



UPDATE OF BEST PRACTICES SEPARATION TECHNOLOGIES



Objective	Updating Best Practices Separation Technologies		
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Disclaimer

References have been obtained from renowned experts listed below.

Traxxys has mitigated the risk of missing out on latest developments by cross-checking different and – more importantly – international commercial as well as academic open sources from around the globe. Completeness has to be judged in the context of available time and budget.

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1. Objective

The objective is to update Best Practices of Membrane Technology, Liquid-Solid Separation Technology, Reactive Distillation and Dividing Wall Column Technology as well as the Introductory Webpage on Separation Technology of RVO.

2. Best Practices Structure

The BP structure applied below has been devised with the needs and concerns of the end user in mind. Most likely the end user is active in the process industry and he or she is working on a process related issue. Since nowadays many professionals in the process industries have an international background Traxxys has chosen to rewrite all BP's in the English language.

The interest and curiosity of the envisaged end user for a Best Practice offered by RVO on their website therefore come from a very practical – i.e. non-academic - background. There is an issue, it needs solving and there is time pressure. By screening lists of commercial applications, the end user can find out quickly, whether an application resembles his/her field of interest. If so, diving deeper into the matter makes sense and the BP accommodates that as well.

- a) Can this technology solve my issue?
- b) What are its specific costs and benefits?
- c) What are TRL-level, operational and safety risks?
- d) Examples?
- e) How does it work?
- f) Where can I find more information?

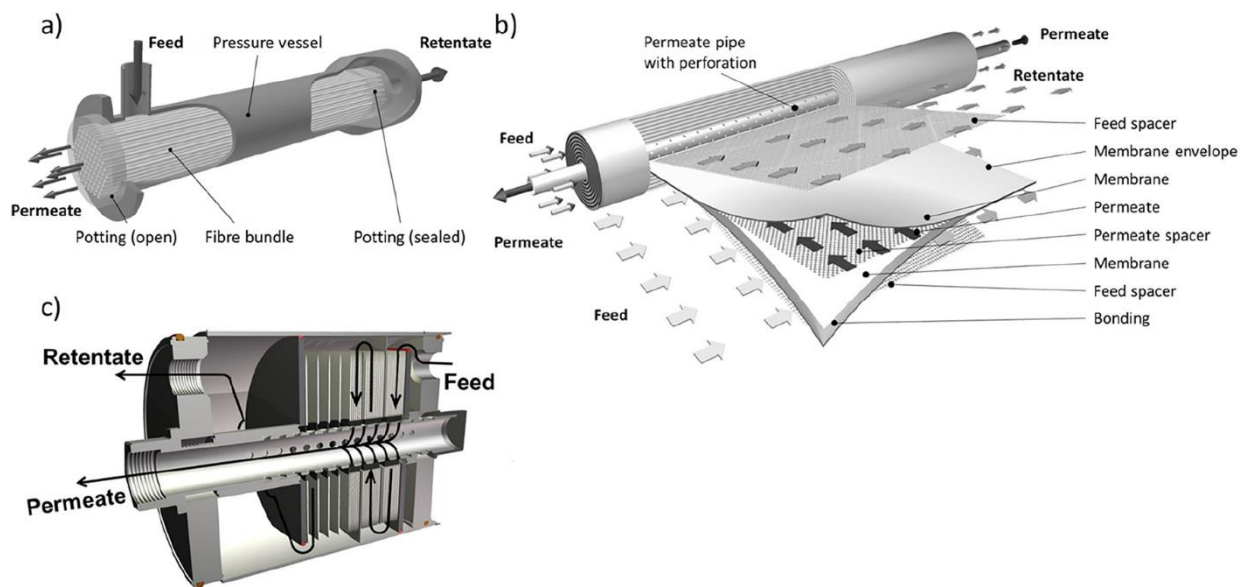
This translates into the following Best Practices structure:

1. Technology function what does it do?
2. Application window what are known applications with which I can compare my issue?
3. Operating window what temperatures / pressures / flow regimes / concentrations?
4. Benefits and Costs what are the profit incentives and how does compare with cost?
5. TRL and Risks is the technology mature? Does it involve HSE- / financial risks?
6. Working principle how does it work?
7. References where can I find more information?
8. Suppliers which companies sell this technology?



3. BP Membrane technology

Best Practice Membrane Technology



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- | | |
|-------------------------|---|
| 4.1 Technology function | what does it do? |
| 4.2 Application window | what are known applications with which I can compare my issue? |
| 4.3 Operating window | what temperatures / pressures / flow regimes / concentrations? |
| 4.4 Benefits and Costs | what are the profit incentives and how does compare with cost? |
| 4.5 TRL and Risks | is the technology mature? Does it involve HSE- / financial risks? |
| 4.6 Working principle | how does it work? |
| 4.7 References | where can I find more information? |
| 4.8 Suppliers | which companies sell this technology? |



4.1 Technology function

The function of membrane technology is to separate liquid/solid, liquid/liquid, liquid/gas and gas/gas mixtures.

4.2 Application window

This subchapter is meant to give an overview of areas where membrane technology is already commercially applied as a solution. The majority of membrane technology applications is associated with water. A minority of applications is associated with non-water solvent recovery but this area is expanding rapidly. Ref. 3 provides an excellent overview of the first subdivision:

4.2.1 Water associated applications

- Process water
- Drinking water
- Process water reuse
- Irrigation water
- Ultrapure water
- Foods and beverages
- Emergency water supply
- Car wash
- Cooling towers

4.2.2 Non-water associated applications (ref.4)

- Solvent recovery in pharma
- Solvent recovery in refining

4.2.1 Water associated applications

4.2.1.1 Process water

Boiler feed water
Boiler water consumption
Boiler make-up water
Boiler blowdown
Boiler water treatment
Characteristics of boiler feed water
Scaling
Corrosion
Foaming and priming
Oxygen attack
Carbon dioxide attack



- Membrane contractors
- Deaeration
- Ultrapure water
- Galvanic-Corrosion
- Caustic corrosion in boilers
- Silica Scaling in Boilers
- Filtration
- Cooling tower water consumption
- Cooling tower blowdown
- Cooling tower make-up water
- Cooling water data-center
- Cooling water quality
- Demineralized water
- Demi Water

4.2.1.2 Drinking water

- Condensate polishing
- Flue Gas Desulfurization
- FGD Wastewater Treatment
- FGD Wet Scrubber Systems
- FGD Equipment
- Removal of sulphate in Chloralkali process
- Chlorine production in chlor alkali industry
- Membrane cell process for chlor alkali production
- Removal of sulfate from chlor alkali brine by nano filtration
- Removal of sulphate in mining
- Salt recovery from sea water
- Spent caustic purification

4.2.1.3 Irrigation water

- Irrigation water quality
- Bicarbonate hazard of irrigation water
- Irrigation water lab analysis
- Nutrients in irrigation water
- Salinity hazard irrigation
- SAR hazard of irrigation water
- Toxic ions hazard of irrigation water
- Waste Water
- Anaerobic/aerobic treatment
- Biological excess sludge reduction
- Grey water recycling



4.2.1.4 Ultrapure water

- Mixed bed Ion exchange
- Water Conductivity
- Boiler feed water
- Demineralized process water
- Laboratory grade water
- Semiconductor
- Hemodialysis
- Hydrogen

4.2.1.5 Foods and Beverages

- Meat, poultry and seafood
- Fruits and vegetables
- Dairy
- Beverages

4.2.1.6 Emergency water supply

- Emergency potabilisation units
- Emergency seawater desalination units

4.2.1.8 Car wash water treatment

4.2.1.9 Cooling towers



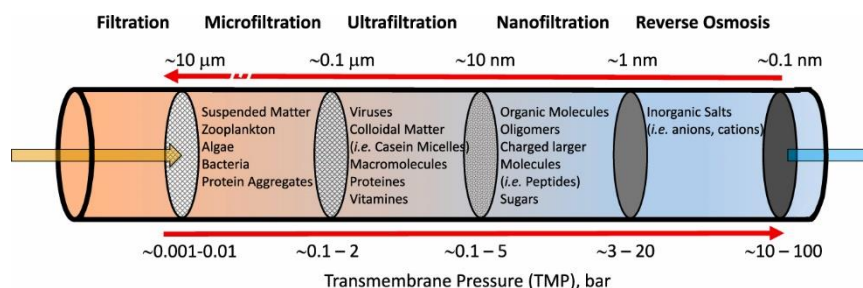
4.2.2 Non water associated applications

Industry	Solute/solvent	Membrane	Reference
Pharma	APIs/methanol	Starmem™120, Starmem™122, Puramem™228	Geens <i>et al.</i> ⁷³
Pharma	APIs/IPAc	Starmem™122, Starmem™240, Puramem™280	Rundquist <i>et al.</i> ⁶⁸
Pharma	APIs/crystallisation mother liquor (82% methanol, 15.9% methyl isobutyl ketone, 2.1% toluene) and ethyl acetate	Starmem™122	Rundquist <i>et al.</i> ¹⁰
Pharma	APIs/methanol and DCM	GMT-oNF-2	Szekely <i>et al.</i> ⁵²
Pharma	Peptide/MeCN and water	Inopor Nano 450 and 750	Marchetti <i>et al.</i> ⁷⁴
Refining	Waxy oil stream/toluene and methyl ethyl ketone	Starmem 228	White <i>et al.</i> ⁷⁵ Gould <i>et al.</i> ⁷⁶
Refining	Free fatty acids/methanol	Nitto Denko, Film-Tec, Osmonics, Desalination Systems, Fluid Systems	Raman <i>et al.</i> ⁷⁷
Refining	Oil/ <i>n</i> -hexane	PDMS/PAN	Stafie <i>et al.</i> ⁷⁸
Refining	Cotton oil/ <i>n</i> -hexane, IPA, ethanol	Romicon, Osmonic, Paterson Candy International	Koseoglu <i>et al.</i> ⁷⁹
Refining	Soybean oil/ <i>n</i> -hexane	Whatman (ceramic membrane)	Wu and Lee ⁸⁰
Refining	Free fatty acids/ soybean oil and <i>n</i> -hexane	Osmonics	Ribeiro <i>et al.</i> ⁴
Refining	Corn oil/ethanol	Koch, FilmTec, Osmonic-Desal, Hydranautics	Kwiatkowski <i>et al.</i> ⁸¹
Refining	Ethanol, isopropanol, acetone, cyclohexane, hexane	GE Osmonic, Nadir, Evonik MET and Solsep	Darvishmanesh <i>et al.</i> ⁸²
Refining	Vegetable oils/hexane	NTGS-2200	Manjula <i>et al.</i> ⁸³
Refining	Soybean oil/hexane	PDMS/PVDF and Zeolite PDMS/PVDF	Weibin <i>et al.</i> ⁸⁴
Refining	Free fatty acids/soybean oil and hexane	PDMS/PVDF and CA/PVDF	Firman <i>et al.</i> ⁸⁵
Refining	Free fatty acids/soybean oil and hexane	Nitto Denko, Film-Tec, Osmonics, Desalination Systems, Fluid Systems	Raman <i>et al.</i> ⁸⁶
Refining	Heavy boilers from a hydroformylation mixture	Puramem S 380, GMT ONF 1, GMT ONF 2, GMT NC 1	Micovic <i>et al.</i> ⁹

Note: references quoted above can all be found in master ref. 4 with their original number

4.2 Operating window

The picture below shows the pressure regimes at which the various membrane processes tend to operate (ref.11).





The temperature range for membrane processes is mainly dictated by the maximum temperature at which the membrane in question is fully stable without deterioration or performance loss.

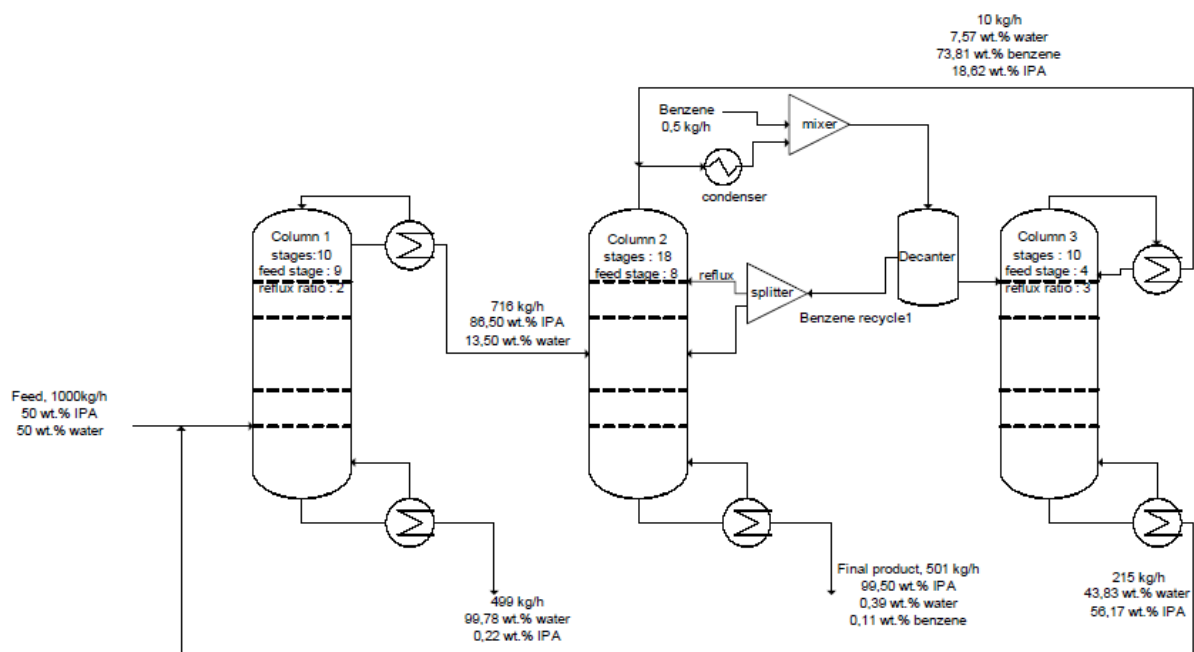
4.3 Benefits and Costs

4.3.1 Water associated applications

Energy saving most of the time is the primary benefit in water associated applications, especially when water evaporation can be avoided. Below you'll find two examples.

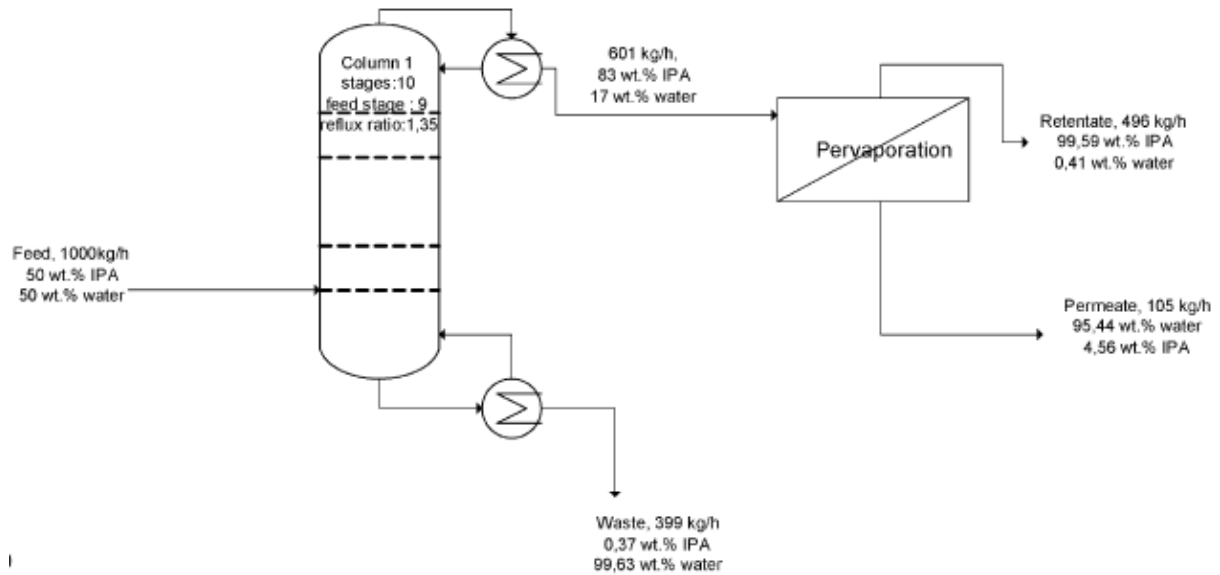
A. Energy saving in hybrid IPA dehydration (ref.6)

Traditional IPA dehydration by Extractive distillation





Hybrid IPA dehydration: Traditional up to azeotrope; membrane from azeotrope to pure IPA



Energy saving in hybrid IPA dehydration

	D-PV (polymeric)	D-PV (polymeric)	D-PV-D (polymeric)	D-PV-D (ceramic)	Azeotropic distillation
Cooling water costs (€/year)	4098	4098	9923	10030	15507
Steam costs (€/year)	52438	52678	98548	100774	103595
Permeate condensing costs (€/year)	5055	4856	4958	4800	NA
Total energy costs (€/year)	61591	61632	113428	115605	119102
Benzene costs (€/year)	NA	NA	NA	NA	13230
Operation costs (€/t product)	17.25	17.12	31.61	32.02	36.65

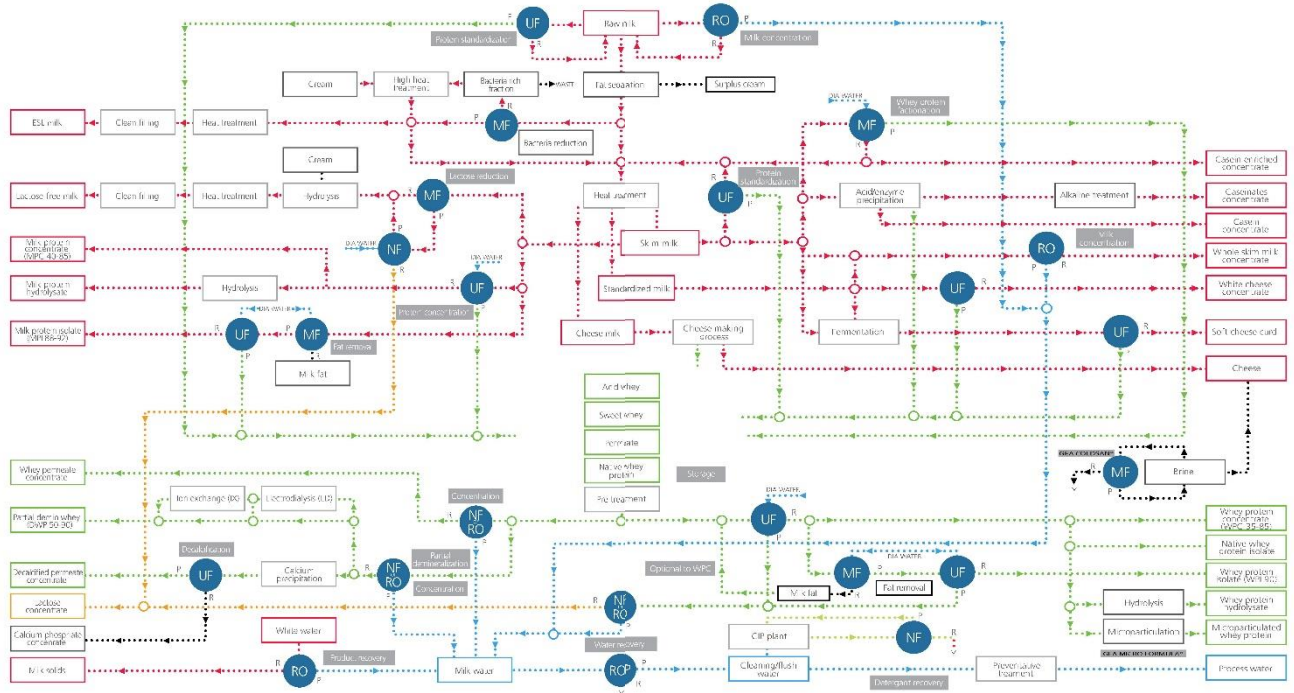
NA: not applicable.

Energy use of hybrid operation using polymeric membranes is 52% of conventional IPA dehydration using an entrainer like glycerol.



B. Energy saving in dairy industry (ref.7)

The figure below not only shows an overview of all relevant dairy process steps; it also shows where membrane separation steps can / have been introduced. On average, introducing a membrane process in a certain step increases energy efficiency of that step by 20-30%.



4.3.2 Non-water associated applications

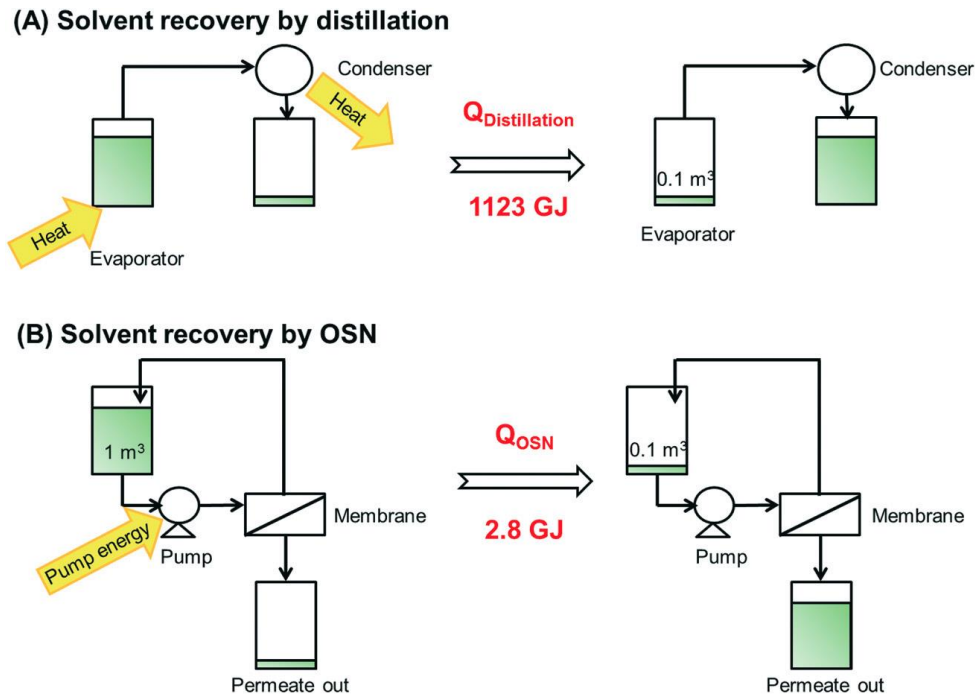
Energy use for solvent recovery by distillation vs. solvent recovery by Organic Solvent Nanofiltration (OSN) (ref. 4, p. 4456)

Solvent	Rank ⁶⁶	Solvent generated [10 ⁶ kg per year]	Q _{distillation} [kWh]	Q _{OSN} [kWh]	Q _{distillation} /Q _{OSN}	CO ₂ footprint [10 ⁶ kg per year]
Methanol	1	44.8	150	0.023	6453	18
Dichloromethane	2	22.3	111	0.014	8010	3
Toluene	3	12.1	197	0.021	9278	12
Acetonitrile	4	7.9	141	0.023	6029	3
Chloroform	7	3.71	131	0.012	10 543	0.4
n-Hexane	8	2.99	149	0.028	5300	3
n-Butyl alcohol	9	2.86	223	0.023	9788	2
DMF	10	2.79	244	0.019	12 569	2
N-Methyl-2-pyrrolidone	12	2.02	303	0.018	16 930	1
Xylene	13	1.47	208	0.021	9748	1
1,1,2-Trichloroethane	15	1.23	194	0.013	15 090	0.2
Methyl tert-butyl ether	16	1.2	126	0.025	5062	1
Ethylene glycol	18	0.82	337	0.017	20 285	0.3

Note: the carbon footprint was calculated for 70% solvent recovery after Kim e.a. (ref. 4 / 53)



An example of the potential of OSN for significant enhancement of energy efficiency is given in the example below. For recovering 451 tons of methanol by distillation the total energy consumption is 1123 GJ. The OSN set-up requires only 2.8 GJ @15 bara operating pressure which is more than 200 times less. (ref. 4, p. 4455).



4.4TRL-level and Risks

All membrane processes quoted in chapter 3.2 are commercial and TRL therefore is 9.

Still there are risks in applying membrane technology which can unexpectedly interfere with your operation. You will find these risks primarily in the area of concentration polarization and membrane fouling / scaling.

4.4.1 Concentration polarization

This phenomenon is an easily understood yet difficult to solve example of mass transfer limitation by counter diffusion. When a membrane does a proper job, it lets one or more components pass through, blocking one or more other components at the same time. These components cannot stay at the membrane surface: they have to diffuse back to the bulk of the mixture at the retentate side of the membrane. It is this back diffusion that hampers the components in easily passing through the membrane. Especially desalting processes like reverse osmosis suffer from this back diffusion which requires *higher* trans-membrane pressures to keep fluxes at a reasonable level.



From an engineering point of view one can think of a few solutions to reduce or eliminate concentration polarization. An obvious solution is to apply crossflow alongside the membrane causing high shear stress in the immediate area of the membrane surface. This ensures a) sweeping non-permeable components off the membrane surface and b) enhancing transport of permeable components to the membrane surface. This comes at the price of higher operational cost since more pumping energy has to be applied. In liquid phase operation pressure drops and associated pump energy will be limited. In gas phase operation these parameters can become significant since volumes in the gas phase tend to be orders of magnitude higher than in liquid phase.

Another solution is the use of turbulence promoters or static mixers, which positively affect mass transfer in the immediate vicinity of the membrane surface. Needless to say these promoters only work when crossflow is applied. They do not work if the mixture flow is perpendicular to the membrane surface. In that case they may even have an unintended opposite effect.

4.4.2 Scaling and fouling

Membrane fouling occurs when components from the feed stream deposit on the membrane surface or in the pores of the membrane. This can decrease the flux through the membrane or change the separation properties of the membrane. As a result, the energy efficiency of the membrane process decreases. In membrane fouling, a distinction is made between four types of fouling, being (i) colloidal (including silica, iron and aluminum oxides), (ii) scaling (including calcium carbonate and sulfate), (iii) organic (including oil, fats, proteins) and (iv) biologically (by bacterial growth). Each type of pollution requires its own approach. See references 8 and 9 for an overview.

4.5 Working principle

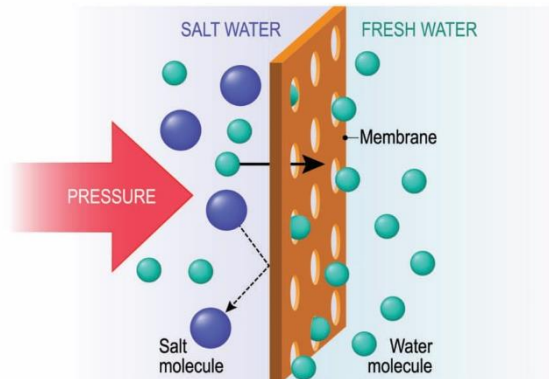
All membrane technologies have in common that when confronted with a mixture of molecules in liquid or gaseous state they show a preference for letting pass one type of molecule and holding back other type(s). They differ however in the type of driving force that governs the separation and in the exact transport phenomena that occur in the membrane material itself. The picture below (ref.5, page 3) shows the driving force can be:

- a) Hydraulic pressure
- b) Electrical voltage
- c) Concentration gradient
- d) Relative volatility



a) Hydraulic pressure

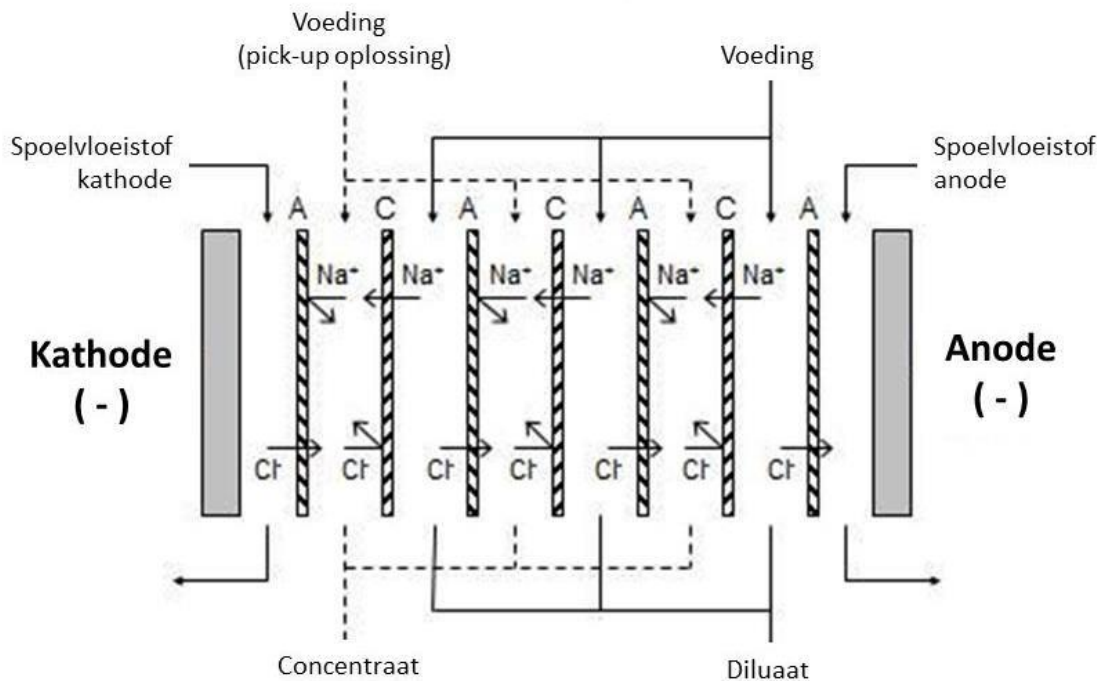
REVERSE OSMOSIS



By exerting a pressure on the left side of the membrane that exceeds the osmotic pressure resulting from the salt concentration difference across the membrane, water molecules are selectively transported through the membrane from left to right.

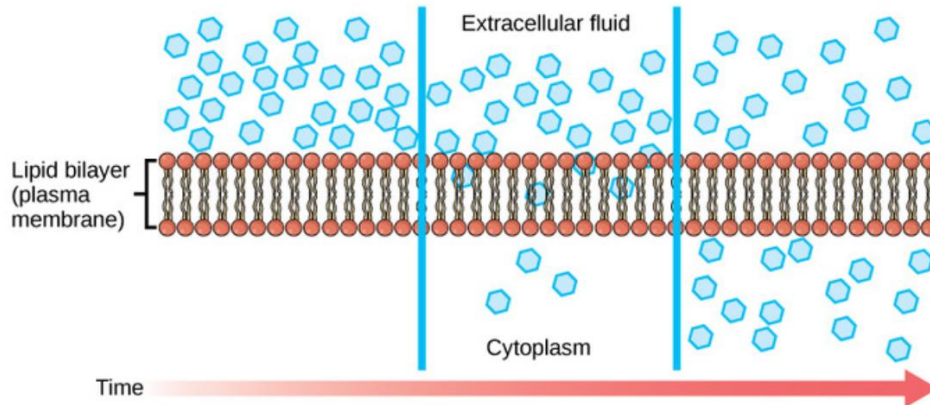
b) Electrical voltage (ref.10)

By applying a voltage difference, ions start moving in opposite directions. Since the membranes preferentially reject one type of ion and let the other type pass, a concentrating effect is obtained.





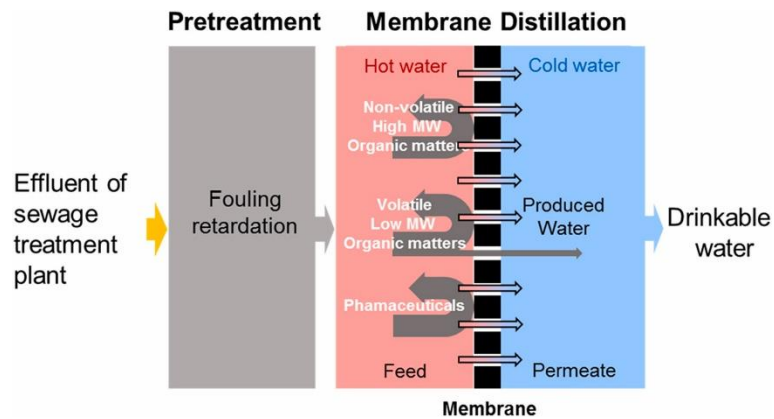
c) Concentration gradient (ref. 12)



Passive Transport: Diffusion is a type of passive transport. Diffusion through a permeable membrane moves a substance from an area of high concentration (extracellular fluid, in this case) down its concentration gradient (into the cytoplasm).

d) Relative volatility (ref.13)

Especially in membrane distillation processes, the relative volatility of components is a driving force. Components with low volatility are rejected; components with high volatility can pass the membrane.





4.6 References

1. 'Water treatment handbook' Vol. 1-2, Degremont, 1991
2. 'Industrial water conditioning', Betzdearborn, 1991
3. www.lenntech.com
4. Sustainability assessment of organic solvent nanofiltration: from fabrication to application Gyorgy Szekely, Maria F. Jimenez-Solomon, Patrizia Marchetti, Jeong F. Kim and Andrew G. Livingston; Green Chem., 2014, 16, 4440.

Sub-referenced articles in ref. 4:

- 73 J. Geens, B. De Witte and B. Van der Bruggen, Sep. Sci. Technol., 2007, 42, 2435–2449.
- 68 E. M. Rundquist, C. J. Pink and A. G. Livingston, Green Chem., 2012, 14, 2197–2205.
- 10 E. Rundquist, C. Pink, E. Vilminot and A. G. Livingston, J. Chromatogr., A, 2012, 1229, 156–163.
- 52 G. Szekely, M. Gil, B. Sellergren, W. Heggie and F. C. Ferreira, Green Chem., 2013, 15, 210–225.
- 74 P. Marchetti, A. Butté and A. G. Livingston, Reactive Peptide Nanofiltration, in Sustainable Nanotechnology and the Environment: Advances and Achievements, ed. N. Shamim and S. Virender, ACS Symp. Ser., 2013.
- 75 L. S. White and A. R. Nitsch, J. Membr. Sci., 2000, 179, 267–274.
- 76 R. M. Gould, L. S. White and C. R. Wildemuth, Environ. Prog., 2001, 20, 12–16.
- 77 L. P. Raman, M. Cheryan and N. Rajagopalan, J. Am. Oil Chem. Soc., 1996, 73, 219.
- 78 N. Stafie, D. F. Stamatialis and M. Wessling, J. Membr. Sci., 2004, 228, 103–116.
- 79 S. S. Koseoglu, J. T. Lawhon and E. W. Lusas, J. Am. Oil Chem. Soc., 1990, 67, 315–322.
- 80 J. C. Wu and E. Lee, J. Membr. Sci., 1999, 154, 251–259.
- 4 A. P. B. Ribeiro, J. M. L. N. de Mouraa, L. A. G. Goncalves, J. C. C. Petrus and L. A. Viotto, J. Membr. Sci., 2006, 282, 328–336.
- 81 J. R. Kwiatkowski and M. Cheryan, J. Am. Oil Chem. Soc., 2005, 82, 221–227.
- 82 S. Darvishmanesh, T. Robberecht, P. Luis, J. Degréve and B. Van der Bruggen, J. Am. Oil Chem. Soc., 2011, 88, 1255–1261.
- 83 S. Manjula, H. Nabetani and R. Subramanian, J. Membr. Sci., 2011, 366, 43–47.
- 84 C. Weibin, S. Yanzhi, P. Xianglan, L. Jiding and Z. Shenlin, Chin. J. Chem. Eng., 2011, 19, 575–580.
- 85 L. R. Firman, N. A. Ochoa, J. Marchese and C. L. Pagliero, J. Membr. Sci., 2013, 431, 187–196.
- 86 L. P. Raman, M. Cheryan and N. Rajagopalan, Lipids, 1996, 98, 10–14.
- 9 J. Micovic, K. Werth and P. Lutze, Chem. Eng. Res. Des., 2014, DOI: 10.1016/j.cherd.2014.02.012.
- 66 C. S. Slater, M. J. Savelski, W. A. Carole and D. J. C. Constable, in Green Chemistry in the Pharmaceutical Industry, ed. P. J. Dunn, A. S. Wells and M. T. Williams, Wiley-VCH Verlag GmbH & Co., Weinheim, 2010, ch. 3, pp. 49–82.
- 53 J. F. Kim, G. Szekely, I. B. Valtcheva and A. G. Livingston, Green Chem., 2014, 16, 133–145.



5. Membrane Technologies in Wastewater Treatment: A Review
Elorm Obotey Ezugbe and Sudesh Rathilal Department of Chemical Engineering, Faculty of Engineering and the Built Environment, Durban University of Technology, Durban 4000, South Africa; rathilals@dut.ac.za. *Membranes* 2020, 10(5), 89
6. Economic comparison between azeotropic distillation and different hybrid systems combining distillation with pervaporation for the dehydration of isopropanol; Veerle Van Hoof, Liesbet Van den Abeele, Anita Buekenhoudt, Chris Dotremont, Roger Leysen Vito (Flemish Institute for Technological Research), Process Technology, Boeretang 200, B-2400 Mol, Belgium Received 6 January 2003; received in revised form 17 July 2003; accepted 1 August 2003
7. Membrane filtration in the Dairy industry; GEA.com. chrome-extension://efaidnbnmnnibpcajpcglclefindmkaj/viewer.html?pdfurl=https%3A%2F%2Fwww.gea.com%2Fen%2Fbinaries%2Fmembrane-filtration-in-dairy-industry_tcm11-17109.pdf&clen=1455289&chunk=true
8. A.C.M. Franken; Prevention and Control of Membrane Fouling: Practical Implications and Examining Recent Innovations; DSTI report 2009. <http://www.ispt.eu/media/CS-01-02-Final-report-Prevention-and-reduction-of-membrane-fouling.pdf>
9. L.Y. Dudley; Membrane Autopsies for Reversing Fouling in Reverse Osmosis; *Membrane Technology* 95 (1998) 9-12.
10. Electrodialysis:
<http://www.aquanederland.nl/Afvalwaterportal/Zuiveringstechnieken/Elektrodialyse>
11. Fabrication and function of polymer membranes, Volker Abetz, Torsten Brinkmann and Mustafa Sözbilir, *Chemistry Teacher International*
<https://doi.org/10.1515/cti-2020-0023>
12. Concentration gradient over membrane: <https://courses.lumenlearning.com/boundless-biology/chapter/passive-transport/>
13. Feasibility of membrane distillation process for potable water reuse: A barrier for dissolved organic matters and pharmaceuticals, SeongpilJeong, Kyung GuenSong, JunkiKim, JaewonShin, Sung KyuMaeng, JoonhongPark, *Journal of Hazardous Materials* Volume 409, 5 May 2021, 124499



4.7 Suppliers

Manufacturers of pressure vessels

LENNTECH

WATER TREATMENT SOLUTIONS Pressure Vessels



Bel Pressure Vessels



Codeline Pressure Vessels



Knappe Pressure Vessels



Pentair Pressure Vessels



Phoenix Pressure Vessels



Protec Bekaert Pressure Vessels



Membranes / Vessels



PWG Membrane Housings

Closed Circuit Reverse Osmosis:



Reflex



Suppliers of membrane spare parts

Membrane adapters

i-lec for Filmtec membranes

Parts for RO systems

Additional information

Competitive Membrane Comparison Guide

Competitive Membrane Comparison Guide NEW

Reverse Osmosis Chemicals

RO cleaning Chemicals

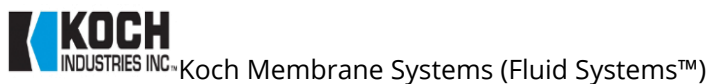
Antiscalant Chemicals (Avista-Vitec)

Antiscalant Chemicals (ROPUR)

GE-Water-Antiscalants

Scaling and Antiscalant

Membrane brands





Inge Membranes



Parker Membranes



Ropur Membranes



TriSep Membranes



Axeon Membranes



Millipore Membranes



LewaBrane Membranes



Pentair RO Membranes



Microdyn Nadir



OLTREMARE
LIQUID SEPARATION

OLTREMARE



LG Chem *Nano*:H₂O

LG RO Elements



Mann + Hummel



membranum
RM Nanotech

Membranum



FILTRATION DIVISION

Porex Membranes



Synder Membranes



Akkim Membranes



Siemens Membrane

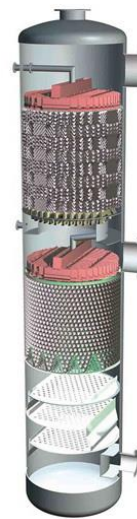


4. BP Reactive distillation

BEST PRACTICE REACTIVE DISTILLATION



®Katapak SP – Sulzer Chemtech



® Sulzer Chemtech – distillation tower with different kind of internals

- | | |
|-------------------------|---|
| 5.1 Technology function | what does it do? |
| 5.2 Application window | what are known applications with which I can compare my issue? |
| 5.3 Operating window | what temperatures / pressures / flow regimes / concentrations? |
| 5.4 Benefits and Costs | what are the profit incentives and how does compare with cost? |
| 5.5 TRL and Risks | is the technology mature? Does it involve HSE- / financial risks? |
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| 5.8 Suppliers | which companies sell this technology? |



5.1 Technology function

The function of reactive distillation (RD) is twofold: first to convert feedstocks into product(s) and second to separate product(s) from feedstocks and from each other.

5.2 Application window

Industrial applications are listed below (ref. 1,16).

Reaction type	Catalyst / internals
<p>Alkylation Alkyl benzene from ethylene/propylene and benzene Motor fuel alkylate production</p>	Zeolite β , molecular sieves Sulphuric Acid
<p>Amination Amines from ammonia and alcohols</p>	H ₂ and hydrogenation catalyst
<p>Carbonylation Acetic acid from CO and methanol / dimethyl ether</p>	Homogeneous
<p>Condensation Diacetone alcohol from acetone Bisphenol-A from phenol and acetone Trioxane from formaldehyde</p>	Heterogeneous N/A Strong Acid catalyst, zeolite ZSM-5
<p>Esterification Methyl acetate from methanol and acetic acid Ethyl acetate from ethanol and acetic acid 2-methyl propyl acetate from 2-methyl propanol and acid Butyl acetate from butanol and acetic acid Fatty acid methyl esters from fatty acids and methanol Fatty acid alkyl esters from fatty acids and alkyl alcohols Cyclohexyl carboxylate from cyclohexene and acids</p>	H ₂ SO ₄ , Dowex 50, Amberlyst-15 N/A Katapak-S Cation exchange resin H ₂ SO ₄ , Amberlyst-15, Metal oxides H ₂ SO ₄ , Amberlyst-15, Metal oxides Ion exchange resin bags
<p>Etherification MTBE from isobutene and methanol MTBE from isobutene and methanol ETBE from isobutene and ethanol</p>	Amberlyst-15 Undisclosed catalytic internals Amberlyst-15 / pellets, structured



TAME from isoamylene and methanol
 TAME from isoamylene and methanol
 DIPE from isopropanol and propylene
 TAEI from C5 feeds and ethanol

Ion exchange resin
 CD IsoTAME catalyst, internals
 ZSM 12, Amberlyst-36, zeolite
 Ion exchange catalyst

Hydration / Dehydration

Mono ethylene glycol from ethylene oxide and water

Homogeneous

Hydrogenation / Dehydrogenation

Cyclohexane from benzene
 MIBK from benzene
 Butenes from butadiene
 Propene from MA/PD

Alumina supported Ni catalyst
 Cation exchange resin with Pd/Ni
 CDModules®
 CDHydro

Hydrolysis

Acetic acid and methanol from methyl acetate and water
 Acrylamide from acrylonitrile
 Isobutene from MTBE

Ion exchange resin bags
 Cation exchanger, copper oxide
 CDIB catalyst

Isomerization

Iso-paraffins from n-paraffins
 Isoamylenes from normal pentenes

Chlorinated alumina and H2
 Zeolite catalyst

Nitration

4-Nitrochlorobenzene from chlorobenzene and nitric acid

Azeotropic removal of water

Transesterification

Ethyl acetate from ethanol and butyl acetate
 Diethyl carbonate from ethanol and dimethyl carbonate
 Vinyl acetate from vinyl stearate and acetic acid

Homogeneous
 Heterogeneous
 N/A

Unclassified reactions

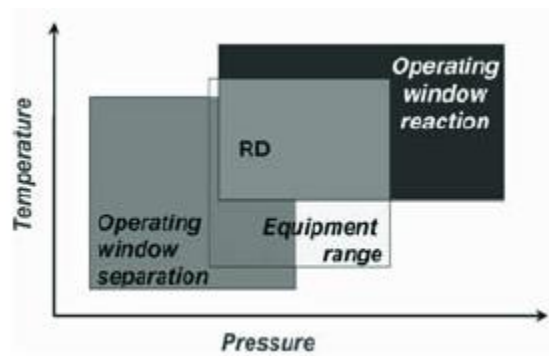
Monosilane from trichlorosilane
 Methanol from syngas
 DEA from monoethanolamine and ethylene oxide
 Polyesterification

Heterogeneous
 Cu/Zn/Al2O3 and inert solvent
 N/A
 Autocatalytic



5.3 Operating window

The operating window of RD is dictated both by the occurring reaction between feedstocks and by the required separation of products. Ideally, one product is the lightest and the other product is the heaviest, with the reactants being the intermediate boiling components (ref.3). Moreover, as both operations occur simultaneously in the same unit, there must be a proper match between the temperatures and pressures required for reaction and separation (ref.4,5). A low temperature yielding high relative volatilities may lead to low reaction rates requiring large amounts of catalyst or liquid holdups to achieve the required conversion. In contrast, a high temperature may promote side reactions or move the equilibrium to the feedstock side making it difficult to drive the reaction to completion.



If there is no significant overlap of the operating envelopes of reaction and separation the combination of reaction and distillation is not possible. An obvious example of the latter is the combination of a high pressure reaction and a vacuum distillation.



5.4 Benefits and Costs

The first benefit of RD is capex reduction. Instead of designing and erecting separate reactors and distillation columns, RD requires only one integrated column. This saves investment in separate reactors, erection structures, piping, heat exchangers and possibly pumps.

The second benefit of RD is in opex reduction. Thermodynamically, the repeated short-length sequence of reaction immediately followed by separation has a higher efficiency than the gross approach of reacting / separating / reacting / etc. in different vessels interconnected with piping.

5.5 TRL and Risks

All quoted examples in chapter 2 are TRL 9.

The main risk associated with reactive distillation comprises the operational controllability of steady state and dynamic behavior of the column. Underlying causes are a) the high degree of non-linearity of reaction-distillation systems in general; b) the limited amount of in-process information like local temperatures and local concentrations of feedstocks and products in column, overhead condenser and reboiler; c) the limited amount of independent process variables available to the operator for steering column performance in the desired direction. Ref. 7-13 give you more background info.

Of these underlying causes, a proper understanding of occurrence and impact of non-linearity is the most important factor. This precedes the design phase of the column. Non-linearity is inherent to the chemical reaction occurring. Local reaction rates are affected by local temperature, local pressure, local feedstock concentrations and catalyst activity. Of these, temperature dependency is always non-linear and concentration dependency can be, depending on the order of the reaction involved.

In this context, imperfect reactant mixing, surface wetting, and/or spatial catalyst activity variations will certainly cause spatial differences in reaction rate. In the case of endothermic reactions, higher rates will cause temperatures to drop which has a mitigating effect on local column temperature swings. In the case of exothermic reactions higher rates will cause temperatures to increase. This in turn will lead to even higher reaction rates. At the same time, higher temperatures promote evaporation of the most volatile component, leading to lower concentrations in the liquid phase of that specific component which can be mitigating.

This brief analysis merely serves to illustrate the need for a thorough understanding of the static and dynamic behavior of combined reaction-distillation steps before entering the design phase of an RD column. It also shows the need for local process information – especially information about local temperatures and local component concentrations. With the advent of cost effective sensors over the past decade, new windows of opportunity have opened up (ref.14,15).



Finally, looking at conventional independent column control parameters, the operator can only steer or affect reboiler duty, reflux ratio, column pressure, feed temperature and feed composition. These parameters will more or less instantaneously affect top, bottom and feed entry areas of the column, but they cannot instantaneously control e.g. temperature excursions somewhere in the intermediate areas of the column. For these intermediate areas to stay inside their operating envelope it is mandatory the reaction-distillation combination is intrinsically stable.

5.6 Working principle

Although hardware designs of reactive distillation columns may look significantly different from one vendor to the next, the working principle invariably is the same.

Somewhere in the column there is catalyst. In most instances the catalyst is heterogeneous. In some instances, homogeneous catalysis is applied in the liquid phase. When feedstocks come in contact with the catalyst, reaction to products takes place. Separation of these products from feedstocks subsequently follows in the immediate vicinity of the reaction area.

Basically there are two classes of hardware designs. They differ in the way the catalyst area and the separation area are located relative to one another. Structured packing with a catalytic surface is one extreme. A set of conventional catalyst loaded distillation trays is the other extreme.

Looking more closely to these hardware layouts one can state that structured packing enables reaction-separation on a micro-scale, whereas catalyst loaded distillation trays enable reaction-separation on a macro-scale. This suggests structured packing will be more effective than conventional catalyst loaded trays for a given equivalent column height, provided the liquid residence time on the catalyst surface of the structured packing is not limiting.

The final choice between these two hardware layouts depends on *technical* factors like:

- ability to coat the structured packing with catalyst
- required residence time of the reaction mixture in contact with the catalyst surface
- achievable liquid hold-up of conventional trays
- required radial and axial heat transfer for temperature control
- allowable pressure drop over the column
- etc.

and on *economical* factors like:

- purchase cost of equipment of structured packing versus conventional trays
- availability of hardware in the required diameters / heights
- maintenance of packing / tray replacement
- replacement of catalyst
- etc.



5.7 References

1. "Advanced Distillation Technologies: Design, Control and Applications", A.A. Kiss, Wiley-Blackwell, ISBN 978-1-1199-9361-2 (2013), Chapter 10 Reactive Distillation
2. "Reactive distillation: The front-runner of industrial process intensification A full review of commercial applications, research, scale-up, design and operation", G.J. Harmsen, Chemical Engineering and Processing 46 (2007) 774-780
3. "Reactive Distillation Design and Control" William L. Luyben, Cheng-Ching Yu, First published: 29 January 2008, Print ISBN:9780470226124 |Online ISBN:9780470377741 |DOI:10.1002/9780470377741
4. "Modelling of reactive separation processes: reactive absorption and reactive distillation" C. Noeres, E.Y. Kenig, A. Górak, Chemical Engineering & Processing: Process Intensification > 2003 > 42 > 3 > 157 - 178
5. "Preliminary Design of Reactive Distillation Columns", R. Thery, X.M. Meyer, X. Joulia, M. Meyer; Chemical Engineering Research and Design, Volume 83, Issue 4, April 2005, Pages 379-400
6. www.sulzer.com/en
7. "A new class of control structures for heterogeneous reactive distillation processes Mihai Daniel Moraru, Iulian Patrascu, Anton A. Kiss, Costin Sorin Bildea; Chemical Engineering and Processing - Process Intensification Volume 171 Published - 2022
8. Al-Arfaj M., Luyben W. L., Comparison of alternative control structures for an ideal two-28 product reactive distillation column, Industrial & Engineering Chemistry Research, 39 29 (2000), 3298-3307. 30
9. Al-Arfaj M., Luyben W. L., Control of ethylene glycol reactive distillation column, 31 AIChE Journal, 48 (2002), 905-908. 32
10. Bildea C. S., Kiss A. A., Dynamics and control of a biodiesel process by reactive 33 absorption, Chemical Engineering Research and Design, 89 (2011), 187-196.
11. Harmsen G. J., Reactive distillation: The front-runner of industrial process intensification. 16 A full review of commercial applications, research, scale-up, design and operation. 17 Chemical Engineering and Processing: Process Intensification. 46 (2007), 774-780. 18
12. Huang S. G., Kuo C. L., Hung S. B., Chen Y. W., Yu C. C., Temperature control of 19 heterogeneous reactive distillation, AIChE Journal, 50 (2004), 2203-2216.
13. Luyben W. L., Yu C. C., Reactive distillation design and control, Wiley-AIChE, New York, 2008.
14. <https://www.danfoss.com/en/products/sen/sensors-and-transmitters/industrial-temperature-sensors/#tab-overview>
15. <https://www.honeywell.com/us/en/industries/products#sensing-and-iot>
16. Lummus - CD Tech RD portfolio:
<https://www.yumpu.com/en/document/view/52709669/mtbe-steam-sheet-cdtech>
17. Oral communication mr. F. Nulle, CEO of Sulzer NL - H.N. Akse of Traxxys on February 7th 2022.



5.8 Suppliers

1. Sulzer Chemtech

Katapak

<https://www.sulzer.com/en/products/separation-technology/structured-packings>

Sulzer offers all sorts of column internals. When asked (ref.17) the company stated on the record they can deliver complete RD columns including internals. They do not see it as a separate type of product next to conventional distillation columns with structured packing.

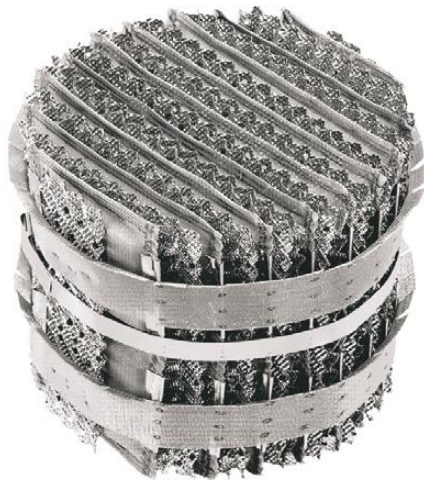
2. Lummus (has acquired the CDTech RD portfolio previously owned by CB&I)

<https://www.yumpu.com/en/document/view/52709669/mtbe-steam-sheet-cdtech>

3. Koch-Glitsch

Katamax reactive distillation structured packing:

<https://koch-glitsch.com/search-results?searchtext=reactive+distillation&searchmode=exactphrase>



Koch Glitsch – Katamax



Sulzer – Katapak

Images of Lummus hardware internals are absent in the public domain. However, from CDTech's original portfolio all RD-technologies and Process flow diagrams are available in the public domain (ref.16). The most straightforward designs are shown down below.



Looking more closely at the Katapak and Katamax internals we see large differences.

The Katapak design is clearly inspired by Sulzer's broad range of structured internals for distillation columns (like Mellapak, Mellapak plus, Mellapak CC, BX, BX plus, CY, CY plus, Mellacarbon, Mellagrid, etc.). This ensures optimal wetting of the surface; low gas phase pressure drop and proper mass transfer between liquid and gas phase. It also means liquid holdup on the surface is low compared to conventional distillation trays, leading to relatively low liquid residence times at the catalyst surface compared to trays.

The Katamax design has the appearance of a conventional distillation tray which has been filled with open gauze envelopes containing catalyst. Depending on the percentage of cross sectional void area of the tray bottom, one can expect to be able to create significant residence time of the liquid phase in close contact with the catalyst.

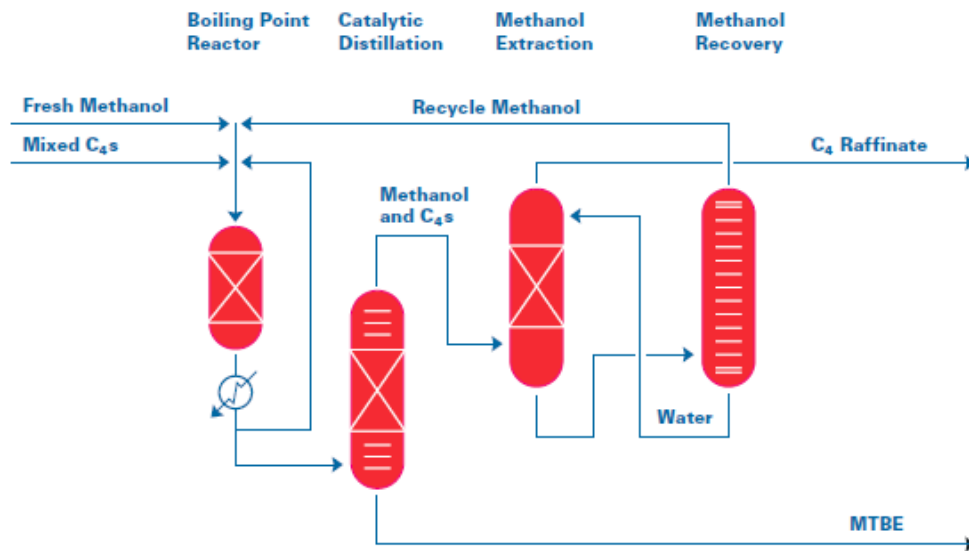
A *cautious* conclusion can be, one type would be the preferred choice for fast reactions (low residence time suffices) while the other type would be the preferred type for slow reactions (higher residence times required).

This is the Lummus / CDTech RD technology portfolio.

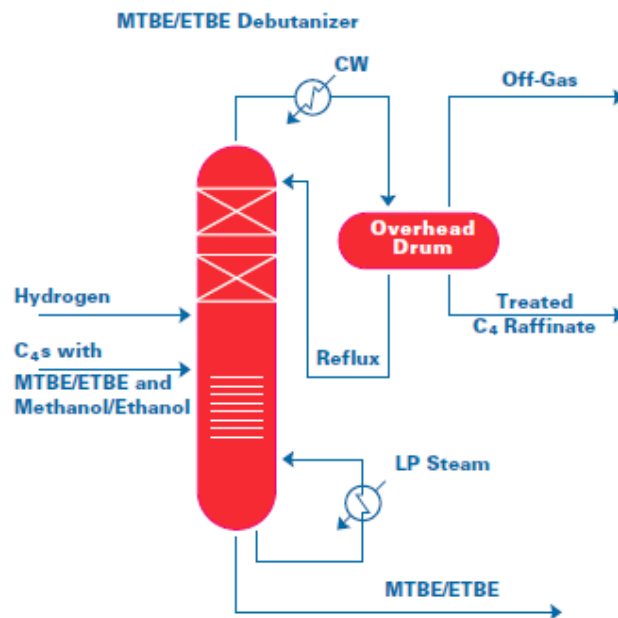
- MTBE From Steam Cracker and Dehydro C4 Feeds
- Selective Hydrogenation of MTBE/ETBE C4 Raffinates
- Isobutylene from MTBE Decomposition
- Advanced Sulfuric Acid Catalyzed Alkylation
- Process for the Production of Motor Fuel Alkylate
- Selective Hydrogenation of MAPD
- Selective Hydrogenation of Refinery C4 Feeds
- Increased TAME From Refinery and Steam Cracker C5 Feeds
- Isoamylenes Production from Normal Pentenes
- TAEE from Refinery C5 Feeds



CDM_{tb}e Process Flow Diagram

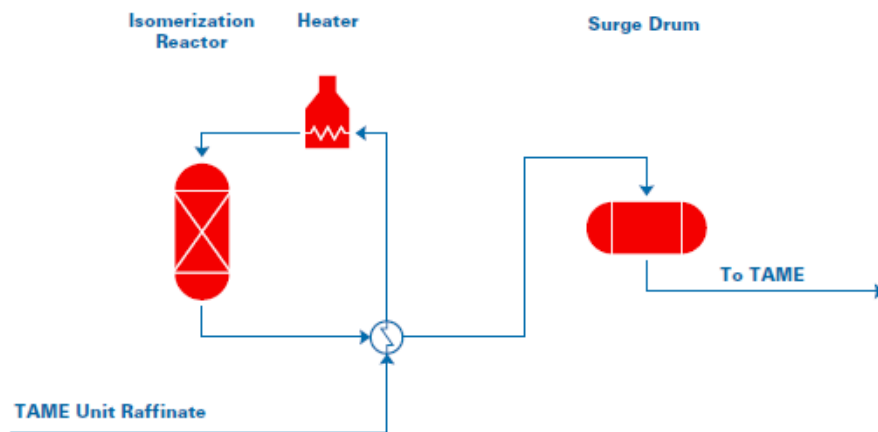


CDHydro Process Flow Diagram





ISOMPLUS Process Flow Diagram





5. BP Liquid / solid separation

Best Practice Liquid / Solid Separation



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- 6.1 Technology function
- 6.2 Application window
- 6.3 Operating window
- 6.4 Benefits and Costs
- 6.5 TRL and Risks
- 6.6 Working principle
- 6.7 References
- 6.8 Suppliers

- what does it do?
- what are known applications with which I can compare my issue?
- what temperatures / pressures / flow regimes / concentrations?
- what are the profit incentives and how does compare with cost?
- is the technology mature? Does it involve HSE- / financial risks?
- how does it work?
- where can I find more information?
- which companies sell this technology?



6.1 Technology function

Liquid - solids separation is a mechanical separation method in which a liquid - solid mixture is separated into a solid (with as little adhering liquid as possible) and a liquid (with as little solid as possible).

This BP relates to processes in which a lot of solids are present in the liquid. The size of the solid particles is in the order of 10 to 500 μm . For filtration of particles $< 1 \mu\text{m}$, reference is made to the Best Practice Membrane Technology.

6.2 Application window

General rules

To evaporate 1 kg of water in a dryer at least 3000 kJ is needed. Any liquid that can be removed mechanically does not need to be evaporated into the dryer.

Vacuum filters are often used as liquid - solids separator, because they are simple devices on which the filter cake can be washed properly if desired. A disadvantage of these filters is the high final moisture content.

There are several methods for further dehumidifying a filter cake (gas blow-through, centrifugation, roll presses) each with advantages and disadvantages. The choice is usually determined by the existing systems and/or the requirements for the solid or liquid.

The driving force when dehumidifying by blowing gas through is a difference in gas pressure over the filter cake, whereby the interstitial liquid can only be emptied when the gas pressure is higher than the capillary pressure. This method is mainly used for open porous structures.

Particles of 100 μm and larger, which do not deform too much and do not fall apart, can be dehumidified well in a continuously filtering centrifuge with a short residence time.

For smaller particles (approx. 20 μm), a discontinuous centrifuge should be used for proper dehumidification (centrifugal force of approximately 2000*g; residence time of a few minutes).

Gas blow-through and centrifuges are mainly used when a cake is compactly stacked with dimensionally stable, non-porous particles.

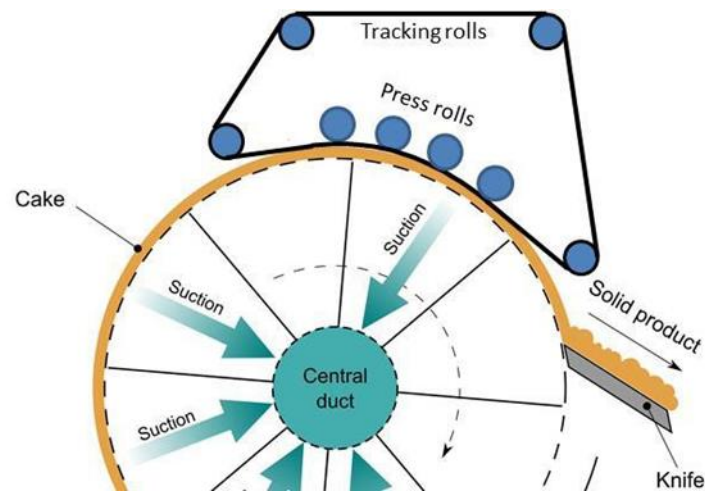
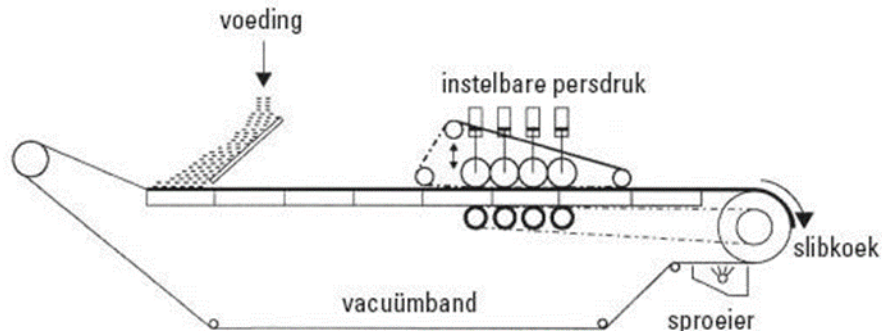
Pressing devices (such as belt press, screw press and diaphragm filter press) squeeze the liquid out of a filter cake. This method is especially beneficial if the particles are porous (by themselves porous, agglomerated or flocculated particles) and/or deformable and/or the original filter cake has a more open structure.



When applying only presses, the interstitial spaces between the particles are filled with liquid after the process. A combination of pressing and blowing can then offer advantages.

Examples of applications

- Roll presses on vacuum belt filter and on rotating vacuum filter



- Filter press machine

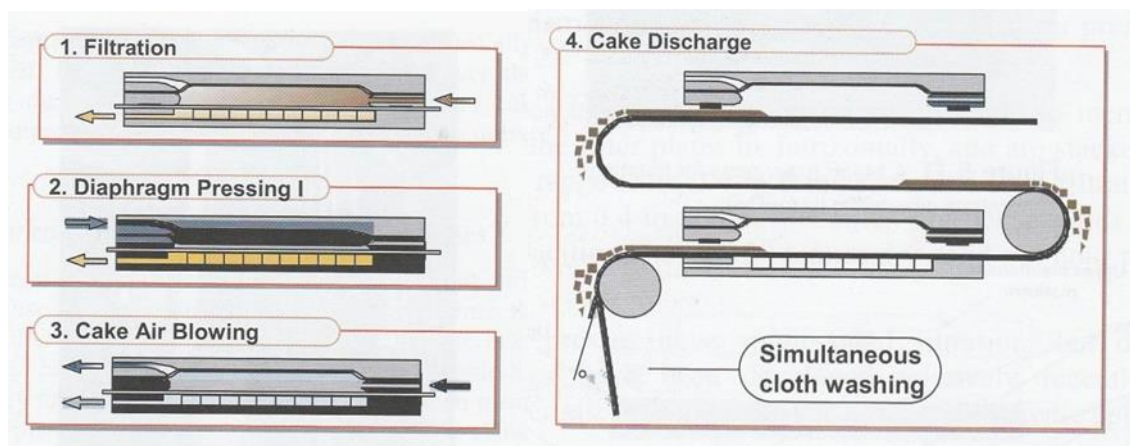
With a filter press machine, the position of the filter cloth is horizontal, so that the filter cake can be pressed, washed, possibly re-pressed, blown dry and unloaded.

Filter press machines are used in various applications. An example is a slurry of solids (waste) in a solvent. In the original process, the slurry was dried in a contact dryer. Because the dried substance contained traces of organic solvent, it was disposed of as chemical waste.



Replacement of the contact dryer by a diaphragm filter press machine, in which the filter cake is washed and then squeezed into a sting-resistant cake with a moisture content of 1.5 kg of moisture per kg of dry matter has meant that the cake could be dumped in designated places without further treatment.

Different process steps of the filter press machine (ref.3)



Another example stems from the starch industry. Here filter press machines replace vacuum filters or decanter centrifuges. The advantage is that the filter press machines generally achieve a 10% lower final moisture content than the centrifuges, which in turn results in energy and investment savings in the dryer.

- Press-blowing installation

With the pressure rollers on a belt filter, the cloth with the cake moves continuously. In a press-blowing installation, the cloth is transported discontinuously with the cake: the cake is pressed with a porous pressure plate and then gas (air) is blown through the cake. This system is mainly used in filter cakes whose rheology has thixotropic properties after vacuum dehumidification. These are filter cakes whose internal viscosity is high if no shear stresses are applied and which are difficult to dehumidify under vacuum but by means of pressing / blowing.

- Belt press after belt filter

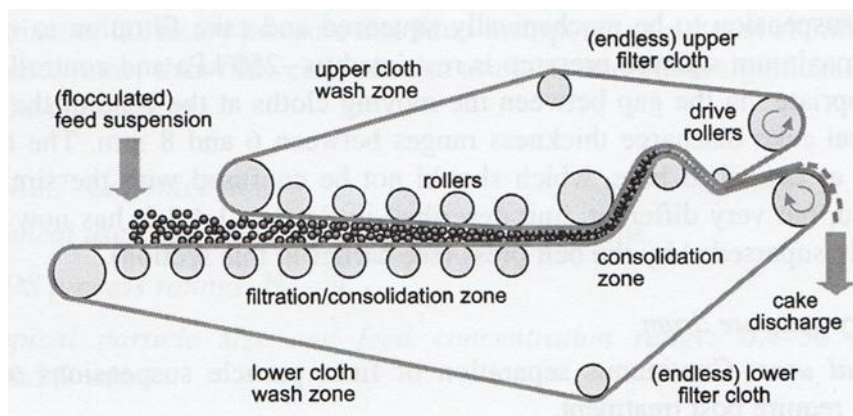
To reduce the moisture content, a belt press can be placed behind a (vacuum) belt filter. If it is clear that a belt press will be used, a simple dewatering table as a first step may suffice if desired. The belt press can be directly connected to the dewatering table or stand separately behind it.

The next figure shows a schematic system in which the (flocculated) suspension is fed to the belt press from a dewatering table. In the first part of the belt press, a cake is formed which is then gradually squeezed out.



Example calculation (ref.9): The moisture content of the highly porous polymer particles after dehumidification on the belt filter is 6.5 kg of water per kg of polymer; after the belt press, the moisture content is 2 kg/kg, so $\Delta X = 4.5$ kg/kg. The line pressure of the last rolls of this press is 200 N/mm, which is a high value for this type of devices. This high pressure is needed to squeeze enough water out of the particles. Because the solid-state flow is high (M is approx. 0.4 kg/s), the pressing achieves large energy savings in the dryer ($3000 * \Delta X * M = 3000 * 4.5 * 0.4 = 5400$ kJ/s). The costs of the belt press are lower than those for the expansion of the dryer capacity, so that the investment is also lower.

Impression of stand-alone belt press (ref.1)

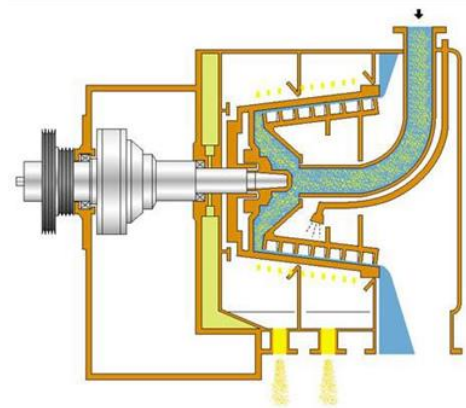


- Centrifuge after belt filter

As already mentioned in section 4.1.3, a continuously filtering centrifuge can be used if the particles are sufficiently large and the solid is suitable for it. With a filtering screw centrifuge, operating at approximately 1000*g, much lower moisture levels can be achieved than with a vacuum filter. In a number of cases, therefore, a screw centrifuge is set up after a belt filter. The centrifuge can be fed directly with the wet filter cake or the cake from the belt filter can be slurred up and fed to the centrifuge as slurry. In the first case, the wet cake is fed into the centrifuge with a conveyor screw.



Filtrating screw centrifuge



Some examples where a screw centrifuge is installed after a vacuum filter:

For a filter cake made up of fibrous material, the moisture content after dry suction on the belt filter is 1.5 kg of moisture per kg of dry matter. In connection with the layout, the cake is not fed directly to the screw centrifuge but as slurry. The moisture content after the centrifuge is 0.7 kg of moisture per kg of dry matter, so $\Delta X = 0.8$ kg/kg. Savings in the dryer section (investment, energy) justify installing the centrifuge after the vacuum filter.

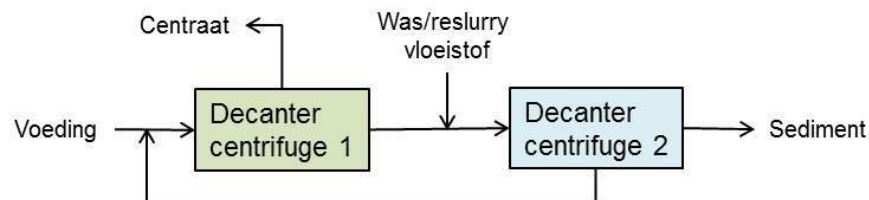
Another example concerns a granular product with an average particle diameter of approximately 100 μm . The wet cake that has been sucked dry on the belt filter still contains approximately 0.2 kg of moisture per kg of dry matter. The product is screwed into the centrifuge like a wet cake and comes out with 0.1 kg of moisture per kg of dry matter, so $\Delta X = 0.1$ kg/kg. With a mass flow of 0.5 kg/s, this results in energy savings of $3000 \cdot 0.1 \cdot 0.5 = 150$ kJ/s. This energy saving in the dryer does not justify the investment in the centrifuge, but because it is an existing installation whose capacity must be increased and where the dryer is the bottleneck, switching the centrifuge is an attractive choice. An additional advantage is that less or no recycle of dry matter is needed for the dryer to function properly.

- Decanting centrifuges with reslurry washing

If it is necessary to work in a closed system and/or the filtration rate is low and therefore a (vacuum) filter becomes too large, systems with two or a maximum of three decanter centrifuges in series can be considered (Figure 8). This system is described in reference [8]. In the example given therein, the solid is biomass (waste) which, with the moisture content with which it comes out of the centrifuge, can be deposited without further drying. The liquid contains the product that is extracted as completely as possible with the reslurry wash.



Two decanting centrifuges in series with slurry wash



6.3 Operating window

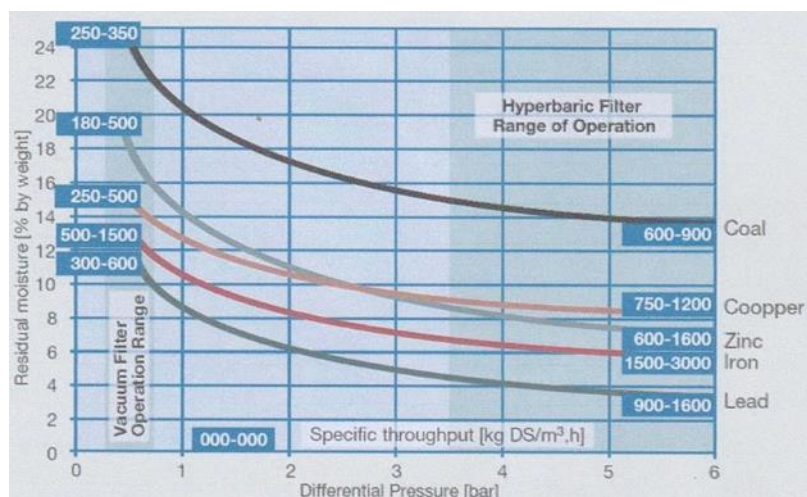
The operating window varies with the type of dehumidification:

- a) Gas blow-through
- b) Centrifugation
- c) Mechanical pressing

Two parameters effectively describe dehumidification of filter cakes:

1. Equilibrium moisture content. This is the finally achieved value after sufficient time. The equilibrium curve indicates the size of minimum required driving force.

Equilibrium moisture content as a function of differential pressure



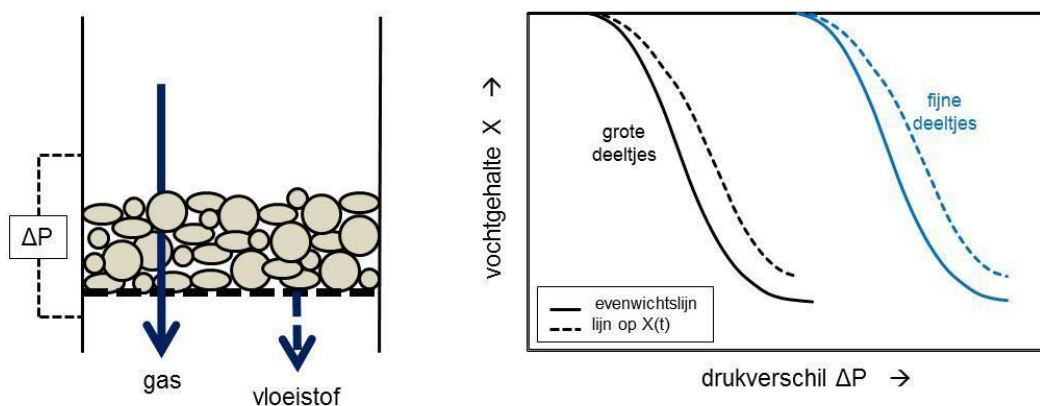
2. Kinetics of dehumidification. This is the course of the moisture content during dehumidification as a function of time. Kinetics indicate the minimum residence time in the dehumidifier.



a) Gas blow-through

The driving force when dehumidifying by means of gas blowing through is a difference in gas pressure over the filter cake. The interstitial fluid is pressed out of the cake by the gas and is dragged along. A channel between particles can only be emptied if the gas pressure is higher than the capillary pressure.

Dehumidification by blow-through of gas.



Qualitatively, this method of dehumidification for filter cakes that are made up of coarse and fine particles is shown in Figure x. It outlines both the equilibrium moisture content X and the value $X(t)$ at the time t when the equilibrium has not yet been reached as a function of the pressure difference Δp .

The above figure shows the following:

- A certain pressure difference is needed (the capillary entry pressure) before the cake starts dehumidifying. This pressure difference is inversely proportional to particle diameter.
- If the pressure difference increases and more gas is blown through the cake, the moisture content decreases.
- In case of further increase in the pressure difference, a constant value is reached for the moisture content. With vacuum filters, the available pressure difference to suck gas through the cake is limited (< 0.6 bar). As a result, the moisture content of such filter cakes is high, especially if they are made up of fine particles. If a cake is made up of stable particles of an average of $100 \mu\text{m}$, then in general the cake on a vacuum filter can be sucked dry fairly well; with a particle diameter of an average of $25 \mu\text{m}$, this is usually no longer the case.



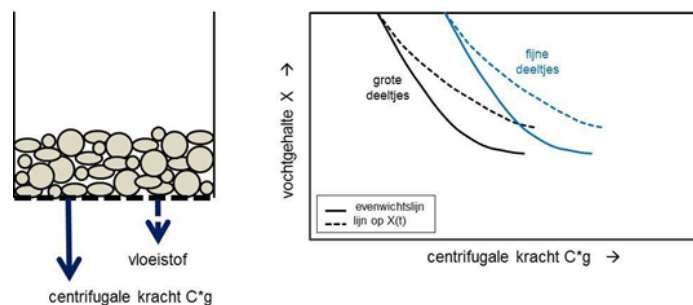
The final result depends on the shape of the particles, the porosity of the cake, the particle size distribution, the viscosity of the liquid and the temperature of the system.

Filters that can dehumidify the filter cake at higher gas pressure are disc filters, drum filters, belt filters built in a pressure vessel (continuous filters) and candle filters (discontinuous filters).

b) Centrifugation

The dehumidification of a filter cake in a centrifugal field is shown in the figure below in a similar way as the former figure. The driving force is the centrifugal acceleration $C \cdot g$, in which g is the acceleration of gravity. The factor C shows how many times the acceleration is greater than gravity.

Dehumidification by means of a filtering centrifuge



Although the physical principles of gas blowing and centrifugation are different, the curves in the last two figures are fairly similar.

The above figure shows that a certain minimum $C \cdot g$ value is required before the liquid starts to run out of the spaces between the particles, that this value is higher for filter cakes made up of fine particles and that the decrease in the moisture content is achieved to a constant minimum value when $C \cdot g$ increases.

The effect of centrifugal force on the dehumidification of solids of different particle sizes can be explained as follows:

- * Particles of 400 μm that do not deform too much and do not fall apart can already be dehumidified at 300 $\cdot g$ in a continuously filtering centrifuge with a short residence time (e.g. sliding centrifuge).

- * For particles of 100 μm , the same applies at 1200 $\cdot g$ (e.g. in a screw centrifuge).



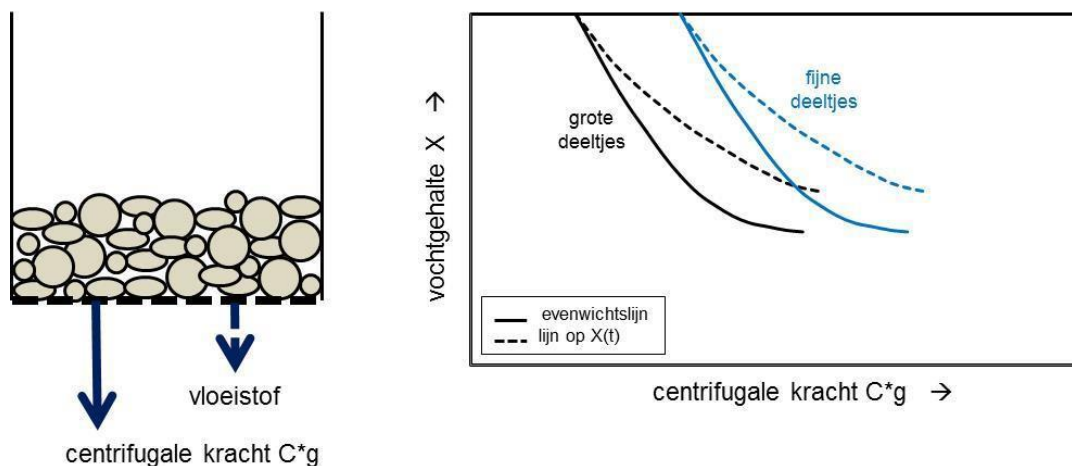
* For particles of 20 μm , a centrifugal force of approximately 2000*g and a residence time of a few minutes are required to dehumidify properly. These values cannot be achieved in a continuous centrifuge but can be achieved in a discontinuous (e.g. peeling) centrifuge.

The above numbers are intended as an indication and apply if the viscosity of the liquid is sufficiently low (such as of aqueous systems). In addition to filtering centrifuges, decanting centrifuges (separation by sedimentation) are used on a large scale for fine particles to dehumidify.

c) Mechanical pressing

The behavior of a filter cake during pressing is described on the basis of the concept of porosity. The porosity ϵ of a filter cake is the volume of spaces between the particles divided by the total volume. Of a liquid-filled filter cake, the volume part is therefore ϵ filled with liquid and $(1 - \epsilon)$ with solid. The value of ϵ is between 0 (volume completely filled with solids) and 1 (no solid present). The extent to which liquid can be removed from a filter cake by pressing depends on the relationship between porosity and press pressure. If a cake is compactly stacked with dimensionally stable, non-porous particles, then when pressing the porosity will decrease little and therefore little liquid will be removed.

On the other hand, if the particles are porous (by themselves porous, agglomerated or flocculated particles) and/or deformable and/or the original filter cake has a more open structure, then the porosity during pressing will decrease sharply and a lot of liquid will be removed.





For a saturated cake, the relationship between the moisture content X and the porosity is ϵ : $X = \epsilon * \rho_L / [(1 - \epsilon) * \rho_S]$ where: X = moisture content in kg of moisture / kg of solid

ϵ = volume of the space between the particles / total volume (porosity) ρ_L = specific gravity of the liquid

ρ_S = specific gravity of the solid

If the filter cake is sufficiently firm and the pressure forces and times are sufficient, the moisture content can be significantly reduced with roll presses on a belt filter or a rotating vacuum filter. The maximum line pressure is 12 (belt filter) to 25 N/mm (rotating vacuum filter).

6.4 Benefits and Costs

A good method to determine whether an investment in an improved dehumidification method pays off is to determine the size of the energy savings. A simple estimate can be made with the following equation:

$$\text{Energy saving} = 1.2 * \Delta X * M * r \text{ kJ/s}$$

where 1.2 = experience factor for evaporation in industrial dryers (this is minimum value; may be higher depending on the type of dryer).

ΔX = difference in moisture content before and after improved dehumidification in kg of moisture per kg of solid. M = mass flow of solid in kg of dry solid per second.

r = heat of evaporation of the liquid in kJ/kg.

If water is the liquid, the above equation is simplified to: Energy saving = 3000 * ΔX * M kJ/s

6.5 TRL and risks

Dehumidification equipment has been around for decades. TRL of separation technologies on the market are invariably TRL=9. The risk associated with dehumidification techniques mainly lies in the combination of the specific liquid/solid mixture and the separation technique chosen. When prior experience with envisaged separation techniques is absent, it is best to set up small scale test programs in cooperation with equipment vendors. This is in fact common practice and many vendors offer test rigs, either on their own premises or mobile units which can be deployed at the customers site.

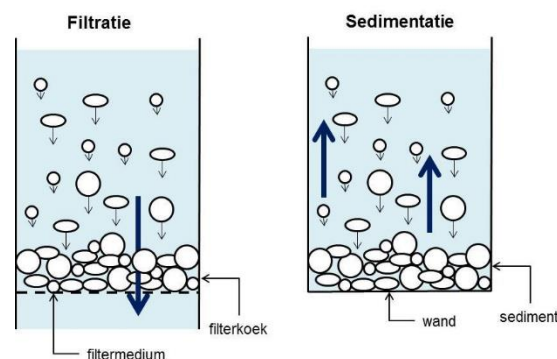


6.6 Working principle

Separation takes place by filtering or sedimentation:

- In filtration, the separation takes place using a porous filter medium, in which the solid-state particles are stopped and a filter cake is formed. The liquid (the filtrate) is discharged through the filter cake and the filter medium. The driving force for this process is a pressure difference. centrifugal force on a filtering centrifuge, under pressure on the filtrate side in vacuum filtration or overpressure on the slurry supply side in pressure filtration.
- Sedimentation occurs due to density differences between solid and liquid. The driving force here is gravity (in the case of thickeners) or a centrifugal force (in the case of a hydrocyclone or decanter centrifuge).

Liquid – solid separation by means of filtration and sedimentation



6.7 References

1. R.J. Wakeman & E.S. Tarleton; Filtration: Equipment Selection, Modelling and Process Simulation; Elsevier, Oxford, 1999; ISBN 1 85617 345 3.
2. R.J. Wakeman & E.S. Tarleton; Solid/Liquid Separation: Principles of Industrial Filtration; Elsevier, Oxford, 2005; ISBN 1 8561 74190.
3. R.J. Wakeman & E.S. Tarleton; Solid/Liquid Separation: Scale-up of Industrial Equipment; Elsevier, Oxford, 2005; ISBN 1 8561 74204.
4. R.J. Wakeman & E.S. Tarleton; Solid/Liquid Separation: Equipment Selection and Process Design; Elsevier, Oxford, 2007; ISBN 978-1-85-6174213.
5. Andritz Separation Systems; brochure Reference Description Alunorte; <http://www.andritz.com/se-references-alunorte.pdf>
6. Alan Records & Ken Sutherland; Decanter Centrifuge Handbook; Elsevier Advanced Technology, Oxford, 2001; ISBN 1-85617-369-0.



6.8 Suppliers

Below you find an overview of leading separation equipment manufacturers. Excerpts from their most recent publications have been added which focus on:

- a) Application areas
- b) Categories / classes of associated equipment



- Alfa Laval: <http://www.alfalaval.com/>

Key application areas

Industry



Water treatment for drill & blast tunnels

Alfa Laval has a range of centrifuge decanters that meet the high environmental demands for solid-liquid separation in drill and blast tunnelling.

Industry



Tailings

Mining dams pose a substantial risk, and residue management clearly needs to change. Alfa Laval is leading that transformation with robust design and large capacity solutions.

Industry



Tailings

Mining dams pose a substantial risk, and residue management clearly needs to change. Alfa Laval is leading that transformation with robust design and large capacity solutions.

Industry



Tailings

Mining dams pose a substantial risk, and residue management clearly needs to change. Alfa Laval is leading that transformation with robust design and large capacity solutions.

Industry



Precious Minerals and Mining

Alfa Laval has a range of equipment to optimize key processes such as separation and heating and cooling in the beneficiation, leaching and extraction of precious mineral ores.

Industry



Coal Beneficiation

Alfa Laval is revolutionising the treatment and disposal of coal tailings. This is being led by a strong demand to look after the environment: to conserve water and remove tailing dams.

Industry



Slurry treatment in tunnel boring

Alfa Laval has a range of cost-effective centrifuge decanters for high volume slurry treatment in tunnel drilling applications that help you to increase site production.

Industry



Slurry treatment for horizontal directional drilling

Alfa Laval has a range of reliable centrifuge decanters for solids control in horizontal directional drilling (HDD) that help boost onsite productivity and working conditions.

Industry



Liquid-solid mixing

Alfa Laval Vortex products are simple, low maintenance solutions based on Venturi technology for the mixing of liquids and solids in a wide range of industrial processing applications.

Industry



Green liquor treatment

Green liquor handling acts as the kidney of the pulp mill removing the non-process elements. At the same time, it ensures process chemicals can be recovered and reused time and time again.

Industry



Industrial fluids

Alfa Laval has a range of equipment for effective cleaning of coolants and wash liquids so that you can prolong your equipment life time and save money from reusing your industrial fluids.

Industry



Base Minerals and Mining

Alfa Laval has a range of equipment and the knowhow to help you optimize key processes in base mineral beneficiation, extraction applications and tailings dewatering.



Industry



Plant-based drink production

A variety of plant based drink processing equipment for all kinds of raw material from soy and oat to almonds, rice and beyond.

Industry



Construction machinery

Alfa Laval construction decanter centrifuges can be optimized in every detail to ensure the best solids removal for any construction drilling site.

Equipment

Product



P3

Alfa Laval's P3 range of decanter centrifuges is built for the toughest applications and is specifically developed for solid-liquid separation in the mining and mineral industry.

Product



FilmVap

These evaporators can process clear, non-fouling liquids as well as moderately fouling liquids.

Product



FOCUS

Alfa Laval Fuel Oil Cleaning Unit Solutions (FOCUS) are automated modular systems for purifying the liquid fuel oils used in gas turbine power plants.

Product



CDNX

Alfa Laval CDNX centrifugal decanter efficiently remove solid particles from water and oil-based slurries resulting in better performance at construction sites.

Product



Emmie 2

This mobile centrifugal separator effectively removes both particles and water from oils widely used in industry.

Product



Vortex Snub Radial Eductor

Rapid volume turnover to ensure fast chemical reaction for swift product separation.

Product



Alfie

Alfie centrifugal separators remove the contaminating oil, grease and solid particles from coolants used in industry, helping prevent tool wear and avoid disposal problems.

Product



Foodec

Alfa Laval Foodec decanter centrifuges are ideal for industries where delicate food and beverage products are processed – and where easy cleaning is crucial.



Product



Clara series

Specially developed for food, beverage and industrial fermentation applications, the Clara range offers gentle product treatment, high separation efficiency and low power consumption.

Product



AlfaPure

The AlfaPure range comprises purpose-built centrifugal separator systems for removing oil, grease and solid particles from water and oil based liquids, such as coolants, lubricants and wash liquids.

Product



BD series

The critical technologies for biodiesel processing are heating, separation and mixing. Alfa Laval supplies products within all three technologies for the different production steps.

Product



FESX

The FESX separators are specially designed for industrial fermentation applications and are available in many different sizes and configurations.

Product



PANX

Alfa Laval PANX-series of decenter centrifuges is designed for palm oil clarification and purification. The units offer maximum oil recovery with low energy consumption.

Product



OCM

The Alfa Laval Oil Cleaning Module (OCM) provides rapid, effective separation of the oil, water and sludge components in contaminated mineral lubricating and hydraulic oils.

Product



Vortex Radial Eductor

A uniquely designed, low pressure mud gun to increase fluid movement in mud pits.

Product



Vortex Shear-Mixer

An advanced mixing solution that reduces additive waste, mixing time and cost.

Product Type



Flat sheet membranes

The range of membranes from Alfa Laval covers all filtration processes: reverse osmosis, nanofiltration, ultrafiltration and microfiltration

Product



PilotUnit Multi

The Alfa Laval PilotUnit Multi is ideal for membrane screening, process development and scale-up for MF,UF, NF and RO. Learn more.

Product



Culturefuge

The Culturefuge is a hermetic separation system, specially designed for gentle harvesting of shear-sensitive material in applications involving mammalian cell cultures and precipitated proteins.

Product Type



Spiral membranes

Alfa Laval produces various types of efficient and premium quality spiral membranes, including RO, NF, UF and MF. Learn more by clicking here.

Product Type



Powder mixers

Our mixers allow you to match the right mixing method to your needs, ensuring greater energy savings, superior cleanliness, and higher process efficiency in terms of reduced process time.

Product



FEQX

Specially designed for industrial fermentation applications, the FEQX separator range is adapted for dealing with the widely varying separation tasks required.

Product



CH

CH-range of separator systems are designed to meet the high and versatile demands of the various applications.

Product



MF flat sheet

The microfiltration (MF) membranes available from Alfa Laval are made of polysulphone polymer or fluoro polymer with pore sizes ranging from 0.1 to 0.5 µm. The membranes are available in two series



Product



OFX

The Alfa Laval OFX 20 disc stack centrifuge system is specially designed to provide the oil industry with a highly efficient way to remove water and solids from heavy crude oil.

Product



Vortex Mixmate

A safe, proven mixing and dispensing solution for caustic mud additives.

Product



FilmVap

These evaporators can process clear, non-fouling liquids as well as moderately fouling liquids.

Product



MF flat sheet

The microfiltration (MF) membranes available from Alfa Laval are made of polysulphone polymer or fluoro polymer with pore sizes ranging from 0.1 to 0.5 μm . The membranes are available in two series

Product Type



Tank mixers

Efficient, effective fluid agitation and shear

Product



UF flat sheet

The selection of ultrafiltration (UF) membranes from Alfa Laval covers a broad spectrum of flux properties and MWCO values ranging from 1,000 to 100,000. More series are offered for many applications

Product Type



Plant-based protein and vegetable processing systems

Boost the quality and yield of plant-based protein food and drink products with our plant-based protein and vegetable processing systems.

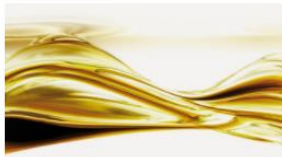
Product



NF flat sheet

For nanofiltration (NF) Alfa Laval offers a thinfilm composite polymeric membrane with a MgSO_4 rejection $\geq 99\%$. A unique construction on polyester support material provides optimum cleaning conditions

Product Type



Edible oil refining process systems

A full range of edible oil refining processes from crude to refined oils. Find out how we can help you.

Product



FAME biodiesel pretreatment systems

Alfa Laval's solutions for pre-treatment of fats and oils in FAME biodiesel production are characterized by the effective removal of impurities and low energy consumption.

Product



HVO pretreatment systems

Our automated HVO pretreatment systems produce feedstock free from impurities and adjust free fatty acids for conversion into renewable hydrocarbon transportation fuels.

Product



Degumming systems

Improve yield and crude oil quality further while minimizing 3-MCPD formation during edible oil refining.

Product



Neutralization systems

Systems for neutralization process of edible oil to remove free fatty acids and other impurities that impact edible oil quality, consistency, appearance, taste and shelf life.

Product



Bleaching systems

Solutions for optimal edible oil bleaching process, built on deep process knowledge and global services.

Product



Compabloc

Alfa Laval Compabloc range is compact and designed for optimum performance and serviceability across a broad spectrum of industrial process applications.

Product Type



Fat modification process systems

A full range of fat modification processes such as fat hardening, interesterification (chemical or enzymatic), dry fractionation and semi-continuous deodorization. Find out more.



Product Type



Pretreatment systems for biofuels

Alfa Laval has a market-leading position with respect to pretreatment process systems for any raw material for these biofuels. Find out how you can benefit from our experience.

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Andritz Separation: <http://www.andritz.com/index/separation.htm>

Key application areas

KEY APPLICATION AREAS



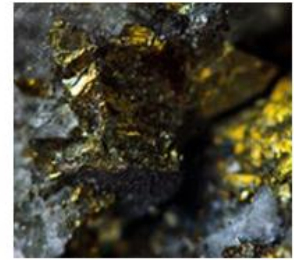
Potash



Coal



Tailings



Metal mining

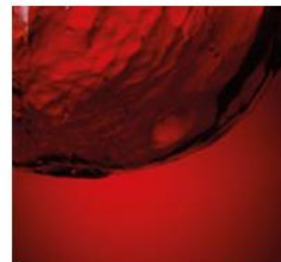
KEY APPLICATION AREAS



Dairy



Vegetable oil



Beverage



Baby food

KEY APPLICATION AREAS



Agrochemicals and fertilizers



Petrochemicals and polymers



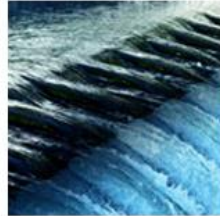
Soda ash and technical salts



KEY APPLICATION AREAS



Industrial wastewater



Municipal wastewater



Potable water

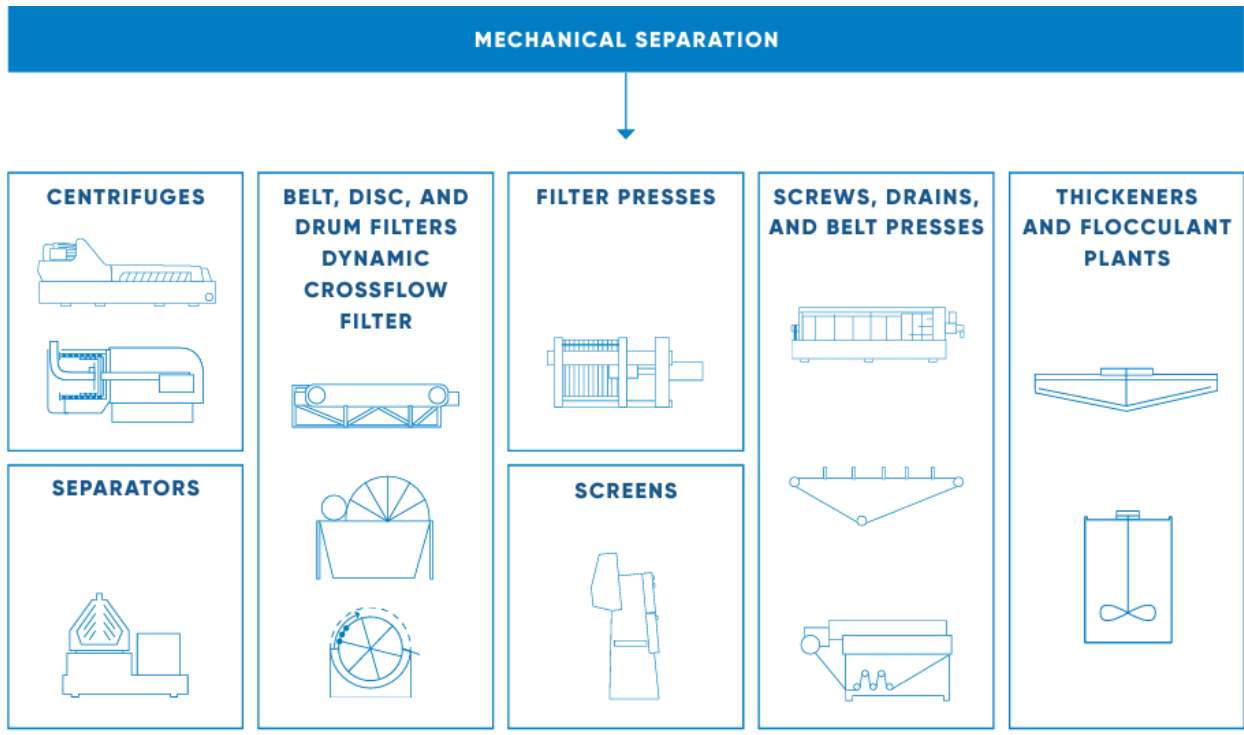


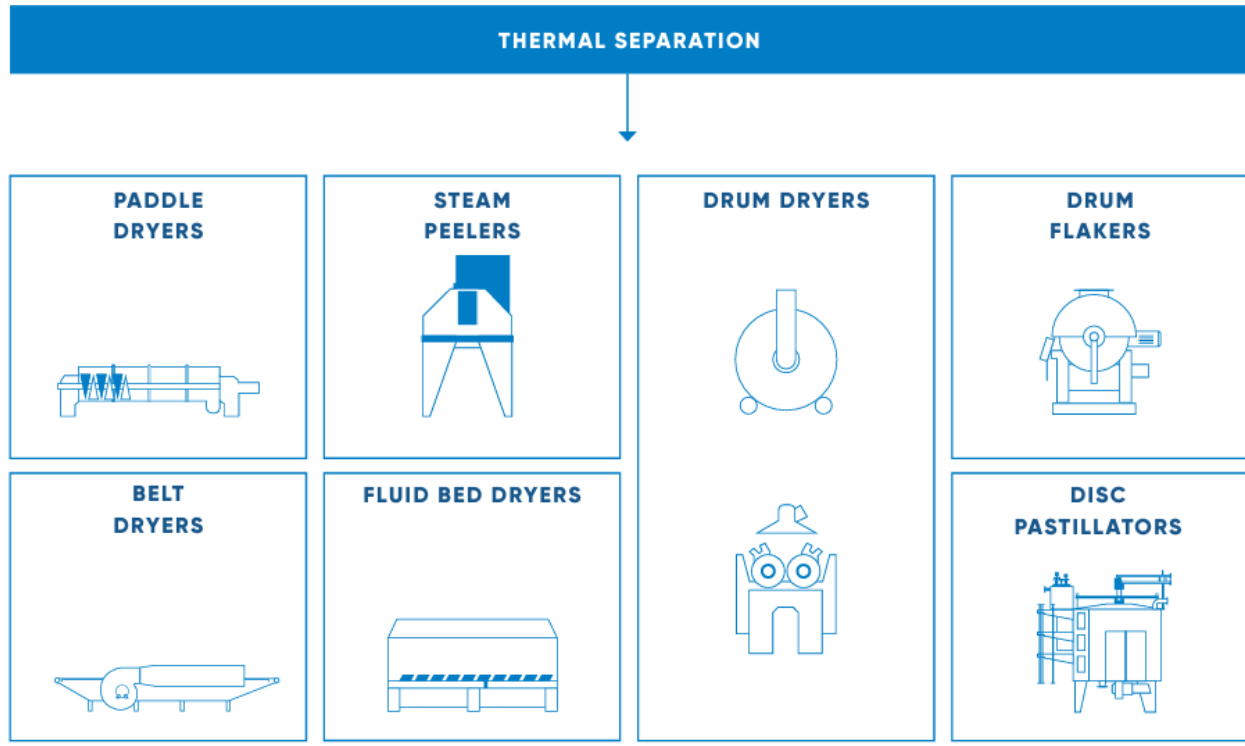
Biomass production



Organic waste

Equipment





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- Broadbent Industrial Centrifuges: <http://www.broadbent.co.uk/>

Key application areas & Equipment



Latest CL1800 Sugar Centrifuges Delivered

Having supplied our latest design CL range basket centrifuges last year, we are pleased to be delivering a further 3 units to our valued customer in the Philippines. These units were supplied from our facility in Thailand. The CL range of sugar centrifuges are fully...



Latest Minerals Tailings Centrifuge

We are very pleased to be delivering our latest solids bowl decanter centrifuge for the Minerals Tailings Application. This heavy duty range has been developed to handle anything up to 250 TPH Feed with solids concentration in the region of 20%. It is equipped with...



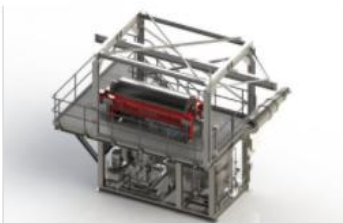
Minerals Tailings Dewatering Lab and Pilot Testing

A new greenfield mine in North America decided to dry stack tailings. Their tailings however posed several challenges: Very high capacity, A difficult to dewater particle size distribution consisting of a high proportion of fines and ultra fines, A small proportion of...



Back in time – 1978

Just looking at some old photos showing the 4 off 900mm diameter Solid Bowl Decanter Centrifuges we supplied via Flottweg to the Basel Municipal Waste Plant in 1978 - Even now the machines look awesome in size. Our Chairman at that time Mr Peter Broadbent stands...



Complete MEG Processing System

Broadbent have engineered, manufactured and supplied a complete MEG recovery package. The system includes continuous decanter centrifuge technology complete with module frame, wash system, receiving vessels, master PLC controls and integrated pipework. The unit was...

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- Flottweg: www.flottweg.com

Key application areas

A

[Algae harvesting](#)
[Avocado oil extraction](#)

B

[Beer production](#)
[Biodiesel manufacturing](#)
[Bioethanol manufacturing](#)

C

[Casein manufacturing](#)
[CRUD processing](#)

D

[Drilling mud treatment](#)

F

[Fermentation broths](#)
[Fish processing](#)
[Food residue processing](#)

I

[Instant coffee production](#)
[Instant tea and tea extract production](#)

J

[Juice manufacturing](#)

L

[Lactose manufacturing](#)
[Limed fleshing](#)
[Lupin protein extraction](#)

M

[Manure processing](#)
[Mining](#)

O

[Oil sludge treatment](#)
[Olive oil extraction](#)

P

[Paint sludge dewatering](#)
[Palm oil extraction](#)
[Paper sludge](#)
[Pea starch production](#)
[Plastic recycling](#)
[Potato starch extraction](#)
[Press oil extraction](#)
[Protein extraction](#)
[PVC dewatering](#)

S

[Sand and gravel wash water](#)
[Seed oil extraction](#)
[Sewage sludge dewatering](#)
[Sewage sludge thickening](#)
[Slaughterhouse waste recycling](#)
[Sludge thickening with starch polymer](#)
[Steelwork sludge treatment](#)
[Surimi processing](#)

T

[Tailings](#)
[Tapioca starch production](#)
[Tar cleaning](#)

U

[Used cooking oil processing](#)

V

[Vegetable milk alternatives production](#)

W

[Waste oil processing](#)
[Waterworks sludge dewatering](#)
[Wheat starch production](#)
[Whey processing](#)
[Wine clarification](#)



Equipment



Decanter Centrifuges

We focus on technological innovations that maximize the performance of our decanters. Our decanter centrifuges are always optimally adapted to the application.

[About Decanter Centrifuges](#)



Separators

Our separators are real all-rounders for clarifying and separating liquids. They are characterized both by their smooth operation and their robustness.

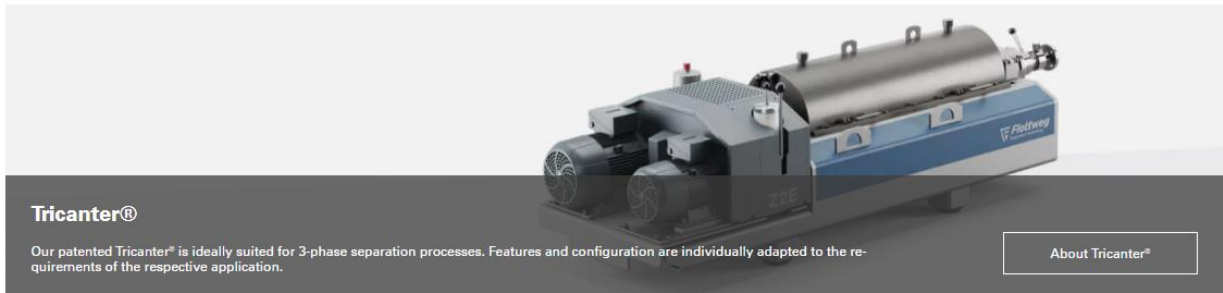
[About Separators](#)



Belt Presses

Our belt presses are used by countless customers worldwide. Particularly in the fruit juice and food industries and often in conjunction with our decanters and separators.

[About Belt Presses](#)



Tricanter®

Our patented Tricanter® is ideally suited for 3-phase separation processes. Features and configuration are individually adapted to the requirements of the respective application.

[About Tricanter®](#)



Sedicanter®

Flottweg has developed the Sedicanter® especially for materials that are difficult to sediment - a combination of decanter centrifuge and separator.

[About Sedicanter®](#)



Sorticanter®

Flottweg developed the Sorticanter® especially for the processing of plastics. The industrial centrifuge ensures the highest grade purity when separating plastics.

[About Sorticanter®](#)



Systems and complete solutions

Systems tailored to the specific application function with increased smoothness and they are also characterized by their higher performance.

[About Systems/Complete Solutions](#)



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- GEA Westfalia:
<http://www.gea.com/global/en/productgroups/centrifuges-separation-equipment/decanter-centrifuge/index.jsp>

Key application areas

-  Beverage
-  Chemical
-  Dairy
-  Dairy farming
-  Environment
-  Food
-  Heating & refrigeration
-  Home & personal care
-  Marine
-  Oil & gas and energy
-  Pharma & healthcare



Equipment



2-Phase Separating Decanter chemMaster

For clear clarification and dewatering in chemical and mineral processing applications. The clarified liquid is discharged under pressure by use of a centripetal pump. CIP-compatibility of the decanter can be assured.



2-Phase Separating Decanter cutMaster

For clear classification in chemical and mineral processing applications. The clarified liquid is discharged freely into a liquid catcher and flows off under gravity. CIP-compatibility of the decanter can be assured.



2-Phase Separating Decanter dryMaster

For clear clarification and dewatering in chemical and mineral processing applications. The clarified liquid is discharged freely into a liquid catcher and flows off under gravity. CIP-compatibility of the decanter can be assured.



2-Phase Separating Decanters for Oil Recovery

The big advantage of the 2-phase separating decanter for olive and palm oil recovery is the enormous savings when it comes to dilution water.



3-Phase Separating Decanter for Industrial Fluids

For the treatment of waste oil, MARPOL liquids, waste emulsions and oily waste water



3-Phase Separating Decanter meatMaster CF for Animal By-Products

For the recovery of animal oils, fats and proteins



3-Phase Separating Decanters for animal and fish by-products

For the recovery of fish oil, proteins and meal



3-Phase Separating Decanters for Oil & Gas

For the Oil & Gas industry GEA offers 3-Phase separating decanters for the treatment of waste and slop oils.



3-Phase Separating Decanters for Oil Recovery

For the recovery of olive, palm and other vegetable crude oil the decanter is always the heart of the installation. 3-Phase decanters separate both, the olive pulp or the palm oil sludge into oil, water and solids.



Bacteria Removal Separators for Milk and Whey

Bacteria removal separators from GEA efficiently remove bacteria and spores from the raw and vat milk and whey.



Chamber Bowl Separators Blood Processing

GEA chamber bowl separators for blood processing



Chamber Bowl Separators Pharma Biotech

This separator has been designed for protein recovery. PKB 25 - 300-600 l/h* & PKB 45 - 500-1000 l/h*



Clarifiers for Beverages

High performance GEA clarifiers for beverages with continuous and automatic operation in hygienic design.



Clarifiers for Biochemicals

The self-cleaning GEA clarifiers for biochemical ensure high product quality and yield. According to model, they are designed to resist concentrated acids, high pressures and inflammable or even explosive substances.



Clarifiers for Blood Processing

GEA clarifier hycon are a two room concept designed for a sterile process in clean rooms while achieving highest concentrations of solids in aseptic processes. According to model, low-temperature applications are available.



Clarifiers for Food Ingredients

For the food ingredients and protein industry GEA clarifiers are used to concentrate algae, recover soy, rice, pea and other vegetable proteins and amino acids.



Clarifiers for Industrial Fluids

For the treatment of cooling lubricants, washing liquids, oil-water mixtures, lube oil, fuel oil, waste oil, etc.



Clarifiers for Milk, Whey and Calcium Phosphate

GEA clarifiers are used in the dairy industry to improve quality.



Clarifiers for Pharma Extraction

GEA clarifiers for pharma extraction are used in solid-liquid extraction processes with low solid contents (up to approx. 7 % by vol.).



Clarifiers for Pilot Scale/ Lab Scale

GEA clarifier for pilot scales are the reliable solution to set up new processes. They offer two key advantages: maximum scale-up reliability with minimal installation work input as well as optimum process safety for every process with only low capital expenditure. Fully equipped with the renowned GEA technology features, they are the best technical and economic solution to start a new process.



Clarifying Decanter chemMaster

For clear clarification and dewatering in chemical and mineral processing applications. The clarified liquid is discharged under pressure by use of a centripetal pump.



Clarifying Decanter drymaster

For clear clarification and dewatering in chemical and mineral processing applications. The clarified liquid is discharged freely into a liquid catcher and flows off under gravity.



Clarifying Decanter gMaster CF for Beverages

For the clarification of beverages



Clarifying decanters for animal and fish by-products

Processes in the fish and animal by-products industry usually impose particularly stringent requirements on the hygienic design as well as the robustness and corrosion-resistance of the materials. These tasks have been solved by the design features of GEA ecoforce generation; high-performance stainless steels, special chute designs for ease of cleaning, additional spray nozzles at critical points as well as high quality wear protection have been installed.



Clarifying Decanters for Cheese Curd, Casein and Lactose

The decanters ensure the efficient production of processed cheese base, raw goods for curd cheese bars or bakers cheese. The decanters are also ideally suited for reprocessing cheese fines and for lactose and casein production thanks to their design, which has been optimized for the production of delicate foods.



Clarifying Decanters for Edible Oil Refining

In oil refining processes clarifying decanters are used for press oil clarification. Compared to conventional hot seed pressing plants with leaf filter the process setup becomes much simpler when using a decanter.



Clarifying Decanters for food ingredients

For food ingredients and protein recovery GEA offers clarifying decanters for applications like the recovery of soy, rice, pea and many other vegetable proteins, for the concentration of algae or amino acids like lysine.



Clarifying Decanters for Industrial Fluids

For the treatment of waste oil, MARPOL liquids, waste emulsions and oily waste water



Clarifying Decanters for Oil & Gas Recovery

GEA has developed special decanters for treating drilling fluids. Apart from high-performing and top separation efficiency the decanter centrifuges distinguish themselves through safe operation and robust design.



Clarifying Decanters for Starch Recovery

For starch recovery clarifying decanters are installed in different process stages depending on the raw material.



Classifying Decanter for Oil & Gas

GEA offers classifying decanters for barite recovery in drilling mud treatment.



Compact Milk Pasteurizer MWA for Milk, Cream and Whey

Pre-assembled and pre-tested compact milk pasteurizer units with integrated skimming separator for milk, cream and whey pasteurizing (2000 - 35,000 l/h).



Decanter pharmMaster for Extraction Products

This decanter has been designed for extraction products.



Dewatering Decanter crudMaster

For clear clarification, liquid separation and solids dewatering in chemical and mineral processing applications. The heavy or light liquid phase is discharged under pressure by use of a centripetal pump while the other liquid phase is discharged by drain tubes. CIP-compatibility of the decanter can be assured.



EnergyMaster

In traditional lube oil treatment systems the hot oil flows back to the engine sump tank to be cooled by the engine cooling system. Therefore the energy for heating the lube oil upstream of the centrifugal separator is lost. GEA EnergyMaster recovers part of this energy.



GEA bilge Separator

GEA bilge Separator with integrated direct drive is designed for cleaning oily water and producing minimum residual oil contents in all performance classes.



GEA biosolids Decanter

The GEA biosolids Decanter is a continuously operating centrifuge with horizontal solid-wall bowl developed specifically for (pre-) dewatering and thickening of municipal sludge.



GEA biosolids Granulator

The GEA biosolids Granulator is an innovative dry-on-demand solution for biosolids treatment from municipal and industrial wastewater treatment plants. It combines existing centrifuge-based dewatering with established drying technology.



GEA Crude Oil Treatment Systems

These ready-to-use treatment systems have been designed for the efficient dehydration and desalting of crude oil. At the heart of each modular system is a high-performance centrifugal separator which can be flexibly supplemented by additional units. The easy-to-integrate treatment system can be customized for various process setups and stages in both upstream and downstream processes.



GEA manure Decanter

The GEA manure Decanter is a continuously operating centrifuge with horizontal solid-wall bowl for the treatment of manure and digestate.



GEA pathfinder GMP

The GEA separator skid in the sophisticated compact format for pharmaceutical applications requires little space in the technical centre and, thanks to its sensible design, reliably fulfills even the most demanding technical tasks. You can easily scale the results to any desired production size with no problem. As such, the full functionality of large pharmaceutical centrifuges is available to you in the simplest way, allowing you to concentrate fully on the creative development of your products.



GEA pectinMaster

Optimizes the entire number of process steps thanks to its maximized separation efficiency. The fleet comes in a hygienic design, is protected against corrosion and abrasion. Explosion-proof designs are also available.



GEA pharma separator aseptic C

Smooth handling of biopharma products, high separation performance, all features for highest cleanability requirements included: automatic SIP, easy validation and high-end qualification package.



GEA pharma separator aseptic N

Smooth handling of biopharma products, high separation performance, all features for highest cleanability requirements included: automatic SIP, easy validation and high-end qualification package.



GEA pharma separator aseptic X

The freedom to produce any product on the same skid. Turns a static production into a flexible one while ensuring optimum yield with every process step. Smooth handling of biopharma products, high separation performance, all features for highest cleanability requirements included.



GEA pharma separator pure C

Smooth handling of biopharma products, high separation performance, all features available for an optimum cleanability according to your process requirements: automatic CIP, easy validation and more.



GEA pharma separator pure N

Smooth handling of biopharma products, high separation performance, all features available for an optimum cleanability according to your process requirements: automatic CIP, easy and fast validation and many more.



GEA pharma separator pure X

The freedom to produce any product on the same skid. Turns a static production into a flexible one while ensuring optimum yield with every process step. Smooth handling of biopharma products, high separation performance, all features available for an optimum cleanability according to your process requirements.



GEA proplus

GEA proplus extends the ejection intervals of milk separators from 20 – 30 minutes to up to 90 minutes. This ensures added value, a significant increase in protein yields from the quantity of milk used and a clear reduction in fresh water consumption and waste water creation.



GEA sludge Decanter

GEA sludge Decanters provide an energy-efficient solution for dewatering of industrial waste water and water treatment sludge.



GEA vacuoliq Vacuum Spiral Filter

GEA vacuoliq Vacuum Spiral Filter for industrial juicing of niche products as well as for small and mid-sized juice producers.



GEA Wine Decanter Skids

Make every grape count. The GEA Wine Decanter is the first decanter centrifuge specially engineered for grape extraction, clarifying and recovering. A single machine that does the work of multiple wine presses and other equipment, adding modern, competitive efficiency, versatility and speed to all processes. With five applications to achieve greater yield and taste, the GEA Wine Decanter has it all.



GEA "Plug & Win" Centrifuge Skids for Craft Brewers

Hop is hip! But a large volume of perfectly brewed beer is lost in the process with hop solids, surplus yeast and trub. It's all money going down the drain. But with a GEA "plug & win" centrifuge skid you can exploit it to the maximum and sell more beer. We have the right solution ready for brewers small and large!



Mobile Decanter Systems

Mobile decanter systems from GEA are designed for flexible process integration. They have a modular, plug-and-play design – as lorry trailers or standardized sea containers.



Multi-Functional Centrifuges for Small and Mid-sized Cideries

This versatile GEA equipment has a variety of applications in the cidery. Each application benefits the cidery by improving the consistency of the product, minimizing product losses, accelerating production time and, ultimately, increasing profitability. In fact, the payback for this equipment has proven to quickly justify the investment.



Nozzle Separators for Baker's Yeast and Yeast Extract

GEA yeast separators are used for the processing of baker's yeast as well as yeast extract for more than a century now. Stable process condition due to the GEA viscon nozzle as well as our direct drive systems are the latest in a long list of innovations we have specifically developed for the yeast industry.



Nozzle Separators for Chemicals and Minerals

GEA nozzle bowl separators for chemicals stand for utmost security of the investment, products and processes. They insure high product quality and yield.



Nozzle Separators for Oil & Gas

For the recovery of crude oil from bitumen



Nozzle Separators for Oil Recovery

Nozzle separators are used in the conventional process with vertical clarifiers in palm oil mills. GEA also offers special nozzle separators to the palm oil industry in order to recover oil from sterilizer condensate.



Nozzle Separators for Starch Recovery

Nozzle separators are used for washing and concentrating the crude starch as well as for gluten thickening. A high quality starch can only be obtained if the small fiber fragments, lipids, proteins and dissolved substances are washed out from the starch fraction efficiently. For this process steps GEA offers 2-phase and 3-phase nozzle separators, each available with either flat belt or direct drive.



Nozzle Separators for Strained Yoghurt, Quark and Fresh Cheeses

GEA has developed highly flexible centrifuges for versatile soft cheese and yoghurt applications.



pilotMaster

Robust decanter for up-scaling tests, available in ATEX design and protected against erosion and corrosion.



PROFI System for Kieselguhrfree Beer Clarification

The PROFI beer filtration is a combination of high performance centrifuge and membrane filtration. It enables optimized beer filtration without kieselguhr.



Separator RSE / RSI for Oil Refining

GEA separators are used for degumming, neutralization, and dewaxing of vegetable as well as animal oils and fats. Special applications for our centrifuges in this industry are Ni-catalyst removal, lecithin deoiling, bleaching earth deoiling, re-refining of used frying fats as well as transesterification processes (e.g. for making biodiesel), epoxidized oils and mono- / diglycerides processing and others for oleochemical applications.



Separators for Animal and Fish By-Products

Rapid and clean processes, high yields and excellent product quality – our customers benefit in many ways with our machines and process lines in a very wide range of different applications



Separators for Beverages

GEA separators are used for the de-oiling of citrus juices and separating citrus oil emulsions



Separators for Biochemicals

GEA separators for biochemicals stand for utmost security of the investment, products and processes. Pre-Testing and development at own labs is possible.



Separators for Chemicals and Minerals

GEA separators for chemicals stand for utmost security of the investment, products and processes. They insure high product quality and yield fulfills international safety requirements.



Separators for Double Cream Fresh Cheese

For the production of double cream fresh cheese from fat milk of 8 to 12 percent fat content. Driven by a frequency-controlled 3-phase AC motor without clutch via a flat belt.



Separators for Industrial Fluids

For the separation of cooling lubricants, washing liquids, oil-water mixtures, lube oil, fuel oil, waste oil, etc.



Separators for Marine

Marine separators cover all capacities up to 80 m³/h for oil and water treatment.



Separators for Milk Skimming

GEA dairy separators are used for warm and cold milk separation, whey separation, buttermilk separation, cream concentration and butter oil concentration and polishing.



Separators for Oil & Gas

GEA separators for the oil & gas industry are used in various applications, e.g. dewatering and desalinating heavy crude oil, processing contaminated drilling suspensions and sludges or de-oiling bilge, drain and produced water.



Separators for Oil Recovery

Polishing separators from GEA ensure the required premium quality of olive, palm, avocado and many other recovered vegetable oils by removing all residues while handling the product with extreme care



Separators for Pharma Extraction

GEA separators for pharma extraction are designed in accordance to GMP requirements.



Separators for Power Plants

High-performance centrifuge for efficient treatment of fuel oil and lube oil in power plants



Separators for recovering plasma and meal from animal blood

GEA offers entry-level separators with smaller capacities which are easy to operate and handle for small scale blood processors, e.g. small abattoirs as well as fully automatic, high efficiency and high capacity centrifuges for full scale blood processing specialists.



Solid-Wall Bowl Separators for Chemical Products

GEA solid-wall disc-type separators are used primarily for separating liquid mixtures with no or with only minimal solid contents (less than < 0.1 % by vol.).



Solid-wall bowl separators for Marine

Manual cleaning separators with solid-wall bowl and single centripetal pump are today used mostly for the treatment of diesel oil and lube oil on smaller ships. They are suitable for clarifying or purifying oils with a low solids content of up to 0.01 percent by vol..



Solid-Wall Bowl Separators for Milk & Whey

This belt-driven solid-wall bowl separator has been designed for milk or whey skimming and milk standardizing.



Solid-Wall Bowl Separators for Pharma Extraction

GEA solid-wall disc-type separators are used for liquid-liquid extraction processes



Solid-wall bowl separators for Power Plants

The continuous treatment of lube oil with centrifugal separation technology significantly extends the service life of diesel engines and gas/ steam turbines



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- Larox: <http://www.outotec.com/en/Products--services/Process-equipment/Filters/Pressure-filters/>

Key application areas



MINING

Supporting your mining operations, from plant design expertise to equipment, parts and services for every stage of your process.



AGGREGATES

Whether you run a quarry or carry out contract crushing, we take your business personally



METALS REFINING

Cost-effective solutions for metals recovery and refining



RECYCLING

Scrap and waste processing equipment for the steel industry, scrap yards and waste handling plants. Plant solutions for renewable or conventional energy production.

Equipment



Dual Media (DM) Filter

Cost efficient, reliable and proven filter for high-capacity, polishing applications



LSF filter

Cost efficient, reliable and proven filter for high-capacity, polishing applications



Larox® PF filter

Larox® PF filters are designed for easy maintenance, superior performance, and consistent results under varying process conditions.



Larox® PF-DS filter

Flexible filter for difficult applications enabling consistent production with reduced downtime



Larox® RT filter

Safe and optimized multi-step processing in a single unit for a wide range of complex Industrial & Chemical Processing Industry applications



Larox® RT-GT filter

Safe and optimized single unit, multi-step processing for a wide range of complex Industrial & Chemical Processing Industry applications.



 Product

Tube press filter

Metso Outotec tube press technology is proven to produce drip-free cakes from concentrate with less energy.

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Driving instructions

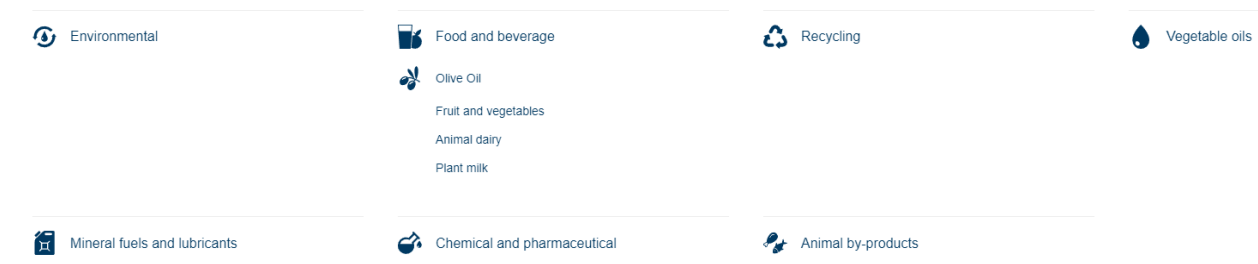
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+358 20 484 100



- Peralisi: <http://www.peralisi.com/NL>

Key application areas



Equipment

Decanter centrifuges

Centrifugal separators

Separators with manual discharge

Separators with automatic discharge

Separators with nozzles

Other components

Olive Oil Plants

Washing

Crushing

Malaxing

Extraction





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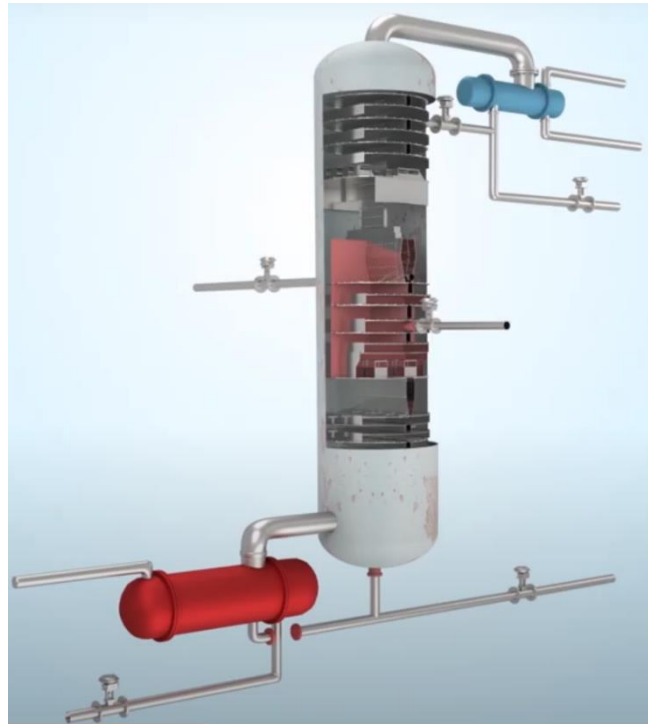
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7. BP Dividing Wall Columns

Best Practice Dividing Wall Columns



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- 7.1 Technology function
- 7.2 Application window
- 7.3 Operating window
- 7.4 Benefits and Costs
- 7.5 TRL and Risks
- 7.6 Working principle
- 7.7 References
- 7.8 Suppliers

- what does it do?
- what are known applications with which I can compare my issue?
- what temperatures / pressures / flow regimes / concentrations?
- what are the profit incentives and how does compare with cost?
- is the technology mature? Does it involve HSE- / financial risks?
- how does it work?
- where can I find more information?
- which companies sell this technology?



7.1 Technology function

A dividing wall distillation column separates mixtures into pure components. When the column contains one vertical wall it separates a three component mixture into three pure components. When the column contains more than one vertical wall it separates a multicomponent mixture into its pure components.

Dividing wall column tray

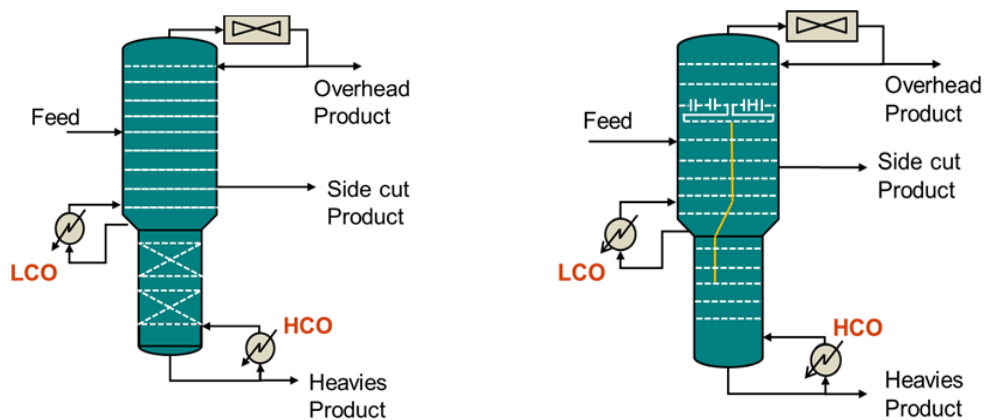


7.2 Application window

Application examples

1. Refinery: retrofit FCC unit naphtha splitter column into light naphtha, heart-cut naphtha and heavy naphtha 2018 (ref.2)

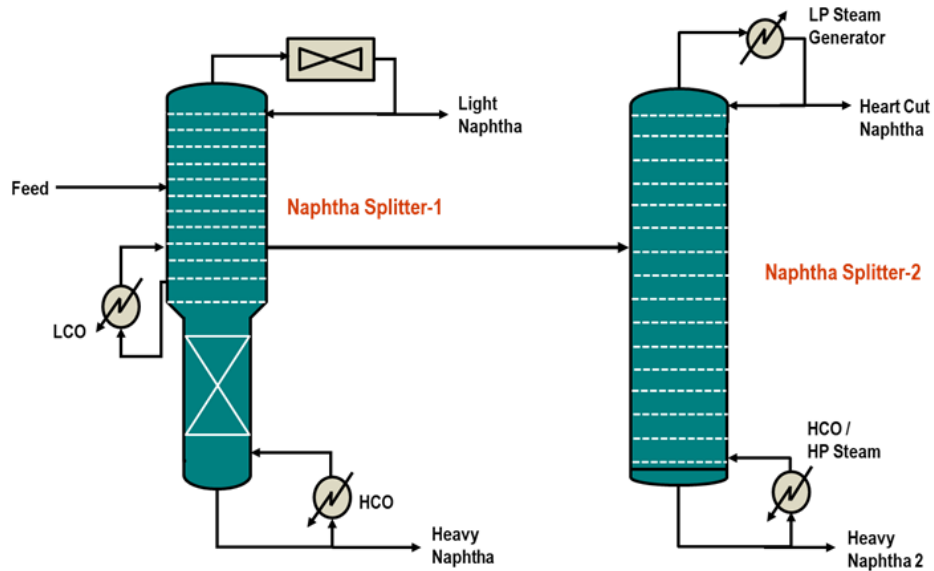
Left: old situation Right: new situation



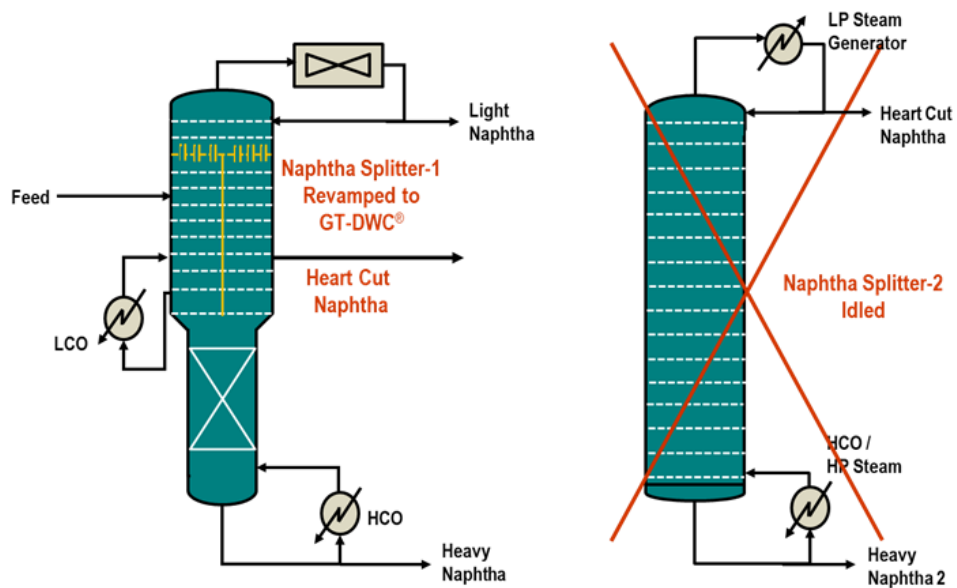


2. Refinery: naphtha splitting from two column to one column operation 2018 (ref.3)

Old situation



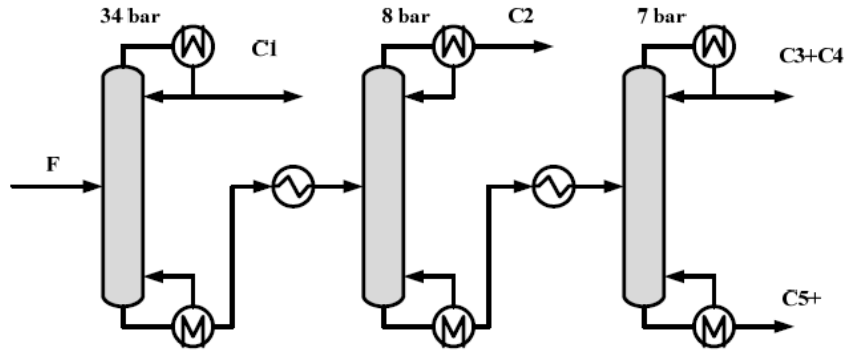
New situation



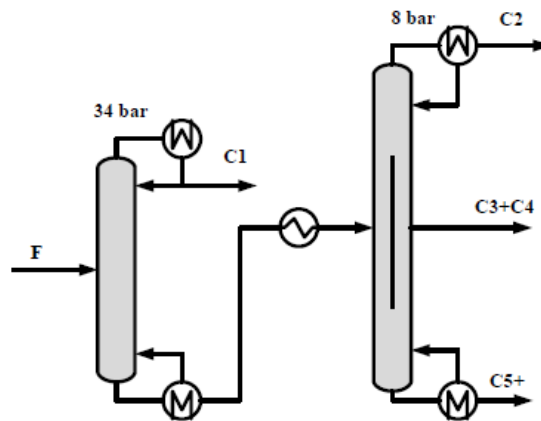


3. Natural gas liquefaction 2018 (ref.4)

Traditional line up

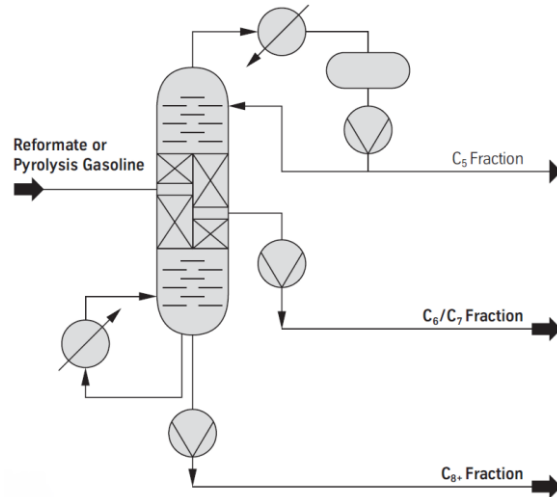


Line up with DWC replacing column 2 and 3





4. Benzene removal from gasoline 2022 (ref.5)

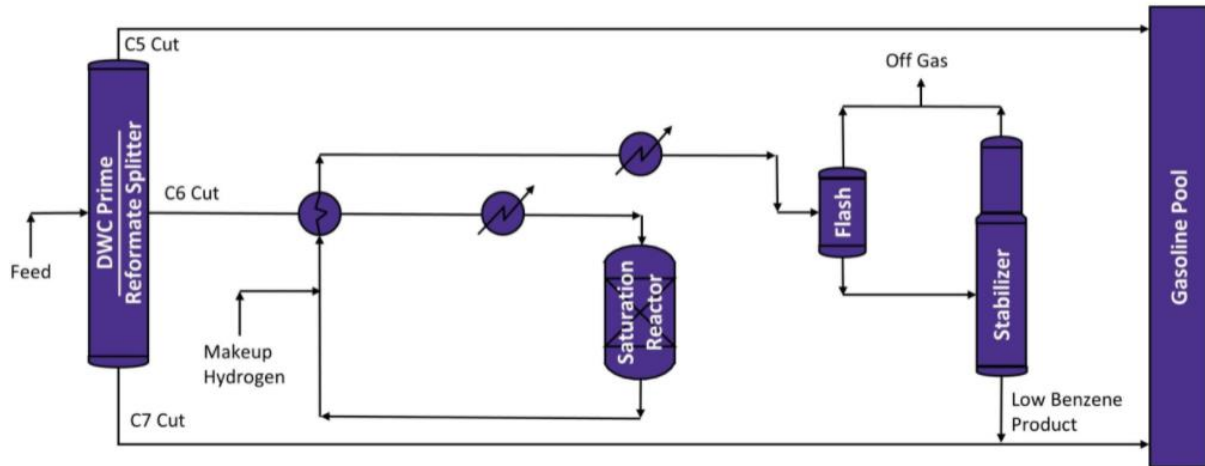


Installation of column on site

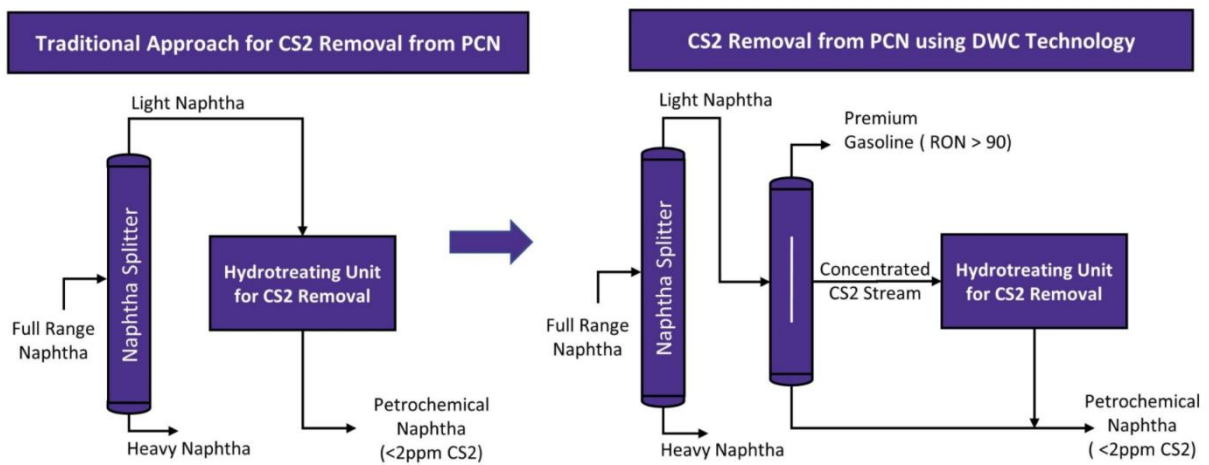




5. Concentrating benzene in a C6 cut (ref. 25)

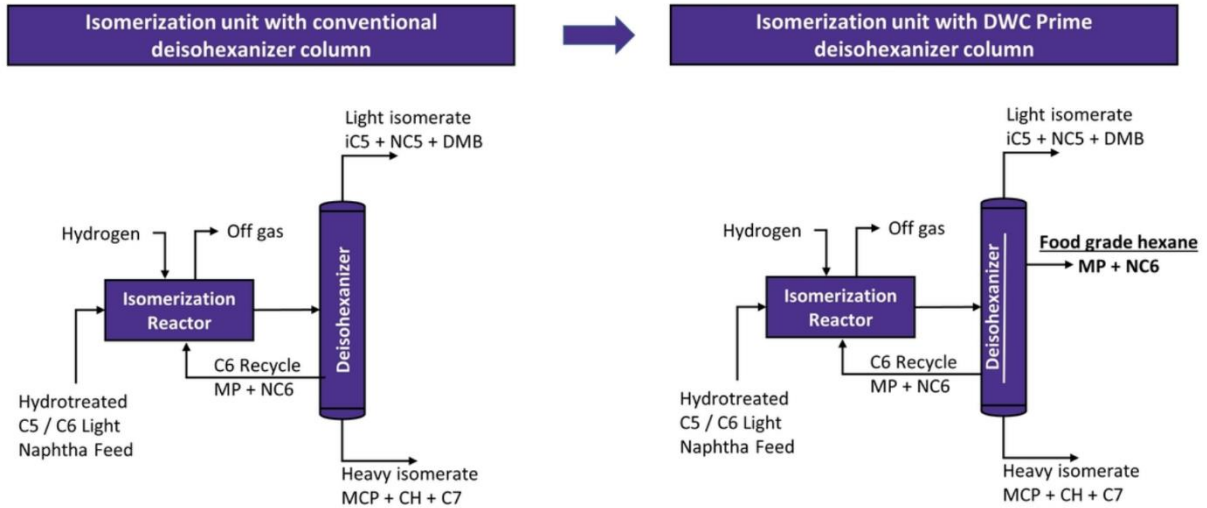


6. CS₂ removal from petrochemical naphtha (ref. 26)

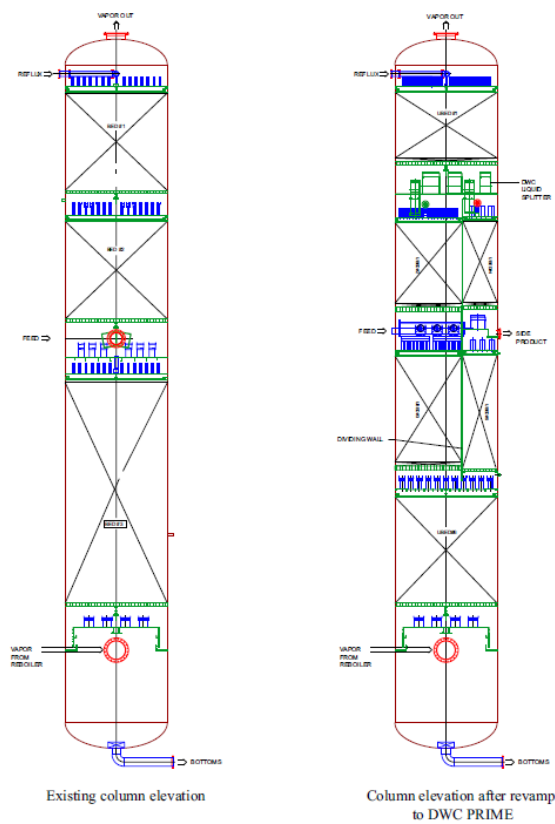




7. Boosting food grade hexane production (ref. 27)



8. Revamping a side cut packed column into a DWC to improve component purities (ref. 28)





7.3 Operating window

Since DWC's essentially are common distillation columns, their operating window in terms of pressures, temperatures, component concentrations, liquid and vapor flows resembles that of the unit operation "distillation" in general. This being said, there are a few additional limitations:

- Operation pressure variation between column sections is not possible
- The temperature difference between reboiler and condenser is higher compared to a two column set up for a three component mixture
- Column length is larger compared to two separate columns in parallel
- Modeling is generally more complex, as is design and control
- Non ideal mixtures require specific research

Next to this, DWC's have to deal with the same limitations as conventional distillation. Examples of this comprise the impact of too high bottom temperatures on product degradation, tray weeping or flooding due to too low/too high vapor flows resulting in poor separation performance, undesired pressure drops across the column, uneven liquid distribution over trays / structured packing, etc.



7.4 Benefits and Costs

- Converting two sequential columns into one by inserting a dividing wall in column one (ref.2)

Parameters	Units	Conventional Design	DWC Design
Feed Rate	t hr-1	308.0	308.0
C8/C9 (naphthenes and aromatics)	t hr-1	110.6	110.6
C8/C9 (naphthenes and aromatics) Concentration	wt.%	63.9	66.5
C8/C9 (naphthenes and aromatics)	t hr-1	105.4	108.6
C8/C9 Recovery in Heart-cut Naphtha	wt.%	95.0	98.0
Reboiler Duty (LCO)	MW	12.8 (NS-1)	14.5
Reboiler Duty (HCO)	MW	10.5 (NS-1) and 6.4 (NS-2)	21.7
Reboiler Duty (HP Steam)	MW	14.3	-
Condenser Duty	MW	23.2 (NS-1) and 19.3	37.2

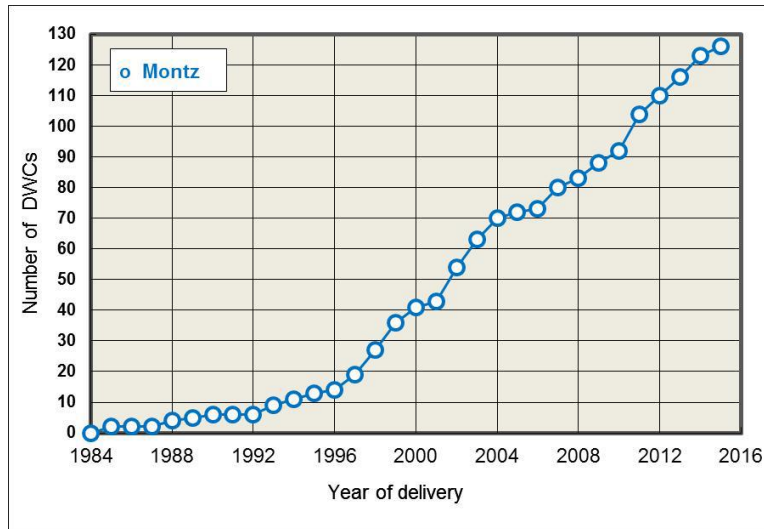
- Heating duty is reduced by approximately 25% (LCO and HCO data combined)
 - High pressure steam use in the reboiler is eliminated
 - Heart-cut naphtha is obtained in one column, resulting in an idle second column
 - Product recoveries are increased by 3.2 t/h as compared to the original design
 - Equipment modifications outside the column are avoided
- Installation of benzene removal column 160.000 ton/jr (ref.5)
 - Capacity is increased from 128.000 to 160.000 ton/yr
 - Yield is increased from 86,6% to 89,1%
 - Plotspace is reduced by 50%
 - Steam consumption is down from 0,244 t/t to 0,21 t/t
 - Benzene content in gasoline is down from 5,2 wt% to 0,76 wt%

7.5 TRL and Risks

Commercial sales of dividing wall column technology began in 1984 and reached a worldwide total of 250 columns in 2016 as is shown in graph and table below. This implies TRL=9.



Number of world-wide installed DWC's by various vendors (status May 2016) (ref.1)



Sulzer:	45
Koch-Glitsch:	30
UOP:	10
KBR:	5
UHDE:	5
Air Products:	5
Linde:	5
Sumitomo (Japan):	5
S. Korean:	5
Indian:	?
Chinese:	10

Despite DWC's well-established commercial status there are risks involved in choosing for the DWC approach. These risks concentrate on two areas:

- Design - ability
- Control - ability

Design – ability

Rigorous mathematical models, physical and chemical property databases and computer tools that simulate conventional distillation have matured over decades. Nowadays these aids often have reached a “near perfection” state of being, supplying output data with mind boggling accuracy and predictive power.

Obviously, there is a reason for this. Distillation is the most important separation technique in the process industries. Even today it is the workhorse of most companies, still beating all new kids on the block.

However, this picture slightly shifts when someone suddenly puts one or more vertical walls inside your trusted and familiar shell and tray design. Some things change and some things stay the same. Which exactly?

Dejanovic, Dimian, Bildea and Kiss came up with a practical list of heuristics to tackle these questions. First they suggest to carry out a brief analysis of your specific separation issue. Then they show steps how you can arrive at your first DWC design.



Analysis of separation issue

- Consider ternary and quaternary liquid mixtures in your process which are now separated by distillation, consider regular distillation and removal of impurities
- Analyze vapor-liquid equilibria if they are not too far from ideal
- Analyze existing operation – prepare mass and energy balances
- Make a quick design of a DWC using heuristic rules given above
- Consider profit of 30% energy reduction and potential profit for improved separation
- Check literature for data of application of the specific mixture or similar
- Check vendor documentation of Montz, Sulzer, Koch-Glitsch, etc.
- Contact consulting and design companies like Montz, Sulzer, etc.

Steps towards DWC design

- Design a conventional two-column system as a base case (e.g. in-/direct sequence)
- Take the total numbers of stages for DWC as 80% of the total number of stages required for the conventional two-column sequence: $NDWC=0.8 (N1+N2)$
- Place the partition (i.e. dividing wall) in the middle third of the column (e.g. 33–66% H)
- Set the internal flow rates in the DWC, as determined by the reboiler or condenser duty, at 70% of the total duties of two conventional columns: $QDWC=0.7 (Q1+Q2)$
- Use equalised vapour and liquid splits ($r_L=0.5, r_V=0.5$) as initial values

Control - ability

The spreading of DWC at industrial scale is still limited to only a few companies (ref.11). One of the major reasons for this status quo is the insufficient insight in operation and control of a DWC. This lack of knowledge makes most chemical companies reticent to large-scale implementation.

Many articles on the controllability of DWC's have been published between 2010-2022, a small yet relevant selection of which can be found below (ref. 7-15).

These publications clearly show, DWC's can be operated and controlled in a reliable and robust way. In view of the obvious advantages of DWC over conventional sequential distillation the best advice this Best Practice can give you is to disclose and absorb the insights and control methods of DWC's described in literature and to follow the analysis / design steps given above.

7.6 Working principle

The working principle of DWC's is identical to that of conventional distillation columns. It is based on the difference in volatility of individual components at varying pressure and temperature, leading to different liquid and vapor compositions inside the column.



7.7 References

1. EFCE Annual Meeting, Zarco Olujic, May 12th – 13th, 2016, Copenhagen, Denmark
2. Dividing Wall Column Applications in FCC Naphtha Splitter Columns, Bhargava M., Kalita, R, Gentry J.C., 2017, Hydrocarbon Processing, September, 63-66
3. Converting Two Columns into One, Bhargava M., Kalita R, Gentry J.C., 2017, PTQ Magazine, Q4, 27-29
4. Dividing wall columns for natural gas liquefaction plants, Halvorsen I.J., Dejanovic I., Olujic Ž., Skogestad S., 2018, Chemical Engineering Transactions, 69, 829-834 DOI: 10.3303/CET1869139
5. Thyssen Krupp aromatics extraction 2022 brochure: <https://www.thyssenkrupp-industrial-solutions.com/en/products-and-services/refining/aromatics-extraction>
6. High-purity DMC production by indirect alcoholysis of urea: Optimal design and control I. Patrascu, C. S. Bildea, A. A. Kiss, Computer Aided Chemical Engineering, 48, 931-936, **2020**. DOI: 10.1016/B978-0-12-823377-1.50156-7
7. Dynamics and control of a heat pump assisted azeotropic dividing-wall column (HP-A-DWC) for biobutanol purification, I. Patrascu, C. S. Bildea, A. A. Kiss, Computer Aided Chemical Engineering, 46, 1339-1344, **2019**. DOI: 10.1016/B978-0-12-818634-3.50098-9
8. Advanced Distillation Technologies: Design, Control and Applications, Anton Alexandru Kiss 12 March 2013 ISBN:9781119993612 |
9. Biobutanol purification by heat pump assisted azeotropic dividing-wall column: Dynamics and control, C. Patrut, C. S. Bildea, A. A. Kiss, Modeling, design and control of (catalytic) cyclic distillation 21st Romanian International Conference on Chemistry and Chemical Engineering, RICCE-21, 4-7 September **2019**, Constanta - Mamaia, Romania
10. Dynamics and control of a heat pump assisted extractive dividing-wall column for bioethanol dehydration, I. Patrascu, C. S. Bildea, A. A. Kiss, Chemical Engineering Research and Design, 119, 66-74, 2017. DOI: 10.1016/j.cherd.**2016**.12.021
11. A control perspective on process intensification in dividing-wall columns, Chemical Engineering and Processing: A. A. Kiss, C. S. Bildea, Process Intensification, 50, 281-292, 2011. DOI: 10.1016/j.cep.**2011**.01.011
12. Dynamic optimization of a dividing-wall column using model predictive control, R. R. Rewagad, A. A. Kiss, Chemical Engineering Science, 68, 132-142, 2012. DOI: 10.1016/j.ces.**2011**.09.022
13. Model predictive control of a dividing-wall column, A. A. Kiss, R. R. Rewagad, Studia Universitatis Babeş-Bolyai Chimia, 56(2), 5-18, **2011**.
14. Dynamics and control of a biodiesel process by reactive absorption, C. S. Bildea, A. A. Kiss Chemical Engineering Research and Design, 89, 187-196, **2011**. DOI: 10.1016/j.cherd.2010.05.007
15. Comparison of control strategies for dividing-wall columns R. C. van Diggelen, A. A. Kiss, A. W. Heemink, Industrial & Engineering Chemistry Research, 49, 288-307, **2010**. DOI: 10.1021/ie9010673
16. Dividing Wall Column as Energy Saving Retrofit Technology Helmut Jansen, Igor Dejanovic, Chem. Ing. Tech. **2016**, 88, No. 1–2, 200–207



17. Internal configurations for a multi-product dividing wall column, I.J. Halvorsena, I. Dejanovi, S. Skogestad, Z. Olujić, *chemical engineering research and design* 91 (2013) 1954–1965
18. Shortcut Method for the Design of Reactive Dividing Wall, Column Lanyi Sun and Xinxin Bi, [dx.doi.org/10.1021/ie402157x](https://doi.org/10.1021/ie402157x), *Ind. Eng. Chem. Res.* **2014**, 53, 2340–2347
19. Application of Vapor Recompression to Heterogeneous Azeotropic Dividing-Wall Distillation Columns, Li Shi, Kejin Huang, San-Jang Wang, Jieping Yu, Yang Yuan, Haisheng Chen, and David S. H. Wong, DOI: 10.1021/acs.iecr.5b02929, *Ind. Eng. Chem. Res.* **2015**, 54, 11592–11609
20. Montz Dividing Wall Column technology: <https://www.montz.de/en-gb/montz-trennwandkollonen>
21. Oral communication mr. F. Nulle, CEO of Sulzer NL – H.N. Akse of Traxxys on February 7th 2022.
22. <https://www.sulzer.com/en/products/separation-technology/structured-packings>
23. Linde Dividing Wall Column technology <https://www.linde-engineering.com/en/process-plants/petrochemical-plants/index.html>
24. <https://www.montz.de/en-gb/montz-trennwandkollonen>
25. <https://www.dwcinnovations.com/benzene-saturation/>
26. <https://www.dwcinnovations.com/cs2-removal-from-petrochemical-naphtha/>
27. <https://www.dwcinnovations.com/food-grade-hexane/>
28. <https://www.dwcinnovations.com/light-naphtha-isomerization/>
29. <https://www.digitalrefining.com/news/1004414/gtc-installs-second-dividing-wall-column-for-reliance>
30. <https://www.chemengonline.com/gtc-technology-provides-isomerization-and-dividing-wall-column-technologies-at-bpcl-refinery-in-india/>
31. Dividing wall column—A breakthrough towards sustainable distilling I. Dejanovic, Lj. Matijasevic, Z. Olujić, *Chemical Engineering and Processing: Process Intensification* Volume 49, Issue 6, June 2010, Pages 559-580
32. Reactive dividing wall columns: A comprehensive review, Jeffrey A. Weinfeld, Scott A. Owens, R. Bruce Eldridge, *Chemical Engineering and Processing - Process Intensification* Volume 123, January 2018, Pages 20-33
33. Dividing wall columns in chemical process industry: A review on current activities Omer Yildirim, Anton A. Kiss, Eugeny Y. Kenig, *Separation and Purification Technology* Volume 80, Issue 3, 18 August 2011, Pages 403-417
34. Dividing Wall Columns in Operation, Roomi Kalita, Joseph C. Gentry, *CHEMICAL ENGINEERING TRANSACTIONS*, VOL. 69, 2018
35. Sumitomo: <https://www.shi.co.jp/english/products/energy/distillation/index.html>
36. Koch-Glitsch / Montz: <https://koch-glitsch.com/>
37. DWC Innovations: <https://www.dwcinnovations.com/>
38. GTC: <https://www.sulzer.com/en/shared/services/gtc>

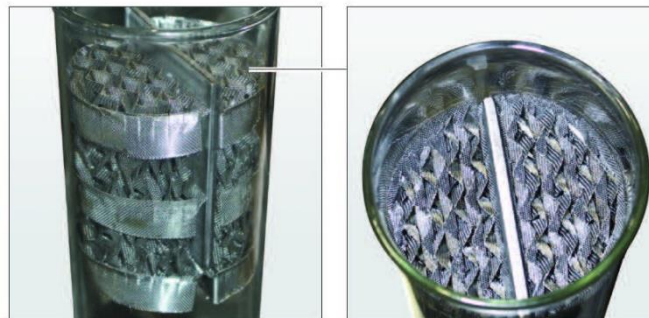


7.8 Suppliers

- Montz / Koch-Glitch (ref. 20)

Montz is part of Koch-Glitch. With Montz as one of their subsidiaries, Koch offers a broad capacity range of DWC's ranging from lab scale to full scale equipment.

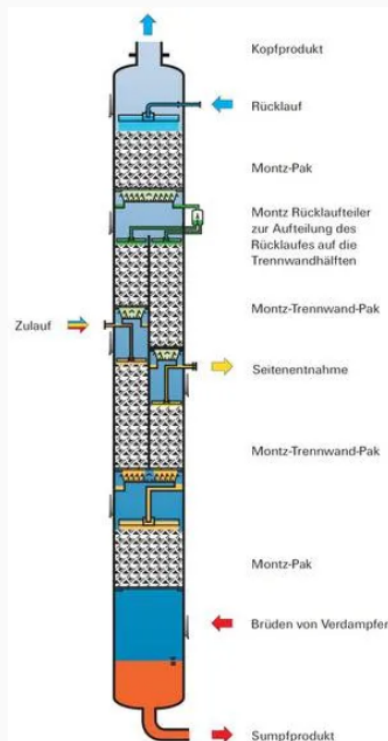
Lab scale



Full scale

Dividing wall columns

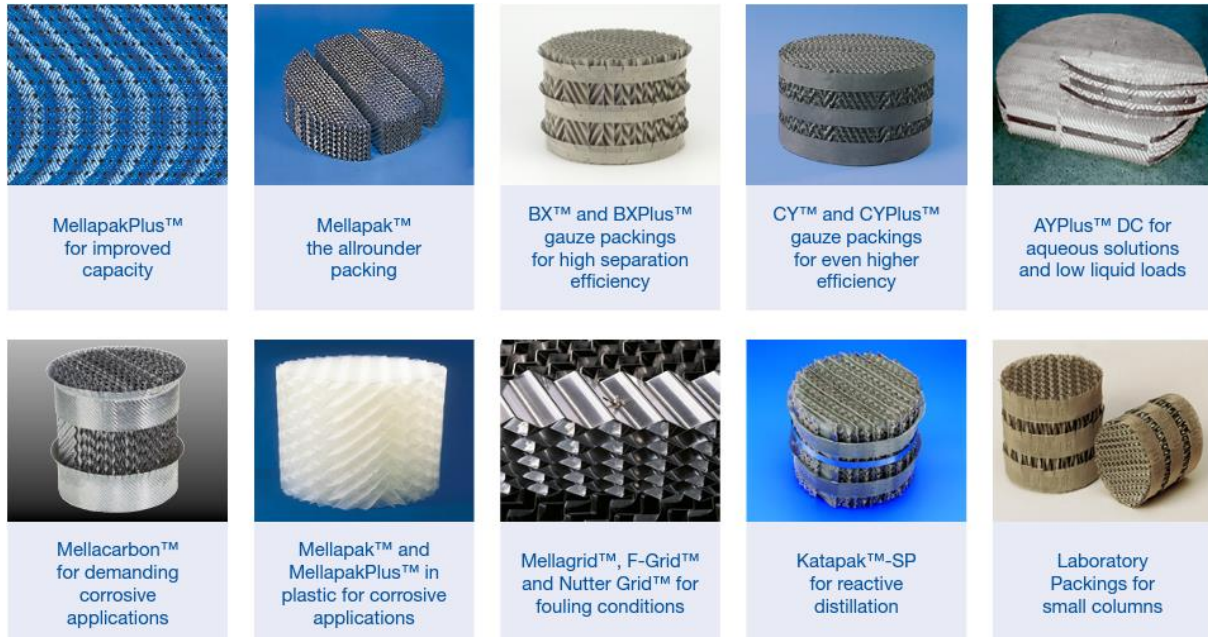
- Dividing wall columns can be used anywhere when complex mixtures are to be split into pure fractions. It is particularly advantageous for the production of pure mid-boiling fractions.
- The separation of a ternary mixture into pure constituents with conventional columns requires a sequential circuit of two columns or a configuration of main columns with side columns. Using a dividing wall column, this task can be achieved in a single distillation column.
- In dividing wall columns, a vertical wall is positioned in the center part of the column shell. The divided wall separates the feeding section from the draw-off section. The gas-tight and liquid-tight separation wall enables an energy efficient separation of low boiling and heavy boiling constituents in the feeding section working as a pre-fractionator. The draw-off section is designed for purification of the mid-boiling species.
- Such setup saves a second column for purification of the mid-boiling fraction. Column shell, internals, evaporators and condensers of a second column are not necessary. Further, the control and maintenance efforts are drastically reduced.
- Dividing wall columns are an alternative to multi-column circuits, which reduces investment and operation costs. As a rule of thumb, investment costs are reduced by minimum 20 - 30 % and operations costs by minimum 25 %.





- Sulzer (ref. 22)

Sulzer offers a wide range of column internals. When asked (ref.21) the company states it can deliver complete DWC's including internals. Sulzer positions DWC as another type of separation technology next to their conventional distillation columns with structured packing. This proves DWC has become a mature technique.



Sulzer has taken over GTC Technology (based in Houston Texas) in 2019. Before the takeover, GTC has built up a track record of successful DWC implementations. The new company is now operating under the name Sulzer GTC Technology Licensing (ref. 38).

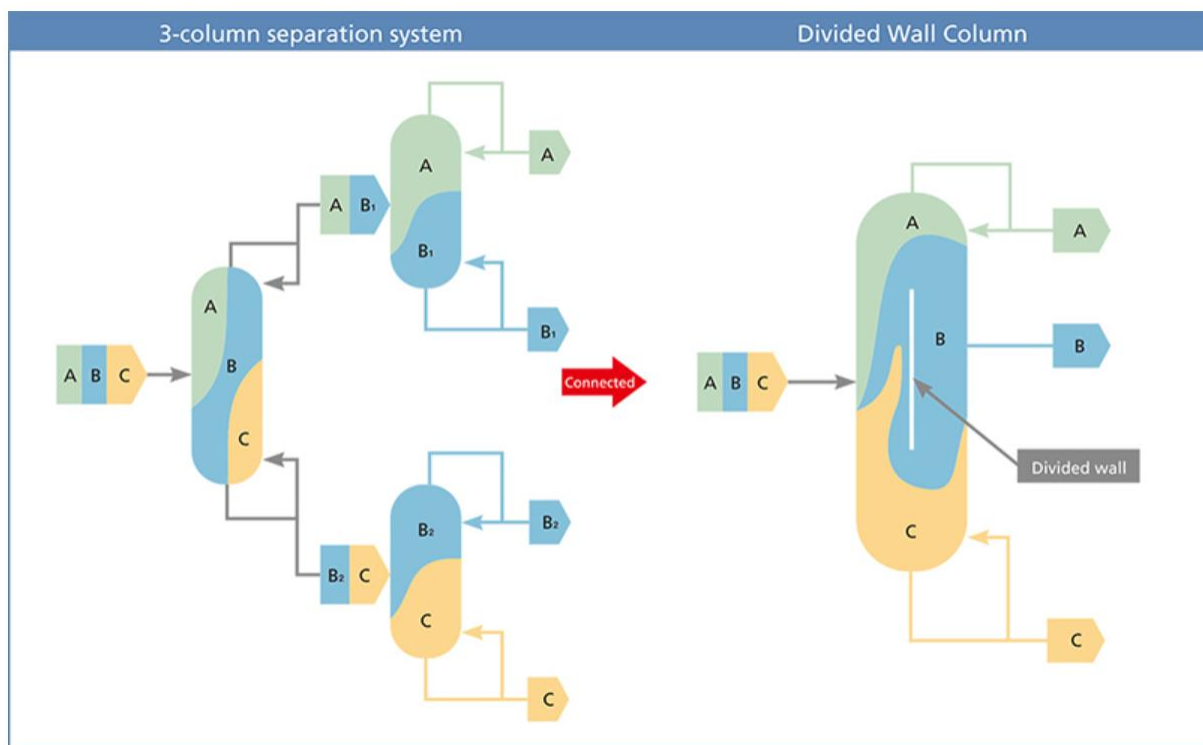


- Linde (ref.23)

The company presents Dividing Wall Columns as one of their technology propositions next to a multitude of other solutions for separation issues. Linde puts no special emphasis on DWC. This in fact proves the fact that DWC has become a mature separation technique among others.

- Sumitomo Heavy Industries (ref.35)

Sumitomo tends to describe DWC as "Column in column" technology.





- Koch-Glitsch / Montz (ref. 36)

Koch-Glitsch owns Montz. With Montz as one of their subsidiaries, Koch offers a broad capacity range of DWC's ranging from lab-scale to full scale equipment (See Montz).

- DWC Innovations (ref. 37)

DWC (Houston, Texas) is an independent company that has gained considerable momentum and growth in the area of DWC over the past 7 years. Their track record shows they offer DWC-solutions for complex multicomponent separations.

