|            |                   | -15.00 | 432.6                       | 1862.8                      | 2295.4                      | 1376.2                 | -23.1                    | 1353.1                         |
|            |                   | -15.50 | 1352.0                      | 1920.1                      | 3272.1                      | 1961.7                 | -23.1                    | 1938.6                         |
|            |                   | -16.00 | 1607.9                      | 2035.6                      | 3643.5                      | 2184.4                 | -23.1                    | 2161.3                         |
|            |                   | -16.50 | 1149.9                      | 2160.7                      | 3310.6                      | 1984.8                 | -23.1                    | 1961.7                         |
|            |                   | -17.00 | 1109.8                      | 2284.4                      | 3394.2                      | 2034.9                 | -23.1                    | 2011.9                         |
|            |                   | -17.50 | 1119.7                      | 2402.5                      | 3522.2                      | 2111.7                 | -23.1                    | 2088.6                         |
|            |                   | -18.00 | 1046.1                      | 2514.0                      | 3560.2                      | 2134.4                 | -23.1                    | 2111.3                         |
|            |                   | -18.50 | 903.9                       | 2639.9                      | 3543.8                      | 2124.6                 | -23.1                    | 2101.5                         |
|            |                   | -19.00 | 680.4                       | 2714.9                      | 3395.3                      | 2035.6                 | -23.1                    | 2012.5                         |
|            |                   | -19.50 | 529.9                       | 2794.7                      | 3324.6                      | 1993.2                 | -23.1                    | 1970.1                         |
|            |                   | -20.00 | 438.1                       | 2892.0                      | 3330.1                      | 1996.4                 | -23.1                    | 1973.4                         |
|            |                   | -20.50 | 310.4                       | 3032.1                      | 3342.5                      | 2003.9                 | -23.1                    | 1980.8                         |
|            |                   | -21.00 | 243.3                       | 3175.4                      | 3418.7                      | 2049.6                 | -23.1                    | 2026.5                         |
| -21.50     | 220.6             | 3234.8 | 3455.4                      | 2071.6                      | -23.1                       | 2048.6                 |                          |                                |
| -22.00     | 223.6             | 3253.5 | 3477.0                      | 2084.6                      | -23.1                       | 2061.5                 |                          |                                |
| -22.50     | 261.7             | 3278.1 | 3539.8                      | 2122.2                      | -23.1                       | 2099.1                 |                          |                                |
| -23.00     | 326.4             | 3317.5 | 3643.9                      | 2184.6                      | -23.1                       | 2161.5                 |                          |                                |
| -23.50     | 432.2             | 3369.1 | 3801.3                      | 2278.9                      | -23.1                       | 2255.9                 |                          |                                |
| -24.00     | 444.7             | 3438.9 | 3883.6                      | 2328.3                      | -23.1                       | 2305.3                 |                          |                                |
| -24.50     | 461.6             | 3502.5 | 3964.1                      | 2376.5                      | -23.1                       | 2353.5                 |                          |                                |
| -25.00     | 698.0             | 3560.2 | 4258.2                      | 2552.9                      | -23.1                       | 2529.8                 |                          |                                |
| 19-1008-22 | 0.18              | -6.00  | 983.7                       | 300.2                       | 1284.0                      | 769.8                  | -24.1                    | 745.7                          |
|            |                   | -6.50  | 1320.1                      | 379.2                       | 1699.4                      | 1018.8                 | -24.1                    | 994.7                          |
|            |                   | -7.00  | 1405.3                      | 478.7                       | 1884.1                      | 1129.5                 | -24.1                    | 1105.4                         |
|            |                   | -7.50  | 1499.0                      | 578.9                       | 2078.0                      | 1245.8                 | -24.1                    | 1221.7                         |
|            |                   | -8.00  | 1589.4                      | 679.0                       | 2268.4                      | 1360.0                 | -24.1                    | 1335.9                         |
|            |                   | -8.50  | 1676.0                      | 778.8                       | 2454.8                      | 1471.7                 | -24.1                    | 1447.6                         |
|            |                   | -9.00  | 1878.4                      | 877.7                       | 2756.1                      | 1652.3                 | -24.1                    | 1628.3                         |
|            |                   | -9.50  | 1387.1                      | 981.7                       | 2368.8                      | 1420.1                 | -24.1                    | 1396.0                         |
|            |                   | -10.00 | 1316.5                      | 1086.0                      | 2402.5                      | 1440.4                 | -24.1                    | 1416.3                         |
|            |                   | -10.50 | 1265.3                      | 1190.4                      | 2455.6                      | 1472.2                 | -24.1                    | 1448.1                         |
|            |                   | -11.00 | 1221.7                      | 1294.3                      | 2516.0                      | 1508.4                 | -24.1                    | 1484.3                         |
|            |                   | -11.50 | 1127.4                      | 1398.0                      | 2525.4                      | 1514.0                 | -24.1                    | 1490.0                         |
|            |                   | -12.00 | 1096.0                      | 1461.8                      | 2557.8                      | 1533.4                 | -24.1                    | 1509.4                         |
|            |                   | -12.50 | 850.6                       | 1518.7                      | 2369.3                      | 1420.4                 | -24.1                    | 1396.3                         |
|            |                   | -13.00 | 843.5                       | 1579.8                      | 2423.3                      | 1452.8                 | -24.1                    | 1428.8                         |
|            |                   | -13.50 | 817.5                       | 1651.9                      | 2469.4                      | 1480.5                 | -24.1                    | 1456.4                         |
|            |                   | -14.00 | 618.9                       | 1714.0                      | 2332.9                      | 1398.6                 | -24.1                    | 1374.6                         |
|            |                   | -14.50 | 477.7                       | 1768.2                      | 2245.9                      | 1346.5                 | -24.1                    | 1322.4                         |
|            |                   | -15.00 | 406.9                       | 1806.5                      | 2213.4                      | 1327.0                 | -24.1                    | 1302.9                         |
|            |                   | -15.50 | 360.1                       | 1868.7                      | 2228.8                      | 1336.2                 | -24.1                    | 1312.1                         |
|            |                   | -16.00 | 324.8                       | 1918.9                      | 2243.7                      | 1345.1                 | -24.1                    | 1321.1                         |
|            |                   | -16.50 | 309.1                       | 1948.0                      | 2257.2                      | 1353.2                 | -24.1                    | 1329.1                         |
|            |                   | -17.00 | 289.3                       | 1970.9                      | 2260.2                      | 1355.1                 | -24.1                    | 1331.0                         |
|            |                   | -17.50 | 382.9                       | 1985.9                      | 2368.8                      | 1420.1                 | -24.1                    | 1396.1                         |
|            |                   | -18.00 | 802.7                       | 2011.3                      | 2814.1                      | 1687.1                 | -24.1                    | 1663.0                         |
| -18.50     | 814.0             | 2085.0 | 2899.0                      | 1738.0                      | -24.1                       | 1713.9                 |                          |                                |
| -19.00     | 855.1             | 2156.1 | 3011.2                      | 1805.3                      | -24.1                       | 1781.2                 |                          |                                |
| -19.50     | 919.3             | 2217.7 | 3137.0                      | 1880.7                      | -24.1                       | 1856.6                 |                          |                                |
| -20.00     | 994.6             | 2286.9 | 3281.5                      | 1967.3                      | -24.1                       | 1943.3                 |                          |                                |
| -20.50     | 920.3             | 2381.5 | 3301.8                      | 1979.5                      | -24.1                       | 1955.4                 |                          |                                |
| -21.00     | 1097.2            | 2446.7 | 3543.9                      | 2124.6                      | -24.1                       | 2100.6                 |                          |                                |
| -21.50     | 1133.7            | 2535.1 | 3668.8                      | 2199.5                      | -24.1                       | 2175.4                 |                          |                                |
| -22.00     | 1093.7            | 2633.7 | 3727.4                      | 2234.7                      | -24.1                       | 2210.6                 |                          |                                |
| -22.50     | 1173.8            | 2702.0 | 3875.8                      | 2323.6                      | -24.1                       | 2299.6                 |                          |                                |
| -23.00     | 1322.3            | 2771.4 | 4093.6                      | 2454.2                      | -24.1                       | 2430.1                 |                          |                                |
| -23.50     | 1350.5            | 2851.8 | 4202.2                      | 2519.3                      | -24.1                       | 2495.3                 |                          |                                |
| -24.00     | 1482.5            | 2931.3 | 4413.9                      | 2646.2                      | -24.1                       | 2622.1                 |                          |                                |
| -24.50     | 1583.2            | 3019.2 | 4602.4                      | 2759.2                      | -24.1                       | 2735.1                 |                          |                                |
| -25.00     | 1777.7            | 3112.8 | 4890.5                      | 2932.0                      | -24.1                       | 2907.9                 |                          |                                |
| 202.S03    | 0.03              | -6.00  | 716.2                       | 82.9                        | 799.2                       | 479.1                  | -67.7                    | 411.4                          |
|            |                   | -6.50  | 983.8                       | 151.0                       | 1134.8                      | 680.3                  | -67.7                    | 612.6                          |
|            |                   | -7.00  | 1085.5                      | 240.5                       | 1326.0                      | 795.0                  | -67.7                    | 727.2                          |
|            |                   | -7.50  | 1593.1                      | 331.6                       | 1924.7                      | 1153.9                 | -67.7                    | 1086.1                         |
|            |                   | -8.00  | 1617.2                      | 431.7                       | 2048.9                      | 1228.4                 | -67.7                    | 1160.6                         |
|            |                   | -8.50  | 1658.3                      | 530.7                       | 2189.0                      | 1312.4                 | -67.7                    | 1244.6                         |
|            |                   | -9.00  | 1990.2                      | 646.5                       | 2636.7                      | 1580.8                 | -67.7                    | 1513.1                         |
|            |                   | -9.50  | 2008.8                      | 771.7                       | 2780.5                      | 1667.0                 | -67.7                    | 1599.2                         |
|            |                   | -10.00 | 1095.6                      | 896.8                       | 1992.4                      | 1194.5                 | -67.7                    | 1126.7                         |
|            |                   | -10.50 | 900.8                       | 1021.9                      | 1922.7                      | 1152.7                 | -67.7                    | 1085.0                         |
|            |                   | -11.00 | 762.5                       | 1137.1                      | 1899.6                      | 1138.8                 | -67.7                    | 1071.1                         |
|            |                   | -11.50 | 646.4                       | 1237.2                      | 1883.5                      | 1129.2                 | -67.7                    | 1061.5                         |
|            |                   | -12.00 | 360.0                       | 1348.1                      | 1708.1                      | 1024.0                 | -67.7                    | 956.3                          |
|            |                   | -12.50 | 375.1                       | 1387.9                      | 1763.0                      | 1056.9                 | -67.7                    | 989.2                          |
|            |                   | -13.00 | 376.7                       | 1427.8                      | 1804.6                      | 1081.9                 | -67.7                    | 1014.1                         |
|            |                   | -13.50 | 612.0                       | 1457.2                      | 2069.2                      | 1240.5                 | -67.7                    | 1172.8                         |
| -14.00     | 677.7             | 1514.9 | 2192.6                      | 1314.5                      | -67.7                       | 1246.8                 |                          |                                |
| -14.50     | 725.2             | 1566.6 | 2291.8                      | 1374.0                      | -67.7                       | 1306.3                 |                          |                                |
| -15.00     | 744.8             | 1628.5 | 2373.3                      | 1422.8                      | -67.7                       | 1355.1                 |                          |                                |
| -15.50     | 771.0             | 1683.2 | 2454.2                      | 1471.3                      | -67.7                       | 1403.6                 |                          |                                |
| -16.00     | 788.6             | 1736.2 | 2524.8                      | 1513.7                      | -67.7                       | 1445.9                 |                          |                                |
| -16.50     | 892.4             | 1783.4 | 2675.8                      | 1604.2                      | -67.7                       | 1536.5                 |                          |                                |



Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen        |                             |                             | Rekenwaarden             |                           |                                |
|-----------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|--------------------------|---------------------------|--------------------------------|
|           |                    |                    | R <sub>o,real</sub><br>[kN] | R <sub>r,real</sub><br>[kN] | R <sub>c,real</sub><br>[kN] | R <sub>o,d</sub><br>[kN] | F <sub>nk,d</sub><br>[kN] | R <sub>o,netto,d</sub><br>[kN] |
| 202.S03   | 0.03               | -17.00             | 972.3                       | 1836.8                      | 2809.0                      | 1684.1                   | -67.7                     | 1616.4                         |
|           |                    | -17.50             | 1118.3                      | 1894.6                      | 3012.9                      | 1806.3                   | -67.7                     | 1738.6                         |
|           |                    | -18.00             | 1164.7                      | 1964.3                      | 3129.0                      | 1875.9                   | -67.7                     | 1808.2                         |
|           |                    | -18.50             | 1085.6                      | 2030.8                      | 3116.3                      | 1868.3                   | -67.7                     | 1800.6                         |
|           |                    | -19.00             | 1082.8                      | 2108.0                      | 3190.8                      | 1912.9                   | -67.7                     | 1845.2                         |
|           |                    | -19.50             | 1079.0                      | 2185.0                      | 3264.0                      | 1956.8                   | -67.7                     | 1889.1                         |
|           |                    | -20.00             | 1038.3                      | 2265.7                      | 3304.1                      | 1980.9                   | -67.7                     | 1913.1                         |
|           |                    | -20.50             | 1004.6                      | 2331.5                      | 3336.1                      | 2000.0                   | -67.7                     | 1932.3                         |
|           |                    | -21.00             | 1098.0                      | 2382.7                      | 3480.8                      | 2086.8                   | -67.7                     | 2019.1                         |
|           |                    | -21.50             | 1411.0                      | 2442.1                      | 3853.0                      | 2310.0                   | -67.7                     | 2242.2                         |
|           |                    | -22.00             | 1648.6                      | 2532.2                      | 4180.9                      | 2506.5                   | -67.7                     | 2438.8                         |
|           |                    | -22.50             | 2034.1                      | 2636.4                      | 4670.6                      | 2800.1                   | -67.7                     | 2732.4                         |
|           |                    | -23.00             | 2140.2                      | 2752.8                      | 4893.0                      | 2933.4                   | -67.7                     | 2865.7                         |
|           |                    | -23.50             | 2776.6                      | 2869.4                      | 5645.9                      | 3384.8                   | -67.7                     | 3317.1                         |
|           |                    | -24.00             | 2313.4                      | 2991.4                      | 5304.8                      | 3180.3                   | -67.7                     | 3112.6                         |
|           |                    | -24.50             | 2381.1                      | 3116.5                      | 5497.6                      | 3295.9                   | -67.7                     | 3228.2                         |
|           |                    | -25.00             | 2209.4                      | 3241.6                      | 5451.0                      | 3268.0                   | -67.7                     | 3200.3                         |

**REKENGEGEVENS SI Ø610/850 druk**

Berekening : Ontwerpend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(gem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{\epsilon,nk}$  : 1.0  
 R<sub>o,real,max,1</sub> begrenzen op 0.75 \* R<sub>o,real,max,1</sub> : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø610/850  
 Niveau paalkop [m] : N.A.P. 0.00  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS SI Ø610/850**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau<br>[m] | Eindniveau<br>[m] | Stapgrootte<br>[m] |
|----|--------------------|-------------------|--------------------|
| 1  | -7.00              | -25.00            | 0.50               |

**RESULTATEN SI Ø610/850 druk (n=1)**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering     | 19-1008-14                   | 19-1008-15                   | 251.S01                      | 19-1008-22                   | 202.S03                      |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| Niveau<br>[m] | F <sub>netto,d</sub><br>[kN] | F <sub>netto,d</sub><br>[kN] | F <sub>netto,d</sub><br>[kN] | F <sub>netto,d</sub><br>[kN] | F <sub>netto,d</sub><br>[kN] |
| -7.00         | 2234                         | 2030                         | 752                          | 1553                         | 1092                         |
| -7.50         | 2368                         | 2154                         | 728                          | 1700                         | 1582                         |
| -8.00         | 2527                         | 2275                         | 720                          | 1844                         | 1663                         |
| -8.50         | 2678                         | 2639                         | 710                          | 1981                         | 1821                         |
| -9.00         | 2819                         | 2981                         | 1111                         | 1761                         | 2149                         |
| -9.50         | 2962                         | 3136                         | 1242                         | 1827                         | 1526                         |
| -10.00        | 3510                         | 3406                         | 1319                         | 1905                         | 1453                         |
| -10.50        | 2551                         | 3366                         | 1371                         | 1992                         | 1398                         |
| -11.00        | 2269                         | 3480                         | 1402                         | 2027                         | 1447                         |
| -11.50        | 2199                         | 3588                         | 1476                         | 1958                         | 1408                         |
| -12.00        | 2193                         | 3731                         | 1758                         | 1836                         | 1255                         |
| -12.50        | 2202                         | 3768                         | 1615                         | 1875                         | 1290                         |
| -13.00        | 2128                         | 3828                         | 1702                         | 1916                         | 1371                         |
| -13.50        | 2136                         | 2954                         | 1783                         | 1770                         | 1556                         |
| -14.00        | 2219                         | 2840                         | 1832                         | 1672                         | 1666                         |
| -14.50        | 2282                         | 2756                         | 1828                         | 1651                         | 1732                         |
| -15.00        | 2338                         | 2704                         | 1791                         | 1673                         | 1790                         |
| -15.50        | 2317                         | 2565                         | 2678                         | 1687                         | 1849                         |
| -16.00        | 2543                         | 2526                         | 2508                         | 1692                         | 1901                         |
| -16.50        | 2591                         | 2555                         | 2569                         | 1699                         | 2023                         |
| -17.00        | 2735                         | 2543                         | 2686                         | 1697                         | 2141                         |
| -17.50        | 2812                         | 2553                         | 2755                         | 1816                         | 2299                         |
| -18.00        | 2884                         | 2550                         | 2764                         | 2173                         | 2302                         |
| -18.50        | 2954                         | 2561                         | 2464                         | 2255                         | 2374                         |
| -19.00        | 3185                         | 2570                         | 2508                         | 2340                         | 2451                         |
| -19.50        | 3300                         | 2589                         | 2483                         | 2438                         | 2515                         |
| -20.00        | 3523                         | 2651                         | 2478                         | 2552                         | 2545                         |
| -20.50        | 3651                         | 2880                         | 2505                         | 2581                         | 2564                         |
| -21.00        | 3768                         | 3036                         | 2550                         | 2752                         | 2694                         |
| -21.50        | 3955                         | 3104                         | 2573                         | 2843                         | 3047                         |
| -22.00        | 4095                         | 3236                         | 2589                         | 2882                         | 3301                         |
| -22.50        | 4227                         | 3441                         | 2676                         | 3010                         | 3718                         |
| -23.00        | 4333                         | 3484                         | 2725                         | 3195                         | 3919                         |
| -23.50        | 4201                         | 3579                         | 2864                         | 3301                         | 4189                         |
| -24.00        | 4292                         | 3633                         | 2924                         | 3496                         | 4317                         |
| -24.50        | 4382                         | 3709                         | 3002                         | 3636                         | 4437                         |
| -25.00        | 4465                         | 3753                         | 3240                         | 3875                         | 4320                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SAMENVATTINGSTABEL SI Ø610/850 druk (n=1)**

**Uitgangspunten**

- paal : SI Ø610/850  
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie  
 - schachtafmeting : 730 mm  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            |                    |                    | $R_{e,real}$<br>[kN] | $R_{b,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{e;d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40               | -7.00              | 2755.7               | 994.9                | 3750.6               | 2248.6            | -14.7              | 2233.8                  |
|            |                    | -7.50              | 2842.7               | 1132.3               | 3975.0               | 2383.1            | -14.7              | 2368.4                  |
|            |                    | -8.00              | 2965.5               | 1273.9               | 4239.4               | 2541.6            | -14.7              | 2526.9                  |
|            |                    | -8.50              | 3063.1               | 1428.7               | 4491.8               | 2692.9            | -14.7              | 2678.2                  |
|            |                    | -9.00              | 3142.8               | 1583.5               | 4726.4               | 2833.6            | -14.7              | 2818.8                  |
|            |                    | -9.50              | 3238.5               | 1726.1               | 4964.6               | 2976.4            | -14.7              | 2961.7                  |
|            |                    | -10.00             | 4015.6               | 1863.1               | 5878.7               | 3524.4            | -14.7              | 3509.7                  |
|            |                    | -10.50             | 2270.4               | 2009.3               | 4279.7               | 2565.7            | -14.7              | 2551.0                  |
|            |                    | -11.00             | 1644.5               | 2164.1               | 3808.6               | 2283.4            | -14.7              | 2268.6                  |
|            |                    | -11.50             | 1373.6               | 2318.9               | 3692.5               | 2213.8            | -14.7              | 2199.0                  |
|            |                    | -12.00             | 1208.5               | 2473.7               | 3682.2               | 2207.6            | -14.7              | 2192.9                  |
|            |                    | -12.50             | 1069.6               | 2628.5               | 3698.1               | 2217.1            | -14.7              | 2202.4                  |
|            |                    | -13.00             | 790.7                | 2782.6               | 3573.3               | 2142.3            | -14.7              | 2127.5                  |
|            |                    | -13.50             | 709.6                | 2878.4               | 3588.0               | 2151.1            | -14.7              | 2136.4                  |
|            |                    | -14.00             | 789.3                | 2936.9               | 3726.1               | 2233.9            | -14.7              | 2219.2                  |
|            |                    | -14.50             | 845.3                | 2986.0               | 3831.3               | 2296.9            | -14.7              | 2282.2                  |
|            |                    | -15.00             | 865.3                | 3059.6               | 3924.9               | 2353.0            | -14.7              | 2338.3                  |
|            |                    | -15.50             | 723.5                | 3165.8               | 3889.3               | 2331.7            | -14.7              | 2317.0                  |
|            |                    | -16.00             | 1058.4               | 3208.5               | 4266.9               | 2558.1            | -14.7              | 2543.4                  |
|            |                    | -16.50             | 1058.0               | 3288.2               | 4346.2               | 2605.6            | -14.7              | 2590.9                  |
|            |                    | -17.00             | 1231.8               | 3355.5               | 4587.3               | 2750.2            | -14.7              | 2735.5                  |
|            |                    | -17.50             | 1278.5               | 3436.8               | 4715.3               | 2826.9            | -14.7              | 2812.2                  |
|            |                    | -18.00             | 1314.3               | 3521.2               | 4835.5               | 2899.0            | -14.7              | 2884.3                  |
|            |                    | -18.50             | 1351.2               | 3601.4               | 4952.6               | 2969.2            | -14.7              | 2954.5                  |
|            |                    | -19.00             | 1658.3               | 3679.4               | 5337.7               | 3200.1            | -14.7              | 3185.3                  |
| -19.50     | 1756.6             | 3772.3             | 5528.8               | 3314.6               | -14.7                | 3299.9            |                    |                         |
| -20.00     | 2037.0             | 3864.2             | 5901.3               | 3537.9               | -14.7                | 3523.2            |                    |                         |
| -20.50     | 2142.1             | 3972.5             | 6114.6               | 3665.8               | -14.7                | 3651.1            |                    |                         |
| -21.00     | 2222.4             | 4087.0             | 6309.5               | 3782.6               | -14.7                | 3767.9            |                    |                         |
| -21.50     | 2423.7             | 4197.4             | 6621.1               | 3969.5               | -14.7                | 3954.8            |                    |                         |
| -22.00     | 2542.2             | 4312.9             | 6855.0               | 4109.7               | -14.7                | 4095.0            |                    |                         |
| -22.50     | 2643.3             | 4432.2             | 7075.5               | 4241.9               | -14.7                | 4227.2            |                    |                         |
| -23.00     | 2696.7             | 4555.1             | 7251.8               | 4347.6               | -14.7                | 4332.9            |                    |                         |
| -23.50     | 2355.2             | 4677.3             | 7032.5               | 4216.1               | -14.7                | 4201.4            |                    |                         |
| -24.00     | 2383.0             | 4801.1             | 7184.1               | 4307.0               | -14.7                | 4292.3            |                    |                         |
| -24.50     | 2408.2             | 4924.9             | 7333.1               | 4396.3               | -14.7                | 4381.6            |                    |                         |
| -25.00     | 2419.5             | 5053.5             | 7473.0               | 4480.2               | -14.7                | 4465.5            |                    |                         |
| 19-1008-15 | 0.75               | -7.00              | 2194.2               | 1200.1               | 3394.3               | 2035.0            | -5.3               | 2029.6                  |
|            |                    | -7.50              | 2278.7               | 1322.5               | 3601.3               | 2159.0            | -5.3               | 2153.7                  |
|            |                    | -8.00              | 2357.2               | 1446.4               | 3803.5               | 2280.3            | -5.3               | 2275.0                  |
|            |                    | -8.50              | 2835.3               | 1575.7               | 4411.0               | 2644.5            | -5.3               | 2639.2                  |
|            |                    | -9.00              | 3250.7               | 1730.5               | 4981.3               | 2986.4            | -5.3               | 2981.0                  |
|            |                    | -9.50              | 3354.2               | 1885.3               | 5239.5               | 3141.2            | -5.3               | 3135.9                  |
|            |                    | -10.00             | 3649.8               | 2040.1               | 5689.9               | 3411.2            | -5.3               | 3405.9                  |
|            |                    | -10.50             | 3428.9               | 2194.9               | 5623.8               | 3371.6            | -5.3               | 3366.3                  |
|            |                    | -11.00             | 3464.3               | 2349.7               | 5814.1               | 3485.6            | -5.3               | 3480.3                  |
|            |                    | -11.50             | 3489.8               | 2504.5               | 5994.3               | 3593.7            | -5.3               | 3588.4                  |
|            |                    | -12.00             | 3572.5               | 2659.3               | 6231.8               | 3736.1            | -5.3               | 3730.8                  |
|            |                    | -12.50             | 3480.2               | 2814.1               | 6294.3               | 3773.6            | -5.3               | 3768.2                  |
|            |                    | -13.00             | 3427.8               | 2966.4               | 6394.1               | 3833.4            | -5.3               | 3828.1                  |
|            |                    | -13.50             | 1834.3               | 3101.4               | 4935.7               | 2959.1            | -5.3               | 2953.7                  |
|            |                    | -14.00             | 1489.3               | 3256.2               | 4745.5               | 2845.0            | -5.3               | 2839.7                  |
|            |                    | -14.50             | 1194.2               | 3411.0               | 4605.3               | 2761.0            | -5.3               | 2755.6                  |
|            |                    | -15.00             | 953.9                | 3565.8               | 4519.7               | 2709.7            | -5.3               | 2704.3                  |
|            |                    | -15.50             | 567.1                | 3720.6               | 4287.8               | 2570.6            | -5.3               | 2565.3                  |
|            |                    | -16.00             | 348.8                | 3874.2               | 4223.0               | 2531.8            | -5.3               | 2526.4                  |
|            |                    | -16.50             | 358.9                | 3911.5               | 4270.4               | 2560.2            | -5.3               | 2554.9                  |
|            |                    | -17.00             | 322.3                | 3928.3               | 4250.6               | 2548.3            | -5.3               | 2543.0                  |
|            |                    | -17.50             | 313.0                | 3953.9               | 4266.8               | 2558.1            | -5.3               | 2552.7                  |
|            |                    | -18.00             | 265.5                | 3997.3               | 4262.8               | 2555.6            | -5.3               | 2550.3                  |
|            |                    | -18.50             | 271.3                | 4008.7               | 4280.0               | 2565.9            | -5.3               | 2560.6                  |
|            |                    | -19.00             | 275.1                | 4020.8               | 4295.9               | 2575.5            | -5.3               | 2570.2                  |
| -19.50     | 291.8              | 4035.2             | 4327.0               | 2594.1               | -5.3                 | 2588.8            |                    |                         |
| -20.00     | 380.4              | 4050.2             | 4430.6               | 2656.2               | -5.3                 | 2650.9            |                    |                         |
| -20.50     | 743.2              | 4070.3             | 4813.5               | 2885.8               | -5.3                 | 2880.4            |                    |                         |
| -21.00     | 955.0              | 4117.5             | 5072.5               | 3041.1               | -5.3                 | 3035.8            |                    |                         |
| -21.50     | 1002.4             | 4184.0             | 5186.3               | 3109.3               | -5.3                 | 3104.0            |                    |                         |
| -22.00     | 1155.3             | 4250.5             | 5405.8               | 3240.9               | -5.3                 | 3235.6            |                    |                         |
| -22.50     | 1429.0             | 4319.7             | 5748.7               | 3446.5               | -5.3                 | 3441.1            |                    |                         |
| -23.00     | 1415.5             | 4404.9             | 5820.5               | 3489.5               | -5.3                 | 3484.2            |                    |                         |
| -23.50     | 1472.4             | 4506.5             | 5978.9               | 3584.4               | -5.3                 | 3579.1            |                    |                         |
| -24.00     | 1471.3             | 4597.3             | 6068.5               | 3638.2               | -5.3                 | 3632.9            |                    |                         |
| -24.50     | 1483.6             | 4712.7             | 6196.3               | 3714.8               | -5.3                 | 3709.5            |                    |                         |
| -25.00     | 1439.3             | 4829.5             | 6268.8               | 3758.3               | -5.3                 | 3752.9            |                    |                         |
| 251.S01    | -1.05              | -7.00              | 575.9                | 725.4                | 1301.2               | 780.1             | -28.5              | 751.6                   |
|            |                    | -7.50              | 417.2                | 845.1                | 1262.3               | 756.8             | -28.5              | 728.3                   |
|            |                    | -8.00              | 293.6                | 955.2                | 1248.9               | 748.7             | -28.5              | 720.2                   |
|            |                    | -8.50              | 202.4                | 1029.3               | 1231.7               | 738.5             | -28.5              | 709.9                   |
|            |                    | -9.00              | 859.6                | 1040.4               | 1900.0               | 1139.1            | -28.5              | 1110.6                  |
|            |                    | -9.50              | 1011.0               | 1108.9               | 2119.8               | 1270.9            | -28.5              | 1242.4                  |
|            |                    | -10.00             | 1035.2               | 1212.6               | 2247.9               | 1347.6            | -28.5              | 1319.1                  |
| -10.50     | 1000.1             | 1334.6             | 2334.7               | 1399.7               | -28.5                | 1371.1            |                    |                         |
| -11.00     | 958.4              | 1427.2             | 2385.7               | 1430.3               | -28.5                | 1401.7            |                    |                         |
| -11.50     | 1026.3             | 1483.6             | 2509.9               | 1504.7               | -28.5                | 1476.2            |                    |                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld paalpunt |        | Beziwkdraagvermogen         |                             |                             | Rekenwaarden           |                          |                                |
|------------|-------------------|--------|-----------------------------|-----------------------------|-----------------------------|------------------------|--------------------------|--------------------------------|
|            | niveau            | niveau | R <sub>b,real</sub><br>[kN] | R <sub>s,real</sub><br>[kN] | R <sub>c,real</sub><br>[kN] | R <sub>d</sub><br>[kN] | F <sub>hkd</sub><br>[kN] | R <sub>z,netto;d</sub><br>[kN] |
| 251.S01    | -1.05             | -12.00 | 1440.9                      | 1539.4                      | 2980.4                      | 1786.8                 | -28.5                    | 1758.3                         |
|            |                   | -12.50 | 1107.2                      | 1634.5                      | 2741.7                      | 1643.7                 | -28.5                    | 1615.2                         |
|            |                   | -13.00 | 1139.0                      | 1746.9                      | 2886.0                      | 1730.2                 | -28.5                    | 1701.7                         |
|            |                   | -13.50 | 1168.1                      | 1852.8                      | 3020.9                      | 1811.1                 | -28.5                    | 1782.6                         |
|            |                   | -14.00 | 1103.3                      | 2000.1                      | 3103.4                      | 1860.5                 | -28.5                    | 1832.0                         |
|            |                   | -14.50 | 950.3                       | 2146.4                      | 3096.7                      | 1856.5                 | -28.5                    | 1828.0                         |
|            |                   | -15.00 | 729.8                       | 2304.8                      | 3034.6                      | 1819.3                 | -28.5                    | 1790.8                         |
|            |                   | -15.50 | 2139.0                      | 2375.7                      | 4514.7                      | 2706.7                 | -28.5                    | 2678.2                         |
|            |                   | -16.00 | 1712.0                      | 2518.6                      | 4230.6                      | 2536.4                 | -28.5                    | 2507.8                         |
|            |                   | -16.50 | 1659.7                      | 2673.4                      | 4333.1                      | 2597.8                 | -28.5                    | 2569.3                         |
|            |                   | -17.00 | 1701.0                      | 2826.5                      | 4527.5                      | 2714.3                 | -28.5                    | 2685.8                         |
|            |                   | -17.50 | 1669.8                      | 2972.6                      | 4642.4                      | 2783.2                 | -28.5                    | 2754.7                         |
|            |                   | -18.00 | 1546.6                      | 3110.6                      | 4657.2                      | 2792.1                 | -28.5                    | 2763.5                         |
|            |                   | -18.50 | 891.3                       | 3266.3                      | 4157.6                      | 2492.6                 | -28.5                    | 2464.0                         |
|            |                   | -19.00 | 871.2                       | 3359.2                      | 4230.3                      | 2536.2                 | -28.5                    | 2507.6                         |
|            |                   | -19.50 | 731.1                       | 3457.9                      | 4188.9                      | 2511.3                 | -28.5                    | 2482.8                         |
|            |                   | -20.00 | 602.8                       | 3578.2                      | 4181.0                      | 2506.6                 | -28.5                    | 2478.1                         |
|            |                   | -20.50 | 475.2                       | 3751.6                      | 4226.8                      | 2534.0                 | -28.5                    | 2505.5                         |
|            |                   | -21.00 | 372.5                       | 3928.9                      | 4301.3                      | 2578.7                 | -28.5                    | 2550.2                         |
|            |                   | -21.50 | 337.7                       | 4002.4                      | 4340.1                      | 2602.0                 | -28.5                    | 2573.5                         |
|            |                   | -22.00 | 341.2                       | 4025.5                      | 4366.7                      | 2617.9                 | -28.5                    | 2589.4                         |
|            |                   | -22.50 | 455.0                       | 4055.9                      | 4510.9                      | 2704.4                 | -28.5                    | 2675.8                         |
|            |                   | -23.00 | 488.4                       | 4104.7                      | 4593.1                      | 2753.6                 | -28.5                    | 2725.1                         |
|            |                   | -23.50 | 656.8                       | 4168.5                      | 4825.3                      | 2892.9                 | -28.5                    | 2864.4                         |
|            |                   | -24.00 | 669.6                       | 4254.9                      | 4924.6                      | 2952.4                 | -28.5                    | 2923.8                         |
| -24.50     | 721.5             | 4333.6 | 5055.0                      | 3030.6                      | -28.5                       | 3002.1                 |                          |                                |
| -25.00     | 1047.3            | 4405.0 | 5452.3                      | 3268.8                      | -28.5                       | 3240.2                 |                          |                                |
| 19-1008-22 | 0.18              | -7.00  | 2047.7                      | 592.3                       | 2640.0                      | 1582.8                 | -29.8                    | 1553.0                         |
|            |                   | -7.50  | 2169.1                      | 716.3                       | 2885.5                      | 1729.9                 | -29.8                    | 1700.1                         |
|            |                   | -8.00  | 2286.1                      | 840.1                       | 3126.3                      | 1874.3                 | -29.8                    | 1844.5                         |
|            |                   | -8.50  | 2390.4                      | 963.6                       | 3354.1                      | 2010.8                 | -29.8                    | 1981.0                         |
|            |                   | -9.00  | 1901.3                      | 1085.9                      | 2987.2                      | 1790.9                 | -29.8                    | 1761.1                         |
|            |                   | -9.50  | 1883.1                      | 1214.7                      | 3097.7                      | 1857.2                 | -29.8                    | 1827.4                         |
|            |                   | -10.00 | 1883.0                      | 1343.7                      | 3226.7                      | 1934.5                 | -29.8                    | 1904.7                         |
|            |                   | -10.50 | 1899.7                      | 1472.8                      | 3372.5                      | 2021.9                 | -29.8                    | 1992.1                         |
|            |                   | -11.00 | 1829.6                      | 1601.4                      | 3431.0                      | 2057.0                 | -29.8                    | 2027.2                         |
|            |                   | -11.50 | 1586.6                      | 1729.8                      | 3316.4                      | 1988.2                 | -29.8                    | 1958.4                         |
|            |                   | -12.00 | 1303.8                      | 1808.7                      | 3112.4                      | 1866.0                 | -29.8                    | 1836.2                         |
|            |                   | -12.50 | 1297.6                      | 1879.1                      | 3176.7                      | 1904.5                 | -29.8                    | 1874.7                         |
|            |                   | -13.00 | 1291.3                      | 1954.7                      | 3246.0                      | 1946.1                 | -29.8                    | 1916.3                         |
|            |                   | -13.50 | 957.5                       | 2043.9                      | 3001.4                      | 1799.4                 | -29.8                    | 1769.6                         |
|            |                   | -14.00 | 717.7                       | 2120.7                      | 2838.4                      | 1701.7                 | -29.8                    | 1671.9                         |
|            |                   | -14.50 | 615.0                       | 2187.8                      | 2802.8                      | 1680.3                 | -29.8                    | 1650.5                         |
|            |                   | -15.00 | 604.3                       | 2235.2                      | 2839.5                      | 1702.4                 | -29.8                    | 1672.6                         |
|            |                   | -15.50 | 551.2                       | 2312.1                      | 2863.3                      | 1716.6                 | -29.8                    | 1686.8                         |
|            |                   | -16.00 | 497.3                       | 2374.2                      | 2871.5                      | 1721.5                 | -29.8                    | 1691.7                         |
|            |                   | -16.50 | 473.2                       | 2410.3                      | 2883.5                      | 1728.7                 | -29.8                    | 1698.9                         |
|            |                   | -17.00 | 442.2                       | 2438.6                      | 2880.8                      | 1727.1                 | -29.8                    | 1697.3                         |
|            |                   | -17.50 | 621.7                       | 2457.2                      | 3078.8                      | 1845.8                 | -29.8                    | 1816.0                         |
|            |                   | -18.00 | 1186.2                      | 2488.6                      | 3674.8                      | 2203.1                 | -29.8                    | 2173.3                         |
|            |                   | -18.50 | 1232.0                      | 2579.8                      | 3811.8                      | 2285.3                 | -29.8                    | 2255.5                         |
|            |                   | -19.00 | 1284.4                      | 2667.7                      | 3952.1                      | 2369.4                 | -29.8                    | 2339.6                         |
| -19.50     | 1372.1            | 2743.9 | 4116.1                      | 2467.7                      | -29.8                       | 2437.9                 |                          |                                |
| -20.00     | 1476.9            | 2829.6 | 4306.5                      | 2581.8                      | -29.8                       | 2552.0                 |                          |                                |
| -20.50     | 1408.5            | 2946.6 | 4355.2                      | 2611.0                      | -29.8                       | 2581.2                 |                          |                                |
| -21.00     | 1612.9            | 3027.3 | 4640.2                      | 2781.9                      | -29.8                       | 2752.1                 |                          |                                |
| -21.50     | 1654.9            | 3136.7 | 4791.6                      | 2872.6                      | -29.8                       | 2842.8                 |                          |                                |
| -22.00     | 1598.2            | 3258.7 | 4856.9                      | 2911.8                      | -29.8                       | 2882.0                 |                          |                                |
| -22.50     | 1726.4            | 3343.2 | 5069.6                      | 3039.3                      | -29.8                       | 3009.5                 |                          |                                |
| -23.00     | 1950.4            | 3429.0 | 5379.4                      | 3225.1                      | -29.8                       | 3195.3                 |                          |                                |
| -23.50     | 2027.5            | 3528.5 | 5556.0                      | 3330.9                      | -29.8                       | 3301.1                 |                          |                                |
| -24.00     | 2254.5            | 3626.9 | 5881.4                      | 3526.0                      | -29.8                       | 3496.2                 |                          |                                |
| -24.50     | 2379.1            | 3735.7 | 6114.8                      | 3665.9                      | -29.8                       | 3636.1                 |                          |                                |
| -25.00     | 2662.6            | 3851.4 | 6514.0                      | 3905.3                      | -29.8                       | 3875.5                 |                          |                                |
| 202.S03    | 0.03              | -7.00  | 1664.5                      | 297.5                       | 1962.0                      | 1176.3                 | -83.8                    | 1092.5                         |
|            |                   | -7.50  | 2367.7                      | 410.3                       | 2777.9                      | 1665.4                 | -83.8                    | 1581.6                         |
|            |                   | -8.00  | 2379.9                      | 534.1                       | 2914.0                      | 1747.0                 | -83.8                    | 1663.2                         |
|            |                   | -8.50  | 2520.4                      | 656.7                       | 3177.0                      | 1904.7                 | -83.8                    | 1820.9                         |
|            |                   | -9.00  | 2923.9                      | 800.0                       | 3723.8                      | 2232.5                 | -83.8                    | 2148.7                         |
|            |                   | -9.50  | 1731.0                      | 954.8                       | 2685.8                      | 1610.2                 | -83.8                    | 1526.4                         |
|            |                   | -10.00 | 1454.6                      | 1109.6                      | 2564.2                      | 1537.3                 | -83.8                    | 1453.5                         |
|            |                   | -10.50 | 1206.8                      | 1264.4                      | 2471.2                      | 1481.5                 | -83.8                    | 1397.7                         |
|            |                   | -11.00 | 1146.3                      | 1406.9                      | 2553.2                      | 1530.7                 | -83.8                    | 1446.9                         |
|            |                   | -11.50 | 957.2                       | 1530.7                      | 2487.9                      | 1491.5                 | -83.8                    | 1407.7                         |
|            |                   | -12.00 | 565.3                       | 1668.0                      | 2233.2                      | 1338.9                 | -83.8                    | 1255.1                         |
|            |                   | -12.50 | 574.1                       | 1717.2                      | 2291.3                      | 1373.7                 | -83.8                    | 1289.9                         |
|            |                   | -13.00 | 659.9                       | 1766.6                      | 2426.5                      | 1454.7                 | -83.8                    | 1370.9                         |
|            |                   | -13.50 | 932.7                       | 1803.0                      | 2735.7                      | 1640.1                 | -83.8                    | 1556.3                         |
|            |                   | -14.00 | 1043.6                      | 1874.4                      | 2918.0                      | 1749.4                 | -83.8                    | 1665.6                         |
|            |                   | -14.50 | 1090.8                      | 1938.3                      | 3029.1                      | 1816.0                 | -83.8                    | 1732.2                         |
|            |                   | -15.00 | 1110.9                      | 2014.9                      | 3125.8                      | 1874.0                 | -83.8                    | 1790.2                         |
|            |                   | -15.50 | 1141.2                      | 2082.6                      | 3223.8                      | 1932.7                 | -83.8                    | 1848.9                         |
|            |                   | -16.00 | 1161.8                      | 2148.1                      | 3309.9                      | 1984.4                 | -83.8                    | 1900.6                         |
|            |                   | -16.50 | 1307.2                      | 2206.6                      | 3513.8                      | 2106.6                 | -83.8                    | 2022.8                         |
|            |                   | -17.00 | 1437.6                      | 2272.6                      | 3710.2                      | 2224.3                 | -83.8                    | 2140.5                         |
|            |                   | -17.50 | 1630.8                      | 2344.2                      | 3975.0                      | 2383.1                 | -83.8                    | 2299.3                         |
|            |                   | -18.00 | 1549.9                      | 2430.4                      | 3980.3                      | 2386.3                 | -83.8                    | 2302.5                         |
|            |                   | -18.50 | 1587.6                      | 2512.6                      | 4100.2                      | 2458.2                 | -83.8                    | 2374.4                         |
|            |                   | -19.00 | 1620.5                      | 2608.2                      | 4228.8                      | 2535.2                 | -83.8                    | 2451.4                         |
| -19.50     | 1631.4            | 2703.4 | 4334.9                      | 2598.8                      | -83.8                       | 2515.0                 |                          |                                |
| -20.00     | 1582.1            | 2803.4 | 4385.4                      | 2629.2                      | -83.8                       | 2545.4                 |                          |                                |
| -20.50     | 1531.8            | 2884.7 | 4416.5                      | 2647.8                      | -83.8                       | 2564.0                 |                          |                                |
| -21.00     | 1685.6            | 2948.1 | 4633.7                      | 2778.0                      | -83.8                       | 2694.2                 |                          |                                |
| -21.50     | 2200.3            | 3021.5 | 5221.9                      | 3130.6                      | -83.8                       | 3046.8                 |                          |                                |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaienveld paalpunt |        | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|-----------|---------------------|--------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|           | niveau              | niveau | $R_{b,calc}$<br>[kN] | $R_{s,calc}$<br>[kN] | $R_{c,calc}$<br>[kN] | $R_{s,d}$<br>[kN] | $F_{nk,d}$<br>[kN] | $R_{c,netto,d}$<br>[kN] |
| 202.S03   | 0.03                | -22.00 | 2512.0               | 3133.1               | 5645.1               | 3384.3            | -83.8              | 3300.5                  |
|           |                     | -22.50 | 3078.8               | 3262.0               | 6340.8               | 3801.5            | -83.8              | 3717.7                  |
|           |                     | -23.00 | 3270.0               | 3406.0               | 6676.0               | 4002.4            | -83.8              | 3918.6                  |
|           |                     | -23.50 | 3577.0               | 3550.2               | 7127.2               | 4272.9            | -83.8              | 4189.1                  |
|           |                     | -24.00 | 3639.6               | 3701.2               | 7340.8               | 4401.0            | -83.8              | 4317.2                  |
|           |                     | -24.50 | 3684.2               | 3856.0               | 7540.2               | 4520.5            | -83.8              | 4436.7                  |
|           |                     | -25.00 | 3334.1               | 4010.8               | 7344.9               | 4403.4            | -83.8              | 4319.6                  |

**REKENGEDEGENS SI Ø762/950 druk**

Berekening : Ontwerpend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n-1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(gem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{f,nk}$  : 1.0  
 $R_{b,calc,max,i}$  begrenzen op  $0.75 * R_{b,calc,max,i}$  : NEE  
 UGT draagvermogen zonder negatieve kleef : NEE

Paal : SI Ø762/950  
 Niveau paalkop [m] : N.A.P. 0.00  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS SI Ø762/950**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|-----------------|----------------|-----------------|
| 1  | -8.00           | -25.00         | 0.50            |

**RESULTATEN SI Ø762/950 druk (n=1)**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering  | 19-1008-14         | 19-1008-15         | 251.S01            | 19-1008-22         | 202.S03            |
|------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| Niveau [m] | $F_{netto,d}$ [kN] | $F_{netto,d}$ [kN] | $F_{netto,d}$ [kN] | $F_{netto,d}$ [kN] | $F_{netto,d}$ [kN] |
| -8.00      | 3239               | 2988               | 880                | 2374               | 2206               |
| -8.50      | 3431               | 3463               | 924                | 2110               | 2539               |
| -9.00      | 3594               | 3848               | 1485               | 2197               | 1940               |
| -9.50      | 3761               | 4026               | 1582               | 2285               | 1860               |
| -10.00     | 3067               | 4103               | 1672               | 2394               | 1765               |
| -10.50     | 2825               | 4293               | 1722               | 2462               | 1777               |
| -11.00     | 2732               | 4414               | 1747               | 2410               | 1800               |
| -11.50     | 2736               | 4531               | 1845               | 2265               | 1801               |
| -12.00     | 2758               | 4696               | 1927               | 2321               | 1545               |
| -12.50     | 2574               | 4765               | 2029               | 2380               | 1590               |
| -13.00     | 2606               | 3596               | 2134               | 2163               | 1756               |
| -13.50     | 2593               | 3466               | 2231               | 2017               | 1949               |
| -14.00     | 2714               | 3402               | 2279               | 1990               | 2088               |
| -14.50     | 2795               | 3328               | 2254               | 2016               | 2168               |
| -15.00     | 2864               | 3146               | 2309               | 2049               | 2233               |
| -15.50     | 2888               | 3057               | 3031               | 2057               | 2301               |
| -16.00     | 3128               | 3013               | 3115               | 2056               | 2369               |
| -16.50     | 3198               | 3055               | 3242               | 2061               | 2519               |
| -17.00     | 3366               | 3033               | 3360               | 2056               | 2686               |
| -17.50     | 3456               | 3047               | 3432               | 2253               | 2764               |
| -18.00     | 3540               | 3039               | 2925               | 2708               | 2859               |
| -18.50     | 3620               | 3051               | 2960               | 2805               | 2946               |
| -19.00     | 3925               | 3062               | 2947               | 2905               | 3037               |
| -19.50     | 4073               | 3086               | 2966               | 3026               | 3123               |
| -20.00     | 4352               | 3180               | 2979               | 3168               | 3167               |
| -20.50     | 4504               | 3514               | 3011               | 3228               | 3205               |
| -21.00     | 4646               | 3690               | 3051               | 3410               | 3405               |
| -21.50     | 4882               | 3770               | 3074               | 3515               | 3895               |
| -22.00     | 5068               | 3956               | 3093               | 3547               | 4209               |
| -22.50     | 5237               | 4138               | 3208               | 3732               | 4936               |
| -23.00     | 5104               | 4251               | 3290               | 3944               | 4997               |
| -23.50     | 5217               | 4363               | 3455               | 4083               | 5370               |
| -24.00     | 5326               | 4419               | 3523               | 4353               | 5589               |
| -24.50     | 5431               | 4505               | 3689               | 4557               | 5668               |
| -25.00     | 5531               | 4545               | 3969               | 4869               | 5567               |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SAMENVATTINGSTABEL SI Ø762/950 druk (n=1)**

**Uitgangspunten**

- paal : SI Ø762/950  
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie  
 - schachtafmeting : 860 mm  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            |                    |                    | $R_{e,paal}$<br>[kN] | $R_{b,paal}$<br>[kN] | $R_{c,paal}$<br>[kN] | $R_{e,d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40               | -8.00              | 3931.3               | 1500.8               | 5432.1               | 3256.6            | -17.3              | 3239.3                  |
|            |                    | -8.50              | 4068.3               | 1683.1               | 5751.4               | 3448.1            | -17.3              | 3430.8                  |
|            |                    | -9.00              | 4158.0               | 1865.5               | 6023.5               | 3611.2            | -17.3              | 3593.9                  |
|            |                    | -9.50              | 4268.3               | 2033.5               | 6301.8               | 3778.0            | -17.3              | 3760.7                  |
|            |                    | -10.00             | 2949.1               | 2194.9               | 5144.0               | 3083.9            | -17.3              | 3066.6                  |
|            |                    | -10.50             | 2374.4               | 2367.1               | 4741.5               | 2842.6            | -17.3              | 2825.3                  |
|            |                    | -11.00             | 2037.2               | 2549.5               | 4586.7               | 2749.8            | -17.3              | 2732.5                  |
|            |                    | -11.50             | 1861.3               | 2731.9               | 4593.2               | 2753.7            | -17.3              | 2736.4                  |
|            |                    | -12.00             | 1715.6               | 2914.2               | 4629.9               | 2775.7            | -17.3              | 2758.4                  |
|            |                    | -12.50             | 1225.3               | 3096.6               | 4321.9               | 2591.1            | -17.3              | 2573.7                  |
|            |                    | -13.00             | 1097.4               | 3278.1               | 4375.5               | 2623.2            | -17.3              | 2605.9                  |
|            |                    | -13.50             | 963.5                | 3391.0               | 4354.5               | 2610.6            | -17.3              | 2593.3                  |
|            |                    | -14.00             | 1095.4               | 3459.9               | 4555.3               | 2731.0            | -17.3              | 2713.6                  |
|            |                    | -14.50             | 1173.2               | 3517.7               | 4690.9               | 2812.3            | -17.3              | 2795.0                  |
|            |                    | -15.00             | 1200.9               | 3604.5               | 4805.4               | 2880.9            | -17.3              | 2863.6                  |
|            |                    | -15.50             | 1116.1               | 3729.6               | 4845.7               | 2905.1            | -17.3              | 2887.8                  |
|            |                    | -16.00             | 1466.3               | 3779.9               | 5246.1               | 3145.2            | -17.3              | 3127.8                  |
|            |                    | -16.50             | 1489.1               | 3873.8               | 5362.8               | 3215.1            | -17.3              | 3197.8                  |
|            |                    | -17.00             | 1690.8               | 3953.0               | 5643.8               | 3383.5            | -17.3              | 3366.2                  |
|            |                    | -17.50             | 1745.3               | 4048.9               | 5794.2               | 3473.7            | -17.3              | 3456.4                  |
|            |                    | -18.00             | 1784.8               | 4148.3               | 5933.1               | 3557.0            | -17.3              | 3539.7                  |
|            |                    | -18.50             | 1824.0               | 4242.8               | 6066.7               | 3637.1            | -17.3              | 3619.8                  |
|            |                    | -19.00             | 2241.8               | 4334.6               | 6576.4               | 3942.7            | -17.3              | 3925.4                  |
|            |                    | -19.50             | 2378.4               | 4444.0               | 6822.4               | 4090.2            | -17.3              | 4072.8                  |
|            |                    | -20.00             | 2735.5               | 4552.4               | 7287.9               | 4369.2            | -17.3              | 4351.9                  |
| -20.50     | 2861.9             | 4680.0             | 7541.9               | 4521.5               | -17.3                | 4504.2            |                    |                         |
| -21.00     | 2964.1             | 4814.8             | 7779.0               | 4663.7               | -17.3                | 4646.3            |                    |                         |
| -21.50     | 3227.3             | 4944.9             | 8172.2               | 4899.4               | -17.3                | 4882.0            |                    |                         |
| -22.00     | 3400.8             | 5080.9             | 8481.7               | 5085.0               | -17.3                | 5067.6            |                    |                         |
| -22.50     | 3543.3             | 5221.5             | 8764.8               | 5254.7               | -17.3                | 5237.4            |                    |                         |
| -23.00     | 3175.3             | 5366.3             | 8541.6               | 5120.9               | -17.3                | 5103.5            |                    |                         |
| -23.50     | 3221.3             | 5510.2             | 8731.5               | 5234.7               | -17.3                | 5217.4            |                    |                         |
| -24.00     | 3256.6             | 5656.1             | 8912.7               | 5343.3               | -17.3                | 5326.0            |                    |                         |
| -24.50     | 3286.3             | 5802.0             | 9088.3               | 5448.6               | -17.3                | 5431.3            |                    |                         |
| -25.00     | 3300.5             | 5953.5             | 9254.0               | 5548.0               | -17.3                | 5530.6            |                    |                         |
| 19-1008-15 | 0.75               | -8.00              | 3290.4               | 1704.0               | 4994.4               | 2994.2            | -6.3               | 2987.9                  |
|            |                    | -8.50              | 3931.2               | 1856.3               | 5787.5               | 3469.7            | -6.3               | 3463.4                  |
|            |                    | -9.00              | 4389.8               | 2038.7               | 6428.5               | 3854.0            | -6.3               | 3847.7                  |
|            |                    | -9.50              | 4504.2               | 2221.1               | 6725.3               | 4032.0            | -6.3               | 4025.7                  |
|            |                    | -10.00             | 4451.6               | 2403.4               | 6855.1               | 4109.8            | -6.3               | 4103.5                  |
|            |                    | -10.50             | 4585.9               | 2585.8               | 7171.7               | 4299.6            | -6.3               | 4293.3                  |
|            |                    | -11.00             | 4605.6               | 2768.2               | 7373.8               | 4420.8            | -6.3               | 4414.5                  |
|            |                    | -11.50             | 4618.4               | 2950.5               | 7568.9               | 4537.7            | -6.3               | 4531.5                  |
|            |                    | -12.00             | 4711.0               | 3132.9               | 7843.9               | 4702.6            | -6.3               | 4696.3                  |
|            |                    | -12.50             | 4642.4               | 3315.3               | 7957.7               | 4770.8            | -6.3               | 4764.5                  |
|            |                    | -13.00             | 2513.6               | 3494.6               | 6008.2               | 3602.0            | -6.3               | 3595.8                  |
|            |                    | -13.50             | 2137.7               | 3653.7               | 5791.5               | 3472.1            | -6.3               | 3465.8                  |
|            |                    | -14.00             | 1849.2               | 3836.1               | 5685.3               | 3408.4            | -6.3               | 3402.2                  |
|            |                    | -14.50             | 1543.5               | 4018.5               | 5562.0               | 3334.5            | -6.3               | 3328.3                  |
|            |                    | -15.00             | 1056.8               | 4200.8               | 5257.7               | 3152.1            | -6.3               | 3145.8                  |
|            |                    | -15.50             | 726.4                | 4383.2               | 5109.6               | 3063.3            | -6.3               | 3057.0                  |
|            |                    | -16.00             | 472.8                | 4564.1               | 5036.9               | 3019.7            | -6.3               | 3013.4                  |
|            |                    | -16.50             | 498.2                | 4608.1               | 5106.2               | 3061.3            | -6.3               | 3055.0                  |
|            |                    | -17.00             | 442.5                | 4627.9               | 5070.3               | 3039.8            | -6.3               | 3033.5                  |
|            |                    | -17.50             | 434.4                | 4658.0               | 5092.4               | 3053.0            | -6.3               | 3046.7                  |
|            |                    | -18.00             | 369.6                | 4709.1               | 5078.8               | 3044.8            | -6.3               | 3038.5                  |
|            |                    | -18.50             | 376.5                | 4722.6               | 5099.1               | 3057.0            | -6.3               | 3050.7                  |
|            |                    | -19.00             | 381.8                | 4736.8               | 5118.6               | 3068.7            | -6.3               | 3062.4                  |
|            |                    | -19.50             | 404.6                | 4753.9               | 5158.5               | 3092.6            | -6.3               | 3086.3                  |
|            |                    | -20.00             | 543.8                | 4771.5               | 5315.3               | 3186.6            | -6.3               | 3180.4                  |
| -20.50     | 1076.5             | 4795.2             | 5871.6               | 3520.2               | -6.3                 | 3513.9            |                    |                         |
| -21.00     | 1315.4             | 4850.8             | 6166.1               | 3696.7               | -6.3                 | 3690.5            |                    |                         |
| -21.50     | 1370.3             | 4929.0             | 6299.4               | 3776.6               | -6.3                 | 3770.3            |                    |                         |
| -22.00     | 1601.9             | 5007.4             | 6609.3               | 3962.4               | -6.3                 | 3956.1            |                    |                         |
| -22.50     | 1823.4             | 5089.0             | 6912.4               | 4144.1               | -6.3                 | 4137.8            |                    |                         |
| -23.00     | 1911.3             | 5189.4             | 7100.7               | 4257.0               | -6.3                 | 4250.8            |                    |                         |
| -23.50     | 1979.4             | 5309.0             | 7288.4               | 4369.6               | -6.3                 | 4363.3            |                    |                         |
| -24.00     | 1965.5             | 5415.9             | 7381.5               | 4425.3               | -6.3                 | 4419.1            |                    |                         |
| -24.50     | 1973.5             | 5552.0             | 7525.5               | 4511.7               | -6.3                 | 4505.4            |                    |                         |
| -25.00     | 1901.3             | 5689.6             | 7590.9               | 4550.9               | -6.3                 | 4544.6            |                    |                         |
| 251.S01    | -1.05              | -8.00              | 397.9                | 1125.3               | 1523.3               | 913.2             | -33.6              | 879.6                   |
|            |                    | -8.50              | 385.3                | 1212.7               | 1597.9               | 958.0             | -33.6              | 924.4                   |
|            |                    | -9.00              | 1307.1               | 1225.7               | 2532.8               | 1518.5            | -33.6              | 1484.9                  |
|            |                    | -9.50              | 1388.7               | 1306.3               | 2695.1               | 1615.8            | -33.6              | 1582.1                  |
|            |                    | -10.00             | 1415.6               | 1428.6               | 2844.2               | 1705.1            | -33.6              | 1671.5                  |
|            |                    | -10.50             | 1356.4               | 1572.3               | 2928.7               | 1755.8            | -33.6              | 1722.2                  |
|            |                    | -11.00             | 1288.3               | 1681.4               | 2969.8               | 1780.4            | -33.6              | 1746.8                  |
|            |                    | -11.50             | 1386.5               | 1747.8               | 3134.2               | 1879.0            | -33.6              | 1845.4                  |
|            |                    | -12.00             | 1456.4               | 1813.6               | 3269.9               | 1960.4            | -33.6              | 1926.8                  |
|            |                    | -12.50             | 1515.7               | 1925.6               | 3441.3               | 2063.1            | -33.6              | 2029.5                  |
|            |                    | -13.00             | 1557.0               | 2058.0               | 3615.0               | 2167.3            | -33.6              | 2133.6                  |
| -13.50     | 1594.4             | 2182.8             | 3777.2               | 2264.5               | -33.6                | 2230.9            |                    |                         |
| -14.00     | 1501.5             | 2356.3             | 3857.8               | 2312.8               | -33.6                | 2279.2            |                    |                         |
| -14.50     | 1286.3             | 2528.6             | 3815.0               | 2287.1               | -33.6                | 2253.5            |                    |                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld |                    | Beziwkdraagvermogen         |                             |                             | Rekenwaarden           |                          |                                |
|------------|----------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|--------------------------|--------------------------------|
|            | niveau   | paalpunt<br>niveau | R <sub>b,real</sub><br>[kN] | R <sub>r,real</sub><br>[kN] | R <sub>c,real</sub><br>[kN] | R <sub>d</sub><br>[kN] | F <sub>hkd</sub><br>[kN] | R <sub>d,netto;d</sub><br>[kN] |
| 251.S01    | -1.05    | -15.00             | 1191.7                      | 2715.2                      | 3906.9                      | 2342.3                 | -33.6                    | 2308.7                         |
|            |          | -15.50             | 2313.0                      | 2798.8                      | 5111.8                      | 3064.6                 | -33.6                    | 3031.0                         |
|            |          | -16.00             | 2285.3                      | 2967.1                      | 5252.5                      | 3149.0                 | -33.6                    | 3115.3                         |
|            |          | -16.50             | 2314.4                      | 3149.5                      | 5463.9                      | 3275.7                 | -33.6                    | 3242.1                         |
|            |          | -17.00             | 2330.9                      | 3329.8                      | 5660.7                      | 3393.7                 | -33.6                    | 3360.1                         |
|            |          | -17.50             | 2278.3                      | 3502.0                      | 5780.2                      | 3465.4                 | -33.6                    | 3431.7                         |
|            |          | -18.00             | 1271.1                      | 3664.5                      | 4935.7                      | 2959.0                 | -33.6                    | 2925.4                         |
|            |          | -18.50             | 1145.8                      | 3848.0                      | 4993.7                      | 2993.8                 | -33.6                    | 2960.2                         |
|            |          | -19.00             | 1013.8                      | 3957.4                      | 4971.2                      | 2980.3                 | -33.6                    | 2946.7                         |
|            |          | -19.50             | 930.4                       | 4073.7                      | 5004.1                      | 3000.0                 | -33.6                    | 2966.4                         |
|            |          | -20.00             | 809.4                       | 4215.4                      | 5024.9                      | 3012.5                 | -33.6                    | 2978.9                         |
|            |          | -20.50             | 659.5                       | 4419.7                      | 5079.2                      | 3045.1                 | -33.6                    | 3011.4                         |
|            |          | -21.00             | 516.9                       | 4628.5                      | 5145.5                      | 3084.8                 | -33.6                    | 3051.2                         |
|            |          | -21.50             | 468.6                       | 4715.2                      | 5183.8                      | 3107.8                 | -33.6                    | 3074.2                         |
|            |          | -22.00             | 472.6                       | 4742.3                      | 5214.9                      | 3126.4                 | -33.6                    | 3092.8                         |
|            |          | -22.50             | 629.6                       | 4778.2                      | 5407.7                      | 3242.0                 | -33.6                    | 3208.4                         |
|            |          | -23.00             | 708.0                       | 4835.6                      | 5543.6                      | 3323.5                 | -33.6                    | 3289.9                         |
|            |          | -23.50             | 907.3                       | 4910.8                      | 5818.2                      | 3488.1                 | -33.6                    | 3454.5                         |
|            |          | -24.00             | 919.5                       | 5012.6                      | 5932.1                      | 3556.4                 | -33.6                    | 3522.8                         |
|            |          | -24.50             | 1104.5                      | 5105.3                      | 6209.8                      | 3722.9                 | -33.6                    | 3689.3                         |
|            |          | -25.00             | 1486.9                      | 5189.5                      | 6676.4                      | 4002.7                 | -33.6                    | 3969.0                         |
| 19-1008-22 | 0.18     | -8.00              | 3029.3                      | 989.8                       | 4019.0                      | 2409.5                 | -35.1                    | 2374.4                         |
|            |          | -8.50              | 2443.4                      | 1135.2                      | 3578.6                      | 2145.5                 | -35.1                    | 2110.4                         |
|            |          | -9.00              | 2444.5                      | 1279.3                      | 3723.8                      | 2232.5                 | -35.1                    | 2197.4                         |
|            |          | -9.50              | 2439.8                      | 1431.0                      | 3870.7                      | 2320.6                 | -35.1                    | 2285.5                         |
|            |          | -10.00             | 2468.6                      | 1583.0                      | 4051.6                      | 2429.0                 | -35.1                    | 2393.9                         |
|            |          | -10.50             | 2429.8                      | 1735.1                      | 4164.9                      | 2497.0                 | -35.1                    | 2461.9                         |
|            |          | -11.00             | 2191.7                      | 1886.6                      | 4078.3                      | 2445.0                 | -35.1                    | 2409.9                         |
|            |          | -11.50             | 1798.0                      | 2037.8                      | 3835.9                      | 2299.7                 | -35.1                    | 2264.6                         |
|            |          | -12.00             | 1799.0                      | 2130.8                      | 3929.7                      | 2356.0                 | -35.1                    | 2320.9                         |
|            |          | -12.50             | 1813.9                      | 2213.7                      | 4027.6                      | 2414.6                 | -35.1                    | 2379.5                         |
|            |          | -13.00             | 1363.4                      | 2302.8                      | 3666.2                      | 2198.0                 | -35.1                    | 2162.9                         |
|            |          | -13.50             | 1014.9                      | 2407.8                      | 3422.7                      | 2052.0                 | -35.1                    | 2016.9                         |
|            |          | -14.00             | 879.6                       | 2498.4                      | 3378.0                      | 2025.2                 | -35.1                    | 1990.1                         |
|            |          | -14.50             | 844.3                       | 2577.4                      | 3421.7                      | 2051.4                 | -35.1                    | 2016.3                         |
|            |          | -15.00             | 843.1                       | 2633.2                      | 3476.3                      | 2084.1                 | -35.1                    | 2049.0                         |
|            |          | -15.50             | 765.0                       | 2723.9                      | 3488.9                      | 2091.7                 | -35.1                    | 2056.6                         |
|            |          | -16.00             | 690.2                       | 2797.0                      | 3487.1                      | 2090.6                 | -35.1                    | 2055.5                         |
|            |          | -16.50             | 656.8                       | 2839.5                      | 3496.3                      | 2096.1                 | -35.1                    | 2061.0                         |
|            |          | -17.00             | 615.7                       | 2872.9                      | 3488.6                      | 2091.5                 | -35.1                    | 2056.4                         |
|            |          | -17.50             | 921.4                       | 2894.7                      | 3816.1                      | 2287.8                 | -35.1                    | 2252.7                         |
|            |          | -18.00             | 1642.9                      | 2931.8                      | 4574.7                      | 2742.6                 | -35.1                    | 2707.5                         |
| -18.50     | 1697.4   | 3039.2             | 4736.7                      | 2839.7                      | -35.1                       | 2804.6                 |                          |                                |
| -19.00     | 1760.8   | 3142.8             | 4903.6                      | 2939.8                      | -35.1                       | 2904.7                 |                          |                                |
| -19.50     | 1873.3   | 3232.6             | 5105.9                      | 3061.1                      | -35.1                       | 3026.0                 |                          |                                |
| -20.00     | 2009.4   | 3333.5             | 5342.9                      | 3203.1                      | -35.1                       | 3168.0                 |                          |                                |
| -20.50     | 1971.0   | 3471.4             | 5442.4                      | 3262.8                      | -35.1                       | 3227.7                 |                          |                                |
| -21.00     | 2180.5   | 3566.4             | 5746.8                      | 3445.3                      | -35.1                       | 3410.2                 |                          |                                |
| -21.50     | 2225.5   | 3695.3             | 5920.8                      | 3549.6                      | -35.1                       | 3514.5                 |                          |                                |
| -22.00     | 2135.5   | 3839.0             | 5974.4                      | 3581.8                      | -35.1                       | 3546.7                 |                          |                                |
| -22.50     | 2345.7   | 3938.6             | 6284.2                      | 3767.5                      | -35.1                       | 3732.4                 |                          |                                |
| -23.00     | 2598.2   | 4039.6             | 6637.8                      | 3979.5                      | -35.1                       | 3944.4                 |                          |                                |
| -23.50     | 2712.3   | 4156.8             | 6869.2                      | 4118.2                      | -35.1                       | 4083.1                 |                          |                                |
| -24.00     | 3046.1   | 4272.8             | 7318.9                      | 4387.8                      | -35.1                       | 4352.7                 |                          |                                |
| -24.50     | 3258.6   | 4400.9             | 7659.6                      | 4592.1                      | -35.1                       | 4557.0                 |                          |                                |
| -25.00     | 3643.4   | 4537.3             | 8180.6                      | 4904.5                      | -35.1                       | 4869.4                 |                          |                                |
| 202.S03    | 0.03     | -8.00              | 3214.9                      | 629.2                       | 3844.1                      | 2304.6                 | -98.7                    | 2205.9                         |
|            |          | -8.50              | 3626.1                      | 773.6                       | 4399.7                      | 2637.7                 | -98.7                    | 2539.0                         |
|            |          | -9.00              | 2458.8                      | 942.4                       | 3401.2                      | 2039.1                 | -98.7                    | 1940.4                         |
|            |          | -9.50              | 2142.6                      | 1124.8                      | 3267.4                      | 1958.9                 | -98.7                    | 1860.1                         |
|            |          | -10.00             | 1801.9                      | 1307.2                      | 3109.0                      | 1863.9                 | -98.7                    | 1765.2                         |
|            |          | -10.50             | 1638.4                      | 1489.5                      | 3127.9                      | 1875.3                 | -98.7                    | 1776.5                         |
|            |          | -11.00             | 1509.5                      | 1657.4                      | 3166.9                      | 1898.6                 | -98.7                    | 1799.9                         |
|            |          | -11.50             | 1365.1                      | 1803.3                      | 3168.4                      | 1899.5                 | -98.7                    | 1800.8                         |
|            |          | -12.00             | 776.5                       | 1965.0                      | 2741.5                      | 1643.6                 | -98.7                    | 1544.9                         |
|            |          | -12.50             | 794.1                       | 2023.0                      | 2817.1                      | 1688.9                 | -98.7                    | 1590.2                         |
|            |          | -13.00             | 1012.7                      | 2081.2                      | 3093.9                      | 1854.9                 | -98.7                    | 1756.1                         |
|            |          | -13.50             | 1290.8                      | 2124.1                      | 3414.9                      | 2047.3                 | -98.7                    | 1948.6                         |
|            |          | -14.00             | 1438.9                      | 2208.2                      | 3647.1                      | 2186.5                 | -98.7                    | 2087.8                         |
|            |          | -14.50             | 1496.7                      | 2283.5                      | 3780.2                      | 2266.3                 | -98.7                    | 2167.6                         |
|            |          | -15.00             | 1515.9                      | 2373.7                      | 3889.6                      | 2331.9                 | -98.7                    | 2233.2                         |
|            |          | -15.50             | 1549.2                      | 2453.5                      | 4002.6                      | 2399.7                 | -98.7                    | 2300.9                         |
|            |          | -16.00             | 1585.7                      | 2530.7                      | 4116.4                      | 2467.9                 | -98.7                    | 2369.2                         |
|            |          | -16.50             | 1766.8                      | 2599.5                      | 4366.3                      | 2617.7                 | -98.7                    | 2519.0                         |
|            |          | -17.00             | 1967.7                      | 2677.3                      | 4645.0                      | 2784.8                 | -98.7                    | 2686.1                         |
|            |          | -17.50             | 2014.0                      | 2761.7                      | 4775.6                      | 2863.1                 | -98.7                    | 2764.4                         |
|            |          | -18.00             | 2070.1                      | 2863.2                      | 4933.3                      | 2957.6                 | -98.7                    | 2858.9                         |
| -18.50     | 2118.9   | 2960.1             | 5079.0                      | 3045.0                      | -98.7                       | 2946.2                 |                          |                                |
| -19.00     | 2158.2   | 3072.7             | 5230.9                      | 3136.0                      | -98.7                       | 3037.3                 |                          |                                |
| -19.50     | 2189.1   | 3184.9             | 5374.0                      | 3221.8                      | -98.7                       | 3123.1                 |                          |                                |
| -20.00     | 2144.0   | 3302.6             | 5446.6                      | 3265.4                      | -98.7                       | 3166.6                 |                          |                                |
| -20.50     | 2111.9   | 3398.4             | 5510.4                      | 3303.6                      | -98.7                       | 3204.9                 |                          |                                |
| -21.00     | 2370.7   | 3473.1             | 5843.9                      | 3503.5                      | -98.7                       | 3404.8                 |                          |                                |
| -21.50     | 3102.7   | 3559.6             | 6662.3                      | 3994.2                      | -98.7                       | 3895.5                 |                          |                                |
| -22.00     | 3494.2   | 3691.0             | 7185.2                      | 4307.7                      | -98.7                       | 4209.0                 |                          |                                |
| -22.50     | 4554.5   | 3842.9             | 8397.4                      | 5034.4                      | -98.7                       | 4935.7                 |                          |                                |
| -23.00     | 4487.7   | 4012.6             | 8500.2                      | 5096.1                      | -98.7                       | 4997.4                 |                          |                                |
| -23.50     | 4938.7   | 4182.4             | 9121.1                      | 5468.3                      | -98.7                       | 5369.6                 |                          |                                |
| -24.00     | 5127.1   | 4360.3             | 9487.4                      | 5687.9                      | -98.7                       | 5589.2                 |                          |                                |
| -24.50     | 5076.2   | 4542.7             | 9618.9                      | 5766.7                      | -98.7                       | 5668.0                 |                          |                                |
| -25.00     | 4725.4   | 4725.1             | 9450.5                      | 5665.7                      | -98.7                       | 5567.0                 |                          |                                |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**REKENGEDEGENS MV Ø914/1074 druk**

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(gem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{f,dk}$  : 1.0  
 $R_{z,calc,max}$  begrenzen op  $0.75 * R_{z,calc,max}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : MV Ø914/1074  
 Niveau paalkop [m] : N.A.P. 0.00  
 $E_{d,1}$  [kN] : 0.00  $E_{d,2}$  [kN] : 0.00  
 $S_{req,1}$  [m] : 0.15  $S_{req,2}$  [m] : 0.05  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS MV Ø914/1074**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

Nr Beginniveau Eindniveau Stapgrootte  
 [m] [m] [m]

|   |        |        |      |
|---|--------|--------|------|
| 1 | -10.00 | -25.00 | 0.50 |
|---|--------|--------|------|

**RESULTATEN MV Ø914/1074 druk (n=1)**

**Sondering : 19-1008-14**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau<br>[m] | $R_b$<br>[kN] | $R_n$<br>[kN] | $R_{z,calc}$<br>[kN] | $R_{z,k}$<br>[kN] | $R_{z,d}$<br>[kN] | $F_{n,k,d}$<br>[kN] | $R_{n,d}$<br>[kN] | $F_{z,tot,1}$<br>[kN] | U.C. | $S_{1,1}$<br>[mm] | $S_{1,2}$<br>[mm] |
|---------------|---------------|---------------|----------------------|-------------------|-------------------|---------------------|-------------------|-----------------------|------|-------------------|-------------------|
| -10.00        | 3551          | 3946          | 7497                 | 5394              | 4495              | -20.0               | 4475              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -10.50        | 3180          | 4256          | 7436                 | 5349              | 4458              | -20.0               | 4438              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -11.00        | 2945          | 4584          | 7529                 | 5417              | 4514              | -20.0               | 4494              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -11.50        | 2806          | 4912          | 7718                 | 5552              | 4627              | -20.0               | 4607              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -12.00        | 2070          | 5240          | 7309                 | 5258              | 4382              | -20.0               | 4362              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -12.50        | 1832          | 5568          | 7399                 | 5323              | 4436              | -20.0               | 4416              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -13.00        | 1629          | 5894          | 7523                 | 5412              | 4510              | -20.0               | 4490              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -13.50        | 1501          | 6093          | 7593                 | 5463              | 4552              | -20.0               | 4532              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -14.00        | 1626          | 6188          | 7814                 | 5622              | 4685              | -20.0               | 4665              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -14.50        | 1741          | 6289          | 8030                 | 5777              | 4814              | -20.0               | 4794              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -15.00        | 1782          | 6445          | 8227                 | 5919              | 4933              | -20.0               | 4912              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -15.50        | 1783          | 6670          | 8453                 | 6081              | 5068              | -20.0               | 5048              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -16.00        | 2173          | 6760          | 8934                 | 6427              | 5356              | -20.0               | 5336              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -16.50        | 2255          | 6929          | 9184                 | 6607              | 5506              | -20.0               | 5486              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -17.00        | 2488          | 7072          | 9560                 | 6878              | 5731              | -20.0               | 5711              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -17.50        | 2558          | 7244          | 9802                 | 7052              | 5876              | -20.0               | 5856              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -18.00        | 2605          | 7423          | 10028                | 7214              | 6012              | -20.0               | 5992              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -18.50        | 2711          | 7593          | 10304                | 7413              | 6177              | -20.0               | 6157              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -19.00        | 3260          | 7758          | 11018                | 7927              | 6606              | -20.0               | 6586              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -19.50        | 3486          | 7954          | 11441                | 8231              | 6859              | -20.0               | 6839              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -20.00        | 3957          | 8149          | 12107                | 8710              | 7258              | -20.0               | 7238              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -20.50        | 4123          | 8379          | 12502                | 8994              | 7495              | -20.0               | 7475              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -21.00        | 4271          | 8621          | 12892                | 9275              | 7729              | -20.0               | 7709              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -21.50        | 4621          | 8855          | 13476                | 9695              | 8079              | -20.0               | 8059              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -22.00        | 4864          | 9099          | 13964                | 10046             | 8372              | -20.0               | 8351              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -22.50        | 4432          | 9352          | 13785                | 9917              | 8264              | -20.0               | 8244              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -23.00        | 4547          | 9613          | 14159                | 10187             | 8489              | -20.0               | 8469              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -23.50        | 4664          | 9871          | 14535                | 10457             | 8714              | -20.0               | 8694              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -24.00        | 4748          | 10134         | 14882                | 10707             | 8922              | -20.0               | 8902              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -24.50        | 4803          | 10396         | 15199                | 10935             | 9112              | -20.0               | 9092              | -20.0                 | 0.00 | -0.0              | -0.0              |
| -25.00        | 4831          | 10668         | 15499                | 11150             | 9292              | -20.0               | 9272              | -20.0                 | 0.00 | -0.0              | -0.0              |

**Sondering : 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau<br>[m] | $R_b$<br>[kN] | $R_n$<br>[kN] | $R_{z,calc}$<br>[kN] | $R_{z,k}$<br>[kN] | $R_{z,d}$<br>[kN] | $F_{n,k,d}$<br>[kN] | $R_{n,d}$<br>[kN] | $F_{z,tot,1}$<br>[kN] | U.C. | $S_{1,1}$<br>[mm] | $S_{1,2}$<br>[mm] |
|---------------|---------------|---------------|----------------------|-------------------|-------------------|---------------------|-------------------|-----------------------|------|-------------------|-------------------|
| -10.00        | 6399          | 4304          | 10703                | 7700              | 6417              | -7.3                | 6410              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -10.50        | 6605          | 4632          | 11237                | 8084              | 6737              | -7.3                | 6730              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -11.00        | 6609          | 4960          | 11569                | 8323              | 6936              | -7.3                | 6928              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -11.50        | 6602          | 5288          | 11890                | 8554              | 7128              | -7.3                | 7121              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -12.00        | 6715          | 5616          | 12330                | 8871              | 7392              | -7.3                | 7385              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -12.50        | 3567          | 5944          | 9510                 | 6842              | 5702              | -7.3                | 5694              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -13.00        | 3190          | 6266          | 9456                 | 6803              | 5669              | -7.3                | 5662              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -13.50        | 2877          | 6552          | 9429                 | 6783              | 5653              | -7.3                | 5645              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -14.00        | 2538          | 6880          | 9418                 | 6776              | 5646              | -7.3                | 5639              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -14.50        | 1882          | 7208          | 9090                 | 6539              | 5449              | -7.3                | 5442              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -15.00        | 1435          | 7536          | 8970                 | 6454              | 5378              | -7.3                | 5371              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -15.50        | 1014          | 7864          | 8878                 | 6387              | 5322              | -7.3                | 5315              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -16.00        | 683.7         | 8189          | 8873                 | 6383              | 5319              | -7.3                | 5312              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -16.50        | 739.4         | 8268          | 9007                 | 6480              | 5400              | -7.3                | 5393              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -17.00        | 656.8         | 8304          | 8960                 | 6446              | 5372              | -7.3                | 5365              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -17.50        | 644.7         | 8358          | 9002                 | 6477              | 5397              | -7.3                | 5390              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -18.00        | 551.2         | 8450          | 9001                 | 6475              | 5396              | -7.3                | 5389              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -18.50        | 558.9         | 8474          | 9033                 | 6498              | 5415              | -7.3                | 5408              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -19.00        | 566.3         | 8499          | 9066                 | 6522              | 5435              | -7.3                | 5428              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -19.50        | 611.1         | 8530          | 9141                 | 6576              | 5480              | -7.3                | 5473              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -20.00        | 844.6         | 8562          | 9406                 | 6767              | 5639              | -7.3                | 5632              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -20.50        | 1640          | 8604          | 10244                | 7370              | 6142              | -7.3                | 6135              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -21.00        | 1941          | 8704          | 10645                | 7659              | 6382              | -7.3                | 6375              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -21.50        | 2009          | 8845          | 10854                | 7808              | 6507              | -7.3                | 6500              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -22.00        | 2381          | 8986          | 11367                | 8178              | 6815              | -7.3                | 6808              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -22.50        | 2659          | 9133          | 11791                | 8483              | 7069              | -7.3                | 7062              | -7.3                  | 0.00 | -0.0              | -0.0              |
| -23.00        | 2672          | 9313          | 11985                | 8622              | 7185              | -7.3                | 7178              | -7.3                  | 0.00 | -0.0              | -0.0              |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**Sondering : 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,sk</sub> [kN] | R <sub>o,td</sub> [kN] | F <sub>n,kd</sub> [kN] | R <sub>o,nd</sub> [kN] | F <sub>o,tot,tj1</sub> [kN] | U.C. | S <sub>1,1</sub> [mm] | S <sub>1,2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------------|------|-----------------------|-----------------------|
| -23.50     | 2742                | 9528                | 12270                    | 8827                   | 7356                   | -7.3                   | 7349                   | -7.3                        | 0.00 | -0.0                  | -0.0                  |
| -24.00     | 2833                | 9720                | 12554                    | 9032                   | 7526                   | -7.3                   | 7519                   | -7.3                        | 0.00 | -0.0                  | -0.0                  |
| -24.50     | 2833                | 9965                | 12798                    | 9207                   | 7673                   | -7.3                   | 7666                   | -7.3                        | 0.00 | -0.0                  | -0.0                  |
| -25.00     | 2714                | 10212               | 12926                    | 9299                   | 7750                   | -7.3                   | 7742                   | -7.3                        | 0.00 | -0.0                  | -0.0                  |

**Sondering : 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,sk</sub> [kN] | R <sub>o,td</sub> [kN] | F <sub>n,kd</sub> [kN] | R <sub>o,nd</sub> [kN] | F <sub>o,tot,tj1</sub> [kN] | U.C. | S <sub>1,1</sub> [mm] | S <sub>1,2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 2065                | 2452                | 4517                     | 3250                   | 2708                   | -38.8                  | 2669                   | -38.8                       | 0.01 | -0.1                  | -0.0                  |
| -10.50     | 1972                | 2711                | 4683                     | 3369                   | 2808                   | -38.8                  | 2769                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.00     | 1865                | 2907                | 4772                     | 3433                   | 2861                   | -38.8                  | 2822                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.50     | 2005                | 3026                | 5032                     | 3620                   | 3016                   | -38.8                  | 2978                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.00     | 2141                | 3145                | 5286                     | 3803                   | 3169                   | -38.8                  | 3130                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.50     | 2226                | 3346                | 5572                     | 4009                   | 3341                   | -38.8                  | 3302                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.00     | 2257                | 3584                | 5841                     | 4202                   | 3502                   | -38.8                  | 3463                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.50     | 2337                | 3808                | 6145                     | 4421                   | 3684                   | -38.8                  | 3645                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.00     | 2195                | 4120                | 6316                     | 4544                   | 3786                   | -38.8                  | 3748                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.50     | 1873                | 4430                | 6303                     | 4534                   | 3779                   | -38.8                  | 3740                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.00     | 2064                | 4710                | 6775                     | 4874                   | 4061                   | -38.8                  | 4023                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.50     | 3246                | 4815                | 8061                     | 5799                   | 4833                   | -38.8                  | 4794                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -16.00     | 3376                | 5118                | 8494                     | 6111                   | 5092                   | -38.8                  | 5053                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -16.50     | 3398                | 5446                | 8844                     | 6363                   | 5302                   | -38.8                  | 5263                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -17.00     | 3426                | 5770                | 9196                     | 6616                   | 5513                   | -38.8                  | 5475                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -17.50     | 1927                | 6080                | 8006                     | 5760                   | 4800                   | -38.8                  | 4761                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -18.00     | 1679                | 6372                | 8051                     | 5792                   | 4827                   | -38.8                  | 4788                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -18.50     | 1701                | 6647                | 8347                     | 6005                   | 5004                   | -38.8                  | 4966                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -19.00     | 1406                | 6773                | 8179                     | 5884                   | 4903                   | -38.8                  | 4864                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -19.50     | 1321                | 6955                | 8275                     | 5953                   | 4961                   | -38.8                  | 4922                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -20.00     | 1229                | 7209                | 8439                     | 6071                   | 5059                   | -38.8                  | 5020                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -20.50     | 978.9               | 7483                | 8462                     | 6088                   | 5073                   | -38.8                  | 5034                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -21.00     | 767.3               | 7724                | 8492                     | 6109                   | 5091                   | -38.8                  | 5052                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -21.50     | 695.6               | 7825                | 8520                     | 6130                   | 5108                   | -38.8                  | 5069                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -22.00     | 700.4               | 7856                | 8556                     | 6156                   | 5130                   | -38.8                  | 5091                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -22.50     | 932.4               | 7897                | 8830                     | 6352                   | 5294                   | -38.8                  | 5255                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -23.00     | 1154                | 7964                | 9118                     | 6560                   | 5466                   | -38.8                  | 5427                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -23.50     | 1342                | 8051                | 9393                     | 6757                   | 5631                   | -38.8                  | 5592                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -24.00     | 1354                | 8168                | 9522                     | 6850                   | 5709                   | -38.8                  | 5670                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -24.50     | 1711                | 8275                | 9987                     | 7185                   | 5987                   | -38.8                  | 5948                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -25.00     | 2326                | 8373                | 10699                    | 7697                   | 6414                   | -38.8                  | 6375                   | -38.8                       | 0.01 | -0.0                  | -0.0                  |

**Sondering : 19-1008-22**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,sk</sub> [kN] | R <sub>o,td</sub> [kN] | F <sub>n,kd</sub> [kN] | R <sub>o,nd</sub> [kN] | F <sub>o,tot,tj1</sub> [kN] | U.C. | S <sub>1,1</sub> [mm] | S <sub>1,2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 3410                | 2846                | 6256                     | 4501                   | 3751                   | -40.6                  | 3710                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -10.50     | 3042                | 3120                | 6162                     | 4433                   | 3694                   | -40.6                  | 3653                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -11.00     | 2633                | 3392                | 6025                     | 4334                   | 3612                   | -40.6                  | 3571                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -11.50     | 2545                | 3664                | 6209                     | 4467                   | 3723                   | -40.6                  | 3682                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -12.00     | 2605                | 3831                | 6436                     | 4630                   | 3859                   | -40.6                  | 3818                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -12.50     | 2030                | 3980                | 6010                     | 4324                   | 3603                   | -40.6                  | 3563                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -13.00     | 1531                | 4140                | 5671                     | 4080                   | 3400                   | -40.6                  | 3359                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -13.50     | 1349                | 4329                | 5678                     | 4085                   | 3404                   | -40.6                  | 3363                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -14.00     | 1293                | 4492                | 5785                     | 4162                   | 3468                   | -40.6                  | 3428                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -14.50     | 1257                | 4634                | 5891                     | 4238                   | 3532                   | -40.6                  | 3491                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -15.00     | 1251                | 4734                | 5986                     | 4306                   | 3589                   | -40.6                  | 3548                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -15.50     | 1136                | 4897                | 6033                     | 4340                   | 3617                   | -40.6                  | 3576                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -16.00     | 1024                | 5029                | 6053                     | 4355                   | 3629                   | -40.6                  | 3588                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -16.50     | 974.9               | 5105                | 6080                     | 4374                   | 3645                   | -40.6                  | 3605                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -17.00     | 932.8               | 5165                | 6098                     | 4387                   | 3656                   | -40.6                  | 3615                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -17.50     | 1504                | 5205                | 6709                     | 4826                   | 4022                   | -40.6                  | 3981                   | -40.6                       | 0.01 | -0.1                  | -0.0                  |
| -18.00     | 2435                | 5271                | 7706                     | 5544                   | 4620                   | -40.6                  | 4579                   | -40.6                       | 0.01 | -0.1                  | -0.0                  |
| -18.50     | 2506                | 5464                | 7970                     | 5734                   | 4778                   | -40.6                  | 4738                   | -40.6                       | 0.01 | -0.1                  | -0.0                  |
| -19.00     | 2589                | 5651                | 8240                     | 5928                   | 4940                   | -40.6                  | 4899                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -19.50     | 2746                | 5812                | 8558                     | 6157                   | 5130                   | -40.6                  | 5090                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -20.00     | 2937                | 5993                | 8931                     | 6425                   | 5354                   | -40.6                  | 5313                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -20.50     | 2954                | 6241                | 9196                     | 6615                   | 5513                   | -40.6                  | 5472                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -21.00     | 3169                | 6412                | 9581                     | 6893                   | 5744                   | -40.6                  | 5704                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -21.50     | 3223                | 6644                | 9867                     | 7099                   | 5916                   | -40.6                  | 5875                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -22.00     | 3077                | 6902                | 9979                     | 7179                   | 5983                   | -40.6                  | 5942                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -22.50     | 3398                | 7081                | 10479                    | 7539                   | 6282                   | -40.6                  | 6242                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -23.00     | 3734                | 7263                | 10997                    | 7912                   | 6593                   | -40.6                  | 6552                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -23.50     | 3933                | 7474                | 11407                    | 8207                   | 6839                   | -40.6                  | 6798                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -24.00     | 4381                | 7682                | 12063                    | 8679                   | 7232                   | -40.6                  | 7192                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -24.50     | 4726                | 7913                | 12638                    | 9092                   | 7577                   | -40.6                  | 7536                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -25.00     | 5244                | 8158                | 13402                    | 9642                   | 8035                   | -40.6                  | 7994                   | -40.6                       | 0.01 | -0.0                  | -0.0                  |

**Sondering : 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,sk</sub> [kN] | R <sub>o,td</sub> [kN] | F <sub>n,kd</sub> [kN] | R <sub>o,nd</sub> [kN] | F <sub>o,tot,tj1</sub> [kN] | U.C. | S <sub>1,1</sub> [mm] | S <sub>1,2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 2565                | 2334                | 4899                     | 3525                   | 2937                   | -114.1                 | 2823                   | -114.1                      | 0.04 | -0.2                  | -0.1                  |
| -10.50     | 2295                | 2662                | 4957                     | 3566                   | 2972                   | -114.1                 | 2858                   | -114.1                      | 0.04 | -0.1                  | -0.1                  |
| -11.00     | 2231                | 2964                | 5195                     | 3738                   | 3115                   | -114.1                 | 3001                   | -114.1                      | 0.04 | -0.1                  | -0.1                  |
| -11.50     | 2001                | 3226                | 5227                     | 3761                   | 3134                   | -114.1                 | 3020                   | -114.1                      | 0.04 | -0.1                  | -0.1                  |
| -12.00     | 1139                | 3488                | 4627                     | 3329                   | 2774                   | -114.1                 | 2660                   | -114.1                      | 0.04 | -0.1                  | -0.1                  |
| -12.50     | 1164                | 3562                | 4726                     | 3400                   | 2834                   | -114.1                 | 2719                   | -114.1                      | 0.04 | -0.1                  | -0.1                  |
| -13.00     | 1611                | 3646                | 5258                     | 3782                   | 3152                   | -114.1                 | 3038                   | -114.1                      | 0.04 | -0.1                  | -0.1                  |
| -13.50     | 1907                | 3714                | 5621                     | 4044                   | 3370                   | -114.1                 | 3256                   | -114.1                      | 0.03 | -0.1                  | -0.1                  |
| -14.00     | 2125                | 3866                | 5991                     | 4310                   | 3592                   | -114.1                 | 3478                   | -114.1                      | 0.03 | -0.1                  | -0.1                  |
| -14.50     | 2202                | 4001                | 6203                     | 4463                   | 3719                   | -114.1                 | 3605                   | -114.1                      | 0.03 | -0.1                  | -0.1                  |
| -15.00     | 2221                | 4163                | 6384                     | 4593                   | 3827                   | -114.1                 | 3713                   | -114.1                      | 0.03 | -0.1                  | -0.1                  |
| -15.50     | 2261                | 4307                | 6567                     | 4725                   | 3937                   | -114.1                 | 3823                   | -114.1                      | 0.03 | -0.1                  | -0.1                  |



Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**Sondering : 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | R <sub>0</sub> | R <sub>0</sub> | R <sub>o,jeel</sub> | R <sub>o,ik</sub> | R <sub>o,rd</sub> | F <sub>o,rd</sub> | R <sub>o,nd</sub> | F <sub>o,totj1</sub> | U.C. | S <sub>1,1</sub> | S <sub>1,2</sub> |
|--------|----------------|----------------|---------------------|-------------------|-------------------|-------------------|-------------------|----------------------|------|------------------|------------------|
| [m]    | [kN]           | [kN]           | [kN]                | [kN]              | [kN]              | [kN]              | [kN]              | [kN]                 |      | [mm]             | [mm]             |
| -16.00 | 2333           | 4445           | 6779                | 4877              | 4064              | -114.1            | 3950              | -114.1               | 0.03 | -0.1             | -0.1             |
| -16.50 | 2583           | 4569           | 7152                | 5145              | 4288              | -114.1            | 4174              | -114.1               | 0.03 | -0.1             | -0.1             |
| -17.00 | 2812           | 4709           | 7521                | 5411              | 4509              | -114.1            | 4395              | -114.1               | 0.03 | -0.1             | -0.1             |
| -17.50 | 2909           | 4861           | 7770                | 5590              | 4658              | -114.1            | 4544              | -114.1               | 0.02 | -0.1             | -0.1             |
| -18.00 | 2982           | 5043           | 8025                | 5773              | 4811              | -114.1            | 4697              | -114.1               | 0.02 | -0.1             | -0.1             |
| -18.50 | 3043           | 5217           | 8261                | 5943              | 4953              | -114.1            | 4838              | -114.1               | 0.02 | -0.1             | -0.1             |
| -19.00 | 3091           | 5420           | 8511                | 6123              | 5102              | -114.1            | 4988              | -114.1               | 0.02 | -0.1             | -0.1             |
| -19.50 | 3129           | 5622           | 8751                | 6296              | 5246              | -114.1            | 5132              | -114.1               | 0.02 | -0.1             | -0.1             |
| -20.00 | 3059           | 5833           | 8893                | 6398              | 5331              | -114.1            | 5217              | -114.1               | 0.02 | -0.1             | -0.1             |
| -20.50 | 3060           | 6006           | 9066                | 6522              | 5435              | -114.1            | 5321              | -114.1               | 0.02 | -0.1             | -0.1             |
| -21.00 | 3550           | 6140           | 9690                | 6971              | 5809              | -114.1            | 5695              | -114.1               | 0.02 | -0.1             | -0.1             |
| -21.50 | 4647           | 6295           | 10943               | 7873              | 6560              | -114.1            | 6446              | -114.1               | 0.02 | -0.1             | -0.1             |
| -22.00 | 5238           | 6532           | 11770               | 8467              | 7056              | -114.1            | 6942              | -114.1               | 0.02 | -0.1             | -0.1             |
| -22.50 | 6306           | 6805           | 13111               | 9432              | 7860              | -114.1            | 7746              | -114.1               | 0.01 | -0.1             | -0.1             |
| -23.00 | 6524           | 7110           | 13634               | 9809              | 8174              | -114.1            | 8060              | -114.1               | 0.01 | -0.2             | -0.1             |
| -23.50 | 7290           | 7415           | 14705               | 10579             | 8816              | -114.1            | 8702              | -114.1               | 0.01 | -0.1             | -0.1             |
| -24.00 | 7577           | 7735           | 15312               | 11016             | 9180              | -114.1            | 9066              | -114.1               | 0.01 | -0.1             | -0.1             |
| -24.50 | 7011           | 8063           | 15074               | 10845             | 9037              | -114.1            | 8923              | -114.1               | 0.01 | -0.1             | -0.1             |
| -25.00 | 6480           | 8391           | 14870               | 10698             | 8915              | -114.1            | 8801              | -114.1               | 0.01 | -0.1             | -0.1             |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SAMENVATTINGSTABEL MV Ø914/1074 druk (n=1)**

**Uitgangspunten**

- paal : MV Ø914/1074  
 - paaltype : Geheide in de grond gevormde betonpaal;terugheind  
 - schachtafmeting : 994 mm  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld paalpunt |         | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|------------|-------------------|---------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            | niveau            | niveau  | $R_{b,real}$<br>[kN] | $R_{s,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{c;d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40              | -10.00  | 3551.1               | 3946.3               | 7497.4               | 4494.8            | -20.0              | 4474.8                  |
|            |                   | -10.50  | 3179.8               | 4256.0               | 7435.7               | 4457.9            | -20.0              | 4437.8                  |
|            |                   | -11.00  | 2945.1               | 4583.8               | 7529.0               | 4513.8            | -20.0              | 4493.7                  |
|            |                   | -11.50  | 2806.1               | 4911.7               | 7717.8               | 4627.0            | -20.0              | 4607.0                  |
|            |                   | -12.00  | 2069.7               | 5239.6               | 7309.3               | 4382.1            | -20.0              | 4362.0                  |
|            |                   | -12.50  | 1831.7               | 5567.5               | 7399.2               | 4436.0            | -20.0              | 4416.0                  |
|            |                   | -13.00  | 1628.9               | 5893.9               | 7522.7               | 4510.0            | -20.0              | 4490.0                  |
|            |                   | -13.50  | 1500.8               | 6092.6               | 7593.4               | 4552.4            | -20.0              | 4532.4                  |
|            |                   | -14.00  | 1625.9               | 6188.1               | 7814.1               | 4684.7            | -20.0              | 4664.7                  |
|            |                   | -14.50  | 1741.4               | 6288.9               | 8030.4               | 4814.4            | -20.0              | 4794.3                  |
|            |                   | -15.00  | 1782.5               | 6445.0               | 8227.5               | 4932.5            | -20.0              | 4912.5                  |
|            |                   | -15.50  | 1783.3               | 6669.9               | 8453.2               | 5067.9            | -20.0              | 5047.8                  |
|            |                   | -16.00  | 2173.5               | 6760.3               | 8933.8               | 5356.0            | -20.0              | 5335.9                  |
|            |                   | -16.50  | 2254.9               | 6929.1               | 9184.0               | 5506.0            | -20.0              | 5486.0                  |
|            |                   | -17.00  | 2488.4               | 7071.5               | 9560.0               | 5731.4            | -20.0              | 5711.4                  |
|            |                   | -17.50  | 2558.0               | 7243.9               | 9801.9               | 5876.4            | -20.0              | 5856.4                  |
|            |                   | -18.00  | 2605.1               | 7422.7               | 10027.8              | 6011.9            | -20.0              | 5991.8                  |
|            |                   | -18.50  | 2711.3               | 7592.5               | 10303.8              | 6177.4            | -20.0              | 6157.3                  |
|            |                   | -19.00  | 3260.5               | 7757.7               | 11018.2              | 6605.6            | -20.0              | 6585.6                  |
|            |                   | -19.50  | 3486.2               | 7954.4               | 11440.5              | 6858.8            | -20.0              | 6838.8                  |
|            |                   | -20.00  | 3957.4               | 8149.2               | 12106.6              | 7258.2            | -20.0              | 7238.1                  |
|            |                   | -20.50  | 4123.3               | 8378.6               | 12501.9              | 7495.2            | -20.0              | 7475.1                  |
|            |                   | -21.00  | 4271.1               | 8621.1               | 12892.2              | 7729.2            | -20.0              | 7709.1                  |
|            |                   | -21.50  | 4621.3               | 8854.8               | 13476.1              | 8079.2            | -20.0              | 8059.2                  |
|            |                   | -22.00  | 4864.3               | 9099.4               | 13963.7              | 8371.5            | -20.0              | 8351.5                  |
| -22.50     | 4432.4            | 9352.2  | 13784.6              | 8264.2               | -20.0                | 8244.1            |                    |                         |
| -23.00     | 4546.9            | 9612.5  | 14159.5              | 8488.9               | -20.0                | 8468.8            |                    |                         |
| -23.50     | 4664.1            | 9871.4  | 14535.4              | 8714.3               | -20.0                | 8694.3            |                    |                         |
| -24.00     | 4748.4            | 10133.7 | 14882.0              | 8922.1               | -20.0                | 8902.0            |                    |                         |
| -24.50     | 4803.1            | 10395.8 | 15199.0              | 9112.1               | -20.0                | 9092.1            |                    |                         |
| -25.00     | 4830.5            | 10668.2 | 15498.7              | 9291.8               | -20.0                | 9271.8            |                    |                         |
| 19-1008-15 | 0.75              | -10.00  | 6399.2               | 4304.2               | 10703.3              | 6416.9            | -7.3               | 6409.6                  |
|            |                   | -10.50  | 6605.0               | 4632.0               | 11237.0              | 6736.8            | -7.3               | 6729.6                  |
|            |                   | -11.00  | 6608.9               | 4959.9               | 11568.8              | 6935.7            | -7.3               | 6928.5                  |
|            |                   | -11.50  | 6602.5               | 5287.8               | 11890.3              | 7128.5            | -7.3               | 7121.2                  |
|            |                   | -12.00  | 6714.5               | 5615.7               | 12330.2              | 7392.2            | -7.3               | 7385.0                  |
|            |                   | -12.50  | 3566.7               | 5943.6               | 9510.3               | 5701.6            | -7.3               | 5694.4                  |
|            |                   | -13.00  | 3190.3               | 6266.1               | 9456.4               | 5669.3            | -7.3               | 5662.0                  |
|            |                   | -13.50  | 2876.7               | 6552.1               | 9428.8               | 5652.7            | -7.3               | 5645.5                  |
|            |                   | -14.00  | 2538.0               | 6880.0               | 9418.0               | 5646.3            | -7.3               | 5639.1                  |
|            |                   | -14.50  | 1881.7               | 7207.9               | 9089.6               | 5449.4            | -7.3               | 5442.2                  |
|            |                   | -15.00  | 1434.6               | 7535.8               | 8970.4               | 5377.9            | -7.3               | 5370.7                  |
|            |                   | -15.50  | 1014.0               | 7863.7               | 8877.7               | 5322.4            | -7.3               | 5315.1                  |
|            |                   | -16.00  | 683.7                | 8188.8               | 8872.5               | 5319.3            | -7.3               | 5312.0                  |
|            |                   | -16.50  | 739.4                | 8267.9               | 9007.3               | 5400.1            | -7.3               | 5392.8                  |
|            |                   | -17.00  | 656.8                | 8303.5               | 8960.3               | 5371.9            | -7.3               | 5364.6                  |
|            |                   | -17.50  | 644.7                | 8357.7               | 9002.4               | 5397.1            | -7.3               | 5389.9                  |
|            |                   | -18.00  | 551.2                | 8449.7               | 9000.8               | 5396.2            | -7.3               | 5388.9                  |
|            |                   | -18.50  | 558.9                | 8473.8               | 9032.6               | 5415.3            | -7.3               | 5408.0                  |
|            |                   | -19.00  | 566.3                | 8499.4               | 9065.7               | 5435.1            | -7.3               | 5427.8                  |
|            |                   | -19.50  | 611.1                | 8530.0               | 9141.2               | 5480.3            | -7.3               | 5473.1                  |
|            |                   | -20.00  | 844.6                | 8561.7               | 9406.3               | 5639.3            | -7.3               | 5632.0                  |
|            |                   | -20.50  | 1640.2               | 8604.3               | 10244.5              | 6141.8            | -7.3               | 6134.5                  |
|            |                   | -21.00  | 1941.2               | 8704.3               | 10645.5              | 6382.2            | -7.3               | 6374.9                  |
|            |                   | -21.50  | 2008.7               | 8845.0               | 10853.8              | 6507.0            | -7.3               | 6499.8                  |
|            |                   | -22.00  | 2381.5               | 8985.9               | 11367.3              | 6814.9            | -7.3               | 6807.7                  |
| -22.50     | 2658.9            | 9132.6  | 11791.4              | 7069.2               | -7.3                 | 7062.0            |                    |                         |
| -23.00     | 2672.1            | 9313.1  | 11985.2              | 7185.4               | -7.3                 | 7178.1            |                    |                         |
| -23.50     | 2741.9            | 9528.2  | 12270.0              | 7356.1               | -7.3                 | 7348.9            |                    |                         |
| -24.00     | 2833.4            | 9720.4  | 12553.8              | 7526.3               | -7.3                 | 7519.0            |                    |                         |
| -24.50     | 2833.1            | 9965.1  | 12798.2              | 7672.8               | -7.3                 | 7665.5            |                    |                         |
| -25.00     | 2713.8            | 10212.5 | 12926.3              | 7749.6               | -7.3                 | 7742.3            |                    |                         |
| 251.S01    | -1.05             | -10.00  | 2065.1               | 2452.3               | 4517.4               | 2708.3            | -38.8              | 2669.4                  |
|            |                   | -10.50  | 1972.5               | 2710.7               | 4683.2               | 2807.7            | -38.8              | 2768.8                  |
|            |                   | -11.00  | 1865.3               | 2906.9               | 4772.2               | 2861.0            | -38.8              | 2822.2                  |
|            |                   | -11.50  | 2005.3               | 3026.2               | 5031.5               | 3016.5            | -38.8              | 2977.6                  |
|            |                   | -12.00  | 2141.4               | 3144.5               | 5286.0               | 3169.0            | -38.8              | 3130.2                  |
|            |                   | -12.50  | 2226.2               | 3345.9               | 5572.1               | 3340.6            | -38.8              | 3301.8                  |
|            |                   | -13.00  | 2256.7               | 3584.1               | 5840.7               | 3501.6            | -38.8              | 3462.8                  |
|            |                   | -13.50  | 2336.6               | 3808.3               | 6145.0               | 3684.0            | -38.8              | 3645.2                  |
|            |                   | -14.00  | 2195.5               | 4120.3               | 6315.7               | 3786.4            | -38.8              | 3747.5                  |
|            |                   | -14.50  | 1872.7               | 4430.2               | 6302.9               | 3778.7            | -38.8              | 3739.9                  |
|            |                   | -15.00  | 2064.2               | 4710.3               | 6774.5               | 4061.5            | -38.8              | 4022.6                  |
|            |                   | -15.50  | 3245.5               | 4815.4               | 8061.0               | 4832.7            | -38.8              | 4793.9                  |
|            |                   | -16.00  | 3375.5               | 5118.1               | 8493.6               | 5092.1            | -38.8              | 5053.3                  |
|            |                   | -16.50  | 3397.9               | 5446.0               | 8843.9               | 5302.1            | -38.8              | 5263.2                  |
|            |                   | -17.00  | 3426.1               | 5770.2               | 9196.4               | 5513.4            | -38.8              | 5474.6                  |
| -17.50     | 1926.8            | 6079.7  | 8006.5               | 4800.0               | -38.8                | 4761.2            |                    |                         |
| -18.00     | 1679.1            | 6372.0  | 8051.0               | 4826.8               | -38.8                | 4787.9            |                    |                         |
| -18.50     | 1700.7            | 6646.6  | 8347.3               | 5004.4               | -38.8                | 4965.6            |                    |                         |
| -19.00     | 1405.6            | 6773.1  | 8178.7               | 4903.3               | -38.8                | 4864.5            |                    |                         |
| -19.50     | 1320.5            | 6954.5  | 8275.1               | 4961.1               | -38.8                | 4922.2            |                    |                         |
| -20.00     | 1229.2            | 7209.4  | 8438.6               | 5059.1               | -38.8                | 5020.3            |                    |                         |
| -20.50     | 978.9             | 7483.0  | 8461.9               | 5073.1               | -38.8                | 5034.2            |                    |                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld<br>niveau | paalpunt<br>niveau | Beziijkdraagvermogen |                      |                      | Rekenwaarden      |                     |                         |       |        |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|---------------------|-------------------------|-------|--------|
|           |                    |                    | $R_{b,real}$<br>[kN] | $R_{s,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{b;d}$<br>[kN] | $F_{b;k;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |       |        |
| 251.S01   | -1.05              | -21.00             | 767.3                | 7724.4               | 8491.7               | 5090.9            | -38.8               | 5052.1                  |       |        |
|           |                    | -21.50             | 695.6                | 7824.5               | 8520.1               | 5108.0            | -38.8               | 5069.1                  |       |        |
|           |                    | -22.00             | 700.4                | 7855.9               | 8556.3               | 5129.7            | -38.8               | 5090.8                  |       |        |
|           |                    | -22.50             | 932.4                | 7897.4               | 8829.7               | 5293.6            | -38.8               | 5254.7                  |       |        |
|           |                    | -23.00             | 1154.1               | 7963.8               | 9117.8               | 5466.3            | -38.8               | 5427.5                  |       |        |
|           |                    | -23.50             | 1342.0               | 8050.7               | 9392.7               | 5631.1            | -38.8               | 5592.2                  |       |        |
|           |                    | -24.00             | 1353.7               | 8168.3               | 9522.1               | 5708.7            | -38.8               | 5669.8                  |       |        |
|           |                    | -24.50             | 1711.4               | 8275.4               | 9986.8               | 5987.3            | -38.8               | 5948.5                  |       |        |
|           |                    | -25.00             | 2325.9               | 8372.7               | 10698.6              | 6414.1            | -38.8               | 6375.2                  |       |        |
|           |                    | 19-1008-22         | 0.18                 | -10.00               | 3410.0               | 2846.2            | 6256.2              | 3750.7                  | -40.6 | 3710.2 |
|           |                    |                    |                      | -10.50               | 3042.0               | 3119.6            | 6161.6              | 3694.0                  | -40.6 | 3653.4 |
| -11.00    | 2632.5             |                    |                      | 3392.0               | 6024.5               | 3611.8            | -40.6               | 3571.3                  |       |        |
| -11.50    | 2545.4             |                    |                      | 3663.9               | 6209.3               | 3722.6            | -40.6               | 3682.0                  |       |        |
| -12.00    | 2605.4             |                    |                      | 3831.0               | 6436.4               | 3858.7            | -40.6               | 3818.2                  |       |        |
| -12.50    | 2030.0             |                    |                      | 3980.1               | 6010.1               | 3603.2            | -40.6               | 3562.6                  |       |        |
| -13.00    | 1531.1             |                    |                      | 4140.2               | 5671.3               | 3400.1            | -40.6               | 3359.5                  |       |        |
| -13.50    | 1348.7             |                    |                      | 4329.1               | 5677.8               | 3404.0            | -40.6               | 3363.4                  |       |        |
| -14.00    | 1293.3             |                    |                      | 4491.9               | 5785.2               | 3468.4            | -40.6               | 3427.8                  |       |        |
| -14.50    | 1257.0             |                    |                      | 4634.0               | 5891.0               | 3531.7            | -40.6               | 3491.2                  |       |        |
| -15.00    | 1251.5             |                    |                      | 4734.4               | 5985.8               | 3588.6            | -40.6               | 3548.1                  |       |        |
| -15.50    | 1135.6             |                    |                      | 4897.3               | 6032.9               | 3616.8            | -40.6               | 3576.3                  |       |        |
| -16.00    | 1024.4             |                    |                      | 5028.8               | 6053.2               | 3629.0            | -40.6               | 3588.4                  |       |        |
| -16.50    | 974.9              |                    |                      | 5105.3               | 6080.2               | 3645.2            | -40.6               | 3604.6                  |       |        |
| -17.00    | 932.8              |                    |                      | 5165.2               | 6098.0               | 3655.8            | -40.6               | 3615.3                  |       |        |
| -17.50    | 1504.0             |                    |                      | 5204.5               | 6708.5               | 4021.9            | -40.6               | 3981.3                  |       |        |
| -18.00    | 2434.9             |                    |                      | 5271.2               | 7706.1               | 4619.9            | -40.6               | 4579.4                  |       |        |
| -18.50    | 2505.6             |                    |                      | 5464.3               | 7969.9               | 4778.1            | -40.6               | 4737.5                  |       |        |
| -19.00    | 2589.2             |                    |                      | 5650.5               | 8239.7               | 4939.9            | -40.6               | 4899.3                  |       |        |
| -19.50    | 2745.6             |                    |                      | 5812.0               | 8557.6               | 5130.5            | -40.6               | 5089.9                  |       |        |
| -20.00    | 2937.2             |                    |                      | 5993.3               | 8930.5               | 5354.0            | -40.6               | 5313.5                  |       |        |
| -20.50    | 2954.2             |                    |                      | 6241.3               | 9195.5               | 5512.9            | -40.6               | 5472.3                  |       |        |
| -21.00    | 3169.2             |                    |                      | 6412.1               | 9581.3               | 5744.2            | -40.6               | 5703.6                  |       |        |
| -21.50    | 3223.3             |                    |                      | 6643.8               | 9867.1               | 5915.5            | -40.6               | 5875.0                  |       |        |
| -22.00    | 3076.8             |                    |                      | 6902.2               | 9979.1               | 5982.6            | -40.6               | 5942.1                  |       |        |
| -22.50    | 3397.9             | 7081.3             | 10479.1              | 6282.4               | -40.6                | 6241.9            |                     |                         |       |        |
| -23.00    | 3734.3             | 7262.9             | 10997.2              | 6593.1               | -40.6                | 6552.5            |                     |                         |       |        |
| -23.50    | 3933.4             | 7473.7             | 11407.1              | 6838.8               | -40.6                | 6798.2            |                     |                         |       |        |
| -24.00    | 4381.0             | 7682.2             | 12063.2              | 7232.1               | -40.6                | 7191.6            |                     |                         |       |        |
| -24.50    | 4725.8             | 7912.5             | 12638.4              | 7577.0               | -40.6                | 7536.4            |                     |                         |       |        |
| -25.00    | 5244.0             | 8157.7             | 13401.8              | 8034.6               | -40.6                | 7994.1            |                     |                         |       |        |
| 202.S03   | 0.03               | -10.00             | 2564.7               | 2334.5               | 4899.2               | 2937.2            | -114.1              | 2823.1                  |       |        |
|           |                    | -10.50             | 2294.6               | 2662.3               | 4956.9               | 2971.8            | -114.1              | 2857.7                  |       |        |
|           |                    | -11.00             | 2231.3               | 2964.2               | 5195.4               | 3114.8            | -114.1              | 3000.7                  |       |        |
|           |                    | -11.50             | 2001.0               | 3226.5               | 5227.5               | 3134.0            | -114.1              | 3019.9                  |       |        |
|           |                    | -12.00             | 1139.1               | 3488.3               | 4627.4               | 2774.2            | -114.1              | 2660.1                  |       |        |
|           |                    | -12.50             | 1164.0               | 3562.4               | 4726.4               | 2833.6            | -114.1              | 2719.5                  |       |        |
|           |                    | -13.00             | 1611.2               | 3646.4               | 5257.6               | 3152.0            | -114.1              | 3037.9                  |       |        |
|           |                    | -13.50             | 1906.9               | 3714.4               | 5621.4               | 3370.1            | -114.1              | 3256.0                  |       |        |
|           |                    | -14.00             | 2125.2               | 3865.6               | 5990.8               | 3591.6            | -114.1              | 3477.5                  |       |        |
|           |                    | -14.50             | 2202.2               | 4001.0               | 6203.3               | 3719.0            | -114.1              | 3604.9                  |       |        |
|           |                    | -15.00             | 2221.1               | 4163.2               | 6384.2               | 3827.5            | -114.1              | 3713.4                  |       |        |
|           |                    | -15.50             | 2260.6               | 4306.6               | 6567.2               | 3937.2            | -114.1              | 3823.1                  |       |        |
|           |                    | -16.00             | 2333.4               | 4445.4               | 6778.8               | 4064.0            | -114.1              | 3949.9                  |       |        |
|           |                    | -16.50             | 2583.0               | 4569.2               | 7152.2               | 4287.9            | -114.1              | 4173.8                  |       |        |
|           |                    | -17.00             | 2812.4               | 4709.0               | 7521.4               | 4509.2            | -114.1              | 4395.1                  |       |        |
|           |                    | -17.50             | 2909.2               | 4860.7               | 7769.9               | 4658.2            | -114.1              | 4544.1                  |       |        |
|           |                    | -18.00             | 2981.8               | 5043.3               | 8025.1               | 4811.2            | -114.1              | 4697.1                  |       |        |
|           |                    | -18.50             | 3043.4               | 5217.5               | 8260.9               | 4952.6            | -114.1              | 4838.5                  |       |        |
|           |                    | -19.00             | 3091.0               | 5420.0               | 8510.9               | 5102.5            | -114.1              | 4988.4                  |       |        |
|           |                    | -19.50             | 3129.2               | 5621.6               | 8750.8               | 5246.3            | -114.1              | 5132.2                  |       |        |
|           |                    | -20.00             | 3059.3               | 5833.3               | 8892.6               | 5331.3            | -114.1              | 5217.2                  |       |        |
|           |                    | -20.50             | 3060.5               | 6005.6               | 9066.1               | 5435.3            | -114.1              | 5321.2                  |       |        |
|           |                    | -21.00             | 3550.3               | 6139.9               | 9690.2               | 5809.5            | -114.1              | 5695.4                  |       |        |
|           |                    | -21.50             | 4647.5               | 6295.4               | 10942.9              | 6560.5            | -114.1              | 6446.4                  |       |        |
|           |                    | -22.00             | 5238.0               | 6531.7               | 11769.7              | 7056.2            | -114.1              | 6942.1                  |       |        |
| -22.50    | 6306.0             | 6804.7             | 13110.7              | 7860.1               | -114.1               | 7746.0            |                     |                         |       |        |
| -23.00    | 6524.4             | 7109.8             | 13634.2              | 8174.0               | -114.1               | 8059.9            |                     |                         |       |        |
| -23.50    | 7290.3             | 7415.2             | 14705.5              | 8816.2               | -114.1               | 8702.1            |                     |                         |       |        |
| -24.00    | 7576.9             | 7735.0             | 15311.9              | 9179.8               | -114.1               | 9065.7            |                     |                         |       |        |
| -24.50    | 7011.5             | 8062.9             | 15074.4              | 9037.4               | -114.1               | 8923.3            |                     |                         |       |        |
| -25.00    | 6479.7             | 8390.8             | 14870.5              | 8915.1               | -114.1               | 8801.0            |                     |                         |       |        |

**REKENGEDEGENS MV Ø1016/1176 druk**

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n-1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(qem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{t,nk}$  : 1.0  
 $R_{b,real,max;i}$  begrenzen op  $0.75 * R_{b,real,max;i}$  : NEE  
 UGT draagvermogen zonder negatieve kleef : NEE

Paal : MV Ø1016/1176  
 Niveau paalkop [m] : N.A.P. 0.00  
 $E_{d,1}$  [kN] : 0.00  $E_{d,2}$  [kN] : 0.00  
 $S_{req,1}$  [m] : 0.15  $S_{req,2}$  [m] : 0.05  
 Bovenbel. [kN/m²] : 0.00

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**PAALPUNTNIVEAUS MV Ø1016/1176**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|-----------------|----------------|-----------------|
| 1  | -10.00          | -25.00         | 0.50            |

**RESULTATEN MV Ø1016/1176 druk (n=1)**

**Sondering : 19-1008-14**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>b</sub> [kN] | R <sub>s</sub> [kN] | R <sub>c,calc</sub> [kN] | R <sub>c,k</sub> [kN] | R <sub>c,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>nd</sub> [kN] | F <sub>c,tot,t;1</sub> [kN] | U.C. | S <sub>1;1</sub> [mm] | S <sub>1;2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 3968                | 4351                | 8319                     | 5985                  | 4988                  | -22.1                   | 4965                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -10.50     | 3776                | 4693                | 8469                     | 6092                  | 5077                  | -22.1                   | 5055                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -11.00     | 3632                | 5054                | 8686                     | 6249                  | 5207                  | -22.1                   | 5185                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -11.50     | 2807                | 5416                | 8222                     | 5915                  | 4929                  | -22.1                   | 4907                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -12.00     | 2540                | 5777                | 8317                     | 5983                  | 4986                  | -22.1                   | 4964                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -12.50     | 2227                | 6139                | 8366                     | 6019                  | 5015                  | -22.1                   | 4993                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -13.00     | 1980                | 6499                | 8479                     | 6100                  | 5083                  | -22.1                   | 5061                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -13.50     | 1880                | 6718                | 8597                     | 6185                  | 5154                  | -22.1                   | 5132                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -14.00     | 1977                | 6823                | 8800                     | 6331                  | 5276                  | -22.1                   | 5254                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -14.50     | 2117                | 6934                | 9051                     | 6512                  | 5427                  | -22.1                   | 5404                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -15.00     | 2167                | 7106                | 9273                     | 6672                  | 5560                  | -22.1                   | 5537                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -15.50     | 2261                | 7354                | 9615                     | 6917                  | 5764                  | -22.1                   | 5742                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -16.00     | 2640                | 7454                | 10094                    | 7262                  | 6052                  | -22.1                   | 6030                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -16.50     | 2786                | 7640                | 10426                    | 7500                  | 6250                  | -22.1                   | 6228                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -17.00     | 3010                | 7797                | 10807                    | 7775                  | 6479                  | -22.1                   | 6457                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -17.50     | 3086                | 7987                | 11073                    | 7966                  | 6639                  | -22.1                   | 6617                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -18.00     | 3135                | 8184                | 11319                    | 8143                  | 6786                  | -22.1                   | 6764                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -18.50     | 3348                | 8372                | 11719                    | 8431                  | 7026                  | -22.1                   | 7004                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -19.00     | 3915                | 8554                | 12469                    | 8971                  | 7475                  | -22.1                   | 7453                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -19.50     | 4224                | 8771                | 12995                    | 9349                  | 7791                  | -22.1                   | 7769                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -20.00     | 4736                | 8985                | 13722                    | 9872                  | 8227                  | -22.1                   | 8204                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -20.50     | 4922                | 9238                | 14161                    | 10188                 | 8490                  | -22.1                   | 8468                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -21.00     | 5105                | 9506                | 14611                    | 10511                 | 8759                  | -22.1                   | 8737                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -21.50     | 5498                | 9763                | 15261                    | 10979                 | 9149                  | -22.1                   | 9127                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -22.00     | 5121                | 10033               | 15154                    | 10902                 | 9085                  | -22.1                   | 9063                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -22.50     | 5253                | 10312               | 15565                    | 11198                 | 9332                  | -22.1                   | 9309                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -23.00     | 5380                | 10599               | 15979                    | 11495                 | 9580                  | -22.1                   | 9557                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -23.50     | 5510                | 10884               | 16394                    | 11794                 | 9828                  | -22.1                   | 9806                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -24.00     | 5629                | 11174               | 16803                    | 12088                 | 10074                 | -22.1                   | 10052                | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -24.50     | 5753                | 11463               | 17216                    | 12385                 | 10321                 | -22.1                   | 10299                | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -25.00     | 5798                | 11763               | 17561                    | 12634                 | 10528                 | -22.1                   | 10506                | -22.1                       | 0.00 | -0.0                  | -0.0                  |

**Sondering : 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>b</sub> [kN] | R <sub>s</sub> [kN] | R <sub>c,calc</sub> [kN] | R <sub>c,k</sub> [kN] | R <sub>c,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>nd</sub> [kN] | F <sub>c,tot,t;1</sub> [kN] | U.C. | S <sub>1;1</sub> [mm] | S <sub>1;2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 7652                | 4746                | 12397                    | 8919                  | 7432                  | -8.0                    | 7424                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -10.50     | 7883                | 5107                | 12991                    | 9346                  | 7788                  | -8.0                    | 7780                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -11.00     | 7870                | 5469                | 13339                    | 9596                  | 7997                  | -8.0                    | 7989                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -11.50     | 7843                | 5830                | 13674                    | 9837                  | 8198                  | -8.0                    | 8190                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -12.00     | 4515                | 6192                | 10707                    | 7703                  | 6419                  | -8.0                    | 6411                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -12.50     | 3894                | 6554                | 10447                    | 7516                  | 6263                  | -8.0                    | 6255                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -13.00     | 3493                | 6909                | 10402                    | 7483                  | 6236                  | -8.0                    | 6228                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -13.50     | 3340                | 7224                | 10565                    | 7601                  | 6334                  | -8.0                    | 6326                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -14.00     | 2655                | 7586                | 10241                    | 7368                  | 6140                  | -8.0                    | 6132                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -14.50     | 2139                | 7948                | 10087                    | 7257                  | 6047                  | -8.0                    | 6039                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -15.00     | 1652                | 8309                | 9961                     | 7166                  | 5972                  | -8.0                    | 5964                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -15.50     | 1180                | 8671                | 9850                     | 7086                  | 5905                  | -8.0                    | 5897                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -16.00     | 826.7               | 9029                | 9856                     | 7091                  | 5909                  | -8.0                    | 5901                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -16.50     | 899.0               | 9116                | 10015                    | 7205                  | 6004                  | -8.0                    | 5996                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -17.00     | 798.5               | 9156                | 9954                     | 7161                  | 5968                  | -8.0                    | 5960                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -17.50     | 783.8               | 9215                | 9999                     | 7194                  | 5995                  | -8.0                    | 5987                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -18.00     | 671.9               | 9317                | 9989                     | 7186                  | 5988                  | -8.0                    | 5980                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -18.50     | 679.4               | 9343                | 10023                    | 7211                  | 6009                  | -8.0                    | 6001                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -19.00     | 693.8               | 9372                | 10065                    | 7241                  | 6034                  | -8.0                    | 6026                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -19.50     | 749.7               | 9405                | 10155                    | 7306                  | 6088                  | -8.0                    | 6080                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -20.00     | 1088                | 9440                | 10528                    | 7574                  | 6312                  | -8.0                    | 6304                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -20.50     | 2029                | 9487                | 11516                    | 8285                  | 6904                  | -8.0                    | 6896                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -21.00     | 2352                | 9597                | 11949                    | 8597                  | 7164                  | -8.0                    | 7156                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -21.50     | 2431                | 9753                | 12183                    | 8765                  | 7304                  | -8.0                    | 7296                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -22.00     | 2901                | 9908                | 12809                    | 9215                  | 7679                  | -8.0                    | 7671                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -22.50     | 3198                | 10070               | 13268                    | 9545                  | 7954                  | -8.0                    | 7946                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -23.00     | 3205                | 10269               | 13474                    | 9693                  | 8078                  | -8.0                    | 8070                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -23.50     | 3281                | 10506               | 13787                    | 9919                  | 8266                  | -8.0                    | 8258                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -24.00     | 3384                | 10718               | 14102                    | 10145                 | 8454                  | -8.0                    | 8446                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -24.50     | 3374                | 10988               | 14362                    | 10332                 | 8610                  | -8.0                    | 8602                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -25.00     | 3221                | 11260               | 14481                    | 10418                 | 8682                  | -8.0                    | 8674                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |

**Sondering : 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>b</sub> [kN] | R <sub>s</sub> [kN] | R <sub>c,calc</sub> [kN] | R <sub>c,k</sub> [kN] | R <sub>c,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>nd</sub> [kN] | F <sub>c,tot,t;1</sub> [kN] | U.C. | S <sub>1;1</sub> [mm] | S <sub>1;2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 2482                | 2704                | 5186                     | 3731                  | 3109                  | -42.8                   | 3066                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -10.50     | 2361                | 2989                | 5350                     | 3849                  | 3207                  | -42.8                   | 3164                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.00     | 2231                | 3205                | 5436                     | 3911                  | 3259                  | -42.8                   | 3216                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.50     | 2422                | 3337                | 5759                     | 4143                  | 3453                  | -42.8                   | 3410                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.00     | 2589                | 3467                | 6056                     | 4357                  | 3631                  | -42.8                   | 3588                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.50     | 2689                | 3689                | 6379                     | 4589                  | 3824                  | -42.8                   | 3781                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.00     | 2724                | 3952                | 6676                     | 4803                  | 4002                  | -42.8                   | 3960                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.50     | 2819                | 4199                | 7018                     | 5049                  | 4207                  | -42.8                   | 4165                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.00     | 2645                | 4543                | 7188                     | 5171                  | 4309                  | -42.8                   | 4267                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.50     | 2250                | 4885                | 7135                     | 5133                  | 4278                  | -42.8                   | 4235                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.00     | 2738                | 5194                | 7931                     | 5706                  | 4755                  | -42.8                   | 4712                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.50     | 3947                | 5310                | 9256                     | 6659                  | 5549                  | -42.8                   | 5507                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -16.00     | 4061                | 5643                | 9704                     | 6981                  | 5818                  | -42.8                   | 5775                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**Sondering : 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | R <sub>0</sub> | R <sub>s</sub> | R <sub>o,caal</sub> | R <sub>o,k</sub> | R <sub>o,d</sub> | F <sub>o,k,d</sub> | R <sub>o,d</sub> | F <sub>o,tot,t,1</sub> | U.C. | S <sub>1,1</sub> | S <sub>1,2</sub> |
|--------|----------------|----------------|---------------------|------------------|------------------|--------------------|------------------|------------------------|------|------------------|------------------|
| [m]    | [kN]           | [kN]           | [kN]                | [kN]             | [kN]             | [kN]               | [kN]             | [kN]                   |      | [mm]             | [mm]             |
| -16.50 | 4078           | 6005           | 10083               | 7254             | 6045             | -42.8              | 6002             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -17.00 | 2760           | 6362           | 9122                | 6562             | 5469             | -42.8              | 5426             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -17.50 | 2207           | 6704           | 8910                | 6410             | 5342             | -42.8              | 5299             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -18.00 | 1944           | 7026           | 8969                | 6453             | 5377             | -42.8              | 5335             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -18.50 | 2068           | 7329           | 9396                | 6760             | 5633             | -42.8              | 5590             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -19.00 | 1647           | 7468           | 9115                | 6558             | 5465             | -42.8              | 5422             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -19.50 | 1624           | 7668           | 9292                | 6685             | 5571             | -42.8              | 5528             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -20.00 | 1499           | 7949           | 9448                | 6797             | 5665             | -42.8              | 5622             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -20.50 | 1190           | 8251           | 9441                | 6792             | 5660             | -42.8              | 5617             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -21.00 | 932.8          | 8517           | 9450                | 6798             | 5665             | -42.8              | 5623             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -21.50 | 845.6          | 8627           | 9473                | 6815             | 5679             | -42.8              | 5636             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -22.00 | 849.7          | 8662           | 9512                | 6843             | 5702             | -42.8              | 5660             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -22.50 | 1132           | 8708           | 9840                | 7079             | 5899             | -42.8              | 5856             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -23.00 | 1500           | 8781           | 10281               | 7396             | 6164             | -42.8              | 6121             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -23.50 | 1628           | 8877           | 10505               | 7557             | 6298             | -42.8              | 6255             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -24.00 | 1628           | 9007           | 10635               | 7651             | 6376             | -42.8              | 6333             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -24.50 | 2068           | 9125           | 11193               | 8052             | 6710             | -42.8              | 6667             | -42.8                  | 0.01 | -0.0             | -0.0             |
| -25.00 | 2965           | 9232           | 12196               | 8774             | 7312             | -42.8              | 7269             | -42.8                  | 0.01 | -0.0             | -0.0             |

**Sondering : 19-1008-22**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | R <sub>0</sub> | R <sub>s</sub> | R <sub>o,caal</sub> | R <sub>o,k</sub> | R <sub>o,d</sub> | F <sub>o,k,d</sub> | R <sub>o,d</sub> | F <sub>o,tot,t,1</sub> | U.C. | S <sub>1,1</sub> | S <sub>1,2</sub> |
|--------|----------------|----------------|---------------------|------------------|------------------|--------------------|------------------|------------------------|------|------------------|------------------|
| [m]    | [kN]           | [kN]           | [kN]                | [kN]             | [kN]             | [kN]               | [kN]             | [kN]                   |      | [mm]             | [mm]             |
| -10.00 | 3798           | 3138           | 6936                | 4990             | 4159             | -44.7              | 4114             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -10.50 | 3163           | 3440           | 6603                | 4750             | 3959             | -44.7              | 3914             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -11.00 | 3140           | 3740           | 6880                | 4949             | 4124             | -44.7              | 4080             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -11.50 | 3022           | 4040           | 7062                | 5081             | 4234             | -44.7              | 4189             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -12.00 | 2383           | 4224           | 6607                | 4753             | 3961             | -44.7              | 3916             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -12.50 | 1939           | 4389           | 6328                | 4553             | 3794             | -44.7              | 3749             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -13.00 | 1708           | 4565           | 6273                | 4513             | 3761             | -44.7              | 3716             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -13.50 | 1619           | 4773           | 6393                | 4599             | 3832             | -44.7              | 3788             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -14.00 | 1573           | 4953           | 6526                | 4695             | 3912             | -44.7              | 3867             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -14.50 | 1528           | 5109           | 6638                | 4775             | 3979             | -44.7              | 3935             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -15.00 | 1521           | 5220           | 6742                | 4850             | 4042             | -44.7              | 3997             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -15.50 | 1381           | 5400           | 6780                | 4878             | 4065             | -44.7              | 4020             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -16.00 | 1245           | 5545           | 6790                | 4885             | 4071             | -44.7              | 4026             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -16.50 | 1185           | 5629           | 6814                | 4902             | 4085             | -44.7              | 4041             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -17.00 | 1172           | 5695           | 6868                | 4941             | 4117             | -44.7              | 4072             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -17.50 | 1992           | 5739           | 7730                | 5561             | 4635             | -44.7              | 4590             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -18.00 | 2958           | 5812           | 8770                | 6309             | 5258             | -44.7              | 5213             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -18.50 | 3036           | 6025           | 9061                | 6519             | 5432             | -44.7              | 5388             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -19.00 | 3130           | 6230           | 9360                | 6734             | 5612             | -44.7              | 5567             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -19.50 | 3313           | 6408           | 9721                | 6994             | 5828             | -44.7              | 5783             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -20.00 | 3538           | 6608           | 10146               | 7299             | 6083             | -44.7              | 6038             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -20.50 | 3585           | 6882           | 10467               | 7530             | 6275             | -44.7              | 6230             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -21.00 | 3804           | 7070           | 10874               | 7823             | 6519             | -44.7              | 6475             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -21.50 | 3861           | 7326           | 11186               | 8048             | 6706             | -44.7              | 6662             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -22.00 | 3673           | 7610           | 11284               | 8118             | 6765             | -44.7              | 6720             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -22.50 | 4075           | 7808           | 11883               | 8549             | 7124             | -44.7              | 7080             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -23.00 | 4451           | 8008           | 12459               | 8964             | 7470             | -44.7              | 7425             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -23.50 | 4705           | 8241           | 12946               | 9313             | 7761             | -44.7              | 7716             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -24.00 | 5228           | 8470           | 13698               | 9855             | 8213             | -44.7              | 8168             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -24.50 | 5718           | 8724           | 14443               | 10390            | 8659             | -44.7              | 8614             | -44.7                  | 0.01 | -0.0             | -0.0             |
| -25.00 | 5648           | 8995           | 14643               | 10535            | 8779             | -44.7              | 8734             | -44.7                  | 0.01 | -0.0             | -0.0             |

**Sondering : 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | R <sub>0</sub> | R <sub>s</sub> | R <sub>o,caal</sub> | R <sub>o,k</sub> | R <sub>o,d</sub> | F <sub>o,k,d</sub> | R <sub>o,d</sub> | F <sub>o,tot,t,1</sub> | U.C. | S <sub>1,1</sub> | S <sub>1,2</sub> |
|--------|----------------|----------------|---------------------|------------------|------------------|--------------------|------------------|------------------------|------|------------------|------------------|
| [m]    | [kN]           | [kN]           | [kN]                | [kN]             | [kN]             | [kN]               | [kN]             | [kN]                   |      | [mm]             | [mm]             |
| -10.00 | 2968           | 2574           | 5542                | 3987             | 3322             | -125.8             | 3197             | -125.8                 | 0.04 | -0.1             | -0.1             |
| -10.50 | 2763           | 2936           | 5698                | 4099             | 3416             | -125.8             | 3290             | -125.8                 | 0.04 | -0.1             | -0.1             |
| -11.00 | 2647           | 3268           | 5915                | 4256             | 3546             | -125.8             | 3421             | -125.8                 | 0.04 | -0.1             | -0.1             |
| -11.50 | 2416           | 3558           | 5974                | 4298             | 3581             | -125.8             | 3456             | -125.8                 | 0.04 | -0.1             | -0.1             |
| -12.00 | 1358           | 3846           | 5204                | 3744             | 3120             | -125.8             | 2994             | -125.8                 | 0.04 | -0.1             | -0.1             |
| -12.50 | 1402           | 3928           | 5330                | 3834             | 3195             | -125.8             | 3069             | -125.8                 | 0.04 | -0.1             | -0.1             |
| -13.00 | 1961           | 4021           | 5981                | 4303             | 3586             | -125.8             | 3460             | -125.8                 | 0.04 | -0.1             | -0.1             |
| -13.50 | 2318           | 4096           | 6414                | 4614             | 3845             | -125.8             | 3719             | -125.8                 | 0.03 | -0.1             | -0.1             |
| -14.00 | 2566           | 4262           | 6829                | 4913             | 4094             | -125.8             | 3968             | -125.8                 | 0.03 | -0.1             | -0.1             |
| -14.50 | 2662           | 4412           | 7073                | 5089             | 4240             | -125.8             | 4115             | -125.8                 | 0.03 | -0.1             | -0.1             |
| -15.00 | 2679           | 4590           | 7270                | 5230             | 4358             | -125.8             | 4232             | -125.8                 | 0.03 | -0.1             | -0.1             |
| -15.50 | 2720           | 4748           | 7469                | 5373             | 4478             | -125.8             | 4352             | -125.8                 | 0.03 | -0.1             | -0.1             |
| -16.00 | 2825           | 4902           | 7727                | 5559             | 4632             | -125.8             | 4506             | -125.8                 | 0.03 | -0.1             | -0.1             |
| -16.50 | 3113           | 5038           | 8151                | 5864             | 4887             | -125.8             | 4761             | -125.8                 | 0.03 | -0.1             | -0.1             |
| -17.00 | 3369           | 5192           | 8561                | 6159             | 5133             | -125.8             | 5007             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -17.50 | 3479           | 5359           | 8838                | 6358             | 5299             | -125.8             | 5173             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -18.00 | 3538           | 5561           | 9099                | 6546             | 5455             | -125.8             | 5329             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -18.50 | 3626           | 5753           | 9379                | 6748             | 5623             | -125.8             | 5497             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -19.00 | 3676           | 5976           | 9652                | 6944             | 5787             | -125.8             | 5661             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -19.50 | 3715           | 6198           | 9913                | 7132             | 5943             | -125.8             | 5817             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -20.00 | 3622           | 6432           | 10054               | 7233             | 6028             | -125.8             | 5902             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -20.50 | 3651           | 6622           | 10273               | 7391             | 6159             | -125.8             | 6033             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -21.00 | 4317           | 6770           | 11087               | 7976             | 6647             | -125.8             | 6521             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -21.50 | 5604           | 6941           | 12546               | 9026             | 7521             | -125.8             | 7395             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -22.00 | 6450           | 7202           | 13652               | 9821             | 8184             | -125.8             | 8059             | -125.8                 | 0.02 | -0.1             | -0.1             |
| -22.50 | 7612           | 7503           | 15115               | 10874            | 9062             | -125.8             | 8936             | -125.8                 | 0.01 | -0.1             | -0.1             |
| -23.00 | 8189           | 7839           | 16028               | 11531            | 9609             | -125.8             | 9483             | -125.8                 | 0.01 | -0.1             | -0.1             |
| -23.50 | 8832           | 8176           | 17008               | 12236            | 10197            | -125.8             | 10071            | -125.8                 | 0.01 | -0.1             | -0.1             |
| -24.00 | 8714           | 8529           | 17243               | 12405            | 10337            | -125.8             | 10212            | -125.8                 | 0.01 | -0.1             | -0.1             |
| -24.50 | 8026           | 8890           | 16916               | 12170            | 10142            | -125.8             | 10016            | -125.8                 | 0.01 | -0.1             | -0.1             |
| -25.00 | 7858           | 9252           | 17110               | 12309            | 10258            | -125.8             | 10132            | -125.8                 | 0.01 | -0.1             | -0.1             |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**SAMENVATTINGSTABEL MV Ø1016/1176 druk (n=1)**

**Uitgangspunten**

- paal : MV Ø1016/1176  
 - paaltype : Geheide in de grond gevormde betonpaal;terugheind  
 - schachtafmeting : 1096 mm  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{3(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Bewijkdraagvermogen  |                      |                      | Rekenwaarden      |                    |                         |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            |                    |                    | $R_{e,real}$<br>[kN] | $R_{b,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{c;d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40               | -10.00             | 3968.0               | 4351.2               | 8319.2               | 4987.6            | -22.1              | 4965.5                  |
|            |                    | -10.50             | 3775.9               | 4692.7               | 8468.5               | 5077.1            | -22.1              | 5055.0                  |
|            |                    | -11.00             | 3631.7               | 5054.2               | 8685.9               | 5207.4            | -22.1              | 5185.3                  |
|            |                    | -11.50             | 2806.5               | 5415.7               | 8222.3               | 4929.4            | -22.1              | 4907.3                  |
|            |                    | -12.00             | 2539.7               | 5777.3               | 8317.0               | 4986.2            | -22.1              | 4964.1                  |
|            |                    | -12.50             | 2227.0               | 6138.8               | 8365.8               | 5015.5            | -22.1              | 4993.4                  |
|            |                    | -13.00             | 1980.3               | 6498.7               | 8479.0               | 5083.3            | -22.1              | 5061.2                  |
|            |                    | -13.50             | 1879.6               | 6717.8               | 8597.3               | 5154.3            | -22.1              | 5132.2                  |
|            |                    | -14.00             | 1976.8               | 6823.1               | 8799.9               | 5275.7            | -22.1              | 5253.6                  |
|            |                    | -14.50             | 2117.2               | 6934.3               | 9051.4               | 5426.5            | -22.1              | 5404.4                  |
|            |                    | -15.00             | 2167.1               | 7106.3               | 9273.4               | 5559.6            | -22.1              | 5537.5                  |
|            |                    | -15.50             | 2260.6               | 7354.4               | 9614.9               | 5764.3            | -22.1              | 5742.2                  |
|            |                    | -16.00             | 2640.3               | 7454.0               | 10094.3              | 6051.7            | -22.1              | 6029.6                  |
|            |                    | -16.50             | 2785.6               | 7640.1               | 10425.7              | 6250.4            | -22.1              | 6228.3                  |
|            |                    | -17.00             | 3009.9               | 7797.2               | 10807.1              | 6479.1            | -22.1              | 6457.0                  |
|            |                    | -17.50             | 3086.1               | 7987.3               | 11073.4              | 6638.7            | -22.1              | 6616.6                  |
|            |                    | -18.00             | 3135.1               | 8184.4               | 11319.5              | 6786.2            | -22.1              | 6764.2                  |
|            |                    | -18.50             | 3347.7               | 8371.7               | 11719.4              | 7026.0            | -22.1              | 7003.9                  |
|            |                    | -19.00             | 3915.3               | 8553.7               | 12469.0              | 7475.4            | -22.1              | 7453.3                  |
|            |                    | -19.50             | 4224.4               | 8770.6               | 12995.0              | 7790.8            | -22.1              | 7768.7                  |
|            |                    | -20.00             | 4736.5               | 8985.4               | 13721.9              | 8226.6            | -22.1              | 8204.5                  |
|            |                    | -20.50             | 4922.4               | 9238.4               | 14160.8              | 8489.7            | -22.1              | 8467.6                  |
|            |                    | -21.00             | 5104.9               | 9505.8               | 14610.6              | 8759.4            | -22.1              | 8737.3                  |
|            |                    | -21.50             | 5497.7               | 9763.5               | 15261.2              | 9149.4            | -22.1              | 9127.3                  |
|            |                    | -22.00             | 5120.8               | 10033.2              | 15153.9              | 9085.1            | -22.1              | 9063.0                  |
| -22.50     | 5253.0             | 10311.9            | 15564.9              | 9331.5               | -22.1                | 9309.4            |                    |                         |
| -23.00     | 5379.7             | 10598.9            | 15978.6              | 9579.5               | -22.1                | 9557.4            |                    |                         |
| -23.50     | 5509.6             | 10884.3            | 16393.9              | 9828.5               | -22.1                | 9806.4            |                    |                         |
| -24.00     | 5629.3             | 11173.5            | 16802.9              | 10073.7              | -22.1                | 10051.6           |                    |                         |
| -24.50     | 5752.9             | 11462.6            | 17215.6              | 10321.1              | -22.1                | 10299.0           |                    |                         |
| -25.00     | 5798.2             | 11763.0            | 17561.1              | 10528.3              | -22.1                | 10506.2           |                    |                         |
| 19-1008-15 | 0.75               | -10.00             | 7651.5               | 4745.8               | 12397.4              | 7432.5            | -8.0               | 7424.5                  |
|            |                    | -10.50             | 7883.3               | 5107.4               | 12990.7              | 7788.2            | -8.0               | 7780.2                  |
|            |                    | -11.00             | 7869.7               | 5468.9               | 13338.6              | 7996.7            | -8.0               | 7988.8                  |
|            |                    | -11.50             | 7843.4               | 5830.4               | 13673.9              | 8197.8            | -8.0               | 8189.8                  |
|            |                    | -12.00             | 4515.3               | 6192.0               | 10707.3              | 6419.2            | -8.0               | 6411.2                  |
|            |                    | -12.50             | 3893.7               | 6553.5               | 10447.2              | 6263.3            | -8.0               | 6255.3                  |
|            |                    | -13.00             | 3492.6               | 6909.1               | 10401.6              | 6236.0            | -8.0               | 6228.0                  |
|            |                    | -13.50             | 3340.4               | 7224.5               | 10564.9              | 6333.9            | -8.0               | 6325.9                  |
|            |                    | -14.00             | 2655.1               | 7586.0               | 10241.1              | 6139.7            | -8.0               | 6131.7                  |
|            |                    | -14.50             | 2139.4               | 7947.5               | 10086.9              | 6047.3            | -8.0               | 6039.3                  |
|            |                    | -15.00             | 1651.8               | 8309.1               | 9960.9               | 5971.8            | -8.0               | 5963.8                  |
|            |                    | -15.50             | 1179.6               | 8670.6               | 9850.2               | 5905.4            | -8.0               | 5897.4                  |
|            |                    | -16.00             | 826.7                | 9029.1               | 9855.8               | 5908.8            | -8.0               | 5900.8                  |
|            |                    | -16.50             | 899.0                | 9116.3               | 10015.3              | 6004.4            | -8.0               | 5996.4                  |
|            |                    | -17.00             | 798.5                | 9155.6               | 9954.1               | 5967.7            | -8.0               | 5959.7                  |
|            |                    | -17.50             | 783.8                | 9215.3               | 9999.2               | 5994.7            | -8.0               | 5986.7                  |
|            |                    | -18.00             | 671.9                | 9316.7               | 9988.6               | 5988.4            | -8.0               | 5980.4                  |
|            |                    | -18.50             | 679.4                | 9343.3               | 10022.7              | 6008.8            | -8.0               | 6000.8                  |
|            |                    | -19.00             | 693.8                | 9371.6               | 10065.4              | 6034.4            | -8.0               | 6026.4                  |
|            |                    | -19.50             | 749.7                | 9405.4               | 10155.1              | 6088.2            | -8.0               | 6080.2                  |
|            |                    | -20.00             | 1088.1               | 9440.3               | 10528.4              | 6312.0            | -8.0               | 6304.0                  |
|            |                    | -20.50             | 2028.9               | 9487.2               | 11516.1              | 6904.1            | -8.0               | 6896.1                  |
|            |                    | -21.00             | 2351.8               | 9597.5               | 11949.3              | 7163.8            | -8.0               | 7155.8                  |
|            |                    | -21.50             | 2430.8               | 9752.7               | 12183.5              | 7304.2            | -8.0               | 7296.3                  |
|            |                    | -22.00             | 2901.2               | 9908.0               | 12809.2              | 7679.4            | -8.0               | 7671.4                  |
| -22.50     | 3197.9             | 10069.7            | 13267.7              | 7954.2               | -8.0                 | 7946.2            |                    |                         |
| -23.00     | 3205.2             | 10268.8            | 13474.0              | 8077.9               | -8.0                 | 8069.9            |                    |                         |
| -23.50     | 3281.2             | 10505.9            | 13787.1              | 8265.7               | -8.0                 | 8257.7            |                    |                         |
| -24.00     | 3383.7             | 10717.9            | 14101.6              | 8454.2               | -8.0                 | 8446.2            |                    |                         |
| -24.50     | 3374.5             | 10987.6            | 14362.1              | 8610.4               | -8.0                 | 8602.4            |                    |                         |
| -25.00     | 3220.6             | 11260.4            | 14481.0              | 8681.7               | -8.0                 | 8673.7            |                    |                         |
| 251.S01    | -1.05              | -10.00             | 2482.4               | 2703.9               | 5186.4               | 3109.3            | -42.8              | 3066.5                  |
|            |                    | -10.50             | 2360.7               | 2988.8               | 5349.5               | 3207.1            | -42.8              | 3164.3                  |
|            |                    | -11.00             | 2231.3               | 3205.2               | 5436.5               | 3259.3            | -42.8              | 3216.4                  |
|            |                    | -11.50             | 2422.3               | 3336.7               | 5759.0               | 3452.7            | -42.8              | 3409.8                  |
|            |                    | -12.00             | 2588.7               | 3467.2               | 6055.9               | 3630.7            | -42.8              | 3587.8                  |
|            |                    | -12.50             | 2689.4               | 3689.3               | 6378.7               | 3824.2            | -42.8              | 3781.3                  |
|            |                    | -13.00             | 2724.1               | 3951.8               | 6675.9               | 4002.4            | -42.8              | 3959.5                  |
|            |                    | -13.50             | 2818.9               | 4199.1               | 7018.1               | 4207.5            | -42.8              | 4164.6                  |
|            |                    | -14.00             | 2644.9               | 4543.1               | 7188.0               | 4309.4            | -42.8              | 4266.5                  |
|            |                    | -14.50             | 2250.2               | 4884.8               | 7135.0               | 4277.6            | -42.8              | 4234.7                  |
|            |                    | -15.00             | 2737.8               | 5193.7               | 7931.4               | 4755.0            | -42.8              | 4712.2                  |
|            |                    | -15.50             | 3946.9               | 5309.6               | 9256.5               | 5549.4            | -42.8              | 5506.6                  |
|            |                    | -16.00             | 4060.9               | 5643.3               | 9704.2               | 5817.9            | -42.8              | 5775.0                  |
|            |                    | -16.50             | 4078.1               | 6004.8               | 10083.0              | 6044.9            | -42.8              | 6002.1                  |
|            |                    | -17.00             | 2759.5               | 6362.3               | 9121.8               | 5468.7            | -42.8              | 5425.9                  |
| -17.50     | 2206.8             | 6703.5             | 8910.3               | 5341.9               | -42.8                | 5299.1            |                    |                         |
| -18.00     | 1943.6             | 7025.9             | 8969.4               | 5377.4               | -42.8                | 5334.5            |                    |                         |
| -18.50     | 2067.7             | 7328.7             | 9396.3               | 5633.3               | -42.8                | 5590.5            |                    |                         |
| -19.00     | 1647.2             | 7468.1             | 9115.4               | 5464.8               | -42.8                | 5422.0            |                    |                         |
| -19.50     | 1624.0             | 7668.2             | 9292.2               | 5570.9               | -42.8                | 5528.0            |                    |                         |
| -20.00     | 1499.2             | 7949.2             | 9448.5               | 5664.5               | -42.8                | 5621.7            |                    |                         |
| -20.50     | 1190.1             | 8250.9             | 9440.9               | 5660.0               | -42.8                | 5617.2            |                    |                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                     |                         |       |        |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|---------------------|-------------------------|-------|--------|
|           |                    |                    | $R_{b,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{o,real}$<br>[kN] | $R_{b;d}$<br>[kN] | $F_{b;k;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |       |        |
| 251.S01   | -1.05              | -21.00             | 932.8                | 8517.0               | 9449.9               | 5665.4            | -42.8               | 5622.5                  |       |        |
|           |                    | -21.50             | 845.6                | 8627.5               | 9473.1               | 5679.3            | -42.8               | 5636.5                  |       |        |
|           |                    | -22.00             | 849.7                | 8662.0               | 9511.7               | 5702.5            | -42.8               | 5659.6                  |       |        |
|           |                    | -22.50             | 1132.0               | 8707.7               | 9839.7               | 5899.1            | -42.8               | 5856.3                  |       |        |
|           |                    | -23.00             | 1500.0               | 8781.0               | 10281.0              | 6163.7            | -42.8               | 6120.8                  |       |        |
|           |                    | -23.50             | 1628.1               | 8876.8               | 10504.9              | 6297.9            | -42.8               | 6255.0                  |       |        |
|           |                    | -24.00             | 1628.3               | 9006.5               | 10634.9              | 6375.8            | -42.8               | 6333.0                  |       |        |
|           |                    | -24.50             | 2068.0               | 9124.6               | 11192.6              | 6710.2            | -42.8               | 6667.4                  |       |        |
|           |                    | -25.00             | 2964.5               | 9231.9               | 12196.4              | 7312.0            | -42.8               | 7269.2                  |       |        |
|           |                    | 19-1008-22         | 0.18                 | -10.00               | 3798.1               | 3138.3            | 6936.4              | 4158.5                  | -44.7 | 4113.8 |
|           |                    |                    |                      | -10.50               | 3163.3               | 3439.7            | 6603.0              | 3958.6                  | -44.7 | 3913.9 |
| -11.00    | 3139.5             |                    |                      | 3740.0               | 6879.6               | 4124.4            | -44.7               | 4079.7                  |       |        |
| -11.50    | 3022.4             |                    |                      | 4039.9               | 7062.2               | 4234.0            | -44.7               | 4189.2                  |       |        |
| -12.00    | 2383.0             |                    |                      | 4224.1               | 6607.1               | 3961.1            | -44.7               | 3916.3                  |       |        |
| -12.50    | 1939.5             |                    |                      | 4388.5               | 6328.0               | 3793.8            | -44.7               | 3749.0                  |       |        |
| -13.00    | 1708.4             |                    |                      | 4565.1               | 6273.5               | 3761.1            | -44.7               | 3716.3                  |       |        |
| -13.50    | 1619.2             |                    |                      | 4773.4               | 6392.5               | 3832.4            | -44.7               | 3787.7                  |       |        |
| -14.00    | 1572.7             |                    |                      | 4952.8               | 6525.6               | 3912.2            | -44.7               | 3867.5                  |       |        |
| -14.50    | 1528.2             |                    |                      | 5109.5               | 6637.7               | 3979.4            | -44.7               | 3934.7                  |       |        |
| -15.00    | 1521.5             |                    |                      | 5220.2               | 6741.7               | 4041.8            | -44.7               | 3997.0                  |       |        |
| -15.50    | 1380.6             |                    |                      | 5399.9               | 6780.4               | 4065.0            | -44.7               | 4020.3                  |       |        |
| -16.00    | 1245.5             |                    |                      | 5544.8               | 6790.3               | 4070.9            | -44.7               | 4026.2                  |       |        |
| -16.50    | 1185.2             |                    |                      | 5629.2               | 6814.4               | 4085.4            | -44.7               | 4040.6                  |       |        |
| -17.00    | 1172.3             |                    |                      | 5695.2               | 6867.6               | 4117.2            | -44.7               | 4072.5                  |       |        |
| -17.50    | 1991.8             |                    |                      | 5738.6               | 7730.4               | 4634.6            | -44.7               | 4589.8                  |       |        |
| -18.00    | 2957.5             |                    |                      | 5812.1               | 8769.6               | 5257.6            | -44.7               | 5212.8                  |       |        |
| -18.50    | 3036.0             |                    |                      | 6025.0               | 9061.1               | 5432.3            | -44.7               | 5387.6                  |       |        |
| -19.00    | 3130.1             |                    |                      | 6230.3               | 9360.4               | 5611.8            | -44.7               | 5567.0                  |       |        |
| -19.50    | 3312.7             |                    |                      | 6408.4               | 9721.0               | 5828.0            | -44.7               | 5783.2                  |       |        |
| -20.00    | 3538.0             |                    |                      | 6608.3               | 10146.3              | 6082.9            | -44.7               | 6038.2                  |       |        |
| -20.50    | 3585.1             | 6881.8             | 10466.9              | 6275.1               | -44.7                | 6230.4            |                     |                         |       |        |
| -21.00    | 3804.1             | 7070.1             | 10874.2              | 6519.3               | -44.7                | 6474.6            |                     |                         |       |        |
| -21.50    | 3860.6             | 7325.6             | 11186.2              | 6706.3               | -44.7                | 6661.6            |                     |                         |       |        |
| -22.00    | 3673.2             | 7610.5             | 11283.7              | 6764.8               | -44.7                | 6720.1            |                     |                         |       |        |
| -22.50    | 4075.4             | 7807.9             | 11883.3              | 7124.3               | -44.7                | 7079.5            |                     |                         |       |        |
| -23.00    | 4451.3             | 8008.2             | 12459.5              | 7469.7               | -44.7                | 7425.0            |                     |                         |       |        |
| -23.50    | 4705.1             | 8240.6             | 12945.7              | 7761.2               | -44.7                | 7716.5            |                     |                         |       |        |
| -24.00    | 5228.0             | 8470.5             | 13698.5              | 8212.5               | -44.7                | 8167.8            |                     |                         |       |        |
| -24.50    | 5718.0             | 8724.5             | 14442.5              | 8658.6               | -44.7                | 8613.9            |                     |                         |       |        |
| -25.00    | 5648.1             | 8994.8             | 14643.0              | 8778.8               | -44.7                | 8734.0            |                     |                         |       |        |
| 202.S03   | 0.03               | -10.00             | 2967.6               | 2574.0               | 5541.7               | 3322.3            | -125.8              | 3196.5                  |       |        |
|           |                    | -10.50             | 2762.5               | 2935.5               | 5698.1               | 3416.1            | -125.8              | 3290.3                  |       |        |
|           |                    | -11.00             | 2646.9               | 3268.3               | 5915.3               | 3546.3            | -125.8              | 3420.5                  |       |        |
|           |                    | -11.50             | 2416.3               | 3557.6               | 5973.8               | 3581.4            | -125.8              | 3455.6                  |       |        |
|           |                    | -12.00             | 1358.0               | 3846.3               | 5204.2               | 3120.0            | -125.8              | 2994.2                  |       |        |
|           |                    | -12.50             | 1401.8               | 3928.0               | 5329.7               | 3195.3            | -125.8              | 3069.5                  |       |        |
|           |                    | -13.00             | 1960.8               | 4020.6               | 5981.4               | 3585.9            | -125.8              | 3460.1                  |       |        |
|           |                    | -13.50             | 2318.2               | 4095.6               | 6413.8               | 3845.2            | -125.8              | 3719.4                  |       |        |
|           |                    | -14.00             | 2566.4               | 4262.3               | 6828.7               | 4094.0            | -125.8              | 3968.2                  |       |        |
|           |                    | -14.50             | 2661.6               | 4411.6               | 7073.1               | 4240.5            | -125.8              | 4114.7                  |       |        |
|           |                    | -15.00             | 2679.2               | 4590.4               | 7269.5               | 4358.2            | -125.8              | 4232.4                  |       |        |
|           |                    | -15.50             | 2720.1               | 4748.5               | 7468.6               | 4477.6            | -125.8              | 4351.8                  |       |        |
|           |                    | -16.00             | 2825.1               | 4901.6               | 7726.7               | 4632.3            | -125.8              | 4506.5                  |       |        |
|           |                    | -16.50             | 3112.7               | 5038.1               | 8150.7               | 4886.5            | -125.8              | 4760.7                  |       |        |
|           |                    | -17.00             | 3368.8               | 5192.3               | 8561.1               | 5132.5            | -125.8              | 5006.7                  |       |        |
|           |                    | -17.50             | 3478.7               | 5359.5               | 8838.2               | 5298.7            | -125.8              | 5172.9                  |       |        |
|           |                    | -18.00             | 3538.3               | 5560.8               | 9099.1               | 5455.1            | -125.8              | 5329.3                  |       |        |
|           |                    | -18.50             | 3626.2               | 5752.9               | 9379.0               | 5622.9            | -125.8              | 5497.1                  |       |        |
|           |                    | -19.00             | 3676.2               | 5976.1               | 9652.3               | 5786.8            | -125.8              | 5660.9                  |       |        |
|           |                    | -19.50             | 3714.8               | 6198.5               | 9913.2               | 5943.2            | -125.8              | 5817.4                  |       |        |
|           |                    | -20.00             | 3622.0               | 6431.9               | 10053.9              | 6027.5            | -125.8              | 5901.7                  |       |        |
| -20.50    | 3651.3             | 6621.9             | 10273.1              | 6158.9               | -125.8               | 6033.1            |                     |                         |       |        |
| -21.00    | 4316.8             | 6769.9             | 11086.8              | 6646.7               | -125.8               | 6520.9            |                     |                         |       |        |
| -21.50    | 5604.2             | 6941.4             | 12545.5              | 7521.3               | -125.8               | 7395.5            |                     |                         |       |        |
| -22.00    | 6449.8             | 7201.9             | 13651.7              | 8184.5               | -125.8               | 8058.7            |                     |                         |       |        |
| -22.50    | 7611.9             | 7503.0             | 15114.9              | 9061.7               | -125.8               | 8935.9            |                     |                         |       |        |
| -23.00    | 8188.8             | 7839.3             | 16028.1              | 9609.2               | -125.8               | 9483.4            |                     |                         |       |        |
| -23.50    | 8832.1             | 8176.1             | 17008.2              | 10196.8              | -125.8               | 10071.0           |                     |                         |       |        |
| -24.00    | 8714.1             | 8528.7             | 17242.8              | 10337.4              | -125.8               | 10211.6           |                     |                         |       |        |
| -24.50    | 8025.9             | 8890.3             | 16916.2              | 10141.6              | -125.8               | 10015.8           |                     |                         |       |        |
| -25.00    | 7858.3             | 9251.8             | 17110.1              | 10257.9              | -125.8               | 10132.0           |                     |                         |       |        |

**PAALGEGEVENS SI Ø508/670**

Type : In de grond gevormde geschroefde paal; groutinjectie  
 Wijze van installeren : Schroeven  
 Wijze van terugwinnen : n.v.t.  
 Diameter [m] : 0.590  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j;k}$  : 1.00  
 Groutomhulling : JA

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**PAALGEGEVENS SI Ø610/850**

Type : In de grond gevormde geschroefde paal; groutinjectie  
 Wijze van installeren : Schroeven  
 Wijze van terugwinnen : n.v.t.  
 Diameter [m] : 0.730  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00  
 Groutomhulling : JA

**PAALGEGEVENS SI Ø762/950**

Type : In de grond gevormde geschroefde paal; groutinjectie  
 Wijze van installeren : Schroeven  
 Wijze van terugwinnen : n.v.t.  
 Diameter [m] : 0.860  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00  
 Groutomhulling : JA

**PAALGEGEVENS MV Ø914/1074**

Type : Geheide in de grond gevormde betonpaal;terugheidend  
 Wijze van installeren : Heien  
 Wijze van terugwinnen : Heien  
 Diameter [m] : 0.994  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00

**PAALGEGEVENS MV Ø1016/1176**

Type : Geheide in de grond gevormde betonpaal;terugheidend  
 Wijze van installeren : Heien  
 Wijze van terugwinnen : Heien  
 Diameter [m] : 1.096  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00



Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**OVERZICHT NETTO DRAAGVERMOGEN DRUKPALEN**

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maalveld<br>niveau | paalpunt<br>niveau | R <sub>netto;d</sub> [kN] |           |           |           |           |  |
|------------|--------------------|--------------------|---------------------------|-----------|-----------|-----------|-----------|--|
|            |                    |                    | SI Ø508/6                 | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |  |
| 19-1008-14 | 0.40               | -6.00              | 1302                      |           |           |           |           |  |
|            |                    | -6.50              | 1472                      |           |           |           |           |  |
|            |                    | -7.00              | 1599                      | 2233      |           |           |           |  |
|            |                    | -7.50              | 1753                      | 2368      |           |           |           |  |
|            |                    | -8.00              | 1837                      | 2526      | 3239      |           |           |  |
|            |                    | -8.50              | 1960                      | 2678      | 3430      |           |           |  |
|            |                    | -9.00              | 2080                      | 2818      | 3593      |           |           |  |
|            |                    | -9.50              | 2159                      | 2961      | 3760      |           |           |  |
|            |                    | -10.00             | 2546                      | 3509      | 3066      | 4474      | 4965      |  |
|            |                    | -10.50             | 2577                      | 2551      | 2825      | 4437      | 5054      |  |
|            |                    | -11.00             | 2052                      | 2268      | 2732      | 4493      | 5185      |  |
|            |                    | -11.50             | 1727                      | 2199      | 2736      | 4606      | 4907      |  |
|            |                    | -12.00             | 1667                      | 2192      | 2758      | 4362      | 4964      |  |
|            |                    | -12.50             | 1674                      | 2202      | 2573      | 4415      | 4993      |  |
|            |                    | -13.00             | 1674                      | 2127      | 2605      | 4489      | 5061      |  |
|            |                    | -13.50             | 1660                      | 2136      | 2593      | 4532      | 5132      |  |
|            |                    | -14.00             | 1720                      | 2219      | 2713      | 4664      | 5253      |  |
|            |                    | -14.50             | 1765                      | 2282      | 2794      | 4794      | 5404      |  |
|            |                    | -15.00             | 1809                      | 2338      | 2863      | 4912      | 5537      |  |
|            |                    | -15.50             | 1765                      | 2317      | 2887      | 5047      | 5742      |  |
|            |                    | -16.00             | 1958                      | 2543      | 3127      | 5335      | 6029      |  |
|            |                    | -16.50             | 1998                      | 2590      | 3197      | 5485      | 6228      |  |
|            |                    | -17.00             | 2104                      | 2735      | 3366      | 5711      | 6457      |  |
|            |                    | -17.50             | 2166                      | 2812      | 3456      | 5856      | 6616      |  |
|            |                    | -18.00             | 2226                      | 2884      | 3539      | 5991      | 6764      |  |
| -18.50     | 2284               | 2954               | 3619                      | 6157      | 7003      |           |           |  |
| -19.00     | 2446               | 3185               | 3925                      | 6585      | 7453      |           |           |  |
| -19.50     | 2534               | 3299               | 4072                      | 6838      | 7768      |           |           |  |
| -20.00     | 2696               | 3523               | 4351                      | 7238      | 8204      |           |           |  |
| -20.50     | 2801               | 3651               | 4504                      | 7475      | 8467      |           |           |  |
| -21.00     | 2881               | 3767               | 4646                      | 7709      | 8737      |           |           |  |
| -21.50     | 2996               | 3954               | 4882                      | 8059      | 9127      |           |           |  |
| -22.00     | 3101               | 4095               | 5067                      | 8351      | 9062      |           |           |  |
| -22.50     | 3201               | 4227               | 5237                      | 8244      | 9309      |           |           |  |
| -23.00     | 3295               | 4332               | 5103                      | 8468      | 9557      |           |           |  |
| -23.50     | 3373               | 4201               | 5217                      | 8694      | 9806      |           |           |  |
| -24.00     | 3265               | 4292               | 5325                      | 8902      | 10051     |           |           |  |
| -24.50     | 3326               | 4381               | 5431                      | 9092      | 10298     |           |           |  |
| -25.00     | 3384               | 4465               | 5530                      | 9271      | 10506     |           |           |  |
| 19-1008-15 | 0.75               | -6.00              | 797                       |           |           |           |           |  |
|            |                    | -6.50              | 1381                      |           |           |           |           |  |
|            |                    | -7.00              | 1448                      | 2029      |           |           |           |  |
|            |                    | -7.50              | 1549                      | 2153      |           |           |           |  |
|            |                    | -8.00              | 1628                      | 2274      | 2987      |           |           |  |
|            |                    | -8.50              | 1892                      | 2639      | 3463      |           |           |  |
|            |                    | -9.00              | 2161                      | 2981      | 3847      |           |           |  |
|            |                    | -9.50              | 2291                      | 3135      | 4025      |           |           |  |
|            |                    | -10.00             | 2533                      | 3405      | 4103      | 6409      | 7424      |  |
|            |                    | -10.50             | 2753                      | 3366      | 4293      | 6729      | 7780      |  |
|            |                    | -11.00             | 2580                      | 3480      | 4414      | 6928      | 7988      |  |
|            |                    | -11.50             | 2635                      | 3588      | 4531      | 7121      | 8189      |  |
|            |                    | -12.00             | 2706                      | 3730      | 4696      | 7384      | 8411      |  |
|            |                    | -12.50             | 2729                      | 3768      | 4764      | 5694      | 6255      |  |
|            |                    | -13.00             | 2727                      | 3828      | 3595      | 5662      | 6227      |  |
|            |                    | -13.50             | 3281                      | 2953      | 3465      | 5645      | 6325      |  |
|            |                    | -14.00             | 2293                      | 2839      | 3402      | 5639      | 6131      |  |
|            |                    | -14.50             | 2186                      | 2755      | 3328      | 5442      | 6039      |  |
|            |                    | -15.00             | 2122                      | 2704      | 3145      | 5370      | 5963      |  |
|            |                    | -15.50             | 2092                      | 2565      | 3057      | 5315      | 5897      |  |
|            |                    | -16.00             | 2019                      | 2526      | 3013      | 5312      | 5900      |  |
|            |                    | -16.50             | 2031                      | 2554      | 3055      | 5392      | 5996      |  |
|            |                    | -17.00             | 2050                      | 2542      | 3033      | 5364      | 5959      |  |
|            |                    | -17.50             | 2034                      | 2552      | 3046      | 5389      | 5986      |  |
|            |                    | -18.00             | 2035                      | 2550      | 3038      | 5388      | 5980      |  |
| -18.50     | 2044               | 2560               | 3050                      | 5408      | 6000      |           |           |  |
| -19.00     | 2051               | 2570               | 3062                      | 5427      | 6026      |           |           |  |
| -19.50     | 2065               | 2588               | 3086                      | 5473      | 6080      |           |           |  |
| -20.00     | 2094               | 2650               | 3180                      | 5632      | 6303      |           |           |  |
| -20.50     | 2232               | 2880               | 3513                      | 6134      | 6896      |           |           |  |
| -21.00     | 2369               | 3035               | 3690                      | 6374      | 7155      |           |           |  |
| -21.50     | 2424               | 3103               | 3770                      | 6499      | 7296      |           |           |  |
| -22.00     | 2504               | 3235               | 3956                      | 6807      | 7671      |           |           |  |
| -22.50     | 2660               | 3441               | 4137                      | 7061      | 7946      |           |           |  |
| -23.00     | 2786               | 3484               | 4250                      | 7178      | 8069      |           |           |  |
| -23.50     | 2784               | 3579               | 4363                      | 7348      | 8257      |           |           |  |
| -24.00     | 2838               | 3632               | 4419                      | 7519      | 8446      |           |           |  |
| -24.50     | 2898               | 3709               | 4505                      | 7665      | 8602      |           |           |  |
| -25.00     | 2940               | 3752               | 4544                      | 7742      | 8673      |           |           |  |
| 251.S01    | -1.05              | -6.00              | 621                       |           |           |           |           |  |
|            |                    | -6.50              | 526                       |           |           |           |           |  |
|            |                    | -7.00              | 556                       | 751       |           |           |           |  |
|            |                    | -7.50              | 553                       | 728       |           |           |           |  |
|            |                    | -8.00              | 557                       | 720       | 879       |           |           |  |
|            |                    | -8.50              | 541                       | 709       | 924       |           |           |  |
|            |                    | -9.00              | 788                       | 1110      | 1484      |           |           |  |
|            |                    | -9.50              | 921                       | 1242      | 1582      |           |           |  |
|            |                    | -10.00             | 979                       | 1319      | 1671      | 2669      | 3066      |  |
|            |                    | -10.50             | 1029                      | 1371      | 1722      | 2768      | 3164      |  |
|            |                    | -11.00             | 1062                      | 1401      | 1746      | 2822      | 3216      |  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld paalpunt |        | R <sub>netto;d</sub> [kN] |           |           |           |           |
|------------|-------------------|--------|---------------------------|-----------|-----------|-----------|-----------|
|            | niveau            | niveau | SI Ø508/6                 | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |
|            | -11.50            | 1120   | 1476                      | 1845      | 2977      |           | 3409      |
|            | -12.00            | 1315   | 1758                      | 1926      | 3130      |           | 3587      |
|            | -12.50            | 1403   | 1615                      | 2029      | 3301      |           | 3781      |
|            | -13.00            | 1280   | 1701                      | 2133      | 3462      |           | 3959      |
|            | -13.50            | 1344   | 1782                      | 2230      | 3645      |           | 4164      |
|            | -14.00            | 1386   | 1831                      | 2279      | 3747      |           | 4266      |
|            | -14.50            | 1391   | 1828                      | 2253      | 3739      |           | 4234      |
|            | -15.00            | 1353   | 1790                      | 2308      | 4022      |           | 4712      |
|            | -15.50            | 1938   | 2678                      | 3030      | 4793      |           | 5506      |
|            | -16.00            | 2161   | 2507                      | 3115      | 5053      |           | 5775      |
|            | -16.50            | 1961   | 2569                      | 3242      | 5263      |           | 6002      |
|            | -17.00            | 2011   | 2685                      | 3360      | 5474      |           | 5425      |
|            | -17.50            | 2088   | 2754                      | 3431      | 4761      |           | 5299      |
|            | -18.00            | 2111   | 2763                      | 2925      | 4787      |           | 5334      |
|            | -18.50            | 2101   | 2464                      | 2960      | 4965      |           | 5590      |
|            | -19.00            | 2012   | 2507                      | 2946      | 4864      |           | 5422      |
|            | -19.50            | 1970   | 2482                      | 2966      | 4922      |           | 5528      |
|            | -20.00            | 1973   | 2478                      | 2978      | 5020      |           | 5621      |
|            | -20.50            | 1980   | 2505                      | 3011      | 5034      |           | 5617      |
|            | -21.00            | 2026   | 2550                      | 3051      | 5052      |           | 5622      |
|            | -21.50            | 2048   | 2573                      | 3074      | 5069      |           | 5636      |
|            | -22.00            | 2061   | 2589                      | 3092      | 5090      |           | 5659      |
|            | -22.50            | 2099   | 2675                      | 3208      | 5254      |           | 5856      |
|            | -23.00            | 2161   | 2725                      | 3289      | 5427      |           | 6120      |
|            | -23.50            | 2255   | 2864                      | 3454      | 5592      |           | 6255      |
|            | -24.00            | 2305   | 2923                      | 3522      | 5669      |           | 6332      |
|            | -24.50            | 2353   | 3002                      | 3689      | 5948      |           | 6667      |
|            | -25.00            | 2529   | 3240                      | 3969      | 6375      |           | 7269      |
| 19-1008-22 | 0.18              | -6.00  | 745                       |           |           |           |           |
|            |                   | -6.50  | 994                       |           |           |           |           |
|            |                   | -7.00  | 1105                      | 1552      |           |           |           |
|            |                   | -7.50  | 1221                      | 1700      |           |           |           |
|            |                   | -8.00  | 1335                      | 1844      | 2374      |           |           |
|            |                   | -8.50  | 1447                      | 1981      | 2110      |           |           |
|            |                   | -9.00  | 1628                      | 1761      | 2197      |           |           |
|            |                   | -9.50  | 1396                      | 1827      | 2285      |           |           |
|            |                   | -10.00 | 1416                      | 1904      | 2393      | 3710      | 4113      |
|            |                   | -10.50 | 1448                      | 1992      | 2461      | 3653      | 3913      |
|            |                   | -11.00 | 1484                      | 2027      | 2409      | 3571      | 4079      |
|            |                   | -11.50 | 1489                      | 1958      | 2264      | 3682      | 4189      |
|            |                   | -12.00 | 1509                      | 1836      | 2320      | 3818      | 3916      |
|            |                   | -12.50 | 1396                      | 1874      | 2379      | 3562      | 3749      |
|            |                   | -13.00 | 1428                      | 1916      | 2162      | 3359      | 3716      |
|            |                   | -13.50 | 1456                      | 1769      | 2016      | 3363      | 3787      |
|            |                   | -14.00 | 1374                      | 1671      | 1990      | 3427      | 3867      |
|            |                   | -14.50 | 1322                      | 1650      | 2016      | 3491      | 3934      |
|            |                   | -15.00 | 1302                      | 1672      | 2049      | 3548      | 3997      |
|            |                   | -15.50 | 1312                      | 1686      | 2056      | 3576      | 4020      |
|            |                   | -16.00 | 1321                      | 1691      | 2055      | 3588      | 4026      |
|            |                   | -16.50 | 1329                      | 1698      | 2061      | 3604      | 4040      |
|            |                   | -17.00 | 1330                      | 1697      | 2056      | 3615      | 4072      |
|            |                   | -17.50 | 1396                      | 1816      | 2252      | 3981      | 4589      |
|            |                   | -18.00 | 1663                      | 2173      | 2707      | 4579      | 5212      |
|            |                   | -18.50 | 1713                      | 2255      | 2804      | 4737      | 5387      |
|            |                   | -19.00 | 1781                      | 2339      | 2904      | 4899      | 5567      |
|            |                   | -19.50 | 1856                      | 2437      | 3025      | 5089      | 5783      |
|            |                   | -20.00 | 1943                      | 2552      | 3168      | 5313      | 6038      |
|            |                   | -20.50 | 1955                      | 2581      | 3227      | 5472      | 6230      |
|            |                   | -21.00 | 2100                      | 2752      | 3410      | 5703      | 6474      |
|            |                   | -21.50 | 2175                      | 2842      | 3514      | 5874      | 6661      |
|            |                   | -22.00 | 2210                      | 2882      | 3546      | 5942      | 6720      |
|            |                   | -22.50 | 2299                      | 3009      | 3732      | 6241      | 7079      |
|            |                   | -23.00 | 2430                      | 3195      | 3944      | 6552      | 7424      |
|            |                   | -23.50 | 2495                      | 3301      | 4083      | 6798      | 7716      |
|            |                   | -24.00 | 2622                      | 3496      | 4352      | 7191      | 8167      |
|            |                   | -24.50 | 2735                      | 3636      | 4556      | 7536      | 8613      |
|            |                   | -25.00 | 2907                      | 3875      | 4869      | 7994      | 8734      |
| 202.S03    | 0.03              | -6.00  | 411                       |           |           |           |           |
|            |                   | -6.50  | 612                       |           |           |           |           |
|            |                   | -7.00  | 727                       | 1092      |           |           |           |
|            |                   | -7.50  | 1086                      | 1581      |           |           |           |
|            |                   | -8.00  | 1160                      | 1663      | 2205      |           |           |
|            |                   | -8.50  | 1244                      | 1820      | 2538      |           |           |
|            |                   | -9.00  | 1513                      | 2148      | 1940      |           |           |
|            |                   | -9.50  | 1599                      | 1526      | 1860      |           |           |
|            |                   | -10.00 | 1126                      | 1453      | 1765      | 2823      | 3196      |
|            |                   | -10.50 | 1084                      | 1397      | 1776      | 2857      | 3290      |
|            |                   | -11.00 | 1071                      | 1446      | 1799      | 3000      | 3420      |
|            |                   | -11.50 | 1061                      | 1407      | 1800      | 3019      | 3455      |
|            |                   | -12.00 | 956                       | 1255      | 1544      | 2660      | 2994      |
|            |                   | -12.50 | 989                       | 1289      | 1590      | 2719      | 3069      |
|            |                   | -13.00 | 1014                      | 1370      | 1756      | 3037      | 3460      |
|            |                   | -13.50 | 1172                      | 1556      | 1948      | 3256      | 3719      |
|            |                   | -14.00 | 1246                      | 1665      | 2087      | 3477      | 3968      |
|            |                   | -14.50 | 1306                      | 1732      | 2167      | 3604      | 4114      |
|            |                   | -15.00 | 1355                      | 1790      | 2233      | 3713      | 4232      |
|            |                   | -15.50 | 1403                      | 1848      | 2300      | 3823      | 4351      |
|            |                   | -16.00 | 1445                      | 1900      | 2369      | 3949      | 4506      |
|            |                   | -16.50 | 1536                      | 2022      | 2518      | 4173      | 4760      |
|            |                   | -17.00 | 1616                      | 2140      | 2686      | 4395      | 5006      |
|            |                   | -17.50 | 1738                      | 2299      | 2764      | 4544      | 5172      |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld paalpunt |        | R <sub>n,netto;d</sub> [kN] |           |           |           |           |
|-----------|-------------------|--------|-----------------------------|-----------|-----------|-----------|-----------|
|           | niveau            | niveau | SI Ø508/6                   | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |
|           | -18.00            |        | 1808                        | 2302      | 2858      | 4697      | 5329      |
|           | -18.50            |        | 1800                        | 2374      | 2946      | 4838      | 5497      |
|           | -19.00            |        | 1845                        | 2451      | 3037      | 4988      | 5660      |
|           | -19.50            |        | 1889                        | 2515      | 3123      | 5132      | 5817      |
|           | -20.00            |        | 1913                        | 2545      | 3166      | 5217      | 5901      |
|           | -20.50            |        | 1932                        | 2563      | 3204      | 5321      | 6033      |
|           | -21.00            |        | 2019                        | 2694      | 3404      | 5695      | 6520      |
|           | -21.50            |        | 2242                        | 3046      | 3895      | 6446      | 7395      |
|           | -22.00            |        | 2438                        | 3300      | 4208      | 6942      | 8058      |
|           | -22.50            |        | 2732                        | 3717      | 4935      | 7746      | 8935      |
|           | -23.00            |        | 2865                        | 3918      | 4997      | 8059      | 9483      |
|           | -23.50            |        | 3317                        | 4189      | 5369      | 8702      | 10070     |
|           | -24.00            |        | 3112                        | 4317      | 5589      | 9065      | 10211     |
|           | -24.50            |        | 3228                        | 4436      | 5668      | 8923      | 10015     |
|           | -25.00            |        | 3200                        | 4319      | 5567      | 8801      | 10132     |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

**OVERZICHT NETTO DRAAGVERMOGEN TREKPALEN (n=1)**

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maalveld<br>niveau | paalpunt<br>niveau | R <sub>d,netto,d</sub> [kN] |           |           |           |           |  |
|------------|--------------------|--------------------|-----------------------------|-----------|-----------|-----------|-----------|--|
|            |                    |                    | SI Ø508/6                   | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |  |
| 19-1008-14 | 0.40               | -6.00              | 231                         |           |           |           |           |  |
|            |                    | -6.50              | 270                         |           |           |           |           |  |
|            |                    | -7.00              | 311                         | 392       |           |           |           |  |
|            |                    | -7.50              | 352                         | 443       |           |           |           |  |
|            |                    | -8.00              | 395                         | 496       | 594       |           |           |  |
|            |                    | -8.50              | 441                         | 554       | 662       |           |           |  |
|            |                    | -9.00              | 487                         | 611       | 730       |           |           |  |
|            |                    | -9.50              | 529                         | 665       | 793       |           |           |  |
|            |                    | -10.00             | 570                         | 716       | 854       | 1301      | 1445      |  |
|            |                    | -10.50             | 614                         | 770       | 919       | 1400      | 1555      |  |
|            |                    | -11.00             | 660                         | 828       | 987       | 1505      | 1671      |  |
|            |                    | -11.50             | 706                         | 885       | 1055      | 1609      | 1787      |  |
|            |                    | -12.00             | 752                         | 943       | 1124      | 1713      | 1902      |  |
|            |                    | -12.50             | 798                         | 1000      | 1192      | 1818      | 2018      |  |
|            |                    | -13.00             | 844                         | 1057      | 1260      | 1922      | 2133      |  |
|            |                    | -13.50             | 873                         | 1094      | 1304      | 1988      | 2206      |  |
|            |                    | -14.00             | 892                         | 1117      | 1331      | 2024      | 2247      |  |
|            |                    | -14.50             | 908                         | 1137      | 1355      | 2059      | 2286      |  |
|            |                    | -15.00             | 930                         | 1166      | 1390      | 2112      | 2344      |  |
|            |                    | -15.50             | 962                         | 1206      | 1438      | 2185      | 2426      |  |
|            |                    | -16.00             | 976                         | 1224      | 1459      | 2217      | 2461      |  |
|            |                    | -16.50             | 1001                        | 1255      | 1496      | 2273      | 2524      |  |
|            |                    | -17.00             | 1022                        | 1281      | 1527      | 2321      | 2577      |  |
|            |                    | -17.50             | 1047                        | 1312      | 1565      | 2378      | 2641      |  |
|            |                    | -18.00             | 1073                        | 1345      | 1603      | 2437      | 2706      |  |
| -18.50     | 1097               | 1376               | 1640                        | 2493      | 2769      |           |           |  |
| -19.00     | 1121               | 1406               | 1677                        | 2548      | 2830      |           |           |  |
| -19.50     | 1149               | 1441               | 1719                        | 2613      | 2901      |           |           |  |
| -20.00     | 1177               | 1476               | 1761                        | 2676      | 2972      |           |           |  |
| -20.50     | 1210               | 1517               | 1810                        | 2751      | 3055      |           |           |  |
| -21.00     | 1245               | 1561               | 1861                        | 2829      | 3142      |           |           |  |
| -21.50     | 1278               | 1602               | 1911                        | 2905      | 3226      |           |           |  |
| -22.00     | 1313               | 1646               | 1962                        | 2984      | 3314      |           |           |  |
| -22.50     | 1349               | 1691               | 2016                        | 3066      | 3404      |           |           |  |
| -23.00     | 1386               | 1737               | 2071                        | 3150      | 3497      |           |           |  |
| -23.50     | 1422               | 1783               | 2125                        | 3233      | 3590      |           |           |  |
| -24.00     | 1459               | 1829               | 2180                        | 3317      | 3683      |           |           |  |
| -24.50     | 1497               | 1876               | 2236                        | 3402      | 3777      |           |           |  |
| -25.00     | 1535               | 1924               | 2293                        | 3489      | 3874      |           |           |  |
| 19-1008-15 | 0.75               | -6.00              | 302                         |           |           |           |           |  |
|            |                    | -6.50              | 320                         |           |           |           |           |  |
|            |                    | -7.00              | 357                         | 449       |           |           |           |  |
|            |                    | -7.50              | 394                         | 495       |           |           |           |  |
|            |                    | -8.00              | 432                         | 542       | 647       |           |           |  |
|            |                    | -8.50              | 470                         | 590       | 705       |           |           |  |
|            |                    | -9.00              | 516                         | 648       | 773       |           |           |  |
|            |                    | -9.50              | 563                         | 705       | 841       |           |           |  |
|            |                    | -10.00             | 609                         | 763       | 909       | 1384      | 1536      |  |
|            |                    | -10.50             | 655                         | 820       | 978       | 1488      | 1652      |  |
|            |                    | -11.00             | 701                         | 878       | 1046      | 1592      | 1768      |  |
|            |                    | -11.50             | 747                         | 935       | 1114      | 1697      | 1883      |  |
|            |                    | -12.00             | 793                         | 993       | 1182      | 1801      | 1999      |  |
|            |                    | -12.50             | 839                         | 1050      | 1250      | 1906      | 2115      |  |
|            |                    | -13.00             | 884                         | 1107      | 1318      | 2009      | 2228      |  |
|            |                    | -13.50             | 925                         | 1157      | 1378      | 2101      | 2330      |  |
|            |                    | -14.00             | 971                         | 1215      | 1446      | 2205      | 2446      |  |
|            |                    | -14.50             | 1017                        | 1272      | 1514      | 2309      | 2562      |  |
|            |                    | -15.00             | 1063                        | 1330      | 1582      | 2414      | 2677      |  |
|            |                    | -15.50             | 1109                        | 1387      | 1651      | 2518      | 2793      |  |
|            |                    | -16.00             | 1155                        | 1445      | 1719      | 2622      | 2908      |  |
|            |                    | -16.50             | 1167                        | 1460      | 1738      | 2651      | 2941      |  |
|            |                    | -17.00             | 1174                        | 1469      | 1748      | 2667      | 2958      |  |
|            |                    | -17.50             | 1183                        | 1480      | 1762      | 2688      | 2982      |  |
|            |                    | -18.00             | 1197                        | 1498      | 1784      | 2720      | 3018      |  |
| -18.50     | 1202               | 1505               | 1792                        | 2732      | 3032      |           |           |  |
| -19.00     | 1207               | 1511               | 1801                        | 2745      | 3046      |           |           |  |
| -19.50     | 1213               | 1519               | 1810                        | 2758      | 3062      |           |           |  |
| -20.00     | 1218               | 1527               | 1820                        | 2773      | 3078      |           |           |  |
| -20.50     | 1226               | 1536               | 1832                        | 2790      | 3098      |           |           |  |
| -21.00     | 1241               | 1556               | 1855                        | 2825      | 3137      |           |           |  |
| -21.50     | 1262               | 1582               | 1886                        | 2873      | 3190      |           |           |  |
| -22.00     | 1282               | 1608               | 1917                        | 2920      | 3243      |           |           |  |
| -22.50     | 1304               | 1635               | 1950                        | 2969      | 3298      |           |           |  |
| -23.00     | 1330               | 1668               | 1989                        | 3029      | 3364      |           |           |  |
| -23.50     | 1361               | 1706               | 2035                        | 3099      | 3442      |           |           |  |
| -24.00     | 1388               | 1741               | 2076                        | 3162      | 3512      |           |           |  |
| -24.50     | 1423               | 1785               | 2128                        | 3242      | 3600      |           |           |  |
| -25.00     | 1459               | 1829               | 2181                        | 3322      | 3689      |           |           |  |
| 251.S01    | -1.05              | -6.00              | 184                         |           |           |           |           |  |
|            |                    | -6.50              | 216                         |           |           |           |           |  |
|            |                    | -7.00              | 253                         | 322       |           |           |           |  |
|            |                    | -7.50              | 289                         | 367       |           |           |           |  |
|            |                    | -8.00              | 323                         | 409       | 492       |           |           |  |
|            |                    | -8.50              | 346                         | 437       | 526       |           |           |  |
|            |                    | -9.00              | 350                         | 444       | 534       |           |           |  |
|            |                    | -9.50              | 372                         | 471       | 566       |           |           |  |
|            |                    | -10.00             | 403                         | 510       | 613       | 894       | 998       |  |
|            |                    | -10.50             | 440                         | 556       | 668       | 977       | 1091      |  |
|            |                    | -11.00             | 468                         | 591       | 710       | 1042      | 1162      |  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

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 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld paalpunt |        | R <sub>n, netto;d</sub> [kN] |           |           |           |           |  |
|------------|-------------------|--------|------------------------------|-----------|-----------|-----------|-----------|--|
|            | niveau            | niveau | SI Ø508/6                    | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |  |
|            | -11.50            |        | 486                          | 614       | 737       | 1083      | 1208      |  |
|            | -12.00            |        | 504                          | 636       | 764       | 1124      | 1253      |  |
|            | -12.50            |        | 532                          | 672       | 807       | 1190      | 1326      |  |
|            | -13.00            |        | 566                          | 715       | 858       | 1267      | 1412      |  |
|            | -13.50            |        | 599                          | 755       | 905       | 1340      | 1493      |  |
|            | -14.00            |        | 642                          | 810       | 971       | 1439      | 1603      |  |
|            | -14.50            |        | 686                          | 864       | 1035      | 1538      | 1713      |  |
|            | -15.00            |        | 733                          | 923       | 1105      | 1633      | 1819      |  |
|            | -15.50            |        | 755                          | 951       | 1138      | 1674      | 1864      |  |
|            | -16.00            |        | 798                          | 1004      | 1202      | 1771      | 1971      |  |
|            | -16.50            |        | 844                          | 1062      | 1270      | 1876      | 2087      |  |
|            | -17.00            |        | 890                          | 1119      | 1337      | 1979      | 2202      |  |
|            | -17.50            |        | 933                          | 1173      | 1402      | 2078      | 2311      |  |
|            | -18.00            |        | 974                          | 1225      | 1463      | 2171      | 2415      |  |
|            | -18.50            |        | 1020                         | 1282      | 1531      | 2265      | 2518      |  |
|            | -19.00            |        | 1049                         | 1317      | 1574      | 2314      | 2573      |  |
|            | -19.50            |        | 1079                         | 1355      | 1619      | 2377      | 2643      |  |
|            | -20.00            |        | 1115                         | 1400      | 1672      | 2459      | 2734      |  |
|            | -20.50            |        | 1165                         | 1463      | 1746      | 2554      | 2839      |  |
|            | -21.00            |        | 1218                         | 1528      | 1824      | 2645      | 2940      |  |
|            | -21.50            |        | 1240                         | 1557      | 1858      | 2685      | 2984      |  |
|            | -22.00            |        | 1249                         | 1568      | 1871      | 2700      | 3002      |  |
|            | -22.50            |        | 1259                         | 1581      | 1888      | 2720      | 3024      |  |
|            | -23.00            |        | 1275                         | 1601      | 1911      | 2748      | 3056      |  |
|            | -23.50            |        | 1295                         | 1626      | 1942      | 2783      | 3095      |  |
|            | -24.00            |        | 1321                         | 1659      | 1981      | 2830      | 3147      |  |
|            | -24.50            |        | 1345                         | 1689      | 2018      | 2872      | 3194      |  |
|            | -25.00            |        | 1367                         | 1717      | 2051      | 2912      | 3238      |  |
| 19-1008-22 | 0.18              | -6.00  | 132                          |           |           |           |           |  |
|            |                   | -6.50  | 162                          |           |           |           |           |  |
|            |                   | -7.00  | 199                          | 254       |           |           |           |  |
|            |                   | -7.50  | 236                          | 300       |           |           |           |  |
|            |                   | -8.00  | 273                          | 347       | 417       |           |           |  |
|            |                   | -8.50  | 310                          | 393       | 473       |           |           |  |
|            |                   | -9.00  | 347                          | 439       | 527       |           |           |  |
|            |                   | -9.50  | 386                          | 487       | 585       |           |           |  |
|            |                   | -10.00 | 425                          | 536       | 642       | 972       | 1083      |  |
|            |                   | -10.50 | 463                          | 584       | 700       | 1060      | 1181      |  |
|            |                   | -11.00 | 502                          | 632       | 757       | 1148      | 1278      |  |
|            |                   | -11.50 | 540                          | 680       | 814       | 1235      | 1375      |  |
|            |                   | -12.00 | 565                          | 711       | 851       | 1291      | 1436      |  |
|            |                   | -12.50 | 586                          | 738       | 884       | 1341      | 1492      |  |
|            |                   | -13.00 | 610                          | 768       | 919       | 1394      | 1551      |  |
|            |                   | -13.50 | 637                          | 802       | 959       | 1456      | 1620      |  |
|            |                   | -14.00 | 661                          | 832       | 995       | 1510      | 1681      |  |
|            |                   | -14.50 | 682                          | 858       | 1026      | 1558      | 1734      |  |
|            |                   | -15.00 | 697                          | 877       | 1050      | 1593      | 1773      |  |
|            |                   | -15.50 | 721                          | 907       | 1085      | 1648      | 1834      |  |
|            |                   | -16.00 | 740                          | 932       | 1115      | 1692      | 1883      |  |
|            |                   | -16.50 | 752                          | 947       | 1133      | 1720      | 1914      |  |
|            |                   | -17.00 | 762                          | 959       | 1149      | 1743      | 1940      |  |
|            |                   | -17.50 | 769                          | 968       | 1160      | 1759      | 1959      |  |
|            |                   | -18.00 | 779                          | 982       | 1176      | 1784      | 1987      |  |
|            |                   | -18.50 | 807                          | 1017      | 1218      | 1848      | 2057      |  |
|            |                   | -19.00 | 834                          | 1051      | 1258      | 1909      | 2125      |  |
|            |                   | -19.50 | 857                          | 1080      | 1294      | 1963      | 2185      |  |
|            |                   | -20.00 | 884                          | 1113      | 1333      | 2023      | 2252      |  |
|            |                   | -20.50 | 919                          | 1157      | 1385      | 2103      | 2341      |  |
|            |                   | -21.00 | 944                          | 1188      | 1422      | 2159      | 2403      |  |
|            |                   | -21.50 | 977                          | 1230      | 1472      | 2234      | 2487      |  |
|            |                   | -22.00 | 1013                         | 1275      | 1526      | 2318      | 2579      |  |
|            |                   | -22.50 | 1039                         | 1308      | 1565      | 2377      | 2645      |  |
|            |                   | -23.00 | 1066                         | 1341      | 1604      | 2437      | 2712      |  |
|            |                   | -23.50 | 1096                         | 1379      | 1649      | 2506      | 2788      |  |
|            |                   | -24.00 | 1126                         | 1416      | 1694      | 2574      | 2863      |  |
|            |                   | -24.50 | 1158                         | 1457      | 1743      | 2648      | 2946      |  |
|            |                   | -25.00 | 1193                         | 1501      | 1795      | 2728      | 3034      |  |
| 202.S03    | 0.03              | -6.00  | 66                           |           |           |           |           |  |
|            |                   | -6.50  | 92                           |           |           |           |           |  |
|            |                   | -7.00  | 126                          | 163       |           |           |           |  |
|            |                   | -7.50  | 160                          | 206       |           |           |           |  |
|            |                   | -8.00  | 197                          | 252       | 306       |           |           |  |
|            |                   | -8.50  | 234                          | 298       | 361       |           |           |  |
|            |                   | -9.00  | 277                          | 352       | 425       |           |           |  |
|            |                   | -9.50  | 323                          | 409       | 493       |           |           |  |
|            |                   | -10.00 | 369                          | 467       | 561       | 837       | 935       |  |
|            |                   | -10.50 | 415                          | 524       | 629       | 942       | 1050      |  |
|            |                   | -11.00 | 457                          | 577       | 693       | 1039      | 1158      |  |
|            |                   | -11.50 | 495                          | 624       | 748       | 1124      | 1252      |  |
|            |                   | -12.00 | 536                          | 675       | 809       | 1211      | 1348      |  |
|            |                   | -12.50 | 552                          | 695       | 833       | 1241      | 1382      |  |
|            |                   | -13.00 | 567                          | 715       | 857       | 1273      | 1418      |  |
|            |                   | -13.50 | 579                          | 731       | 876       | 1299      | 1447      |  |
|            |                   | -14.00 | 601                          | 758       | 909       | 1350      | 1504      |  |
|            |                   | -14.50 | 621                          | 784       | 939       | 1396      | 1555      |  |
|            |                   | -15.00 | 645                          | 813       | 975       | 1450      | 1615      |  |
|            |                   | -15.50 | 666                          | 840       | 1006      | 1498      | 1669      |  |
|            |                   | -16.00 | 687                          | 866       | 1037      | 1545      | 1721      |  |
|            |                   | -16.50 | 705                          | 889       | 1065      | 1587      | 1768      |  |
|            |                   | -17.00 | 725                          | 915       | 1096      | 1634      | 1820      |  |
|            |                   | -17.50 | 748                          | 943       | 1130      | 1685      | 1877      |  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten steun druk en trek

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld paalpunt |        | R <sub>n, netto;d</sub> [kN] |           |           |           |           |
|-----------|-------------------|--------|------------------------------|-----------|-----------|-----------|-----------|
|           | niveau            | niveau | SI Ø508/6                    | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |
|           | -18.00            |        | 774                          | 976       | 1169      | 1745      | 1944      |
|           | -18.50            |        | 799                          | 1007      | 1207      | 1803      | 2008      |
|           | -19.00            |        | 828                          | 1044      | 1250      | 1869      | 2081      |
|           | -19.50            |        | 857                          | 1080      | 1294      | 1935      | 2155      |
|           | -20.00            |        | 888                          | 1118      | 1339      | 2004      | 2231      |
|           | -20.50            |        | 913                          | 1149      | 1376      | 2061      | 2295      |
|           | -21.00            |        | 932                          | 1174      | 1406      | 2107      | 2345      |
|           | -21.50            |        | 955                          | 1203      | 1440      | 2158      | 2403      |
|           | -22.00            |        | 989                          | 1245      | 1491      | 2235      | 2488      |
|           | -22.50            |        | 1027                         | 1293      | 1548      | 2323      | 2585      |
|           | -23.00            |        | 1070                         | 1347      | 1612      | 2420      | 2693      |
|           | -23.50            |        | 1113                         | 1401      | 1676      | 2518      | 2802      |
|           | -24.00            |        | 1159                         | 1457      | 1742      | 2620      | 2915      |
|           | -24.50            |        | 1205                         | 1515      | 1811      | 2725      | 3031      |
|           | -25.00            |        | 1251                         | 1572      | 1879      | 2829      | 3146      |

**ALGEMENE GEGEVENS**

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek  
 Datum : 29-09-2020  
 Bestand : P:\EANL\_Projects\10124719 - TenneT Engineering  
 ZW380 kV Oost\2 Content\010 D1.3  
 Reconstructiemasten\Technosoft\D1.3  
 Reconstructiemasten hoek druk en trek.pvw  
 Berekeningstype : Verticaal belaste paal  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

**Toegepaste normen volgens Eurocode met Nederlandse NB**

|             |                    |            |         |
|-------------|--------------------|------------|---------|
| Geotechniek | EN 1997-1:2004     | AC:2009    |         |
|             | NEN-EN 1997-1:2005 | C1+A1:2013 | NB:2016 |
|             | NEN 9997-1:2016    | C2:2017    |         |

**BODEMPROFIELGEGEVENS: 14**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

Hoogte maaiveld [m] : 0.40 Grondwaterstand [m] : -0.60

| Laag | Van [m] | Tot [m] | Omschrijving                 | OCR | Aandeel pos. kleef [%] | $\alpha_0$ | $d_{50}$ [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1    | 0.40    | -1.35   | Klei - Organisch - Matig     | 1.0 | 50.0                   |            |               |
| 2    | -1.35   | -1.55   | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 3    | -1.55   | -1.75   | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 4    | -1.75   | -2.65   | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 5    | -2.65   | -2.85   | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 6    | -2.85   | -3.75   | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 7    | -3.75   | -4.15   | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 8    | -4.15   | -12.95  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 9    | -12.95  | -13.45  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 10   | -13.45  | -13.65  | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 11   | -13.65  | -13.85  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 12   | -13.85  | -14.05  | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 13   | -14.05  | -14.97  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 14   | -14.97  | -15.37  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 15   | -15.37  | -15.77  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 16   | -15.77  | -16.17  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 17   | -16.17  | -16.37  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 18   | -16.37  | -16.67  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 19   | -16.67  | -16.97  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 20   | -16.97  | -18.27  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 21   | -18.27  | -18.47  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 22   | -18.47  | -18.77  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 23   | -18.77  | -19.07  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 24   | -19.07  | -20.66  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 25   | -20.66  | -20.96  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 26   | -20.96  | -21.16  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 27   | -21.16  | -21.46  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 28   | -21.46  | -21.76  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 29   | -21.76  | -22.06  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 30   | -22.06  | -22.76  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 31   | -22.76  | -23.46  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 32   | -23.46  | -25.96  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 33   | -25.96  | -26.36  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 34   | -26.36  | -26.75  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 35   | -26.75  | -26.95  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 36   | -26.95  | -27.15  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 37   | -27.15  | -27.35  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 38   | -27.35  | -29.37  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 39   | -29.37  | -29.56  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 40   | -29.56  | -30.86  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 41   | -30.86  | -31.26  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 42   | -31.26  | -31.46  | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 43   | -31.46  | -31.66  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 44   | -31.66  | -31.88  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 45   | -31.88  | -32.51  | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 46   | -32.51  | -32.73  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 47   | -32.73  | -32.93  | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 48   | -32.93  | -33.16  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 49   | -33.16  | -34.45  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 50   | -34.45  | -34.59  | Grind - Zwak siltig - Vast   | 1.0 | 50.0                   |            |               |

**BODEMPROFIELGEGEVENS: 15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)

Hoogte maaiveld [m] : 0.75 Grondwaterstand [m] : -0.25

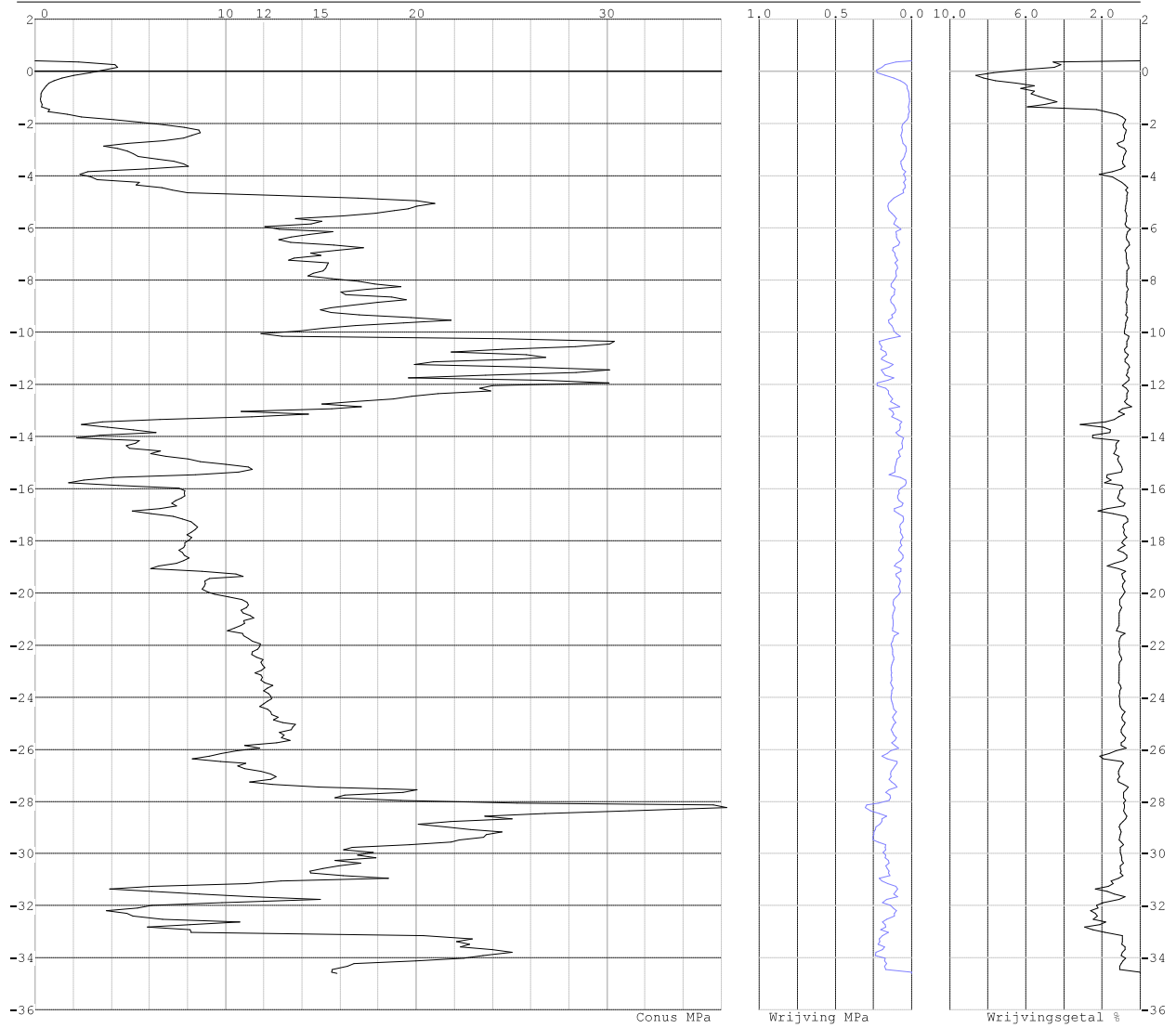
| Laag | Van [m] | Tot [m] | Omschrijving                 | OCR | Aandeel pos. kleef [%] | $\alpha_0$ | $d_{50}$ [mm] |
|------|---------|---------|------------------------------|-----|------------------------|------------|---------------|
| 1    | 0.75    | -0.60   | Klei - Organisch - Matig     | 1.0 | 50.0                   |            |               |
| 2    | -0.60   | -5.90   | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 3    | -5.90   | -6.20   | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 4    | -6.20   | -15.89  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 5    | -15.89  | -20.68  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 6    | -20.68  | -32.95  | Zand - Schoon - Matig        | 1.0 | 100.0                  |            |               |
| 7    | -32.95  | -33.18  | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 8    | -33.18  | -33.40  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 9    | -33.40  | -33.64  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |
| 10   | -33.64  | -33.88  | Zand - Sterk siltig - Kleiig | 1.0 | 100.0                  |            |               |
| 11   | -33.88  | -34.24  | Klei - Zwak zandig - Vast    | 1.0 | 50.0                   |            |               |
| 12   | -34.24  | -34.41  | Zand - Schoon - Vast         | 1.0 | 100.0                  |            |               |





Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SONDERINGSGEGEVENS GRAFIEK: 19-1008-14**

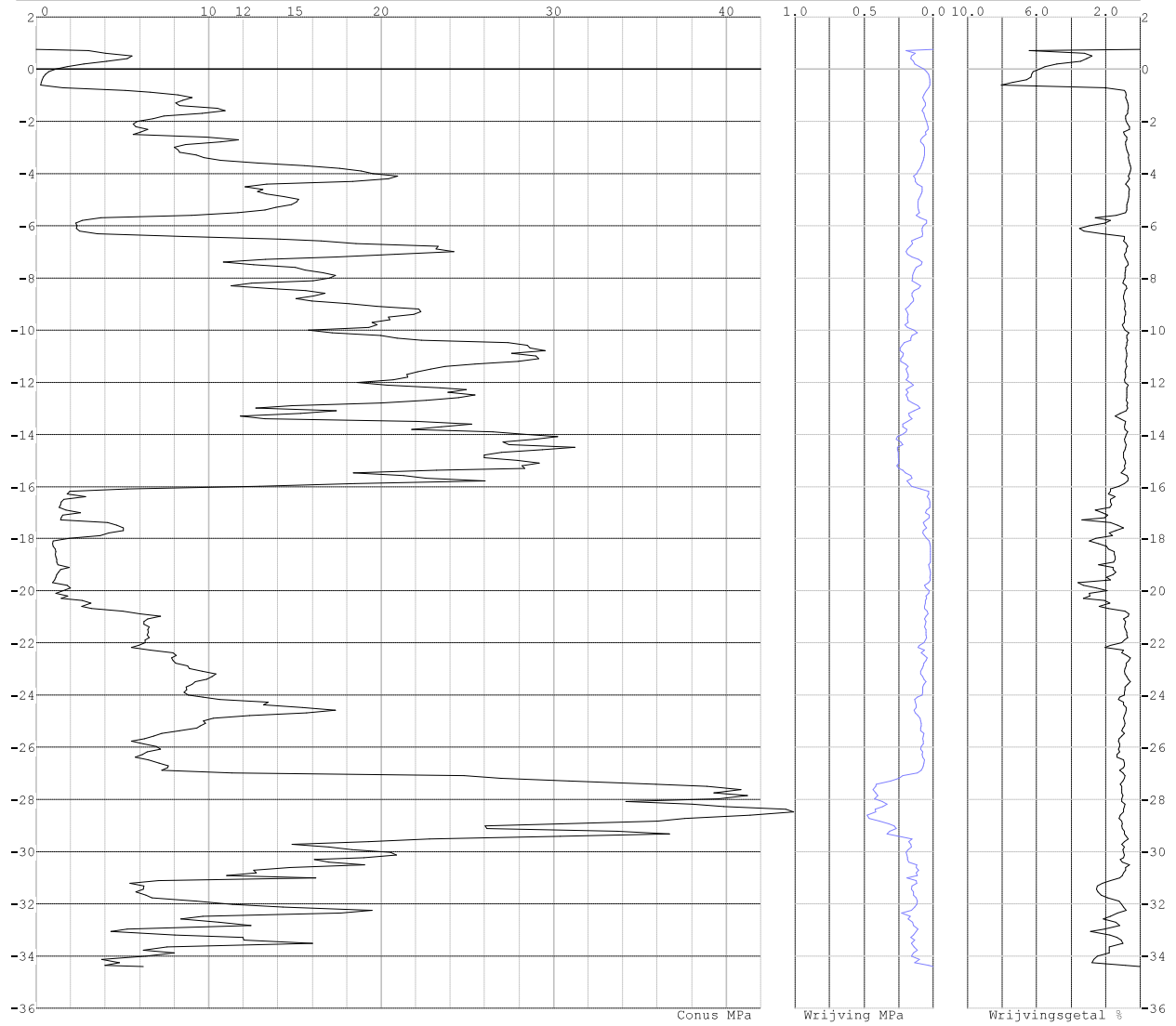


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : 0.75 Bodemprofiel: 15  
Traject negatieve kleeft : 0.75 tot -0.59 [m]  
Traject positieve kleeft : -0.60 tot -34.41 [m]

**SONDERINGSGEGEVENS GRAFIEK: 19-1008-15**

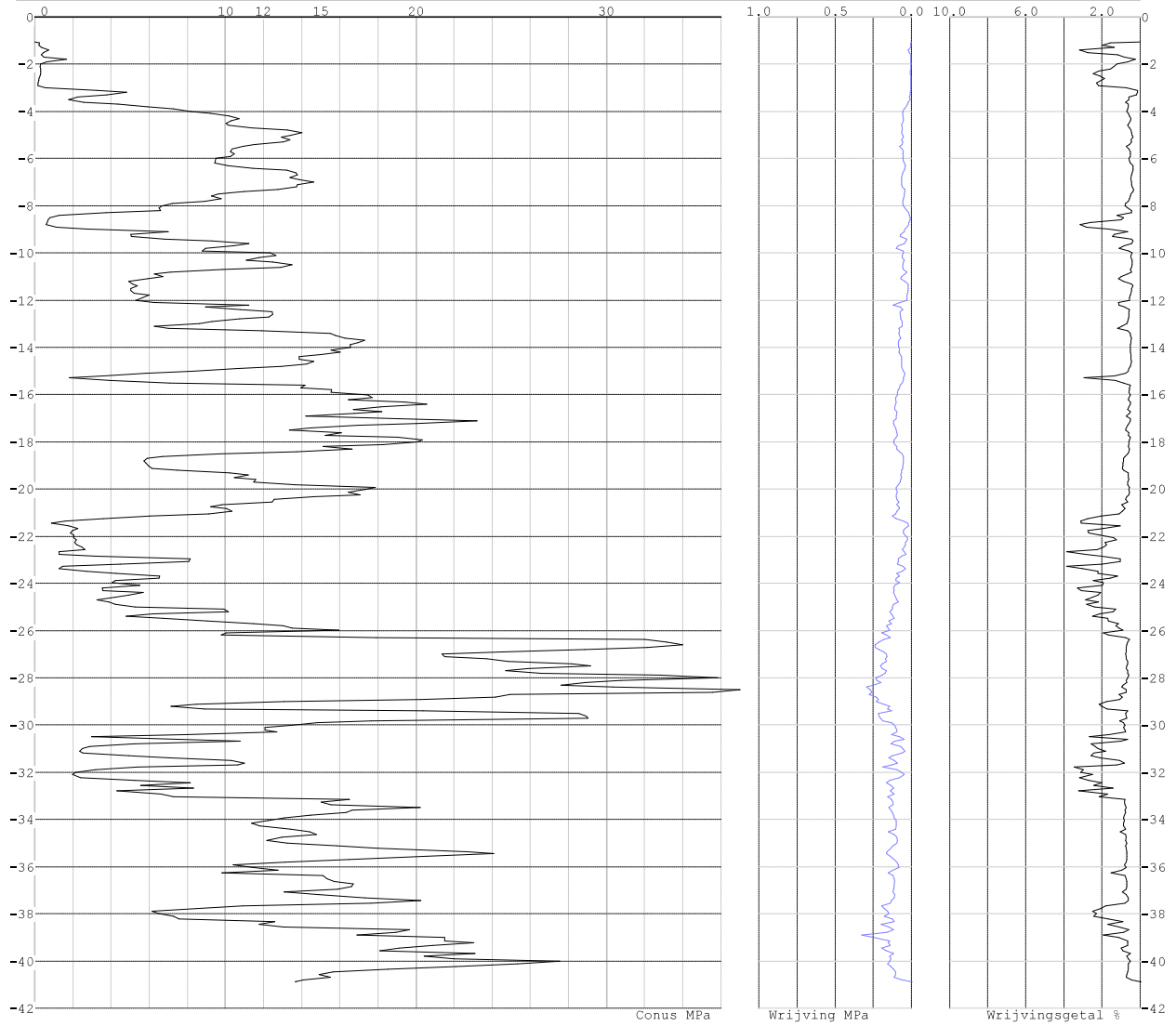


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : -1.05 Bodemprofiel: 251.S01  
Traject negatieve kleeft : -1.05 tot -3.60 [m]  
Traject positieve kleeft : -3.60 tot -40.88 [m]

**SONDERINGSGEGEVENS GRAFIEK: 251.S01**

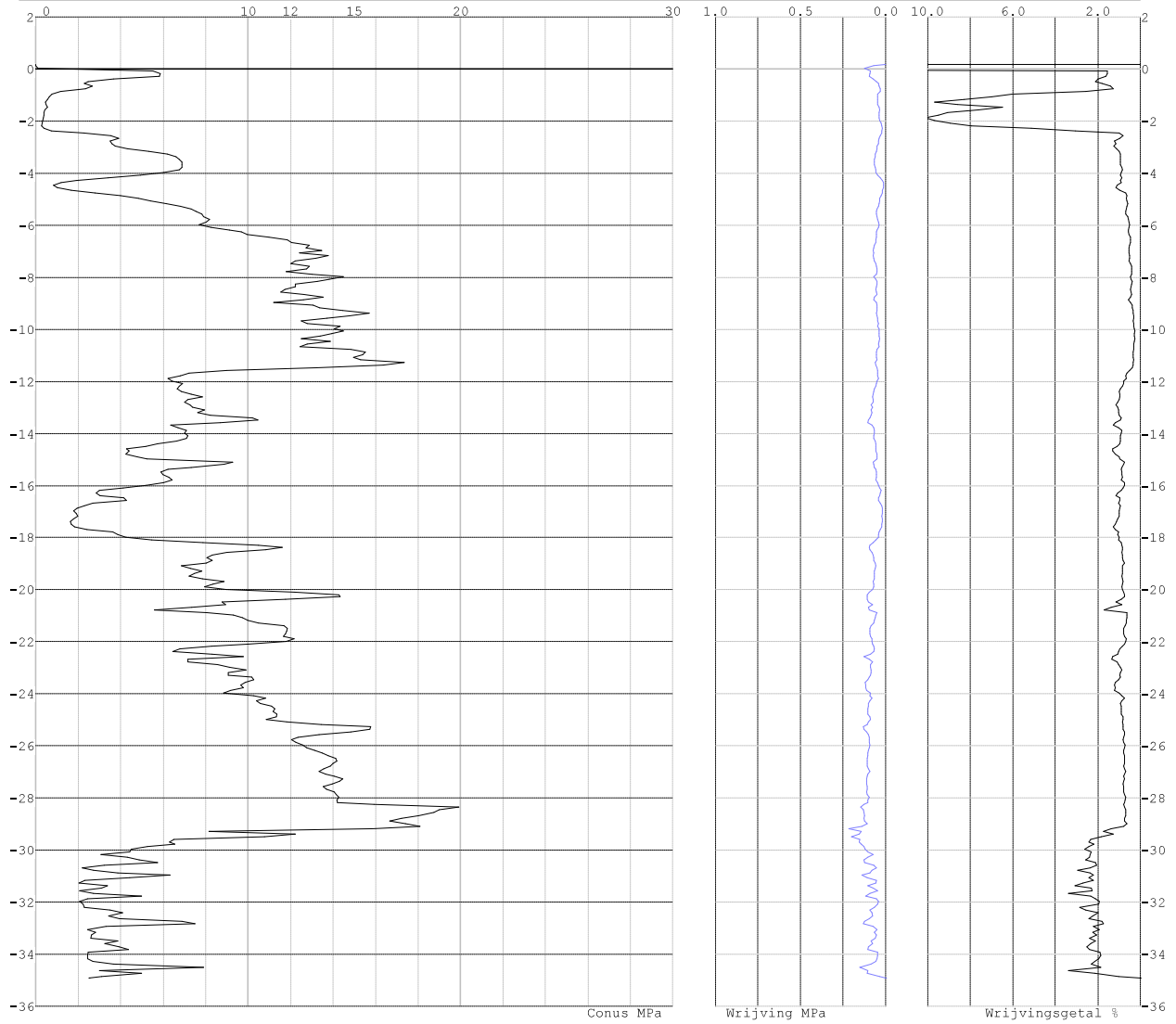


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 19-1008-22**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : 0.18 Bodemprofiel: 22  
Traject negatieve kleeft : 0.18 tot -2.46 [m]  
Traject positieve kleeft : -2.47 tot -34.92 [m]

**SONDERINGSGEGEVENS GRAFIEK: 19-1008-22**

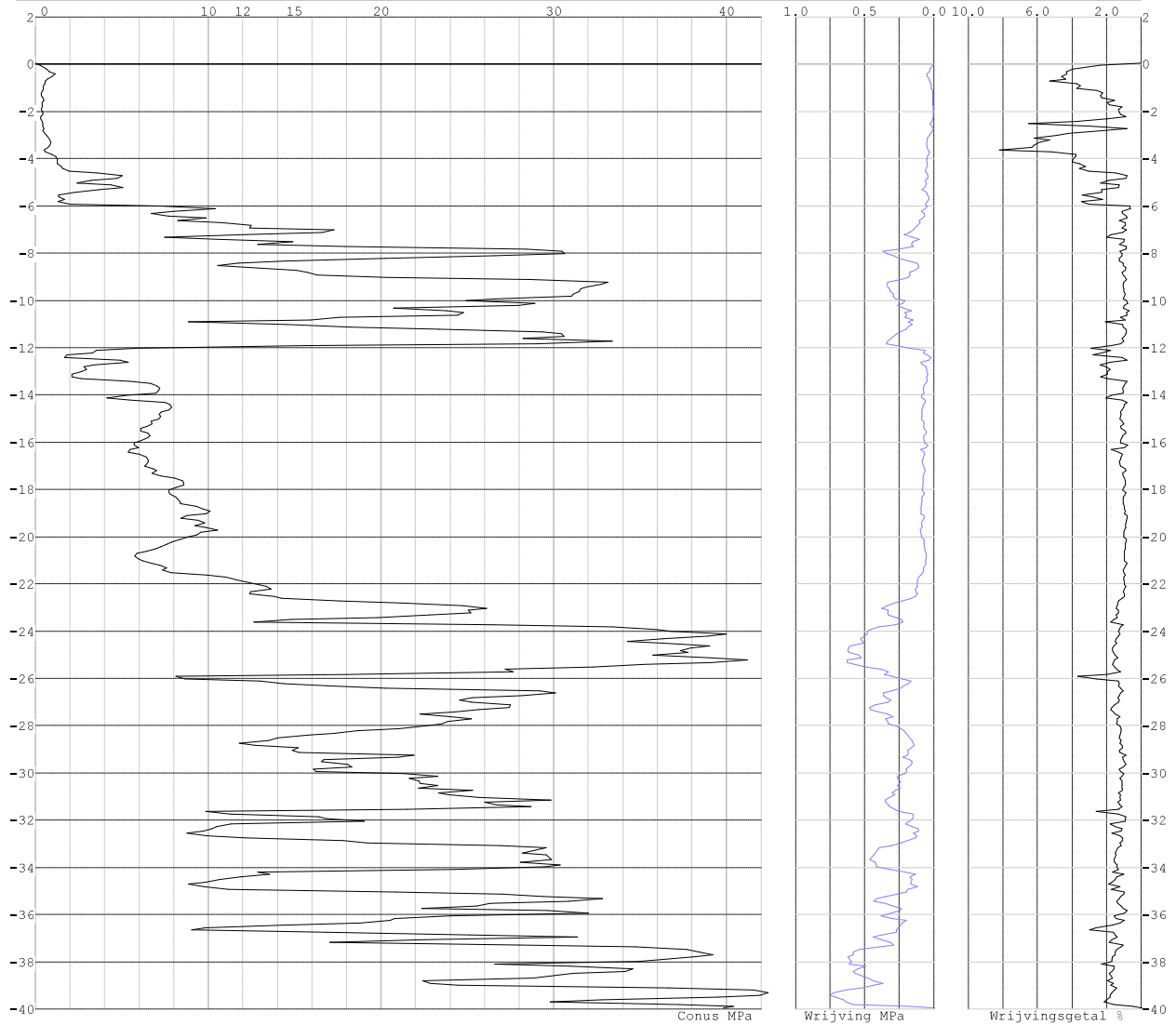


Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
 Hoogte maaiveld [m] : 0.03 Bodemprofiel: 202.S03 wrijf  
 Traject negatieve kleeft : 0.03 tot -4.52 [m]  
 Traject positieve kleeft : -4.52 tot -39.95 [m]

**SONDERINGSGEGEVENS GRAFIEK: 202.S03**



**REKENGEVENS SI Ø508/670 druk**

Berekening : Ontwerpend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_3 (n=1)$  : 1.39 (handmatig)  
 Factor  $\xi_3 (gem)$  : 1.39 (handmatig)  
 Factor  $\xi_4 (min)$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{f;nk}$  : 1.0  
 $R_{s;cal;max;l}$  begrenzen op  $0.75 * R_{u;cal;max;l}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø508/670  
 Niveau paalkop [m] : N.A.P. 0.00  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS SI Ø508/670**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|-----------------|----------------|-----------------|
| 1  | -6.00           | -25.00         | 0.50            |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**RESULTATEN SI Ø508/670 druk (n=1)**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

Sondering 19-1008-14 19-1008-15 251.S01 19-1008-22 202.S03

| Niveau<br>[m] | F <sub>netto;d</sub><br>[kN] | F <sub>netto;d</sub><br>[kN] | F <sub>netto;d</sub><br>[kN] | F <sub>netto;d</sub><br>[kN] | F <sub>netto;d</sub><br>[kN] |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| -6.00         | <b>1303</b>                  | 797                          | 621                          | 746                          | <u>417</u>                   |
| -6.50         | <b>1473</b>                  | 1382                         | <u>526</u>                   | 995                          | 618                          |
| -7.00         | <b>1599</b>                  | 1449                         | <u>556</u>                   | 1105                         | 732                          |
| -7.50         | <b>1754</b>                  | 1550                         | <u>554</u>                   | 1222                         | 1091                         |
| -8.00         | <b>1837</b>                  | 1629                         | <u>558</u>                   | 1336                         | 1166                         |
| -8.50         | <b>1960</b>                  | 1893                         | <u>542</u>                   | 1448                         | 1250                         |
| -9.00         | 2081                         | <b>2161</b>                  | <u>788</u>                   | 1628                         | 1518                         |
| -9.50         | 2160                         | <b>2292</b>                  | <u>921</u>                   | 1396                         | 1604                         |
| -10.00        | <b>2546</b>                  | 2534                         | <u>979</u>                   | 1416                         | 1132                         |
| -10.50        | 2578                         | <b>2753</b>                  | <u>1029</u>                  | 1448                         | 1090                         |
| -11.00        | 2053                         | <b>2581</b>                  | <u>1062</u>                  | 1484                         | 1076                         |
| -11.50        | 1728                         | <b>2636</b>                  | 1121                         | 1490                         | <u>1067</u>                  |
| -12.00        | 1668                         | <b>2706</b>                  | 1315                         | 1509                         | <u>962</u>                   |
| -12.50        | 1675                         | <b>2730</b>                  | 1403                         | 1396                         | <u>994</u>                   |
| -13.00        | 1674                         | <b>2727</b>                  | 1280                         | 1429                         | <u>1019</u>                  |
| -13.50        | 1661                         | <b>3282</b>                  | 1344                         | 1456                         | <u>1178</u>                  |
| -14.00        | 1720                         | <b>2293</b>                  | 1386                         | 1375                         | <u>1252</u>                  |
| -14.50        | 1766                         | <b>2187</b>                  | 1392                         | 1322                         | <u>1312</u>                  |
| -15.00        | 1809                         | <b>2122</b>                  | 1353                         | <u>1303</u>                  | 1360                         |
| -15.50        | 1765                         | <b>2092</b>                  | 1939                         | <u>1312</u>                  | 1409                         |
| -16.00        | 1958                         | 2020                         | <b>2161</b>                  | <u>1321</u>                  | 1451                         |
| -16.50        | 1999                         | <b>2032</b>                  | 1962                         | <u>1329</u>                  | 1542                         |
| -17.00        | <b>2105</b>                  | 2050                         | 2012                         | <u>1331</u>                  | 1622                         |
| -17.50        | <b>2167</b>                  | 2035                         | 2089                         | <u>1396</u>                  | 1744                         |
| -18.00        | <b>2226</b>                  | 2036                         | 2111                         | <u>1663</u>                  | 1813                         |
| -18.50        | <b>2284</b>                  | 2044                         | 2102                         | <u>1714</u>                  | 1806                         |
| -19.00        | <b>2447</b>                  | 2052                         | 2013                         | <u>1781</u>                  | 1850                         |
| -19.50        | <b>2535</b>                  | 2065                         | 1970                         | <u>1857</u>                  | 1894                         |
| -20.00        | <b>2696</b>                  | 2094                         | 1973                         | 1943                         | <u>1918</u>                  |
| -20.50        | <b>2801</b>                  | 2232                         | 1981                         | 1955                         | <u>1938</u>                  |
| -21.00        | <b>2881</b>                  | 2369                         | 2027                         | 2101                         | <u>2024</u>                  |
| -21.50        | <b>2996</b>                  | 2425                         | <u>2049</u>                  | 2175                         | 2248                         |
| -22.00        | <b>3101</b>                  | 2505                         | <u>2061</u>                  | 2211                         | 2444                         |
| -22.50        | <b>3202</b>                  | 2661                         | <u>2099</u>                  | 2300                         | 2738                         |
| -23.00        | <b>3295</b>                  | 2786                         | <u>2162</u>                  | 2430                         | 2871                         |
| -23.50        | <b>3374</b>                  | 2784                         | <u>2256</u>                  | 2495                         | 3322                         |
| -24.00        | <b>3266</b>                  | 2838                         | <u>2305</u>                  | 2622                         | 3118                         |
| -24.50        | <b>3326</b>                  | 2898                         | <u>2353</u>                  | 2735                         | 3233                         |
| -25.00        | <b>3384</b>                  | 2940                         | <u>2530</u>                  | 2908                         | 3206                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SAMENVATTINGSTABEL SI Ø508/670 druk (n=1)**

**Uitgangspunten**

- paal : SI Ø508/670  
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie  
 - schachtafmeting : 590 mm  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Beziijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            |                    |                    | $R_{e,real}$<br>[kN] | $R_{s,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{e;d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40               | -6.00              | 1606.6               | 586.5                | 2193.1               | 1314.8            | -11.9              | 1302.9                  |
|            |                    | -6.50              | 1782.9               | 693.1                | 2476.0               | 1484.4            | -11.9              | 1472.5                  |
|            |                    | -7.00              | 1883.5               | 804.1                | 2687.5               | 1611.2            | -11.9              | 1599.3                  |
|            |                    | -7.50              | 2030.3               | 915.1                | 2945.4               | 1765.8            | -11.9              | 1753.9                  |
|            |                    | -8.00              | 2054.6               | 1029.6               | 3084.2               | 1849.0            | -11.9              | 1837.1                  |
|            |                    | -8.50              | 2134.9               | 1154.7               | 3289.6               | 1972.2            | -11.9              | 1960.3                  |
|            |                    | -9.00              | 2210.6               | 1279.8               | 3490.5               | 2092.6            | -11.9              | 2080.7                  |
|            |                    | -9.50              | 2227.5               | 1395.1               | 3622.6               | 2171.8            | -11.9              | 2159.9                  |
|            |                    | -10.00             | 2761.1               | 1505.8               | 4266.9               | 2558.1            | -11.9              | 2546.2                  |
|            |                    | -10.50             | 2696.0               | 1624.0               | 4319.9               | 2589.9            | -11.9              | 2578.0                  |
|            |                    | -11.00             | 1694.4               | 1749.1               | 3443.5               | 2064.5            | -11.9              | 2052.6                  |
|            |                    | -11.50             | 1027.8               | 1874.2               | 2902.0               | 1739.8            | -11.9              | 1727.9                  |
|            |                    | -12.00             | 802.3                | 1999.3               | 2801.7               | 1679.6            | -11.9              | 1667.8                  |
|            |                    | -12.50             | 689.2                | 2124.4               | 2813.6               | 1686.8            | -11.9              | 1674.9                  |
|            |                    | -13.00             | 563.9                | 2249.0               | 2812.8               | 1686.3            | -11.9              | 1674.4                  |
|            |                    | -13.50             | 463.5                | 2326.4               | 2789.9               | 1672.6            | -11.9              | 1660.7                  |
|            |                    | -14.00             | 515.6                | 2373.6               | 2889.2               | 1732.1            | -11.9              | 1720.2                  |
|            |                    | -14.50             | 552.2                | 2413.3               | 2965.5               | 1777.9            | -11.9              | 1766.0                  |
|            |                    | -15.00             | 565.2                | 2472.8               | 3038.1               | 1821.4            | -11.9              | 1809.5                  |
|            |                    | -15.50             | 405.5                | 2558.7               | 2964.2               | 1777.1            | -11.9              | 1765.2                  |
|            |                    | -16.00             | 693.3                | 2593.2               | 3286.5               | 1970.3            | -11.9              | 1958.4                  |
|            |                    | -16.50             | 695.8                | 2657.6               | 3353.4               | 2010.4            | -11.9              | 1998.5                  |
|            |                    | -17.00             | 818.6                | 2711.9               | 3530.6               | 2116.6            | -11.9              | 2104.7                  |
|            |                    | -17.50             | 856.6                | 2777.7               | 3634.4               | 2178.9            | -11.9              | 2167.0                  |
|            |                    | -18.00             | 887.6                | 2845.9               | 3733.5               | 2238.3            | -11.9              | 2226.4                  |
| -18.50     | 919.2              | 2910.7             | 3829.9               | 2296.1               | -11.9                | 2284.2            |                    |                         |
| -19.00     | 1127.3             | 2973.8             | 4101.1               | 2458.7               | -11.9                | 2446.8            |                    |                         |
| -19.50     | 1198.9             | 3048.8             | 4247.7               | 2546.6               | -11.9                | 2534.7            |                    |                         |
| -20.00     | 1394.2             | 3123.2             | 4517.3               | 2708.2               | -11.9                | 2696.3            |                    |                         |
| -20.50     | 1481.3             | 3210.7             | 4691.9               | 2812.9               | -11.9                | 2801.0            |                    |                         |
| -21.00     | 1522.1             | 3303.2             | 4825.4               | 2892.9               | -11.9                | 2881.0            |                    |                         |
| -21.50     | 1625.4             | 3392.4             | 5017.8               | 3008.3               | -11.9                | 2996.4            |                    |                         |
| -22.00     | 1706.9             | 3485.7             | 5192.6               | 3113.1               | -11.9                | 3101.2            |                    |                         |
| -22.50     | 1777.8             | 3582.2             | 5360.0               | 3213.5               | -11.9                | 3201.6            |                    |                         |
| -23.00     | 1834.5             | 3681.5             | 5516.1               | 3307.0               | -11.9                | 3295.1            |                    |                         |
| -23.50     | 1867.0             | 3780.3             | 5647.2               | 3385.6               | -11.9                | 3373.7            |                    |                         |
| -24.00     | 1587.1             | 3880.4             | 5467.5               | 3277.9               | -11.9                | 3266.0            |                    |                         |
| -24.50     | 1587.5             | 3980.4             | 5567.9               | 3338.1               | -11.9                | 3326.2            |                    |                         |
| -25.00     | 1580.4             | 4084.4             | 5664.8               | 3396.2               | -11.9                | 3384.3            |                    |                         |
| 19-1008-15 | 0.75               | -6.00              | 512.7                | 824.0                | 1336.7               | 801.4             | -4.3               | 797.1                   |
|            |                    | -6.50              | 1441.9               | 869.8                | 2311.7               | 1385.9            | -4.3               | 1381.6                  |
|            |                    | -7.00              | 1453.8               | 969.9                | 2423.7               | 1453.0            | -4.3               | 1448.7                  |
|            |                    | -7.50              | 1522.9               | 1068.9               | 2591.8               | 1553.9            | -4.3               | 1549.6                  |
|            |                    | -8.00              | 1555.2               | 1169.0               | 2724.2               | 1633.2            | -4.3               | 1628.9                  |
|            |                    | -8.50              | 1890.4               | 1273.5               | 3164.0               | 1896.9            | -4.3               | 1892.6                  |
|            |                    | -9.00              | 2213.5               | 1398.6               | 3612.1               | 2165.6            | -4.3               | 2161.2                  |
|            |                    | -9.50              | 2306.0               | 1523.8               | 3829.7               | 2296.0            | -4.3               | 2291.7                  |
|            |                    | -10.00             | 2584.5               | 1648.9               | 4233.4               | 2538.0            | -4.3               | 2533.7                  |
|            |                    | -10.50             | 2825.5               | 1774.0               | 4599.4               | 2757.5            | -4.3               | 2753.2                  |
|            |                    | -11.00             | 2412.7               | 1899.1               | 4311.8               | 2585.0            | -4.3               | 2580.7                  |
|            |                    | -11.50             | 2379.1               | 2024.2               | 4403.3               | 2639.9            | -4.3               | 2635.6                  |
|            |                    | -12.00             | 2372.2               | 2149.3               | 4521.5               | 2710.7            | -4.3               | 2706.4                  |
|            |                    | -12.50             | 2286.3               | 2274.4               | 4560.8               | 2734.3            | -4.3               | 2730.0                  |
|            |                    | -13.00             | 2158.5               | 2397.5               | 4556.0               | 2731.4            | -4.3               | 2727.1                  |
|            |                    | -13.50             | 2974.7               | 2506.6               | 5481.4               | 3286.2            | -4.3               | 3281.9                  |
|            |                    | -14.00             | 1200.6               | 2631.7               | 3832.4               | 2297.6            | -4.3               | 2293.3                  |
|            |                    | -14.50             | 897.6                | 2756.9               | 3654.5               | 2190.9            | -4.3               | 2186.6                  |
|            |                    | -15.00             | 664.9                | 2882.0               | 3546.9               | 2126.4            | -4.3               | 2122.1                  |
|            |                    | -15.50             | 490.3                | 3007.1               | 3497.4               | 2096.8            | -4.3               | 2092.5                  |
|            |                    | -16.00             | 244.5                | 3131.2               | 3375.7               | 2023.8            | -4.3               | 2019.5                  |
|            |                    | -16.50             | 234.5                | 3161.3               | 3395.8               | 2035.9            | -4.3               | 2031.5                  |
|            |                    | -17.00             | 251.9                | 3174.9               | 3426.8               | 2054.4            | -4.3               | 2050.1                  |
|            |                    | -17.50             | 205.6                | 3195.6               | 3401.2               | 2039.1            | -4.3               | 2034.8                  |
|            |                    | -18.00             | 171.8                | 3230.7               | 3402.5               | 2039.9            | -4.3               | 2035.6                  |
| -18.50     | 177.2              | 3239.9             | 3417.1               | 2048.6               | -4.3                 | 2044.3            |                    |                         |
| -19.00     | 179.7              | 3249.7             | 3429.4               | 2056.0               | -4.3                 | 2051.7            |                    |                         |
| -19.50     | 190.6              | 3261.4             | 3452.0               | 2069.5               | -4.3                 | 2065.2            |                    |                         |
| -20.00     | 226.5              | 3273.4             | 3500.0               | 2098.3               | -4.3                 | 2094.0            |                    |                         |
| -20.50     | 441.1              | 3289.7             | 3730.8               | 2236.7               | -4.3                 | 2232.4            |                    |                         |
| -21.00     | 631.3              | 3327.9             | 3959.1               | 2373.6               | -4.3                 | 2369.3            |                    |                         |
| -21.50     | 670.2              | 3381.6             | 4051.7               | 2429.1               | -4.3                 | 2424.8            |                    |                         |
| -22.00     | 750.1              | 3435.3             | 4185.4               | 2509.2               | -4.3                 | 2504.9            |                    |                         |
| -22.50     | 953.8              | 3491.3             | 4445.1               | 2664.9               | -4.3                 | 2660.6            |                    |                         |
| -23.00     | 1094.3             | 3560.2             | 4654.5               | 2790.4               | -4.3                 | 2786.1            |                    |                         |
| -23.50     | 1009.0             | 3642.2             | 4651.2               | 2788.5               | -4.3                 | 2784.2            |                    |                         |
| -24.00     | 1025.7             | 3715.6             | 4741.3               | 2842.5               | -4.3                 | 2838.2            |                    |                         |
| -24.50     | 1032.1             | 3808.9             | 4841.1               | 2902.3               | -4.3                 | 2898.0            |                    |                         |
| -25.00     | 1008.3             | 3903.3             | 4911.6               | 2944.6               | -4.3                 | 2940.3            |                    |                         |
| 251.S01    | -1.05              | -6.00              | 673.9                | 400.4                | 1074.3               | 644.1             | -23.1              | 621.0                   |
|            |                    | -6.50              | 430.4                | 486.2                | 916.6                | 549.5             | -23.1              | 526.4                   |
|            |                    | -7.00              | 379.8                | 586.3                | 966.1                | 579.2             | -23.1              | 556.1                   |
|            |                    | -7.50              | 278.9                | 683.1                | 962.0                | 576.7             | -23.1              | 553.7                   |
|            |                    | -8.00              | 196.5                | 772.0                | 968.5                | 580.6             | -23.1              | 557.6                   |
| -8.50      | 110.3              | 831.9              | 942.2                | 564.9                | -23.1                | 541.8             |                    |                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maai/veld paalpunt |        | Beziwkdraagvermogen         |                             |                             | Rekenwaarden           |                          |                                |
|------------|--------------------|--------|-----------------------------|-----------------------------|-----------------------------|------------------------|--------------------------|--------------------------------|
|            | niveau             | niveau | R <sub>b,real</sub><br>[kN] | R <sub>v,real</sub><br>[kN] | R <sub>c,real</sub><br>[kN] | R <sub>d</sub><br>[kN] | F <sub>hkd</sub><br>[kN] | R <sub>d,netto;d</sub><br>[kN] |
| 251.S01    | -1.05              | -9.00  | 512.4                       | 840.9                       | 1353.3                      | 811.3                  | -23.1                    | 788.3                          |
|            |                    | -9.50  | 679.2                       | 896.2                       | 1575.4                      | 944.5                  | -23.1                    | 921.4                          |
|            |                    | -10.00 | 691.9                       | 980.1                       | 1671.9                      | 1002.4                 | -23.1                    | 979.3                          |
|            |                    | -10.50 | 676.5                       | 1078.7                      | 1755.2                      | 1052.3                 | -23.1                    | 1029.2                         |
|            |                    | -11.00 | 657.0                       | 1153.5                      | 1810.5                      | 1085.4                 | -23.1                    | 1062.4                         |
|            |                    | -11.50 | 709.0                       | 1199.0                      | 1908.0                      | 1143.9                 | -23.1                    | 1120.8                         |
|            |                    | -12.00 | 988.0                       | 1244.2                      | 2232.2                      | 1338.3                 | -23.1                    | 1315.2                         |
|            |                    | -12.50 | 1058.4                      | 1321.1                      | 2379.4                      | 1426.5                 | -23.1                    | 1403.5                         |
|            |                    | -13.00 | 761.7                       | 1411.9                      | 2173.6                      | 1303.1                 | -23.1                    | 1280.0                         |
|            |                    | -13.50 | 782.8                       | 1497.5                      | 2280.3                      | 1367.1                 | -23.1                    | 1344.0                         |
|            |                    | -14.00 | 733.8                       | 1616.5                      | 2350.3                      | 1409.1                 | -23.1                    | 1386.0                         |
|            |                    | -14.50 | 624.8                       | 1734.8                      | 2359.6                      | 1414.6                 | -23.1                    | 1391.6                         |
|            |                    | -15.00 | 432.6                       | 1862.8                      | 2295.4                      | 1376.2                 | -23.1                    | 1353.1                         |
|            |                    | -15.50 | 1352.0                      | 1920.1                      | 3272.1                      | 1961.7                 | -23.1                    | 1938.6                         |
|            |                    | -16.00 | 1607.9                      | 2035.6                      | 3643.5                      | 2184.4                 | -23.1                    | 2161.3                         |
|            |                    | -16.50 | 1149.9                      | 2160.7                      | 3310.6                      | 1984.8                 | -23.1                    | 1961.7                         |
|            |                    | -17.00 | 1109.8                      | 2284.4                      | 3394.2                      | 2034.9                 | -23.1                    | 2011.9                         |
|            |                    | -17.50 | 1119.7                      | 2402.5                      | 3522.2                      | 2111.7                 | -23.1                    | 2088.6                         |
|            |                    | -18.00 | 1046.1                      | 2514.0                      | 3560.2                      | 2134.4                 | -23.1                    | 2111.3                         |
|            |                    | -18.50 | 903.9                       | 2639.9                      | 3543.8                      | 2124.6                 | -23.1                    | 2101.5                         |
|            |                    | -19.00 | 680.4                       | 2714.9                      | 3395.3                      | 2035.6                 | -23.1                    | 2012.5                         |
|            |                    | -19.50 | 529.9                       | 2794.7                      | 3324.6                      | 1993.2                 | -23.1                    | 1970.1                         |
|            |                    | -20.00 | 438.1                       | 2892.0                      | 3330.1                      | 1996.4                 | -23.1                    | 1973.4                         |
|            |                    | -20.50 | 310.4                       | 3032.1                      | 3342.5                      | 2003.9                 | -23.1                    | 1980.8                         |
|            |                    | -21.00 | 243.3                       | 3175.4                      | 3418.7                      | 2049.6                 | -23.1                    | 2026.5                         |
| -21.50     | 220.6              | 3234.8 | 3455.4                      | 2071.6                      | -23.1                       | 2048.6                 |                          |                                |
| -22.00     | 223.6              | 3253.5 | 3477.0                      | 2084.6                      | -23.1                       | 2061.5                 |                          |                                |
| -22.50     | 261.7              | 3278.1 | 3539.8                      | 2122.2                      | -23.1                       | 2099.1                 |                          |                                |
| -23.00     | 326.4              | 3317.5 | 3643.9                      | 2184.6                      | -23.1                       | 2161.5                 |                          |                                |
| -23.50     | 432.2              | 3369.1 | 3801.3                      | 2278.9                      | -23.1                       | 2255.9                 |                          |                                |
| -24.00     | 444.7              | 3438.9 | 3883.6                      | 2328.3                      | -23.1                       | 2305.3                 |                          |                                |
| -24.50     | 461.6              | 3502.5 | 3964.1                      | 2376.5                      | -23.1                       | 2353.5                 |                          |                                |
| -25.00     | 698.0              | 3560.2 | 4258.2                      | 2552.9                      | -23.1                       | 2529.8                 |                          |                                |
| 19-1008-22 | 0.18               | -6.00  | 983.7                       | 300.2                       | 1284.0                      | 769.8                  | -24.1                    | 745.7                          |
|            |                    | -6.50  | 1320.1                      | 379.2                       | 1699.4                      | 1018.8                 | -24.1                    | 994.7                          |
|            |                    | -7.00  | 1405.3                      | 478.7                       | 1884.1                      | 1129.5                 | -24.1                    | 1105.4                         |
|            |                    | -7.50  | 1499.0                      | 578.9                       | 2078.0                      | 1245.8                 | -24.1                    | 1221.7                         |
|            |                    | -8.00  | 1589.4                      | 679.0                       | 2268.4                      | 1360.0                 | -24.1                    | 1335.9                         |
|            |                    | -8.50  | 1676.0                      | 778.8                       | 2454.8                      | 1471.7                 | -24.1                    | 1447.6                         |
|            |                    | -9.00  | 1878.4                      | 877.7                       | 2756.1                      | 1652.3                 | -24.1                    | 1628.3                         |
|            |                    | -9.50  | 1387.1                      | 981.7                       | 2368.8                      | 1420.1                 | -24.1                    | 1396.0                         |
|            |                    | -10.00 | 1316.5                      | 1086.0                      | 2402.5                      | 1440.4                 | -24.1                    | 1416.3                         |
|            |                    | -10.50 | 1265.3                      | 1190.4                      | 2455.6                      | 1472.2                 | -24.1                    | 1448.1                         |
|            |                    | -11.00 | 1221.7                      | 1294.3                      | 2516.0                      | 1508.4                 | -24.1                    | 1484.3                         |
|            |                    | -11.50 | 1127.4                      | 1398.0                      | 2525.4                      | 1514.0                 | -24.1                    | 1490.0                         |
|            |                    | -12.00 | 1096.0                      | 1461.8                      | 2557.8                      | 1533.4                 | -24.1                    | 1509.4                         |
|            |                    | -12.50 | 850.6                       | 1518.7                      | 2369.3                      | 1420.4                 | -24.1                    | 1396.3                         |
|            |                    | -13.00 | 843.5                       | 1579.8                      | 2423.3                      | 1452.8                 | -24.1                    | 1428.8                         |
|            |                    | -13.50 | 817.5                       | 1651.9                      | 2469.4                      | 1480.5                 | -24.1                    | 1456.4                         |
|            |                    | -14.00 | 618.9                       | 1714.0                      | 2332.9                      | 1398.6                 | -24.1                    | 1374.6                         |
|            |                    | -14.50 | 477.7                       | 1768.2                      | 2245.9                      | 1346.5                 | -24.1                    | 1322.4                         |
|            |                    | -15.00 | 406.9                       | 1806.5                      | 2213.4                      | 1327.0                 | -24.1                    | 1302.9                         |
|            |                    | -15.50 | 360.1                       | 1868.7                      | 2228.8                      | 1336.2                 | -24.1                    | 1312.1                         |
|            |                    | -16.00 | 324.8                       | 1918.9                      | 2243.7                      | 1345.1                 | -24.1                    | 1321.1                         |
|            |                    | -16.50 | 309.1                       | 1948.0                      | 2257.2                      | 1353.2                 | -24.1                    | 1329.1                         |
|            |                    | -17.00 | 289.3                       | 1970.9                      | 2260.2                      | 1355.1                 | -24.1                    | 1331.0                         |
|            |                    | -17.50 | 382.9                       | 1985.9                      | 2368.8                      | 1420.1                 | -24.1                    | 1396.1                         |
|            |                    | -18.00 | 802.7                       | 2011.3                      | 2814.1                      | 1687.1                 | -24.1                    | 1663.0                         |
| -18.50     | 814.0              | 2085.0 | 2899.0                      | 1738.0                      | -24.1                       | 1713.9                 |                          |                                |
| -19.00     | 855.1              | 2156.1 | 3011.2                      | 1805.3                      | -24.1                       | 1781.2                 |                          |                                |
| -19.50     | 919.3              | 2217.7 | 3137.0                      | 1880.7                      | -24.1                       | 1856.6                 |                          |                                |
| -20.00     | 994.6              | 2286.9 | 3281.5                      | 1967.3                      | -24.1                       | 1943.3                 |                          |                                |
| -20.50     | 920.3              | 2381.5 | 3301.8                      | 1979.5                      | -24.1                       | 1955.4                 |                          |                                |
| -21.00     | 1097.2             | 2446.7 | 3543.9                      | 2124.6                      | -24.1                       | 2100.6                 |                          |                                |
| -21.50     | 1133.7             | 2535.1 | 3668.8                      | 2199.5                      | -24.1                       | 2175.4                 |                          |                                |
| -22.00     | 1093.7             | 2633.7 | 3727.4                      | 2234.7                      | -24.1                       | 2210.6                 |                          |                                |
| -22.50     | 1173.8             | 2702.0 | 3875.8                      | 2323.6                      | -24.1                       | 2299.6                 |                          |                                |
| -23.00     | 1322.3             | 2771.4 | 4093.6                      | 2454.2                      | -24.1                       | 2430.1                 |                          |                                |
| -23.50     | 1350.5             | 2851.8 | 4202.2                      | 2519.3                      | -24.1                       | 2495.3                 |                          |                                |
| -24.00     | 1482.5             | 2931.3 | 4413.9                      | 2646.2                      | -24.1                       | 2622.1                 |                          |                                |
| -24.50     | 1583.2             | 3019.2 | 4602.4                      | 2759.2                      | -24.1                       | 2735.1                 |                          |                                |
| -25.00     | 1777.7             | 3112.8 | 4890.5                      | 2932.0                      | -24.1                       | 2907.9                 |                          |                                |
| 202.S03    | 0.03               | -6.00  | 716.2                       | 82.3                        | 798.5                       | 478.7                  | -62.1                    | 416.6                          |
|            |                    | -6.50  | 983.8                       | 150.3                       | 1134.2                      | 680.0                  | -62.1                    | 617.9                          |
|            |                    | -7.00  | 1085.5                      | 239.8                       | 1325.4                      | 794.6                  | -62.1                    | 732.5                          |
|            |                    | -7.50  | 1593.1                      | 330.9                       | 1924.0                      | 1153.5                 | -62.1                    | 1091.4                         |
|            |                    | -8.00  | 1617.2                      | 431.0                       | 2048.3                      | 1228.0                 | -62.1                    | 1165.9                         |
|            |                    | -8.50  | 1658.3                      | 530.1                       | 2188.4                      | 1312.0                 | -62.1                    | 1249.9                         |
|            |                    | -9.00  | 1990.2                      | 645.9                       | 2636.1                      | 1580.4                 | -62.1                    | 1518.3                         |
|            |                    | -9.50  | 2008.8                      | 771.0                       | 2779.9                      | 1666.6                 | -62.1                    | 1604.5                         |
|            |                    | -10.00 | 1095.6                      | 896.1                       | 1991.7                      | 1194.1                 | -62.1                    | 1132.0                         |
|            |                    | -10.50 | 900.8                       | 1021.2                      | 1922.1                      | 1152.3                 | -62.1                    | 1090.2                         |
|            |                    | -11.00 | 762.5                       | 1136.4                      | 1898.9                      | 1138.4                 | -62.1                    | 1076.3                         |
|            |                    | -11.50 | 646.4                       | 1236.5                      | 1882.9                      | 1128.8                 | -62.1                    | 1066.7                         |
|            |                    | -12.00 | 360.0                       | 1347.4                      | 1707.4                      | 1023.6                 | -62.1                    | 961.6                          |
|            |                    | -12.50 | 375.1                       | 1387.2                      | 1762.3                      | 1056.5                 | -62.1                    | 994.5                          |
|            |                    | -13.00 | 376.7                       | 1427.2                      | 1803.9                      | 1081.5                 | -62.1                    | 1019.4                         |
|            |                    | -13.50 | 612.0                       | 1456.6                      | 2068.6                      | 1240.2                 | -62.1                    | 1178.1                         |
| -14.00     | 677.7              | 1514.3 | 2192.0                      | 1314.2                      | -62.1                       | 1252.1                 |                          |                                |
| -14.50     | 725.2              | 1565.9 | 2291.2                      | 1373.6                      | -62.1                       | 1311.5                 |                          |                                |
| -15.00     | 744.8              | 1627.8 | 2372.6                      | 1422.5                      | -62.1                       | 1360.4                 |                          |                                |
| -15.50     | 771.0              | 1682.5 | 2453.6                      | 1471.0                      | -62.1                       | 1408.9                 |                          |                                |
| -16.00     | 788.6              | 1735.5 | 2524.1                      | 1513.3                      | -62.1                       | 1451.2                 |                          |                                |
| -16.50     | 892.4              | 1782.8 | 2675.2                      | 1603.8                      | -62.1                       | 1541.7                 |                          |                                |



Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maai veld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                     |                         |
|-----------|---------------------|--------------------|----------------------|----------------------|----------------------|-------------------|---------------------|-------------------------|
|           |                     |                    | $R_{b,real}$<br>[kN] | $R_{s,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{b;d}$<br>[kN] | $F_{bkk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 202.S03   | 0.03                | -17.00             | 972.3                | 1836.1               | 2808.4               | 1683.7            | -62.1               | 1621.6                  |
|           |                     | -17.50             | 1118.3               | 1894.0               | 3012.3               | 1805.9            | -62.1               | 1743.8                  |
|           |                     | -18.00             | 1164.7               | 1963.7               | 3128.4               | 1875.5            | -62.1               | 1813.5                  |
|           |                     | -18.50             | 1085.6               | 2030.1               | 3115.7               | 1867.9            | -62.1               | 1805.8                  |
|           |                     | -19.00             | 1082.8               | 2107.4               | 3190.1               | 1912.6            | -62.1               | 1850.5                  |
|           |                     | -19.50             | 1079.0               | 2184.3               | 3263.4               | 1956.5            | -62.1               | 1894.4                  |
|           |                     | -20.00             | 1038.3               | 2265.1               | 3303.4               | 1980.5            | -62.1               | 1918.4                  |
|           |                     | -20.50             | 1004.6               | 2330.8               | 3335.4               | 1999.7            | -62.1               | 1937.6                  |
|           |                     | -21.00             | 1098.0               | 2382.1               | 3480.1               | 2086.4            | -62.1               | 2024.3                  |
|           |                     | -21.50             | 1411.0               | 2441.4               | 3852.4               | 2309.6            | -62.1               | 2247.5                  |
|           |                     | -22.00             | 1648.6               | 2531.6               | 4180.2               | 2506.1            | -62.1               | 2444.0                  |
|           |                     | -22.50             | 2034.1               | 2635.8               | 4669.9               | 2799.7            | -62.1               | 2737.6                  |
|           |                     | -23.00             | 2140.2               | 2752.2               | 4892.4               | 2933.1            | -62.1               | 2871.0                  |
|           |                     | -23.50             | 2776.6               | 2868.7               | 5645.3               | 3384.5            | -62.1               | 3322.4                  |
|           |                     | -24.00             | 2313.4               | 2990.7               | 5304.2               | 3180.0            | -62.1               | 3117.9                  |
|           |                     | -24.50             | 2381.1               | 3115.9               | 5496.9               | 3295.5            | -62.1               | 3233.4                  |
|           |                     | -25.00             | 2209.4               | 3241.0               | 5450.3               | 3267.6            | -62.1               | 3205.5                  |

**REKENGEGEVENS SI Ø610/850 druk**

Berekening : Ontwerpend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(gem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{E,nk}$  : 1.0  
 $R_{b,real,max;E}$  begrenzen op  $0.75 * R_{b,real,max;E}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : SI Ø610/850  
 Niveau paalkop [m] : N.A.P. 0.00  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS SI Ø610/850**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau<br>[m] | Eindniveau<br>[m] | Stapgrootte<br>[m] |
|----|--------------------|-------------------|--------------------|
| 1  | -7.00              | -25.00            | 0.50               |

**RESULTATEN SI Ø610/850 druk (n=1)**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering     | 19-1008-14            | 19-1008-15            | 251.S01               | 19-1008-22            | 202.S03               |
|---------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| Niveau<br>[m] | $F_{netto;d}$<br>[kN] | $F_{netto;d}$<br>[kN] | $F_{netto;d}$<br>[kN] | $F_{netto;d}$<br>[kN] | $F_{netto;d}$<br>[kN] |
| -7.00         | 2234                  | 2030                  | 752                   | 1553                  | 1099                  |
| -7.50         | 2368                  | 2154                  | 728                   | 1700                  | 1588                  |
| -8.00         | 2527                  | 2275                  | 720                   | 1844                  | 1670                  |
| -8.50         | 2678                  | 2639                  | 710                   | 1981                  | 1827                  |
| -9.00         | 2819                  | 2981                  | 1111                  | 1761                  | 2155                  |
| -9.50         | 2962                  | 3136                  | 1242                  | 1827                  | 1533                  |
| -10.00        | 3510                  | 3406                  | 1319                  | 1905                  | 1460                  |
| -10.50        | 2551                  | 3366                  | 1371                  | 1992                  | 1404                  |
| -11.00        | 2269                  | 3480                  | 1402                  | 2027                  | 1453                  |
| -11.50        | 2199                  | 3588                  | 1476                  | 1958                  | 1414                  |
| -12.00        | 2193                  | 3731                  | 1758                  | 1836                  | 1262                  |
| -12.50        | 2202                  | 3768                  | 1615                  | 1875                  | 1296                  |
| -13.00        | 2128                  | 3828                  | 1702                  | 1916                  | 1377                  |
| -13.50        | 2136                  | 2954                  | 1783                  | 1770                  | 1563                  |
| -14.00        | 2219                  | 2840                  | 1832                  | 1672                  | 1672                  |
| -14.50        | 2282                  | 2756                  | 1828                  | 1651                  | 1739                  |
| -15.00        | 2338                  | 2704                  | 1791                  | 1673                  | 1797                  |
| -15.50        | 2317                  | 2565                  | 2678                  | 1687                  | 1855                  |
| -16.00        | 2543                  | 2526                  | 2508                  | 1692                  | 1907                  |
| -16.50        | 2591                  | 2555                  | 2569                  | 1699                  | 2029                  |
| -17.00        | 2735                  | 2543                  | 2686                  | 1697                  | 2147                  |
| -17.50        | 2812                  | 2553                  | 2755                  | 1816                  | 2306                  |
| -18.00        | 2884                  | 2550                  | 2764                  | 2173                  | 2309                  |
| -18.50        | 2954                  | 2561                  | 2464                  | 2255                  | 2381                  |
| -19.00        | 3185                  | 2570                  | 2508                  | 2340                  | 2458                  |
| -19.50        | 3300                  | 2589                  | 2483                  | 2438                  | 2522                  |
| -20.00        | 3523                  | 2651                  | 2478                  | 2552                  | 2552                  |
| -20.50        | 3651                  | 2880                  | 2505                  | 2581                  | 2570                  |
| -21.00        | 3768                  | 3036                  | 2550                  | 2752                  | 2701                  |
| -21.50        | 3955                  | 3104                  | 2573                  | 2843                  | 3053                  |
| -22.00        | 4095                  | 3236                  | 2589                  | 2882                  | 3307                  |
| -22.50        | 4227                  | 3441                  | 2676                  | 3010                  | 3724                  |
| -23.00        | 4333                  | 3484                  | 2725                  | 3195                  | 3925                  |
| -23.50        | 4201                  | 3579                  | 2864                  | 3301                  | 4196                  |
| -24.00        | 4292                  | 3633                  | 2924                  | 3496                  | 4324                  |
| -24.50        | 4382                  | 3709                  | 3002                  | 3636                  | 4443                  |
| -25.00        | 4465                  | 3753                  | 3240                  | 3875                  | 4326                  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SAMENVATTINGSTABEL SI Ø610/850 druk (n=1)**

**Uitgangspunten**

- paal : SI Ø610/850  
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie  
 - schachtafmeting : 730 mm  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            |                    |                    | $R_{e,soal}$<br>[kN] | $R_{b,soal}$<br>[kN] | $R_{c,soal}$<br>[kN] | $R_{e;d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40               | -7.00              | 2755.7               | 994.9                | 3750.6               | 2248.6            | -14.7              | 2233.8                  |
|            |                    | -7.50              | 2842.7               | 1132.3               | 3975.0               | 2383.1            | -14.7              | 2368.4                  |
|            |                    | -8.00              | 2965.5               | 1273.9               | 4239.4               | 2541.6            | -14.7              | 2526.9                  |
|            |                    | -8.50              | 3063.1               | 1428.7               | 4491.8               | 2692.9            | -14.7              | 2678.2                  |
|            |                    | -9.00              | 3142.8               | 1583.5               | 4726.4               | 2833.6            | -14.7              | 2818.8                  |
|            |                    | -9.50              | 3238.5               | 1726.1               | 4964.6               | 2976.4            | -14.7              | 2961.7                  |
|            |                    | -10.00             | 4015.6               | 1863.1               | 5878.7               | 3524.4            | -14.7              | 3509.7                  |
|            |                    | -10.50             | 2270.4               | 2009.3               | 4279.7               | 2565.7            | -14.7              | 2551.0                  |
|            |                    | -11.00             | 1644.5               | 2164.1               | 3808.6               | 2283.4            | -14.7              | 2268.6                  |
|            |                    | -11.50             | 1373.6               | 2318.9               | 3692.5               | 2213.8            | -14.7              | 2199.0                  |
|            |                    | -12.00             | 1208.5               | 2473.7               | 3682.2               | 2207.6            | -14.7              | 2192.9                  |
|            |                    | -12.50             | 1069.6               | 2628.5               | 3698.1               | 2217.1            | -14.7              | 2202.4                  |
|            |                    | -13.00             | 790.7                | 2782.6               | 3573.3               | 2142.3            | -14.7              | 2127.5                  |
|            |                    | -13.50             | 709.6                | 2878.4               | 3588.0               | 2151.1            | -14.7              | 2136.4                  |
|            |                    | -14.00             | 789.3                | 2936.9               | 3726.1               | 2233.9            | -14.7              | 2219.2                  |
|            |                    | -14.50             | 845.3                | 2986.0               | 3831.3               | 2296.9            | -14.7              | 2282.2                  |
|            |                    | -15.00             | 865.3                | 3059.6               | 3924.9               | 2353.0            | -14.7              | 2338.3                  |
|            |                    | -15.50             | 723.5                | 3165.8               | 3889.3               | 2331.7            | -14.7              | 2317.0                  |
|            |                    | -16.00             | 1058.4               | 3208.5               | 4266.9               | 2558.1            | -14.7              | 2543.4                  |
|            |                    | -16.50             | 1058.0               | 3288.2               | 4346.2               | 2605.6            | -14.7              | 2590.9                  |
|            |                    | -17.00             | 1231.8               | 3355.5               | 4587.3               | 2750.2            | -14.7              | 2735.5                  |
|            |                    | -17.50             | 1278.5               | 3436.8               | 4715.3               | 2826.9            | -14.7              | 2812.2                  |
|            |                    | -18.00             | 1314.3               | 3521.2               | 4835.5               | 2899.0            | -14.7              | 2884.3                  |
|            |                    | -18.50             | 1351.2               | 3601.4               | 4952.6               | 2969.2            | -14.7              | 2954.5                  |
|            |                    | -19.00             | 1658.3               | 3679.4               | 5337.7               | 3200.1            | -14.7              | 3185.3                  |
| -19.50     | 1756.6             | 3772.3             | 5528.8               | 3314.6               | -14.7                | 3299.9            |                    |                         |
| -20.00     | 2037.0             | 3864.2             | 5901.3               | 3537.9               | -14.7                | 3523.2            |                    |                         |
| -20.50     | 2142.1             | 3972.5             | 6114.6               | 3665.8               | -14.7                | 3651.1            |                    |                         |
| -21.00     | 2222.4             | 4087.0             | 6309.5               | 3782.6               | -14.7                | 3767.9            |                    |                         |
| -21.50     | 2423.7             | 4197.4             | 6621.1               | 3969.5               | -14.7                | 3954.8            |                    |                         |
| -22.00     | 2542.2             | 4312.9             | 6855.0               | 4109.7               | -14.7                | 4095.0            |                    |                         |
| -22.50     | 2643.3             | 4432.2             | 7075.5               | 4241.9               | -14.7                | 4227.2            |                    |                         |
| -23.00     | 2696.7             | 4555.1             | 7251.8               | 4347.6               | -14.7                | 4332.9            |                    |                         |
| -23.50     | 2355.2             | 4677.3             | 7032.5               | 4216.1               | -14.7                | 4201.4            |                    |                         |
| -24.00     | 2383.0             | 4801.1             | 7184.1               | 4307.0               | -14.7                | 4292.3            |                    |                         |
| -24.50     | 2408.2             | 4924.9             | 7333.1               | 4396.3               | -14.7                | 4381.6            |                    |                         |
| -25.00     | 2419.5             | 5053.5             | 7473.0               | 4480.2               | -14.7                | 4465.5            |                    |                         |
| 19-1008-15 | 0.75               | -7.00              | 2194.2               | 1200.1               | 3394.3               | 2035.0            | -5.3               | 2029.6                  |
|            |                    | -7.50              | 2278.7               | 1322.5               | 3601.3               | 2159.0            | -5.3               | 2153.7                  |
|            |                    | -8.00              | 2357.2               | 1446.4               | 3803.5               | 2280.3            | -5.3               | 2275.0                  |
|            |                    | -8.50              | 2835.3               | 1575.7               | 4411.0               | 2644.5            | -5.3               | 2639.2                  |
|            |                    | -9.00              | 3250.7               | 1730.5               | 4981.3               | 2986.4            | -5.3               | 2981.0                  |
|            |                    | -9.50              | 3354.2               | 1885.3               | 5239.5               | 3141.2            | -5.3               | 3135.9                  |
|            |                    | -10.00             | 3649.8               | 2040.1               | 5689.9               | 3411.2            | -5.3               | 3405.9                  |
|            |                    | -10.50             | 3428.9               | 2194.9               | 5623.8               | 3371.6            | -5.3               | 3366.3                  |
|            |                    | -11.00             | 3464.3               | 2349.7               | 5814.1               | 3485.6            | -5.3               | 3480.3                  |
|            |                    | -11.50             | 3489.8               | 2504.5               | 5994.3               | 3593.7            | -5.3               | 3588.4                  |
|            |                    | -12.00             | 3572.5               | 2659.3               | 6231.8               | 3736.1            | -5.3               | 3730.8                  |
|            |                    | -12.50             | 3480.2               | 2814.1               | 6294.3               | 3773.6            | -5.3               | 3768.2                  |
|            |                    | -13.00             | 3427.8               | 2966.4               | 6394.1               | 3833.4            | -5.3               | 3828.1                  |
|            |                    | -13.50             | 1834.3               | 3101.4               | 4935.7               | 2959.1            | -5.3               | 2953.7                  |
|            |                    | -14.00             | 1489.3               | 3256.2               | 4745.5               | 2845.0            | -5.3               | 2839.7                  |
|            |                    | -14.50             | 1194.2               | 3411.0               | 4605.3               | 2761.0            | -5.3               | 2755.6                  |
|            |                    | -15.00             | 953.9                | 3565.8               | 4519.7               | 2709.7            | -5.3               | 2704.3                  |
|            |                    | -15.50             | 567.1                | 3720.6               | 4287.8               | 2570.6            | -5.3               | 2565.3                  |
|            |                    | -16.00             | 348.8                | 3874.2               | 4223.0               | 2531.8            | -5.3               | 2526.4                  |
|            |                    | -16.50             | 358.9                | 3911.5               | 4270.4               | 2560.2            | -5.3               | 2554.9                  |
|            |                    | -17.00             | 322.3                | 3928.3               | 4250.6               | 2548.3            | -5.3               | 2543.0                  |
|            |                    | -17.50             | 313.0                | 3953.9               | 4266.8               | 2558.1            | -5.3               | 2552.7                  |
|            |                    | -18.00             | 265.5                | 3997.3               | 4262.8               | 2555.6            | -5.3               | 2550.3                  |
|            |                    | -18.50             | 271.3                | 4008.7               | 4280.0               | 2565.9            | -5.3               | 2560.6                  |
|            |                    | -19.00             | 275.1                | 4020.8               | 4295.9               | 2575.5            | -5.3               | 2570.2                  |
| -19.50     | 291.8              | 4035.2             | 4327.0               | 2594.1               | -5.3                 | 2588.8            |                    |                         |
| -20.00     | 380.4              | 4050.2             | 4430.6               | 2656.2               | -5.3                 | 2650.9            |                    |                         |
| -20.50     | 743.2              | 4070.3             | 4813.5               | 2885.8               | -5.3                 | 2880.4            |                    |                         |
| -21.00     | 955.0              | 4117.5             | 5072.5               | 3041.1               | -5.3                 | 3035.8            |                    |                         |
| -21.50     | 1002.4             | 4184.0             | 5186.3               | 3109.3               | -5.3                 | 3104.0            |                    |                         |
| -22.00     | 1155.3             | 4250.5             | 5405.8               | 3240.9               | -5.3                 | 3235.6            |                    |                         |
| -22.50     | 1429.0             | 4319.7             | 5748.7               | 3446.5               | -5.3                 | 3441.1            |                    |                         |
| -23.00     | 1415.5             | 4404.9             | 5820.5               | 3489.5               | -5.3                 | 3484.2            |                    |                         |
| -23.50     | 1472.4             | 4506.5             | 5978.9               | 3584.4               | -5.3                 | 3579.1            |                    |                         |
| -24.00     | 1471.3             | 4597.3             | 6068.5               | 3638.2               | -5.3                 | 3632.9            |                    |                         |
| -24.50     | 1483.6             | 4712.7             | 6196.3               | 3714.8               | -5.3                 | 3709.5            |                    |                         |
| -25.00     | 1439.3             | 4829.5             | 6268.8               | 3758.3               | -5.3                 | 3752.9            |                    |                         |
| 251.S01    | -1.05              | -7.00              | 575.9                | 725.4                | 1301.2               | 780.1             | -28.5              | 751.6                   |
|            |                    | -7.50              | 417.2                | 845.1                | 1262.3               | 756.8             | -28.5              | 728.3                   |
|            |                    | -8.00              | 293.6                | 955.2                | 1248.9               | 748.7             | -28.5              | 720.2                   |
|            |                    | -8.50              | 202.4                | 1029.3               | 1231.7               | 738.5             | -28.5              | 709.9                   |
|            |                    | -9.00              | 859.6                | 1040.4               | 1900.0               | 1139.1            | -28.5              | 1110.6                  |
|            |                    | -9.50              | 1011.0               | 1108.9               | 2119.8               | 1270.9            | -28.5              | 1242.4                  |
|            |                    | -10.00             | 1035.2               | 1212.6               | 2247.9               | 1347.6            | -28.5              | 1319.1                  |
| -10.50     | 1000.1             | 1334.6             | 2334.7               | 1399.7               | -28.5                | 1371.1            |                    |                         |
| -11.00     | 958.4              | 1427.2             | 2385.7               | 1430.3               | -28.5                | 1401.7            |                    |                         |
| -11.50     | 1026.3             | 1483.6             | 2509.9               | 1504.7               | -28.5                | 1476.2            |                    |                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Beziwkdraagvermogen         |                             |                             | Rekenwaarden           |                          |                                |
|------------|--------------------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|--------------------------|--------------------------------|
|            |                    |                    | R <sub>b,real</sub><br>[kN] | R <sub>s,real</sub><br>[kN] | R <sub>c,real</sub><br>[kN] | R <sub>d</sub><br>[kN] | F <sub>hkd</sub><br>[kN] | R <sub>c,netto;d</sub><br>[kN] |
| 251.S01    | -1.05              | -12.00             | 1440.9                      | 1539.4                      | 2980.4                      | 1786.8                 | -28.5                    | 1758.3                         |
|            |                    | -12.50             | 1107.2                      | 1634.5                      | 2741.7                      | 1643.7                 | -28.5                    | 1615.2                         |
|            |                    | -13.00             | 1139.0                      | 1746.9                      | 2886.0                      | 1730.2                 | -28.5                    | 1701.7                         |
|            |                    | -13.50             | 1168.1                      | 1852.8                      | 3020.9                      | 1811.1                 | -28.5                    | 1782.6                         |
|            |                    | -14.00             | 1103.3                      | 2000.1                      | 3103.4                      | 1860.5                 | -28.5                    | 1832.0                         |
|            |                    | -14.50             | 950.3                       | 2146.4                      | 3096.7                      | 1856.5                 | -28.5                    | 1828.0                         |
|            |                    | -15.00             | 729.8                       | 2304.8                      | 3034.6                      | 1819.3                 | -28.5                    | 1790.8                         |
|            |                    | -15.50             | 2139.0                      | 2375.7                      | 4514.7                      | 2706.7                 | -28.5                    | 2678.2                         |
|            |                    | -16.00             | 1712.0                      | 2518.6                      | 4230.6                      | 2536.4                 | -28.5                    | 2507.8                         |
|            |                    | -16.50             | 1659.7                      | 2673.4                      | 4333.1                      | 2597.8                 | -28.5                    | 2569.3                         |
|            |                    | -17.00             | 1701.0                      | 2826.5                      | 4527.5                      | 2714.3                 | -28.5                    | 2685.8                         |
|            |                    | -17.50             | 1669.8                      | 2972.6                      | 4642.4                      | 2783.2                 | -28.5                    | 2754.7                         |
|            |                    | -18.00             | 1546.6                      | 3110.6                      | 4657.2                      | 2792.1                 | -28.5                    | 2763.5                         |
|            |                    | -18.50             | 891.3                       | 3266.3                      | 4157.6                      | 2492.6                 | -28.5                    | 2464.0                         |
|            |                    | -19.00             | 871.2                       | 3359.2                      | 4230.3                      | 2536.2                 | -28.5                    | 2507.6                         |
|            |                    | -19.50             | 731.1                       | 3457.9                      | 4188.9                      | 2511.3                 | -28.5                    | 2482.8                         |
|            |                    | -20.00             | 602.8                       | 3578.2                      | 4181.0                      | 2506.6                 | -28.5                    | 2478.1                         |
|            |                    | -20.50             | 475.2                       | 3751.6                      | 4226.8                      | 2534.0                 | -28.5                    | 2505.5                         |
|            |                    | -21.00             | 372.5                       | 3928.9                      | 4301.3                      | 2578.7                 | -28.5                    | 2550.2                         |
|            |                    | -21.50             | 337.7                       | 4002.4                      | 4340.1                      | 2602.0                 | -28.5                    | 2573.5                         |
|            |                    | -22.00             | 341.2                       | 4025.5                      | 4366.7                      | 2617.9                 | -28.5                    | 2589.4                         |
|            |                    | -22.50             | 455.0                       | 4055.9                      | 4510.9                      | 2704.4                 | -28.5                    | 2675.8                         |
|            |                    | -23.00             | 488.4                       | 4104.7                      | 4593.1                      | 2753.6                 | -28.5                    | 2725.1                         |
|            |                    | -23.50             | 656.8                       | 4168.5                      | 4825.3                      | 2892.9                 | -28.5                    | 2864.4                         |
|            |                    | -24.00             | 669.6                       | 4254.9                      | 4924.6                      | 2952.4                 | -28.5                    | 2923.8                         |
| -24.50     | 721.5              | 4333.6             | 5055.0                      | 3030.6                      | -28.5                       | 3002.1                 |                          |                                |
| -25.00     | 1047.3             | 4405.0             | 5452.3                      | 3268.8                      | -28.5                       | 3240.2                 |                          |                                |
| 19-1008-22 | 0.18               | -7.00              | 2047.7                      | 592.3                       | 2640.0                      | 1582.8                 | -29.8                    | 1553.0                         |
|            |                    | -7.50              | 2169.1                      | 716.3                       | 2885.5                      | 1729.9                 | -29.8                    | 1700.1                         |
|            |                    | -8.00              | 2286.1                      | 840.1                       | 3126.3                      | 1874.3                 | -29.8                    | 1844.5                         |
|            |                    | -8.50              | 2390.4                      | 963.6                       | 3354.1                      | 2010.8                 | -29.8                    | 1981.0                         |
|            |                    | -9.00              | 1901.3                      | 1085.9                      | 2987.2                      | 1790.9                 | -29.8                    | 1761.1                         |
|            |                    | -9.50              | 1883.1                      | 1214.7                      | 3097.7                      | 1857.2                 | -29.8                    | 1827.4                         |
|            |                    | -10.00             | 1883.0                      | 1343.7                      | 3226.7                      | 1934.5                 | -29.8                    | 1904.7                         |
|            |                    | -10.50             | 1899.7                      | 1472.8                      | 3372.5                      | 2021.9                 | -29.8                    | 1992.1                         |
|            |                    | -11.00             | 1829.6                      | 1601.4                      | 3431.0                      | 2057.0                 | -29.8                    | 2027.2                         |
|            |                    | -11.50             | 1586.6                      | 1729.8                      | 3316.4                      | 1988.2                 | -29.8                    | 1958.4                         |
|            |                    | -12.00             | 1303.8                      | 1808.7                      | 3112.4                      | 1866.0                 | -29.8                    | 1836.2                         |
|            |                    | -12.50             | 1297.6                      | 1879.1                      | 3176.7                      | 1904.5                 | -29.8                    | 1874.7                         |
|            |                    | -13.00             | 1291.3                      | 1954.7                      | 3246.0                      | 1946.1                 | -29.8                    | 1916.3                         |
|            |                    | -13.50             | 957.5                       | 2043.9                      | 3001.4                      | 1799.4                 | -29.8                    | 1769.6                         |
|            |                    | -14.00             | 717.7                       | 2120.7                      | 2838.4                      | 1701.7                 | -29.8                    | 1671.9                         |
|            |                    | -14.50             | 615.0                       | 2187.8                      | 2802.8                      | 1680.3                 | -29.8                    | 1650.5                         |
|            |                    | -15.00             | 604.3                       | 2235.2                      | 2839.5                      | 1702.4                 | -29.8                    | 1672.6                         |
|            |                    | -15.50             | 551.2                       | 2312.1                      | 2863.3                      | 1716.6                 | -29.8                    | 1686.8                         |
|            |                    | -16.00             | 497.3                       | 2374.2                      | 2871.5                      | 1721.5                 | -29.8                    | 1691.7                         |
|            |                    | -16.50             | 473.2                       | 2410.3                      | 2883.5                      | 1728.7                 | -29.8                    | 1698.9                         |
|            |                    | -17.00             | 442.2                       | 2438.6                      | 2880.8                      | 1727.1                 | -29.8                    | 1697.3                         |
|            |                    | -17.50             | 621.7                       | 2457.2                      | 3078.8                      | 1845.8                 | -29.8                    | 1816.0                         |
|            |                    | -18.00             | 1186.2                      | 2488.6                      | 3674.8                      | 2203.1                 | -29.8                    | 2173.3                         |
|            |                    | -18.50             | 1232.0                      | 2579.8                      | 3811.8                      | 2285.3                 | -29.8                    | 2255.5                         |
|            |                    | -19.00             | 1284.4                      | 2667.7                      | 3952.1                      | 2369.4                 | -29.8                    | 2339.6                         |
| -19.50     | 1372.1             | 2743.9             | 4116.1                      | 2467.7                      | -29.8                       | 2437.9                 |                          |                                |
| -20.00     | 1476.9             | 2829.6             | 4306.5                      | 2581.8                      | -29.8                       | 2552.0                 |                          |                                |
| -20.50     | 1408.5             | 2946.6             | 4355.2                      | 2611.0                      | -29.8                       | 2581.2                 |                          |                                |
| -21.00     | 1612.9             | 3027.3             | 4640.2                      | 2781.9                      | -29.8                       | 2752.1                 |                          |                                |
| -21.50     | 1654.9             | 3136.7             | 4791.6                      | 2872.6                      | -29.8                       | 2842.8                 |                          |                                |
| -22.00     | 1598.2             | 3258.7             | 4856.9                      | 2911.8                      | -29.8                       | 2882.0                 |                          |                                |
| -22.50     | 1726.4             | 3343.2             | 5069.6                      | 3039.3                      | -29.8                       | 3009.5                 |                          |                                |
| -23.00     | 1950.4             | 3429.0             | 5379.4                      | 3225.1                      | -29.8                       | 3195.3                 |                          |                                |
| -23.50     | 2027.5             | 3528.5             | 5556.0                      | 3330.9                      | -29.8                       | 3301.1                 |                          |                                |
| -24.00     | 2254.5             | 3626.9             | 5881.4                      | 3526.0                      | -29.8                       | 3496.2                 |                          |                                |
| -24.50     | 2379.1             | 3735.7             | 6114.8                      | 3665.9                      | -29.8                       | 3636.1                 |                          |                                |
| -25.00     | 2662.6             | 3851.4             | 6514.0                      | 3905.3                      | -29.8                       | 3875.5                 |                          |                                |
| 202.S03    | 0.03               | -7.00              | 1664.5                      | 296.7                       | 1961.3                      | 1175.8                 | -76.8                    | 1099.0                         |
|            |                    | -7.50              | 2367.7                      | 409.5                       | 2777.1                      | 1664.9                 | -76.8                    | 1588.1                         |
|            |                    | -8.00              | 2379.9                      | 533.3                       | 2913.3                      | 1746.6                 | -76.8                    | 1669.7                         |
|            |                    | -8.50              | 2520.4                      | 655.9                       | 3176.2                      | 1904.2                 | -76.8                    | 1827.4                         |
|            |                    | -9.00              | 2923.9                      | 799.2                       | 3723.0                      | 2232.0                 | -76.8                    | 2155.2                         |
|            |                    | -9.50              | 1731.0                      | 954.0                       | 2685.0                      | 1609.7                 | -76.8                    | 1532.9                         |
|            |                    | -10.00             | 1454.6                      | 1108.8                      | 2563.4                      | 1536.8                 | -76.8                    | 1460.0                         |
|            |                    | -10.50             | 1206.8                      | 1263.6                      | 2470.4                      | 1481.1                 | -76.8                    | 1404.2                         |
|            |                    | -11.00             | 1146.3                      | 1406.1                      | 2552.4                      | 1530.2                 | -76.8                    | 1453.4                         |
|            |                    | -11.50             | 957.2                       | 1529.9                      | 2487.1                      | 1491.1                 | -76.8                    | 1414.2                         |
|            |                    | -12.00             | 565.3                       | 1667.2                      | 2232.4                      | 1338.4                 | -76.8                    | 1261.6                         |
|            |                    | -12.50             | 574.1                       | 1716.4                      | 2290.5                      | 1373.2                 | -76.8                    | 1296.4                         |
|            |                    | -13.00             | 659.9                       | 1765.8                      | 2425.7                      | 1454.3                 | -76.8                    | 1377.4                         |
|            |                    | -13.50             | 932.7                       | 1802.2                      | 2734.9                      | 1639.6                 | -76.8                    | 1562.8                         |
|            |                    | -14.00             | 1043.6                      | 1873.6                      | 2917.2                      | 1748.9                 | -76.8                    | 1672.1                         |
|            |                    | -14.50             | 1090.8                      | 1937.5                      | 3028.3                      | 1815.5                 | -76.8                    | 1738.7                         |
|            |                    | -15.00             | 1110.9                      | 2014.1                      | 3125.0                      | 1873.5                 | -76.8                    | 1796.7                         |
|            |                    | -15.50             | 1141.2                      | 2081.8                      | 3223.0                      | 1932.2                 | -76.8                    | 1855.4                         |
|            |                    | -16.00             | 1161.8                      | 2147.3                      | 3309.1                      | 1983.9                 | -76.8                    | 1907.1                         |
|            |                    | -16.50             | 1307.2                      | 2205.8                      | 3513.0                      | 2106.1                 | -76.8                    | 2029.3                         |
|            |                    | -17.00             | 1437.6                      | 2271.8                      | 3709.4                      | 2223.8                 | -76.8                    | 2147.0                         |
|            |                    | -17.50             | 1630.8                      | 2343.4                      | 3974.2                      | 2382.6                 | -76.8                    | 2305.8                         |
|            |                    | -18.00             | 1549.9                      | 2429.6                      | 3979.5                      | 2385.8                 | -76.8                    | 2309.0                         |
|            |                    | -18.50             | 1587.6                      | 2511.8                      | 4099.4                      | 2457.7                 | -76.8                    | 2380.9                         |
|            |                    | -19.00             | 1620.5                      | 2607.4                      | 4228.0                      | 2534.8                 | -76.8                    | 2457.9                         |
| -19.50     | 1631.4             | 2702.6             | 4334.1                      | 2598.4                      | -76.8                       | 2521.5                 |                          |                                |
| -20.00     | 1582.1             | 2802.6             | 4384.6                      | 2628.7                      | -76.8                       | 2551.9                 |                          |                                |
| -20.50     | 1531.8             | 2883.9             | 4415.7                      | 2647.3                      | -76.8                       | 2570.5                 |                          |                                |
| -21.00     | 1685.6             | 2947.3             | 4632.9                      | 2777.5                      | -76.8                       | 2700.7                 |                          |                                |
| -21.50     | 2200.3             | 3020.7             | 5221.1                      | 3130.1                      | -76.8                       | 3053.3                 |                          |                                |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|-----------|-------------------|--------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|           | niveau            | niveau | $R_{b,calc}$<br>[kN] | $R_{s,calc}$<br>[kN] | $R_{c,calc}$<br>[kN] | $R_{c,d}$<br>[kN] | $F_{nk,d}$<br>[kN] | $R_{c,netto,d}$<br>[kN] |
| 202.S03   | 0.03              | -22.00 | 2512.0               | 3132.3               | 5644.3               | 3383.9            | -76.8              | 3307.0                  |
|           |                   | -22.50 | 3078.8               | 3261.2               | 6340.0               | 3801.0            | -76.8              | 3724.2                  |
|           |                   | -23.00 | 3270.0               | 3405.2               | 6675.2               | 4001.9            | -76.8              | 3925.1                  |
|           |                   | -23.50 | 3577.0               | 3549.4               | 7126.4               | 4272.4            | -76.8              | 4195.6                  |
|           |                   | -24.00 | 3639.6               | 3700.4               | 7340.0               | 4400.5            | -76.8              | 4323.7                  |
|           |                   | -24.50 | 3684.2               | 3855.2               | 7539.4               | 4520.0            | -76.8              | 4443.2                  |
|           |                   | -25.00 | 3334.1               | 4010.0               | 7344.1               | 4403.0            | -76.8              | 4326.1                  |

**REKENGEDEGENS SI Ø762/950 druk**

Berekening : Ontwerpend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n-1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(gem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{nk}$  : 1.0  
 $R_{b,calc,max,i}$  begrenzen op  $0.75 * R_{b,calc,max,i}$  : NEE  
 UGT draagvermogen zonder negatieve kleef : NEE

Paal : SI Ø762/950  
 Niveau paalkop [m] : N.A.P. 0.00  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS SI Ø762/950**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau<br>[m] | Eindniveau<br>[m] | Stapgrootte<br>[m] |
|----|--------------------|-------------------|--------------------|
| 1  | -8.00              | -25.00            | 0.50               |

**RESULTATEN SI Ø762/950 druk (n=1)**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Sondering     | 19-1008-14            | 19-1008-15            | 251.S01               | 19-1008-22            | 202.S03               |
|---------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| Niveau<br>[m] | $F_{netto,d}$<br>[kN] | $F_{netto,d}$<br>[kN] | $F_{netto,d}$<br>[kN] | $F_{netto,d}$<br>[kN] | $F_{netto,d}$<br>[kN] |
| -8.00         | <b>3239</b>           | 2988                  | <u>880</u>            | 2374                  | 2214                  |
| -8.50         | 3431                  | <b>3463</b>           | <u>924</u>            | 2110                  | 2547                  |
| -9.00         | 3594                  | <b>3848</b>           | <u>1485</u>           | 2197                  | 1948                  |
| -9.50         | 3761                  | <b>4026</b>           | <u>1582</u>           | 2285                  | 1868                  |
| -10.00        | 3067                  | <b>4103</b>           | <u>1672</u>           | 2394                  | 1773                  |
| -10.50        | 2825                  | <b>4293</b>           | <u>1722</u>           | 2462                  | 1784                  |
| -11.00        | 2732                  | <b>4414</b>           | <u>1747</u>           | 2410                  | 1808                  |
| -11.50        | 2736                  | <b>4531</b>           | <u>1845</u>           | 2265                  | <u>1808</u>           |
| -12.00        | 2758                  | <b>4696</b>           | <u>1927</u>           | 2321                  | <u>1553</u>           |
| -12.50        | 2574                  | <b>4765</b>           | <u>2029</u>           | 2380                  | <u>1598</u>           |
| -13.00        | 2606                  | <b>3596</b>           | <u>2134</u>           | 2163                  | <u>1764</u>           |
| -13.50        | 2593                  | <b>3466</b>           | <u>2231</u>           | 2017                  | <u>1956</u>           |
| -14.00        | 2714                  | <b>3402</b>           | <u>2279</u>           | <u>1990</u>           | 2095                  |
| -14.50        | 2795                  | <b>3328</b>           | <u>2254</u>           | <u>2016</u>           | 2175                  |
| -15.00        | 2864                  | <b>3146</b>           | <u>2309</u>           | <u>2049</u>           | 2241                  |
| -15.50        | 2888                  | <b>3057</b>           | <u>3031</u>           | <u>2057</u>           | 2309                  |
| -16.00        | <b>3128</b>           | 3013                  | <u>3115</u>           | <u>2056</u>           | 2377                  |
| -16.50        | 3198                  | 3055                  | <b>3242</b>           | <u>2061</u>           | 2527                  |
| -17.00        | <b>3366</b>           | 3033                  | 3360                  | <u>2056</u>           | 2694                  |
| -17.50        | <b>3456</b>           | 3047                  | 3432                  | <u>2253</u>           | 2772                  |
| -18.00        | <b>3540</b>           | 3039                  | 2925                  | <u>2708</u>           | 2867                  |
| -18.50        | <b>3620</b>           | 3051                  | 2960                  | <u>2805</u>           | 2954                  |
| -19.00        | <b>3925</b>           | 3062                  | 2947                  | <u>2905</u>           | 3045                  |
| -19.50        | <b>4073</b>           | 3086                  | <u>2966</u>           | 3026                  | 3131                  |
| -20.00        | <b>4352</b>           | 3180                  | <u>2979</u>           | 3168                  | 3174                  |
| -20.50        | <b>4504</b>           | 3514                  | <u>3011</u>           | 3228                  | 3213                  |
| -21.00        | <b>4646</b>           | 3690                  | <u>3051</u>           | 3410                  | 3412                  |
| -21.50        | <b>4882</b>           | 3770                  | <u>3074</u>           | 3515                  | 3903                  |
| -22.00        | <b>5068</b>           | 3956                  | <u>3093</u>           | 3547                  | 4217                  |
| -22.50        | <b>5237</b>           | 4138                  | <u>3208</u>           | 3732                  | 4943                  |
| -23.00        | <b>5104</b>           | 4251                  | <u>3290</u>           | 3944                  | 5005                  |
| -23.50        | 5217                  | 4363                  | <u>3455</u>           | 4083                  | <b>5377</b>           |
| -24.00        | 5326                  | 4419                  | <u>3523</u>           | 4353                  | <b>5597</b>           |
| -24.50        | 5431                  | 4505                  | <u>3689</u>           | 4557                  | <b>5676</b>           |
| -25.00        | 5531                  | 4545                  | <u>3969</u>           | 4869                  | <b>5575</b>           |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SAMENVATTINGSTABEL SI Ø762/950 druk (n=1)**

**Uitgangspunten**

- paal : SI Ø762/950  
 - paaltype : In de grond gevormde geschroefde paal; groutinjectie  
 - schachtafmeting : 860 mm  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            |                    |                    | $R_{e,paal}$<br>[kN] | $R_{b,paal}$<br>[kN] | $R_{c,paal}$<br>[kN] | $R_{e,d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40               | -8.00              | 3931.3               | 1500.8               | 5432.1               | 3256.6            | -17.3              | 3239.3                  |
|            |                    | -8.50              | 4068.3               | 1683.1               | 5751.4               | 3448.1            | -17.3              | 3430.8                  |
|            |                    | -9.00              | 4158.0               | 1865.5               | 6023.5               | 3611.2            | -17.3              | 3593.9                  |
|            |                    | -9.50              | 4268.3               | 2033.5               | 6301.8               | 3778.0            | -17.3              | 3760.7                  |
|            |                    | -10.00             | 2949.1               | 2194.9               | 5144.0               | 3083.9            | -17.3              | 3066.6                  |
|            |                    | -10.50             | 2374.4               | 2367.1               | 4741.5               | 2842.6            | -17.3              | 2825.3                  |
|            |                    | -11.00             | 2037.2               | 2549.5               | 4586.7               | 2749.8            | -17.3              | 2732.5                  |
|            |                    | -11.50             | 1861.3               | 2731.9               | 4593.2               | 2753.7            | -17.3              | 2736.4                  |
|            |                    | -12.00             | 1715.6               | 2914.2               | 4629.9               | 2775.7            | -17.3              | 2758.4                  |
|            |                    | -12.50             | 1225.3               | 3096.6               | 4321.9               | 2591.1            | -17.3              | 2573.7                  |
|            |                    | -13.00             | 1097.4               | 3278.1               | 4375.5               | 2623.2            | -17.3              | 2605.9                  |
|            |                    | -13.50             | 963.5                | 3391.0               | 4354.5               | 2610.6            | -17.3              | 2593.3                  |
|            |                    | -14.00             | 1095.4               | 3459.9               | 4555.3               | 2731.0            | -17.3              | 2713.6                  |
|            |                    | -14.50             | 1173.2               | 3517.7               | 4690.9               | 2812.3            | -17.3              | 2795.0                  |
|            |                    | -15.00             | 1200.9               | 3604.5               | 4805.4               | 2880.9            | -17.3              | 2863.6                  |
|            |                    | -15.50             | 1116.1               | 3729.6               | 4845.7               | 2905.1            | -17.3              | 2887.8                  |
|            |                    | -16.00             | 1466.3               | 3779.9               | 5246.1               | 3145.2            | -17.3              | 3127.8                  |
|            |                    | -16.50             | 1489.1               | 3873.8               | 5362.8               | 3215.1            | -17.3              | 3197.8                  |
|            |                    | -17.00             | 1690.8               | 3953.0               | 5643.8               | 3383.5            | -17.3              | 3366.2                  |
|            |                    | -17.50             | 1745.3               | 4048.9               | 5794.2               | 3473.7            | -17.3              | 3456.4                  |
|            |                    | -18.00             | 1784.8               | 4148.3               | 5933.1               | 3557.0            | -17.3              | 3539.7                  |
|            |                    | -18.50             | 1824.0               | 4242.8               | 6066.7               | 3637.1            | -17.3              | 3619.8                  |
|            |                    | -19.00             | 2241.8               | 4334.6               | 6576.4               | 3942.7            | -17.3              | 3925.4                  |
|            |                    | -19.50             | 2378.4               | 4444.0               | 6822.4               | 4090.2            | -17.3              | 4072.8                  |
|            |                    | -20.00             | 2735.5               | 4552.4               | 7287.9               | 4369.2            | -17.3              | 4351.9                  |
| -20.50     | 2861.9             | 4680.0             | 7541.9               | 4521.5               | -17.3                | 4504.2            |                    |                         |
| -21.00     | 2964.1             | 4814.8             | 7779.0               | 4663.7               | -17.3                | 4646.3            |                    |                         |
| -21.50     | 3227.3             | 4944.9             | 8172.2               | 4899.4               | -17.3                | 4882.0            |                    |                         |
| -22.00     | 3400.8             | 5080.9             | 8481.7               | 5085.0               | -17.3                | 5067.6            |                    |                         |
| -22.50     | 3543.3             | 5221.5             | 8764.8               | 5254.7               | -17.3                | 5237.4            |                    |                         |
| -23.00     | 3175.3             | 5366.3             | 8541.6               | 5120.9               | -17.3                | 5103.5            |                    |                         |
| -23.50     | 3221.3             | 5510.2             | 8731.5               | 5234.7               | -17.3                | 5217.4            |                    |                         |
| -24.00     | 3256.6             | 5656.1             | 8912.7               | 5343.3               | -17.3                | 5326.0            |                    |                         |
| -24.50     | 3286.3             | 5802.0             | 9088.3               | 5448.6               | -17.3                | 5431.3            |                    |                         |
| -25.00     | 3300.5             | 5953.5             | 9254.0               | 5548.0               | -17.3                | 5530.6            |                    |                         |
| 19-1008-15 | 0.75               | -8.00              | 3290.4               | 1704.0               | 4994.4               | 2994.2            | -6.3               | 2987.9                  |
|            |                    | -8.50              | 3931.2               | 1856.3               | 5787.5               | 3469.7            | -6.3               | 3463.4                  |
|            |                    | -9.00              | 4389.8               | 2038.7               | 6428.5               | 3854.0            | -6.3               | 3847.7                  |
|            |                    | -9.50              | 4504.2               | 2221.1               | 6725.3               | 4032.0            | -6.3               | 4025.7                  |
|            |                    | -10.00             | 4451.6               | 2403.4               | 6855.1               | 4109.8            | -6.3               | 4103.5                  |
|            |                    | -10.50             | 4585.9               | 2585.8               | 7171.7               | 4299.6            | -6.3               | 4293.3                  |
|            |                    | -11.00             | 4605.6               | 2768.2               | 7373.8               | 4420.8            | -6.3               | 4414.5                  |
|            |                    | -11.50             | 4618.4               | 2950.5               | 7568.9               | 4537.7            | -6.3               | 4531.5                  |
|            |                    | -12.00             | 4711.0               | 3132.9               | 7843.9               | 4702.6            | -6.3               | 4696.3                  |
|            |                    | -12.50             | 4642.4               | 3315.3               | 7957.7               | 4770.8            | -6.3               | 4764.5                  |
|            |                    | -13.00             | 2513.6               | 3494.6               | 6008.2               | 3602.0            | -6.3               | 3595.8                  |
|            |                    | -13.50             | 2137.7               | 3653.7               | 5791.5               | 3472.1            | -6.3               | 3465.8                  |
|            |                    | -14.00             | 1849.2               | 3836.1               | 5685.3               | 3408.4            | -6.3               | 3402.2                  |
|            |                    | -14.50             | 1543.5               | 4018.5               | 5562.0               | 3334.5            | -6.3               | 3328.3                  |
|            |                    | -15.00             | 1056.8               | 4200.8               | 5257.7               | 3152.1            | -6.3               | 3145.8                  |
|            |                    | -15.50             | 726.4                | 4383.2               | 5109.6               | 3063.3            | -6.3               | 3057.0                  |
|            |                    | -16.00             | 472.8                | 4564.1               | 5036.9               | 3019.7            | -6.3               | 3013.4                  |
|            |                    | -16.50             | 498.2                | 4608.1               | 5106.2               | 3061.3            | -6.3               | 3055.0                  |
|            |                    | -17.00             | 442.5                | 4627.9               | 5070.3               | 3039.8            | -6.3               | 3033.5                  |
|            |                    | -17.50             | 434.4                | 4658.0               | 5092.4               | 3053.0            | -6.3               | 3046.7                  |
|            |                    | -18.00             | 369.6                | 4709.1               | 5078.8               | 3044.8            | -6.3               | 3038.5                  |
|            |                    | -18.50             | 376.5                | 4722.6               | 5099.1               | 3057.0            | -6.3               | 3050.7                  |
|            |                    | -19.00             | 381.8                | 4736.8               | 5118.6               | 3068.7            | -6.3               | 3062.4                  |
|            |                    | -19.50             | 404.6                | 4753.9               | 5158.5               | 3092.6            | -6.3               | 3086.3                  |
|            |                    | -20.00             | 543.8                | 4771.5               | 5315.3               | 3186.6            | -6.3               | 3180.4                  |
| -20.50     | 1076.5             | 4795.2             | 5871.6               | 3520.2               | -6.3                 | 3513.9            |                    |                         |
| -21.00     | 1315.4             | 4850.8             | 6166.1               | 3696.7               | -6.3                 | 3690.5            |                    |                         |
| -21.50     | 1370.3             | 4929.0             | 6299.4               | 3776.6               | -6.3                 | 3770.3            |                    |                         |
| -22.00     | 1601.9             | 5007.4             | 6609.3               | 3962.4               | -6.3                 | 3956.1            |                    |                         |
| -22.50     | 1823.4             | 5089.0             | 6912.4               | 4144.1               | -6.3                 | 4137.8            |                    |                         |
| -23.00     | 1911.3             | 5189.4             | 7100.7               | 4257.0               | -6.3                 | 4250.8            |                    |                         |
| -23.50     | 1979.4             | 5309.0             | 7288.4               | 4369.6               | -6.3                 | 4363.3            |                    |                         |
| -24.00     | 1965.5             | 5415.9             | 7381.5               | 4425.3               | -6.3                 | 4419.1            |                    |                         |
| -24.50     | 1973.5             | 5552.0             | 7525.5               | 4511.7               | -6.3                 | 4505.4            |                    |                         |
| -25.00     | 1901.3             | 5689.6             | 7590.9               | 4550.9               | -6.3                 | 4544.6            |                    |                         |
| 251.S01    | -1.05              | -8.00              | 397.9                | 1125.3               | 1523.3               | 913.2             | -33.6              | 879.6                   |
|            |                    | -8.50              | 385.3                | 1212.7               | 1597.9               | 958.0             | -33.6              | 924.4                   |
|            |                    | -9.00              | 1307.1               | 1225.7               | 2532.8               | 1518.5            | -33.6              | 1484.9                  |
|            |                    | -9.50              | 1388.7               | 1306.3               | 2695.1               | 1615.8            | -33.6              | 1582.1                  |
|            |                    | -10.00             | 1415.6               | 1428.6               | 2844.2               | 1705.1            | -33.6              | 1671.5                  |
|            |                    | -10.50             | 1356.4               | 1572.3               | 2928.7               | 1755.8            | -33.6              | 1722.2                  |
|            |                    | -11.00             | 1288.3               | 1681.4               | 2969.8               | 1780.4            | -33.6              | 1746.8                  |
|            |                    | -11.50             | 1386.5               | 1747.8               | 3134.2               | 1879.0            | -33.6              | 1845.4                  |
|            |                    | -12.00             | 1456.4               | 1813.6               | 3269.9               | 1960.4            | -33.6              | 1926.8                  |
|            |                    | -12.50             | 1515.7               | 1925.6               | 3441.3               | 2063.1            | -33.6              | 2029.5                  |
|            |                    | -13.00             | 1557.0               | 2058.0               | 3615.0               | 2167.3            | -33.6              | 2133.6                  |
| -13.50     | 1594.4             | 2182.8             | 3777.2               | 2264.5               | -33.6                | 2230.9            |                    |                         |
| -14.00     | 1501.5             | 2356.3             | 3857.8               | 2312.8               | -33.6                | 2279.2            |                    |                         |
| -14.50     | 1286.3             | 2528.6             | 3815.0               | 2287.1               | -33.6                | 2253.5            |                    |                         |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld |                    | Beziwkdraagvermogen         |                             |                             | Rekenwaarden           |                          |                                |
|------------|----------|--------------------|-----------------------------|-----------------------------|-----------------------------|------------------------|--------------------------|--------------------------------|
|            | niveau   | paalpunt<br>niveau | R <sub>b,real</sub><br>[kN] | R <sub>r,real</sub><br>[kN] | R <sub>c,real</sub><br>[kN] | R <sub>d</sub><br>[kN] | F <sub>hkd</sub><br>[kN] | R <sub>z netto;d</sub><br>[kN] |
| 251.S01    | -1.05    | -15.00             | 1191.7                      | 2715.2                      | 3906.9                      | 2342.3                 | -33.6                    | 2308.7                         |
|            |          | -15.50             | 2313.0                      | 2798.8                      | 5111.8                      | 3064.6                 | -33.6                    | 3031.0                         |
|            |          | -16.00             | 2285.3                      | 2967.1                      | 5252.5                      | 3149.0                 | -33.6                    | 3115.3                         |
|            |          | -16.50             | 2314.4                      | 3149.5                      | 5463.9                      | 3275.7                 | -33.6                    | 3242.1                         |
|            |          | -17.00             | 2330.9                      | 3329.8                      | 5660.7                      | 3393.7                 | -33.6                    | 3360.1                         |
|            |          | -17.50             | 2278.3                      | 3502.0                      | 5780.2                      | 3465.4                 | -33.6                    | 3431.7                         |
|            |          | -18.00             | 1271.1                      | 3664.5                      | 4935.7                      | 2959.0                 | -33.6                    | 2925.4                         |
|            |          | -18.50             | 1145.8                      | 3848.0                      | 4993.7                      | 2993.8                 | -33.6                    | 2960.2                         |
|            |          | -19.00             | 1013.8                      | 3957.4                      | 4971.2                      | 2980.3                 | -33.6                    | 2946.7                         |
|            |          | -19.50             | 930.4                       | 4073.7                      | 5004.1                      | 3000.0                 | -33.6                    | 2966.4                         |
|            |          | -20.00             | 809.4                       | 4215.4                      | 5024.9                      | 3012.5                 | -33.6                    | 2978.9                         |
|            |          | -20.50             | 659.5                       | 4419.7                      | 5079.2                      | 3045.1                 | -33.6                    | 3011.4                         |
|            |          | -21.00             | 516.9                       | 4628.5                      | 5145.5                      | 3084.8                 | -33.6                    | 3051.2                         |
|            |          | -21.50             | 468.6                       | 4715.2                      | 5183.8                      | 3107.8                 | -33.6                    | 3074.2                         |
|            |          | -22.00             | 472.6                       | 4742.3                      | 5214.9                      | 3126.4                 | -33.6                    | 3092.8                         |
|            |          | -22.50             | 629.6                       | 4778.2                      | 5407.7                      | 3242.0                 | -33.6                    | 3208.4                         |
|            |          | -23.00             | 708.0                       | 4835.6                      | 5543.6                      | 3323.5                 | -33.6                    | 3289.9                         |
|            |          | -23.50             | 907.3                       | 4910.8                      | 5818.2                      | 3488.1                 | -33.6                    | 3454.5                         |
|            |          | -24.00             | 919.5                       | 5012.6                      | 5932.1                      | 3556.4                 | -33.6                    | 3522.8                         |
|            |          | -24.50             | 1104.5                      | 5105.3                      | 6209.8                      | 3722.9                 | -33.6                    | 3689.3                         |
|            |          | -25.00             | 1486.9                      | 5189.5                      | 6676.4                      | 4002.7                 | -33.6                    | 3969.0                         |
| 19-1008-22 | 0.18     | -8.00              | 3029.3                      | 989.8                       | 4019.0                      | 2409.5                 | -35.1                    | 2374.4                         |
|            |          | -8.50              | 2443.4                      | 1135.2                      | 3578.6                      | 2145.5                 | -35.1                    | 2110.4                         |
|            |          | -9.00              | 2444.5                      | 1279.3                      | 3723.8                      | 2232.5                 | -35.1                    | 2197.4                         |
|            |          | -9.50              | 2439.8                      | 1431.0                      | 3870.7                      | 2320.6                 | -35.1                    | 2285.5                         |
|            |          | -10.00             | 2468.6                      | 1583.0                      | 4051.6                      | 2429.0                 | -35.1                    | 2393.9                         |
|            |          | -10.50             | 2429.8                      | 1735.1                      | 4164.9                      | 2497.0                 | -35.1                    | 2461.9                         |
|            |          | -11.00             | 2191.7                      | 1886.6                      | 4078.3                      | 2445.0                 | -35.1                    | 2409.9                         |
|            |          | -11.50             | 1798.0                      | 2037.8                      | 3835.9                      | 2299.7                 | -35.1                    | 2264.6                         |
|            |          | -12.00             | 1799.0                      | 2130.8                      | 3929.7                      | 2356.0                 | -35.1                    | 2320.9                         |
|            |          | -12.50             | 1813.9                      | 2213.7                      | 4027.6                      | 2414.6                 | -35.1                    | 2379.5                         |
|            |          | -13.00             | 1363.4                      | 2302.8                      | 3666.2                      | 2198.0                 | -35.1                    | 2162.9                         |
|            |          | -13.50             | 1014.9                      | 2407.8                      | 3422.7                      | 2052.0                 | -35.1                    | 2016.9                         |
|            |          | -14.00             | 879.6                       | 2498.4                      | 3378.0                      | 2025.2                 | -35.1                    | 1990.1                         |
|            |          | -14.50             | 844.3                       | 2577.4                      | 3421.7                      | 2051.4                 | -35.1                    | 2016.3                         |
|            |          | -15.00             | 843.1                       | 2633.2                      | 3476.3                      | 2084.1                 | -35.1                    | 2049.0                         |
|            |          | -15.50             | 765.0                       | 2723.9                      | 3488.9                      | 2091.7                 | -35.1                    | 2056.6                         |
|            |          | -16.00             | 690.2                       | 2797.0                      | 3487.1                      | 2090.6                 | -35.1                    | 2055.5                         |
|            |          | -16.50             | 656.8                       | 2839.5                      | 3496.3                      | 2096.1                 | -35.1                    | 2061.0                         |
|            |          | -17.00             | 615.7                       | 2872.9                      | 3488.6                      | 2091.5                 | -35.1                    | 2056.4                         |
|            |          | -17.50             | 921.4                       | 2894.7                      | 3816.1                      | 2287.8                 | -35.1                    | 2252.7                         |
|            |          | -18.00             | 1642.9                      | 2931.8                      | 4574.7                      | 2742.6                 | -35.1                    | 2707.5                         |
| -18.50     | 1697.4   | 3039.2             | 4736.7                      | 2839.7                      | -35.1                       | 2804.6                 |                          |                                |
| -19.00     | 1760.8   | 3142.8             | 4903.6                      | 2939.8                      | -35.1                       | 2904.7                 |                          |                                |
| -19.50     | 1873.3   | 3232.6             | 5105.9                      | 3061.1                      | -35.1                       | 3026.0                 |                          |                                |
| -20.00     | 2009.4   | 3333.5             | 5342.9                      | 3203.1                      | -35.1                       | 3168.0                 |                          |                                |
| -20.50     | 1971.0   | 3471.4             | 5442.4                      | 3262.8                      | -35.1                       | 3227.7                 |                          |                                |
| -21.00     | 2180.5   | 3566.4             | 5746.8                      | 3445.3                      | -35.1                       | 3410.2                 |                          |                                |
| -21.50     | 2225.5   | 3695.3             | 5920.8                      | 3549.6                      | -35.1                       | 3514.5                 |                          |                                |
| -22.00     | 2135.5   | 3839.0             | 5974.4                      | 3581.8                      | -35.1                       | 3546.7                 |                          |                                |
| -22.50     | 2345.7   | 3938.6             | 6284.2                      | 3767.5                      | -35.1                       | 3732.4                 |                          |                                |
| -23.00     | 2598.2   | 4039.6             | 6637.8                      | 3979.5                      | -35.1                       | 3944.4                 |                          |                                |
| -23.50     | 2712.3   | 4156.8             | 6869.2                      | 4118.2                      | -35.1                       | 4083.1                 |                          |                                |
| -24.00     | 3046.1   | 4272.8             | 7318.9                      | 4387.8                      | -35.1                       | 4352.7                 |                          |                                |
| -24.50     | 3258.6   | 4400.9             | 7659.6                      | 4592.1                      | -35.1                       | 4557.0                 |                          |                                |
| -25.00     | 3643.4   | 4537.3             | 8180.6                      | 4904.5                      | -35.1                       | 4869.4                 |                          |                                |
| 202.S03    | 0.03     | -8.00              | 3214.9                      | 628.3                       | 3843.2                      | 2304.1                 | -90.5                    | 2213.5                         |
|            |          | -8.50              | 3626.1                      | 772.7                       | 4398.7                      | 2637.1                 | -90.5                    | 2546.6                         |
|            |          | -9.00              | 2458.8                      | 941.5                       | 3400.3                      | 2038.5                 | -90.5                    | 1948.0                         |
|            |          | -9.50              | 2142.6                      | 1123.9                      | 3266.4                      | 1958.3                 | -90.5                    | 1867.8                         |
|            |          | -10.00             | 1801.9                      | 1306.2                      | 3108.1                      | 1863.4                 | -90.5                    | 1772.9                         |
|            |          | -10.50             | 1638.4                      | 1488.6                      | 3127.0                      | 1874.7                 | -90.5                    | 1784.2                         |
|            |          | -11.00             | 1509.5                      | 1656.5                      | 3166.0                      | 1898.1                 | -90.5                    | 1807.6                         |
|            |          | -11.50             | 1365.1                      | 1802.4                      | 3167.4                      | 1898.9                 | -90.5                    | 1808.4                         |
|            |          | -12.00             | 776.5                       | 1964.1                      | 2740.6                      | 1643.0                 | -90.5                    | 1552.5                         |
|            |          | -12.50             | 794.1                       | 2022.0                      | 2816.1                      | 1688.3                 | -90.5                    | 1597.8                         |
|            |          | -13.00             | 1012.7                      | 2080.3                      | 3093.0                      | 1854.3                 | -90.5                    | 1763.8                         |
|            |          | -13.50             | 1290.8                      | 2123.2                      | 3413.9                      | 2046.7                 | -90.5                    | 1956.2                         |
|            |          | -14.00             | 1438.9                      | 2207.3                      | 3646.2                      | 2186.0                 | -90.5                    | 2095.5                         |
|            |          | -14.50             | 1496.7                      | 2282.6                      | 3779.2                      | 2265.7                 | -90.5                    | 2175.2                         |
|            |          | -15.00             | 1515.9                      | 2372.8                      | 3888.7                      | 2331.4                 | -90.5                    | 2240.9                         |
|            |          | -15.50             | 1549.2                      | 2452.5                      | 4001.7                      | 2399.1                 | -90.5                    | 2308.6                         |
|            |          | -16.00             | 1585.7                      | 2529.8                      | 4115.5                      | 2467.3                 | -90.5                    | 2376.8                         |
|            |          | -16.50             | 1766.8                      | 2598.6                      | 4365.4                      | 2617.1                 | -90.5                    | 2526.6                         |
|            |          | -17.00             | 1967.7                      | 2676.4                      | 4644.1                      | 2784.2                 | -90.5                    | 2693.7                         |
|            |          | -17.50             | 2014.0                      | 2760.7                      | 4774.7                      | 2862.5                 | -90.5                    | 2772.0                         |
|            |          | -18.00             | 2070.1                      | 2862.3                      | 4932.4                      | 2957.1                 | -90.5                    | 2866.6                         |
| -18.50     | 2118.9   | 2959.2             | 5078.0                      | 3044.4                      | -90.5                       | 2953.9                 |                          |                                |
| -19.00     | 2158.2   | 3071.8             | 5230.0                      | 3135.5                      | -90.5                       | 3045.0                 |                          |                                |
| -19.50     | 2189.1   | 3183.9             | 5373.1                      | 3221.3                      | -90.5                       | 3130.8                 |                          |                                |
| -20.00     | 2144.0   | 3301.7             | 5445.7                      | 3264.8                      | -90.5                       | 3174.3                 |                          |                                |
| -20.50     | 2111.9   | 3397.5             | 5509.4                      | 3303.0                      | -90.5                       | 3212.5                 |                          |                                |
| -21.00     | 2370.7   | 3472.2             | 5842.9                      | 3503.0                      | -90.5                       | 3412.5                 |                          |                                |
| -21.50     | 3102.7   | 3558.7             | 6661.4                      | 3993.6                      | -90.5                       | 3903.1                 |                          |                                |
| -22.00     | 3494.2   | 3690.1             | 7184.3                      | 4307.1                      | -90.5                       | 4216.6                 |                          |                                |
| -22.50     | 4554.5   | 3842.0             | 8396.5                      | 5033.9                      | -90.5                       | 4943.4                 |                          |                                |
| -23.00     | 4487.7   | 4011.6             | 8499.3                      | 5095.5                      | -90.5                       | 5005.0                 |                          |                                |
| -23.50     | 4938.7   | 4181.5             | 9120.2                      | 5467.7                      | -90.5                       | 5377.2                 |                          |                                |
| -24.00     | 5127.1   | 4359.4             | 9486.5                      | 5687.3                      | -90.5                       | 5596.8                 |                          |                                |
| -24.50     | 5076.2   | 4541.8             | 9618.0                      | 5766.2                      | -90.5                       | 5675.7                 |                          |                                |
| -25.00     | 4725.4   | 4724.1             | 9449.5                      | 5665.2                      | -90.5                       | 5574.7                 |                          |                                |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**REKENGEGEVENS MV Ø914/1074 druk**

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(gem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{f,dk}$  : 1.0  
 $R_{z,calc,max}$  begrenzen op  $0.75 * R_{z,calc,max}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : MV Ø914/1074  
 Niveau paalkop [m] : N.A.P. 0.00  
 $E_{d,1}$  [kN] : 0.00  $E_{d,2}$  [kN] : 0.00  
 $S_{req,1}$  [m] : 0.15  $S_{req,2}$  [m] : 0.05  
 Bovenbel. [kN/m²] : 0.00

**PAALPUNTNIVEAUS MV Ø914/1074**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

Nr Beginniveau Eindniveau Stapgrootte

|   | [m]    | [m]    | [m]  |
|---|--------|--------|------|
| 1 | -10.00 | -25.00 | 0.50 |

**RESULTATEN MV Ø914/1074 druk) (n=1)**

**Sondering : 19-1008-14**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | $R_b$ | $R_s$ | $R_{z,calc}$ | $R_{z,k}$ | $R_{z,d}$ | $F_{n,k,d}$ | $R_{n,d}$ | $F_{z,tot,1}$ | U.C. | $S_{1,1}$ | $S_{1,2}$ |
|--------|-------|-------|--------------|-----------|-----------|-------------|-----------|---------------|------|-----------|-----------|
| [m]    | [kN]  | [kN]  | [kN]         | [kN]      | [kN]      | [kN]        | [kN]      | [kN]          |      | [mm]      | [mm]      |
| -10.00 | 3551  | 3946  | 7497         | 5394      | 4495      | -20.0       | 4475      | -20.0         | 0.00 | -0.0      | -0.0      |
| -10.50 | 3180  | 4256  | 7436         | 5349      | 4458      | -20.0       | 4438      | -20.0         | 0.00 | -0.0      | -0.0      |
| -11.00 | 2945  | 4584  | 7529         | 5417      | 4514      | -20.0       | 4494      | -20.0         | 0.00 | -0.0      | -0.0      |
| -11.50 | 2806  | 4912  | 7718         | 5552      | 4627      | -20.0       | 4607      | -20.0         | 0.00 | -0.0      | -0.0      |
| -12.00 | 2070  | 5240  | 7309         | 5258      | 4382      | -20.0       | 4362      | -20.0         | 0.00 | -0.0      | -0.0      |
| -12.50 | 1832  | 5568  | 7399         | 5323      | 4436      | -20.0       | 4416      | -20.0         | 0.00 | -0.0      | -0.0      |
| -13.00 | 1629  | 5894  | 7523         | 5412      | 4510      | -20.0       | 4490      | -20.0         | 0.00 | -0.0      | -0.0      |
| -13.50 | 1501  | 6093  | 7593         | 5463      | 4552      | -20.0       | 4532      | -20.0         | 0.00 | -0.0      | -0.0      |
| -14.00 | 1626  | 6188  | 7814         | 5622      | 4685      | -20.0       | 4665      | -20.0         | 0.00 | -0.0      | -0.0      |
| -14.50 | 1741  | 6289  | 8030         | 5777      | 4814      | -20.0       | 4794      | -20.0         | 0.00 | -0.0      | -0.0      |
| -15.00 | 1782  | 6445  | 8227         | 5919      | 4933      | -20.0       | 4912      | -20.0         | 0.00 | -0.0      | -0.0      |
| -15.50 | 1783  | 6670  | 8453         | 6081      | 5068      | -20.0       | 5048      | -20.0         | 0.00 | -0.0      | -0.0      |
| -16.00 | 2173  | 6760  | 8934         | 6427      | 5356      | -20.0       | 5336      | -20.0         | 0.00 | -0.0      | -0.0      |
| -16.50 | 2255  | 6929  | 9184         | 6607      | 5506      | -20.0       | 5486      | -20.0         | 0.00 | -0.0      | -0.0      |
| -17.00 | 2488  | 7072  | 9560         | 6878      | 5731      | -20.0       | 5711      | -20.0         | 0.00 | -0.0      | -0.0      |
| -17.50 | 2558  | 7244  | 9802         | 7052      | 5876      | -20.0       | 5856      | -20.0         | 0.00 | -0.0      | -0.0      |
| -18.00 | 2605  | 7423  | 10028        | 7214      | 6012      | -20.0       | 5992      | -20.0         | 0.00 | -0.0      | -0.0      |
| -18.50 | 2711  | 7593  | 10304        | 7413      | 6177      | -20.0       | 6157      | -20.0         | 0.00 | -0.0      | -0.0      |
| -19.00 | 3260  | 7758  | 11018        | 7927      | 6606      | -20.0       | 6586      | -20.0         | 0.00 | -0.0      | -0.0      |
| -19.50 | 3486  | 7954  | 11441        | 8231      | 6859      | -20.0       | 6839      | -20.0         | 0.00 | -0.0      | -0.0      |
| -20.00 | 3957  | 8149  | 12107        | 8710      | 7258      | -20.0       | 7238      | -20.0         | 0.00 | -0.0      | -0.0      |
| -20.50 | 4123  | 8379  | 12502        | 8994      | 7495      | -20.0       | 7475      | -20.0         | 0.00 | -0.0      | -0.0      |
| -21.00 | 4271  | 8621  | 12892        | 9275      | 7729      | -20.0       | 7709      | -20.0         | 0.00 | -0.0      | -0.0      |
| -21.50 | 4621  | 8855  | 13476        | 9695      | 8079      | -20.0       | 8059      | -20.0         | 0.00 | -0.0      | -0.0      |
| -22.00 | 4864  | 9099  | 13964        | 10046     | 8372      | -20.0       | 8351      | -20.0         | 0.00 | -0.0      | -0.0      |
| -22.50 | 4432  | 9352  | 13785        | 9917      | 8264      | -20.0       | 8244      | -20.0         | 0.00 | -0.0      | -0.0      |
| -23.00 | 4547  | 9613  | 14159        | 10187     | 8489      | -20.0       | 8469      | -20.0         | 0.00 | -0.0      | -0.0      |
| -23.50 | 4664  | 9871  | 14535        | 10457     | 8714      | -20.0       | 8694      | -20.0         | 0.00 | -0.0      | -0.0      |
| -24.00 | 4748  | 10134 | 14882        | 10707     | 8922      | -20.0       | 8902      | -20.0         | 0.00 | -0.0      | -0.0      |
| -24.50 | 4803  | 10396 | 15199        | 10935     | 9112      | -20.0       | 9092      | -20.0         | 0.00 | -0.0      | -0.0      |
| -25.00 | 4831  | 10668 | 15499        | 11150     | 9292      | -20.0       | 9272      | -20.0         | 0.00 | -0.0      | -0.0      |

**Sondering : 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | $R_b$ | $R_s$ | $R_{z,calc}$ | $R_{z,k}$ | $R_{z,d}$ | $F_{n,k,d}$ | $R_{n,d}$ | $F_{z,tot,1}$ | U.C. | $S_{1,1}$ | $S_{1,2}$ |
|--------|-------|-------|--------------|-----------|-----------|-------------|-----------|---------------|------|-----------|-----------|
| [m]    | [kN]  | [kN]  | [kN]         | [kN]      | [kN]      | [kN]        | [kN]      | [kN]          |      | [mm]      | [mm]      |
| -10.00 | 6399  | 4304  | 10703        | 7700      | 6417      | -7.3        | 6410      | -7.3          | 0.00 | -0.0      | -0.0      |
| -10.50 | 6605  | 4632  | 11237        | 8084      | 6737      | -7.3        | 6730      | -7.3          | 0.00 | -0.0      | -0.0      |
| -11.00 | 6609  | 4960  | 11569        | 8323      | 6936      | -7.3        | 6928      | -7.3          | 0.00 | -0.0      | -0.0      |
| -11.50 | 6602  | 5288  | 11890        | 8554      | 7128      | -7.3        | 7121      | -7.3          | 0.00 | -0.0      | -0.0      |
| -12.00 | 6715  | 5616  | 12330        | 8871      | 7392      | -7.3        | 7385      | -7.3          | 0.00 | -0.0      | -0.0      |
| -12.50 | 3567  | 5944  | 9510         | 6842      | 5702      | -7.3        | 5694      | -7.3          | 0.00 | -0.0      | -0.0      |
| -13.00 | 3190  | 6266  | 9456         | 6803      | 5669      | -7.3        | 5662      | -7.3          | 0.00 | -0.0      | -0.0      |
| -13.50 | 2877  | 6552  | 9429         | 6783      | 5653      | -7.3        | 5645      | -7.3          | 0.00 | -0.0      | -0.0      |
| -14.00 | 2538  | 6880  | 9418         | 6776      | 5646      | -7.3        | 5639      | -7.3          | 0.00 | -0.0      | -0.0      |
| -14.50 | 1882  | 7208  | 9090         | 6539      | 5449      | -7.3        | 5442      | -7.3          | 0.00 | -0.0      | -0.0      |
| -15.00 | 1435  | 7536  | 8970         | 6454      | 5378      | -7.3        | 5371      | -7.3          | 0.00 | -0.0      | -0.0      |
| -15.50 | 1014  | 7864  | 8878         | 6387      | 5322      | -7.3        | 5315      | -7.3          | 0.00 | -0.0      | -0.0      |
| -16.00 | 683.7 | 8189  | 8873         | 6383      | 5319      | -7.3        | 5312      | -7.3          | 0.00 | -0.0      | -0.0      |
| -16.50 | 739.4 | 8268  | 9007         | 6480      | 5400      | -7.3        | 5393      | -7.3          | 0.00 | -0.0      | -0.0      |
| -17.00 | 656.8 | 8304  | 8960         | 6446      | 5372      | -7.3        | 5365      | -7.3          | 0.00 | -0.0      | -0.0      |
| -17.50 | 644.7 | 8358  | 9002         | 6477      | 5397      | -7.3        | 5390      | -7.3          | 0.00 | -0.0      | -0.0      |
| -18.00 | 551.2 | 8450  | 9001         | 6475      | 5396      | -7.3        | 5389      | -7.3          | 0.00 | -0.0      | -0.0      |
| -18.50 | 558.9 | 8474  | 9033         | 6498      | 5415      | -7.3        | 5408      | -7.3          | 0.00 | -0.0      | -0.0      |
| -19.00 | 566.3 | 8499  | 9066         | 6522      | 5435      | -7.3        | 5428      | -7.3          | 0.00 | -0.0      | -0.0      |
| -19.50 | 611.1 | 8530  | 9141         | 6576      | 5480      | -7.3        | 5473      | -7.3          | 0.00 | -0.0      | -0.0      |
| -20.00 | 844.6 | 8562  | 9406         | 6767      | 5639      | -7.3        | 5632      | -7.3          | 0.00 | -0.0      | -0.0      |
| -20.50 | 1640  | 8604  | 10244        | 7370      | 6142      | -7.3        | 6135      | -7.3          | 0.00 | -0.0      | -0.0      |
| -21.00 | 1941  | 8704  | 10645        | 7659      | 6382      | -7.3        | 6375      | -7.3          | 0.00 | -0.0      | -0.0      |
| -21.50 | 2009  | 8845  | 10854        | 7808      | 6507      | -7.3        | 6500      | -7.3          | 0.00 | -0.0      | -0.0      |
| -22.00 | 2381  | 8986  | 11367        | 8178      | 6815      | -7.3        | 6808      | -7.3          | 0.00 | -0.0      | -0.0      |
| -22.50 | 2659  | 9133  | 11791        | 8483      | 7069      | -7.3        | 7062      | -7.3          | 0.00 | -0.0      | -0.0      |
| -23.00 | 2672  | 9313  | 11985        | 8622      | 7185      | -7.3        | 7178      | -7.3          | 0.00 | -0.0      | -0.0      |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**Sondering : 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,k</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>o,tot,t,j</sub> [kN] | U.C. | S <sub>1,j</sub> [mm] | S <sub>1,j</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|-----------------------|-----------------------------|------|-----------------------|-----------------------|
| -23.50     | 2742                | 9528                | 12270                    | 8827                  | 7356                  | -7.3                    | 7349                  | -7.3                        | 0.00 | -0.0                  | -0.0                  |
| -24.00     | 2833                | 9720                | 12554                    | 9032                  | 7526                  | -7.3                    | 7519                  | -7.3                        | 0.00 | -0.0                  | -0.0                  |
| -24.50     | 2833                | 9965                | 12798                    | 9207                  | 7673                  | -7.3                    | 7666                  | -7.3                        | 0.00 | -0.0                  | -0.0                  |
| -25.00     | 2714                | 10212               | 12926                    | 9299                  | 7750                  | -7.3                    | 7742                  | -7.3                        | 0.00 | -0.0                  | -0.0                  |

**Sondering : 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,k</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>o,tot,t,j</sub> [kN] | U.C. | S <sub>1,j</sub> [mm] | S <sub>1,j</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|-----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 2065                | 2452                | 4517                     | 3250                  | 2708                  | -38.8                   | 2669                  | -38.8                       | 0.01 | -0.1                  | -0.0                  |
| -10.50     | 1972                | 2711                | 4683                     | 3369                  | 2808                  | -38.8                   | 2769                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.00     | 1865                | 2907                | 4772                     | 3433                  | 2861                  | -38.8                   | 2822                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.50     | 2005                | 3026                | 5032                     | 3620                  | 3016                  | -38.8                   | 2978                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.00     | 2141                | 3145                | 5286                     | 3803                  | 3169                  | -38.8                   | 3130                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.50     | 2226                | 3346                | 5572                     | 4009                  | 3341                  | -38.8                   | 3302                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.00     | 2257                | 3584                | 5841                     | 4202                  | 3502                  | -38.8                   | 3463                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.50     | 2337                | 3808                | 6145                     | 4421                  | 3684                  | -38.8                   | 3645                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.00     | 2195                | 4120                | 6316                     | 4544                  | 3786                  | -38.8                   | 3748                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.50     | 1873                | 4430                | 6303                     | 4534                  | 3779                  | -38.8                   | 3740                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.00     | 2064                | 4710                | 6775                     | 4874                  | 4061                  | -38.8                   | 4023                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.50     | 3246                | 4815                | 8061                     | 5799                  | 4833                  | -38.8                   | 4794                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -16.00     | 3376                | 5118                | 8494                     | 6111                  | 5092                  | -38.8                   | 5053                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -16.50     | 3398                | 5446                | 8844                     | 6363                  | 5302                  | -38.8                   | 5263                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -17.00     | 3426                | 5770                | 9196                     | 6616                  | 5513                  | -38.8                   | 5475                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -17.50     | 1927                | 6080                | 8006                     | 5760                  | 4800                  | -38.8                   | 4761                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -18.00     | 1679                | 6372                | 8051                     | 5792                  | 4827                  | -38.8                   | 4788                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -18.50     | 1701                | 6647                | 8347                     | 6005                  | 5004                  | -38.8                   | 4966                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -19.00     | 1406                | 6773                | 8179                     | 5884                  | 4903                  | -38.8                   | 4864                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -19.50     | 1321                | 6955                | 8275                     | 5953                  | 4961                  | -38.8                   | 4922                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -20.00     | 1229                | 7209                | 8439                     | 6071                  | 5059                  | -38.8                   | 5020                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -20.50     | 978.9               | 7483                | 8462                     | 6088                  | 5073                  | -38.8                   | 5034                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -21.00     | 767.3               | 7724                | 8492                     | 6109                  | 5091                  | -38.8                   | 5052                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -21.50     | 695.6               | 7825                | 8520                     | 6130                  | 5108                  | -38.8                   | 5069                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -22.00     | 700.4               | 7856                | 8556                     | 6156                  | 5130                  | -38.8                   | 5091                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -22.50     | 932.4               | 7897                | 8830                     | 6352                  | 5294                  | -38.8                   | 5255                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -23.00     | 1154                | 7964                | 9118                     | 6560                  | 5466                  | -38.8                   | 5427                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -23.50     | 1342                | 8051                | 9393                     | 6757                  | 5631                  | -38.8                   | 5592                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -24.00     | 1354                | 8168                | 9522                     | 6850                  | 5709                  | -38.8                   | 5670                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -24.50     | 1711                | 8275                | 9987                     | 7185                  | 5987                  | -38.8                   | 5948                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |
| -25.00     | 2326                | 8373                | 10699                    | 7697                  | 6414                  | -38.8                   | 6375                  | -38.8                       | 0.01 | -0.0                  | -0.0                  |

**Sondering : 19-1008-22**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,k</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>o,tot,t,j</sub> [kN] | U.C. | S <sub>1,j</sub> [mm] | S <sub>1,j</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|-----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 3410                | 2846                | 6256                     | 4501                  | 3751                  | -40.6                   | 3710                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -10.50     | 3042                | 3120                | 6162                     | 4433                  | 3694                  | -40.6                   | 3653                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -11.00     | 2633                | 3392                | 6025                     | 4334                  | 3612                  | -40.6                   | 3571                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -11.50     | 2545                | 3664                | 6209                     | 4467                  | 3723                  | -40.6                   | 3682                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -12.00     | 2605                | 3831                | 6436                     | 4630                  | 3859                  | -40.6                   | 3818                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -12.50     | 2030                | 3980                | 6010                     | 4324                  | 3603                  | -40.6                   | 3563                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -13.00     | 1531                | 4140                | 5671                     | 4080                  | 3400                  | -40.6                   | 3359                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -13.50     | 1349                | 4329                | 5678                     | 4085                  | 3404                  | -40.6                   | 3363                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -14.00     | 1293                | 4492                | 5785                     | 4162                  | 3468                  | -40.6                   | 3428                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -14.50     | 1257                | 4634                | 5891                     | 4238                  | 3532                  | -40.6                   | 3491                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -15.00     | 1251                | 4734                | 5986                     | 4306                  | 3589                  | -40.6                   | 3548                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -15.50     | 1136                | 4897                | 6033                     | 4340                  | 3617                  | -40.6                   | 3576                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -16.00     | 1024                | 5029                | 6053                     | 4355                  | 3629                  | -40.6                   | 3588                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -16.50     | 974.9               | 5105                | 6080                     | 4374                  | 3645                  | -40.6                   | 3605                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -17.00     | 932.8               | 5165                | 6098                     | 4387                  | 3656                  | -40.6                   | 3615                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -17.50     | 1504                | 5205                | 6709                     | 4826                  | 4022                  | -40.6                   | 3981                  | -40.6                       | 0.01 | -0.1                  | -0.0                  |
| -18.00     | 2435                | 5271                | 7706                     | 5544                  | 4620                  | -40.6                   | 4579                  | -40.6                       | 0.01 | -0.1                  | -0.0                  |
| -18.50     | 2506                | 5464                | 7970                     | 5734                  | 4778                  | -40.6                   | 4738                  | -40.6                       | 0.01 | -0.1                  | -0.0                  |
| -19.00     | 2589                | 5651                | 8240                     | 5928                  | 4940                  | -40.6                   | 4899                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -19.50     | 2746                | 5812                | 8558                     | 6157                  | 5130                  | -40.6                   | 5090                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -20.00     | 2937                | 5993                | 8931                     | 6425                  | 5354                  | -40.6                   | 5313                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -20.50     | 2954                | 6241                | 9196                     | 6615                  | 5513                  | -40.6                   | 5472                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -21.00     | 3169                | 6412                | 9581                     | 6893                  | 5744                  | -40.6                   | 5704                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -21.50     | 3223                | 6644                | 9867                     | 7099                  | 5916                  | -40.6                   | 5875                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -22.00     | 3077                | 6902                | 9979                     | 7179                  | 5983                  | -40.6                   | 5942                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -22.50     | 3398                | 7081                | 10479                    | 7539                  | 6282                  | -40.6                   | 6242                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -23.00     | 3734                | 7263                | 10997                    | 7912                  | 6593                  | -40.6                   | 6552                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -23.50     | 3933                | 7474                | 11407                    | 8207                  | 6839                  | -40.6                   | 6798                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -24.00     | 4381                | 7682                | 12063                    | 8679                  | 7232                  | -40.6                   | 7192                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -24.50     | 4726                | 7913                | 12638                    | 9092                  | 7577                  | -40.6                   | 7536                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |
| -25.00     | 5244                | 8158                | 13402                    | 9642                  | 8035                  | -40.6                   | 7994                  | -40.6                       | 0.01 | -0.0                  | -0.0                  |

**Sondering : 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>0</sub> [kN] | R <sub>0</sub> [kN] | R <sub>o,caal</sub> [kN] | R <sub>o,k</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>o,d</sub> [kN] | F <sub>o,tot,t,j</sub> [kN] | U.C. | S <sub>1,j</sub> [mm] | S <sub>1,j</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|-----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 2565                | 2333                | 4898                     | 3523                  | 2936                  | -104.6                  | 2832                  | -104.6                      | 0.04 | -0.1                  | -0.1                  |
| -10.50     | 2295                | 2661                | 4955                     | 3565                  | 2971                  | -104.6                  | 2866                  | -104.6                      | 0.04 | -0.1                  | -0.1                  |
| -11.00     | 2231                | 2962                | 5194                     | 3737                  | 3114                  | -104.6                  | 3009                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |
| -11.50     | 2001                | 3225                | 5226                     | 3760                  | 3133                  | -104.6                  | 3028                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |
| -12.00     | 1139                | 3487                | 4626                     | 3328                  | 2773                  | -104.6                  | 2669                  | -104.6                      | 0.04 | -0.1                  | -0.1                  |
| -12.50     | 1164                | 3561                | 4725                     | 3399                  | 2833                  | -104.6                  | 2728                  | -104.6                      | 0.04 | -0.1                  | -0.1                  |
| -13.00     | 1611                | 3645                | 5256                     | 3781                  | 3151                  | -104.6                  | 3046                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |
| -13.50     | 1907                | 3713                | 5620                     | 4043                  | 3369                  | -104.6                  | 3265                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |
| -14.00     | 2125                | 3864                | 5989                     | 4309                  | 3591                  | -104.6                  | 3486                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |
| -14.50     | 2202                | 3999                | 6202                     | 4462                  | 3718                  | -104.6                  | 3613                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |
| -15.00     | 2221                | 4161                | 6383                     | 4592                  | 3826                  | -104.6                  | 3722                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |
| -15.50     | 2261                | 4305                | 6565                     | 4723                  | 3936                  | -104.6                  | 3832                  | -104.6                      | 0.03 | -0.1                  | -0.1                  |



Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**Sondering : 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau<br>[m] | R <sub>0</sub><br>[kN] | R <sub>0</sub><br>[kN] | R <sub>o,jeal</sub><br>[kN] | R <sub>o,ek</sub><br>[kN] | R <sub>o,ed</sub><br>[kN] | F <sub>o,kid</sub><br>[kN] | R <sub>o,nd</sub><br>[kN] | F <sub>o,totj1</sub><br>[kN] | U.C. | S <sub>1j1</sub><br>[mm] | S <sub>1j2</sub><br>[mm] |
|---------------|------------------------|------------------------|-----------------------------|---------------------------|---------------------------|----------------------------|---------------------------|------------------------------|------|--------------------------|--------------------------|
| -16.00        | 2333                   | 4444                   | 6777                        | 4876                      | 4063                      | -104.6                     | 3958                      | -104.6                       | 0.03 | -0.1                     | -0.1                     |
| -16.50        | 2583                   | 4568                   | 7150                        | 5144                      | 4287                      | -104.6                     | 4182                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -17.00        | 2812                   | 4707                   | 7520                        | 5410                      | 4508                      | -104.6                     | 4404                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -17.50        | 2909                   | 4859                   | 7768                        | 5589                      | 4657                      | -104.6                     | 4553                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -18.00        | 2982                   | 5042                   | 8023                        | 5772                      | 4810                      | -104.6                     | 4706                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -18.50        | 3043                   | 5216                   | 8259                        | 5942                      | 4952                      | -104.6                     | 4847                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -19.00        | 3091                   | 5418                   | 8509                        | 6122                      | 5101                      | -104.6                     | 4997                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -19.50        | 3129                   | 5620                   | 8749                        | 6294                      | 5245                      | -104.6                     | 5141                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -20.00        | 3059                   | 5832                   | 8891                        | 6396                      | 5330                      | -104.6                     | 5226                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -20.50        | 3060                   | 6004                   | 9064                        | 6521                      | 5434                      | -104.6                     | 5330                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -21.00        | 3550                   | 6138                   | 9688                        | 6970                      | 5808                      | -104.6                     | 5704                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -21.50        | 4647                   | 6294                   | 10941                       | 7871                      | 6559                      | -104.6                     | 6455                      | -104.6                       | 0.02 | -0.1                     | -0.1                     |
| -22.00        | 5238                   | 6530                   | 11768                       | 8466                      | 7055                      | -104.6                     | 6951                      | -104.6                       | 0.01 | -0.1                     | -0.1                     |
| -22.50        | 6306                   | 6803                   | 13109                       | 9431                      | 7859                      | -104.6                     | 7755                      | -104.6                       | 0.01 | -0.1                     | -0.1                     |
| -23.00        | 6524                   | 7108                   | 13632                       | 9808                      | 8173                      | -104.6                     | 8068                      | -104.6                       | 0.01 | -0.1                     | -0.1                     |
| -23.50        | 7290                   | 7414                   | 14704                       | 10578                     | 8815                      | -104.6                     | 8711                      | -104.6                       | 0.01 | -0.1                     | -0.1                     |
| -24.00        | 7577                   | 7733                   | 15310                       | 11015                     | 9179                      | -104.6                     | 9074                      | -104.6                       | 0.01 | -0.1                     | -0.1                     |
| -24.50        | 7011                   | 8061                   | 15073                       | 10844                     | 9036                      | -104.6                     | 8932                      | -104.6                       | 0.01 | -0.1                     | -0.1                     |
| -25.00        | 6480                   | 8389                   | 14869                       | 10697                     | 8914                      | -104.6                     | 8810                      | -104.6                       | 0.01 | -0.1                     | -0.1                     |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SAMENVATTINGSTABEL MV Ø914/1074 druk) (n=1)**

**Uitgangspunten**

- paal : MV Ø914/1074  
 - paaltype : Geheide in de grond gevormde betonpaal;terugheind  
 - schachtafmeting : 994 mm  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                    |                         |
|------------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|--------------------|-------------------------|
|            |                    |                    | $R_{e,real}$<br>[kN] | $R_{b,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{c;d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 19-1008-14 | 0.40               | -10.00             | 3551.1               | 3946.3               | 7497.4               | 4494.8            | -20.0              | 4474.8                  |
|            |                    | -10.50             | 3179.8               | 4256.0               | 7435.7               | 4457.9            | -20.0              | 4437.8                  |
|            |                    | -11.00             | 2945.1               | 4583.8               | 7529.0               | 4513.8            | -20.0              | 4493.7                  |
|            |                    | -11.50             | 2806.1               | 4911.7               | 7717.8               | 4627.0            | -20.0              | 4607.0                  |
|            |                    | -12.00             | 2069.7               | 5239.6               | 7309.3               | 4382.1            | -20.0              | 4362.0                  |
|            |                    | -12.50             | 1831.7               | 5567.5               | 7399.2               | 4436.0            | -20.0              | 4416.0                  |
|            |                    | -13.00             | 1628.9               | 5893.9               | 7522.7               | 4510.0            | -20.0              | 4490.0                  |
|            |                    | -13.50             | 1500.8               | 6092.6               | 7593.4               | 4552.4            | -20.0              | 4532.4                  |
|            |                    | -14.00             | 1625.9               | 6188.1               | 7814.1               | 4684.7            | -20.0              | 4664.7                  |
|            |                    | -14.50             | 1741.4               | 6288.9               | 8030.4               | 4814.4            | -20.0              | 4794.3                  |
|            |                    | -15.00             | 1782.5               | 6445.0               | 8227.5               | 4932.5            | -20.0              | 4912.5                  |
|            |                    | -15.50             | 1783.3               | 6669.9               | 8453.2               | 5067.9            | -20.0              | 5047.8                  |
|            |                    | -16.00             | 2173.5               | 6760.3               | 8933.8               | 5356.0            | -20.0              | 5335.9                  |
|            |                    | -16.50             | 2254.9               | 6929.1               | 9184.0               | 5506.0            | -20.0              | 5486.0                  |
|            |                    | -17.00             | 2488.4               | 7071.5               | 9560.0               | 5731.4            | -20.0              | 5711.4                  |
|            |                    | -17.50             | 2558.0               | 7243.9               | 9801.9               | 5876.4            | -20.0              | 5856.4                  |
|            |                    | -18.00             | 2605.1               | 7422.7               | 10027.8              | 6011.9            | -20.0              | 5991.8                  |
|            |                    | -18.50             | 2711.3               | 7592.5               | 10303.8              | 6177.4            | -20.0              | 6157.3                  |
|            |                    | -19.00             | 3260.5               | 7757.7               | 11018.2              | 6605.6            | -20.0              | 6585.6                  |
|            |                    | -19.50             | 3486.2               | 7954.4               | 11440.5              | 6858.8            | -20.0              | 6838.8                  |
|            |                    | -20.00             | 3957.4               | 8149.2               | 12106.6              | 7258.2            | -20.0              | 7238.1                  |
|            |                    | -20.50             | 4123.3               | 8378.6               | 12501.9              | 7495.2            | -20.0              | 7475.1                  |
|            |                    | -21.00             | 4271.1               | 8621.1               | 12892.2              | 7729.2            | -20.0              | 7709.1                  |
|            |                    | -21.50             | 4621.3               | 8854.8               | 13476.1              | 8079.2            | -20.0              | 8059.2                  |
|            |                    | -22.00             | 4864.3               | 9099.4               | 13963.7              | 8371.5            | -20.0              | 8351.5                  |
| -22.50     | 4432.4             | 9352.2             | 13784.6              | 8264.2               | -20.0                | 8244.1            |                    |                         |
| -23.00     | 4546.9             | 9612.5             | 14159.5              | 8488.9               | -20.0                | 8468.8            |                    |                         |
| -23.50     | 4664.1             | 9871.4             | 14535.4              | 8714.3               | -20.0                | 8694.3            |                    |                         |
| -24.00     | 4748.4             | 10133.7            | 14882.0              | 8922.1               | -20.0                | 8902.0            |                    |                         |
| -24.50     | 4803.1             | 10395.8            | 15199.0              | 9112.1               | -20.0                | 9092.1            |                    |                         |
| -25.00     | 4830.5             | 10668.2            | 15498.7              | 9291.8               | -20.0                | 9271.8            |                    |                         |
| 19-1008-15 | 0.75               | -10.00             | 6399.2               | 4304.2               | 10703.3              | 6416.9            | -7.3               | 6409.6                  |
|            |                    | -10.50             | 6605.0               | 4632.0               | 11237.0              | 6736.8            | -7.3               | 6729.6                  |
|            |                    | -11.00             | 6608.9               | 4959.9               | 11568.8              | 6935.7            | -7.3               | 6928.5                  |
|            |                    | -11.50             | 6602.5               | 5287.8               | 11890.3              | 7128.5            | -7.3               | 7121.2                  |
|            |                    | -12.00             | 6714.5               | 5615.7               | 12330.2              | 7392.2            | -7.3               | 7385.0                  |
|            |                    | -12.50             | 3566.7               | 5943.6               | 9510.3               | 5701.6            | -7.3               | 5694.4                  |
|            |                    | -13.00             | 3190.3               | 6266.1               | 9456.4               | 5669.3            | -7.3               | 5662.0                  |
|            |                    | -13.50             | 2876.7               | 6552.1               | 9428.8               | 5652.7            | -7.3               | 5645.5                  |
|            |                    | -14.00             | 2538.0               | 6880.0               | 9418.0               | 5646.3            | -7.3               | 5639.1                  |
|            |                    | -14.50             | 1881.7               | 7207.9               | 9089.6               | 5449.4            | -7.3               | 5442.2                  |
|            |                    | -15.00             | 1434.6               | 7535.8               | 8970.4               | 5377.9            | -7.3               | 5370.7                  |
|            |                    | -15.50             | 1014.0               | 7863.7               | 8877.7               | 5322.4            | -7.3               | 5315.1                  |
|            |                    | -16.00             | 683.7                | 8188.8               | 8872.5               | 5319.3            | -7.3               | 5312.0                  |
|            |                    | -16.50             | 739.4                | 8267.9               | 9007.3               | 5400.1            | -7.3               | 5392.8                  |
|            |                    | -17.00             | 656.8                | 8303.5               | 8960.3               | 5371.9            | -7.3               | 5364.6                  |
|            |                    | -17.50             | 644.7                | 8357.7               | 9002.4               | 5397.1            | -7.3               | 5389.9                  |
|            |                    | -18.00             | 551.2                | 8449.7               | 9000.8               | 5396.2            | -7.3               | 5388.9                  |
|            |                    | -18.50             | 558.9                | 8473.8               | 9032.6               | 5415.3            | -7.3               | 5408.0                  |
|            |                    | -19.00             | 566.3                | 8499.4               | 9065.7               | 5435.1            | -7.3               | 5427.8                  |
|            |                    | -19.50             | 611.1                | 8530.0               | 9141.2               | 5480.3            | -7.3               | 5473.1                  |
|            |                    | -20.00             | 844.6                | 8561.7               | 9406.3               | 5639.3            | -7.3               | 5632.0                  |
|            |                    | -20.50             | 1640.2               | 8604.3               | 10244.5              | 6141.8            | -7.3               | 6134.5                  |
|            |                    | -21.00             | 1941.2               | 8704.3               | 10645.5              | 6382.2            | -7.3               | 6374.9                  |
|            |                    | -21.50             | 2008.7               | 8845.0               | 10853.8              | 6507.0            | -7.3               | 6499.8                  |
|            |                    | -22.00             | 2381.5               | 8985.9               | 11367.3              | 6814.9            | -7.3               | 6807.7                  |
| -22.50     | 2658.9             | 9132.6             | 11791.4              | 7069.2               | -7.3                 | 7062.0            |                    |                         |
| -23.00     | 2672.1             | 9313.1             | 11985.2              | 7185.4               | -7.3                 | 7178.1            |                    |                         |
| -23.50     | 2741.9             | 9528.2             | 12270.0              | 7356.1               | -7.3                 | 7348.9            |                    |                         |
| -24.00     | 2833.4             | 9720.4             | 12553.8              | 7526.3               | -7.3                 | 7519.0            |                    |                         |
| -24.50     | 2833.1             | 9965.1             | 12798.2              | 7672.8               | -7.3                 | 7665.5            |                    |                         |
| -25.00     | 2713.8             | 10212.5            | 12926.3              | 7749.6               | -7.3                 | 7742.3            |                    |                         |
| 251.S01    | -1.05              | -10.00             | 2065.1               | 2452.3               | 4517.4               | 2708.3            | -38.8              | 2669.4                  |
|            |                    | -10.50             | 1972.5               | 2710.7               | 4683.2               | 2807.7            | -38.8              | 2768.8                  |
|            |                    | -11.00             | 1865.3               | 2906.9               | 4772.2               | 2861.0            | -38.8              | 2822.2                  |
|            |                    | -11.50             | 2005.3               | 3026.2               | 5031.5               | 3016.5            | -38.8              | 2977.6                  |
|            |                    | -12.00             | 2141.4               | 3144.5               | 5286.0               | 3169.0            | -38.8              | 3130.2                  |
|            |                    | -12.50             | 2226.2               | 3345.9               | 5572.1               | 3340.6            | -38.8              | 3301.8                  |
|            |                    | -13.00             | 2256.7               | 3584.1               | 5840.7               | 3501.6            | -38.8              | 3462.8                  |
|            |                    | -13.50             | 2336.6               | 3808.3               | 6145.0               | 3684.0            | -38.8              | 3645.2                  |
|            |                    | -14.00             | 2195.5               | 4120.3               | 6315.7               | 3786.4            | -38.8              | 3747.5                  |
|            |                    | -14.50             | 1872.7               | 4430.2               | 6302.9               | 3778.7            | -38.8              | 3739.9                  |
|            |                    | -15.00             | 2064.2               | 4710.3               | 6774.5               | 4061.5            | -38.8              | 4022.6                  |
|            |                    | -15.50             | 3245.5               | 4815.4               | 8061.0               | 4832.7            | -38.8              | 4793.9                  |
|            |                    | -16.00             | 3375.5               | 5118.1               | 8493.6               | 5092.1            | -38.8              | 5053.3                  |
|            |                    | -16.50             | 3397.9               | 5446.0               | 8843.9               | 5302.1            | -38.8              | 5263.2                  |
|            |                    | -17.00             | 3426.1               | 5770.2               | 9196.4               | 5513.4            | -38.8              | 5474.6                  |
|            |                    | -17.50             | 1926.8               | 6079.7               | 8006.5               | 4800.0            | -38.8              | 4761.2                  |
|            |                    | -18.00             | 1679.1               | 6372.0               | 8051.0               | 4826.8            | -38.8              | 4787.9                  |
|            |                    | -18.50             | 1700.7               | 6646.6               | 8347.3               | 5004.4            | -38.8              | 4965.6                  |
|            |                    | -19.00             | 1405.6               | 6773.1               | 8178.7               | 4903.3            | -38.8              | 4864.5                  |
|            |                    | -19.50             | 1320.5               | 6954.5               | 8275.1               | 4961.1            | -38.8              | 4922.2                  |
|            |                    | -20.00             | 1229.2               | 7209.4               | 8438.6               | 5059.1            | -38.8              | 5020.3                  |
|            |                    | -20.50             | 978.9                | 7483.0               | 8461.9               | 5073.1            | -38.8              | 5034.2                  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld<br>niveau | paalpunt<br>niveau | Beziijkdraagvermogen |                      |                      | Rekenwaarden      |                     |                         |       |        |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|---------------------|-------------------------|-------|--------|
|           |                    |                    | $R_{b,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{o,real}$<br>[kN] | $R_{c,d}$<br>[kN] | $F_{b,k;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |       |        |
| 251.S01   | -1.05              | -21.00             | 767.3                | 7724.4               | 8491.7               | 5090.9            | -38.8               | 5052.1                  |       |        |
|           |                    | -21.50             | 695.6                | 7824.5               | 8520.1               | 5108.0            | -38.8               | 5069.1                  |       |        |
|           |                    | -22.00             | 700.4                | 7855.9               | 8556.3               | 5129.7            | -38.8               | 5090.8                  |       |        |
|           |                    | -22.50             | 932.4                | 7897.4               | 8829.7               | 5293.6            | -38.8               | 5254.7                  |       |        |
|           |                    | -23.00             | 1154.1               | 7963.8               | 9117.8               | 5466.3            | -38.8               | 5427.5                  |       |        |
|           |                    | -23.50             | 1342.0               | 8050.7               | 9392.7               | 5631.1            | -38.8               | 5592.2                  |       |        |
|           |                    | -24.00             | 1353.7               | 8168.3               | 9522.1               | 5708.7            | -38.8               | 5669.8                  |       |        |
|           |                    | -24.50             | 1711.4               | 8275.4               | 9986.8               | 5987.3            | -38.8               | 5948.5                  |       |        |
|           |                    | -25.00             | 2325.9               | 8372.7               | 10698.6              | 6414.1            | -38.8               | 6375.2                  |       |        |
|           |                    | 19-1008-22         | 0.18                 | -10.00               | 3410.0               | 2846.2            | 6256.2              | 3750.7                  | -40.6 | 3710.2 |
|           |                    |                    |                      | -10.50               | 3042.0               | 3119.6            | 6161.6              | 3694.0                  | -40.6 | 3653.4 |
| -11.00    | 2632.5             |                    |                      | 3392.0               | 6024.5               | 3611.8            | -40.6               | 3571.3                  |       |        |
| -11.50    | 2545.4             |                    |                      | 3663.9               | 6209.3               | 3722.6            | -40.6               | 3682.0                  |       |        |
| -12.00    | 2605.4             |                    |                      | 3831.0               | 6436.4               | 3858.7            | -40.6               | 3818.2                  |       |        |
| -12.50    | 2030.0             |                    |                      | 3980.1               | 6010.1               | 3603.2            | -40.6               | 3562.6                  |       |        |
| -13.00    | 1531.1             |                    |                      | 4140.2               | 5671.3               | 3400.1            | -40.6               | 3359.5                  |       |        |
| -13.50    | 1348.7             |                    |                      | 4329.1               | 5677.8               | 3404.0            | -40.6               | 3363.4                  |       |        |
| -14.00    | 1293.3             |                    |                      | 4491.9               | 5785.2               | 3468.4            | -40.6               | 3427.8                  |       |        |
| -14.50    | 1257.0             |                    |                      | 4634.0               | 5891.0               | 3531.7            | -40.6               | 3491.2                  |       |        |
| -15.00    | 1251.5             |                    |                      | 4734.4               | 5985.8               | 3588.6            | -40.6               | 3548.1                  |       |        |
| -15.50    | 1135.6             |                    |                      | 4897.3               | 6032.9               | 3616.8            | -40.6               | 3576.3                  |       |        |
| -16.00    | 1024.4             |                    |                      | 5028.8               | 6053.2               | 3629.0            | -40.6               | 3588.4                  |       |        |
| -16.50    | 974.9              |                    |                      | 5105.3               | 6080.2               | 3645.2            | -40.6               | 3604.6                  |       |        |
| -17.00    | 932.8              |                    |                      | 5165.2               | 6098.0               | 3655.8            | -40.6               | 3615.3                  |       |        |
| -17.50    | 1504.0             |                    |                      | 5204.5               | 6708.5               | 4021.9            | -40.6               | 3981.3                  |       |        |
| -18.00    | 2434.9             |                    |                      | 5271.2               | 7706.1               | 4619.9            | -40.6               | 4579.4                  |       |        |
| -18.50    | 2505.6             |                    |                      | 5464.3               | 7969.9               | 4778.1            | -40.6               | 4737.5                  |       |        |
| -19.00    | 2589.2             |                    |                      | 5650.5               | 8239.7               | 4939.9            | -40.6               | 4899.3                  |       |        |
| -19.50    | 2745.6             |                    |                      | 5812.0               | 8557.6               | 5130.5            | -40.6               | 5089.9                  |       |        |
| -20.00    | 2937.2             |                    |                      | 5993.3               | 8930.5               | 5354.0            | -40.6               | 5313.5                  |       |        |
| -20.50    | 2954.2             |                    |                      | 6241.3               | 9195.5               | 5512.9            | -40.6               | 5472.3                  |       |        |
| -21.00    | 3169.2             |                    |                      | 6412.1               | 9581.3               | 5744.2            | -40.6               | 5703.6                  |       |        |
| -21.50    | 3223.3             |                    |                      | 6643.8               | 9867.1               | 5915.5            | -40.6               | 5875.0                  |       |        |
| -22.00    | 3076.8             |                    |                      | 6902.2               | 9979.1               | 5982.6            | -40.6               | 5942.1                  |       |        |
| -22.50    | 3397.9             | 7081.3             | 10479.1              | 6282.4               | -40.6                | 6241.9            |                     |                         |       |        |
| -23.00    | 3734.3             | 7262.9             | 10997.2              | 6593.1               | -40.6                | 6552.5            |                     |                         |       |        |
| -23.50    | 3933.4             | 7473.7             | 11407.1              | 6838.8               | -40.6                | 6798.2            |                     |                         |       |        |
| -24.00    | 4381.0             | 7682.2             | 12063.2              | 7232.1               | -40.6                | 7191.6            |                     |                         |       |        |
| -24.50    | 4725.8             | 7912.5             | 12638.4              | 7577.0               | -40.6                | 7536.4            |                     |                         |       |        |
| -25.00    | 5244.0             | 8157.7             | 13401.8              | 8034.6               | -40.6                | 7994.1            |                     |                         |       |        |
| 202.S03   | 0.03               | -10.00             | 2564.7               | 2332.8               | 4897.5               | 2936.2            | -104.6              | 2831.6                  |       |        |
|           |                    | -10.50             | 2294.6               | 2660.7               | 4955.2               | 2970.8            | -104.6              | 2866.2                  |       |        |
|           |                    | -11.00             | 2231.3               | 2962.5               | 5193.8               | 3113.8            | -104.6              | 3009.2                  |       |        |
|           |                    | -11.50             | 2001.0               | 3224.8               | 5225.8               | 3133.0            | -104.6              | 3028.4                  |       |        |
|           |                    | -12.00             | 1139.1               | 3486.6               | 4625.7               | 2773.2            | -104.6              | 2668.6                  |       |        |
|           |                    | -12.50             | 1164.0               | 3560.7               | 4724.7               | 2832.6            | -104.6              | 2728.0                  |       |        |
|           |                    | -13.00             | 1611.2               | 3644.7               | 5255.9               | 3151.0            | -104.6              | 3046.4                  |       |        |
|           |                    | -13.50             | 1906.9               | 3712.8               | 5619.7               | 3369.1            | -104.6              | 3264.5                  |       |        |
|           |                    | -14.00             | 2125.2               | 3864.0               | 5989.2               | 3590.6            | -104.6              | 3486.0                  |       |        |
|           |                    | -14.50             | 2202.2               | 3999.3               | 6201.6               | 3718.0            | -104.6              | 3613.4                  |       |        |
|           |                    | -15.00             | 2221.1               | 4161.5               | 6382.6               | 3826.5            | -104.6              | 3721.9                  |       |        |
|           |                    | -15.50             | 2260.6               | 4304.9               | 6565.5               | 3936.1            | -104.6              | 3831.5                  |       |        |
|           |                    | -16.00             | 2333.4               | 4443.8               | 6777.1               | 4063.0            | -104.6              | 3958.4                  |       |        |
|           |                    | -16.50             | 2583.0               | 4567.5               | 7150.5               | 4286.9            | -104.6              | 4182.3                  |       |        |
|           |                    | -17.00             | 2812.4               | 4707.4               | 7519.7               | 4508.2            | -104.6              | 4403.6                  |       |        |
|           |                    | -17.50             | 2909.2               | 4859.0               | 7768.3               | 4657.2            | -104.6              | 4552.6                  |       |        |
|           |                    | -18.00             | 2981.8               | 5041.6               | 8023.4               | 4810.2            | -104.6              | 4705.6                  |       |        |
|           |                    | -18.50             | 3043.4               | 5215.8               | 8259.2               | 4951.6            | -104.6              | 4846.9                  |       |        |
|           |                    | -19.00             | 3091.0               | 5418.3               | 8509.3               | 5101.5            | -104.6              | 4996.9                  |       |        |
|           |                    | -19.50             | 3129.2               | 5619.9               | 8749.1               | 5245.3            | -104.6              | 5140.7                  |       |        |
|           |                    | -20.00             | 3059.3               | 5831.6               | 8990.9               | 5330.3            | -104.6              | 5225.7                  |       |        |
|           |                    | -20.50             | 3060.5               | 6003.9               | 9064.4               | 5434.3            | -104.6              | 5329.7                  |       |        |
|           |                    | -21.00             | 3550.3               | 6138.2               | 9688.5               | 5808.4            | -104.6              | 5703.8                  |       |        |
|           |                    | -21.50             | 4647.5               | 6293.7               | 10941.2              | 6559.5            | -104.6              | 6454.9                  |       |        |
|           |                    | -22.00             | 5238.0               | 6530.0               | 11768.0              | 7055.2            | -104.6              | 6950.6                  |       |        |
| -22.50    | 6306.0             | 6803.0             | 13109.0              | 7859.1               | -104.6               | 7754.5            |                     |                         |       |        |
| -23.00    | 6524.4             | 7108.1             | 13632.5              | 8173.0               | -104.6               | 8068.3            |                     |                         |       |        |
| -23.50    | 7290.3             | 7413.5             | 14703.8              | 8815.2               | -104.6               | 8710.6            |                     |                         |       |        |
| -24.00    | 7576.9             | 7733.3             | 15310.2              | 9178.8               | -104.6               | 9074.2            |                     |                         |       |        |
| -24.50    | 7011.5             | 8061.2             | 15072.7              | 9036.4               | -104.6               | 8931.8            |                     |                         |       |        |
| -25.00    | 6479.7             | 8389.1             | 14868.8              | 8914.1               | -104.6               | 8809.5            |                     |                         |       |        |

**REKENGEDEGENS MV Ø1016/1176 druk**

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 19-1008-14, 19-1008-15, 251.S01, 19-1008-22, 202.S03

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 5  
 Factor  $\xi_{s(n-1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(qem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{t,nk}$  : 1.0  
 $R_{b,real,max;i}$  begrenzen op  $0.75 * R_{b,real,max;i}$  : NEE  
 UGT draagvermogen zonder negatieve kleef : NEE

Paal : MV Ø1016/1176  
 Niveau paalkop [m] : N.A.P. 0.00  
 $E_{d,1}$  [kN] : 0.00  $E_{d,2}$  [kN] : 0.00  
 $S_{req,1}$  [m] : 0.15  $S_{req,2}$  [m] : 0.05  
 Bovenbel. [kN/m²] : 0.00

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**PAALPUNTNIVEAUS MV Ø1016/1176**

Alle niveaus/hoogtes/peilmaten zijn t.o.v. : N.A.P.

| Nr | Beginniveau [m] | Eindniveau [m] | Stapgrootte [m] |
|----|-----------------|----------------|-----------------|
| 1  | -10.00          | -25.00         | 0.50            |

**RESULTATEN MV Ø1016/1176 druk (n=1)**

**Sondering : 19-1008-14**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>b</sub> [kN] | R <sub>e</sub> [kN] | R <sub>c,real</sub> [kN] | R <sub>c,k</sub> [kN] | R <sub>c,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>nd</sub> [kN] | F <sub>c,tot,t;1</sub> [kN] | U.C. | S <sub>1;1</sub> [mm] | S <sub>1;2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 3968                | 4351                | 8319                     | 5985                  | 4988                  | -22.1                   | 4965                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -10.50     | 3776                | 4693                | 8469                     | 6092                  | 5077                  | -22.1                   | 5055                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -11.00     | 3632                | 5054                | 8686                     | 6249                  | 5207                  | -22.1                   | 5185                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -11.50     | 2807                | 5416                | 8222                     | 5915                  | 4929                  | -22.1                   | 4907                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -12.00     | 2540                | 5777                | 8317                     | 5983                  | 4986                  | -22.1                   | 4964                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -12.50     | 2227                | 6139                | 8366                     | 6019                  | 5015                  | -22.1                   | 4993                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -13.00     | 1980                | 6499                | 8479                     | 6100                  | 5083                  | -22.1                   | 5061                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -13.50     | 1880                | 6718                | 8597                     | 6185                  | 5154                  | -22.1                   | 5132                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -14.00     | 1977                | 6823                | 8800                     | 6331                  | 5276                  | -22.1                   | 5254                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -14.50     | 2117                | 6934                | 9051                     | 6512                  | 5427                  | -22.1                   | 5404                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -15.00     | 2167                | 7106                | 9273                     | 6672                  | 5560                  | -22.1                   | 5537                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -15.50     | 2261                | 7354                | 9615                     | 6917                  | 5764                  | -22.1                   | 5742                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -16.00     | 2640                | 7454                | 10094                    | 7262                  | 6052                  | -22.1                   | 6030                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -16.50     | 2786                | 7640                | 10426                    | 7500                  | 6250                  | -22.1                   | 6228                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -17.00     | 3010                | 7797                | 10807                    | 7775                  | 6479                  | -22.1                   | 6457                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -17.50     | 3086                | 7987                | 11073                    | 7966                  | 6639                  | -22.1                   | 6617                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -18.00     | 3135                | 8184                | 11319                    | 8143                  | 6786                  | -22.1                   | 6764                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -18.50     | 3348                | 8372                | 11719                    | 8431                  | 7026                  | -22.1                   | 7004                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -19.00     | 3915                | 8554                | 12469                    | 8971                  | 7475                  | -22.1                   | 7453                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -19.50     | 4224                | 8771                | 12995                    | 9349                  | 7791                  | -22.1                   | 7769                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -20.00     | 4736                | 8985                | 13722                    | 9872                  | 8227                  | -22.1                   | 8204                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -20.50     | 4922                | 9238                | 14161                    | 10188                 | 8490                  | -22.1                   | 8468                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -21.00     | 5105                | 9506                | 14611                    | 10511                 | 8759                  | -22.1                   | 8737                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -21.50     | 5498                | 9763                | 15261                    | 10979                 | 9149                  | -22.1                   | 9127                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -22.00     | 5121                | 10033               | 15154                    | 10902                 | 9085                  | -22.1                   | 9063                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -22.50     | 5253                | 10312               | 15565                    | 11198                 | 9332                  | -22.1                   | 9309                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -23.00     | 5380                | 10599               | 15979                    | 11495                 | 9580                  | -22.1                   | 9557                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -23.50     | 5510                | 10884               | 16394                    | 11794                 | 9828                  | -22.1                   | 9806                 | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -24.00     | 5629                | 11174               | 16803                    | 12088                 | 10074                 | -22.1                   | 10052                | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -24.50     | 5753                | 11463               | 17216                    | 12385                 | 10321                 | -22.1                   | 10299                | -22.1                       | 0.00 | -0.0                  | -0.0                  |
| -25.00     | 5798                | 11763               | 17561                    | 12634                 | 10528                 | -22.1                   | 10506                | -22.1                       | 0.00 | -0.0                  | -0.0                  |

**Sondering : 19-1008-15**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>b</sub> [kN] | R <sub>e</sub> [kN] | R <sub>c,real</sub> [kN] | R <sub>c,k</sub> [kN] | R <sub>c,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>nd</sub> [kN] | F <sub>c,tot,t;1</sub> [kN] | U.C. | S <sub>1;1</sub> [mm] | S <sub>1;2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 7652                | 4746                | 12397                    | 8919                  | 7432                  | -8.0                    | 7424                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -10.50     | 7883                | 5107                | 12991                    | 9346                  | 7788                  | -8.0                    | 7780                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -11.00     | 7870                | 5469                | 13339                    | 9596                  | 7997                  | -8.0                    | 7989                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -11.50     | 7843                | 5830                | 13674                    | 9837                  | 8198                  | -8.0                    | 8190                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -12.00     | 4515                | 6192                | 10707                    | 7703                  | 6419                  | -8.0                    | 6411                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -12.50     | 3894                | 6554                | 10447                    | 7516                  | 6263                  | -8.0                    | 6255                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -13.00     | 3493                | 6909                | 10402                    | 7483                  | 6236                  | -8.0                    | 6228                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -13.50     | 3340                | 7224                | 10565                    | 7601                  | 6334                  | -8.0                    | 6326                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -14.00     | 2655                | 7586                | 10241                    | 7368                  | 6140                  | -8.0                    | 6132                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -14.50     | 2139                | 7948                | 10087                    | 7257                  | 6047                  | -8.0                    | 6039                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -15.00     | 1652                | 8309                | 9961                     | 7166                  | 5972                  | -8.0                    | 5964                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -15.50     | 1180                | 8671                | 9850                     | 7086                  | 5905                  | -8.0                    | 5897                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -16.00     | 826.7               | 9029                | 9856                     | 7091                  | 5909                  | -8.0                    | 5901                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -16.50     | 899.0               | 9116                | 10015                    | 7205                  | 6004                  | -8.0                    | 5996                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -17.00     | 798.5               | 9156                | 9954                     | 7161                  | 5968                  | -8.0                    | 5960                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -17.50     | 783.8               | 9215                | 9999                     | 7194                  | 5995                  | -8.0                    | 5987                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -18.00     | 671.9               | 9317                | 9989                     | 7186                  | 5988                  | -8.0                    | 5980                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -18.50     | 679.4               | 9343                | 10023                    | 7211                  | 6009                  | -8.0                    | 6001                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -19.00     | 693.8               | 9372                | 10065                    | 7241                  | 6034                  | -8.0                    | 6026                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -19.50     | 749.7               | 9405                | 10155                    | 7306                  | 6088                  | -8.0                    | 6080                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -20.00     | 1088                | 9440                | 10528                    | 7574                  | 6312                  | -8.0                    | 6304                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -20.50     | 2029                | 9487                | 11516                    | 8285                  | 6904                  | -8.0                    | 6896                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -21.00     | 2352                | 9597                | 11949                    | 8597                  | 7164                  | -8.0                    | 7156                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -21.50     | 2431                | 9753                | 12183                    | 8765                  | 7304                  | -8.0                    | 7296                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -22.00     | 2901                | 9908                | 12809                    | 9215                  | 7679                  | -8.0                    | 7671                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -22.50     | 3198                | 10070               | 13268                    | 9545                  | 7954                  | -8.0                    | 7946                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -23.00     | 3205                | 10269               | 13474                    | 9693                  | 8078                  | -8.0                    | 8070                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -23.50     | 3281                | 10506               | 13787                    | 9919                  | 8266                  | -8.0                    | 8258                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -24.00     | 3384                | 10718               | 14102                    | 10145                 | 8454                  | -8.0                    | 8446                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -24.50     | 3374                | 10988               | 14362                    | 10332                 | 8610                  | -8.0                    | 8602                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |
| -25.00     | 3221                | 11260               | 14481                    | 10418                 | 8682                  | -8.0                    | 8674                 | -8.0                        | 0.00 | -0.0                  | -0.0                  |

**Sondering : 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau [m] | R <sub>b</sub> [kN] | R <sub>e</sub> [kN] | R <sub>c,real</sub> [kN] | R <sub>c,k</sub> [kN] | R <sub>c,d</sub> [kN] | F <sub>n,k,d</sub> [kN] | R <sub>nd</sub> [kN] | F <sub>c,tot,t;1</sub> [kN] | U.C. | S <sub>1;1</sub> [mm] | S <sub>1;2</sub> [mm] |
|------------|---------------------|---------------------|--------------------------|-----------------------|-----------------------|-------------------------|----------------------|-----------------------------|------|-----------------------|-----------------------|
| -10.00     | 2482                | 2704                | 5186                     | 3731                  | 3109                  | -42.8                   | 3066                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -10.50     | 2361                | 2989                | 5350                     | 3849                  | 3207                  | -42.8                   | 3164                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.00     | 2231                | 3205                | 5436                     | 3911                  | 3259                  | -42.8                   | 3216                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -11.50     | 2422                | 3337                | 5759                     | 4143                  | 3453                  | -42.8                   | 3410                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.00     | 2589                | 3467                | 6056                     | 4357                  | 3631                  | -42.8                   | 3588                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -12.50     | 2689                | 3689                | 6379                     | 4589                  | 3824                  | -42.8                   | 3781                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.00     | 2724                | 3952                | 6676                     | 4803                  | 4002                  | -42.8                   | 3960                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -13.50     | 2819                | 4199                | 7018                     | 5049                  | 4207                  | -42.8                   | 4165                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.00     | 2645                | 4543                | 7188                     | 5171                  | 4309                  | -42.8                   | 4267                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -14.50     | 2250                | 4885                | 7135                     | 5133                  | 4278                  | -42.8                   | 4235                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.00     | 2738                | 5194                | 7931                     | 5706                  | 4755                  | -42.8                   | 4712                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -15.50     | 3947                | 5310                | 9256                     | 6659                  | 5549                  | -42.8                   | 5507                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |
| -16.00     | 4061                | 5643                | 9704                     | 6981                  | 5818                  | -42.8                   | 5775                 | -42.8                       | 0.01 | -0.0                  | -0.0                  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**Sondering : 251.S01**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | R <sub>0</sub> | R <sub>s</sub> | R <sub>o,real</sub> | R <sub>o,k</sub> | R <sub>o,d</sub> | F <sub>o,k,d</sub> | R <sub>o,nd</sub> | F <sub>o,tot,t,1</sub> | U.C. | S <sub>1,1</sub> | S <sub>1,2</sub> |
|--------|----------------|----------------|---------------------|------------------|------------------|--------------------|-------------------|------------------------|------|------------------|------------------|
| [m]    | [kN]           | [kN]           | [kN]                | [kN]             | [kN]             | [kN]               | [kN]              | [kN]                   |      | [mm]             | [mm]             |
| -16.50 | 4078           | 6005           | 10083               | 7254             | 6045             | -42.8              | 6002              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -17.00 | 2760           | 6362           | 9122                | 6562             | 5469             | -42.8              | 5426              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -17.50 | 2207           | 6704           | 8910                | 6410             | 5342             | -42.8              | 5299              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -18.00 | 1944           | 7026           | 8969                | 6453             | 5377             | -42.8              | 5335              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -18.50 | 2068           | 7329           | 9396                | 6760             | 5633             | -42.8              | 5590              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -19.00 | 1647           | 7468           | 9115                | 6558             | 5465             | -42.8              | 5422              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -19.50 | 1624           | 7668           | 9292                | 6685             | 5571             | -42.8              | 5528              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -20.00 | 1499           | 7949           | 9448                | 6797             | 5665             | -42.8              | 5622              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -20.50 | 1190           | 8251           | 9441                | 6792             | 5660             | -42.8              | 5617              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -21.00 | 932.8          | 8517           | 9450                | 6798             | 5665             | -42.8              | 5623              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -21.50 | 845.6          | 8627           | 9473                | 6815             | 5679             | -42.8              | 5636              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -22.00 | 849.7          | 8662           | 9512                | 6843             | 5702             | -42.8              | 5660              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -22.50 | 1132           | 8708           | 9840                | 7079             | 5899             | -42.8              | 5856              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -23.00 | 1500           | 8781           | 10281               | 7396             | 6164             | -42.8              | 6121              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -23.50 | 1628           | 8877           | 10505               | 7557             | 6298             | -42.8              | 6255              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -24.00 | 1628           | 9007           | 10635               | 7651             | 6376             | -42.8              | 6333              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -24.50 | 2068           | 9125           | 11193               | 8052             | 6710             | -42.8              | 6667              | -42.8                  | 0.01 | -0.0             | -0.0             |
| -25.00 | 2965           | 9232           | 12196               | 8774             | 7312             | -42.8              | 7269              | -42.8                  | 0.01 | -0.0             | -0.0             |

**Sondering : 19-1008-22**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | R <sub>0</sub> | R <sub>s</sub> | R <sub>o,real</sub> | R <sub>o,k</sub> | R <sub>o,d</sub> | F <sub>o,k,d</sub> | R <sub>o,nd</sub> | F <sub>o,tot,t,1</sub> | U.C. | S <sub>1,1</sub> | S <sub>1,2</sub> |
|--------|----------------|----------------|---------------------|------------------|------------------|--------------------|-------------------|------------------------|------|------------------|------------------|
| [m]    | [kN]           | [kN]           | [kN]                | [kN]             | [kN]             | [kN]               | [kN]              | [kN]                   |      | [mm]             | [mm]             |
| -10.00 | 3798           | 3138           | 6936                | 4990             | 4159             | -44.7              | 4114              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -10.50 | 3163           | 3440           | 6603                | 4750             | 3959             | -44.7              | 3914              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -11.00 | 3140           | 3740           | 6880                | 4949             | 4124             | -44.7              | 4080              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -11.50 | 3022           | 4040           | 7062                | 5081             | 4234             | -44.7              | 4189              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -12.00 | 2383           | 4224           | 6607                | 4753             | 3961             | -44.7              | 3916              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -12.50 | 1939           | 4389           | 6328                | 4553             | 3794             | -44.7              | 3749              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -13.00 | 1708           | 4565           | 6273                | 4513             | 3761             | -44.7              | 3716              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -13.50 | 1619           | 4773           | 6393                | 4599             | 3832             | -44.7              | 3788              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -14.00 | 1573           | 4953           | 6526                | 4695             | 3912             | -44.7              | 3867              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -14.50 | 1528           | 5109           | 6638                | 4775             | 3979             | -44.7              | 3935              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -15.00 | 1521           | 5220           | 6742                | 4850             | 4042             | -44.7              | 3997              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -15.50 | 1381           | 5400           | 6780                | 4878             | 4065             | -44.7              | 4020              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -16.00 | 1245           | 5545           | 6790                | 4885             | 4071             | -44.7              | 4026              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -16.50 | 1185           | 5629           | 6814                | 4902             | 4085             | -44.7              | 4041              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -17.00 | 1172           | 5695           | 6868                | 4941             | 4117             | -44.7              | 4072              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -17.50 | 1992           | 5739           | 7730                | 5561             | 4635             | -44.7              | 4590              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -18.00 | 2958           | 5812           | 8770                | 6309             | 5258             | -44.7              | 5213              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -18.50 | 3036           | 6025           | 9061                | 6519             | 5432             | -44.7              | 5388              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -19.00 | 3130           | 6230           | 9360                | 6734             | 5612             | -44.7              | 5567              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -19.50 | 3313           | 6408           | 9721                | 6994             | 5828             | -44.7              | 5783              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -20.00 | 3538           | 6608           | 10146               | 7299             | 6083             | -44.7              | 6038              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -20.50 | 3585           | 6882           | 10467               | 7530             | 6275             | -44.7              | 6230              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -21.00 | 3804           | 7070           | 10874               | 7823             | 6519             | -44.7              | 6475              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -21.50 | 3861           | 7326           | 11186               | 8048             | 6706             | -44.7              | 6662              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -22.00 | 3673           | 7610           | 11284               | 8118             | 6765             | -44.7              | 6720              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -22.50 | 4075           | 7808           | 11883               | 8549             | 7124             | -44.7              | 7080              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -23.00 | 4451           | 8008           | 12459               | 8964             | 7470             | -44.7              | 7425              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -23.50 | 4705           | 8241           | 12946               | 9313             | 7761             | -44.7              | 7716              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -24.00 | 5228           | 8470           | 13698               | 9855             | 8213             | -44.7              | 8168              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -24.50 | 5718           | 8724           | 14443               | 10390            | 8659             | -44.7              | 8614              | -44.7                  | 0.01 | -0.0             | -0.0             |
| -25.00 | 5648           | 8995           | 14643               | 10535            | 8779             | -44.7              | 8734              | -44.7                  | 0.01 | -0.0             | -0.0             |

**Sondering : 202.S03**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| Niveau | R <sub>0</sub> | R <sub>s</sub> | R <sub>o,real</sub> | R <sub>o,k</sub> | R <sub>o,d</sub> | F <sub>o,k,d</sub> | R <sub>o,nd</sub> | F <sub>o,tot,t,1</sub> | U.C. | S <sub>1,1</sub> | S <sub>1,2</sub> |
|--------|----------------|----------------|---------------------|------------------|------------------|--------------------|-------------------|------------------------|------|------------------|------------------|
| [m]    | [kN]           | [kN]           | [kN]                | [kN]             | [kN]             | [kN]               | [kN]              | [kN]                   |      | [mm]             | [mm]             |
| -10.00 | 2968           | 2572           | 5540                | 3985             | 3321             | -115.3             | 3206              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -10.50 | 2763           | 2934           | 5696                | 4098             | 3415             | -115.3             | 3300              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -11.00 | 2647           | 3266           | 5913                | 4254             | 3545             | -115.3             | 3430              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -11.50 | 2416           | 3556           | 5972                | 4296             | 3580             | -115.3             | 3465              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -12.00 | 1358           | 3844           | 5202                | 3743             | 3119             | -115.3             | 3004              | -115.3                 | 0.04 | -0.1             | -0.1             |
| -12.50 | 1402           | 3926           | 5328                | 3833             | 3194             | -115.3             | 3079              | -115.3                 | 0.04 | -0.1             | -0.1             |
| -13.00 | 1961           | 4019           | 5980                | 4302             | 3585             | -115.3             | 3469              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -13.50 | 2318           | 4094           | 6412                | 4613             | 3844             | -115.3             | 3729              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -14.00 | 2566           | 4260           | 6827                | 4911             | 4093             | -115.3             | 3978              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -14.50 | 2662           | 4410           | 7071                | 5087             | 4239             | -115.3             | 4124              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -15.00 | 2679           | 4589           | 7268                | 5229             | 4357             | -115.3             | 4242              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -15.50 | 2720           | 4747           | 7467                | 5372             | 4476             | -115.3             | 4361              | -115.3                 | 0.03 | -0.1             | -0.1             |
| -16.00 | 2825           | 4900           | 7725                | 5557             | 4631             | -115.3             | 4516              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -16.50 | 3113           | 5036           | 8149                | 5862             | 4885             | -115.3             | 4770              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -17.00 | 3369           | 5190           | 8559                | 6158             | 5131             | -115.3             | 5016              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -17.50 | 3479           | 5358           | 8836                | 6357             | 5298             | -115.3             | 5182              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -18.00 | 3538           | 5559           | 9097                | 6545             | 5454             | -115.3             | 5339              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -18.50 | 3626           | 5751           | 9377                | 6746             | 5622             | -115.3             | 5506              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -19.00 | 3676           | 5974           | 9650                | 6943             | 5786             | -115.3             | 5670              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -19.50 | 3715           | 6197           | 9911                | 7130             | 5942             | -115.3             | 5827              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -20.00 | 3622           | 6430           | 10052               | 7232             | 6026             | -115.3             | 5911              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -20.50 | 3651           | 6620           | 10271               | 7389             | 6158             | -115.3             | 6042              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -21.00 | 4317           | 6768           | 11085               | 7975             | 6646             | -115.3             | 6530              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -21.50 | 5604           | 6940           | 12544               | 9024             | 7520             | -115.3             | 7405              | -115.3                 | 0.02 | -0.1             | -0.1             |
| -22.00 | 6450           | 7200           | 13650               | 9820             | 8183             | -115.3             | 8068              | -115.3                 | 0.01 | -0.1             | -0.1             |
| -22.50 | 7612           | 7501           | 15113               | 10873            | 9061             | -115.3             | 8945              | -115.3                 | 0.01 | -0.1             | -0.1             |
| -23.00 | 8189           | 7837           | 16026               | 11530            | 9608             | -115.3             | 9493              | -115.3                 | 0.01 | -0.1             | -0.1             |
| -23.50 | 8832           | 8174           | 17006               | 12235            | 10196            | -115.3             | 10080             | -115.3                 | 0.01 | -0.1             | -0.1             |
| -24.00 | 8714           | 8527           | 17241               | 12404            | 10336            | -115.3             | 10221             | -115.3                 | 0.01 | -0.1             | -0.1             |
| -24.50 | 8026           | 8888           | 16914               | 12169            | 10141            | -115.3             | 10025             | -115.3                 | 0.01 | -0.1             | -0.1             |
| -25.00 | 7858           | 9250           | 17108               | 12308            | 10257            | -115.3             | 10141             | -115.3                 | 0.01 | -0.1             | -0.1             |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**SAMENVATTINGSTABEL MV Ø1016/1176 druk (n=1)**

**Uitgangspunten**

- paal : MV Ø1016/1176  
 - paaltype : Geheide in de grond gevormde betonpaal;terugheind  
 - schachtafmeting : 1096 mm  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld niveau | paalpunt niveau | Beziijkdraagvermogen |                   |                   | Rekenwaarden   |                 |                      |
|------------|-----------------|-----------------|----------------------|-------------------|-------------------|----------------|-----------------|----------------------|
|            |                 |                 | $R_{e,paal}$ [kN]    | $R_{b,paal}$ [kN] | $R_{c,paal}$ [kN] | $R_{c,d}$ [kN] | $F_{nk,d}$ [kN] | $R_{c,netto,d}$ [kN] |
| 19-1008-14 | 0.40            | -10.00          | 3968.0               | 4351.2            | 8319.2            | 4987.6         | -22.1           | 4965.5               |
|            |                 | -10.50          | 3775.9               | 4692.7            | 8468.5            | 5077.1         | -22.1           | 5055.0               |
|            |                 | -11.00          | 3631.7               | 5054.2            | 8685.9            | 5207.4         | -22.1           | 5185.3               |
|            |                 | -11.50          | 2806.5               | 5415.7            | 8222.3            | 4929.4         | -22.1           | 4907.3               |
|            |                 | -12.00          | 2539.7               | 5777.3            | 8317.0            | 4986.2         | -22.1           | 4964.1               |
|            |                 | -12.50          | 2227.0               | 6138.8            | 8365.8            | 5015.5         | -22.1           | 4993.4               |
|            |                 | -13.00          | 1980.3               | 6498.7            | 8479.0            | 5083.3         | -22.1           | 5061.2               |
|            |                 | -13.50          | 1879.6               | 6717.8            | 8597.3            | 5154.3         | -22.1           | 5132.2               |
|            |                 | -14.00          | 1976.8               | 6823.1            | 8799.9            | 5275.7         | -22.1           | 5253.6               |
|            |                 | -14.50          | 2117.2               | 6934.3            | 9051.4            | 5426.5         | -22.1           | 5404.4               |
|            |                 | -15.00          | 2167.1               | 7106.3            | 9273.4            | 5559.6         | -22.1           | 5537.5               |
|            |                 | -15.50          | 2260.6               | 7354.4            | 9614.9            | 5764.3         | -22.1           | 5742.2               |
|            |                 | -16.00          | 2640.3               | 7454.0            | 10094.3           | 6051.7         | -22.1           | 6029.6               |
|            |                 | -16.50          | 2785.6               | 7640.1            | 10425.7           | 6250.4         | -22.1           | 6228.3               |
|            |                 | -17.00          | 3009.9               | 7797.2            | 10807.1           | 6479.1         | -22.1           | 6457.0               |
|            |                 | -17.50          | 3086.1               | 7987.3            | 11073.4           | 6638.7         | -22.1           | 6616.6               |
|            |                 | -18.00          | 3135.1               | 8184.4            | 11319.5           | 6786.2         | -22.1           | 6764.2               |
|            |                 | -18.50          | 3347.7               | 8371.7            | 11719.4           | 7026.0         | -22.1           | 7003.9               |
|            |                 | -19.00          | 3915.3               | 8553.7            | 12469.0           | 7475.4         | -22.1           | 7453.3               |
|            |                 | -19.50          | 4224.4               | 8770.6            | 12995.0           | 7790.8         | -22.1           | 7768.7               |
|            |                 | -20.00          | 4736.5               | 8985.4            | 13721.9           | 8226.6         | -22.1           | 8204.5               |
|            |                 | -20.50          | 4922.4               | 9238.4            | 14160.8           | 8489.7         | -22.1           | 8467.6               |
|            |                 | -21.00          | 5104.9               | 9505.8            | 14610.6           | 8759.4         | -22.1           | 8737.3               |
|            |                 | -21.50          | 5497.7               | 9763.5            | 15261.2           | 9149.4         | -22.1           | 9127.3               |
|            |                 | -22.00          | 5120.8               | 10033.2           | 15153.9           | 9085.1         | -22.1           | 9063.0               |
| -22.50     | 5253.0          | 10311.9         | 15564.9              | 9331.5            | -22.1             | 9309.4         |                 |                      |
| -23.00     | 5379.7          | 10598.9         | 15978.6              | 9579.5            | -22.1             | 9557.4         |                 |                      |
| -23.50     | 5509.6          | 10884.3         | 16393.9              | 9828.5            | -22.1             | 9806.4         |                 |                      |
| -24.00     | 5629.3          | 11173.5         | 16802.9              | 10073.7           | -22.1             | 10051.6        |                 |                      |
| -24.50     | 5752.9          | 11462.6         | 17215.6              | 10321.1           | -22.1             | 10299.0        |                 |                      |
| -25.00     | 5798.2          | 11763.0         | 17561.1              | 10528.3           | -22.1             | 10506.2        |                 |                      |
| 19-1008-15 | 0.75            | -10.00          | 7651.5               | 4745.8            | 12397.4           | 7432.5         | -8.0            | 7424.5               |
|            |                 | -10.50          | 7883.3               | 5107.4            | 12990.7           | 7788.2         | -8.0            | 7780.2               |
|            |                 | -11.00          | 7869.7               | 5468.9            | 13338.6           | 7996.7         | -8.0            | 7988.8               |
|            |                 | -11.50          | 7843.4               | 5830.4            | 13673.9           | 8197.8         | -8.0            | 8189.8               |
|            |                 | -12.00          | 4515.3               | 6192.0            | 10707.3           | 6419.2         | -8.0            | 6411.2               |
|            |                 | -12.50          | 3893.7               | 6553.5            | 10447.2           | 6263.3         | -8.0            | 6255.3               |
|            |                 | -13.00          | 3492.6               | 6909.1            | 10401.6           | 6236.0         | -8.0            | 6228.0               |
|            |                 | -13.50          | 3340.4               | 7224.5            | 10564.9           | 6333.9         | -8.0            | 6325.9               |
|            |                 | -14.00          | 2655.1               | 7586.0            | 10241.1           | 6139.7         | -8.0            | 6131.7               |
|            |                 | -14.50          | 2139.4               | 7947.5            | 10086.9           | 6047.3         | -8.0            | 6039.3               |
|            |                 | -15.00          | 1651.8               | 8309.1            | 9960.9            | 5971.8         | -8.0            | 5963.8               |
|            |                 | -15.50          | 1179.6               | 8670.6            | 9850.2            | 5905.4         | -8.0            | 5897.4               |
|            |                 | -16.00          | 826.7                | 9029.1            | 9855.8            | 5908.8         | -8.0            | 5900.8               |
|            |                 | -16.50          | 899.0                | 9116.3            | 10015.3           | 6004.4         | -8.0            | 5996.4               |
|            |                 | -17.00          | 798.5                | 9155.6            | 9954.1            | 5967.7         | -8.0            | 5959.7               |
|            |                 | -17.50          | 783.8                | 9215.3            | 9999.2            | 5994.7         | -8.0            | 5986.7               |
|            |                 | -18.00          | 671.9                | 9316.7            | 9988.6            | 5988.4         | -8.0            | 5980.4               |
|            |                 | -18.50          | 679.4                | 9343.3            | 10022.7           | 6008.8         | -8.0            | 6000.8               |
|            |                 | -19.00          | 693.8                | 9371.6            | 10065.4           | 6034.4         | -8.0            | 6026.4               |
|            |                 | -19.50          | 749.7                | 9405.4            | 10155.1           | 6088.2         | -8.0            | 6080.2               |
|            |                 | -20.00          | 1088.1               | 9440.3            | 10528.4           | 6312.0         | -8.0            | 6304.0               |
|            |                 | -20.50          | 2028.9               | 9487.2            | 11516.1           | 6904.1         | -8.0            | 6896.1               |
|            |                 | -21.00          | 2351.8               | 9597.5            | 11949.3           | 7163.8         | -8.0            | 7155.8               |
|            |                 | -21.50          | 2430.8               | 9752.7            | 12183.5           | 7304.2         | -8.0            | 7296.3               |
|            |                 | -22.00          | 2901.2               | 9908.0            | 12809.2           | 7679.4         | -8.0            | 7671.4               |
| -22.50     | 3197.9          | 10069.7         | 13267.7              | 7954.2            | -8.0              | 7946.2         |                 |                      |
| -23.00     | 3205.2          | 10268.8         | 13474.0              | 8077.9            | -8.0              | 8069.9         |                 |                      |
| -23.50     | 3281.2          | 10505.9         | 13787.1              | 8265.7            | -8.0              | 8257.7         |                 |                      |
| -24.00     | 3383.7          | 10717.9         | 14101.6              | 8454.2            | -8.0              | 8446.2         |                 |                      |
| -24.50     | 3374.5          | 10987.6         | 14362.1              | 8610.4            | -8.0              | 8602.4         |                 |                      |
| -25.00     | 3220.6          | 11260.4         | 14481.0              | 8681.7            | -8.0              | 8673.7         |                 |                      |
| 251.S01    | -1.05           | -10.00          | 2482.4               | 2703.9            | 5186.4            | 3109.3         | -42.8           | 3066.5               |
|            |                 | -10.50          | 2360.7               | 2988.8            | 5349.5            | 3207.1         | -42.8           | 3164.3               |
|            |                 | -11.00          | 2231.3               | 3205.2            | 5436.5            | 3259.3         | -42.8           | 3216.4               |
|            |                 | -11.50          | 2422.3               | 3336.7            | 5759.0            | 3452.7         | -42.8           | 3409.8               |
|            |                 | -12.00          | 2588.7               | 3467.2            | 6055.9            | 3630.7         | -42.8           | 3587.8               |
|            |                 | -12.50          | 2689.4               | 3689.3            | 6378.7            | 3824.2         | -42.8           | 3781.3               |
|            |                 | -13.00          | 2724.1               | 3951.8            | 6675.9            | 4002.4         | -42.8           | 3959.5               |
|            |                 | -13.50          | 2818.9               | 4199.1            | 7018.1            | 4207.5         | -42.8           | 4164.6               |
|            |                 | -14.00          | 2644.9               | 4543.1            | 7188.0            | 4309.4         | -42.8           | 4266.5               |
|            |                 | -14.50          | 2250.2               | 4884.8            | 7135.0            | 4277.6         | -42.8           | 4234.7               |
|            |                 | -15.00          | 2737.8               | 5193.7            | 7931.4            | 4755.0         | -42.8           | 4712.2               |
|            |                 | -15.50          | 3946.9               | 5309.6            | 9256.5            | 5549.4         | -42.8           | 5506.6               |
|            |                 | -16.00          | 4060.9               | 5643.3            | 9704.2            | 5817.9         | -42.8           | 5775.0               |
|            |                 | -16.50          | 4078.1               | 6004.8            | 10083.0           | 6044.9         | -42.8           | 6002.1               |
|            |                 | -17.00          | 2759.5               | 6362.3            | 9121.8            | 5468.7         | -42.8           | 5425.9               |
| -17.50     | 2206.8          | 6703.5          | 8910.3               | 5341.9            | -42.8             | 5299.1         |                 |                      |
| -18.00     | 1943.6          | 7025.9          | 8969.4               | 5377.4            | -42.8             | 5334.5         |                 |                      |
| -18.50     | 2067.7          | 7328.7          | 9396.3               | 5633.3            | -42.8             | 5590.5         |                 |                      |
| -19.00     | 1647.2          | 7468.1          | 9115.4               | 5464.8            | -42.8             | 5422.0         |                 |                      |
| -19.50     | 1624.0          | 7668.2          | 9292.2               | 5570.9            | -42.8             | 5528.0         |                 |                      |
| -20.00     | 1499.2          | 7949.2          | 9448.5               | 5664.5            | -42.8             | 5621.7         |                 |                      |
| -20.50     | 1190.1          | 8250.9          | 9440.9               | 5660.0            | -42.8             | 5617.2         |                 |                      |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld<br>niveau | paalpunt<br>niveau | Bezwijkdraagvermogen |                      |                      | Rekenwaarden      |                     |                         |       |        |
|-----------|--------------------|--------------------|----------------------|----------------------|----------------------|-------------------|---------------------|-------------------------|-------|--------|
|           |                    |                    | $R_{b,real}$<br>[kN] | $R_{s,real}$<br>[kN] | $R_{c,real}$<br>[kN] | $R_{s,d}$<br>[kN] | $F_{b,k;d}$<br>[kN] | $R_{s,netto;d}$<br>[kN] |       |        |
| 251.S01   | -1.05              | -21.00             | 932.8                | 8517.0               | 9449.9               | 5665.4            | -42.8               | 5622.5                  |       |        |
|           |                    | -21.50             | 845.6                | 8627.5               | 9473.1               | 5679.3            | -42.8               | 5636.5                  |       |        |
|           |                    | -22.00             | 849.7                | 8662.0               | 9511.7               | 5702.5            | -42.8               | 5659.6                  |       |        |
|           |                    | -22.50             | 1132.0               | 8707.7               | 9839.7               | 5899.1            | -42.8               | 5856.3                  |       |        |
|           |                    | -23.00             | 1500.0               | 8781.0               | 10281.0              | 6163.7            | -42.8               | 6120.8                  |       |        |
|           |                    | -23.50             | 1628.1               | 8876.8               | 10504.9              | 6297.9            | -42.8               | 6255.0                  |       |        |
|           |                    | -24.00             | 1628.3               | 9006.5               | 10634.9              | 6375.8            | -42.8               | 6333.0                  |       |        |
|           |                    | -24.50             | 2068.0               | 9124.6               | 11192.6              | 6710.2            | -42.8               | 6667.4                  |       |        |
|           |                    | -25.00             | 2964.5               | 9231.9               | 12196.4              | 7312.0            | -42.8               | 7269.2                  |       |        |
|           |                    | 19-1008-22         | 0.18                 | -10.00               | 3798.1               | 3138.3            | 6936.4              | 4158.5                  | -44.7 | 4113.8 |
|           |                    |                    |                      | -10.50               | 3163.3               | 3439.7            | 6603.0              | 3958.6                  | -44.7 | 3913.9 |
| -11.00    | 3139.5             |                    |                      | 3740.0               | 6879.6               | 4124.4            | -44.7               | 4079.7                  |       |        |
| -11.50    | 3022.4             |                    |                      | 4039.9               | 7062.2               | 4234.0            | -44.7               | 4189.2                  |       |        |
| -12.00    | 2383.0             |                    |                      | 4224.1               | 6607.1               | 3961.1            | -44.7               | 3916.3                  |       |        |
| -12.50    | 1939.5             |                    |                      | 4388.5               | 6328.0               | 3793.8            | -44.7               | 3749.0                  |       |        |
| -13.00    | 1708.4             |                    |                      | 4565.1               | 6273.5               | 3761.1            | -44.7               | 3716.3                  |       |        |
| -13.50    | 1619.2             |                    |                      | 4773.4               | 6392.5               | 3832.4            | -44.7               | 3787.7                  |       |        |
| -14.00    | 1572.7             |                    |                      | 4952.8               | 6525.6               | 3912.2            | -44.7               | 3867.5                  |       |        |
| -14.50    | 1528.2             |                    |                      | 5109.5               | 6637.7               | 3979.4            | -44.7               | 3934.7                  |       |        |
| -15.00    | 1521.5             |                    |                      | 5220.2               | 6741.7               | 4041.8            | -44.7               | 3997.0                  |       |        |
| -15.50    | 1380.6             |                    |                      | 5399.9               | 6780.4               | 4065.0            | -44.7               | 4020.3                  |       |        |
| -16.00    | 1245.5             |                    |                      | 5544.8               | 6790.3               | 4070.9            | -44.7               | 4026.2                  |       |        |
| -16.50    | 1185.2             |                    |                      | 5629.2               | 6814.4               | 4085.4            | -44.7               | 4040.6                  |       |        |
| -17.00    | 1172.3             |                    |                      | 5695.2               | 6867.6               | 4117.2            | -44.7               | 4072.5                  |       |        |
| -17.50    | 1991.8             |                    |                      | 5738.6               | 7730.4               | 4634.6            | -44.7               | 4589.8                  |       |        |
| -18.00    | 2957.5             |                    |                      | 5812.1               | 8769.6               | 5257.6            | -44.7               | 5212.8                  |       |        |
| -18.50    | 3036.0             |                    |                      | 6025.0               | 9061.1               | 5432.3            | -44.7               | 5387.6                  |       |        |
| -19.00    | 3130.1             |                    |                      | 6230.3               | 9360.4               | 5611.8            | -44.7               | 5567.0                  |       |        |
| -19.50    | 3312.7             |                    |                      | 6408.4               | 9721.0               | 5828.0            | -44.7               | 5783.2                  |       |        |
| -20.00    | 3538.0             |                    |                      | 6608.3               | 10146.3              | 6082.9            | -44.7               | 6038.2                  |       |        |
| -20.50    | 3585.1             |                    |                      | 6881.8               | 10466.9              | 6275.1            | -44.7               | 6230.4                  |       |        |
| -21.00    | 3804.1             |                    |                      | 7070.1               | 10874.2              | 6519.3            | -44.7               | 6474.6                  |       |        |
| -21.50    | 3860.6             |                    |                      | 7325.6               | 11186.2              | 6706.3            | -44.7               | 6661.6                  |       |        |
| -22.00    | 3673.2             |                    |                      | 7610.5               | 11283.7              | 6764.8            | -44.7               | 6720.1                  |       |        |
| -22.50    | 4075.4             | 7807.9             | 11883.3              | 7124.3               | -44.7                | 7079.5            |                     |                         |       |        |
| -23.00    | 4451.3             | 8008.2             | 12459.5              | 7469.7               | -44.7                | 7425.0            |                     |                         |       |        |
| -23.50    | 4705.1             | 8240.6             | 12945.7              | 7761.2               | -44.7                | 7716.5            |                     |                         |       |        |
| -24.00    | 5228.0             | 8470.5             | 13698.5              | 8212.5               | -44.7                | 8167.8            |                     |                         |       |        |
| -24.50    | 5718.0             | 8724.5             | 14442.5              | 8658.6               | -44.7                | 8613.9            |                     |                         |       |        |
| -25.00    | 5648.1             | 8994.8             | 14643.0              | 8778.8               | -44.7                | 8734.0            |                     |                         |       |        |
| 202.S03   | 0.03               | -10.00             | 2967.6               | 2572.2               | 5539.8               | 3321.2            | -115.3              | 3205.9                  |       |        |
|           |                    | -10.50             | 2762.5               | 2933.7               | 5696.2               | 3415.0            | -115.3              | 3299.7                  |       |        |
|           |                    | -11.00             | 2646.9               | 3266.5               | 5913.4               | 3545.2            | -115.3              | 3429.9                  |       |        |
|           |                    | -11.50             | 2416.3               | 3555.7               | 5972.0               | 3580.3            | -115.3              | 3465.0                  |       |        |
|           |                    | -12.00             | 1358.0               | 3844.4               | 5202.4               | 3118.9            | -115.3              | 3003.6                  |       |        |
|           |                    | -12.50             | 1401.8               | 3926.1               | 5327.9               | 3194.2            | -115.3              | 3078.8                  |       |        |
|           |                    | -13.00             | 1960.8               | 4018.7               | 5979.5               | 3584.8            | -115.3              | 3469.5                  |       |        |
|           |                    | -13.50             | 2318.2               | 4093.7               | 6411.9               | 3844.1            | -115.3              | 3728.7                  |       |        |
|           |                    | -14.00             | 2566.4               | 4260.5               | 6826.9               | 4092.9            | -115.3              | 3977.5                  |       |        |
|           |                    | -14.50             | 2661.6               | 4409.7               | 7071.3               | 4239.4            | -115.3              | 4124.0                  |       |        |
|           |                    | -15.00             | 2679.2               | 4588.5               | 7267.7               | 4357.1            | -115.3              | 4241.8                  |       |        |
|           |                    | -15.50             | 2720.1               | 4746.6               | 7466.7               | 4476.5            | -115.3              | 4361.1                  |       |        |
|           |                    | -16.00             | 2825.1               | 4899.7               | 7724.8               | 4631.2            | -115.3              | 4515.8                  |       |        |
|           |                    | -16.50             | 3112.7               | 5036.2               | 8148.9               | 4885.4            | -115.3              | 4770.1                  |       |        |
|           |                    | -17.00             | 3368.8               | 5190.4               | 8559.2               | 5131.4            | -115.3              | 5016.1                  |       |        |
|           |                    | -17.50             | 3478.7               | 5357.6               | 8836.3               | 5297.6            | -115.3              | 5182.2                  |       |        |
|           |                    | -18.00             | 3538.3               | 5559.0               | 9097.2               | 5454.0            | -115.3              | 5338.6                  |       |        |
|           |                    | -18.50             | 3626.2               | 5751.0               | 9377.2               | 5621.8            | -115.3              | 5506.5                  |       |        |
|           |                    | -19.00             | 3676.2               | 5974.3               | 9650.5               | 5785.6            | -115.3              | 5670.3                  |       |        |
|           |                    | -19.50             | 3714.8               | 6196.6               | 9911.4               | 5942.1            | -115.3              | 5826.7                  |       |        |
|           |                    | -20.00             | 3622.0               | 6430.1               | 10052.1              | 6026.4            | -115.3              | 5911.1                  |       |        |
|           |                    | -20.50             | 3651.3               | 6620.0               | 10271.3              | 6157.8            | -115.3              | 6042.5                  |       |        |
|           |                    | -21.00             | 4316.8               | 6768.1               | 11084.9              | 6645.6            | -115.3              | 6530.3                  |       |        |
|           |                    | -21.50             | 5604.2               | 6939.5               | 12543.7              | 7520.2            | -115.3              | 7404.9                  |       |        |
|           |                    | -22.00             | 6449.8               | 7200.1               | 13649.9              | 8183.4            | -115.3              | 8068.0                  |       |        |
| -22.50    | 7611.9             | 7501.1             | 15113.1              | 9060.6               | -115.3               | 8945.2            |                     |                         |       |        |
| -23.00    | 8188.8             | 7837.5             | 16026.3              | 9608.1               | -115.3               | 9492.7            |                     |                         |       |        |
| -23.50    | 8832.1             | 8174.2             | 17006.4              | 10195.7              | -115.3               | 10080.3           |                     |                         |       |        |
| -24.00    | 8714.1             | 8526.9             | 17240.9              | 10336.3              | -115.3               | 10221.0           |                     |                         |       |        |
| -24.50    | 8025.9             | 8888.4             | 16914.4              | 10140.5              | -115.3               | 10025.2           |                     |                         |       |        |
| -25.00    | 7858.3             | 9249.9             | 17108.3              | 10256.7              | -115.3               | 10141.4           |                     |                         |       |        |

**PAALGEGEVENS SI Ø508/670**

Type : In de grond gevormde geschroefde paal; groutinjection  
 Wijze van installeren : Schroeven  
 Wijze van terugwinnen : n.v.t.  
 Diameter [m] : 0.590  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{s;k}$  : 1.00  
 Groutomhulling : JA

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**PAALGEGEVENS SI Ø610/850**

Type : In de grond gevormde geschroefde paal; groutinjectie  
 Wijze van installeren : Schroeven  
 Wijze van terugwinnen : n.v.t.  
 Diameter [m] : 0.730  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00  
 Groutomhulling : JA

**PAALGEGEVENS SI Ø762/950**

Type : In de grond gevormde geschroefde paal; groutinjectie  
 Wijze van installeren : Schroeven  
 Wijze van terugwinnen : n.v.t.  
 Diameter [m] : 0.860  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.009 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0090 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.63  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00  
 Groutomhulling : JA

**PAALGEGEVENS MV Ø914/1074**

Type : Geheide in de grond gevormde betonpaal;terugheidend  
 Wijze van installeren : Heien  
 Wijze van terugwinnen : Heien  
 Diameter [m] : 0.994  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00

**PAALGEGEVENS MV Ø1016/1176**

Type : Geheide in de grond gevormde betonpaal;terugheidend  
 Wijze van installeren : Heien  
 Wijze van terugwinnen : Heien  
 Diameter [m] : 1.096  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 0.70  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakkingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 1.00



Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**OVERZICHT NETTO DRAAGVERMOGEN DRUKPALEN**

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maalveld<br>niveau | paalpunt<br>niveau | R <sub>z, netto, d</sub> [kN] |           |           |           |           |  |
|------------|--------------------|--------------------|-------------------------------|-----------|-----------|-----------|-----------|--|
|            |                    |                    | SI Ø508/6                     | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |  |
| 19-1008-14 | 0.40               | -6.00              | 1302                          |           |           |           |           |  |
|            |                    | -6.50              | 1472                          |           |           |           |           |  |
|            |                    | -7.00              | 1599                          | 2233      |           |           |           |  |
|            |                    | -7.50              | 1753                          | 2368      |           |           |           |  |
|            |                    | -8.00              | 1837                          | 2526      | 3239      |           |           |  |
|            |                    | -8.50              | 1960                          | 2678      | 3430      |           |           |  |
|            |                    | -9.00              | 2080                          | 2818      | 3593      |           |           |  |
|            |                    | -9.50              | 2159                          | 2961      | 3760      |           |           |  |
|            |                    | -10.00             | 2546                          | 3509      | 3066      | 4474      | 4965      |  |
|            |                    | -10.50             | 2577                          | 2551      | 2825      | 4437      | 5054      |  |
|            |                    | -11.00             | 2052                          | 2268      | 2732      | 4493      | 5185      |  |
|            |                    | -11.50             | 1727                          | 2199      | 2736      | 4606      | 4907      |  |
|            |                    | -12.00             | 1667                          | 2192      | 2758      | 4362      | 4964      |  |
|            |                    | -12.50             | 1674                          | 2202      | 2573      | 4415      | 4993      |  |
|            |                    | -13.00             | 1674                          | 2127      | 2605      | 4489      | 5061      |  |
|            |                    | -13.50             | 1660                          | 2136      | 2593      | 4532      | 5132      |  |
|            |                    | -14.00             | 1720                          | 2219      | 2713      | 4664      | 5253      |  |
|            |                    | -14.50             | 1765                          | 2282      | 2794      | 4794      | 5404      |  |
|            |                    | -15.00             | 1809                          | 2338      | 2863      | 4912      | 5537      |  |
|            |                    | -15.50             | 1765                          | 2317      | 2887      | 5047      | 5742      |  |
|            |                    | -16.00             | 1958                          | 2543      | 3127      | 5335      | 6029      |  |
|            |                    | -16.50             | 1998                          | 2590      | 3197      | 5485      | 6228      |  |
|            |                    | -17.00             | 2104                          | 2735      | 3366      | 5711      | 6457      |  |
|            |                    | -17.50             | 2166                          | 2812      | 3456      | 5856      | 6616      |  |
|            |                    | -18.00             | 2226                          | 2884      | 3539      | 5991      | 6764      |  |
| -18.50     | 2284               | 2954               | 3619                          | 6157      | 7003      |           |           |  |
| -19.00     | 2446               | 3185               | 3925                          | 6585      | 7453      |           |           |  |
| -19.50     | 2534               | 3299               | 4072                          | 6838      | 7768      |           |           |  |
| -20.00     | 2696               | 3523               | 4351                          | 7238      | 8204      |           |           |  |
| -20.50     | 2801               | 3651               | 4504                          | 7475      | 8467      |           |           |  |
| -21.00     | 2881               | 3767               | 4646                          | 7709      | 8737      |           |           |  |
| -21.50     | 2996               | 3954               | 4882                          | 8059      | 9127      |           |           |  |
| -22.00     | 3101               | 4095               | 5067                          | 8351      | 9062      |           |           |  |
| -22.50     | 3201               | 4227               | 5237                          | 8244      | 9309      |           |           |  |
| -23.00     | 3295               | 4332               | 5103                          | 8468      | 9557      |           |           |  |
| -23.50     | 3373               | 4201               | 5217                          | 8694      | 9806      |           |           |  |
| -24.00     | 3265               | 4292               | 5325                          | 8902      | 10051     |           |           |  |
| -24.50     | 3326               | 4381               | 5431                          | 9092      | 10298     |           |           |  |
| -25.00     | 3384               | 4465               | 5530                          | 9271      | 10506     |           |           |  |
| 19-1008-15 | 0.75               | -6.00              | 797                           |           |           |           |           |  |
|            |                    | -6.50              | 1381                          |           |           |           |           |  |
|            |                    | -7.00              | 1448                          | 2029      |           |           |           |  |
|            |                    | -7.50              | 1549                          | 2153      |           |           |           |  |
|            |                    | -8.00              | 1628                          | 2274      | 2987      |           |           |  |
|            |                    | -8.50              | 1892                          | 2639      | 3463      |           |           |  |
|            |                    | -9.00              | 2161                          | 2981      | 3847      |           |           |  |
|            |                    | -9.50              | 2291                          | 3135      | 4025      |           |           |  |
|            |                    | -10.00             | 2533                          | 3405      | 4103      | 6409      | 7424      |  |
|            |                    | -10.50             | 2753                          | 3366      | 4293      | 6729      | 7780      |  |
|            |                    | -11.00             | 2580                          | 3480      | 4414      | 6928      | 7988      |  |
|            |                    | -11.50             | 2635                          | 3588      | 4531      | 7121      | 8189      |  |
|            |                    | -12.00             | 2706                          | 3730      | 4696      | 7384      | 8411      |  |
|            |                    | -12.50             | 2729                          | 3768      | 4764      | 5694      | 6255      |  |
|            |                    | -13.00             | 2727                          | 3828      | 3595      | 5662      | 6227      |  |
|            |                    | -13.50             | 3281                          | 2953      | 3465      | 5645      | 6325      |  |
|            |                    | -14.00             | 2293                          | 2839      | 3402      | 5639      | 6131      |  |
|            |                    | -14.50             | 2186                          | 2755      | 3328      | 5442      | 6039      |  |
|            |                    | -15.00             | 2122                          | 2704      | 3145      | 5370      | 5963      |  |
|            |                    | -15.50             | 2092                          | 2565      | 3057      | 5315      | 5897      |  |
|            |                    | -16.00             | 2019                          | 2526      | 3013      | 5312      | 5900      |  |
|            |                    | -16.50             | 2031                          | 2554      | 3055      | 5392      | 5996      |  |
|            |                    | -17.00             | 2050                          | 2542      | 3033      | 5364      | 5959      |  |
|            |                    | -17.50             | 2034                          | 2552      | 3046      | 5389      | 5986      |  |
|            |                    | -18.00             | 2035                          | 2550      | 3038      | 5388      | 5980      |  |
| -18.50     | 2044               | 2560               | 3050                          | 5408      | 6000      |           |           |  |
| -19.00     | 2051               | 2570               | 3062                          | 5427      | 6026      |           |           |  |
| -19.50     | 2065               | 2588               | 3086                          | 5473      | 6080      |           |           |  |
| -20.00     | 2094               | 2650               | 3180                          | 5632      | 6303      |           |           |  |
| -20.50     | 2232               | 2880               | 3513                          | 6134      | 6896      |           |           |  |
| -21.00     | 2369               | 3035               | 3690                          | 6374      | 7155      |           |           |  |
| -21.50     | 2424               | 3103               | 3770                          | 6499      | 7296      |           |           |  |
| -22.00     | 2504               | 3235               | 3956                          | 6807      | 7671      |           |           |  |
| -22.50     | 2660               | 3441               | 4137                          | 7061      | 7946      |           |           |  |
| -23.00     | 2786               | 3484               | 4250                          | 7178      | 8069      |           |           |  |
| -23.50     | 2784               | 3579               | 4363                          | 7348      | 8257      |           |           |  |
| -24.00     | 2838               | 3632               | 4419                          | 7519      | 8446      |           |           |  |
| -24.50     | 2898               | 3709               | 4505                          | 7665      | 8602      |           |           |  |
| -25.00     | 2940               | 3752               | 4544                          | 7742      | 8673      |           |           |  |
| 251.S01    | -1.05              | -6.00              | 621                           |           |           |           |           |  |
|            |                    | -6.50              | 526                           |           |           |           |           |  |
|            |                    | -7.00              | 556                           | 751       |           |           |           |  |
|            |                    | -7.50              | 553                           | 728       |           |           |           |  |
|            |                    | -8.00              | 557                           | 720       | 879       |           |           |  |
|            |                    | -8.50              | 541                           | 709       | 924       |           |           |  |
|            |                    | -9.00              | 788                           | 1110      | 1484      |           |           |  |
|            |                    | -9.50              | 921                           | 1242      | 1582      |           |           |  |
|            |                    | -10.00             | 979                           | 1319      | 1671      | 2669      | 3066      |  |
|            |                    | -10.50             | 1029                          | 1371      | 1722      | 2768      | 3164      |  |
|            |                    | -11.00             | 1062                          | 1401      | 1746      | 2822      | 3216      |  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld paalpunt |        | R <sub>netto;d</sub> [kN] |           |           |           |           |
|------------|-------------------|--------|---------------------------|-----------|-----------|-----------|-----------|
|            | niveau            | niveau | SI Ø508/6                 | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |
|            | -11.50            | 1120   | 1476                      | 1845      | 2977      |           | 3409      |
|            | -12.00            | 1315   | 1758                      | 1926      | 3130      |           | 3587      |
|            | -12.50            | 1403   | 1615                      | 2029      | 3301      |           | 3781      |
|            | -13.00            | 1280   | 1701                      | 2133      | 3462      |           | 3959      |
|            | -13.50            | 1344   | 1782                      | 2230      | 3645      |           | 4164      |
|            | -14.00            | 1386   | 1831                      | 2279      | 3747      |           | 4266      |
|            | -14.50            | 1391   | 1828                      | 2253      | 3739      |           | 4234      |
|            | -15.00            | 1353   | 1790                      | 2308      | 4022      |           | 4712      |
|            | -15.50            | 1938   | 2678                      | 3030      | 4793      |           | 5506      |
|            | -16.00            | 2161   | 2507                      | 3115      | 5053      |           | 5775      |
|            | -16.50            | 1961   | 2569                      | 3242      | 5263      |           | 6002      |
|            | -17.00            | 2011   | 2685                      | 3360      | 5474      |           | 5425      |
|            | -17.50            | 2088   | 2754                      | 3431      | 4761      |           | 5299      |
|            | -18.00            | 2111   | 2763                      | 2925      | 4787      |           | 5334      |
|            | -18.50            | 2101   | 2464                      | 2960      | 4965      |           | 5590      |
|            | -19.00            | 2012   | 2507                      | 2946      | 4864      |           | 5422      |
|            | -19.50            | 1970   | 2482                      | 2966      | 4922      |           | 5528      |
|            | -20.00            | 1973   | 2478                      | 2978      | 5020      |           | 5621      |
|            | -20.50            | 1980   | 2505                      | 3011      | 5034      |           | 5617      |
|            | -21.00            | 2026   | 2550                      | 3051      | 5052      |           | 5622      |
|            | -21.50            | 2048   | 2573                      | 3074      | 5069      |           | 5636      |
|            | -22.00            | 2061   | 2589                      | 3092      | 5090      |           | 5659      |
|            | -22.50            | 2099   | 2675                      | 3208      | 5254      |           | 5856      |
|            | -23.00            | 2161   | 2725                      | 3289      | 5427      |           | 6120      |
|            | -23.50            | 2255   | 2864                      | 3454      | 5592      |           | 6255      |
|            | -24.00            | 2305   | 2923                      | 3522      | 5669      |           | 6332      |
|            | -24.50            | 2353   | 3002                      | 3689      | 5948      |           | 6667      |
|            | -25.00            | 2529   | 3240                      | 3969      | 6375      |           | 7269      |
| 19-1008-22 | 0.18              | -6.00  | 745                       |           |           |           |           |
|            |                   | -6.50  | 994                       |           |           |           |           |
|            |                   | -7.00  | 1105                      | 1552      |           |           |           |
|            |                   | -7.50  | 1221                      | 1700      |           |           |           |
|            |                   | -8.00  | 1335                      | 1844      | 2374      |           |           |
|            |                   | -8.50  | 1447                      | 1981      | 2110      |           |           |
|            |                   | -9.00  | 1628                      | 1761      | 2197      |           |           |
|            |                   | -9.50  | 1396                      | 1827      | 2285      |           |           |
|            |                   | -10.00 | 1416                      | 1904      | 2393      | 3710      | 4113      |
|            |                   | -10.50 | 1448                      | 1992      | 2461      | 3653      | 3913      |
|            |                   | -11.00 | 1484                      | 2027      | 2409      | 3571      | 4079      |
|            |                   | -11.50 | 1489                      | 1958      | 2264      | 3682      | 4189      |
|            |                   | -12.00 | 1509                      | 1836      | 2320      | 3818      | 3916      |
|            |                   | -12.50 | 1396                      | 1874      | 2379      | 3562      | 3749      |
|            |                   | -13.00 | 1428                      | 1916      | 2162      | 3359      | 3716      |
|            |                   | -13.50 | 1456                      | 1769      | 2016      | 3363      | 3787      |
|            |                   | -14.00 | 1374                      | 1671      | 1990      | 3427      | 3867      |
|            |                   | -14.50 | 1322                      | 1650      | 2016      | 3491      | 3934      |
|            |                   | -15.00 | 1302                      | 1672      | 2049      | 3548      | 3997      |
|            |                   | -15.50 | 1312                      | 1686      | 2056      | 3576      | 4020      |
|            |                   | -16.00 | 1321                      | 1691      | 2055      | 3588      | 4026      |
|            |                   | -16.50 | 1329                      | 1698      | 2061      | 3604      | 4040      |
|            |                   | -17.00 | 1330                      | 1697      | 2056      | 3615      | 4072      |
|            |                   | -17.50 | 1396                      | 1816      | 2252      | 3981      | 4589      |
|            |                   | -18.00 | 1663                      | 2173      | 2707      | 4579      | 5212      |
|            |                   | -18.50 | 1713                      | 2255      | 2804      | 4737      | 5387      |
|            |                   | -19.00 | 1781                      | 2339      | 2904      | 4899      | 5567      |
|            |                   | -19.50 | 1856                      | 2437      | 3025      | 5089      | 5783      |
|            |                   | -20.00 | 1943                      | 2552      | 3168      | 5313      | 6038      |
|            |                   | -20.50 | 1955                      | 2581      | 3227      | 5472      | 6230      |
|            |                   | -21.00 | 2100                      | 2752      | 3410      | 5703      | 6474      |
|            |                   | -21.50 | 2175                      | 2842      | 3514      | 5874      | 6661      |
|            |                   | -22.00 | 2210                      | 2882      | 3546      | 5942      | 6720      |
|            |                   | -22.50 | 2299                      | 3009      | 3732      | 6241      | 7079      |
|            |                   | -23.00 | 2430                      | 3195      | 3944      | 6552      | 7424      |
|            |                   | -23.50 | 2495                      | 3301      | 4083      | 6798      | 7716      |
|            |                   | -24.00 | 2622                      | 3496      | 4352      | 7191      | 8167      |
|            |                   | -24.50 | 2735                      | 3636      | 4556      | 7536      | 8613      |
|            |                   | -25.00 | 2907                      | 3875      | 4869      | 7994      | 8734      |
| 202.S03    | 0.03              | -6.00  | 416                       |           |           |           |           |
|            |                   | -6.50  | 617                       |           |           |           |           |
|            |                   | -7.00  | 732                       | 1098      |           |           |           |
|            |                   | -7.50  | 1091                      | 1588      |           |           |           |
|            |                   | -8.00  | 1165                      | 1669      | 2213      |           |           |
|            |                   | -8.50  | 1249                      | 1827      | 2546      |           |           |
|            |                   | -9.00  | 1518                      | 2155      | 1948      |           |           |
|            |                   | -9.50  | 1604                      | 1532      | 1867      |           |           |
|            |                   | -10.00 | 1131                      | 1459      | 1772      | 2831      | 3205      |
|            |                   | -10.50 | 1090                      | 1404      | 1784      | 2866      | 3299      |
|            |                   | -11.00 | 1076                      | 1453      | 1807      | 3009      | 3429      |
|            |                   | -11.50 | 1066                      | 1414      | 1808      | 3028      | 3464      |
|            |                   | -12.00 | 961                       | 1261      | 1552      | 2668      | 3003      |
|            |                   | -12.50 | 994                       | 1296      | 1597      | 2727      | 3078      |
|            |                   | -13.00 | 1019                      | 1377      | 1763      | 3046      | 3469      |
|            |                   | -13.50 | 1178                      | 1562      | 1956      | 3264      | 3728      |
|            |                   | -14.00 | 1252                      | 1672      | 2095      | 3486      | 3977      |
|            |                   | -14.50 | 1311                      | 1738      | 2175      | 3613      | 4124      |
|            |                   | -15.00 | 1360                      | 1796      | 2240      | 3721      | 4241      |
|            |                   | -15.50 | 1408                      | 1855      | 2308      | 3831      | 4361      |
|            |                   | -16.00 | 1451                      | 1907      | 2376      | 3958      | 4515      |
|            |                   | -16.50 | 1541                      | 2029      | 2526      | 4182      | 4770      |
|            |                   | -17.00 | 1621                      | 2147      | 2693      | 4403      | 5016      |
|            |                   | -17.50 | 1743                      | 2305      | 2772      | 4552      | 5182      |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld paalpunt |        | R <sub>n, netto;d</sub> [kN] |           |           |           |           |
|-----------|-------------------|--------|------------------------------|-----------|-----------|-----------|-----------|
|           | niveau            | niveau | SI Ø508/6                    | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |
|           | -18.00            | 1813   | 2308                         | 2308      | 2866      | 4705      | 5338      |
|           | -18.50            | 1805   | 2380                         | 2380      | 2953      | 4846      | 5506      |
|           | -19.00            | 1850   | 2457                         | 2457      | 3044      | 4996      | 5670      |
|           | -19.50            | 1894   | 2521                         | 2521      | 3130      | 5140      | 5826      |
|           | -20.00            | 1918   | 2551                         | 2551      | 3174      | 5225      | 5911      |
|           | -20.50            | 1937   | 2570                         | 2570      | 3212      | 5329      | 6042      |
|           | -21.00            | 2024   | 2700                         | 2700      | 3412      | 5703      | 6530      |
|           | -21.50            | 2247   | 3053                         | 3053      | 3903      | 6454      | 7404      |
|           | -22.00            | 2444   | 3307                         | 3307      | 4216      | 6950      | 8068      |
|           | -22.50            | 2737   | 3724                         | 3724      | 4943      | 7754      | 8945      |
|           | -23.00            | 2870   | 3925                         | 3925      | 5005      | 8068      | 9492      |
|           | -23.50            | 3322   | 4195                         | 4195      | 5377      | 8710      | 10080     |
|           | -24.00            | 3117   | 4323                         | 4323      | 5596      | 9074      | 10220     |
|           | -24.50            | 3233   | 4443                         | 4443      | 5675      | 8931      | 10025     |
|           | -25.00            | 3205   | 4326                         | 4326      | 5574      | 8809      | 10141     |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

**OVERZICHT NETTO DRAAGVERMOGEN TREKPALEN (n=1)**

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maalveld<br>niveau | paalpunt<br>niveau | R <sub>netto;d</sub> [kN] |           |           |           |           |  |
|------------|--------------------|--------------------|---------------------------|-----------|-----------|-----------|-----------|--|
|            |                    |                    | SI Ø508/6                 | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |  |
| 19-1008-14 | 0.40               | -6.00              | 273                       |           |           |           |           |  |
|            |                    | -6.50              | 320                       |           |           |           |           |  |
|            |                    | -7.00              | 369                       | 463       |           |           |           |  |
|            |                    | -7.50              | 418                       | 524       |           |           |           |  |
|            |                    | -8.00              | 468                       | 587       | 701       |           |           |  |
|            |                    | -8.50              | 523                       | 656       | 782       |           |           |  |
|            |                    | -9.00              | 578                       | 724       | 863       |           |           |  |
|            |                    | -9.50              | 629                       | 788       | 938       |           |           |  |
|            |                    | -10.00             | 678                       | 849       | 1011      | 1542      | 1711      |  |
|            |                    | -10.50             | 730                       | 914       | 1088      | 1660      | 1842      |  |
|            |                    | -11.00             | 785                       | 982       | 1169      | 1784      | 1979      |  |
|            |                    | -11.50             | 840                       | 1050      | 1250      | 1909      | 2117      |  |
|            |                    | -12.00             | 895                       | 1119      | 1331      | 2033      | 2255      |  |
|            |                    | -12.50             | 950                       | 1187      | 1412      | 2158      | 2393      |  |
|            |                    | -13.00             | 1004                      | 1256      | 1493      | 2282      | 2530      |  |
|            |                    | -13.50             | 1039                      | 1299      | 1545      | 2360      | 2616      |  |
|            |                    | -14.00             | 1061                      | 1327      | 1578      | 2402      | 2664      |  |
|            |                    | -14.50             | 1079                      | 1350      | 1606      | 2444      | 2710      |  |
|            |                    | -15.00             | 1106                      | 1384      | 1646      | 2506      | 2779      |  |
|            |                    | -15.50             | 1145                      | 1432      | 1703      | 2592      | 2875      |  |
|            |                    | -16.00             | 1161                      | 1452      | 1728      | 2630      | 2917      |  |
|            |                    | -16.50             | 1190                      | 1489      | 1772      | 2696      | 2991      |  |
|            |                    | -17.00             | 1215                      | 1520      | 1809      | 2753      | 3054      |  |
|            |                    | -17.50             | 1244                      | 1557      | 1853      | 2820      | 3129      |  |
|            |                    | -18.00             | 1275                      | 1595      | 1899      | 2890      | 3206      |  |
| -18.50     | 1304               | 1632               | 1943                      | 2957      | 3280      |           |           |  |
| -19.00     | 1333               | 1668               | 1985                      | 3022      | 3352      |           |           |  |
| -19.50     | 1367               | 1710               | 2035                      | 3098      | 3437      |           |           |  |
| -20.00     | 1400               | 1752               | 2085                      | 3174      | 3521      |           |           |  |
| -20.50     | 1439               | 1800               | 2143                      | 3263      | 3619      |           |           |  |
| -21.00     | 1480               | 1852               | 2204                      | 3356      | 3723      |           |           |  |
| -21.50     | 1519               | 1901               | 2262                      | 3446      | 3822      |           |           |  |
| -22.00     | 1561               | 1953               | 2324                      | 3540      | 3926      |           |           |  |
| -22.50     | 1604               | 2006               | 2387                      | 3637      | 4034      |           |           |  |
| -23.00     | 1648               | 2061               | 2452                      | 3736      | 4144      |           |           |  |
| -23.50     | 1691               | 2116               | 2517                      | 3836      | 4254      |           |           |  |
| -24.00     | 1736               | 2171               | 2583                      | 3936      | 4365      |           |           |  |
| -24.50     | 1780               | 2226               | 2649                      | 4036      | 4477      |           |           |  |
| -25.00     | 1826               | 2283               | 2717                      | 4141      | 4592      |           |           |  |
| 19-1008-15 | 0.75               | -6.00              | 359                       |           |           |           |           |  |
|            |                    | -6.50              | 380                       |           |           |           |           |  |
|            |                    | -7.00              | 424                       | 532       |           |           |           |  |
|            |                    | -7.50              | 468                       | 587       |           |           |           |  |
|            |                    | -8.00              | 513                       | 642       | 765       |           |           |  |
|            |                    | -8.50              | 559                       | 700       | 834       |           |           |  |
|            |                    | -9.00              | 614                       | 768       | 915       |           |           |  |
|            |                    | -9.50              | 669                       | 837       | 996       |           |           |  |
|            |                    | -10.00             | 724                       | 905       | 1077      | 1642      | 1821      |  |
|            |                    | -10.50             | 779                       | 974       | 1158      | 1766      | 1958      |  |
|            |                    | -11.00             | 834                       | 1042      | 1240      | 1890      | 2096      |  |
|            |                    | -11.50             | 889                       | 1111      | 1321      | 2015      | 2234      |  |
|            |                    | -12.00             | 944                       | 1179      | 1402      | 2139      | 2371      |  |
|            |                    | -12.50             | 999                       | 1248      | 1483      | 2264      | 2509      |  |
|            |                    | -13.00             | 1053                      | 1315      | 1563      | 2386      | 2645      |  |
|            |                    | -13.50             | 1101                      | 1375      | 1635      | 2496      | 2766      |  |
|            |                    | -14.00             | 1156                      | 1444      | 1716      | 2620      | 2904      |  |
|            |                    | -14.50             | 1211                      | 1512      | 1797      | 2744      | 3041      |  |
|            |                    | -15.00             | 1266                      | 1581      | 1878      | 2869      | 3179      |  |
|            |                    | -15.50             | 1321                      | 1649      | 1959      | 2993      | 3317      |  |
|            |                    | -16.00             | 1376                      | 1717      | 2040      | 3117      | 3454      |  |
|            |                    | -16.50             | 1390                      | 1736      | 2062      | 3151      | 3491      |  |
|            |                    | -17.00             | 1397                      | 1746      | 2074      | 3168      | 3511      |  |
|            |                    | -17.50             | 1408                      | 1759      | 2091      | 3193      | 3539      |  |
|            |                    | -18.00             | 1424                      | 1780      | 2116      | 3231      | 3581      |  |
| -18.50     | 1430               | 1787               | 2125                      | 3244      | 3597      |           |           |  |
| -19.00     | 1436               | 1795               | 2134                      | 3258      | 3613      |           |           |  |
| -19.50     | 1442               | 1803               | 2145                      | 3274      | 3631      |           |           |  |
| -20.00     | 1449               | 1812               | 2156                      | 3290      | 3649      |           |           |  |
| -20.50     | 1458               | 1823               | 2170                      | 3310      | 3672      |           |           |  |
| -21.00     | 1476               | 1846               | 2197                      | 3351      | 3717      |           |           |  |
| -21.50     | 1500               | 1877               | 2234                      | 3407      | 3780      |           |           |  |
| -22.00     | 1525               | 1908               | 2270                      | 3464      | 3842      |           |           |  |
| -22.50     | 1550               | 1940               | 2309                      | 3522      | 3907      |           |           |  |
| -23.00     | 1581               | 1978               | 2355                      | 3592      | 3985      |           |           |  |
| -23.50     | 1618               | 2024               | 2409                      | 3675      | 4077      |           |           |  |
| -24.00     | 1651               | 2065               | 2458                      | 3750      | 4160      |           |           |  |
| -24.50     | 1692               | 2117               | 2520                      | 3845      | 4265      |           |           |  |
| -25.00     | 1734               | 2170               | 2582                      | 3940      | 4370      |           |           |  |
| 251.S01    | -1.05              | -6.00              | 216                       |           |           |           |           |  |
|            |                    | -6.50              | 254                       |           |           |           |           |  |
|            |                    | -7.00              | 298                       | 378       |           |           |           |  |
|            |                    | -7.50              | 341                       | 431       |           |           |           |  |
|            |                    | -8.00              | 381                       | 481       | 577       |           |           |  |
|            |                    | -8.50              | 408                       | 515       | 617       |           |           |  |
|            |                    | -9.00              | 414                       | 522       | 626       |           |           |  |
|            |                    | -9.50              | 439                       | 554       | 664       |           |           |  |
|            |                    | -10.00             | 476                       | 600       | 720       | 1051      | 1172      |  |
|            |                    | -10.50             | 520                       | 655       | 784       | 1151      | 1281      |  |
|            |                    | -11.00             | 554                       | 697       | 835       | 1227      | 1366      |  |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

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 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering  | maaiveld paalpunt |        | R <sub>n, netto;d</sub> [kN] |           |           |           |           |
|------------|-------------------|--------|------------------------------|-----------|-----------|-----------|-----------|
|            | niveau            | niveau | SI Ø508/6                    | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |
|            | -11.50            |        | 575                          | 724       | 866       | 1275      | 1420      |
|            | -12.00            |        | 595                          | 750       | 898       | 1323      | 1473      |
|            | -12.50            |        | 630                          | 793       | 949       | 1401      | 1560      |
|            | -13.00            |        | 670                          | 843       | 1009      | 1493      | 1662      |
|            | -13.50            |        | 708                          | 891       | 1066      | 1580      | 1758      |
|            | -14.00            |        | 761                          | 956       | 1143      | 1699      | 1889      |
|            | -14.50            |        | 813                          | 1021      | 1220      | 1816      | 2020      |
|            | -15.00            |        | 869                          | 1091      | 1303      | 1930      | 2145      |
|            | -15.50            |        | 895                          | 1124      | 1342      | 1978      | 2198      |
|            | -16.00            |        | 946                          | 1188      | 1418      | 2093      | 2326      |
|            | -16.50            |        | 1001                         | 1256      | 1499      | 2217      | 2464      |
|            | -17.00            |        | 1056                         | 1324      | 1579      | 2341      | 2600      |
|            | -17.50            |        | 1108                         | 1389      | 1656      | 2458      | 2731      |
|            | -18.00            |        | 1157                         | 1450      | 1729      | 2570      | 2854      |
|            | -18.50            |        | 1212                         | 1518      | 1810      | 2681      | 2977      |
|            | -19.00            |        | 1245                         | 1560      | 1860      | 2739      | 3042      |
|            | -19.50            |        | 1281                         | 1605      | 1913      | 2813      | 3124      |
|            | -20.00            |        | 1324                         | 1659      | 1977      | 2911      | 3232      |
|            | -20.50            |        | 1384                         | 1733      | 2065      | 3024      | 3358      |
|            | -21.00            |        | 1447                         | 1812      | 2158      | 3132      | 3477      |
|            | -21.50            |        | 1474                         | 1845      | 2198      | 3179      | 3530      |
|            | -22.00            |        | 1483                         | 1858      | 2213      | 3197      | 3550      |
|            | -22.50            |        | 1495                         | 1873      | 2232      | 3219      | 3575      |
|            | -23.00            |        | 1514                         | 1896      | 2260      | 3252      | 3612      |
|            | -23.50            |        | 1537                         | 1926      | 2295      | 3294      | 3658      |
|            | -24.00            |        | 1569                         | 1965      | 2342      | 3349      | 3719      |
|            | -24.50            |        | 1597                         | 2001      | 2385      | 3399      | 3775      |
|            | -25.00            |        | 1624                         | 2034      | 2424      | 3445      | 3826      |
| 19-1008-22 | 0.18              | -6.00  | 155                          |           |           |           |           |
|            |                   | -6.50  | 190                          |           |           |           |           |
|            |                   | -7.00  | 234                          | 297       |           |           |           |
|            |                   | -7.50  | 278                          | 352       |           |           |           |
|            |                   | -8.00  | 323                          | 407       | 489       |           |           |
|            |                   | -8.50  | 367                          | 463       | 555       |           |           |
|            |                   | -9.00  | 411                          | 517       | 620       |           |           |
|            |                   | -9.50  | 457                          | 575       | 688       |           |           |
|            |                   | -10.00 | 503                          | 632       | 756       | 1147      | 1276      |
|            |                   | -10.50 | 549                          | 690       | 824       | 1252      | 1392      |
|            |                   | -11.00 | 595                          | 747       | 892       | 1356      | 1507      |
|            |                   | -11.50 | 641                          | 804       | 960       | 1460      | 1623      |
|            |                   | -12.00 | 669                          | 841       | 1003      | 1526      | 1696      |
|            |                   | -12.50 | 695                          | 873       | 1042      | 1585      | 1761      |
|            |                   | -13.00 | 723                          | 908       | 1084      | 1648      | 1831      |
|            |                   | -13.50 | 755                          | 948       | 1132      | 1722      | 1913      |
|            |                   | -14.00 | 783                          | 983       | 1174      | 1786      | 1984      |
|            |                   | -14.50 | 808                          | 1015      | 1211      | 1842      | 2047      |
|            |                   | -15.00 | 826                          | 1037      | 1238      | 1883      | 2093      |
|            |                   | -15.50 | 854                          | 1072      | 1280      | 1948      | 2164      |
|            |                   | -16.00 | 877                          | 1101      | 1315      | 2000      | 2223      |
|            |                   | -16.50 | 891                          | 1119      | 1337      | 2033      | 2259      |
|            |                   | -17.00 | 903                          | 1134      | 1354      | 2059      | 2289      |
|            |                   | -17.50 | 911                          | 1144      | 1367      | 2078      | 2310      |
|            |                   | -18.00 | 923                          | 1160      | 1386      | 2107      | 2343      |
|            |                   | -18.50 | 956                          | 1201      | 1435      | 2182      | 2426      |
|            |                   | -19.00 | 988                          | 1241      | 1483      | 2255      | 2507      |
|            |                   | -19.50 | 1016                         | 1276      | 1525      | 2318      | 2577      |
|            |                   | -20.00 | 1047                         | 1315      | 1571      | 2389      | 2656      |
|            |                   | -20.50 | 1089                         | 1368      | 1633      | 2485      | 2762      |
|            |                   | -21.00 | 1118                         | 1405      | 1677      | 2552      | 2836      |
|            |                   | -21.50 | 1158                         | 1454      | 1736      | 2641      | 2935      |
|            |                   | -22.00 | 1201                         | 1508      | 1800      | 2740      | 3045      |
|            |                   | -22.50 | 1232                         | 1547      | 1846      | 2810      | 3122      |
|            |                   | -23.00 | 1263                         | 1586      | 1893      | 2881      | 3201      |
|            |                   | -23.50 | 1299                         | 1631      | 1946      | 2962      | 3292      |
|            |                   | -24.00 | 1335                         | 1675      | 1999      | 3043      | 3381      |
|            |                   | -24.50 | 1374                         | 1724      | 2057      | 3132      | 3480      |
|            |                   | -25.00 | 1415                         | 1776      | 2119      | 3226      | 3584      |
| 202.S03    | 0.03              | -6.00  | 75                           |           |           |           |           |
|            |                   | -6.50  | 106                          |           |           |           |           |
|            |                   | -7.00  | 146                          | 188       |           |           |           |
|            |                   | -7.50  | 187                          | 239       |           |           |           |
|            |                   | -8.00  | 231                          | 294       | 356       |           |           |
|            |                   | -8.50  | 275                          | 349       | 421       |           |           |
|            |                   | -9.00  | 326                          | 412       | 496       |           |           |
|            |                   | -9.50  | 381                          | 481       | 577       |           |           |
|            |                   | -10.00 | 436                          | 549       | 658       | 985       | 1097      |
|            |                   | -10.50 | 491                          | 618       | 740       | 1110      | 1235      |
|            |                   | -11.00 | 541                          | 681       | 815       | 1225      | 1363      |
|            |                   | -11.50 | 586                          | 737       | 881       | 1326      | 1475      |
|            |                   | -12.00 | 635                          | 797       | 953       | 1430      | 1590      |
|            |                   | -12.50 | 653                          | 821       | 981       | 1465      | 1629      |
|            |                   | -13.00 | 672                          | 844       | 1009      | 1502      | 1671      |
|            |                   | -13.50 | 686                          | 863       | 1031      | 1533      | 1705      |
|            |                   | -14.00 | 712                          | 895       | 1070      | 1593      | 1772      |
|            |                   | -14.50 | 736                          | 925       | 1106      | 1647      | 1832      |
|            |                   | -15.00 | 764                          | 960       | 1148      | 1711      | 1903      |
|            |                   | -15.50 | 789                          | 992       | 1185      | 1768      | 1966      |
|            |                   | -16.00 | 813                          | 1022      | 1222      | 1823      | 2027      |
|            |                   | -16.50 | 835                          | 1049      | 1254      | 1873      | 2083      |
|            |                   | -17.00 | 859                          | 1080      | 1291      | 1928      | 2145      |
|            |                   | -17.50 | 885                          | 1113      | 1330      | 1988      | 2211      |

Project : D1.3 ZWO380 Nieuwe reconstructiemasten  
 Onderdeel : GT-RLL & GT-EHV reconstructiemasten hoek druk en trek

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maalveld paalpunt |        | R <sub>n, netto;d</sub> [kN] |           |           |           |           |
|-----------|-------------------|--------|------------------------------|-----------|-----------|-----------|-----------|
|           | niveau            | niveau | SI Ø508/6                    | SI Ø610/8 | SI Ø762/9 | MV Ø914/1 | MV Ø1016/ |
|           | -18.00            |        | 917                          | 1152      | 1377      | 2060      | 2291      |
|           | -18.50            |        | 947                          | 1190      | 1422      | 2128      | 2366      |
|           | -19.00            |        | 981                          | 1233      | 1473      | 2207      | 2454      |
|           | -19.50            |        | 1016                         | 1276      | 1525      | 2285      | 2540      |
|           | -20.00            |        | 1052                         | 1321      | 1578      | 2367      | 2631      |
|           | -20.50            |        | 1081                         | 1358      | 1622      | 2434      | 2706      |
|           | -21.00            |        | 1105                         | 1388      | 1658      | 2488      | 2766      |
|           | -21.50            |        | 1132                         | 1422      | 1698      | 2549      | 2834      |
|           | -22.00            |        | 1172                         | 1472      | 1758      | 2640      | 2935      |
|           | -22.50            |        | 1218                         | 1529      | 1826      | 2745      | 3051      |
|           | -23.00            |        | 1269                         | 1593      | 1902      | 2861      | 3179      |
|           | -23.50            |        | 1320                         | 1657      | 1977      | 2977      | 3308      |
|           | -24.00            |        | 1374                         | 1724      | 2057      | 3099      | 3443      |
|           | -24.50            |        | 1429                         | 1793      | 2138      | 3223      | 3581      |
|           | -25.00            |        | 1484                         | 1861      | 2219      | 3348      | 3718      |

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLI overgangsmasten druk en trek

**ALGEMENE GEGEVENS**

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLI overgangsmasten druk en trek  
 Datum : 12-08-2019  
 Bestand : P:\EANL\_Projects\10124719 - TenneT Engineering  
 ZW380 kV Oost\2 Content\010 D1.3  
 Reconstructiemasten\Technosoft\D1.3 GT-RLI  
 Overgangsmasten druk en trek.pvw  
 Berekeningstype : Verticaal belaste paal  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

**Toegepaste normen volgens Eurocode met Nederlandse NB**

|             |                    |            |         |
|-------------|--------------------|------------|---------|
| Geotechniek | EN 1997-1:2004     | AC:2009    |         |
|             | NEN-EN 1997-1:2005 | C1+A1:2013 | NB:2016 |
|             | NEN 9997-1:2016    | C2:2017    |         |

**BODEMPROFIELGEGEVENS: M16-Oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)  
 Hoogte maaiveld [m] : 0.00 Grondwaterstand [m] : -0.50

| Laag | Van [m] | Tot [m] | Omschrijving              | OCR | Aandeel pos. kleef [%] | $\alpha_s$ | $d_{s,0}$ [mm] |
|------|---------|---------|---------------------------|-----|------------------------|------------|----------------|
| 1    | 0.00    | -1.00   | Klei - Schoon - Matig     | 1.0 | 0.0                    |            |                |
| 2    | -1.00   | -2.50   | Zand - Schoon - Matig     | 1.0 | 100.0                  |            |                |
| 3    | -2.50   | -3.00   | Klei - Schoon - Vast      | 1.0 | 50.0                   |            |                |
| 4    | -3.00   | -6.00   | Zand - Schoon - Matig     | 1.0 | 100.0                  |            |                |
| 5    | -6.00   | -6.50   | Leem - Zwak zandig - Vast | 1.0 | 50.0                   |            |                |
| 6    | -6.50   | -12.50  | Zand - Schoon - Los       | 1.0 | 100.0                  |            |                |
| 7    | -12.50  | -13.75  | Leem - Zwak zandig - Vast | 1.0 | 50.0                   |            |                |
| 8    | -13.75  | -21.50  | Zand - Schoon - Los       | 1.0 | 100.0                  |            |                |
| 9    | -21.50  | -22.50  | Leem - Zwak zandig - Vast | 1.0 | 50.0                   |            |                |
| 10   | -22.50  | -24.00  | Zand - Schoon - Los       | 1.0 | 100.0                  |            |                |
| 11   | -24.00  | -24.30  | Leem - Zwak zandig - Vast | 1.0 | 50.0                   |            |                |
| 12   | -24.30  | -24.50  | Zand - Schoon - Los       | 1.0 | 100.0                  |            |                |
| 13   | -24.50  | -25.00  | Leem - Zwak zandig - Vast | 1.0 | 50.0                   |            |                |

**BODEMPROFIELGEGEVENS: M68-oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)  
 Hoogte maaiveld [m] : 0.00 Grondwaterstand [m] : -1.00

| Laag | Van [m] | Tot [m] | Omschrijving               | OCR | Aandeel pos. kleef [%] | $\alpha_s$ | $d_{s,0}$ [mm] |
|------|---------|---------|----------------------------|-----|------------------------|------------|----------------|
| 1    | 0.00    | -3.00   | Klei - Zwak zandig - Matig | 1.0 | 50.0                   |            |                |
| 2    | -3.00   | -4.50   | Zand - Schoon - Matig      | 1.0 | 100.0                  |            |                |
| 3    | -4.50   | -5.00   | Klei - Zwak zandig - Matig | 1.0 | 50.0                   |            |                |
| 4    | -5.00   | -7.00   | Zand - Schoon - Los        | 1.0 | 100.0                  |            |                |
| 5    | -7.00   | -8.00   | Klei - Schoon - Vast       | 1.0 | 50.0                   |            |                |
| 6    | -8.00   | -9.00   | Zand - Schoon - Los        | 1.0 | 100.0                  |            |                |
| 7    | -9.00   | -10.50  | Klei - Zwak zandig - Vast  | 1.0 | 50.0                   |            |                |
| 8    | -10.50  | -11.50  | Zand - Schoon - Los        | 1.0 | 100.0                  |            |                |
| 9    | -11.50  | -13.00  | Zand - Schoon - Los        | 1.0 | 100.0                  |            |                |
| 10   | -13.00  | -14.00  | Klei - Zwak zandig - Matig | 1.0 | 50.0                   |            |                |
| 11   | -14.00  | -23.00  | Zand - Schoon - Los        | 1.0 | 100.0                  |            |                |
| 12   | -23.00  | -24.00  | Leem - Zwak zandig - Vast  | 1.0 | 50.0                   |            |                |
| 13   | -24.00  | -24.50  | Zand - Schoon - Los        | 1.0 | 100.0                  |            |                |
| 14   | -24.50  | -25.00  | Leem - Zwak zandig - Vast  | 1.0 | 50.0                   |            |                |

**BODEMPROFIELGEGEVENS: 26-oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)  
 Hoogte maaiveld [m] : 0.04 Grondwaterstand [m] : -0.96

| Laag | Van [m] | Tot [m] | Omschrijving               | OCR | Aandeel pos. kleef [%] | $\alpha_s$ | $d_{s,0}$ [mm] |
|------|---------|---------|----------------------------|-----|------------------------|------------|----------------|
| 1    | 0.04    | -3.20   | Klei - Zwak zandig - Matig | 1.0 | 50.0                   |            |                |
| 2    | -3.20   | -24.57  | Zand - Schoon - Matig      | 1.0 | 100.0                  |            |                |

**BODEMPROFIELGEGEVENS: 78-oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

d50-reductie is meegenomen overeenkomstig NEN-EN 9997 art. 7.6.2.3 (i)  
 Hoogte maaiveld [m] : 0.04 Grondwaterstand [m] : -0.96

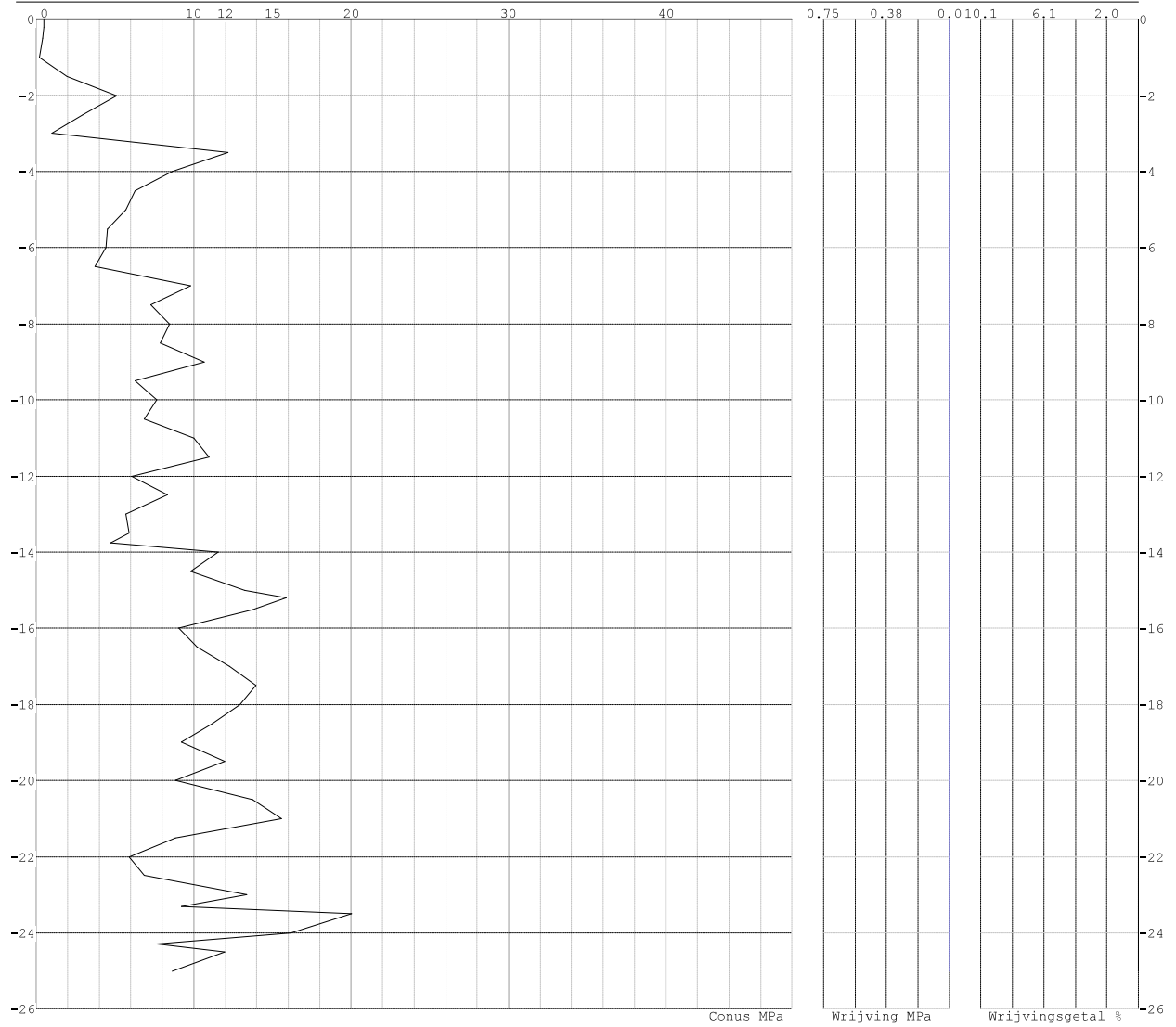
| Laag | Van [m] | Tot [m] | Omschrijving               | OCR | Aandeel pos. kleef [%] | $\alpha_s$ | $d_{s,0}$ [mm] |
|------|---------|---------|----------------------------|-----|------------------------|------------|----------------|
| 1    | 0.04    | -14.02  | Zand - Schoon - Matig      | 1.0 | 100.0                  |            |                |
| 2    | -14.02  | -15.38  | Klei - Zwak zandig - Matig | 1.0 | 50.0                   |            |                |
| 3    | -15.38  | -25.01  | Zand - Schoon - Los        | 1.0 | 100.0                  |            |                |

**SONDERINGSGEGEVENS ALGEMEEN: M16-Oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
 Hoogte maaiveld [m] : 0.00 Bodemprofiel: M16-Oud  
 Traject negatieve kleef : 0.00 tot -1.00 [m]  
 Traject positieve kleef : -1.00 tot -25.00 [m]

Project : D1.3 ZWO380 Bestaande overgangsmasten  
Onderdeel : GT-RLl overgangsmasten druk en trek

**SONDERINGSGEGEVENS GRAFIEK: M16-Oud**



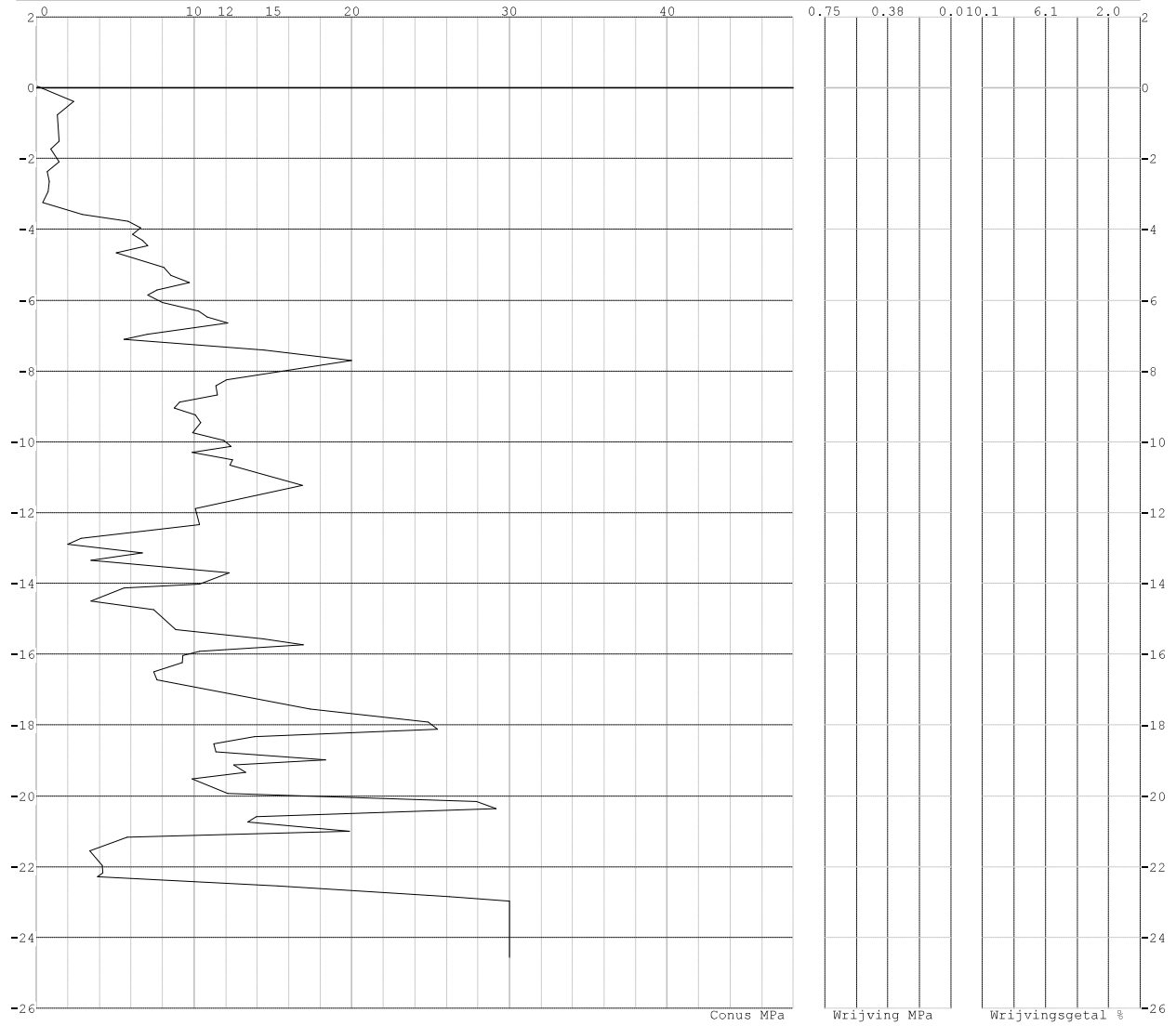


Project : D1.3 ZWO380 Bestaande overgangsmasten  
Onderdeel : GT-RLl overgangsmasten druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 26-oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : 0.04 Bodemprofiel: 26-oud  
Traject negatieve kleeft : 0.04 tot -3.19 [m]  
Traject positieve kleeft : -3.20 tot -24.58 [m]

**SONDERINGSGEGEVENS GRAFIEK: 26-oud**

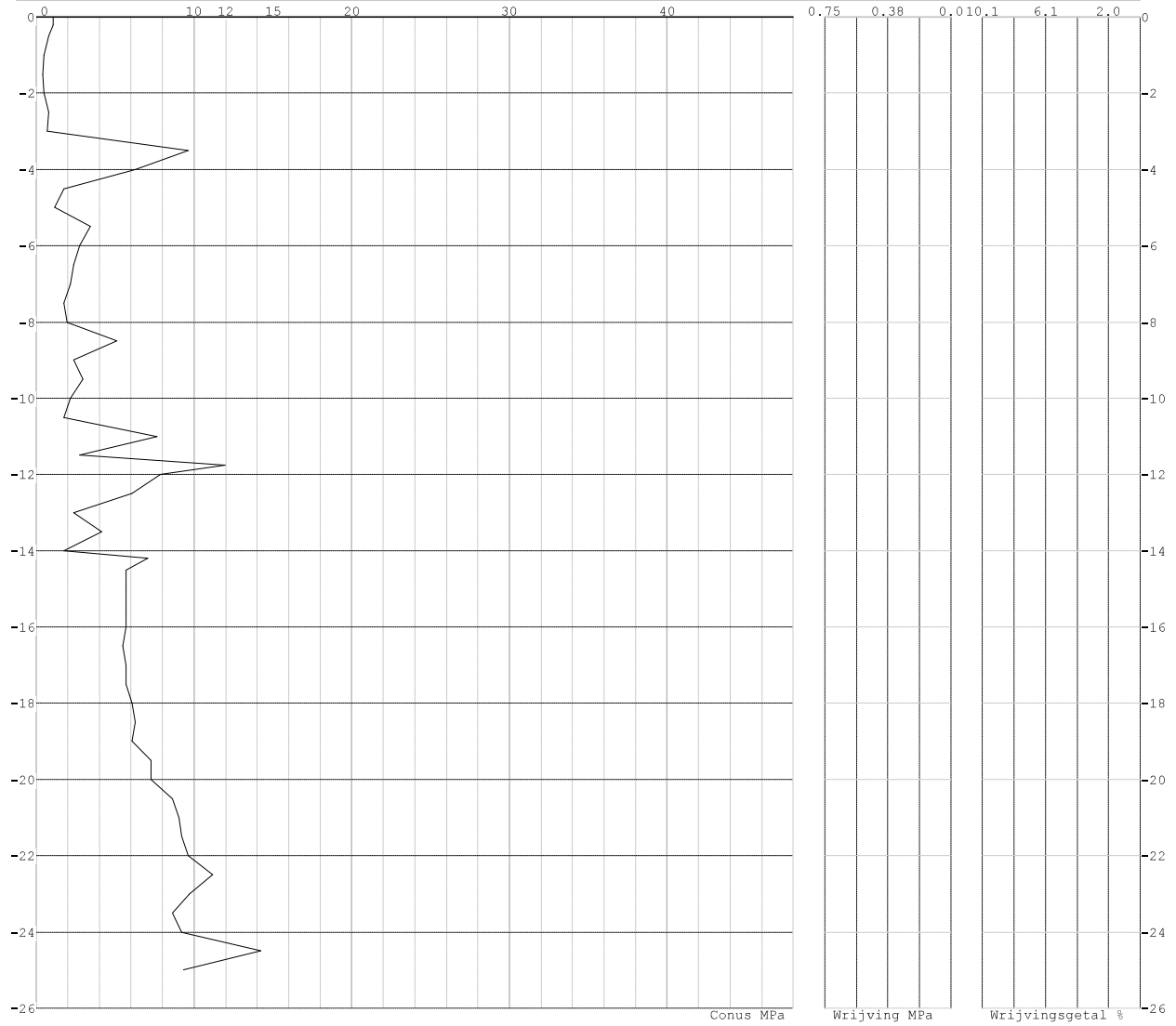


Project : D1.3 ZWO380 Bestaande overgangsmasten  
Onderdeel : GT-RLl overgangsmasten druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: M68-oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : 0.00 Bodemprofiel: M68-oud  
Traject negatieve kleeft : 0.00 tot -2.99 [m]  
Traject positieve kleeft : -3.00 tot -25.00 [m]

**SONDERINGSGEGEVENS GRAFIEK: M68-oud**

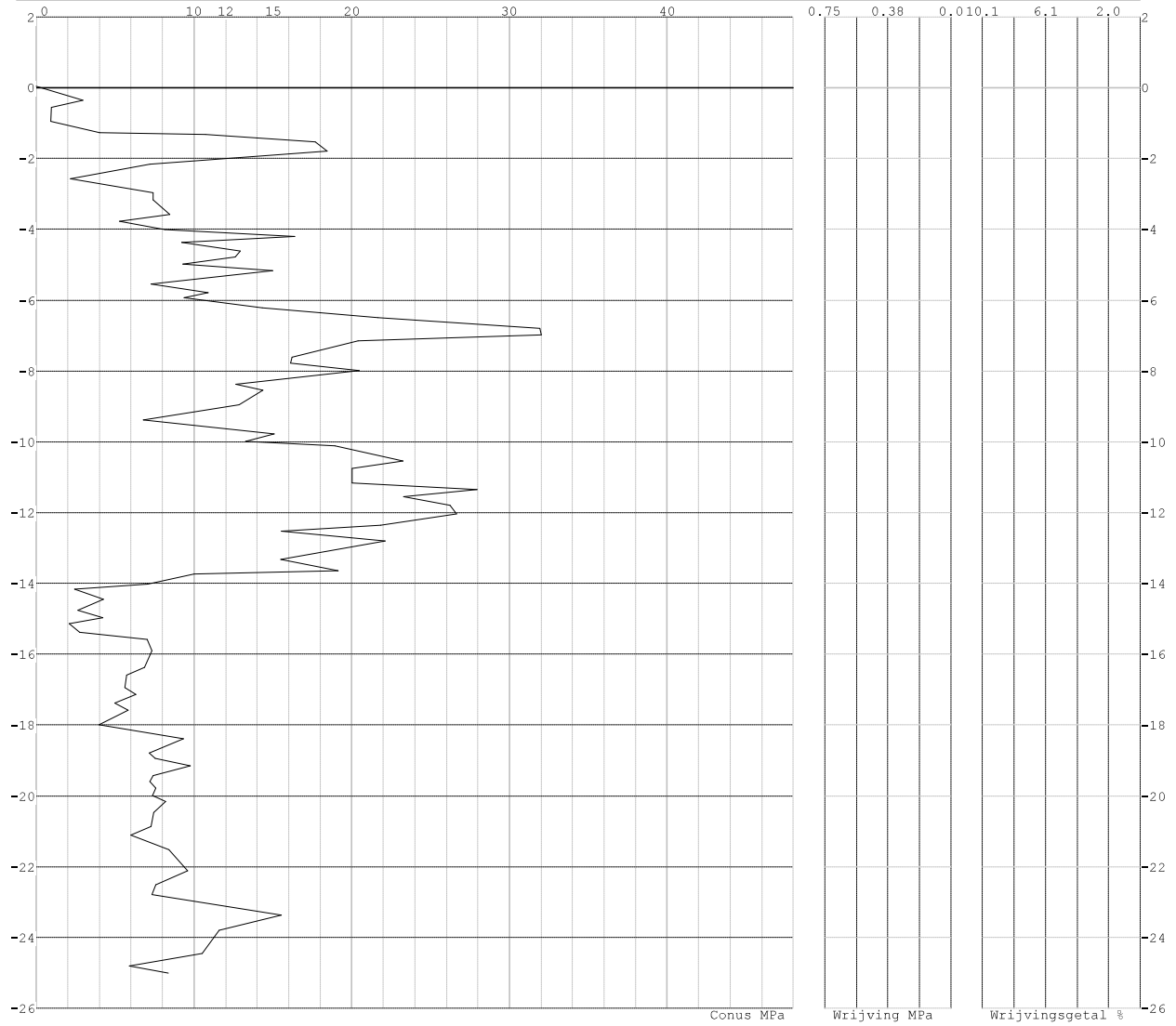


Project : D1.3 ZWO380 Bestaande overgangsmasten  
Onderdeel : GT-RLl overgangsmasten druk en trek

**SONDERINGSGEGEVENS ALGEMEEN: 78-oud**

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.  
Hoogte maaiveld [m] : 0.04 Bodemprofiel: 78-oud  
Traject negatieve kleeft : 0.04 tot 0.04 [m]  
Traject positieve kleeft : 0.03 tot -25.01 [m]

**SONDERINGSGEGEVENS GRAFIEK: 78-oud**



Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLI overgangsmasten druk en trek

**REKENGEGEVENS Mast 16 druk**

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : M16-Oud

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(gem)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{f,ok}$  : 1.0  
 $R_{d,calc,max;1}$  begrenzen op  $0.75 * R_{d,calc,max;1}$  : NEE  
 UGT draagvermogen zonder negatieve kleef : NEE

Paal : RP-53-124 met grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -18.85  
 $E_{d;1}$  [kN] : 0.00  $E_{d;2}$  [kN] : 0.00  
 $s_{req;1}$  [m] : 0.15  $s_{req;2}$  [m] : 0.05  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLl overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 16 druk (n=1)

#### Uitgangspunten

- paal : RP-53-124 met grout  
 - paaltype : Stalen profiel (geheid, grout)  
 - schachtafmeting : 796 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{3(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                     |                     |                   |                     | Rekenwaarden            |  |
|-----------|-------------------|--------|----------------------|---------------------|---------------------|-------------------|---------------------|-------------------------|--|
|           | niveau            | niveau | $R_{b,cal}$<br>[kN]  | $R_{b,cal}$<br>[kN] | $R_{c,cal}$<br>[kN] | $R_{c;d}$<br>[kN] | $F_{bkk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |  |
| M16-Oud   | 0.00              | -18.85 | 3507.4               | 4498.1              | 8005.4              | 4799.4            | -5.2                | 4794.3                  |  |

### REKENGEGEVENS Mast 68 druk

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : M68-oud

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{3(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{3(geom)}$  : 1.39 (handmatig)  
 Factor  $\xi_{3(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{sink}$  : 1.0  
 $R_{b,cal,max;i}$  begrenzen op  $0.75 * R_{b,cal,max;i}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : RP-53-124 met grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -19.85  
 $E_{d;1}$  [kN] : 0.00  $E_{d;2}$  [kN] : 0.00  
 $s_{req;1}$  [m] : 0.15  $s_{req;2}$  [m] : 0.05  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLI overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 68 druk (n=1)

#### Uitgangspunten

- paal : RP-53-124 met grout  
 - paaltype : Stalen profiel (geheid, grout)  
 - schachtafmeting : 796 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{3(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                      |                      |                   |                     |                         |
|-----------|-------------------|--------|----------------------|----------------------|----------------------|-------------------|---------------------|-------------------------|
|           | niveau            | niveau | $R_{b,calc}$<br>[kN] | $R_{b,calc}$<br>[kN] | $R_{b,calc}$<br>[kN] | $R_{b,d}$<br>[kN] | $F_{bkk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| M68-oud   | 0.00              | -19.85 | 3272.8               | 2415.6               | 5688.3               | 3410.3            | -43.5               | 3366.8                  |

### REKENGEGEVENS Mast 78 druk

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 78-oud

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{3(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{3(geom)}$  : 1.39 (handmatig)  
 Factor  $\xi_{3(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{sink}$  : 1.0  
 $R_{b,calc,max;i}$  begrenzen op  $0.75 * R_{b,calc,max;i}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : RP-53-124 met grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -12.85  
 $E_{d;1}$  [kN] : 0.00  $E_{d;2}$  [kN] : 0.00  
 $s_{req;1}$  [m] : 0.15  $s_{req;2}$  [m] : 0.05  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLI overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 78 druk (n=1)

#### Uitgangspunten

- paal : RP-53-124 met grout  
 - paaltype : Stalen profiel (geheid, grout)  
 - schachtafmeting : 796 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_c$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{3(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                     |                     |                   |                     | Rekenwaarden            |  |
|-----------|-------------------|--------|----------------------|---------------------|---------------------|-------------------|---------------------|-------------------------|--|
|           | niveau            | niveau | $R_{b,cal}$<br>[kN]  | $R_{b,cal}$<br>[kN] | $R_{c,cal}$<br>[kN] | $R_{c;d}$<br>[kN] | $F_{bkk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |  |
| 78-oud    | 0.04              | -12.85 | 1936.2               | 4743.4              | 6679.5              | 4004.5            | 0.0                 | 4004.5                  |  |

### REKENGEGEVENS Mast 26 druk

Berekening : Controlerend  
 Rekenmethode : Drukpalen volgens NEN-EN 1997-1, art. 7.6.2  
 Sondering(en) : 26-oud

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{3(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{3(geom)}$  : 1.39 (handmatig)  
 Factor  $\xi_{3(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.20  
 $\gamma_{sink}$  : 1.0  
 $R_{b,cal,max;i}$  begrenzen op  $0.75 * R_{b,cal,max;i}$  : NEE  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : RP-53-124 zonder grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -15.35  
 $E_{d;1}$  [kN] : 0.00  $E_{d;2}$  [kN] : 0.00  
 $s_{req;1}$  [m] : 0.15  $s_{req;2}$  [m] : 0.05  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLl overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 26 druk (n=1)

#### Uitgangspunten

- paal : RP-53-124 zonder grout  
 - paaltype : Stalen buispaal (gesloten)  
 - schachtafmeting : 579 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.010 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                     |                     |                   |                    |                         |
|-----------|-------------------|--------|----------------------|---------------------|---------------------|-------------------|--------------------|-------------------------|
|           | niveau            | niveau | $R_{e,cal}$<br>[kN]  | $R_{g,cal}$<br>[kN] | $R_{c,cal}$<br>[kN] | $R_{e;d}$<br>[kN] | $F_{nk;d}$<br>[kN] | $R_{c,netto;d}$<br>[kN] |
| 26-oud    | 0.04              | -15.35 | 1638.0               | 1778.1              | 3416.1              | 2048.0            | -36.1              | 2011.9                  |

### REKENGEGEVENS Mast 16 HC+0 trek

Berekening : Controlerend  
 Rekenmethode : Trekpalen volgens NEN-EN 1997-1, art. 7.6.3  
 Sondering(en) : M16-Oud  
 Let op: trekcapaciteit t.p.v. negatief kleeftraject is meegerekend.

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(geom)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.35  
 $\gamma_{m;varejige}$  : 1.25  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : RP-53-124 met grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -18.85  
 $E_{d;1}$  [kN] : 0.00  $E_{d;2}$  [kN] : 0.00  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00



Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLl overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 16 HC+0 trek (n=1)

#### Uitgangspunten

- paal : RP-53-124 met grout  
 - paaltype : Stalen profiel (geheid, grout)  
 - schachtafmeting : 796 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                   |                         |
|-----------|-------------------|--------|----------------------|-------------------|-------------------------|
|           | niveau            | niveau | $R_{t,calc}$<br>[kN] | $R_{t,d}$<br>[kN] | $R_{t,netto,d}$<br>[kN] |
| M16-Oud   | 0.00              | -18.85 | 1934.9               | 1934.9            | 1934.9                  |

### REKENGEDEEVENS Mast 68 HB+0 trek

Berekening : Controlerend  
 Rekenmethode : Trekpalen volgens NEN-EN 1997-1, art. 7.6.3  
 Sondering(en) : M68-oud  
 Let op: trekcapaciteit t.p.v. negatief kleefttraject is meegerekend.

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(geom)}$  : 1.39 (handmatig)  
 Factor  $\xi_{d(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.35  
 $\gamma_{m,drag}$  : 1.25  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : RP-53-124 met grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -19.85  
 $E_{d,1}$  [kN] : 0.00  $E_{d,2}$  [kN] : 0.00  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLl overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 68 HB+0 trek (n=1)

#### Uitgangspunten

- paal : RP-53-124 met grout  
 - paaltype : Stalen profiel (geheid, grout)  
 - schachtafmeting : 796 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                   |                         |
|-----------|-------------------|--------|----------------------|-------------------|-------------------------|
|           | niveau            | niveau | $R_{t,calc}$<br>[kN] | $R_{t,d}$<br>[kN] | $R_{t,netto,d}$<br>[kN] |
| M68-oud   | 0.00              | -19.85 | 1126.6               | 1126.6            | 1126.6                  |

### REKENGEDEEVENS Mast 78 HB+0 trek

Berekening : Controlerend  
 Rekenmethode : Trekpalen volgens NEN-EN 1997-1, art. 7.6.3  
 Sondering(en) : 78-oud  
 Let op: trekcapaciteit t.p.v. negatief kleeftraject is meegerekend.

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(geom)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.35  
 $\gamma_{m,drag}$  : 1.25  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : RP-53-124 met grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -12.85  
 $E_{d,1}$  [kN] : 0.00  $E_{d,2}$  [kN] : 0.00  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLl overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 78 HB+0 trek (n=1)

#### Uitgangspunten

- paal : RP-53-124 met grout  
 - paaltype : Stalen profiel (geheid, grout)  
 - schachtafmeting : 796 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezuikdraagvermogen  |                   |                         |
|-----------|-------------------|--------|----------------------|-------------------|-------------------------|
|           | niveau            | niveau | $R_{t,calc}$<br>[kN] | $R_{t,d}$<br>[kN] | $R_{t,netto,d}$<br>[kN] |
| 78-oud    | 0.04              | -12.85 | 1896.8               | 1896.8            | 1896.8                  |

### REKENGEDEEVENS Mast 26 HS+0 trek

Berekening : Controlerend  
 Rekenmethode : Trekpalen volgens NEN-EN 1997-1, art. 7.6.3  
 Sondering(en) : 26-oud  
 Let op: trekcapaciteit t.p.v. negatief kleefttraject is meegerekend.

Stijf bouwwerk : NEE  
 Paalgroep : NEE  
 Aantal sonderingen : 1  
 Factor  $\xi_{s(n=1)}$  : 1.39 (handmatig)  
 Factor  $\xi_{s(geom)}$  : 1.39 (handmatig)  
 Factor  $\xi_{d(min)}$  : 1.39 (handmatig)  
 Weerstandsfactor  $\gamma_R$  : 1.35  
 $\gamma_{m,drag}$  : 1.50  
 UGT draagvermogen zonder negatieve kleeft : NEE

Paal : RP-53-124 zonder grout  
 Niveau paalkop [m] : N.A.P. 0.65  
 Paalpuntniveau : N.A.P. -15.35  
 $E_{d,1}$  [kN] : 0.00  $E_{d,2}$  [kN] : 0.00  
 Bovenbel. [kN/m<sup>2</sup>] : 0.00

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLl overgangsmasten druk en trek

### SAMENVATTINGSTABEL Mast 26 HS+0 trek (n=1)

#### Uitgangspunten

- paal : RP-53-124 zonder grout  
 - paaltype : Stalen buispaal (gesloten)  
 - schachtafmeting : 579 mm  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.0070 (zandlagen; voor kleilagen zie tabel 7.d)  
 Correlatiefactor  $\xi_{s(n=1)}$  : 1.39

Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | Bezwijkdraagvermogen |                   |                         |
|-----------|-------------------|--------|----------------------|-------------------|-------------------------|
|           | niveau            | niveau | $R_{t,calc}$<br>[kN] | $R_{t,d}$<br>[kN] | $R_{t,netto,d}$<br>[kN] |
| 26-oud    | 0.04              | -15.35 | 553.1                | 553.1             | 553.1                   |

#### PAALGEGEVENS RP-53-124 met grout

Type : Stalen profiel (geheid, grout)  
 Wijze van installeren : Heien  
 Diameter [m] : 0.796  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.014 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.0120 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 0.75  
 Groutomhulling : JA

#### PAALGEGEVENS RP-53-124 zonder grout

Type : Stalen buispaal (gesloten)  
 Wijze van installeren : Heien  
 Diameter [m] : 0.579  
 Elasticiteitsmodulus [N/mm<sup>2</sup>] : 20000  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.010 (zandlagen; voor kleilagen zie tabel 7.d)  
 Factor  $\alpha_s$  (tabel 7.c EC 7.1) : 0.0070 (zandlagen; voor kleilagen zie tabel 7.d)  
 Paalklassefactor  $\alpha_p$  : 1.00  
 Paalvoetvormfactor  $\beta$  : 1.00  
 Type lastzakingsdiagram : Grondverdringende paal  
 Verm.factor \*  $\varphi'_{j,k}$  : 0.75  
 Groutomhulling : NEE

Project : D1.3 ZWO380 Bestaande overgangsmasten  
 Onderdeel : GT-RLI overgangsmasten druk en trek

#### OVERZICHT NETTO DRAAGVERMOGEN DRUKPALEN

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | $R_{d, netto;d}$ [kN] |           |           |           |
|-----------|-------------------|--------|-----------------------|-----------|-----------|-----------|
|           | niveau            | niveau | Mast 16 d             | Mast 68 d | Mast 78 d | Mast 26 d |
| M16-Oud   | 0.00              | -18.85 | 4794                  |           |           |           |
| 26-oud    | 0.04              | -15.35 |                       |           |           | 2011      |
| M68-oud   | 0.00              | -19.85 |                       | 3366      |           |           |
| 78-oud    | 0.04              | -12.85 |                       |           | 4004      |           |

#### OVERZICHT NETTO DRAAGVERMOGEN TREKPALEN (n=1)

Netto paal draagvermogen(s) zijn naar beneden toe afgerond op: 1.0 kN nauwkeurig  
 Alle niveaus/hoogtes/peilmaten zijn t.o.v.: N.A.P.

| sondering | maaiveld paalpunt |        | $R_{d, netto;d}$ [kN] |           |           |           |
|-----------|-------------------|--------|-----------------------|-----------|-----------|-----------|
|           | niveau            | niveau | Mast 16 H             | Mast 68 H | Mast 78 H | Mast 26 H |
| M16-Oud   | 0.00              | -18.85 | 1934                  |           |           |           |
| 26-oud    | 0.04              | -15.35 |                       |           |           | 553       |
| M68-oud   | 0.00              | -19.85 |                       | 1126      |           |           |
| 78-oud    | 0.04              | -12.85 |                       |           | 1896      |           |

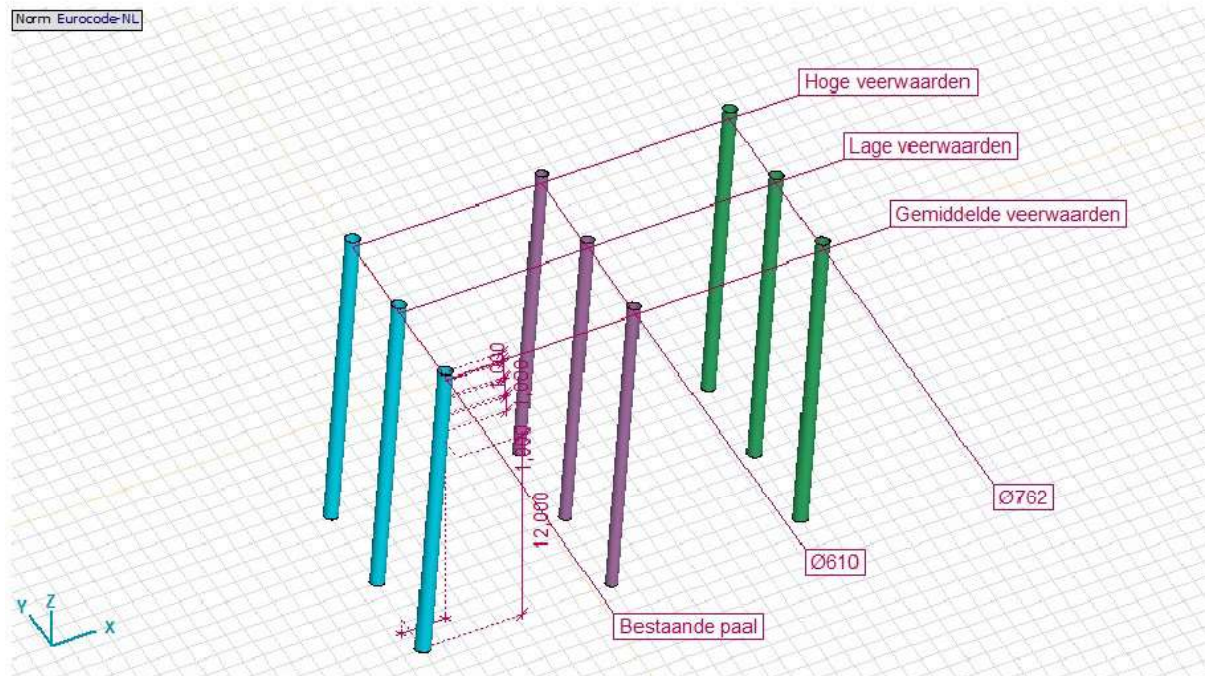
## APPENDIX E

### Berekening horizontale afdracht

In deze Appendix wordt de horizontale krachtsafdracht van de enkelpaalsfundering aangetoond.

#### Schematisering

De constructie wordt geschematiseerd als een elastisch ondersteunde ligger met begrensde beddingweerstand tot de passieve gronddruk met dwarsbelasting op de paalkop.



**Figuur 13 Rekenmodel**

In hoofdstuk 2.8.6 zijn de uitgangspunten gegeven voor de beddingen tegen de palen. Er is in het kader van de berekening voldoende nauwkeurigheid als onderscheid wordt gemaakt in beddingwaarde voor drie grondsoorten. Er zijn drie berekeningen uitgevoerd: één met gemiddelde veerwaarde, één met lage veerwaarde ( $k$  gedeeld door  $\sqrt{2}$ ) en één met hoge veerwaarde ( $k$  maal  $\sqrt{2}$ ).

**Tabel 18 Beddingwaarden**

| Paal      | Grond | $k_h$<br>[kN/m <sup>3</sup> ] | schelp<br>[-] | Diameter<br>[m] | Gem.<br>[kN/m] | Laag<br>[kN/m] | Hoog<br>[kN/m] |
|-----------|-------|-------------------------------|---------------|-----------------|----------------|----------------|----------------|
| RP-53-124 | Veen  | 1500                          | 1,2           | 0,796           | 1433           | 1013           | 2026           |
|           | Klei  | 3000                          | 1,3           | 0,796           | 3104           | 2195           | 4390           |
|           | Zand  | 15000                         | 2             | 0,796           | 23880          | 16886          | 33771          |
| Ø610/850  | Veen  | 1500                          | 1,2           | 0,85            | 1530           | 1082           | 2164           |
|           | Klei  | 3000                          | 1,3           | 0,85            | 3315           | 2344           | 4688           |
|           | Zand  | 15000                         | 2             | 0,85            | 25500          | 18031          | 36062          |
| Ø762/950  | Veen  | 1500                          | 1,2           | 0,95            | 1710           | 1209           | 2418           |
|           | Klei  | 3000                          | 1,3           | 0,95            | 3705           | 2620           | 5240           |
|           | Zand  | 15000                         | 2             | 0,95            | 28500          | 20153          | 40305          |

De berekening voor de horizontale krachtsafdracht is uitgevoerd uitgaande van een globaal beeld van de bodemgelaagdheid van de sonderingen, zie Tabel 19.

**Tabel 19 Gehanteerd bodemprofiel – nieuwe masten**

| Van<br>[m] | Tot<br>[m] | Omschrijving |
|------------|------------|--------------|
| 0,0        | -3,0       | Klei         |
| -3,0       | dieper     | Zand         |

Voor de bestaande palen wordt uitgegaan van de sondering bij de maatgevende mast (mast 16), zie Tabel 20.

**Tabel 20 Gehanteerd bodemprofiel – bestaande masten**

| Van<br>[m] | Tot<br>[m] | Omschrijving |
|------------|------------|--------------|
| 0,0        | -1,0       | Klei         |
| -1,0       | -2,0       | Zand         |
| -2,0       | -3,0       | Klei         |
| -3,0       | dieper     | Zand         |

De maximale weerstand die in rekening mag worden gebracht kan niet groter zijn dan de passieve gronddruk. Over de bovenste meters waar de grootste verplaatsingen optreden, is vanuit die overweging de maximale reactie van de lijnondersteuning aan de paal in de berekening begrensd. Er is uitgegaan van een volumiek gewicht van 17 kN/m<sup>3</sup>, een grondwaterstand van 0,5 m beneden maaiveld.

De methode van Bijlage C van NEN 1997-1 is gevolgd. De factor voor passieve gronddruk is voor klei of veen op 2 aangehouden, voor zand op 3. Onderstaand zijn de maximale grondweerstanden samengevat die zijn toegekend aan de elastische ondersteuning van de palen.

**Tabel 21 Begrenzing passieve gronddruk**

| Paal      | Grond | Niveau<br>[m] | p<br>[kN/m <sup>3</sup> ] | k <sub>pa</sub><br>[kN/m <sup>3</sup> ] | schelp<br>[-] | Diameter<br>[m] | Max. druk<br>[kN] | Max. druk<br>[kN] 50% |
|-----------|-------|---------------|---------------------------|---|---------------|-----------------|-------------------|-----------------------|
| RP-53-124 | Klei  | 0             | 0                         |   |               |                 |                   |                       |
|           |       | -1            | 12                        | 2                                       | 1,3           | 0,796           | 12,4              | 6,2                   |
|           | Zand  | -2            | 19                        | 3                                       | 2             | 0,796           | 74,0              | 37,0                  |
|           |       | -3            | 26                        | 2                                       | 1,3           | 0,796           | 46,6              | 23,3                  |
|           | Zand  | -4            | 34                        | 3                                       | 2             | 0,796           | 143,3             | 143,3                 |
|           |       | -5            | 42                        | 3                                       | 2             | 0,796           | 181,5             | 181,5                 |
| Ø610/850  | Klei  | 0             | 0                         |   |               |                 |                   |                       |
|           |       | -1            | 12                        | 2                                       | 1,3           | 0,85            | 13,3              | 0                     |
|           |       | -2            | 19                        | 2                                       | 1,3           | 0,85            | 34,3              | 17,1                  |
|           | Zand  | -3            | 26                        | 2                                       | 1,3           | 0,85            | 49,7              | 24,9                  |
|           |       | -4            | 34                        | 3                                       | 2             | 0,85            | 153,0             | 153,0                 |
|           |       | -5            | 42                        | 3                                       | 2             | 0,85            | 193,8             | 193,8                 |
| Ø762/950  | Klei  | 0             | 0                         |   |               |                 |                   |                       |
|           |       | -1            | 12                        | 2                                       | 1,3           | 0,95            | 14,8              | 0                     |
|           |       | -2            | 19                        | 2                                       | 1,3           | 0,95            | 38,3              | 19,1                  |
|           | Zand  | -3            | 26                        | 2                                       | 1,3           | 0,95            | 55,6              | 27,8                  |
|           |       | -4            | 34                        | 3                                       | 2             | 0,95            | 171,0             | 171,0                 |
|           |       | -5            | 42                        | 3                                       | 2             | 0,95            | 216,6             | 216,6                 |

## Belasting

De belastingen zijn ontleend aan PLS-TOWER en opgenomen in Appendix A. De belastingen in de lokale richting van de paal zijn ingevoerd. Per paaltype is er een maatgevend masttype aangehouden:

- Bestaande paal HC+0 (16)
- Ø610/850 S+0/n
- Ø762/950 S+32/n (trek en druk) & HC+0/n (torsie)

De belastingen zijn opgenomen in Tabel 22 tot en met Tabel 24. Alle belastinggevallen, die zijn weergegeven in de tabellen, zijn ingevoerd in AxisVM.

**Tabel 22 Belastingen HC+0(16)**

| Belasting         | Combinatie                   | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>n</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | SPLS 3_120.38 Ba All Cts     | -233                   | -250                   | -1458                  | -12                    | -342                   | 19                         | -1497                      |
| Max. trek         | SPLS 3_0,9_120.38 Ba All Cts | -203                   | -189                   | 1171                   | -10                    | 277                    | -19                        | 1203                       |
| Max. pos. torsie  | SPLS 6a_90 Ba Ct2 Ah Ct2     | -34                    | -160                   | -371                   | 137                    | -89                    | 7                          | -381                       |
| Max. neg. torsie  | SPLS 6a_90 Ba Ct1 Ah Ct1     | -91                    | -116                   | 57                     | -147                   | 18                     | -5                         | 60                         |
| Comb. trek+torsie | SPLS 6a_90 Ba Ct1 Ah Ct1     | -247                   | -40                    | 854                    | -146                   | 204                    | -15                        | 878                        |

**Tabel 23 Belastingen S+0/n**

| Belasting         | Combinatie         | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>n</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|--------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | ULS 1a_45          | -177                   | -167                   | -984                   | 7                      | -243                   | 43                         | -1013                      |
| Max. trek         | ULS 1a_0,9_0,9_135 | 139                    | -128                   | 774                    | 7                      | 189                    | -31                        | 796                        |
| Max. pos. torsie  | ULS 5a Ba 21       | 32                     | -27                    | -2                     | 42                     | -4                     | 3                          | -3                         |
| Max. neg. torsie  | ULS 5a Ah 21       | -32                    | -27                    | -2                     | -42                    | -4                     | 3                          | -3                         |
| Comb. trek+torsie | ULS 1a 0,9 0,9 90  | 139                    | -91                    | 684                    | 34                     | 162                    | -23                        | 703                        |

**Tabel 24 Belastingen S+32/n (trek en druk) & HC+0/n (torsie)**

| Belasting         | Combinatie                     | R <sub>x</sub><br>[kN] | R <sub>y</sub><br>[kN] | R <sub>z</sub><br>[kN] | R <sub>n</sub><br>[kN] | R <sub>ξ</sub><br>[kN] | R <sub>ξ,lok</sub><br>[kN] | R <sub>z,lok</sub><br>[kN] |
|-------------------|--------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|----------------------------|----------------------------|
| Max. druk         | ULS 1a_45                      | -361                   | -353                   | -2164                  | 5                      | -505                   | -21                        | -2222                      |
| Max. trek         | ULS 1a_0,9_0,9_135             | 281                    | -272                   | 1699                   | 6                      | 391                    | 22                         | 1743                       |
| Max. pos. torsie  | SPLS 3_0,9_110 Ah Ct1_(140 gr) | 106                    | -128                   | 58                     | 166                    | 15                     | -3                         | 60                         |
| Max. neg. torsie  | SPLS 3_0,9_70 Ba Ct1_(140 gr)  | -106                   | -128                   | 58                     | -166                   | 15                     | -3                         | 60                         |
| Comb. trek+torsie | SPLS 3_0,9_90 Ah Ct1           | 301                    | -103                   | 1203                   | 140                    | 286                    | -20                        | 1237                       |

## Toetsing

De volgende aspecten zijn getoetst:

- Horizontale verplaatsing < 1/400 x b
- Buigspanning in de paal < f<sub>y</sub>

De gronddruk wordt niet getoetst, deze is immers reeds begrensd.

Verplaatsingseisen worden gesteld voor de karakteristieke belastingen, zonder belastingfactoren. In de berekening is gewerkt met rekenwaarden. Als de berekening wordt uitgevoerd met belastingfactor (ULS of SpLS) moet om terug te rekenen worden gedeeld door de belastingfactor. De methode wordt hier toegelicht.

Er wordt gerekend met een verhouding ULS/SLS van 1,35. Voor de load case ULS-5a met maximale torsiebelasting wordt een factor 1,0 gerekend aangezien de belastingfactor in dat geval 1,0 bedraagt.

Onder de belasting door torsie verplaatsen beide poten in dezelfde richting, theoretisch wordt dan altijd voldaan aan de eis. Gekozen is om ook hier het uitgangspunt te hanteren van 1/400 x b. In de overige load cases met maximale wind



(ULS-1a) kunnen beide poten tegengesteld vervormen. De toelaatbare vervorming is in die gevallen 50% van de toelaatbare waarde. De eisen zijn in Tabel 25 samengevat.

**Tabel 25 Toelaatbare horizontale belasting**

| Type | Belasting | b<br>[mm] | eis    |      | Factor 1 | Factor 2 | Eis<br>[mm] |
|------|-----------|-----------|--------|------|----------|----------|-------------|
| S+0  | Extreem   | 9000      | 0,0025 | 22,5 | 1,35     | 0,5      | 15,2        |
|      | Torsie    | 9000      | 0,0025 | 22,5 | 1        | 1        | 22,5        |
| HC+0 | Extreem   | 11000     | 0,0025 | 27,5 | 1,35     | 0,5      | 18,6        |
|      | Torsie    | 11000     | 0,0025 | 27,5 | 1        | 1        | 27,5        |

## Resultaten

Zie berekening AxisVM:

**Tabel 26 Resultaten Ø610/850**

|                         | Berekend | Toelaatbaar           | Unity-check |
|-------------------------|----------|-----------------------|-------------|
| Spanningscheck buispaal | 91       | 355 N/mm <sup>2</sup> | 0,26 OK     |
| Verplaatsing Extreem    | 9,5      | 15,2 mm               | 0,63 OK     |
| Verplaatsing Torsie     | 9,4      | 22,5 mm               | 0,42 OK     |

**Tabel 27 Resultaten Ø762/950**

|                         | Berekend | Toelaatbaar           | Unity-check |
|-------------------------|----------|-----------------------|-------------|
| Spanningscheck buispaal | 130      | 355 N/mm <sup>2</sup> | 0,37 OK     |
| Verplaatsing Extreem    | 8,7      | 18,6 mm               | 0,47 OK     |
| Verplaatsing Torsie     | 24,3     | 27,5 mm               | 0,88 OK     |

Conclusie: de enkelpaalsfundering voldoet.

### **Bestaande palen**

De bestaande palen worden enkel op sterkte getoetst. De maximale optredende spanning is 195 MPa en voldoet aan de vloeispanning van 235 MPa (UC = 0,83). Deze spanning is wel zonder staalafname. De maximale afname die nog door de doorsnede opgenomen kan worden is ca. (12 mm – (0,83 · 12mm =)) 2 mm. Dit is minder dan de omschreven waarde van 3,1 mm in hoofdstuk 2.8.5. Het lijkt echter niet aannemelijk dat de afname werkelijk 3,1 mm zal kunnen worden ter plaatse van het maximale moment, omdat:

- De stalen paal is omhuld door een groutschil en daardoor grotendeels beschermd zal zijn;
- De grondlaag op deze diepte waarschijnlijk lijkt niet vervuild of zuur zal zijn, waardoor de afname maximaal 1,2 mm in 100 jaar is.

Om deze reden zal de bestaande paal naar verwachting voldoen. Na uitvoeren van het bodemonderzoek moet bevestigd worden dat er daadwerkelijk geen verontreinigde bodem is aangetroffen.

Bijlage: rapport AxisVM

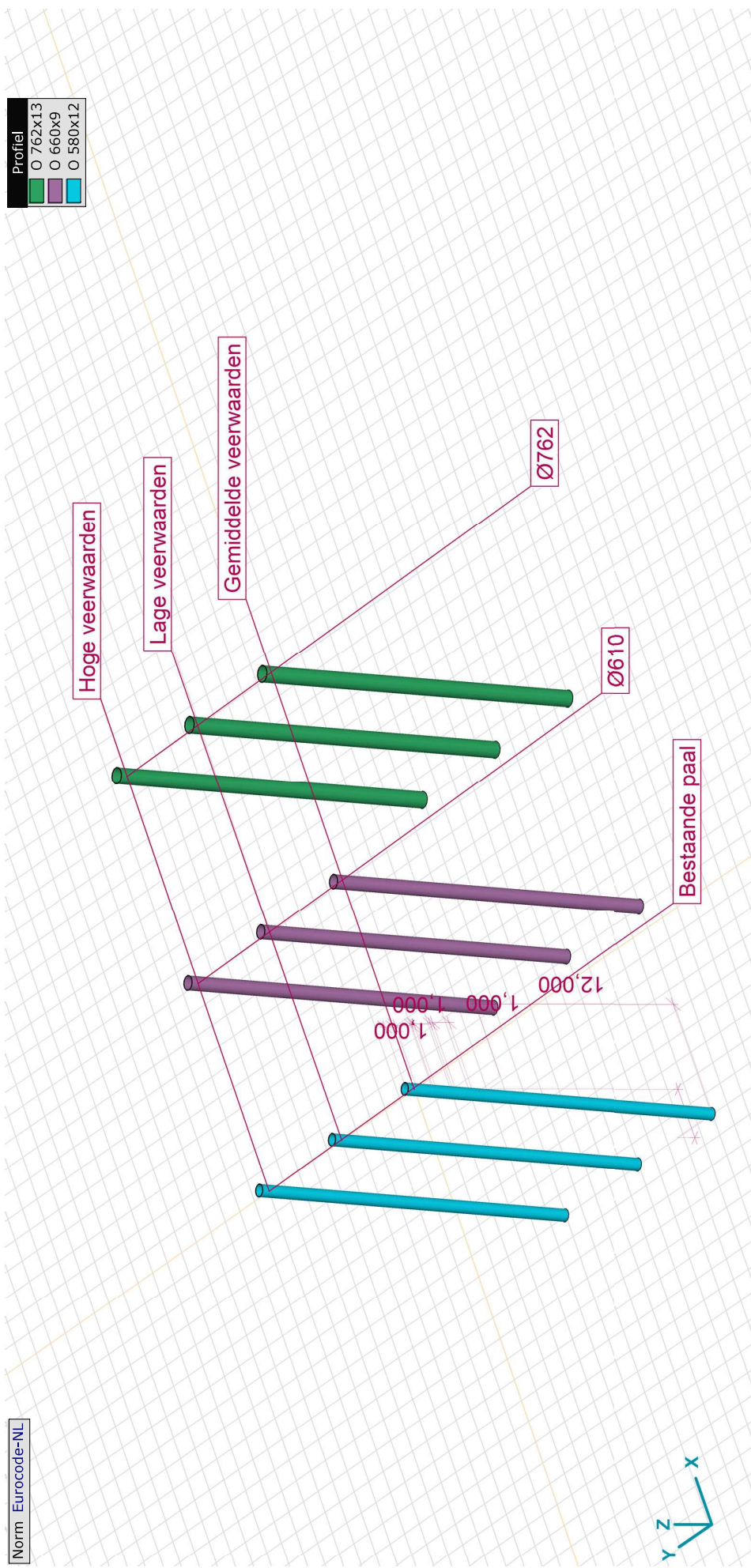
## **Project:**

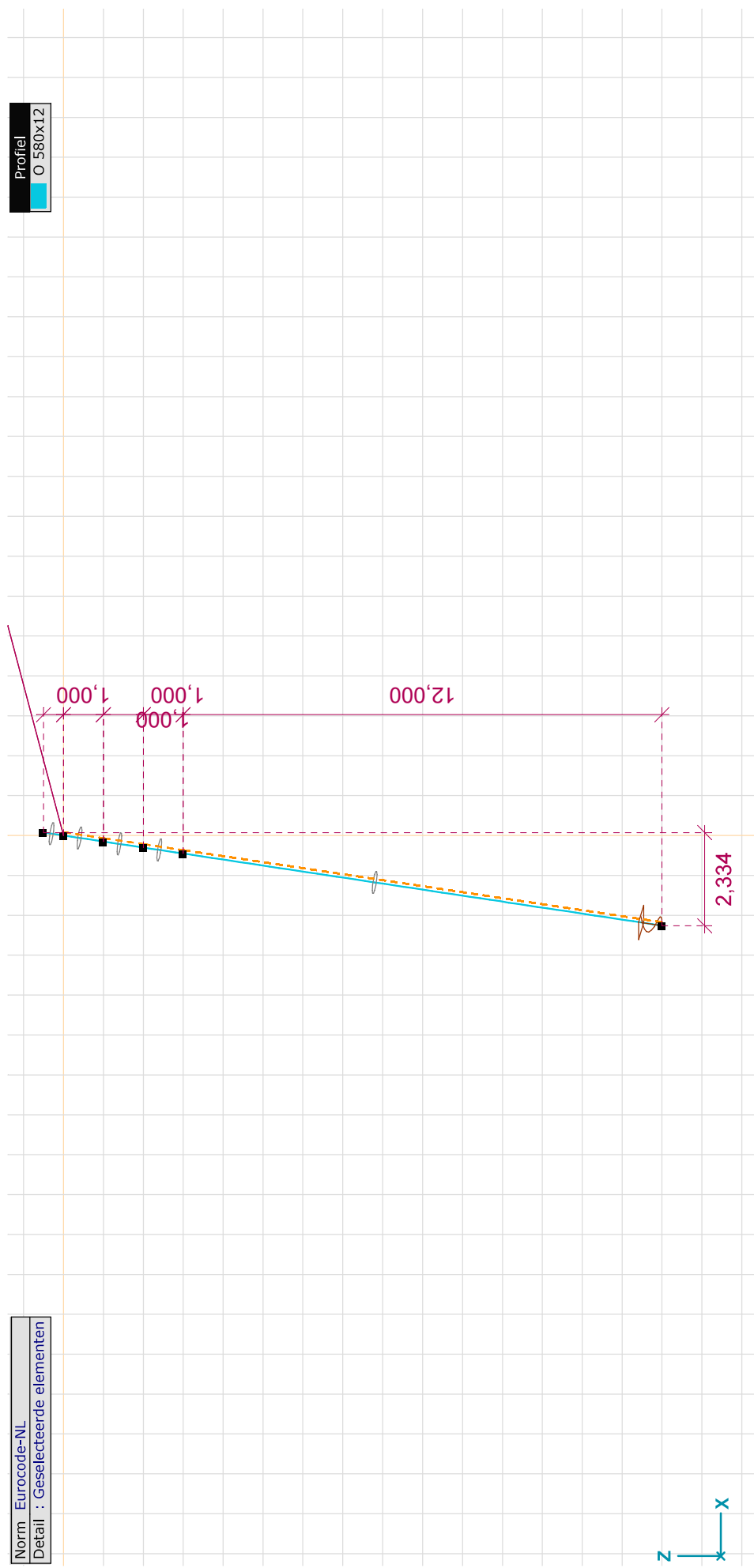
**Constructeur: DNV GL - Energy**

AxisVM X6 R10-hf1 - Geregistreerd aan DNV GL - Energy  
1-paals reconstructie 2-cl.axs

**Rapport**

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| [III], > ~3, Non-lin., Max. Trek [I] (1,000), Onmiddellijke doorbuiging, eR, Lijnen                        | 20     |
| [III], > ~3, Non-lin., Max. Druk [I] (1,000), Onmiddellijke doorbuiging, eR, Lijnen                        | 21     |
| [III], > ~2, Non-lin., Omhullende (Belastinggevallen), Onmiddellijke doorbuiging, eX, Lijnen               | 22     |
| [III], > ~2, Non-lin., Omhullende (Belastinggevallen), Onmiddellijke doorbuiging, eY, Lijnen               | 23     |
| Knoopverplaatsingen [Non-lin., Omhullende (Belastinggevallen)]   | 24     |
| [III], Non-lin., Omhullende (Belastinggevallen), Onmiddellijke doorbuiging, Somminmax, Lijnen (gevuld)     | 25     |
| Staafspanningen [Non-lin., Omhullende (Belastinggevallen)]   | 26     |
| Staafspanningen [Non-lin., Omhullende (Belastinggevallen)]   | 26     |
| Staafspanningen [Non-lin., Omhullende (Belastinggevallen)]   | 27     |
| [III], Non-lin., Omhullende (Belastinggevallen), Onmiddellijke doorbuiging, Ry (lijnopp.), Lijnen (gevuld) | 28     |
| Interne krachten lijnoplegging [Non-lin., Omhullende (Belastinggevallen)]                                  | 29     |
| Interne krachten lijnoplegging [Non-lin., Omhullende (Belastinggevallen)]                                  | 29     |
| Interne krachten lijnoplegging [Non-lin., Omhullende (Belastinggevallen)]                                  | 29     |



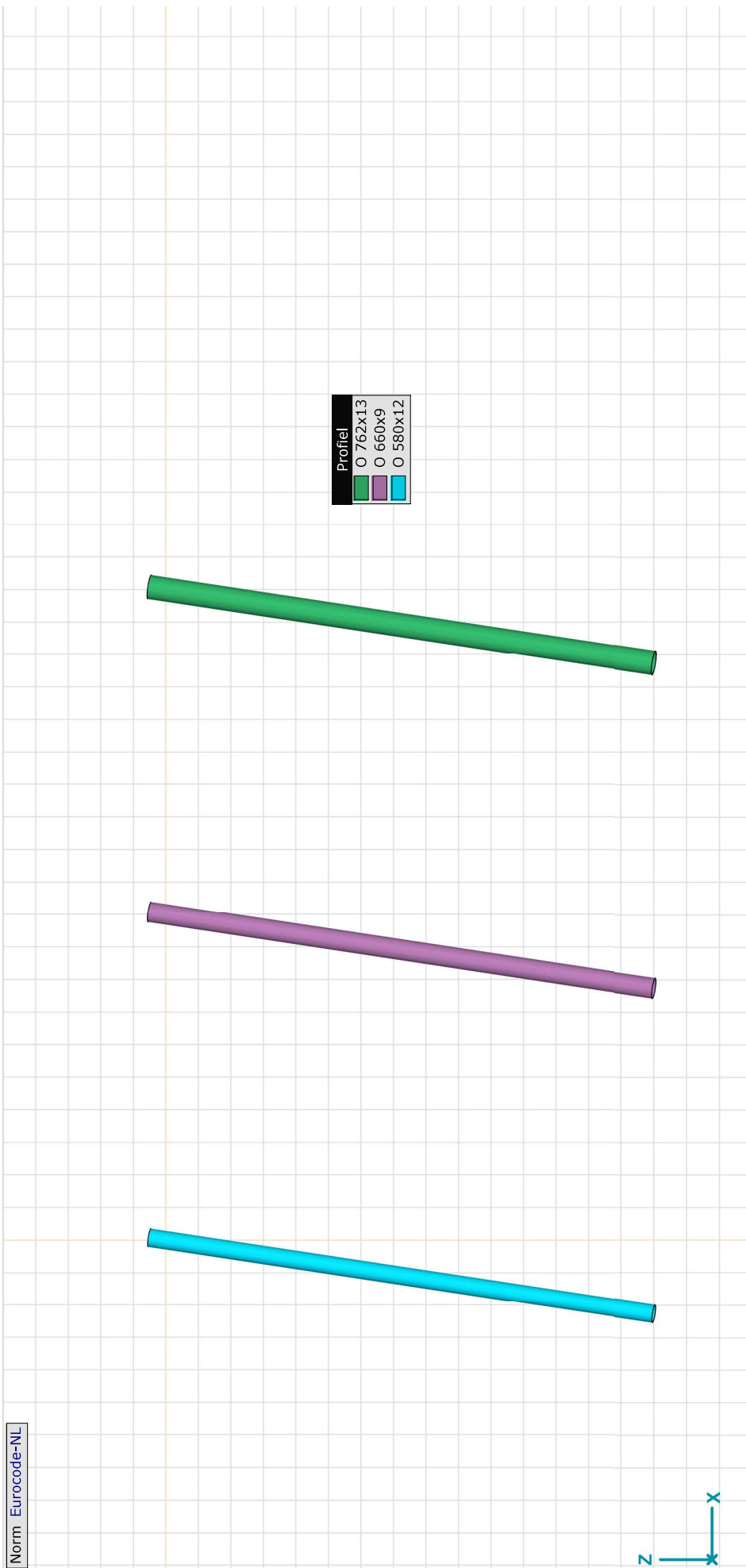


**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

Norm Eurocode-NL



Profielen

**Project:**







Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Materialen**

| Naam    | Type  | Nationale norm | Materiaalnorm | Model   | $E_x$ [N/mm <sup>2</sup> ] | $E_y$ [N/mm <sup>2</sup> ] | $\nu$ | $\alpha_T$ [1/°C] | $\rho$ [kg/m <sup>3</sup> ] | Materiaal kleur   | Contour kleur   | Structuur   | $P_1$                               |
|---------|-------|----------------|---------------|---------|----------------------------|----------------------------|-------|-------------------|-----------------------------|---|---|---|-------------------------------------|
| 1 S 355 | Staal | Eurocode-NL    | 10025-2       | Lineair | 210000                     | 210000                     | 0,30  | 1,2E-5            | 7850                        |  |  |  | $f_y$ [N/mm <sup>2</sup> ] = 355,00 |
| 2 S 235 | Staal | Eurocode-NL    | 10025-2       | Lineair | 210000                     | 210000                     | 0,30  | 1,2E-5            | 7850                        |  |  |  | $f_y$ [N/mm <sup>2</sup> ] = 235,00 |

| Naam    | $P_2$                               | $P_3$                               | $P_4$                               | $P_5$ | $P_6$ | $P_7$ | $P_8$ | $P_9$ | $P_{10}$ | $P_{11}$ | $P_{12}$ | $P_{13}$ | $P_{14}$ |
|---------|-------------------------------------|-------------------------------------|-------------------------------------|-------|-------|-------|-------|-------|----------|----------|----------|----------|----------|
| 1 S 355 | $f_u$ [N/mm <sup>2</sup> ] = 510,00 | $f_y$ [N/mm <sup>2</sup> ] = 335,00 | $f_u$ [N/mm <sup>2</sup> ] = 470,00 |       |       |       |       |       |          |          |          |          |          |
| 2 S 235 | $f_u$ [N/mm <sup>2</sup> ] = 360,00 | $f_y$ [N/mm <sup>2</sup> ] = 215,00 | $f_u$ [N/mm <sup>2</sup> ] = 360,00 |       |       |       |       |       |          |          |          |          |          |

Naam: Materiaalnaam; Type: Type materiaal; Model: Materiaal model;  $E_x$ : Elasticiteitsmodulus in lokale x richting;  $E_y$ : Elasticiteitsmodulus in lokale y richting;  $\nu$ : Poisson's verhouding;  $\alpha_T$ : Warmteuitzettingscoëfficiënt;  $\rho$ : Dichtheid; **Materiaal kleur**: Materiaalkleur; **Contour kleur**: Contourkleur;  $P_1, P_2, P_3, P_4, P_5, P_6, P_7, P_8, P_9, P_{10}, P_{11}, P_{12}, P_{13}, P_{14}$ : Ontwerpparameter;

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**Profielen**

| Naam       | Tekening | Productie | Vorm | h<br>[mm] | b<br>[mm] | tw<br>[mm] | tf<br>[mm] | r <sub>1</sub><br>[mm] | r <sub>2</sub><br>[mm] | r <sub>3</sub><br>[mm] | A <sub>x</sub><br>[mm <sup>2</sup> ] | A <sub>y</sub><br>[mm <sup>2</sup> ] | A <sub>z</sub><br>[mm <sup>2</sup> ] | I <sub>x</sub><br>[mm <sup>4</sup> ] | I <sub>y</sub><br>[mm <sup>4</sup> ] | I <sub>z</sub><br>[mm <sup>4</sup> ] | I <sub>yz</sub><br>[mm <sup>4</sup> ] |
|------------|----------|-----------|------|-----------|-----------|------------|------------|------------------------|------------------------|------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------------------------------|
| 1 O 762x13 |          | Gewalst   | Buis | 762,0     | 762,0     | 12,8       | 12,8       | 0                      | 0                      | 0                      | 30005,34                             | 15009,80                             | 15009,92                             | 4,2E+09                              | 2,1E+09                              | 2,1E+09                              | 0                                     |
| 2 O 660x9  |          | Gewalst   | Buis | 660,0     | 660,0     | 8,8        | 8,8        | 0                      | 0                      | 0                      | 17898,53                             | 8951,80                              | 8951,96                              | 1,9E+09                              | 9,5E+08                              | 9,5E+08                              | 0                                     |
| 3 O 580x12 |          | Gewalst   | Buis | 580,0     | 580,0     | 12,0       | 12,0       | 0                      | 0                      | 0                      | 21408,75                             | 10711,55                             | 10712,40                             | 1,7E+09                              | 8,6E+08                              | 8,6E+08                              | 0                                     |

| Naam       | I <sub>1</sub><br>[mm <sup>4</sup> ] | I <sub>2</sub><br>[mm <sup>4</sup> ] | α<br>[°] | I <sub>ω</sub><br>[mm <sup>6</sup> ] | W <sub>1,elt</sub><br>[mm <sup>3</sup> ] | W <sub>1,el,b</sub><br>[mm <sup>3</sup> ] | W <sub>2,elt</sub><br>[mm <sup>3</sup> ] | W <sub>2,el,b</sub><br>[mm <sup>3</sup> ] | W <sub>1,pl</sub><br>[mm <sup>3</sup> ] | W <sub>2,pl</sub><br>[mm <sup>3</sup> ] | i <sub>y</sub><br>[mm] | i <sub>z</sub><br>[mm] | H <sub>y</sub><br>[mm] | H <sub>z</sub><br>[mm] | y <sub>G</sub><br>[mm] | z <sub>G</sub><br>[mm] |
|------------|--------------------------------------|--------------------------------------|----------|--------------------------------------|--|---|--|---|---|---|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| 1 O 762x13 | 2,1E+09                              | 2,1E+09                              | 0        | 0                                    | 5526812,0                                | 5526812,0                                 | 5526812,0                                | 5526812,0                                 | 7156049,0                               | 7156096,0                               | 264,9                  | 264,9                  | 762,0                  | 762,0                  | 381,0                  | 381,0                  |
| 2 O 660x9  | 9,5E+08                              | 9,5E+08                              | 0        | 0                                    | 2875406,0                                | 2875406,0                                 | 2875406,0                                | 2875406,0                                 | 3710200,0                               | 3710225,0                               | 230,2                  | 230,2                  | 660,0                  | 660,0                  | 330,0                  | 330,0                  |
| 3 O 580x12 | 8,6E+08                              | 8,6E+08                              | 0        | 0                                    | 2977869,0                                | 2977869,0                                 | 2977869,0                                | 2977869,0                                 | 3870885,0                               | 3870910,0                               | 200,8                  | 200,8                  | 580,0                  | 580,0                  | 290,0                  | 290,0                  |

| Naam       | y <sub>s</sub><br>[mm] | z <sub>s</sub><br>[mm] | S.p. |
|------------|------------------------|------------------------|------|
| 1 O 762x13 | 0                      | 0                      | 5    |
| 2 O 660x9  | 0                      | 0                      | 5    |
| 3 O 580x12 | 0                      | 0                      | 5    |

**Naam:** Doorsnede naam; **Productie:** Productieproces; **Vorm:** Profiel; **h:** Doorsnede hoogte; **b:** Doorsnede breedte; **tw:** Lijfdikte; **tf:** Flensdikte; **r<sub>1</sub>, r<sub>2</sub>, r<sub>3</sub>:** Afrondingswaarde; **A<sub>x</sub>, A<sub>y</sub>, A<sub>z</sub>:** Afschuivingsoppervlak; **I<sub>x</sub>, I<sub>y</sub>, I<sub>z</sub>:** Buigtraagheidsmoment; **I<sub>yz</sub>:** Centrifugaal traagheidsmoment; **I<sub>1</sub>, I<sub>2</sub>:** Hoofdbuigtraagheidsmoment; **α:** Hoofdrichtingen; **I<sub>ω</sub>:** Krommingsconstante; **W<sub>1,elt</sub>, W<sub>1,el,b</sub>, W<sub>2,elt</sub>, W<sub>2,el,b</sub>:** Elastisch weerstandsmoment; **W<sub>1,pl</sub>, W<sub>2,pl</sub>:** Plastisch weerstandsmoment; **i<sub>y</sub>, i<sub>z</sub>:** Traagheidsstraal; **H<sub>y</sub>:** Afmeting in lokale Y-richting; **H<sub>z</sub>:** Afmeting in lokale Z-richting; **y<sub>G</sub>:** Y-coördinaat van het zwaartepunt; **z<sub>G</sub>:** Z-coördinaat van het zwaartepunt; **y<sub>s</sub>:** Y-coördinaat van het afschuivingsmiddelpunt (torsie); **z<sub>s</sub>:** Z-coördinaat van het afschuivingsmiddelpunt (torsie); **S.p.:** Spanningspunten;



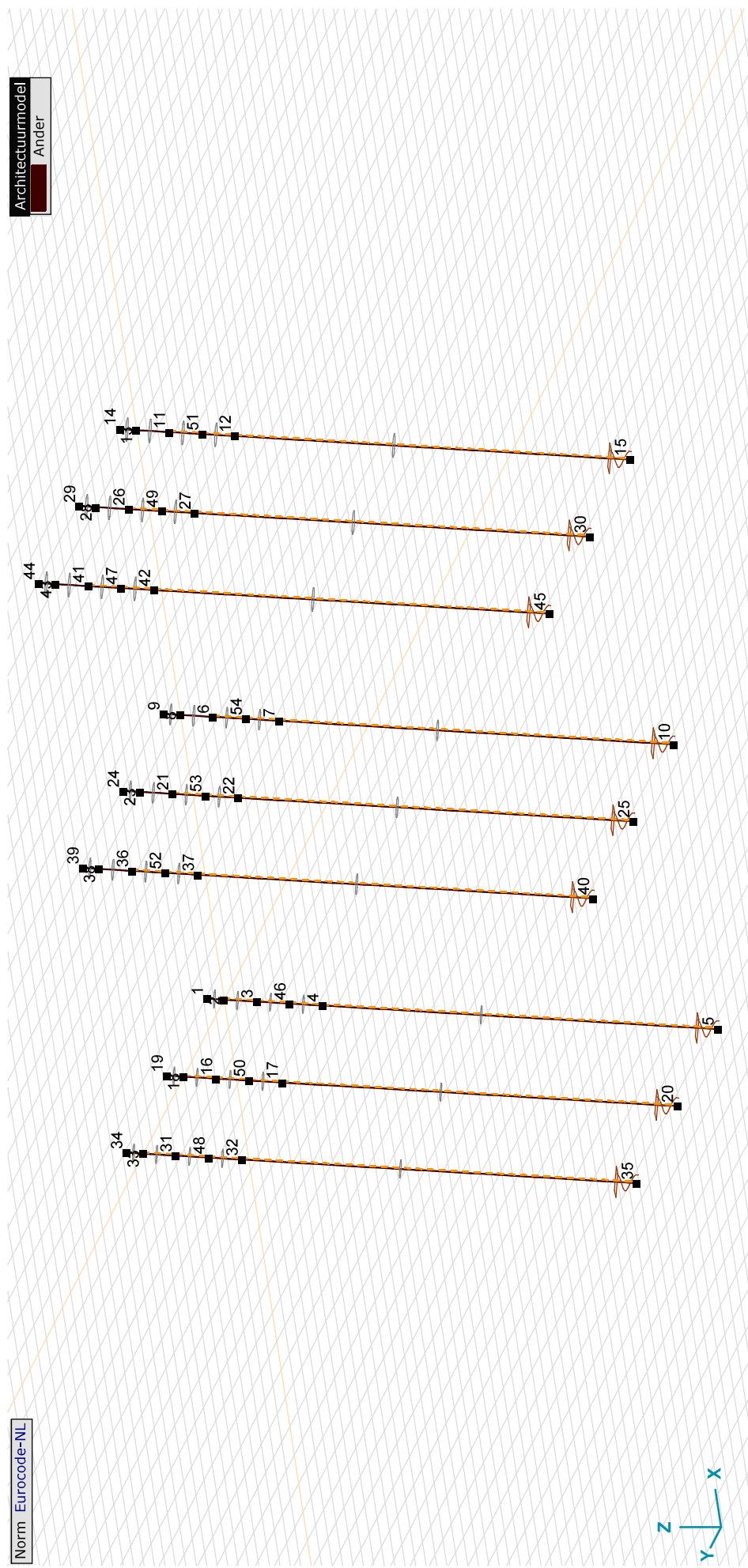
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Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Project:**

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Model: 1-paals reconstructie 2-ct.axs

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**Staven**

|    | Start-punt | Eind-punt | Lengte | Lokaal X | Material | Doorsnede |    | Start-punt | Eind-punt | Lengte | Lokaal X | Material | Doorsnede |
|----|------------|-----------|--------|----------|----------|-----------|----|------------|-----------|--------|----------|----------|-----------|
| 1  | 3          | 46        | 1,022  | i-j      | S 235    | 3         | 24 | 27         | 30        | 12,269 | i-j      | S 235    | 1         |
| 2  | 2          | 3         | 1,023  | i-j      | S 235    | 3         | 25 | 31         | 48        | 1,022  | i-j      | S 235    | 3         |
| 3  | 1          | 2         | 0,511  | i-j      | S 235    | 3         | 26 | 33         | 31        | 1,023  | j-i      | S 235    | 3         |
| 4  | 4          | 5         | 12,269 | i-j      | S 235    | 3         | 27 | 34         | 33        | 0,511  | j-i      | S 235    | 3         |
| 5  | 6          | 54        | 1,022  | i-j      | S 355    | 2         | 28 | 32         | 35        | 12,269 | i-j      | S 235    | 3         |
| 6  | 8          | 6         | 1,023  | j-i      | S 355    | 2         | 29 | 36         | 52        | 1,022  | i-j      | S 355    | 2         |
| 7  | 9          | 8         | 0,511  | j-i      | S 355    | 2         | 30 | 38         | 36        | 1,023  | j-i      | S 355    | 2         |
| 8  | 7          | 10        | 12,269 | i-j      | S 355    | 2         | 31 | 39         | 38        | 0,511  | j-i      | S 355    | 2         |
| 9  | 11         | 51        | 1,022  | i-j      | S 235    | 1         | 32 | 37         | 40        | 12,269 | i-j      | S 355    | 2         |
| 10 | 13         | 11        | 1,023  | j-i      | S 235    | 1         | 33 | 41         | 47        | 1,022  | i-j      | S 235    | 1         |
| 11 | 14         | 13        | 0,511  | j-i      | S 235    | 1         | 34 | 43         | 41        | 1,023  | j-i      | S 235    | 1         |
| 12 | 12         | 15        | 12,269 | i-j      | S 235    | 1         | 35 | 44         | 43        | 0,511  | j-i      | S 235    | 1         |
| 13 | 16         | 50        | 1,022  | i-j      | S 235    | 3         | 36 | 42         | 45        | 12,269 | i-j      | S 235    | 1         |
| 14 | 18         | 16        | 1,023  | j-i      | S 235    | 3         | 37 | 46         | 4         | 1,022  | j-i      | S 235    | 3         |
| 15 | 19         | 18        | 0,511  | j-i      | S 235    | 3         | 38 | 51         | 12        | 1,022  | j-i      | S 235    | 1         |
| 16 | 17         | 20        | 12,269 | i-j      | S 235    | 3         | 39 | 50         | 17        | 1,022  | j-i      | S 235    | 3         |
| 17 | 21         | 53        | 1,022  | i-j      | S 355    | 2         | 40 | 49         | 27        | 1,022  | j-i      | S 235    | 1         |
| 18 | 23         | 21        | 1,023  | j-i      | S 355    | 2         | 41 | 48         | 32        | 1,022  | j-i      | S 235    | 3         |
| 19 | 24         | 23        | 0,511  | j-i      | S 355    | 2         | 42 | 47         | 42        | 1,022  | j-i      | S 235    | 1         |
| 20 | 22         | 25        | 12,269 | i-j      | S 355    | 2         | 43 | 54         | 7         | 1,022  | j-i      | S 355    | 2         |
| 21 | 26         | 49        | 1,022  | i-j      | S 235    | 1         | 44 | 53         | 22        | 1,022  | j-i      | S 355    | 2         |
| 22 | 28         | 26        | 1,023  | j-i      | S 235    | 1         | 45 | 52         | 37        | 1,022  | j-i      | S 355    | 2         |
| 23 | 29         | 28        | 0,511  | j-i      | S 235    | 1         |    |            |           |        |          |          |           |

Lengte: Elementlengte; Lokaal X: Lokale X-richting.

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Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Knoopopleggingen**

| Knoop | X [m] | Y [m]  | Z [m]   | Type    | Ref. elem.  | N <sub>aa</sub> m <sub>x</sub> | K <sub>x</sub> [kN/m] | K <sub>xy</sub> [kN/m] | N <sub>aa</sub> m <sub>y</sub> | K <sub>y</sub> [kN/m] | K <sub>yy</sub> [kN/m] | N <sub>aa</sub> m <sub>z</sub> | K <sub>z</sub> [kN/m] | K <sub>yz</sub> [kN/m] | N <sub>aa</sub> m <sub>xx</sub> | K <sub>xx</sub> [kN/m/rad] |
|-------|-------|--------|---------|---------|-------------|--------------------------------|-----------------------|------------------------|--------------------------------|-----------------------|------------------------|--------------------------------|-----------------------|------------------------|---------------------------------|----------------------------|
| 1     | 5     | -2,259 | -15,000 | Staafr. | Staafr. 63  | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 2     | 10    | 7,741  | -15,000 | Staafr. | Staafr. 126 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 3     | 15    | 17,741 | -15,000 | Staafr. | Staafr. 189 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 4     | 20    | -2,259 | -15,000 | Staafr. | Staafr. 252 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 5     | 25    | 7,741  | -15,000 | Staafr. | Staafr. 315 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 6     | 30    | 17,741 | -15,000 | Staafr. | Staafr. 378 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 7     | 35    | -2,259 | -15,000 | Staafr. | Staafr. 441 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 8     | 40    | 7,741  | -15,000 | Staafr. | Staafr. 504 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |
| 9     | 45    | 17,741 | -15,000 | Staafr. | Staafr. 567 | Vast - translatie              | IE+10                 | IE+10                  | —                              | —                     | —                      | —                              | —                     | —                      | Vast - rotatie                  | IE+10                      |

| Knoop | K <sub>xx</sub> [kN/m/rad] | N <sub>aa</sub> m <sub>yy</sub> | K <sub>yy</sub> [kN/m/rad] | K <sub>xy</sub> [kN/m/rad] | N <sub>aa</sub> m <sub>zz</sub> | K <sub>zz</sub> [kN/m/rad] | K <sub>zy</sub> [kN/m/rad] |
|-------|----------------------------|---------------------------------|----------------------------|----------------------------|---------------------------------|----------------------------|----------------------------|
| 1     | 5                          | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 2     | 10                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 3     | 15                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 4     | 20                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 5     | 25                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 6     | 30                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 7     | 35                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 8     | 40                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |
| 9     | 45                         | IE+10                           | —                          | —                          | —                               | —                          | —                          |

Knoop: Ondersteunde knoop. Type: Opleggingstype. Ref. elem.: Referentie-element. K<sub>x</sub>, K<sub>y</sub>, K<sub>xx</sub>, K<sub>yy</sub>, K<sub>zz</sub>: Initiele stijfheid.**Lijnopleggingen**

| Lijn | Type    | Ref. elem. | R <sub>x</sub> [kN/m/m] | R <sub>y</sub> [kN/m/m] | R <sub>z</sub> [kN/m/m] | R <sub>xx</sub> [kNm/rad/m] | R <sub>yy</sub> [kNm/rad/m] | R <sub>zz</sub> [kNm/rad/m] | NL(x) | NL(y) | NL(z) | NL(xx) | NL(yy) | NL(zz) |
|------|---------|------------|-------------------------|-------------------------|-------------------------|-----------------------------|-----------------------------|-----------------------------|-------|-------|-------|--------|--------|--------|
| 1    | Staafr. |            |                         |                         |                         |                             |                             |                             |       |       |       |        |        |        |
| 28   | Staafr. |            | 0                       | 2,39E+4                 | 2,39E+4                 |                             |                             |                             |       |       |       |        |        |        |
| 28   | Staafr. |            | 0                       | 3,1E+3                  | 3,1E+3                  |                             |                             |                             |       |       |       |        |        |        |

| Lijn | F(x) [kN/m] | F(y) [kN/m] | F(z) [kN/m] | M(x) [kNm/m] | M(y) [kNm/m] | M(z) [kNm/m] |
|------|-------------|-------------|-------------|--------------|--------------|--------------|
| 1    |             |             |             |              |              |              |
| 28   |             | 37,000      | 37,000      |              |              |              |
| 28   |             | 6,200       | 6,200       |              |              |              |

**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Lijnopleggingen**

| Lijn | Type    | Ref. elem. | Rx<br>[kNm/m] | Ry<br>[kNm/m] | Rz<br>[kNm/m] | Rxx<br>[kNm/rad/m] | Ryy<br>[kNm/rad/m] | Rzz<br>[kNm/rad/m] | NL(x) | NL(y)       | NL(z)       | NL(xx) | NL(yy) | NL(zz) |
|------|---------|------------|---------------|---------------|---------------|--------------------|--------------------|--------------------|-------|-------------|-------------|--------|--------|--------|
| 2    | Staafr. |            | 0             | 2,39E+4       | 2,39E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 3    | Staafr. |            | 0             | 3,32E+3       | 3,32E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 4    | Staafr. |            | 0             | 2,55E+4       | 2,55E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 5    | Staafr. |            | 0             | 3,71E+3       | 3,71E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 6    | Staafr. |            | 0             | 2,85E+4       | 2,85E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 7    | Staafr. |            | 0             | 1,69E+4       | 1,69E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 29   | Staafr. |            | 0             | 2,2E+3        | 2,2E+3        |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 8    | Staafr. |            | 0             | 1,69E+4       | 1,69E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 9    | Staafr. |            | 0             | 2,34E+3       | 2,34E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 10   | Staafr. |            | 0             | 1,8E+4        | 1,8E+4        |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 11   | Staafr. |            | 0             | 2,62E+3       | 2,62E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 12   | Staafr. |            | 0             | 2,02E+4       | 2,02E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 13   | Staafr. |            | 0             | 3,38E+4       | 3,38E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 30   | Staafr. |            | 0             | 4,39E+3       | 4,39E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 14   | Staafr. |            | 0             | 3,38E+4       | 3,38E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 15   | Staafr. |            | 0             | 4,69E+3       | 4,69E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 16   | Staafr. |            | 0             | 3,66E+4       | 3,66E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 17   | Staafr. |            | 0             | 5,24E+3       | 5,24E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |

| Lijn | F(x)<br>[kN/m] | F(y)<br>[kN/m] | F(z)<br>[kN/m] | M(x)<br>[kNm/m] | M(y)<br>[kNm/m] | M(z)<br>[kNm/m] |
|------|----------------|----------------|----------------|-----------------|-----------------|-----------------|
| 2    |                | 143,400        | 143,400        |                 |                 |                 |
| 3    |                | 17,100         | 17,100         |                 |                 |                 |
| 4    |                | 153,000        | 153,000        |                 |                 |                 |
| 5    |                | 19,100         | 19,100         |                 |                 |                 |
| 6    |                | 171,000        | 171,000        |                 |                 |                 |
| 7    |                | 37,000         | 37,000         |                 |                 |                 |
| 29   |                | 6,100          | 6,100          |                 |                 |                 |
| 8    |                | 143,400        | 143,400        |                 |                 |                 |
| 9    |                | 17,100         | 17,100         |                 |                 |                 |
| 10   |                | 153,000        | 153,000        |                 |                 |                 |
| 11   |                | 19,100         | 19,100         |                 |                 |                 |
| 12   |                | 171,000        | 171,000        |                 |                 |                 |
| 13   |                | 37,000         | 37,000         |                 |                 |                 |
| 30   |                | 6,100          | 6,100          |                 |                 |                 |
| 14   |                | 143,400        | 143,400        |                 |                 |                 |
| 15   |                | 17,100         | 17,100         |                 |                 |                 |
| 16   |                | 153,000        | 153,000        |                 |                 |                 |
| 17   |                | 19,100         | 19,100         |                 |                 |                 |

**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Lijnopleggingen**

| Lijn | Type    | Ref. elem. | Rx<br>[kNm/m] | Ry<br>[kNm/m] | Rz<br>[kNm/m] | Rxx<br>[kNm/rad/m] | Ryy<br>[kNm/rad/m] | Rzz<br>[kNm/rad/m] | NL(x) | NL(y)       | NL(z)       | NL(xx) | NL(yy) | NL(zz) |
|------|---------|------------|---------------|---------------|---------------|--------------------|--------------------|--------------------|-------|-------------|-------------|--------|--------|--------|
| 18   | Staafr. |            | 0             | 4,03E+4       | 4,03E+4       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 19   | Staafr. |            | 0             | 3,1E+3        | 3,1E+3        |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 20   | Staafr. |            | 0             | 3,71E+3       | 3,71E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 21   | Staafr. |            | 0             | 2,2E+3        | 2,2E+3        |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 22   | Staafr. |            | 0             | 2,62E+3       | 2,62E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 23   | Staafr. |            | 0             | 4,39E+3       | 4,39E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 24   | Staafr. |            | 0             | 5,24E+3       | 5,24E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 25   | Staafr. |            | 0             | 3,32E+3       | 3,32E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 26   | Staafr. |            | 0             | 2,34E+3       | 2,34E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |
| 27   | Staafr. |            | 0             | 4,69E+3       | 4,69E+3       |                    |                    |                    |       | Symmetrisch | Symmetrisch |        |        |        |

| Lijn | F(x)<br>[kN/m] | F(y)<br>[kN/m] | F(z)<br>[kN/m] | M(x)<br>[kNm/m] | M(y)<br>[kNm/m] | M(z)<br>[kNm/m] |
|------|----------------|----------------|----------------|-----------------|-----------------|-----------------|
| 18   |                | 171,000        | 171,000        |                 |                 |                 |
| 19   |                | 23,300         | 23,300         |                 |                 |                 |
| 20   |                | 27,800         | 27,800         |                 |                 |                 |
| 21   |                | 23,300         | 23,300         |                 |                 |                 |
| 22   |                | 27,800         | 27,800         |                 |                 |                 |
| 23   |                | 23,300         | 23,300         |                 |                 |                 |
| 24   |                | 27,800         | 27,800         |                 |                 |                 |
| 25   |                | 24,900         | 24,900         |                 |                 |                 |
| 26   |                | 24,900         | 24,900         |                 |                 |                 |
| 27   |                | 24,900         | 24,900         |                 |                 |                 |

Lijn: Ondersteund lijnelement; Type: Opleggingsstype; Ref. elem.: Referentie-element; Rx, Ry, Rz: Verplaatsingsstijfheid; Rxx, Ryy, Rzz: Rotatiestijfheid; NL(x), NL(y), NL(z), NL(xx), NL(yy), NL(zz): Niet-lineaire parameters; F(x): Weerstand in X-richting; F(y): Weerstand in Y-richting; F(z): Weerstand in Z-richting; M(x): Weerstandsmoment in X-richting; M(y): Weerstandsmoment in Y-richting; M(z): Weerstandsmoment in Z-richting.

**Project:**

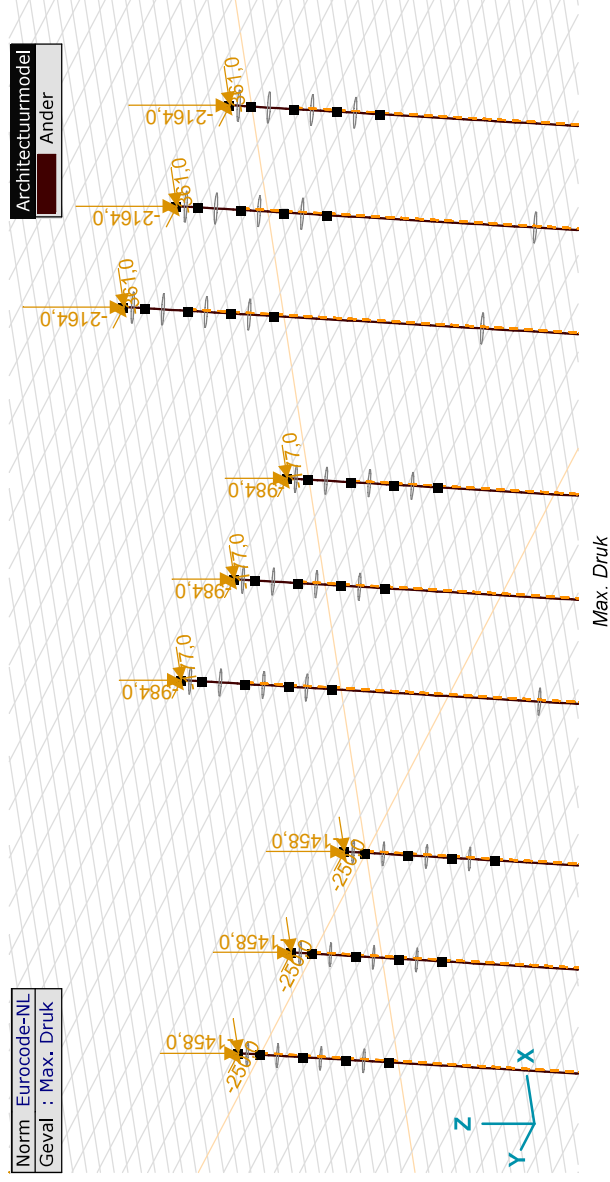
Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

**Max. Druk: Knoopbelastingen**

|    | Riching | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Mx<br>[kNm] | My<br>[kNm] | Mz<br>[kNm] |
|----|---------|------------|------------|------------|-------------|-------------|-------------|
| 1  | Globaal | -233,1     | -250,0     | -1458,0    | 0           | 0           | 0           |
| 9  | Globaal | -177,0     | -167,0     | -984,0     | 0           | 0           | 0           |
| 14 | Globaal | -361,0     | -353,0     | -2164,0    | 0           | 0           | 0           |
| 19 | Globaal | -233,1     | -250,0     | -1458,0    | 0           | 0           | 0           |
| 24 | Globaal | -177,0     | -167,0     | -984,0     | 0           | 0           | 0           |
| 29 | Globaal | -361,0     | -353,0     | -2164,0    | 0           | 0           | 0           |
| 34 | Globaal | -233,1     | -250,0     | -1458,0    | 0           | 0           | 0           |
| 39 | Globaal | -177,0     | -167,0     | -984,0     | 0           | 0           | 0           |
| 44 | Globaal | -361,0     | -353,0     | -2164,0    | 0           | 0           | 0           |

Fx, Fy, Fz: Belastingkracht component; Mx, My, Mz: Belastingmoment component;





**Project:**

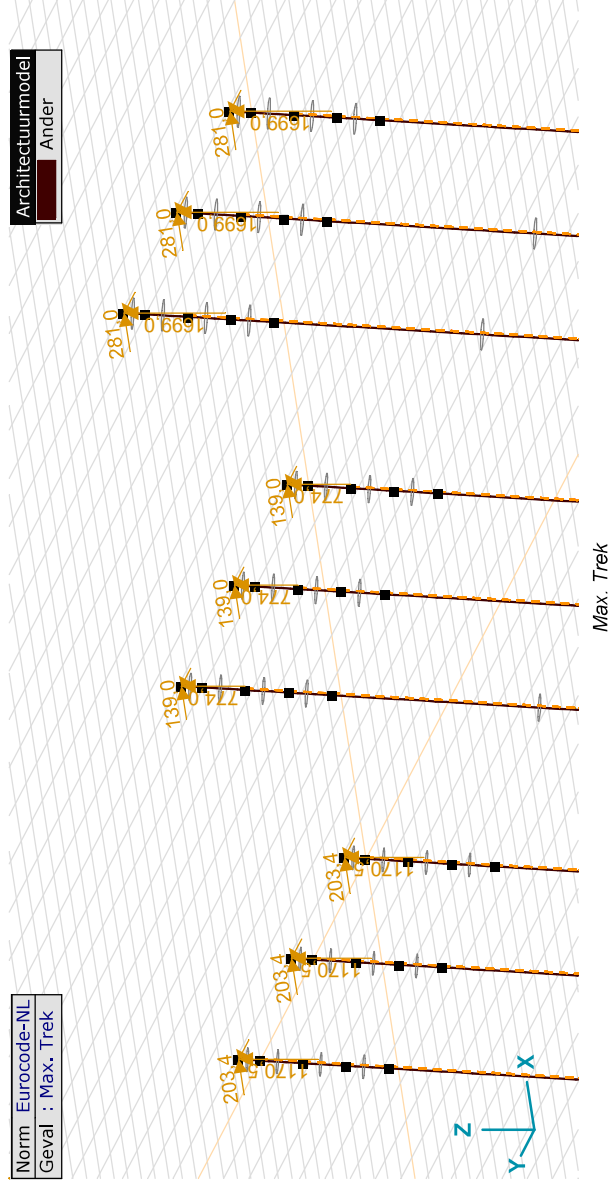
Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

**Max. Trek: Knoopbelastingen**

|    | Richting | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Mx<br>[kNm] | My<br>[kNm] | Mz<br>[kNm] |
|----|----------|------------|------------|------------|-------------|-------------|-------------|
| 1  | Globaal  | 203,4      | 188,9      | 1170,5     | 0           | 0           | 0           |
| 9  | Globaal  | 139,0      | 128,0      | 774,0      | 0           | 0           | 0           |
| 14 | Globaal  | 281,0      | 272,0      | 1699,0     | 0           | 0           | 0           |
| 19 | Globaal  | 203,4      | 188,9      | 1170,5     | 0           | 0           | 0           |
| 24 | Globaal  | 139,0      | 128,0      | 774,0      | 0           | 0           | 0           |
| 29 | Globaal  | 281,0      | 272,0      | 1699,0     | 0           | 0           | 0           |
| 34 | Globaal  | 203,4      | 188,9      | 1170,5     | 0           | 0           | 0           |
| 39 | Globaal  | 139,0      | 128,0      | 774,0      | 0           | 0           | 0           |
| 44 | Globaal  | 281,0      | 272,0      | 1699,0     | 0           | 0           | 0           |

Fx, Fy, Fz: Belastingkracht component; Mx, My, Mz: Belastingmoment component;



**Project:**

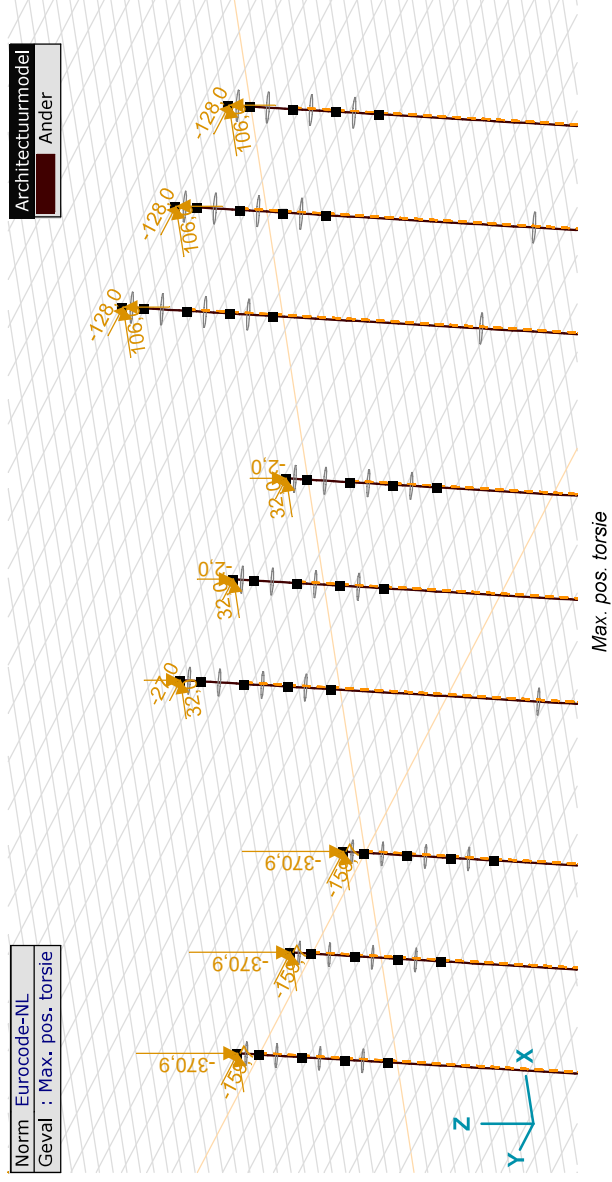
Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

**Max. pos. torsie: Knoopbelastingen**

|    | Riching | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Mx<br>[kNm] | My<br>[kNm] | Mz<br>[kNm] |
|----|---------|------------|------------|------------|-------------|-------------|-------------|
| 1  | Globaal | 33,9       | -159,7     | -370,9     | 0           | 0           | 0           |
| 9  | Globaal | 32,0       | -27,0      | -2,0       | 0           | 0           | 0           |
| 14 | Globaal | 106,0      | -128,0     | 58,0       | 0           | 0           | 0           |
| 19 | Globaal | 33,9       | -159,7     | -370,9     | 0           | 0           | 0           |
| 24 | Globaal | 32,0       | -27,0      | -2,0       | 0           | 0           | 0           |
| 29 | Globaal | 106,0      | -128,0     | 58,0       | 0           | 0           | 0           |
| 34 | Globaal | 33,9       | -159,7     | -370,9     | 0           | 0           | 0           |
| 39 | Globaal | 32,0       | -27,0      | -2,0       | 0           | 0           | 0           |
| 44 | Globaal | 106,0      | -128,0     | 58,0       | 0           | 0           | 0           |

Fx, Fy, Fz: Belastingkracht component; Mx, My, Mz: Belastingmoment component;



**Project:**

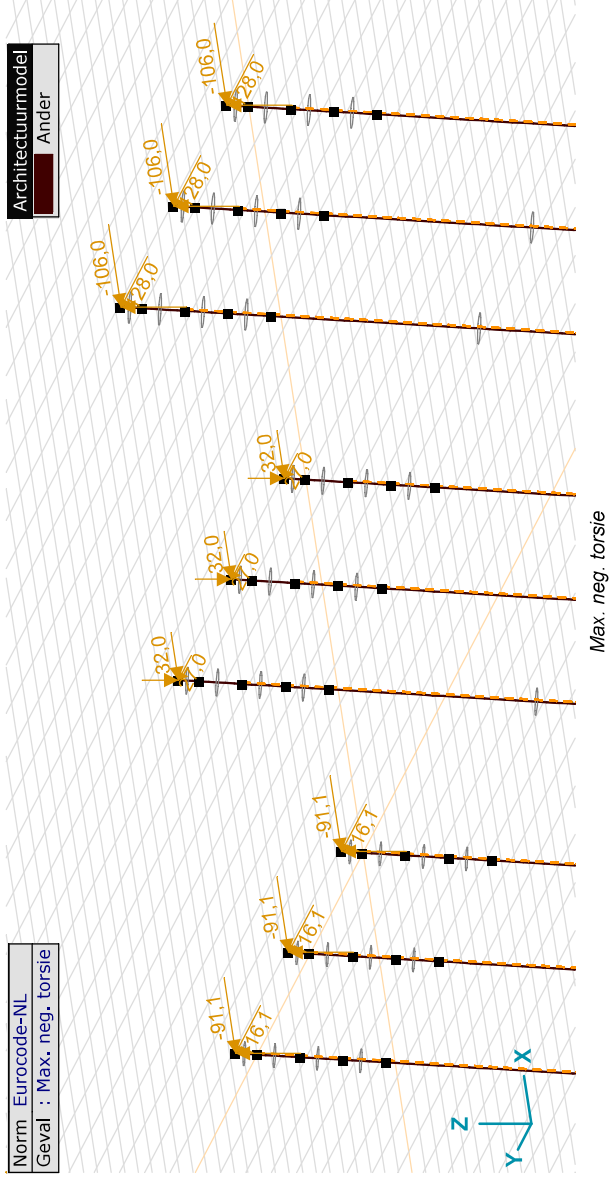
Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

**Max. neg. torsie: Knoopbelastingen**

|    | Richting | $F_x$<br>[kN] | $F_y$<br>[kN] | $F_z$<br>[kN] | $M_x$<br>[kNm] | $M_y$<br>[kNm] | $M_z$<br>[kNm] |
|----|----------|---------------|---------------|---------------|----------------|----------------|----------------|
| 1  | Globaal  | -91,1         | 116,1         | 57,0          | 0              | 0              | 0              |
| 9  | Globaal  | -32,0         | 27,0          | -2,0          | 0              | 0              | 0              |
| 14 | Globaal  | -106,0        | 128,0         | 58,0          | 0              | 0              | 0              |
| 19 | Globaal  | -91,1         | 116,1         | 57,0          | 0              | 0              | 0              |
| 24 | Globaal  | -32,0         | 27,0          | -2,0          | 0              | 0              | 0              |
| 29 | Globaal  | -106,0        | 128,0         | 58,0          | 0              | 0              | 0              |
| 34 | Globaal  | -91,1         | 116,1         | 57,0          | 0              | 0              | 0              |
| 39 | Globaal  | -32,0         | 27,0          | -2,0          | 0              | 0              | 0              |
| 44 | Globaal  | -106,0        | 128,0         | 58,0          | 0              | 0              | 0              |

$F_x, F_y, F_z$ : Belastingkracht component;  $M_x, M_y, M_z$ : Belastingmoment component;



**Project:**

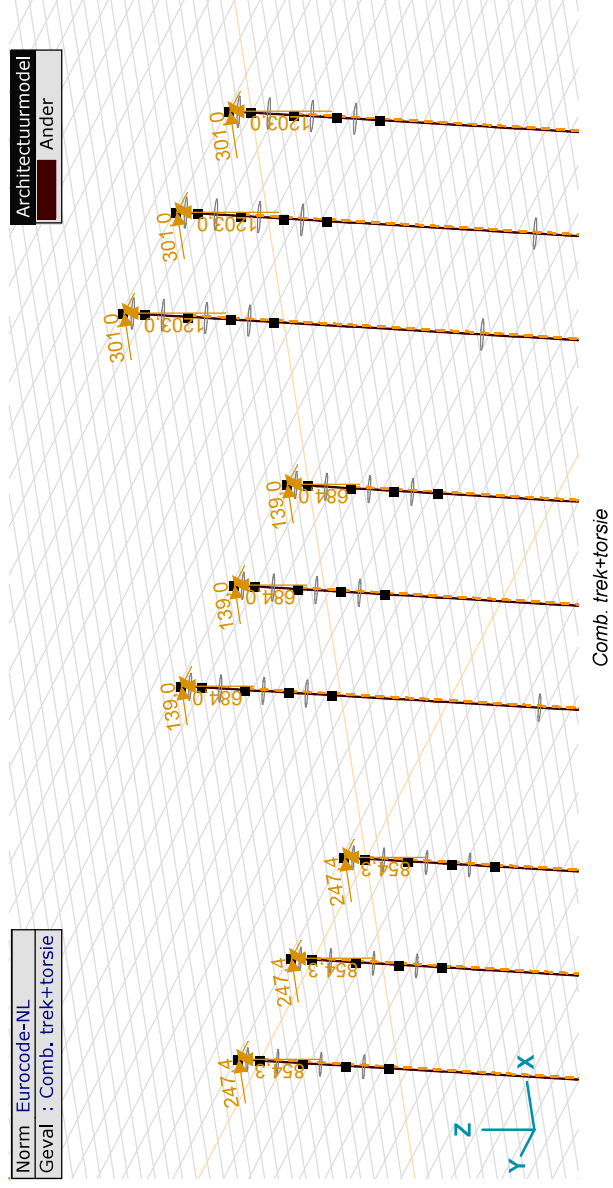
Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

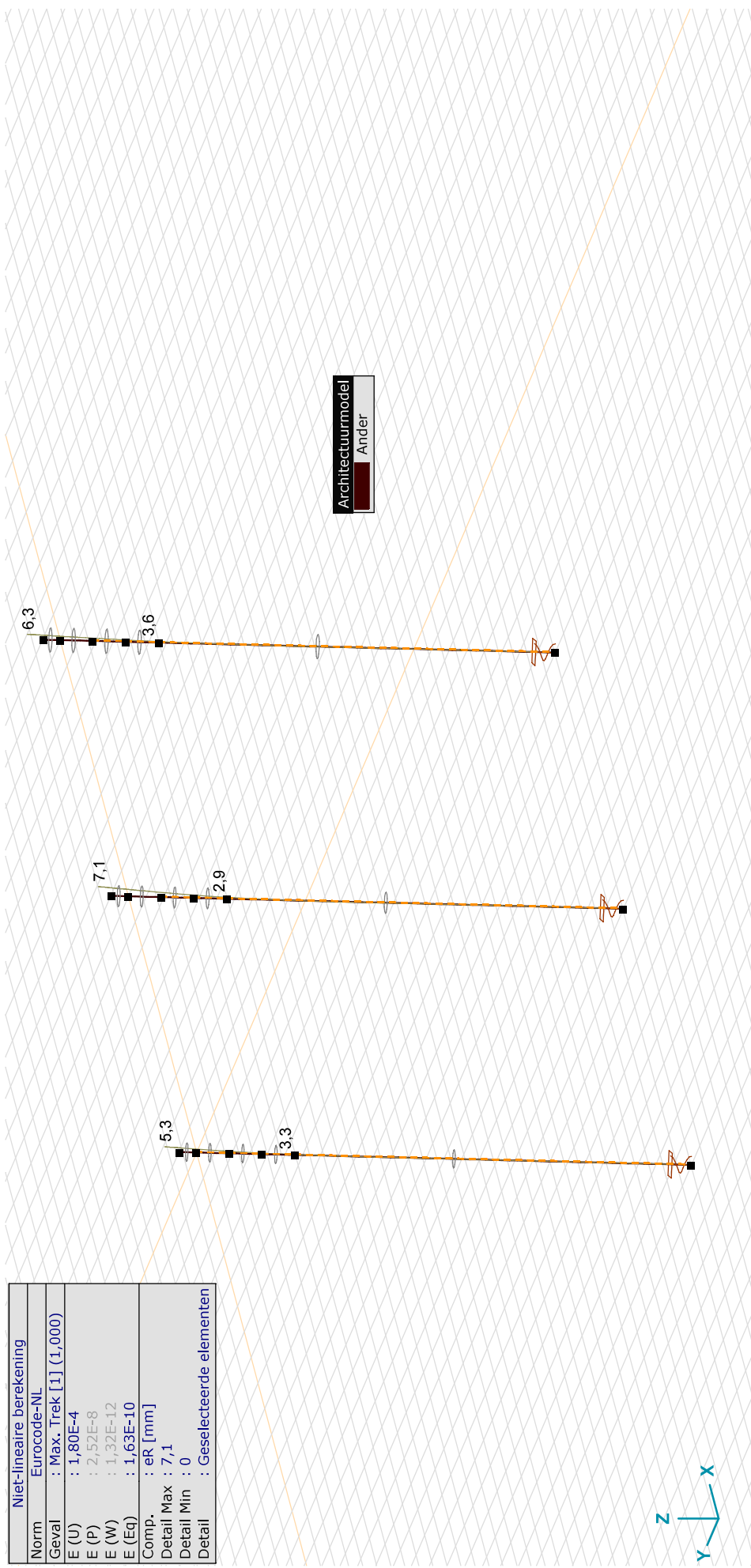
**Comb. trek+torsie: Knoopbelastingen**

|    | Richting | Fx<br>[kN] | Fy<br>[kN] | Fz<br>[kN] | Mx<br>[kNm] | My<br>[kNm] | Mz<br>[kNm] |
|----|----------|------------|------------|------------|-------------|-------------|-------------|
| 1  | Globaal  | 247,4      | 40,4       | 854,3      | 0           | 0           | 0           |
| 9  | Globaal  | 139,0      | 91,0       | 684,0      | 0           | 0           | 0           |
| 14 | Globaal  | 301,0      | 103,0      | 1203,0     | 0           | 0           | 0           |
| 19 | Globaal  | 247,4      | 40,4       | 854,3      | 0           | 0           | 0           |
| 24 | Globaal  | 139,0      | 91,0       | 684,0      | 0           | 0           | 0           |
| 29 | Globaal  | 301,0      | 103,0      | 1203,0     | 0           | 0           | 0           |
| 34 | Globaal  | 247,4      | 40,4       | 854,3      | 0           | 0           | 0           |
| 39 | Globaal  | 139,0      | 91,0       | 684,0      | 0           | 0           | 0           |
| 44 | Globaal  | 301,0      | 103,0      | 1203,0     | 0           | 0           | 0           |

Fx, Fy, Fz: Belastingkracht component; Mx, My, Mz: Belastingmoment component;



**Project:**  
 Constructeur: DNV GL - Energy  
 Model: 1-paals reconstructie 2-ct.axs



[1] > ~3. Non-lin., Max. Trek [1] (1,000), Onmiddellijke doorbuiging, eR, Lijnen

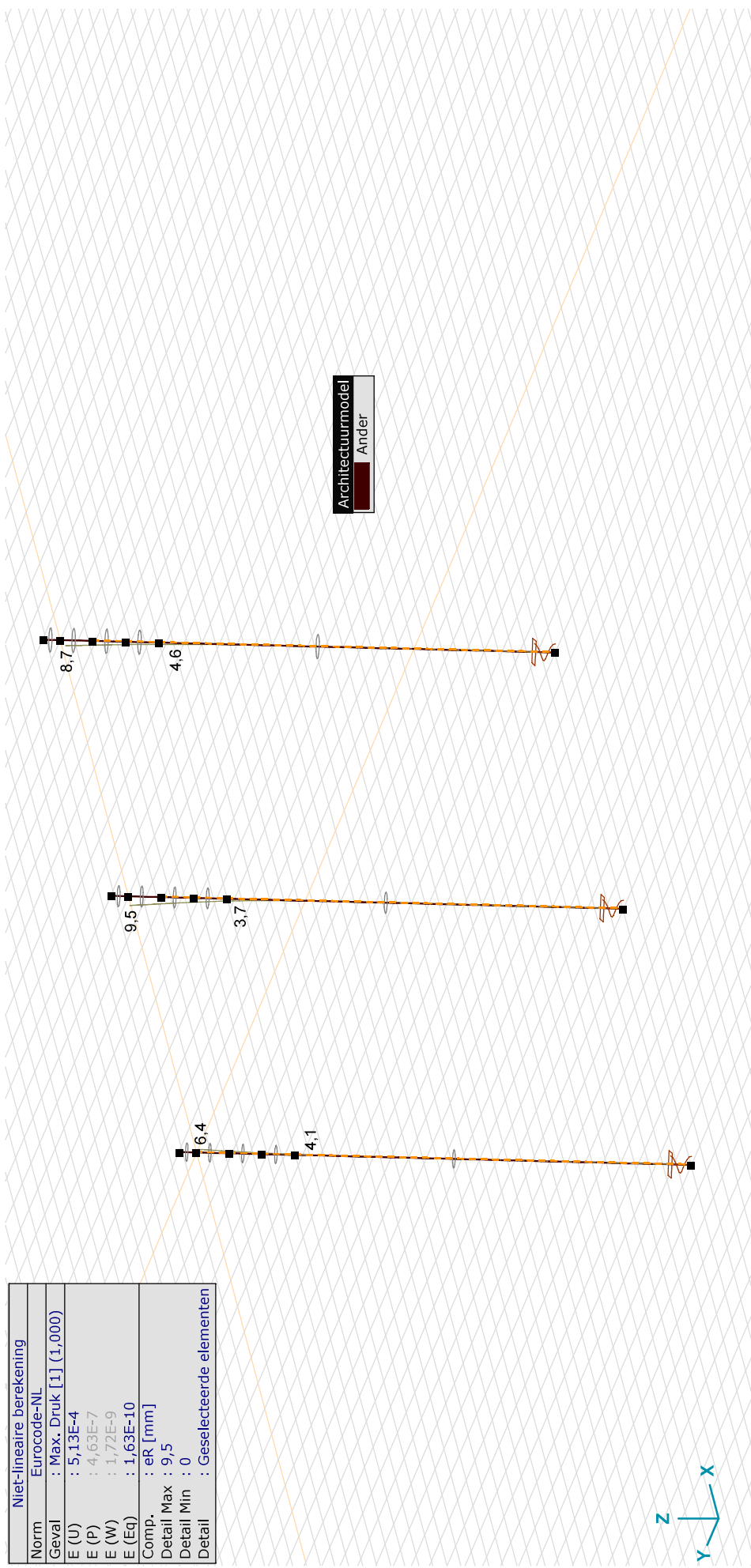
**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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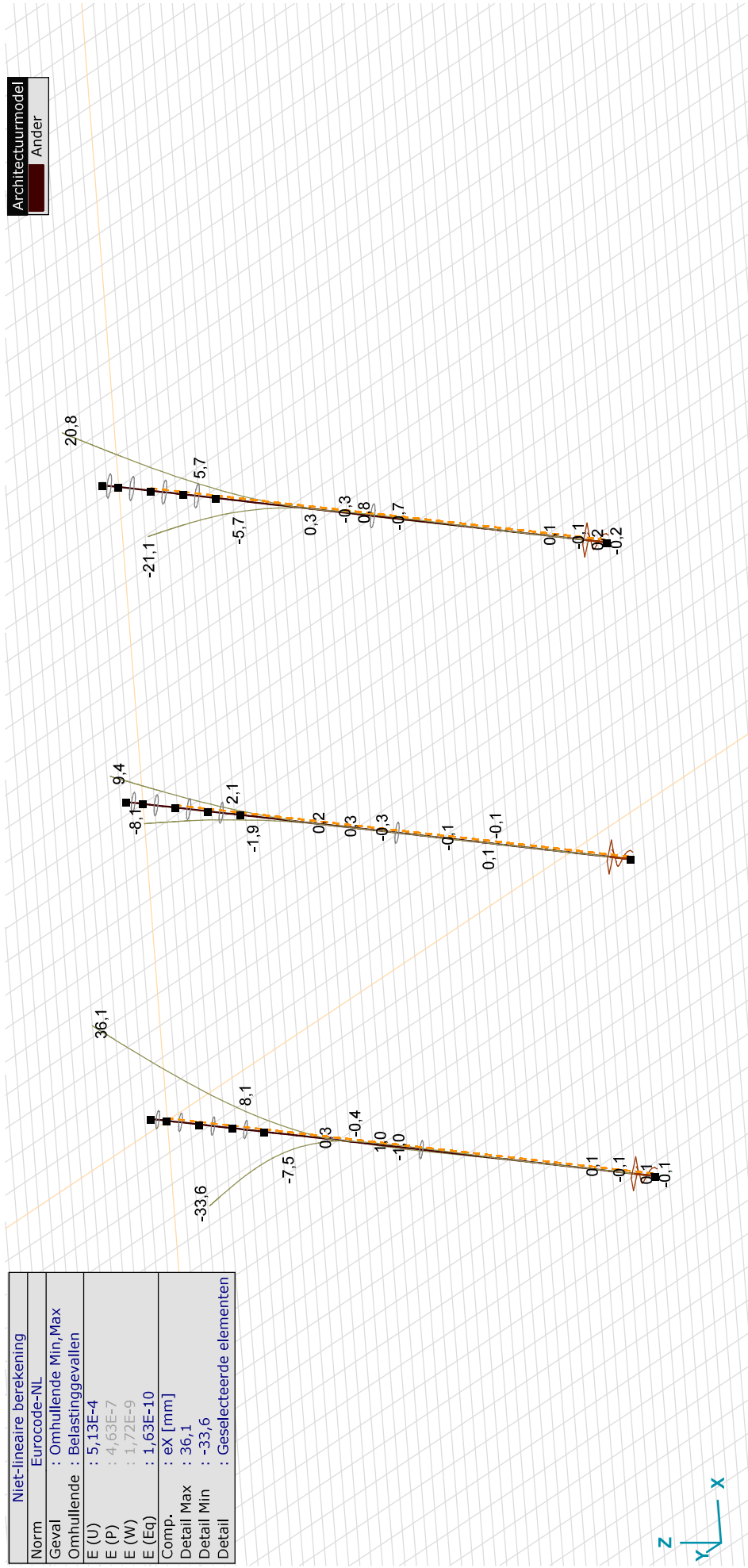
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[1] > ~3. Non-lin., Max. Druk [1] (1,000), Onmiddellijke doorbuiging, eR, Lijnen



**Project:**  
 Constructeur: DNV GL - Energy  
 Model: 1-paals reconstructie 2-ct.axs



[U], > ~2, Non-in., Omhullende (Belastinggevallen), Onmiddellijke doorbuiging, eX, Lijnen

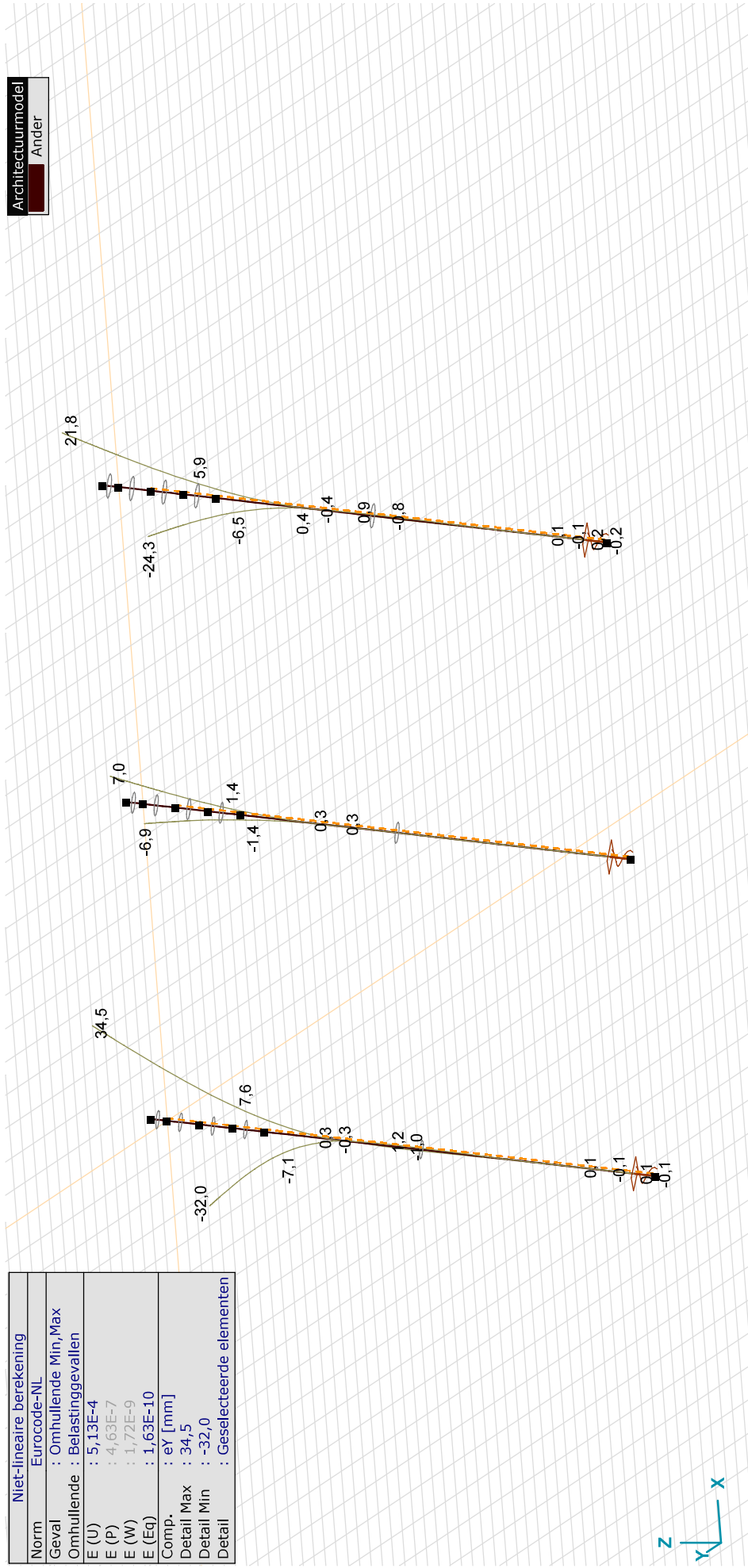
**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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[U], > ~2, Non-in., Omhullende (Belastinggevallen), Onmiddellijke doorbuiging, eY, Lijnen



**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Knoopverplaatsingen [Non-lin., Omhullende (Belastinggevallen)]**

|    | C    | min.<br>max. | Geval                         | eX<br>[mm] | eY<br>[mm] | eZ<br>[mm] | eR<br>[mm] | fX<br>[rad] | fY<br>[rad] | fZ<br>[rad] | fR<br>[rad] |
|----|------|--------------|-------------------------------|------------|------------|------------|------------|-------------|-------------|-------------|-------------|
| 1  | eX   | min          | Max. neg. torsie [I] (1,000)  | -33,6      | 34,5       | 0,1        | 48,2       | -0,009      | -0,008      | 0,003       | 0,012       |
|    |      | max          | Comb. trek+torsie [I] (1,000) | 36,1       | -32,0      | 2,5        | 48,3       | 0,008       | 0,009       | -0,003      | 0,012       |
|    | eY   | min          | Comb. trek+torsie [I] (1,000) | 36,1       | -32,0      | 2,5        | 48,3       | 0,008       | 0,009       | -0,003      | 0,012       |
|    |      | max          | Max. neg. torsie [I] (1,000)  | -33,6      | 34,5       | 0,1        | 48,2       | -0,009      | -0,008      | 0,003       | 0,012       |
| 9  | eX   | min          | Max. neg. torsie [I] (1,000)  | -8,1       | 7,0        | 0,1        | 10,8       | -0,002      | -0,002      | 0,001       | 0,003       |
|    |      | max          | Comb. trek+torsie [I] (1,000) | 9,4        | -2,7       | 2,0        | 10,0       | 0,001       | 0,002       | 0           | 0,003       |
|    | eY   | min          | Max. pos. torsie [I] (1,000)  | 8,3        | -6,9       | -0,2       | 10,8       | 0,002       | 0,002       | -0,001      | 0,003       |
|    |      | max          | Max. neg. torsie [I] (1,000)  | -8,1       | 7,0        | 0,1        | 10,8       | -0,002      | -0,002      | 0,001       | 0,003       |
| 14 | eX   | min          | Max. neg. torsie [I] (1,000)  | -21,1      | 21,8       | 0          | 30,3       | -0,005      | -0,005      | 0,001       | 0,007       |
|    |      | max          | Comb. trek+torsie [I] (1,000) | 20,8       | -13,7      | 2,1        | 25,0       | 0,003       | 0,005       | -0,001      | 0,006       |
|    | eY   | min          | Max. pos. torsie [I] (1,000)  | 18,6       | -24,3      | 1,0        | 30,6       | 0,006       | 0,004       | -0,001      | 0,007       |
|    |      | max          | Max. neg. torsie [I] (1,000)  | -21,1      | 21,8       | 0          | 30,3       | -0,005      | -0,005      | 0,001       | 0,007       |
|    | Ext. |              |                               |            |            |            |            |             |             |             |             |
| 1  | eX   | min          | Max. neg. torsie [I] (1,000)  | -33,6      | 34,5       | 0,1        | 48,2       | -0,009      | -0,008      | 0,003       | 0,012       |
|    |      | max          | Comb. trek+torsie [I] (1,000) | 36,1       | -32,0      | 2,5        | 48,3       | 0,008       | 0,009       | -0,003      | 0,012       |
| 1  | eY   | min          | Comb. trek+torsie [I] (1,000) | 36,1       | -32,0      | 2,5        | 48,3       | 0,008       | 0,009       | -0,003      | 0,012       |
|    |      | max          | Max. neg. torsie [I] (1,000)  | -33,6      | 34,5       | 0,1        | 48,2       | -0,009      | -0,008      | 0,003       | 0,012       |
| 9  | eR   | min          | Comb. trek+torsie [I] (1,000) | 9,4        | -2,7       | 2,0        | 10,0       | 0,001       | 0,002       | 0           | 0,003       |
|    |      | max          | Comb. trek+torsie [I] (1,000) | 36,1       | -32,0      | 2,5        | 48,3       | 0,008       | 0,009       | -0,003      | 0,012       |

C: Extreme component; min, max.: Extreme type; Geval: Belastinggeval van de extreme; eX: Verplaatsing in X-richting; eY: Verplaatsing in Y-richting; eZ: Verplaatsing in Z-richting; eR: Resulterende verplaatsing; fX: Rotatie in X-richting; fY: Rotatie in Y-richting; fZ: Rotatie in Z-richting; fR: Resulterende rotatie.



**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Staafspanningen [Non-lin., Omhullende (Belastinggevallen)]**

| Ext. | Prof. | Doorsnede naam | C     | min.<br>max. | Geval                         | Pos.<br>[m] | Knoop | S <sub>x</sub> :min<br>[N/mm <sup>2</sup> ] | S <sub>x</sub> :max<br>[N/mm <sup>2</sup> ] | V <sub>min</sub><br>[N/mm <sup>2</sup> ] | V <sub>max</sub><br>[N/mm <sup>2</sup> ] | Somin<br>[N/mm <sup>2</sup> ] | Somax<br>[N/mm <sup>2</sup> ] | V <sub>y</sub> :gem<br>[N/mm <sup>2</sup> ] | V <sub>z</sub> :gem<br>[N/mm <sup>2</sup> ] |
|------|-------|----------------|-------|--------------|-------------------------------|-------------|-------|---|---|--|--|-------------------------------|-------------------------------|---|---|
| 4    | 3     | O 580x12       | Somin | min          | Max. neg. torsie [I] (1,000)  | 10,061      | (105) | 0,02  | 5,53  | 0  | 0,56                                     | 0,03                          | 5,53                          | 0,28  | 0   |
| 3    | 3     | O 580x12       |       | max          | Max. Druk [I] (1,000)         | 0           | (1)   | -69,93                                      | -69,93                                      | 0  | 2,95                                     | 69,93                         | 70,12                         | -0,56                                       | -1,48                                       |
| 4    | 3     | O 580x12       |       | max          | Max. Druk [I] (1,000)         | 12,269      | (5)   | -69,93                                      | -69,93                                      | 0  | 0  | 69,93                         | 69,93                         | 0   | 0   |
| 15   | 3     | O 580x12       |       | max          | Max. Druk [I] (1,000)         | 0           | (19)  | -69,93                                      | -69,93                                      | 0  | 2,95                                     | 69,93                         | 70,12                         | -0,56                                       | -1,48                                       |
| 16   | 3     | O 580x12       |       | max          | Max. Druk [I] (1,000)         | 12,269      | (20)  | -69,93                                      | -69,93                                      | 0  | 0  | 69,93                         | 69,93                         | 0   | 0   |
| 27   | 3     | O 580x12       |       | max          | Max. Druk [I] (1,000)         | 0           | (34)  | -69,93                                      | -69,93                                      | 0  | 2,95                                     | 69,93                         | 70,12                         | -0,56                                       | -1,48                                       |
| 28   | 3     | O 580x12       |       | max          | Max. Druk [I] (1,000)         | 12,269      | (35)  | -69,93                                      | -69,93                                      | 0  | 0  | 69,93                         | 69,93                         | 0   | 0   |
| 4    | 3     | O 580x12       | Somax | min          | Max. neg. torsie [I] (1,000)  | 12,269      | (5)   | 2,78  | 2,78  | 0  | 0,05                                     | 2,78                          | 2,78                          | 0,02  | 0   |
| 16   | 3     | O 580x12       |       | min          | Max. neg. torsie [I] (1,000)  | 12,269      | (20)  | 2,78  | 2,78  | 0  | 0,06                                     | 2,78                          | 2,78                          | 0,03  | 0   |
| 28   | 3     | O 580x12       |       | min          | Max. neg. torsie [I] (1,000)  | 12,269      | (35)  | 2,78  | 2,78  | 0  | 0,03                                     | 2,78                          | 2,78                          | 0,02  | 0   |
| 4    | 3     | O 580x12       |       | max          | Comb. trek+torsie [I] (1,000) | 0,491       | (66)  | -112,99                                     | 195,01                                      | 0  | 0,90                                     | 32,56                         | 195,01                        | 0,45  | -0,38                                       |
| 16   | 3     | O 580x12       |       | max          | Comb. trek+torsie [I] (1,000) | 0,491       | (243) | -113,09                                     | 195,11                                      | 0  | 0,77                                     | 31,28                         | 195,11                        | 0,38  | -0,34                                       |
| 28   | 3     | O 580x12       |       | max          | Comb. trek+torsie [I] (1,000) | 0,491       | (420) | -113,09                                     | 195,11                                      | 0  | 0,89                                     | 33,78                         | 195,12                        | 0,44  | -0,41                                       |

Prof.: Profiel; C: Extreem type; min, max.: Extreem type; Geval: Belastinggeval van de extreme; Pos.: Lokale X-positie van de doorsnede op de staaf; S<sub>x</sub>:min: Doorsnede minimum normaalspanning; S<sub>x</sub>:max: Doorsnede maximum normaalspanning;V<sub>min</sub>: Doorsnede minimum afschuifspanning; V<sub>max</sub>: Doorsnede maximum afschuifspanning; Somax: Doorsnede maximum Von Mises spanning; Somax: Doorsnede maximum Von Mises spanning; V<sub>y</sub>:gem: Afschuifspanning in lokale Y-richting; V<sub>z</sub>:gem: Afschuifspanning in lokale Z-richting;**Staafspanningen [Non-lin., Omhullende (Belastinggevallen)]**

| Ext. | Prof. | Doorsnede naam | C     | min.<br>max. | Geval                        | Pos.<br>[m] | Knoop | S <sub>x</sub> :min<br>[N/mm <sup>2</sup> ] | S <sub>x</sub> :max<br>[N/mm <sup>2</sup> ] | V <sub>min</sub><br>[N/mm <sup>2</sup> ] | V <sub>max</sub><br>[N/mm <sup>2</sup> ] | Somin<br>[N/mm <sup>2</sup> ] | Somax<br>[N/mm <sup>2</sup> ] | V <sub>y</sub> :gem<br>[N/mm <sup>2</sup> ] | V <sub>z</sub> :gem<br>[N/mm <sup>2</sup> ] |
|------|-------|----------------|-------|--------------|------------------------------|-------------|-------|---|---|--|--|-------------------------------|-------------------------------|---|---|
| 8    | 2     | O 660x9        | Somin | min          | Max. neg. torsie [I] (1,000) | 11,288      | (169) | -0,31                                       | 0,01  | 0  | 0,09                                     | 0,01                          | 0,31                          | 0,04  | 0   |
| 7    | 2     | O 660x9        |       | max          | Max. Druk [I] (1,000)        | 0           | (9)   | -56,60                                      | -56,60                                      | 0  | 3,77                                     | 56,60                         | 56,98                         | 0,40  | -1,89                                       |
| 8    | 2     | O 660x9        |       | max          | Max. Druk [I] (1,000)        | 12,269      | (10)  | -56,60                                      | -56,60                                      | 0  | 0,01                                     | 56,60                         | 56,60                         | 0   | -0,01                                       |
| 19   | 2     | O 660x9        |       | max          | Max. Druk [I] (1,000)        | 0           | (24)  | -56,60                                      | -56,60                                      | 0  | 3,77                                     | 56,60                         | 56,98                         | 0,40  | -1,89                                       |
| 20   | 2     | O 660x9        |       | max          | Max. Druk [I] (1,000)        | 12,269      | (25)  | -56,60                                      | -56,60                                      | 0  | 0,02                                     | 56,60                         | 56,60                         | 0   | -0,01                                       |
| 31   | 2     | O 660x9        |       | max          | Max. Druk [I] (1,000)        | 0           | (39)  | -56,60                                      | -56,60                                      | 0  | 3,77                                     | 56,60                         | 56,98                         | 0,40  | -1,89                                       |
| 32   | 2     | O 660x9        |       | max          | Max. Druk [I] (1,000)        | 12,269      | (40)  | -56,60                                      | -56,60                                      | 0  | 0,01                                     | 56,60                         | 56,60                         | 0   | 0   |
| 32   | 2     | O 660x9        | Somax | min          | Max. pos. torsie [I] (1,000) | 12,269      | (40)  | -0,07                                       | -0,07                                       | 0  | 0,01                                     | 0,07                          | 0,07                          | 0   | 0   |
| 20   | 2     | O 660x9        |       | max          | Max. Druk [I] (1,000)        | 0,491       | (302) | -90,62                                      | -22,58                                      | 0  | 0,62                                     | 22,58                         | 90,62                         | -0,07                                       | 0,31  |

Prof.: Profiel; C: Extreem type; min, max.: Extreem type; Geval: Belastinggeval van de extreme; Pos.: Lokale X-positie van de doorsnede op de staaf; S<sub>x</sub>:min: Doorsnede minimum normaalspanning; S<sub>x</sub>:max: Doorsnede maximum normaalspanning;V<sub>min</sub>: Doorsnede minimum afschuifspanning; V<sub>max</sub>: Doorsnede maximum afschuifspanning; Somax: Doorsnede maximum Von Mises spanning; Somax: Doorsnede maximum Von Mises spanning; V<sub>y</sub>:gem: Afschuifspanning in lokale Y-richting; V<sub>z</sub>:gem: Afschuifspanning in lokale Z-richting;

**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Staafspanningen [Non-lin., Omhullende (Belastingevallen)]**

| Ext. | Prof. | Doorsnede naam | C     | min.<br>max. | Geval                        | Pos.<br>[m] | Knoop | S <sub>x,min</sub><br>[N/mm <sup>2</sup> ] | S <sub>x,max</sub><br>[N/mm <sup>2</sup> ] | V <sub>min</sub><br>[N/mm <sup>2</sup> ] | V <sub>max</sub><br>[N/mm <sup>2</sup> ] | S <sub>omin</sub><br>[N/mm <sup>2</sup> ] | S <sub>omax</sub><br>[N/mm <sup>2</sup> ] | V <sub>y,gem</sub><br>[N/mm <sup>2</sup> ] | V <sub>z,gem</sub><br>[N/mm <sup>2</sup> ] |       |
|------|-------|----------------|-------|--------------|------------------------------|-------------|-------|--|--|--|--|---|---|--|--|-------|
|      |       |                |       |              |                              |             |       |  |  |  |  |   |   |  |  |       |
| 12   | 1     | O 762x13       | Somin | min          | Max. neg. torsie [I](1,000)  | 10,061      | (223) | 0,01                                       | 3,98                                       | 0  | 0,37                                     | 0,02                                      | 3,98                                      | 0,18                                       |  | 0     |
| 11   | 1     | O 762x13       |       | max          | Max. Druk [I](1,000)         | 0           | (14)  | -74,04                                     | -74,04                                     | 0  | 2,99                                     | 74,04                                     | 74,22                                     | 0,19                                       |  | -1,49 |
| 12   | 1     | O 762x13       |       | max          | Max. Druk [I](1,000)         | 12,269      | (15)  | -74,04                                     | -74,04                                     | 0  | 0,01                                     | 74,04                                     | 74,04                                     | 0  |  | -0,01 |
| 23   | 1     | O 762x13       |       | max          | Max. Druk [I](1,000)         | 0           | (29)  | -74,04                                     | -74,04                                     | 0  | 2,99                                     | 74,04                                     | 74,22                                     | 0,19                                       |  | -1,49 |
| 24   | 1     | O 762x13       |       | max          | Max. Druk [I](1,000)         | 12,269      | (30)  | -74,04                                     | -74,04                                     | 0  | 0,01                                     | 74,04                                     | 74,04                                     | 0  |  | -0,01 |
| 35   | 1     | O 762x13       |       | max          | Max. Druk [I](1,000)         | 0           | (44)  | -74,04                                     | -74,04                                     | 0  | 2,99                                     | 74,04                                     | 74,22                                     | 0,19                                       |  | -1,49 |
| 36   | 1     | O 762x13       |       | max          | Max. Druk [I](1,000)         | 12,269      | (45)  | -74,04                                     | -74,04                                     | 0  | 0,01                                     | 74,04                                     | 74,04                                     | 0  |  | -0,01 |
| 12   | 1     | O 762x13       | Somax | min          | Max. pos. torsie [I](1,000)  | 12,269      | (15)  | 1,78                                       | 1,78                                       | 0  | 0,06                                     | 1,78                                      | 1,79                                      | -0,03                                      |  | 0     |
| 24   | 1     | O 762x13       |       | min          | Max. pos. torsie [I](1,000)  | 12,269      | (30)  | 1,78                                       | 1,78                                       | 0  | 0,05                                     | 1,78                                      | 1,78                                      | -0,03                                      |  | 0     |
| 36   | 1     | O 762x13       |       | min          | Max. pos. torsie [I](1,000)  | 12,269      | (45)  | 1,78                                       | 1,78                                       | 0  | 0,06                                     | 1,78                                      | 1,79                                      | -0,03                                      |  | 0     |
| 24   | 1     | O 762x13       |       | max          | Comb. trek+torsie [I](1,000) | 0,736       | (362) | -47,19                                     | 129,59                                     | 0  | 0,89                                     | 24,37                                     | 129,59                                    | 0,45                                       |  | -0,12 |

**Prof.:** Profiel; **C:** Extreme component; **min, max.:** Extreme type; **Geval:** Belastinggeval van de extreme; **Pos.:** Lokale X-positie van de doorsnede op de staaf; **S<sub>x,min</sub>:** Doorsnede minimum normaalspanning; **S<sub>x,max</sub>:** Doorsnede maximum normaalspanning;

**V<sub>min</sub>:** Doorsnede minimum afschuifspanning; **V<sub>max</sub>:** Doorsnede maximum afschuifspanning; **S<sub>omin</sub>:** Doorsnede minimum Von Mises spanning; **S<sub>omax</sub>:** Doorsnede maximum Von Mises spanning; **V<sub>y,gem</sub>:** Afschuifspanning in lokale Y-richting; **V<sub>z,gem</sub>:** Afschuifspanning in lokale Z-richting;

**Project:**

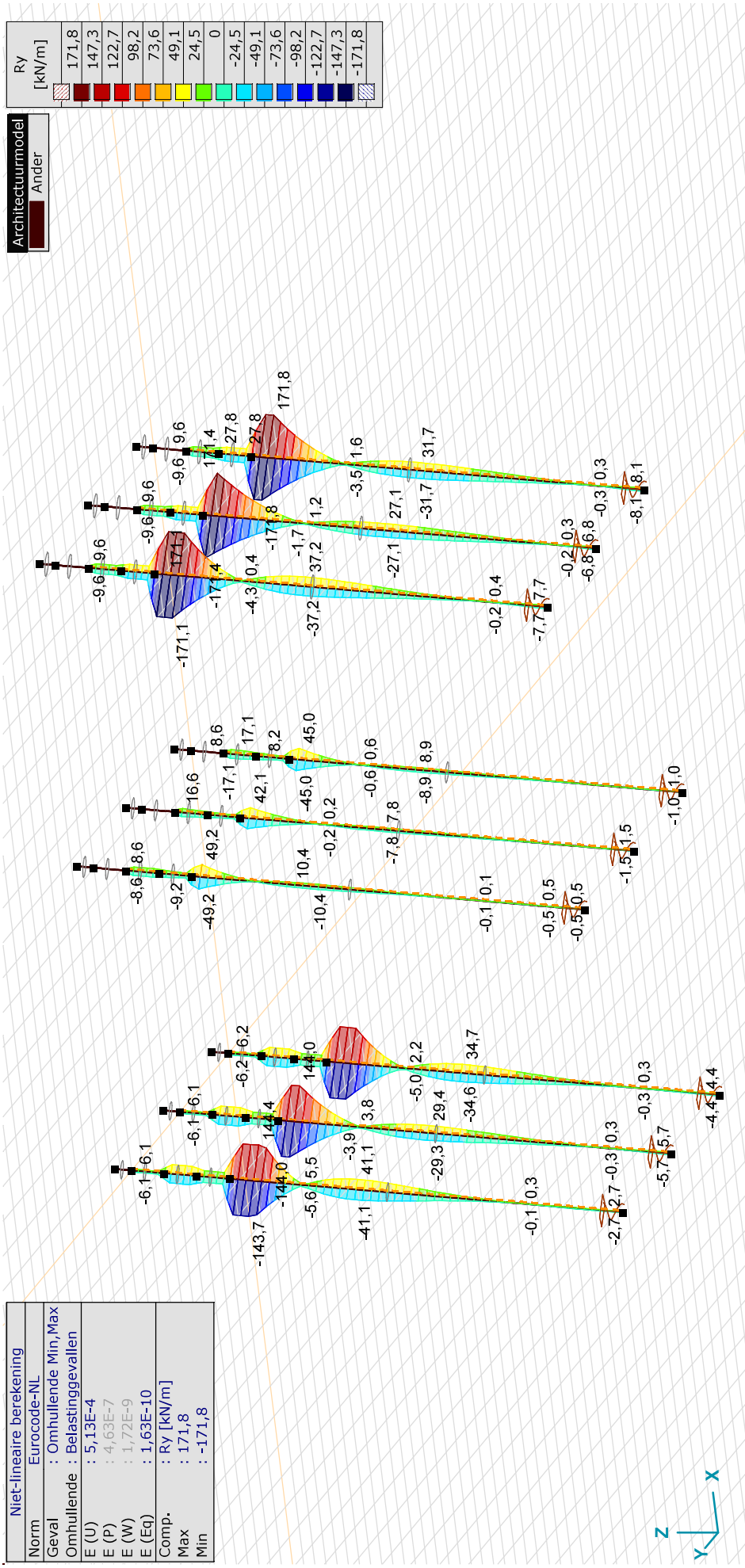
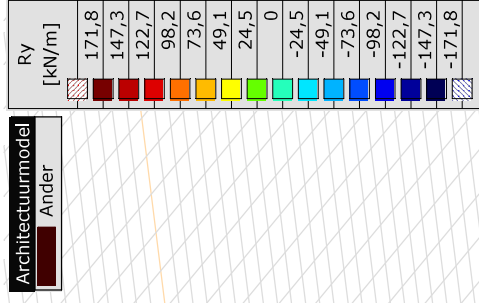
Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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| Niet-lineaire berekening |                      |
|--------------------------|----------------------|
| Norm                     | Eurocode-NL          |
| Geval                    | : Omhullende Min_Max |
| Omhullende               | : Belastinggevallen  |
| E (U)                    | : 5,13E-4            |
| E (P)                    | : 4,63E-7            |
| E (W)                    | : 1,72E-9            |
| E (Eq)                   | : 1,63E-10           |
| Comp.                    | : Ry [kN/m]          |
| Max                      | : 171,8              |
| Min                      | : -171,8             |



[II], Non-lin., Omhullende (Belastinggevallen), Onmiddellijke doorbuiging, Ry (lijnopp.), Lijnen (gevuld)

**Project:**

Constructeur: DNV GL - Energy

Model: 1-paals reconstructie 2-ct.axs

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**Interne krachten lijnoplegging [Non-lin., Omhullende (Belastinggevallen)]**

|      | Lijn      | Type      | C  | min.<br>max. | Geval                        | Knoop | Pos.<br>[m] | Ry<br>[kN/m] | Rz<br>[kN/m] |
|------|-----------|-----------|----|--------------|------------------------------|-------|-------------|--------------|--------------|
| Ext. |           |           |    |              |                              |       |             |              |              |
| 8    | Staafl 16 | Staafl r. | Ry | min          | Max. neg. torsie [1] (1.000) | 243   | 0,491       | -144,0       | -0,9         |
| 14   | Staafl 28 | Staafl r. |    | max          | Max. pos. torsie [1] (1.000) | 421   | 0,736       | 144,4        | 0,1          |
| 13   | Staafl 25 | Staafl r. | Rz | min          | Max. Trek [1] (1.000)        | 409   | 0,204       | 12,8         | -35,9        |
| 13   | Staafl 25 | Staafl r. |    | max          | Max. Druk [1] (1.000)        | 409   | 0,204       | 15,0         | 37,0         |

Lijn: Ondersteund lijnelement. Type: Opleggingsstype. C: Extreme component. min. max.: Extreme type. Geval: Belastinggeval van de extreme. Pos.: Lokale X-positie van de doorsnede op de staaf. Ry: Y-component opleggingsreactiekracht. Rz: Z-component opleggingsreactiekracht.

**Interne krachten lijnoplegging [Non-lin., Omhullende (Belastinggevallen)]**

|      | Lijn      | Type      | C  | min.<br>max. | Geval                        | Knoop | Pos.<br>[m] | Ry<br>[kN/m] | Rz<br>[kN/m] |
|------|-----------|-----------|----|--------------|------------------------------|-------|-------------|--------------|--------------|
| Ext. |           |           |    |              |                              |       |             |              |              |
| 16   | Staafl 32 | Staafl r. | Ry | min          | Max. neg. torsie [1] (1.000) | 478   | 0,245       | -49,2        | 3,3          |
| 16   | Staafl 32 | Staafl r. |    | max          | Max. pos. torsie [1] (1.000) | 478   | 0,245       | 49,2         | -4,3         |
| 16   | Staafl 32 | Staafl r. | Rz | min          | Max. Trek [1] (1.000)        | 478   | 0,245       | 8,5          | -25,8        |
| 16   | Staafl 32 | Staafl r. |    | max          | Max. Druk [1] (1.000)        | 478   | 0,245       | -7,8         | 36,6         |

Lijn: Ondersteund lijnelement. Type: Opleggingsstype. C: Extreme component. min. max.: Extreme type. Geval: Belastinggeval van de extreme. Pos.: Lokale X-positie van de doorsnede op de staaf. Ry: Y-component opleggingsreactiekracht. Rz: Z-component opleggingsreactiekracht.

**Interne krachten lijnoplegging [Non-lin., Omhullende (Belastinggevallen)]**

|      | Lijn      | Type      | C  | min.<br>max. | Geval                         | Knoop | Pos.<br>[m] | Ry<br>[kN/m] | Rz<br>[kN/m] |
|------|-----------|-----------|----|--------------|-------------------------------|-------|-------------|--------------|--------------|
| Ext. |           |           |    |              |                               |       |             |              |              |
| 6    | Staafl 12 | Staafl r. | Ry | min          | Max. neg. torsie [1] (1.000)  | 184   | 0,491       | -171,8       | -2,5         |
| 6    | Staafl 12 | Staafl r. |    | max          | Max. pos. torsie [1] (1.000)  | 184   | 0,491       | 171,8        | 22,0         |
| 18   | Staafl 36 | Staafl r. | Rz | min          | Comb. trek+torsie [1] (1.000) | 537   | 0,245       | 170,2        | -29,1        |
| 18   | Staafl 36 | Staafl r. |    | max          | Max. Druk [1] (1.000)         | 537   | 0,245       | -5,7         | 43,4         |

Lijn: Ondersteund lijnelement. Type: Opleggingsstype. C: Extreme component. min. max.: Extreme type. Geval: Belastinggeval van de extreme. Pos.: Lokale X-positie van de doorsnede op de staaf. Ry: Y-component opleggingsreactiekracht. Rz: Z-component opleggingsreactiekracht.



## **About DNV**

DNV is the independent expert in risk management and assurance, operating in more than 100 countries. Through its broad experience and deep expertise DNV advances safety and sustainable performance, sets industry benchmarks, and inspires and invents solutions.

Whether assessing a new ship design, optimizing the performance of a wind farm, analyzing sensor data from a gas pipeline or certifying a food company's supply chain, DNV enables its customers and their stakeholders to make critical decisions with confidence.

Driven by its purpose, to safeguard life, property, and the environment, DNV helps tackle the challenges and global transformations facing its customers and the world today and is a trusted voice for many of the world's most successful and forward-thinking companies.